Table 1. Transmissivity and storage coefficients from aquifer pumping tests.

[Reference citations in the remarks column were created by outside sources, and although an attempt was made to locate the complete references, not all were found. Thus, some citations do not have corresponding entries in the references cited section of this report. Results shown here are for wells that have open intervals at least 30 feet in length. The remarks field from the original database is provided with no editing for consistency or content. ID, identifier; gpd, gallon per day; gpm, gallon per minute; ft, foot; ft2, square foot; mg/L, milligrams per liter; TDS, total dissolved solids; NAD27, North American Datum of 1927; NAD83, North American Datum of 1983; WGS84, World Geodetic System 1984; AL, Alabama, FL, Florida; GA, Georgia; SC, South Carolina; FAS, Floridan aquifer system; IA, intermediate aquifer system; LFA, Lower Floridan aquifer, MCU, middle confining unit; SCP Southeastern Coastal Plain aquifer; UFA, Upper Floridan aquifer]

Unique ID	Latitude (decimal degrees)	Longitude (decimal degrees)	Horizontal datum	State	County	Transmissivity (square feet per day)	Storage coefficient (dimensionless)	Remarks	Open interval (feet below land surface)		Hydrologic unit tested
									Top	Bottom	
usgs162	32.13833	-85.72194	unk	AL	BULLOCK	590			968	1278	SCP
gsa001	31.10222	-87.08333	NAD27	AL	ESCAMBIA	3,400	0.000009	Average of two obs wells O-141 T=27750 gpd/ft S= 7.85e-6 O-147 T=23000 gpd/ft S=1.04e-5 drawdown analyzed		731	FAS
gsa002	31.08090	-87.09970	WGS84	AL	ESCAMBIA	1,700		Single well test recovery analysis, Specific capacity mentions in report as 4.3 gpm/ft. This well is not in NWIS location determined from map in report and google maps.		485	FAS
usgs266	31.12270	-86.04890	NAD83	AL	GENEVA	400		loc .7 mile north of Main St on Broad St from Google map, analysis Cooper-Jacob 1963 pumping and recovery analyzed for same result (Eve Kuniansky analyzed-Rod Sheets approved).	300	519	FAS
usgs173	31.62500	-85.06361	unk	AL	HENRY	6,700	0.00311				SCP
usgs181	31.25962	-85.11021	NAD27	AL	HOUSTON	130	0.0001		132	137	LFA
usgs182	31.25934	-85.10993	NAD27	AL	HOUSTON	128	0.0004		136	141	LFA
usgs248	29.76083	-82.38889	unk	FL	ALACHUA	25,000		SRWMD files in Live Oak	184	500	FAS
sjrwmd029	29.68500	-82.28750	unk	FL	ALACHUA	23,835		Cooper-Jacob	205	608	FAS
usgs249	29.65972	-82.62806	unk	FL	ALACHUA	24,987		SRWMD files in Live Oak	77	117	UFA
sjrwmd001	30.29806	-82.08611	unk	FL	BAKER	15,000	0.04	S= 0.08 if recovery data used, T=14000 ft2/day, S=0.01 for observation well.	480	650	UFA
nwfwmd088	30.27211	-85.69974	NAD83	FL	BAY	4,000	0.0003	Latitude and longitude based on center of reported township, range, and section.	100	307	FAS
nwfwmd006	30.40773	-85.76351	unk	FL	BAY	48,000		No construction information given. Lat/long picked from Google Earth.			FAS
nwfwmd001	30.31083	-85.62817	unk	FL	BAY	13,333	0.00042	mccall sod farm apt well-1_nwfid_975.pdf	280	614	FAS
nwfwmd004	30.43946	-85.81786	unk	FL	BAY	4,600		Flow meter test shows 90% of flow coming from Suwannee at 205-300. Remaining 10% from 520-570 in LFA. Interval depths from table 2.2.	485	675	LFA

nwfwmd005	30.39131	-85.82475	unk	FL	BAY	660,000		Major water-producing interval (carbonate permeable zone) was 320-398. Modeled transmissivity zone is a 3.2 mile radius centered on the well, and is in contact with a regional transmissivity zone of 43000 ft2/d.	292	495	UFA
nwfwmd003	30.43946	-85.81786	unk	FL	BAY	41,000		Flow meter test shows 90% of flow coming from Suwannee at 205-300. Remaining 10% from 520-570 in LFA. Interval depths from table 2.2.	170	380	UFA
sjrwmd258	28.15833	-80.72500	unk	FL	BREVARD	38,786	0.000795	average Jacob-straight line and Neuman and Witherspoon	245	850	FAS
sjrwmd172	28.14944	-80.73222	unk	FL	BREVARD	9,108	0.0007	average Neuman and Witherspoon and Jacob-straight line (geometric mean values). Transmissivity value appears to be in gpd/ft.	450	950	FAS
sjrwmd031	27.94861	-80.66750	unk	FL	BREVARD	71,693	0.000413	average Cooper-Jacob time drawdown and Walton	350	850	FAS
sfwmd374	28.15029	-80.73299	unk	FL	BREVARD	45,392	0.000637	TRANS AND STORATIVITY VALUES ARE MEANS FROM MONITOR WELLS. NO UNITS FOR LEAKANCE WERE GIVEN IN REPORT. TRANSMISSIVITY REPORTED IN GPD/FT (339552.85). LEAKANCE GIVEN HERE IN UNITS OF PER DAY	240	864	FAS
sfwmd375	28.01797	-80.59922	unk	FL	BREVARD	23,306	0.00015		298	370	UFA
sfwmd373	28.15029	-80.73299	unk	FL	BREVARD	34,577	0.00118	PARAMETER VALUES ARE MEANS FROM MONITORING WELLS. SEE ANALYSIS INFO FOR INDIVIDUAL DATA. IN ANALYSIS INFO, IN STATION BR-0916 RECOVERY METHOD, THE TRANS VALUE IS MEAN OF 197000 TO 394000.	240	550	UFA
sjrwmd261	27.99167	-80.54166	unk	FL	BREVARD	24,614	0.00137	Type-curve solutions or non-steady state flow within a confined aquifer (Lohman 1979)	305	412	UFA
sjrwmd246	28.77463	-80.92783	unk	FL	BREVARD	7,533	0.00021	average Cooper and Jacob (1946) drawdown and Theis and Jacob recovery	108	210	UFA
sjrwmd259	27.89167	-80.69166	unk	FL	BREVARD	170,230		Type-curve matching	240	525	UFA
sfwmd401	26.17349	-80.17852	unk	FL	BROWARD	9,044	0.00005	CROSS WELL TOMOGRAPHY WAS ALSO CONDUCTED BY U OF M (TOKUO YAMAMOTO) AT THIS SITE TO MEASURE PERMEABILITY BETWEEN WELLS. REPORT PREPARED FOR THE DISTRICT AND PUBLISHED SEP 8, 1997. 4 WELLS CONTRUCTED HERE. 3 EAST OF THE S36 CAGE AND 1 WEST. TWO PRODUCTION	1500	1600	MCU
sfwmd395	26.17620	-80.26088	unk	FL	BROWARD	5,827		ACIDIZATION OF WELL DONE AFTER STEP TEST AND BEFORE CONSTANT RATE TEST. INTERPRETATION OF RECOVERY DATA FAVORED LATE TIME DATA. ANAYLZED USING JACOB STRAIGHT LINE METHOD (1944), IGNORED LEAKANCE.	1110	1270	UFA
sfwmd393	26.17536	-80.15394	unk	FL	BROWARD	19,500			1055	1200	UFA

sfwmd392	25.96971	-80.32654	unk	FL	BROWARD	5,214	0.00001	Trans is average from two analysisSPECIFIC CAPACITY = 1.1 GPM/FT	1050	1350	UFA
sfwmd386	26.31619	-80.12366	unk	FL	BROWARD	24,390	0.00017	SFWMD FUNDED CONSTRUCTION OF THE 2ND FLORIDAN 6 INCH MONITOR WELL ,BF-6, ON SITE. CUTTINGS WERE COLLECTED AND DESCRIBED BY SFWMD & FGS. CITY OF DEERFIELD BCH FUNDED THE INITIAL RO TEST/PRODUCTION WELL. FAS WQ DATA AVAILABLE IN CDM REPORT. L	960	1128	UFA
sfwmd387	26.29342	-80.10671	unk	FL	BROWARD	5,041	0.000053	WALTON METHOD SHOULD GIVE SAME TRANSMISSIVITY IF NO LEAKANCE AS C-J METHOD (?), CURVE MATCHES LOOK OKAY. RECOMMENDED T VALUE DETERMINED WITH C-J METHOD.	995	1200	UFA
sfwmd384	26.01409	-80.17721	unk	FL	BROWARD	24,390	0.0003		930	1314	UFA
sfwmd170	26.33407	-80.22233	unk	FL	BROWARD	19,241		INCREMENTAL PUMPING RATES OF APPROXIMATELY 1800 GPM, 3000 GPM AND 3400GPM WERE UTILIZED FOR THE PUMPING TEST. WATER LEVELS WERE MEASURED IN THE WELL DURING EACH PUMPING RATE FOR APPROX. 1 HOUR THEN THE RATE WAS INCREASED TO THE NEXT PUMPING RATE. THE FINA	1010	1225	UFA
sfwmd391	26.17314	-80.17921	unk	FL	BROWARD	16,206	0.00037	TWO ATTEMPTS AT THIS APT, THE FIRST ONE WAS CONDUCTED IN 1993 AND FAILED 12 HOURS AFTER PUMPING BEGAN BECAUSE OF SEDIMENT LOAD UP IN THE WELL. THIS SECOND ONE CONDUCTED 4 YEARS LATER. ALSO AVAILABLE ON THIS SITE IS A CROSSWELL TOMPOGRAPHY EXPERIMENT BY	1000	1200	UFA
sfwmd385	26.31619	-80.12366	unk	FL	BROWARD	24,200	0.00000133		956	1130	UFA
nwfwmd007	30.42000	-85.30400	unk	FL	CALHOUN	7,300	0.000161		264	703	UFA
sfwmd026	26.98886	-81.63504	unk	FL	CHARLOTTE	8,808			78	533	IA
sfwmd027	26.94478	-81.80786	unk	FL	CHARLOTTE	1,390	0.0021	APT PARAMETERS REPRESENT THE AVERAGE OF THREE ANALYTICAL METHODS.	130	230	IA
sfwmd030	26.94478	-81.80786	unk	FL	CHARLOTTE	2,970		NO OBSERVATION WELL WAS AVAILABLE AT THE SITE FOR THIS APT.	450	600	IA
sfwmd034	26.86190	-81.72408	unk	FL	CHARLOTTE	3,700	0.00135	THE TEST WAS STOPPED PREMATURELY BY AN UNKNOWN PERSON WHO TURNED OFF THE PUMP. HOWEVER THE DATA COLLECTED WERE USEABLE	566	942	UFA
sfwmd007	27.01645	-82.25676	NAD27	FL	CHARLOTTE	8,900		Test #2. Value reported in CH2M Hill report is 108,000 gpd/ft (14,438 ft2/d). No observable effects on Warm Mineral Springs.	560	1100	UFA
sfwmd031	26.82568	-81.70848	unk	FL	CHARLOTTE	10,827	0.000156		500	620	UFA
sfwmd033	26.90450	-82.26760	unk	FL	CHARLOTTE	61		MULTIWELL AQUIFER TEST PLANNED IN THE FUTURE	563	583	UFA

sfwmd275	27.01583	-82.25722	unk	FL	CHARLOTTE	374,661		TRANSMISSIVITY ESTIMATED BY JACOB STRAIGHT LINE METHOD USING RECOVERY	1105	1150	UFA
sfwmd273	27.01583	-82.25722	unk	FL	CHARLOTTE	262,872		TRANSMISSIVITY ESTIMATED BY JACOB STRAIGHT LINE METHOD	1100	1150	UFA
swfwmd247	27.01150	-81.80100	unk	FL	CHARLOTTE	5,080	0.0023	No data available; vert. K = 0.0025 ft/day.	604	840	UFA
swfwmd090	27.01583	-82.25722	unk	FL	CHARLOTTE	135,000	0.0015	Test results affected by density stratification in borehole; S value represents entire system; best T value estimated from pumped well; nearby recharge boundaries (fractures) present.	560	1600	UFA
swfwmd140	26.93810	-81.80120	unk	FL	CHARLOTTE	2,610	0.408	Parameters represent avg. of 3 analytical methods; no data corrections applied; Intermediate aquifer monitor well declined 0.7' during APT drawdown & recovered to static levels @ end of recovery test.	720	970	UFA
swfwmd005	28.95450	-82.62890	unk	FL	CITRUS	210,480	0.05	Partially penetrating; T represents log. avg. from flow-net analysis of several specific capacity tests; multizoned well drilled to 476' encountered evaporites; S value could not be confirmed.	35	200	UFA
swfwmd182	28.74530	-82.54400	unk	FL	CITRUS	38,102	0.008	Partially penetrating; questionable leakance value obtained; Walton's 1970 analytical methods used (leaky aquifer distance-drawdown).	158	250	UFA
swfwmd013	28.88500	-82.44260	unk	FL	CITRUS	2,751,203		Data obtained from pumped well only; regional & barometric effects accounted for; 9' cavity near bottom of well; extremely high T value.	220	422	UFA
swfwmd063	28.88370	-82.59550	unk	FL	CITRUS	200,535		Partially penetrating; extremely high leakance value indicates direct connectivity of Floridan w/ surficial aquifer; regional trends corrected.	62	172	UFA
sjrwmd036	30.17805	-81.80583	unk	FL	CLAY	37,437	0.0008	leaky aquifer	460	1000	FAS
sjrwmd033	30.11580	-81.77593	NAD27	FL	CLAY	87,000		Jacob straight-line drawdown	391	1197	FAS
sjrwmd035	30.17805	-81.80583	unk	FL	CLAY	35,998	0.0008	Cooper-Jacob	460	1000	FAS
sjrwmd037	30.05833	-81.85416	unk	FL	CLAY	29,664	0.002735	Average of Cooper-Jacob, Hantush, and Theis&Jacob	378	1000	FAS
sjrwmd038	30.12916	-81.78472	unk	FL	CLAY	41,613	0.00025	Average of Cooper-Jacob, Hantush, and Theis & Jacob	400	1000	FAS
sjrwmd039	29.99639	-81.73527	unk	FL	CLAY	12,011		Coopy Jacob Straight Line	440	1000	FAS
sjrwmd040	29.99555	-81.73611	unk	FL	CLAY	9,149	0.000225	Average of Theis and Hantush	440	1000	FAS
sjrwmd308	29.74916	-82.00722	unk	FL	CLAY	80,743	0.00021		683	950	FAS
sjrwmd041	30.10750	-81.83889	unk	FL	CLAY	19,918		Theis & Jacob Recovery	432	1002	FAS
sjrwmd034	30.07361	-81.70389	unk	FL	CLAY	30,880	0.0002	Updated lat/long based on Google Earth	419	1000	FAS
sjrwmd110	29.86247	-81.62120	NAD27	FL	CLAY	7,800		Jacob straight-line recovery	260	340	UFA
sfwmd562	26.24306	-81.78806	unk	FL	COLLIER	2,304		COOPER JACOB (1946) MODIFICATION OF THEIS (1935) ANALYSIS METHOD SPECIFIC CAPACITY: 7.3 GPM/FT		421	IA
sfwmd492	25.89362	-81.30919	unk	FL	COLLIER	68,022	0.000068	BASED ON THE MOENCH ANALYTICAL MODEL.	465	550	IA

sfwmd490	26.24434	-81.67881	unk	FL	COLLIER	2,805	0.000484	PARAMETER VALUES DETERMINED FROM AVERAGE OF COOPER '63 AND JACOB '50 VALUES. LEAKANCE FROM COOPER ONLY. * IN ANALYSIS INFO, METHOD IS LISTED AS OTHER IS COOPER 1963 AND THAT LISTED AS UNKNOWN IS JACOB 1950.	398	514	IA
sfwmd489	26.28750	-81.58694	unk	FL	COLLIER	2,406	0.00007	The date of the APT test is the year of the report.	350	420	IA
sfwmd487	26.24050	-81.80858	unk	FL	COLLIER	8,943	0.0002		315	371	IA
sfwmd485	26.17339	-81.65671	unk	FL	COLLIER	13,099	0.000153	PARAMETER VALUES TAKEN FROM AVERAGE OF CURVE MATCHING METHOD OF DRAWDOWN, STRAIGHT LINE OF DRAWDOWN AND RECOVERY AT MON. WELL MC-5056.	299	399	IA
sfwmd484	26.06509	-81.69230	unk	FL	COLLIER	42,400		ESTIMATED TRANSMISSIVITY IN LOWER HAWTHORN ZONE I (550 TO 622 FEET) WAS TOO LOW FOR CONSIDERATION AS AN ASR INTERVAL. NO DATES REPORTED FOR ANY TESTS. GOOD AGREEMENT BETWEEN TESTS.	296	399	IA
sfwmd483	26.06509	-81.69230	unk	FL	COLLIER	67,000		ESTIMATED TRANSMISSIVITY IN LOWER HAWTHORN ZONE I (550 TO 622 FEET) WAS TOO LOW FOR CONSIDERATION AS AN ASR INTERVAL. NO DATES REPORTED FOR ANY TESTS. GOOD AGREEMENT BETWEEN TESTS.	296	399	IA
sfwmd482	26.19246	-81.68618	unk	FL	COLLIER	5,971	0.0000833	PARAMETER VALUES TAKEN FROM CURVE MATCHING METHOD OF DRAWDOWN, STRAIGHT LINE METHOD OF DRAWDOWN AND RECOVERY AT MON. WELL MC-5069.	296	420	IA
sfwmd481	26.16449	-81.68471	unk	FL	COLLIER	13,144	0.000217	TRANS, STORATIVITY AND LEAKANCE AVERAGED FROM DATA FROM TWO MONITOR WELLS - C-1103 (CO-2081) AND MC-5054 (HZ1-MW1). VALUES FROM CURVE MATCHING METHOD OF DRAWDOWN, STRAIGHT LINE METHOD OF DRAWDOWN AND RECOVERY.	295	400	IA
sfwmd479	25.86278	-81.01056	unk	FL	COLLIER	180		1. DATE IS YEAR OF PUBLICATION 2. SINGLE WELL TEST WITH THEIS (1935) RECOVERY SOLUTION 3. CONDUCTIVITY IS ESTIMATED USING FULL THICKNESS OF AQUIFER 4. STORATIVITY IS RATIO OF STORATIVITY DURING DRAWDOWN TO THAT OF RECOVERY	120	130	IA

sfwmd480	25.86278	-81.01056	unk	FL	COLLIER	1,500		1. DATE IS YEAR OF PUBLICATION 2. SINGLE WELL TEST WITH THEIS (1935) RECOVERY SOLUTION 3. CONDUCTIVITY IS ESTIMATED USING FULL THICKNESS OF AQUIFER 4. STORATIVITY IS RATIO OF STORATIVITY DURING DRAWDOWN TO THAT OF RECOVERY	180	200	IA
sfwmd488	26.28204	-81.75371	unk	FL	COLLIER	8,422		The date of the APT test is the year of the report.	322	833	IA-UFA
sfwmd508	25.89362	-81.30919	unk	FL	COLLIER	11,209	0.000005	LEAKANCE WAS FOUND TO BE EVENLY DISTRIBUTED BETWEEN THE UPPER AND LOWER CONFININING UNITS. T & S VALUES CALCULATED USING THE MOENCH SOLUTION.	840	1010	UFA
sfwmd493	26.04676	-81.69453	unk	FL	COLLIER	9,400	0.0001	FOR THE MULTIWELL TEST, 670 GALLONS PER MINUTE WAS AN INJECTION RATE.	465	528	UFA
sfwmd494	26.04676	-81.69453	unk	FL	COLLIER	12,000		FOR THE MULTIWELL TEST, 670 GALLONS PER MINUTE WAS AN INJECTION RATE.	465	528	UFA
sfwmd496	26.17339	-81.65600	unk	FL	COLLIER	35,230		SINGLE WELL RECOVERY TEST. PARAMETER VALUES DETERMINED BY STRAIGHT LINE METHOD OF RECOVERY.	635	760	UFA
sfwmd497	26.19097	-81.68626	unk	FL	COLLIER	1,369		SINGLE WELL RECOVERY TEST. PARAMETER VALUES DETERMINED BY STRAIGHT LINE METHOD OF RECOVERY.	640	810	UFA
sfwmd498	26.16772	-81.68498	unk	FL	COLLIER	3,062	0.000085	PARAMETER VALUES TAKEN FROM CURVE MATCHING METHOD OF DRAWDOWN, STRAIGHT LINE METHOD OF DRAWDOWN AND RECOVERY AT MON. WELL MC-5067.	650	762	UFA
sfwmd500	26.17081	-81.73058	unk	FL	COLLIER	15,772	0.00001664	THE MOENCH ANALYTICAL MODEL WAS USED TO ANALYZE DATA W-17405 = I75-TW	690	780	UFA
sfwmd502	26.06694	-81.69445	unk	FL	COLLIER	10,860	0.000039	"TRANSMISSIVITY (T) WAS CALCULATED USING DISTANCE DRAWDOWN CURVES GENERATED FROM PUMP TEST DATA BY THE ANALYSIS TECHNIQUES DESCRIBED BY DRICOLL (1986)."	730	780	UFA
sfwmd503	26.06889	-81.69361	unk	FL	COLLIER	8,743		DISCHARGE RATE AVERAGE OF: 600 GPM, 790 GPM, AND 1,120 GPM.	735	780	UFA
sfwmd504	26.06509	-81.69230	unk	FL	COLLIER	54,612		The date of the APT test is the year of the report. Several Methods	745	817	UFA
sfwmd505	26.06509	-81.69230	unk	FL	COLLIER	8,200		ESTIMATED TRANSMISSIVITY IN LOWER HAWTHORN ZONE I (550 TO 622 FEET) WAS TOO LOW FOR CONSIDERATION AS AN ASR INTERVAL. NO DATES REPORTED FOR ANY TESTS. GOOD AGREEMENT BETWEEN TESTS.	745	811	UFA

sfwmd501	26.24469	-81.67881	unk	FL	COLLIER	379,404	0.0000215	PARAMETER VALUES DETERMINED FROM AVERAGE OF 2 MON. WELLS, MC-5000 AND MC-5007 USING COOPER 1963 JACOB 1950 METHODS. * LATE STORATIVITY (JACOB '50) FOR MC-5000 IS 0.043 AND FOR MC-5007 IS 0.11 IN ANALYSIS INFO, METHOD LISTED AS OTHER IS COOPER 1963 AND THA	700	800	UFA
sfwmd507	26.06750	-81.69333	unk	FL	COLLIER	2,146		PUMP RATES FOR FOUR STEPS: 250 GPM, 512 GPM, 667 GPM, 848 = DISCHARGE RATE TRANSMISSIVITY BASED ON SPECIFIC CAPACITY VALUES: 14.8 GPM/FT AT 255 GPM, 12.9 GPM/FT AT 542 GPM, 11.3 GPM/FT AT 656 GPM, 11.7 GPM/FT AT 828 GPM	746	775	UFA
sfwmd509	26.17081	-81.73058	unk	FL	COLLIER	7,114	0.000023	THE MOENCH ANALYTICAL MODEL WAS USED TO ANALYZE DATA W-17405 = I75-TW	890	1050	UFA
sfwmd514	26.41344	-81.43152	unk	FL	COLLIER	36,314	0.01	THE MOENCH ANALYTICAL MODEL WAS USED TO ANALYZE DATA W-17391 = IWSD-TW TEST IS PARTIALLY PENETRATING OF THE UPPER FAS, OMITTING THE LOWER HAWTHORN PRODUCING ZONE	1050	1160	UFA
sfwmd506	26.06592	-81.69314	unk	FL	COLLIER	9,100	0.000065	ESTIMATED TRANSMISSIVITY IN LOWER HAWTHORN ZONE I (550 TO 622 FEET) WAS TOO LOW FOR CONSIDERATION AS AN ASR INTERVAL. NO DATES REPORTED FOR ANY TESTS. GOOD AGREEMENT BETWEEN TESTS.	745	790	UFA
sjrwmd111	30.18579	-82.62318	NAD27	FL	COLUMBIA	36,000	0.0008	Theis type-curve solution	157	275	UFA
sjrwmd112	30.32606	-82.58457	NAD27	FL	COLUMBIA	33,000	0.00007	Average of Hantush and Jacob method and Neuman and Witherspoon method	160	262	UFA
usgs246	29.92619	-82.71603	unk	FL	COLUMBIA	30,000		SRWMD files in Live Oak	82	147	UFA
sfwmd564	25.70038	-80.47478	NAD27	FL	DADE	15,400	0.0003625	**RECOMMENDED PARAMETER AVERAGE OF WALTON METHOD FOR BOTH OBSERVATION WELLS. All three ASR wells heavily acidized prior to all tests. Late time drawdown data problematic becauase of pump going down several times.	850	1302	FAS
sfwmd579	25.91732	-80.47589	unk	FL	DADE	4,298	0.0000903	DISCHARGE RATE RANGED FROM 76 - 110 GPM BUT HELD RELATIVELY CONSTANT AT 100 GPM. SPECIFIC CAPACITY = 32 GPM/FT	1700	1800	MCU
sfwmd577	25.90927	-80.46920	unk	FL	DADE	7,220	0.0013	DISCHARGE RATE RANGED FROM 420 - 510 GPM BUT HELD RELATIVELY CONSTANT AT 435 GPM ANLAYSIS METHOD IS MOENCH, 1985. SPECIFIC CAPACITY = 140 GPM/FT	1140	1230	UFA

usgs011	25.35483	-80.43033	NAD83	FL	DADE	31,000		USGS files (Miami, FL). Thickness of aquifer tested, 230 ft.			UFA
usgs010	25.83033	-80.30217	NAD83	FL	DADE	12,000		USGS files (Miami, FL). Thickness of aquifer tested, 150 ft.			UFA
sfwmd571	25.82927	-80.28811	unk	FL	DADE	11,000	0.000084	TRANSMISSIVITY ESTIMATE FROM MEYER (1989B). STORAGE COEFFICIENT ESTIMATED BY MODEL SIMULATION OF PUMPING TEST. ANALYSIS METHOD JACOB & LOHMAN (1952).	953	1060	UFA
sfwmd572	25.94953	-80.21646	unk	FL	DADE	21,859	0.00014	AQUIFER PARAMETERS WERE CALCULATED USING AVERAGE OF DRAWDOWN AND RECOVERY VALUES.	1000	1231	UFA
sfwmd573	25.43952	-80.33816	unk	FL	DADE	33,062	0.0002	AVERAGE OF RESULTS FROM HANTUSH-JACOB, LEAKY CONFINED AQUIFER SOLUTION. TIDAL EFFECTS NEGLIGIBLE.	1003	1242	UFA
sfwmd574	25.95083	-80.21500	unk	FL	DADE	20,804	0.00016	OBSERVATION WELLS: NMB-1F, MAX DRAWDOWN 13 FT, RADIAL DISTANCE = 475 FT NMB-2F, MAX DRAWDOWN 17 FT, RADIAL DISTANCE = 686 FT NMB-3F, MAX DRAWDOWN 12.5 FT, RADIAL DISTANCE = 950 FT	1020	1250	UFA
sfwmd576	25.35234	-80.40977	unk	FL	DADE	67,751	0.005	VERY LONG-TERM (90 DAY) TEST. BAROMETRIC EFF. EST. = 100%. GRAPHICAL PLOTS OF DRAWDOWN VS TIME INDICATED THAT DESPITE THE VERY LONG DURATION OF THE TEST FULL EQUILIBRIUM HAD NOT BEEN REACHED. RECOMMENDED VALUES BASED ON DRAWDOWNS FROM THE FURTHEST OBSE	1120	1350	UFA
sfwmd563	25.70038	-80.47478	unk	FL	DADE	13,978	0.000711	CONSTANT RATE PUMPING TEST TO EVALUATE AQUIFER CHARACTERISTICS OF STORAGE AREA PARAMETER VALUES WERE AVERAGE OF COOPER-JACOB STRAIGHT-LINE, WALTON AND HANTUSH-JACOB LEAKANCE: 0.00321 CM/SEC	760	1200	UFA
sfwmd569	25.83711	-80.12764	unk	FL	DADE	12,395		SPECIFIC CAPACITY = 28.15 GPM/FT AT 60 MIN. TRANSMISSIVITY DETERMINED BY COOPER-JACOB ANALYSIS METHOD USING SPECIFIC CAPACITY VALUE.	915	1206	UFA
sfwmd568	25.83711	-80.12764	unk	FL	DADE	4,193		SPECIFIC CAPACITY = 35.65 GPM/FT AT 60 MIN. TRANSMISSIVITY DETERMINED BY COOPER-JACOB ANALYSIS METHOD USING SPECIFIC CAPACITY VALUE.	915	1206	UFA
sfwmd567	25.44388	-80.51348	unk	FL	DADE	29,084	0.00235	Theis analysis	880	1266	UFA

sfwmd566	25.44333	-80.50861	unk	FL	DADE	10,790		SPECIFIC CAPACITY: 15 GPM/FT **WATER WAS BLENDED WITH RAW WATER FROM BISCAYNE AQUIFER WELLFIELD AND APT INITIATED AS STEP TEST TO ACCOMODATE DISCHARGE TO SEWER SYSTEM. INITAL PUMP RATE OF 280 GPM; INCREASED TO 500 GPM AND 750 GPM FOR FIRST 24 HOURS. RAT	880	1353	UFA
sfwmd570	25.83711	-80.12764	unk	FL	DADE	12,179		SPECIFIC CAPACITY = 32.05 GPM/FT AT 60 MIN. TRANSMISSIVITY DETERMINED BY COOPER-JACOB ANALYSIS METHOD USING SPECIFIC CAPACITY VALUE.	915	1206	UFA
sfwmd585	27.04111	-81.74239	unk	FL	DE SOTO	1,210	0.000289	ANALYSIS METHOD: HANTUSH, THEIS, THEIS-JACOB RECOVERY	280	409	IA
sfwmd586	27.07172	-81.61564	unk	FL	DE SOTO	258	0.0000763		282	417	IA
sfwmd582	27.17422	-81.97648	unk	FL	DE SOTO	7,100		THE REPORT DID NOT SPECIFY START TEST DATE & TIME, STORATIVITY, K-VALUE(S), OR LEAKANCE.	110	357	IA
sfwmd587	27.06144	-81.88369	unk	FL	DE SOTO	4,910	0.000413	LOWER PERMEABLE ZONE OF THE IAS. TRANSMISSIVITY, HORIZONTAL K-VALUE, VERTICAL K-VALUE, LEAKANCE AND STORAVITY ARE AVERAGES OF FOUR METHODS: HANTUSH-JACOB, HANTUSH, MOENCH, AND NEUMAN-WITHERSPOON.	347	461	IA
sfwmd584	27.13339	-82.05537	unk	FL	DE SOTO	9,945	0.000218	ANALYTICAL METHODS NOT RECOMMENDED BECAUSE THE TEST DID NOT MEET ASSUMPTIONS OF HOMOGENEITY AND ISOTROPY. REPORTED VALUES ARE BASED ON NUMERICAL MODELING ANALYSIS. REPORTED LEAKANCE IS BETWEEN THIS PRODUCING ZONE AND THE UPPER FLORIDAN BELOW. LEAKANCE	205	330	IA
sfwmd580	27.06144	-81.88369	unk	FL	DE SOTO	614	0.000191	UPPER PERMEABLE ZONE OF THE IAS. TRANSMISSIVITY, HORIZONTAL K-VALUE, VERTICAL K-VALUE, LEAKANCE AND STORAVITY ARE AVERAGES OF FOUR METHODS: HANTUSH-JACOB, HANTUSH, MOENCH, AND NEUMAN-WITHERSPOON.	56	90	IA
sfwmd581	27.04111	-81.74239	unk	FL	DE SOTO	5,550	0.0000476	ANALYSIS METHODS: HANTUSH, THEIS, AND THEIS-JACOB RECOVERY	60	110	IA
sfwmd588	27.07172	-81.61564	unk	FL	DE SOTO	766	0.000119		514	596	IA
swfwmd183	27.05410	-81.57030	unk	FL	DE SOTO	300,802		Step-drawdown test; T value estimated from analysis of recovery data.	638	1547	UFA
swfwmd118	27.04130	-81.73540	unk	FL	DE SOTO	42,600	0.0000806	Transducer failed 520 min into unmanned recovery phase, however data suitable for analysis; drawdown data from OB well analyzed using Theis confined, Hantush leaky aquifer & Cooper-Jacob time-drawdown methods; recovery data from both wells analyzed using	487	710	UFA

sfwmd589	27.28505	-82.03898	unk	FL	DE SOTO	8,297	0.000225	Drawdown & recovery data from OB well analyzed using Hantush-Jacob (1955) & Theis recovery (1935) curve-matching methods.	536	741	UFA
swfwmd117	27.04130	-81.73540	unk	FL	DE SOTO	7,060	0.00039	OB well is dual-zone mon. well; also monitored Suwannee from 725'-909'; drawdown & recovery data from OB well analyzed using Theis confined, Hantush leaky aquifer & Cooper-Jacob time-drawdown methods; discrepancies in T & S values between drawdown & reco	720	905	UFA
swfwmd145	27.12697	-82.04931	unk	FL	DE SOTO	5,446	0.0003	Drawdown data from OB well analyzed using Hantush method; recovery data from OB well analyzed using Theis & Jacob curve-matching method; T value represents log. avg. of analytical method results; water levels in semi-confining units also monitored.	505	801	UFA
swfwmd223	27.06990	-81.61890	unk	FL	DE SOTO	2,353	0.086	No data correction applied; refer to ROMP 13 APT report for more detailed information.	674	786	UFA
swfwmd121	27.20130	-81.65340	unk	FL	DE SOTO	3,610		Barometric fluctuations & local pumping effects accounted for; k = 87.7 gpd/ft2.	576	880	UFA
sfwmd590	27.13339	-82.05537	unk	FL	DE SOTO	6,193	0.00028	ANALYTICAL METHODS NOT RECOMMENDED BECAUSE THE TEST DID NOT MEET ASSUMPTIONS OF HOMOGENEITY AND ISOTROPY. REPORTED VALUES ARE BASED ON NUMERICAL MODELING ANALYSIS. REPORTED LEAKANCE IS BETWEEN THIS PRODUCING ZONE AND PRODUCING ZONE 3 OF THE INTERMEDIATE	550	800	UFA
swfwmd133	27.28530	-82.04090	unk	FL	DE SOTO	8,297	0.000225	Drawdown & recovery data from OB well analyzed using Hantush-Jacob (1955) & Theis recovery (1935) curve-matching methods.	536	741	UFA
swfwmd123	27.06117	-81.88400	NAD83	FL	DE SOTO	3,566	0.000786	Several analytical methods used to analyze drawdown & recovery data from pumped well; Note: Leakance value considered to be questionable.	715	1537	UFA
swfwmd105	27.24420	-82.04830	unk	FL	DE SOTO	160,428	0.0004	Shallow and deep zones above & below also monitored; corrections made for barometirc & regional fluctuations;numerous regional monitoring wells also monitored; this site fka "Amax".	280	1550	UFA
swfwmd122	27.05650	-81.88490	unk	FL	DE SOTO	559	0.000000003	Several analytical methods used to analyze drawdown & recovery data from pumped well; Note: Storativity value considered to be questionable.	600	827	UFA
swfwmd185	27.09960	-81.61880	unk	FL	DE SOTO	6,283		Step-drawdown test; T value estimated from analysis of recovery data.	662	1042	UFA

swfwmd196	27.28199	-81.61286	NAD27	FL	DE SOTO	920,000		Test duration incl. recovery; data corrected for regional water-level changes; Q value is combined pumpage from 7 wells, all open to same interval; pumping well also tapped lower Intermediate Aquifer; T value is log. avg. of two test results; S & L values	397	1317	UFA
swfwmd259	27.33084	-82.04749	unk	FL	DE SOTO	160,427	0.0004	Shallow and deep zones above & below also monitored; corrections made for barometirc & regional fluctuations;numerous regional monitoring wells also monitored; this site fka "Amax".	280	1550	UFA
swfwmd003	27.07150	-81.98380	unk	FL	DE SOTO	13,400	0.0002	No data corrections applied; short duration test; test well open to lower Intermediate & upper Floridan Aquifers; low T value indicates partial penetration (not full UFA test); data from 1 OB well only available; T value plausible; S value plausible consi	160	1090	UFA
swfwmd002	27.07150	-81.98380	unk	FL	DE SOTO	9,090	0.00036	Zones above & below & regional wells also monitored; corrections made for barometric & tidal effects; multi-zoned well drilled 200' from production well yielded very little drawdown, poss. due to well construction or geologic structure; low T value indica	270	1000	UFA
swfwmd116	27.04130	-81.73540	unk	FL	DE SOTO	1,600,000	0.000805	Noted - Tropical Storm occurred during test. Four inches of rainfall received durig test.	1100	1373	UFA
swfwmd050	27.07030	-81.66940	unk	FL	DE SOTO	117,647	0.02	OB well partially penetrating; casing depths unknown; no data corrections applied; 3 other wells monitored, but drawdowns masked by regional fluctuations.		1600	UFA
swfwmd088	27.08380	-81.58910	unk	FL	DE SOTO	111,898	0.01	Drawdown values corrected for regional trends; partial penetration; T value confirms step-drawdown test result of 803,352 gpd/ft.	650	1544	UFA
sfwmd583	27.27500	-81.62100	unk	FL	DE SOTO	267,379	0.00003	Seven pumping wells; all wells open to the same intervals; power failure influenced the data; no adjustment for barometric or regional trends.:Tested Formation -H-Tp-S-Oc-AP	175	1340	UFA
swfwmd103	27.06740	-81.99910	unk	FL	DE SOTO	10,900	0.0002	Hantush (1964) inflection-point method was used for analysis; raw data not available.	105	1072	UFA
swfwmd184	27.08400	-81.56970	unk	FL	DE SOTO	132,352		Step-drawdown test; T value estimated from analysis of recovery data.	668	1154	UFA
sjrwmd168	30.15139	-81.64472	unk	FL	DUVAL	35,786	0.00131	average Cooper-Jacob	482	1100	FAS
usgs056	30.32222	-81.94556	unk	FL	DUVAL	75,000			538	1265	FAS
sjrwmd171	30.15000	-81.63528	unk	FL	DUVAL	22,899	0.0009	average Hantush	485	1225	FAS
sjrwmd169	30.15047	-81.64663	unk	FL	DUVAL	19,007	0.000546	average Cooper-Jacob straight line and Theis	482	1100	FAS
sjrwmd043	30.14166	-81.65833	unk	FL	DUVAL	19,952	0.000286	Average of Modified Hantush 1960	485	1225	FAS
sjrwmd059	30.28333	-81.89750	unk	FL	DUVAL	19,399	0.000085	Hantush-Jacob	415	1250	FAS

sjrwmd055	30.46011	-81.64321	unk	FL	DUVAL	8,343	0.0039	Hantush leaky confined aquifer	620	1100	FAS
sjrwmd054	30.46011	-81.64321	unk	FL	DUVAL	10,446	0.0039	Hantush confined aquifer	620	1100	FAS
usgs015	30.15139	-81.64472	unk	FL	DUVAL	19,000	0.00015	T & S from observation well; T=24000 ft2/day & S= 0.000033 using Theis analysis, and T=25000 ft2/day & S=0.00002 using Hantush analysis.	482	1100	FAS
sjrwmd051	30.15139	-81.64472	unk	FL	DUVAL	33,310	0.001384	Average of Cooper-Jacob, Theis, and Hantush	482	1100	FAS
sjrwmd050	30.15139	-81.64472	unk	FL	DUVAL	25,150	0.000428667	Average of Cooper-Jacob, Theis, and Hantush	482	1100	FAS
usgs052	30.25389	-81.61361	unk	FL	DUVAL	22,000	0.0005	T=15000 if recovery analysis utilized; S from observation well (T=18000 ft2/day).	514	1100	FAS
usgs053	30.40861	-81.52417	unk	FL	DUVAL	110,000	0.02	T & S from obs well; additional obs well yields T of 65000 ft2/day & S of 0.000125	457	1192	FAS
usgs055	30.40944	-81.52583	unk	FL	DUVAL	24,000	0.0004	S value from obs well (also S of 0.004 at additional obs well); T's from obs wells of 62000 ft2/day & 18000 ft2/day.	480	1048	FAS
sjrwmd046	30.15000	-81.63528	unk	FL	DUVAL	17,421	0.00026	Hantush	485	1225	FAS
sjrwmd170	30.15000	-81.63528	unk	FL	DUVAL	19,959	0.000286	average modified Hantush	485	1225	FAS
sjrwmd105	30.29778	-81.60139	unk	FL	DUVAL	20,000	0.0013	Average of 3 observation wells.	6	700	IA-UFA
sjrwmd044	30.15833	-81.64166	unk	FL	DUVAL	9,108	0.0007	Modified Hantush 1960	450	950	UFA
sjrwmd047	30.46778	-81.57278	unk	FL	DUVAL	26,469	0.001	Hantush	500	750	UFA
sjrwmd048	30.28028	-81.43028	unk	FL	DUVAL	20,399	0.00027	Curve matching	347	835	UFA
sjrwmd049	30.24250	-81.54055	unk	FL	DUVAL	20,159	0.00537	Average of Cooper-Jacob, Hantush, and Thies &Jacob	519	970	UFA
sjrwmd052	30.29055	-81.39972	unk	FL	DUVAL	34,669	0.0009275	Average of Theis and Jacob	400	900	UFA
sjrwmd053	30.34222	-81.53583	unk	FL	DUVAL	24,694	0.000488	Average of Theis and Hantush	565	807	UFA
sjrwmd056	30.32750	-81.59083	unk	FL	DUVAL	17,583		Cooper Jacob / Theis Recovery	550	963	UFA
sjrwmd057	30.37778	-81.84278	unk	FL	DUVAL	22,263	0.00083	Average of Hantush-Jacob	435	920	UFA
sjrwmd058	30.29111	-81.50389	unk	FL	DUVAL	40,104	0.001	Hantush-Jacob	417	1000	UFA
sjrwmd081	30.34222	-81.53583	unk	FL	DUVAL	15,000	0.0005	T from recovery analysis, S from obs well; additional obs well yields T=24000 ft2/day and S=0.0005 using leaky aquifer analytical solution.	565	807	UFA
sjrwmd202	30.29055	-81.39972	unk	FL	DUVAL	29,247	0.00093	average Theis and Jacob drawdown and recovery	400	900	UFA
sjrwmd083	30.25222	-81.61167	unk	FL	DUVAL	13,000	0.002	S value from observation well (T=14000 ft2/day at obs. well).	514	950	UFA
sjrwmd175	30.15083	-81.63444	unk	FL	DUVAL	12,482	0.0016	modified Hantush	450	600	UFA
sjrwmd042	30.14166	-81.64166	unk	FL	DUVAL	9,104	0.0007			650	UFA
sjrwmd030	30.43583	-81.64611	unk	FL	DUVAL	9,443		Average of Hantush inflection point, Jacob straight line, and Theis	600	908	UFA
sjrwmd002	30.32278	-81.94472	unk	FL	DUVAL	15,000		T from observation well (no T given for production well); 2nd observation well yielded a T of 16000 ft2/day.	536	837	UFA
sjrwmd174	30.15055	-81.63444	unk	FL	DUVAL	10,841	0.007	average Hantush and Theis and Jacob recovery	460	624	UFA
sjrwmd179	30.34222	-81.53583	unk	FL	DUVAL	21,456	0.000488	average recovery and Theis	565	807	UFA
sjrwmd183	30.32778	-81.49166	unk	FL	DUVAL	20,599	0.00028	average Cooper-Jacob and Hantush-Jacob curve matching	430	900	UFA

sjrwmd184	30.32611	-81.49028	unk	FL	DUVAL	17,499	0.000275	average Cooper-Jacob and Jacob straight line	425	920	UFA
sjrwmd045	30.40833	-81.52500	unk	FL	DUVAL	39,963	0.00444	Average of Jacob straight-line	480	1048	UFA
sjrwmd198	30.26139	-81.45361	unk	FL	DUVAL	26,068	0.00054	Hantush-Jacob	353	875	UFA
sjrwmd082	30.29056	-81.39972	unk	FL	DUVAL	20,000	0.001	T from recovery analysis at pumping well, S from obs well, which also yielded a T of 32000 ft2/day.	400	900	UFA
sjrwmd173	30.14972	-81.63472	unk	FL	DUVAL	12,486	0.0016	curve matching	460	900	UFA
usgs286	30.22250	-81.87650	NAD83	FL	DUVAL	27,000		Franks and Phelps (1979) and USGS files (Jacksonville, FL). Thickness of aquifer tested, 542 ft.			UFA
usgs285	30.23517	-81.70617	NAD83	FL	DUVAL	200,000		Franks and Phelps (1979) and USGS files (Jacksonville, FL). Thickness of aquifer tested, 697 ft.			UFA
usgs284	30.28733	-81.52200	NAD83	FL	DUVAL	130,000	0.0004	Franks and Phelps (1979) and USGS files (Jacksonville, FL). Thickness of aquifer tested, 756 ft.			UFA
usgs283	30.31133	-81.64200	NAD83	FL	DUVAL	13,000	0.0005	Franks and Phelps (1979) and USGS files (Jacksonville, FL). Thickness of aquifer tested, 565 ft.			UFA
usgs282	30.38483	-81.42950	NAD83	FL	DUVAL	27,000	0.0006	Franks and Phelps (1979) and USGS files (Jacksonville, FL). Thickness of aquifer tested, 565 ft.			UFA
nwfwmd030	30.38303	-86.85477	unk	FL	ESCAMBIA	920		Plot and data only, no analysis or other well documentation.			FAS
sjrwmd218	29.41359	-81.20339	NAD27	FL	FLAGLER	12,000	0.00036	Not published		225	UFA
sjrwmd300	29.42250	-81.17083	unk	FL	FLAGLER	27,993	0.00011	Average Time-Drawdown, Walton, Recovery, Distance-Drawdown	105	130	UFA
sjrwmd103	29.39327	-81.18786	unk	FL	FLAGLER	20,052		Step Drawdown Test	102	160	UFA
sjrwmd104	29.27555	-81.15527	unk	FL	FLAGLER	26,201	0.0001	average pump and recovery of Walton	99	271	UFA
sjrwmd182	29.62111	-81.49333	unk	FL	FLAGLER	26,000		Transmissivity value an estimate due to poorly defined drawdown curve (fig.16). Aquifer thickness is 250 ft.	155	405	UFA
sjrwmd212	29.43778	-81.22055	unk	FL	FLAGLER	23,000		modified Jacob recovery	102	223	UFA
sjrwmd213	29.43130	-81.21983	unk	FL	FLAGLER	30,813	0.000315	average Jacob modification of drawdown and recovery	0	320	UFA
sjrwmd214	29.55694	-81.21333	unk	FL	FLAGLER	50,000	0.0001	Two tests at this site. Aquifer thickness is 153 ft. Higher pumping rate, report emphasizes leakance value from this test. Leakance expressed in units per day.		330	UFA
sjrwmd012	29.51000	-81.28722	unk	FL	FLAGLER	9,400	0.0001	Hantush and Jacob (1955) leaky artesian aquifer type-curve matching method modified by Cooper; a composite analysis	123	172	UFA
sjrwmd217	29.42500	-81.20833	unk	FL	FLAGLER	7,673		average recovery and Jacob modification of drawdown and recovery	104	140	UFA
sjrwmd223	29.27500	-81.15833	unk	FL	FLAGLER	9,759	0.0006	Step-drawdown pump test; Jacob-Rorabaugh; the Walton formula (S values assumed Rutledge 1982)	87	200	UFA
sjrwmd225	29.37500	-81.15833	unk	FL	FLAGLER	1,631	0.00015	Walton's type-curve method	105	140	UFA
sjrwmd226	29.39166	-81.15833	unk	FL	FLAGLER	4,585	0.0001	Walton's formula; Six-step step-drawdown tests, 7 gpm to 129 gpm	118	180	UFA
sjrwmd227	29.35778	-81.15833	unk	FL	FLAGLER	33,554	0.0006	recovery	88	240	UFA

sjrwmd293	29.47944	-81.37583	unk	FL	FLAGLER	37,000	0.0009	Hantush and Jacob (1955) leaky artesian matchpoint	160	495	UFA
sjrwmd294	29.47139	-81.37222	unk	FL	FLAGLER	36,000	0.00047	Leakance is expressed in gpd/ft3.	120	345	UFA
sjrwmd215	29.55694	-81.21333	unk	FL	FLAGLER	61,000	0.0007	Two tests at this site. Aquifer thickness is 153 ft. Leakance expressed in units per day.		330	UFA
sjrwmd010	29.49664	-81.29507	NAD27	FL	FLAGLER	9,270	0.00042	Not published		180	UFA
sjrwmd006	29.31722	-81.31555	unk	FL	FLAGLER	36,762		Jacob straight-line recovery	60	350	UFA
nwfwmd010	29.94583	-84.48333	unk	FL	FRANKLIN	7,875			82	125	UFA
nwfwmd009	29.87160	-84.65350	unk	FL	FRANKLIN	6,109	0.00029	Lat/long from Google Earth.	82	150	UFA
nwfwmd008	29.71958	-85.02670	unk	FL	FRANKLIN	44,500	0.00012	Floridan aquifer zone 1 (FAZ-1) from 315 to 400. FAZ-2 from 585 to > 615.	326	402	UFA
nwfwmd016	30.65000	-84.82000	unk	FL	GADSDEN	12,845		Lat/long estimated from Google Earth. T value is average of 3 values.	189	308	UFA
nwfwmd012	30.57714	-84.58047	NAD27	FL	GADSDEN	3,671		Lat/long estimated from Google Earth. Page 15 is missing, includes results for OW-2 and OW-3. T value is for pumped well only.	434	681	UFA
nwfwmd013	30.59853	-84.57991	NAD83	FL	GADSDEN	1,200	0.00018	Lat/long from Google Earth.	332	1346	UFA
usgs050	30.56850	-84.58933	NAD83	FL	GADSDEN	5,100		Pascale and Wagner (1982). Thickness of aquifer tested, 247 ft.			UFA
usgs039	30.61067	-84.59200	NAD83	FL	GADSDEN	1,400	0.0002	Pascale and Wagner (1982). Thickness of aquifer tested, 1014 ft.			UFA
nwfwmd015	30.68000	-84.69000	unk	FL	GADSDEN	19,562		Lat/long estimated from Google Earth.	356	469	UFA
usgs288	30.52900	-84.46567	NAD83	FL	GADSDEN	1,300	0.0003	Pascale and Wagner (1982). Thickness of aquifer tested, 123 ft.			UFA
usgs251	29.64248	-82.85387	unk	FL	GILCHRIST	650,000		SRWMD files in Live Oak, value is an average of 300,00 and 1,000,000 in table 3	75	160	UFA
sfwmd594	26.79523	-81.54054	unk	FL	GLADES	2,005	0.000002		100	180	IA
sfwmd054	27.15472	-80.87533	unk	FL	GLADES	26,884	0.0002	PRELIMINARY RESULTS FROM SFWMD FILES	562	875	UFA
nwfwmd076	29.82785	-85.29635	NAD83	FL	GULF	1,450	0.00038	Latitude and longitude based on center of reported township, range, and section. multiple observation wells used; well no 3 pumped for 50 hours at 435 gpm; specific capacity 2.4 gpm/ft	202	656	FAS
nwfwmd018	30.08000	-85.34000	unk	FL	GULF	6,600	0.00007	Lat/long grossly estimated from Google Earth. Value from average of two observation wells.	294	665	UFA
other001	30.45250	-82.86417	unk	FL	HAMILTON	190,000	0.001		173	805	UFA
swfwmd093	27.47810	-81.93340	unk	FL	HARDEE	115,000		No additional data available.			FAS
swfwmd169	27.56530	-81.94870	unk	FL	HARDEE	173,797		No additional data available.			FAS
sfwmd595	27.36658	-82.00706	unk	FL	HARDEE	1		ANALYSIS METHOD: THEIS-JACOB	105	145	IA
swfwmd246	27.57970	-81.98110	unk	FL	HARDEE	400	0.0000632	T value represents log. avg.of values estimated by analysis of recovery data; S value is log. avg. of range of values from 2x10-1 to 2x10-8; measurement of static level prior to test indicated similar head to Suwannee Ls, but different from Hawthorn Grp.	370	433	IA
swfwmd245	27.57970	-81.98110	unk	FL	HARDEE	187		Used airlift pump test; total drawdown was 58'.	1500	1702	MCU

swfwmd243	27.57970	-81.98110	unk	FL	HARDEE	25,400	0.00005	T value is avg. estimate resulting from airlift pumping tests; S value calculated is for Suwannee Ls only.	519	1073	UFA
swfwmd069	27.63850	-82.03030	unk	FL	HARDEE	102,941	0.0005	Monitor wells open only to same zone; corrections made for barometric & regional trends; monitored upper & lower zones.	950	1320	UFA
swfwmd242	27.57970	-81.98110	unk	FL	HARDEE	347,600		T value represents airlift pump test & specific capacity method (2.1 x 106 gpd/ft), partially-penetrating; total depth during airlift test was 1356' (@ 3200 gpm); total depth during spec. capacity test was 1702' (@ 3700 gpm).	514	1356	UFA
sfwmd596	27.36651	-82.00703	unk	FL	HARDEE	7,767	0.000102	UPPER FLORIDAN - SUWANEE TEST, MAX DRAWDOWN 20' IN THE PRODUCTION WELL. T & S VALUES ARE AVERAGE OF 2 ANALYSIS METHODS.	300	676	UFA
swfwmd197	27.64170	-81.86342	NAD27	FL	HARDEE	9,331,551	0.00024	Extremely high T value is log. avg. between 2 x 106 & 9.57 x 107 gpd/ft (caution is advised when using this high value for regional analysis); very little drawdown observed in pumped well (only 1.2'); corrections made for barometric & regional trends; dis	400	1050	UFA
swfwmd072	27.47810	-81.90100	unk	FL	HARDEE	70,600	0.0025	T value is avg. estimate from analysis of 3 OB wells' drawdown data & 1 OB well's recovery data; regional fluctuations accounted for; upper artesian & surficial zones also monitored; barometric & precipitation trends unknown	472	1400	UFA
swfwmd073	27.47810	-81.90100	unk	FL	HARDEE	5,789	0.000252	L value could not be confirmed; T value is calculated from analysis of 2 OB wells drawdown data; S value is arithmetic avg. of reported OB well values; both Surficial & Floridan aquifers were monitored; used Hantush-Jacob's (1955) no-steady flow in leaky	125	425	UFA
swfwmd038	27.50680	-82.02930	unk	FL	HARDEE	133,689	0.002	Well construction data based upon a scope of work; test duration is avg. of 72 & 96 hrs; actual depths may vary; hydraulic coefficients obtained from a chart; no data analysis included.	700	1100	UFA
swfwmd244	27.57970	-81.98110	unk	FL	HARDEE	267,380	0.001	L value could not be confirmed; only AP limestone tested; monitor wells open to same interval; corrections made for barometric & regional trends; monitored zone below AP (Lake City Limestone), upper artesian & surficial levels; anisotropic conditions; T v	950	1175	UFA
swfwmd138	27.58350	-81.58850	unk	FL	HARDEE	13,000	0.00005	Regional corrections made. Possible influences from nearby agricultural operation not well known , however affects were minor.	310	464	UFA

swfwmd137	27.58350	-81.58850	unk	FL	HARDEE	350,000	0.002	Regional corrections made. Possible influences from nearby agricultural operation not well known , however affects were minor.	310	1210	UFA
swfwmd136	27.58350	-81.58850	unk	FL	HARDEE	340,000	0.001	Regional corrections made. Possible influences from nearby agricultural operation not well known , however affects were minor.	720	1210	UFA
swfwmd135	27.59740	-81.84190	unk	FL	HARDEE	25,000	0.0008	Hantush-Jacob and Theis Recovery methods used. Average of methods reported.	475	591	UFA
swfwmd134	27.59820	-81.84190	unk	FL	HARDEE	244,000	0.0016	Cooper-Jacob and Theis Recovery methods used. Average of methods reported.	835	1400	UFA
swfwmd128	27.36644	-82.00703	NAD83	FL	HARDEE	313,000	0.000292	Water levels in OB well appeared to be influenced by offsite pumping after 2000 min.; drawdown data from OB well analyzed using Cooper & Jacob time drawdown & Hantush leaky aquifer methods; recovery data from OB well analyzed using Theis & Jacob confined	960	1785	UFA
swfwmd129	27.35920	-82.01420	unk	FL	HARDEE	7,773	0.0000982	Slight drawdown observed I Arcadia IAS mon. well during pumping; slight increases occurred in surficial & Avon Park mon. wells during drawdown phase; corrections made for regional trends; sharp drawdown & recovery fluctuations due to nearby citrus irrigat	300	676	UFA
sfwmd608	26.60762	-80.94928	unk	FL	HENDRY	1,375	0.00012	THE MOENCH ANALYTICAL MODEL WAS USED TO ANALYZE DATA W-17093 = L2-TW	1400	1810	FAS
sfwmd607	26.75318	-81.47160	unk	FL	HENDRY	3,585	0.00012	TRANSMISSIVITY AND STORATIVITY ESTIMATED USING THE MOENCH ANALYTICAL METHOD.	1110	1465	FAS
sfwmd618	26.39638	-80.97107	unk	FL	HENDRY	33,422	0.0005			120	IA
sfwmd609	26.75318	-81.47160	unk	FL	HENDRY	561,258	0.00066	T = AVERAGE OF HANTUSH-JACOB (701,890 FT2/D) & THEIS RECOVERY (420,626 FT2/D). AFTER BAROMETRIC CORRECTION, ONLY 0.2 FT OF DRAWDOWN OCCURRED IN THE MONITOR WELL LAB-TW, 270 AWAY.	1658	1758	MCU
sfwmd600	26.74175	-80.93186	unk	FL	HENDRY	23,800	0.00032	CORRECTED FOR BAROMETRIC EFFECTS. TEST INDICATES POSSIBILITY OF DIRECTIONAL ANISOTROPY IN PERMEABILITY OF WELLFIELD. FLOW LOGS INDICATE THAT GREATEST PERMEABILITY BETWEEN 700 AND 800 FEET BLS.	700	1250	UFA
sfwmd606	26.60800	-80.94937	unk	FL	HENDRY	3,476	0.000114	T = AVERAGE VALUE, STORAGE COEFFICIENT ESTIMATED FROM BAROMETRIC EFFICIENCY USING JACOB (1940) ANALYSIS METHOD.	810	1160	UFA
sfwmd605	26.74269	-80.92842	unk	FL	HENDRY	16,019		SPECIFIC CAPACITY = 118.8 gpm/ft drawdown	730	1250	UFA
sfwmd604	26.74269	-80.92842	unk	FL	HENDRY	12,478		SPECIFIC CAPACITY = 178.95 gpm/ft drawdown	730	1250	UFA

sfwmd603	26.74175	-80.93186	unk	FL	HENDRY	2,252		SPECIFIC CAPACITY = 29 gpm/ft drawdown	720	1250	UFA
sfwmd601	26.74175	-80.93186	unk	FL	HENDRY	1,151		SPECIFIC CAPACITY = 30 gpm/ft drawdown	720	1250	UFA
sfwmd599	26.74103	-80.93975	unk	FL	HENDRY	12,800	0.00043	PUMP FAILED AFTER 2 DAYS OF PUMPING, NO COLLECTION OF RECOVERY DATA. CHLORIDE CONCENTRATION AT END OF TEST = 1140 MG/L.	700	1200	UFA
sfwmd598	26.75318	-81.47160	unk	FL	HENDRY	9,299	0.000067	SPECIFIC CAPACITY = 17.3 GPM/FT TRANSMISSIVITY AND STORATIVITY ESTIMATED USING THE MOENCH ANALYTICAL METHOD	670	850	UFA
sfwmd597	26.68696	-81.55360	unk	FL	HENDRY	2,710		SUSPECT PARTIAL PENETRATION.	634	658	UFA
sfwmd602	26.74175	-80.93186	unk	FL	HENDRY	3,119		SPECIFIC CAPACITY = 29.5 gpm/ft drawdown	720	1250	UFA
swfwmd040	28.64706	-82.33450	unk	FL	HERNANDO	43,048	0.001	Mon. wells constructed on 4 sides of production well at approx. radius of 1000'; data analyzed by USGS; little data available; obs. wells open to same interval as prod. well; L value represents log. avg. of reported range of values.	100	500	UFA
swfwmd147	28.44080	-82.64160	unk	FL	HERNANDO	8,823		Upper zone monitored; distortion of drawdown curve due to tidal effects & well development; T value est. from recovery data; adj. Caribbean Lake affected aquifer recharge.	58	378	UFA
swfwmd146	28.45510	-82.65820	unk	FL	HERNANDO	56,551		Minimal tidal effect; T value est. from analyss of early recovery data; significant effects from water density & well development.	447	820	UFA
swfwmd220	28.51460	-82.59240	unk	FL	HERNANDO	2,100,000		Special case: site is a spring; T value calculated using flow-net analysis of Dec 1975 potentiometric surface map & closed-contour analysis (Lohman 1972).			UFA
sfwmd625	27.26671	-81.33951	unk	FL	HIGHLANDS	59,600		:Tested Formation -Ap	585	1385	FAS
sfwmd619	27.36893	-81.43424	unk	FL	HIGHLANDS	162	0.0002		370	430	IA
sfwmd623	27.14922	-81.35368	unk	FL	HIGHLANDS	31	0.00253		460	521	IA
sfwmd626	27.36893	-81.43424	unk	FL	HIGHLANDS	59,600		LOWER PERMEABLE ZONE OF THE UPPER FLORIDAN-AVON PARK FORMATION	960	1642	MCU
swfwmd004	27.57960	-81.49050	unk	FL	HIGHLANDS	69,518	0.00046	Barrier boundary encountered; regional pumpage uncorrected & noticeable; casing depth of monitor well unknown.	425	1492	UFA
swfwmd119	27.14977	-81.35285	NAD27	FL	HIGHLANDS	7,580	0.0000223	Parameters represent avg. of 2 analytical methods; no drawdown data could be made useful for calculation of parameters, but recovery data was used to calculate T & S values; low T value may be due to well construction constraints; potentiometric level ros	1003	1670	UFA
swfwmd120	27.15440	-81.35850	unk	FL	HIGHLANDS	6,564	0.00099	Parameters represent avg. of 4 analytical methods; this test encompasses lower 47.5' of Suwannee Ls & upper 23.5' of the Ocala Ls; no data correction applied.	650	730	UFA

swfwmd131	27.50270	-81.41997	unk	FL	HIGHLANDS	40,000	0.0005	Used Theis (1935) for Confined Aquifers (Drawdown and Recovery phases), Data corrected for reginal trends	478	1640	UFA
swfwmd130	27.36100	-81.44110	unk	FL	HIGHLANDS	333	0.00019	100' radius well monitored dual zones; drawdown & recovery data from test & OB wells analyzed using Hantush Jacob type curevs for leaky confined aquifers & Jacob's straight-line method.	485	600	UFA
swfwmd157	27.50226	-81.44396	NAD27	FL	HIGHLANDS	26,737	0.00033	Test interrupted for 2 min. after pumping for 110 min.; no recovery data collected; no data corrections applied.	520	1400	UFA
swfwmd060	27.21470	-81.34190	unk	FL	HIGHLANDS	56,149	0.0002	No data corrections applied; regional well was monitored.	682	1682	UFA
swfwmd092	27.72740	-82.37770	unk	FL	HILLSBOROUGH	76,203		No additional data available.			FAS
sfwmd632	27.65300	-82.06300	unk	FL	HILLSBOROUGH	280,748	0.001	One OB well's data was analyzed for the hydraulic characteristics; barometric and regional fluctuations were corrected; recovery data invalid due to change in regional trend; monitored both the upper artesian and surficial levels.:Tested Formation -Tp-S-O	400	1140	FAS
swfwmd091	27.81490	-82.11230	unk	FL	HILLSBOROUGH	119,000		No additional data available.			FAS
swfwmd174	27.65320	-82.07910	unk	FL	HILLSBOROUGH	104,011		No additional data available.			FAS
swfwmd054	27.75480	-82.09580	unk	FL	HILLSBOROUGH	104,000		No additional data available.			FAS
sfwmd631	27.65300	-82.07900	unk	FL	HILLSBOROUGH	735,294	0.0002	Regional water level trend and barometric pressure changes were accounted for; this is mainly the result of one OB well's data analysis; recovery data invalid due to change in regional trend; monitored both the upper artesian and surficial levels; L value	400	1140	FAS
sjrwmd282	27.97154	-82.25775	unk	FL	HILLSBOROUGH	14,636	0.000288	Used Stallman, 1952 Image Well Analysis (Brandon Carst Terrain); Corrected for regional trends	133	400	UFA
swfwmd044	28.11960	-82.32810	unk	FL	HILLSBOROUGH	40,000	0.0015	No data correction applied; test duration incl. recovery time; anisotropic aquifer; lower zones also monitored; T value is eff. T (Tx/Ty = 4.3).	100	884	UFA
swfwmd043	28.11960	-82.32810	unk	FL	HILLSBOROUGH	35,000	0.001	No data correction applied; lower zones also monitored; no penetration is apparent in most permeable; test duration incl. recovery time; L value represents log. avg. of reported values.	100	500	UFA
swfwmd045	28.10610	-82.32700	unk	FL	HILLSBOROUGH	38,000	0.001	Slight regional water level flux; no data correction applied; anisotropic aquifer; T value is eff. T (Tx/Ty = 6.9); lower zones monitored; test duration incl. recovery time.	120	600	UFA

swfwmd051	27.98870	-82.21250	unk	FL	HILLSBOROUGH	30,615	0.0012	No data corrections applied; monitored upper zones; T & S values avgs.; vert. K = 0.565 gpd/ft2.	530	850	UFA
swfwmd219	27.65142	-82.09370	NAD27	FL	HILLSBOROUGH	207,219		T value re-evaluated from Geraghty & Miller's 1981 data (See Grace 4 Corners GD-8).	400	1140	UFA
swfwmd042	28.11960	-82.32810	unk	FL	HILLSBOROUGH	53,500	0.001	Data analyzed with Jacob-Hantush type-curve method (1955) for infinite leaky aquifer; raw data not available.			UFA
swfwmd186	28.13730	-82.62550	unk	FL	HILLSBOROUGH	28,500	0.0055	No data available; values obtained form Plate 12 following pg. C-22 in Vol. II of referenced report.			UFA
swfwmd187	28.13730	-82.62550	unk	FL	HILLSBOROUGH	33,000	0.0009	No data correction applied; short duration test; minimal regional trends; partial penetration; OB wells assumed to be same spec as pumping well.	110	350	UFA
sjrwmd283	28.01791	-82.32712	unk	FL	HILLSBOROUGH	53,472	0.0005	Partially penetrating; little data available; T, S & L values represent avgs. of test data from two seperate test sites, calculated by fitting observed values of drawdown of each OB well to Hantush-Jacob (1955) leaky aquifer type-curves.	30	100	UFA
swfwmd189	28.03240	-82.24430	unk	FL	HILLSBOROUGH	15,374	0.001	Short duration test; ob. wells partially penetrating; data not available (memo).	150	640	UFA
sjrwmd286	28.11386	-82.50311	unk	FL	HILLSBOROUGH	85,794	0.0032	Drawdown and Recovery monitored at seven wells; data corrected for regional trends; analysis performed using Cooper-Jacob, Theis, Hantush-Jacob and Theis (Recovery).	200	700	UFA
usgs308	28.11615	-82.53133	NAD83	FL	HILLSBOROUGH	67,000	0.0007	USGS files (Tampa, FL). Thickness of aquifer tested, 400 ft.			UFA
swfwmd161	28.12739	-82.50934	unk	FL	HILLSBOROUGH	67,700	0.00084	Drawdown and Recovery monitored at five wells; data corrected for regional trends; analysis performed using Cooper-Jacob, Theis, Hantush-Jacob and Theis (Recovery).	197	663	UFA
usgs309	27.82783	-82.34100	NAD83	FL	HILLSBOROUGH	71,000	0.0004	USGS files (Tampa, FL). Thickness of aquifer tested, 515 ft.			UFA
swfwmd037	27.93060	-82.16220	unk	FL	HILLSBOROUGH	29,545	0.0011	Monitored lower zone; barometric & regional trends accounted for; incl. 7 day recovery test; >4 in. rainfall during test.	123	900	UFA
swfwmd033	27.85690	-82.19460	unk	FL	HILLSBOROUGH	36,096	0.0009	Both drawdown & recovery analyzed; regional trends corrected; water table monitored.	212	926	UFA
swfwmd019	27.80120	-82.06400	unk	FL	HILLSBOROUGH	125,668		No additional data available.	350	950	UFA
swfwmd041	28.07640	-82.32700	unk	FL	HILLSBOROUGH	129,947	0.0002	Special case: site is a spring; no available data.			UFA
swfwmd104	28.03100	-82.22940	unk	FL	HILLSBOROUGH	29,947	0.0023	No data available.	546	800	UFA

swfwmd150	27.77100	-82.39270	unk	FL	HILLSBOROUGH	73,529	0.000103	Accounted for barometric pressure changes, tidal effects, local agricultural pumpage & well development; OB well data could not be verified.	714	1260	UFA
swfwmd074	28.10610	-82.32700	unk	FL	HILLSBOROUGH	56,000	0.0012	No data correction applied; anisotropic aquifer; T value is eff. T; lower zones monitored; test duration incl. recovery time.	100	661	UFA
swfwmd081	28.03100	-82.22940	unk	FL	HILLSBOROUGH	4,679	0.00005	One ob. well (r = 50') opened to 560' deep zone showed excellent K between both wells; no significant water level changes.	68	227	UFA
swfwmd082	28.03100	-82.22940	unk	FL	HILLSBOROUGH	29,410	0.002	Test #6. Continuous rainfall throughout test; only 1 ob. well open to same interval (r = 400').	72	800	UFA
swfwmd083	28.03100	-82.22940	unk	FL	HILLSBOROUGH	13,369	0.0003	No data available; analysis of another test (Q = 1520 gpm for 32 hrs) in same zone reveals T = 5x104 gpd/ft2, s = 7x104, S = 1x10-3 gpd/ft3.	68	413	UFA
swfwmd164	27.98850	-82.34410	unk	FL	HILLSBOROUGH	86,000	0.0009	No data corrections applied; partial penetration of all wells, but insig. effects due to distances from pumping to ob. wells; anisotropic aquifer; T value is eff. T (Tx/Ty = 2.3); test duration incl. recovery time.	45	100	UFA
swfwmd089	28.10570	-82.49320	unk	FL	HILLSBOROUGH	13,503	0.0007	No data corrections applied; water levels monitored by 6 Floridan & 10 surficial OB wells, ranging from 66-1041' in radius; hydraulic parameters represent arithmetic avg. of analyses using all Floridan OB wells.	93	255	UFA
swfwmd070	28.01850	-82.32540	unk	FL	HILLSBOROUGH	120,000	0.0011	No data corrections applied; mod. regional water level changes; short duration test, incl. recovery time; partial penetration; no vert. flow correction; anisotropic aquifer; T is eff. T (Tx/Ty = 5.3).	25	75	UFA
usgs320	28.09779	-82.54426	NAD27	FL	HILLSBOROUGH	15,000	0.00192	Cooper-Jacob (1946), Neuman (1994), and OPTIM (Halford, 1992). Ss = 3x10-6.	210	850	UFA
swfwmd106	28.00350	-82.16240	unk	FL	HILLSBOROUGH	23,663	0.002	Recovery measured; regional trends not corrected.	198	746	UFA
swfwmd107	28.03100	-82.22940	unk	FL	HILLSBOROUGH	37,100	0.0015	Adjustments made for vert. flow effects between pumping and ob. wells; mod. regional water level changes during test; only ob. well data available; ob. well tapped lower zone; partial penetration; T, S & L all good estimates; L value assumed to be less th	70	810	UFA
swfwmd111	27.81430	-82.32610	unk	FL	HILLSBOROUGH	46,791	0.001	Short duration test; barometric & regional trends accounted for; drawdown shift occurred midwaythrough test; L value is questionable.	220	750	UFA
swfwmd112	28.04770	-82.19390	unk	FL	HILLSBOROUGH	15,642	0.0004	Short duration test; ob. wells partially penetrating; data not available (memo).	102	640	UFA
swfwmd114	28.00350	-82.47540	unk	FL	HILLSBOROUGH	20,321	0.000098	L value questionable; model results do not correspond to empirical potentiometric drawdown data.	295	385	UFA

swfwmd084	28.13561	-82.54217	unk	FL	HILLSBOROUGH	50,133	0.000062	Rainfall & regional trends accounted for; GW flow model used to calculate hydraulic coefficients by comparing calibrated vs. actual drawdowns.	200	700	UFA
swfwmd165	27.94560	-82.09770	unk	FL	HILLSBOROUGH	27,005		T value questionable due to lack of crucial early time data, estimated from analysis of 5-hr recovery following specific capacity test; little additional. data available; very short duration test; (memo).	252	874	UFA
swfwmd057	28.11930	-82.13050	unk	FL	HILLSBOROUGH	23,200	0.00082	Corrections applied for fluctuations due to precipitation events & regional trends; approx. 6.4 in. rainfall received at test site in first 4 days of test; parameters represent harmonic mean of 5 analytical methods.	150	700	UFA
swfwmd058	28.09060	-82.08400	unk	FL	HILLSBOROUGH	24,800	0.00054	Corrections applied for fluctuations due to precipitation events & regional trends; approx. 1.7 in. rainfall received at test site in first 4 days of test; parameters represent harmonic mean of 5 analytical methods.	150	700	UFA
swfwmd175	27.74050	-82.16270	unk	FL	HILLSBOROUGH	160,000		No additional data available.			UFA
swfwmd059	28.14820	-82.09800	unk	FL	HILLSBOROUGH	37,000	0.00028	Corrections applied for fluctuations due to precipitation events & regional trends; approx. 1.7 in. rainfall received at test site in first 4 days of test; parameters represent harmonic mean of 5 analytical methods.	150	700	UFA
swfwmd061	28.10650	-82.59140	unk	FL	HILLSBOROUGH	53,476	0.0006	Partial penetration; upper zone also monitored; corrections made for regional trends; parameters calculated from distance-drawdown data; other tests were performed, but data was highly influenced by pumpage & large radii; L value could not be confirmed.	105	345	UFA
swfwmd168	27.81400	-82.29380	unk	FL	HILLSBOROUGH	61,500		No additional data available.			UFA
swfwmd151	27.77100	-82.39270	unk	FL	HILLSBOROUGH	14,570	0.000147	Fully penetrating well; influenced by local agricultural pumping; monitored upper zones.	247	462	UFA
swfwmd166	27.88680	-82.07960	unk	FL	HILLSBOROUGH	152,406		T value representative of western side of area well corridor, along US 39; values range from 3.3x105 to 2.08x106 gpd/ft; used modified Jacob (Driscoll, 1986) and Cooper-Jacob (1946) for analysis.	217	877	UFA
swfwmd152	27.71340	-82.39410	unk	FL	HILLSBOROUGH	80,213	0.002	Two other OB wells were used for comparison, depths unknown; barometric & regional trends accounted for; L value is questionable.	170	810	UFA
swfwmd162	28.06240	-82.59040	unk	FL	HILLSBOROUGH	26,737	0.001	Values obtained form step-drawdown tests; ob. well monitored shallower zone; correlates with estimates obtained from original well data.	101	650	UFA

swfwmd239	27.98000	-82.25200	unk	FL	HILLSBOROUGH	22,900	0.001	Used Stallman, 1952 Image Well Analysis (Brandon Carst Terrain); Corrected for regional trends	120	710	UFA
swfwmd160	28.11386	-82.50310	unk	FL	HILLSBOROUGH	85,800	0.0032	Drawdown and Recovery monitored at seven wells; data corrected for regional trends; analysis performed using Cooper-Jacob, Theis, Hantush-Jacob and Theis (Recovery).	200	700	UFA
swfwmd159	28.12080	-82.50970	unk	FL	HILLSBOROUGH	60,160	0.0007	L value calculated from value of 28,000 gpd/mi2; drawdowns corrected for regional trends; low precip. cond.; lower upper and lower zones also monitored; computed distance-drawdown; other tests performed, but data highly influenced by pumpage and large rad	75	601	UFA
swfwmd158	28.12080	-82.50970	unk	FL	HILLSBOROUGH	71,000	0.0013	Modest regional trends; no corrections applied; lower zones also monitored; erratic pumping rate; T, S & L values are good estimates; test duration incl. recovery time.	116	551	UFA
swfwmd055	27.68350	-82.46060	unk	FL	HILLSBOROUGH	15,320	0.0006	Leaky artesian type curve may have yielded different results; no corrections were applied; well construction data not verified; low values indicate partial penetration.	65	770	UFA
swfwmd167	27.88984	-82.13399	NAD83	FL	HILLSBOROUGH	36,096		T value representative of eastern side of area well corridor, along US 39; values range from 1.7x105 to 6.8x105 gpd/ft; used Cooper-Jacob (1946) and Hantush-Jacob type curve (1954) for analysis.	200	920	UFA
swfwmd193	28.03667	-82.38528	unk	FL	HILLSBOROUGH	106,000	0.0008	Data corrected for barometric pressure changes & vert. flow; partial penetration; lower zones monitored; L is log. avg. of two end values reported; test duration incl. recovery time.	93	480	UFA
usgs007	27.72660	-82.34350	NAD83	FL	HILLSBOROUGH	66,000	0.0007	USGS files (Tampa, FL). Thickness of aquifer tested, 612 ft.			UFA
sfwmd629	28.16751	-82.64249	unk	FL	HILLSBOROUGH	93,582	0.00019	Shallower and deeper zones were monitored; regional water level fluctuations and barometric pressure changes were monitored prior to test; correction was made for a regional potentiometric surface decline from the APT drawdown data	84	777	UFA
sfwmd628	27.98900	-82.34400	unk	FL	HILLSBOROUGH	65,508	0.0008	Partially penetrating; little data available; values obtained from a re-analysis by R. Wolansky, USGS.:Tested Formation -Tp-S	20	100	UFA
swfwmd236	27.94540	-82.27690	unk	FL	HILLSBOROUGH	569,519	0.045	T & S values represent avg. of 2 analytical methods; short duration test; no L value; no data corrections applied.	119	400	UFA

swfwmd068	27.66820	-82.27790	unk	FL	HILLSBOROUGH	6,550		T value is representative of tight zone in AP Fmn., evaluated from analysis of 6 hr recovery test data; partial penetration into AP Fmn.; questionable field data acquisition.	209	750	UFA
swfwmd237	27.94540	-82.27690	unk	FL	HILLSBOROUGH	1,040,107	0.02	T & S values represent avg. of 2 analytical methods; short duration test; no L value; no data corrections applied.	120	400	UFA
swfwmd235	27.98810	-82.27910	unk	FL	HILLSBOROUGH	7,995	0.0006	T & S values represent avg. of 2 analytical methods; short duration test; questionable L value; no data corrections applied.	100	400	UFA
sfwmd630	28.12147	-82.50918	unk	FL	HILLSBOROUGH	60,160	0.0007	Drawdowns corrected for regional trends; low rainfall conditions; also monitored lower upper and lower zones; computed distance-drawdown; other tests were performed, but the data was highly influenced by pumpage and large radii.:Tested Formation -Tp-S-Oc-	94	601	UFA
swfwmd233	27.74050	-82.11270	unk	FL	HILLSBOROUGH	467,914	0.001	All upper zones and two production zones also monitored; no construction details; encountered barrier boundary @ t=100 min.; substantial background effects; corrections made for barometric & regional trends; Cooper-Jacob modified Theis & Theis-type curves	275	993	UFA
swfwmd238	27.93120	-82.29260	unk	FL	HILLSBOROUGH	18,449	0.0012	T & S values represent avg. of 2 analytical methods; short duration test; no L value; no data corrections applied.	104	425	UFA
swfwmd225	27.85740	-82.14480	unk	FL	HILLSBOROUGH	24,197	0.00083	Both drawdown & recovery analyzed; corrections applied for barometric & regional trends; water table monitored.	211	918	UFA
swfwmd192	28.03667	-82.38528	unk	FL	HILLSBOROUGH	130,000	0.00034	Slight water level flux observed during last 3 hrs of test; partially penetrating; all pumpage in wf ceased 12 hrs prior to test start; used Hantush-Jacob's (1955) nonsteady state leaky artesian aquifer method for analysis.	93	480	UFA
swfwmd230	27.75610	-82.06290	unk	FL	HILLSBOROUGH	103,610	0.00035	Upper zones monitored; corrections made for regional trends; several other regional wells also monitored; no data analyses in report; mon. wells located in same direction.	252	805	UFA
swfwmd191	27.65320	-82.34300	unk	FL	HILLSBOROUGH	240,642	0.00001	Well only penetrates lower Floridan; no adjustments made for barometric or regional trends; also monitored upper zones; regional pumpage influenced late data.	633	1061	UFA
swfwmd190	27.96200	-82.34600	unk	FL	HILLSBOROUGH	62,000	0.0023	Modeled (MODFLOW) derived leakance and storage; Applied regional data correction.	206	710	UFA

swfwmd017	27.93010	-82.11350	unk	FL	HILLSBOROUGH	60,160		Very short duration; essentially a specific capacity test.	130	695	UFA
swfwmd008	27.65350	-82.09640	unk	FL	HILLSBOROUGH	548,128	0.002	T value represents log. avg. of 3.2x106 & 5.5x106, the result of 4 OB wells; two OB well IDs areprod. wells GD-7 & GD-10; barometric & regional fluctuations were corrected; recovery data invalid due to change in regional trend; both upper artesian & surf	400	1140	UFA
swfwmd006	27.86990	-82.39600	unk	FL	HILLSBOROUGH	100,000		No data available; Q value obtained from Fig. 8, p. 15 of referenced report.			UFA
swfwmd234	27.98870	-82.31070	unk	FL	HILLSBOROUGH	6,845	0.0003	T & S values represent avg. of 2 analytical methods; short duration test; no L value; no data corrections applied.	102	470	UFA
nwfwmd058	30.79795	-85.79462	NAD83	FL	HOLMES	12,800	0.0004	Latitude and longitude in error in original database now based on center of reported township, range, and section.T5N R16W S36 Location updated by L.E. Jones, 2013. one-observation well 200 feet from production well; March 1975; pumped production well 72 hours at 402 gpm; recovery observed for 72 hours; Specific capacity of production well 20 gpm/ft; analysis Theis non-equilibrium.	240	460	FAS
sfwmd652	27.74614	-80.39950	unk	FL	INDIAN RIVER	7,500	0.0005			1000	FAS
sfwmd639	27.58642	-80.48172	NAD27	FL	INDIAN RIVER	1,500,000			2400	3005	LFA
sjrwmd106	27.74167	-80.40833	unk	FL	INDIAN RIVER	6,150	0.00075	Average of 2 observation wells. Jacob 1940 type-curve matching. Top of casing not listed in table 4, interpreted from geophysical log in figure 12.	260	991	UFA
sfwmd638	27.75697	-80.40200	NAD27	FL	INDIAN RIVER	23,000	0.0004	TRANSMISSIVITY DETERMINED BY AVERAGE OF TIME-RECOVERY RESULTS: 132,000 82,500 GAL/D FT. RESIDUAL DRAWDOWN VS TIME RATIOS AS FOLLOWS: 264,000 132,000 82,500 GAL/DAY FT.	460	960	UFA
sfwmd653	27.78336	-80.41172	unk	FL	INDIAN RIVER	19,400	0.0014			760	UFA
sfwmd636	27.66678	-80.41025	unk	FL	INDIAN RIVER	28,455			380	570	UFA
sfwmd640	27.59364	-80.40005	NAD27	FL	INDIAN RIVER	56,800	0.00039			704	UFA
sjrwmd113	27.75919	-80.40477	NAD27	FL	INDIAN RIVER	5,895				1000	UFA
sfwmd637	27.59087	-80.40172	NAD27	FL	INDIAN RIVER	50,000	0.0004		384	745	UFA

nwfwmd054	30.81967	-85.20416	NAD83	FL	JACKSON	50,000	0.0003	Latitude and longitude based on center of reported township, range, and section. 72 hour pump test plus 142 hours of recovery; observation well depth 183 ft cased to 82 ft (upper Floridan Aquifer); pumping rate 240 gpm; specific capacity 31.49 gpm/ft	44	168	FAS
usgs243	30.63081	-83.66059	unk	FL	JEFFERSON	214,000		SRWMD files in Live Oak	122	239	UFA
usgs250	29.99925	-83.05760	unk	FL	LAFAYETTE	1,604		SRWMD files in Live Oak	24	44	UFA
sjrwmd165	28.82500	-81.92500	unk	FL	LAKE	20,092	0.012	average recovery and Hantush and Jacob (1955) and Jacob (1963)	199	594	FAS
sjrwmd115	28.85500	-81.65055	unk	FL	LAKE	150,123	0.000092	average Hantush and Jacob (1955) solution for leaky confined aquifers	280	760	FAS
sjrwmd275	28.47500	-81.90833	unk	FL	LAKE	39,000	0.013	Theis (1935); Cooper (1963); and Jacob (1950)			FAS
swfwmd143	29.15720	-81.56540	unk	FL	LAKE	16,167	0.00017	AQTESOLV® sofware using Hantush-Jacob (1955) and Theis (1935); No reginal correction was made; Low T resulting from sediment infilling of secondary porosity.	450	740	LFA
sjrwmd114	28.58583	-81.69694	unk	FL	LAKE	96,023		average Cooper and Jacob (1946) and Theis (1946)	490	850	LFA
swfwmd025	28.38280	-81.68790	unk	FL	LAKE	735,294	0.00062	Specific capacity test, Theis, 1963, Lohman, 1972. No recovery analysis.	900	1520	LFA
swfwmd217	28.88923	-81.94836	unk	FL	LAKE	479,602	0.00641	7 day test, discharge to lined pond	597	983	LFA
sjrwmd306	28.35725	-81.73091	unk	FL	LAKE	11,403	0.0066	Hantush-Jacob (1955)	118	200	UFA
sfwmd655	28.85805	-81.54479	unk	FL	LAKE	42,700	0.000029	3 OBSERVATION WELLS: 10, S-1, S-2 (S-1, S-2 USED FOR OBSERVING THE SURFICIAL AQUIFER). TRANSMISSIVITY, LEAKANCE, AND STORATIVITY FROM OBS. WELL 10.	65	200	UFA
swfwmd010	28.38862	-81.91091	NAD27	FL	LAKE	13,000	0.00025	Partially penetrating; regional trends, barometric & tidal effects accounted for; surf. aquifer also monitored & analyzed; T, S & L values log. avgs. of several analytical methods.	66	192	UFA
sjrwmd307	28.35725	-81.73091	unk	FL	LAKE	100,996	0.0071	Hantush-Jacob (1955), Theis (1935), Neuman-Witherspoon (1969)	323	460	UFA
usgs298	28.50150	-81.93100	NAD83	FL	LAKE	39,000	0.013	Pride and others (1966). Thickness of aquifer tested, 260 ft.			UFA
sfwmd660	26.35194	-81.80722	unk	FL	LEE	11,096	0.000041	The date of the APT test is the year of the report. Hant-Jac/Jacob Method	213	238	IA
sfwmd656	26.73667	-81.92750	unk	FL	LEE	574	0.00046	The date of the APT test is the year of the report. Theis Method	137	160	IA
sfwmd657	26.71167	-81.83639	unk	FL	LEE	320	0.0000487	The date of the APT test is the year of the report. Jacob/Iterat. Method	140	200	IA
sfwmd659	26.74528	-81.94417	unk	FL	LEE	1,737	0.00044	The date of the APT test is the year of the report. Jacob/Theis Method	160	225	IA
sfwmd658	26.74083	-81.93167	unk	FL	LEE	891	0.00014	The date of the APT test is the year of the report. Theis/Jacob Method	155	180	IA

sfwmd666	26.57313	-82.00731	unk	FL	LEE	4,743	0.003	IN ANALYSIS INFO FOR STATIONS AT CCRO-9, CCRO-9A, AND CCRO-9B, THE METHOD USED LISTED AS OTHER IS TIME-DRAWDOWN ALSO BUT PLOTTED ON LOG-LOG SCALE INSTEAD OF THE SEMI-LOG PLOT THAT THE PREVIOUS RESULTS ARE IN.	350	748	IA-UFA
sfwmd773	26.59006	-82.01694	unk	FL	LEE	43,115		INJECTION TEST, T ESTIMATED FROM SPECIFIC CAPACITY. PRESSURE INCREASE NOT ADJUSTED FOR FRICTION LOSS, ALLOWING FOR 12.6 PSI FRICTION LOSS (HAZEN-WILLIAMS, C=150), YIELDS MUCH LARGER SPECIFIC CAPACITY (498 GPM/FT ==> T ~ 113,111 FT2/D)	2951	3280	LFA
sfwmd735	26.62803	-81.82700	unk	FL	LEE	1	0.028	TRANS IS AVG FROM CJ AND THEIS RECOVERY METHODS. SEE ANALYSIS INFO FOR DETAILS. SPECIFIC CAPACITY = 0.006 GPM/FT	1584	1620	MCU
swfwmd007	26.76570	-82.25350	unk	FL	LEE	64,037		No additional data available.	1702	1926	UFA
sfwmd668	26.63000	-82.03167	unk	FL	LEE	13,904	0.00033	ESTIMATED TRANSMISSIVITY OF BASED ON COMBINED THICKNESSES OF BOTH AQUIFERS TRANSMISSIVITY OF LOWER HAWTHORN: 54000 GPD/FT TRANSMISSITY OF UPPER SUWANEE: 50000 GPD/FT ADDITIONAL INFORMATION: MISSIMER & ASSOC. JUNE, 1984	360	863	UFA
usgs008	26.43983	-82.12222	NAD83	FL	LEE	10,000	0.0002	USGS files (Miami, FL). Thickness of aquifer tested, 115 ft.			UFA
sfwmd679	26.68150	-82.03033	unk	FL	LEE	19,369	0.00000039	TRANSMISSIVITY CALCULATED FROM RECOVERY DATA	523	694	UFA
sfwmd677	26.62575	-81.82390	unk	FL	LEE	8,045	0.0002	TRANSMISSIVITY, STORATIVITY AND LEAKANCE VALUES ARE AVERAGES OF CJ AND THEIS AND THEIS RECOVERY METHODS	510	837	UFA
sfwmd676	26.69639	-82.02194	unk	FL	LEE	6,640	0.00023		500	735	UFA
sfwmd667	26.37869	-81.82148	unk	FL	LEE	8,130	0.00088	ANALYSIS METHOD: SEMILOG RECOVERY	350	660	UFA
sfwmd663	26.46841	-81.70703	unk	FL	LEE	4,020		TRANSMISSIVITY CALCULATED USING MODIFIED WALTON METHOD.	310	368	UFA
sfwmd661	26.47563	-81.71036	unk	FL	LEE	13,400		TRANSMISSIVITY CALCULATED USING MODIFIED WALTON METHOD. SECOND STEP TEST OF ASR-5 WAS POST-ACIDIZATION OF THE WELL.	253	291	UFA
sfwmd662	26.47202	-81.70869	unk	FL	LEE	7,350		TRANSMISSIVITY VALUES WERE CALCULATED USING MODIFIED WALTON METHOD.	285	347	UFA
sfwmd682	26.71090	-81.83842	unk	FL	LEE	8,290	0.000327		540	642	UFA
sfwmd665	26.46258	-81.70425	unk	FL	LEE	2,040		TRANSMISSIVITY VALUES CALCULATED USING MODIFIED WALTON METHOD	337	397	UFA

sfwmd671	26.71951	-81.68091	unk	FL	LEE	800	0.0001	STORAGE ZONE IN ASR-1 [L-3225] IS LOCATED IN LOWER HAWTHORN PRODUCING ZONE OF THE UPPER FLORIDAN AQUIFER AS DEFINED BY REESE (2000).	445	600	UFA
sfwmd664	26.46480	-81.70425	unk	FL	LEE	3,410	0.000077	RECOMMENDED PARAMETERS FOR TRANSMISSIVITY AND STORATIVITY USE HANTUSH METHOD	328	397	UFA
sfwmd688	26.45258	-82.12593	unk	FL	LEE	6,233	0.000034	LEAKANCE VALUE OF .000267/DAY WAS ALSO DETERMINED BUT MOST LIKELY CORRESPONDS TO THE LEAKANCE OF THE CONFINING BEDS BENEATH SUWANNEE-ZONE I - FROM HANTUSH-JACOB METHOD. THIS METHOD APPEARS TO BE THE MOST ACCURATE ANALYSIS BUT OTHER METHODS WERE USED - SE	664	770	UFA
sfwmd675	26.62605	-81.81180	unk	FL	LEE	7,230		TRANS IS FROM CJ USING RECOVERY DATA	490	680	UFA
sfwmd699	26.71985	-81.68222	unk	FL	LEE	8,300	0.000053	H-J RESULTS FOR MULTIWELL TEST AGREE BETTER WTIH SINGLE WELL AND PACKER TESTS THAN C-J RESULTS. RECOMMENDED PARAMETERS ARE AVERAGE OF H-J RESULTS. A SECOND CONSTANT RATE TEST WAS RUN BUT IS NOT REPORTED HERE. STORAGE ZONE IS ABOUT 150 FT BELOW TOP OF SU	859	920	UFA
sfwmd670	26.61585	-81.82383	unk	FL	LEE	21,260	0.0004	TRANSMISSIVITY, STORATIVITY AND LEAKANCE VALUES ARE AVERAGES OF CJ, THEIS AND THEIS RECOVERY METHODS.	445	805	UFA
sfwmd698	26.72062	-81.68314	unk	FL	LEE	8,700			857	945	UFA
sfwmd683	26.62946	-81.81555	unk	FL	LEE	2,017		TRANS IS FROM CJ USING RECOVERY DATA	580	700	UFA
sfwmd686	26.38952	-81.77342	unk	FL	LEE	70,000		C-J SOLUTION FOR DRAWDOWN IN SZMW-1R IS SUSPECT. SOLUTION IS FOR VERY LATE TIME ONLY, AND BACKGROUND CHANGES DUE TO PRIOR RECHARGE MAY HAVE AFFECTED RESPONSE.	650	701	UFA
sfwmd687	26.44147	-82.10898	unk	FL	LEE	9,893	0.0002	SUWANEE IS PROBABLY PARTIALLY PENETRATED. TIDAL EFFICIENCY = 22%	660	775	UFA
sfwmd694	26.68868	-81.94148	unk	FL	LEE	9,214	0.00025		785	1100	UFA
sfwmd674	26.61915	-81.82385	unk	FL	LEE	15,060	0.00022	HYDRAULIC PARAMETERS ARE THE AVERAGE OF SEVERAL ANALYSIS METHODS.	480	832	UFA
sfwmd691	26.45203	-82.13343	unk	FL	LEE	6,759	0.000034	ESTIMATED TRANSMISSIVITY OF BASED ON COMBINED THICKNESSES OF BOTH AQUIFERS TRANSMISSIVITY OF LOWER HAWTHORN: 17000 GPD/FT TRANSMISSITY OF UPPER SUWANEE: 32880 GPD/FT	740	770	UFA

nwfwmd062	30.49998	-84.23526	NAD83	FL	LEON	127,000	0.00017	Latitude and longitude based on center of reported township, range, and section. Multi-observation well test production well pumped for 72 hours at 4500 gpm Specific Capacity was 250 gpm/ft. 2 observation wells one 164 ft away the other 1,165 ft away. Used Theis non-equlibrium analysis. Observation wells not open to exact same interva	257	310	FAS
nwfwmd041	30.51334	-84.47157	NAD83	FL	LEON	1,260	0.00026	Latitude and longitude in error in original database and based on center of reported township, range, and section. T1N R2W S6 Location updated by L.E.Jones, 2013 (County Leon not Gadsen) . 72 hour pump test plus 48 hours of recovery; multiple observation wells (upper Floridan Aquifer); pumping rate 114 gpm; specific capacity 4 gpm/ft; obs wells 210 ft away, well in unit above Floridan at 65 ft indicated that confining conditions existed use	237	360	FAS
usgs161	30.45290	-84.27638	unk	FL	LEON	1,300,000		Data from first 24 hours used to calculate T, wells 3, 4, and 5.	213	415	UFA
nwfwmd014	30.62000	-84.32000	unk	FL	LEON	53,875		Lat/long estimated from Google Earth. Average of two observation wells.	237	347	UFA
usgs247	29.46359	-82.84809	unk	FL	LEVY	25,800		SRWMD files in Live Oak	199	320	UFA
sjrwmd299	29.13391	-82.57724	unk	FL	LEVY	20,052	0.00054	Fully penetrating; barometric, tidal & regional fluctuations accounted for; upper zone also monitored.	300	780	UFA
swfwmd053	27.47640	-82.16230	unk	FL	MANATEE	60,160		No additional data available.			FAS
swfwmd113	27.44900	-82.21120	unk	FL	MANATEE	294,118	0.0004	No additional data available.			FAS
swfwmd110	27.63811	-82.47428	unk	FL	MANATEE	10,160	0.001	No additional data available.	100	580	IA-UFA
usgs029	27.56430	-82.50710	unk	FL	MANATEE	67,000	0.0011	Test duration includes recovery; no data corrections were applied; moderate regional water level changes; partial penetration. Wolansky value does not match Peek's reported value of 100,000 gpd/ft (13,368 ft2/d) in FGS RI 18. Re-evaluated by Wolansky?	225	700	IA-UFA
sjrwmd279	27.47767	-82.19599	unk	FL	MANATEE	260,677	0.00072	No additional data available.	522	1200	UFA
swfwmd071	27.43900	-82.48800	unk	FL	MANATEE	37,433	0.00055	Regional trends monitored; partially penetrating; recovery data also analyzed.	360	659	UFA
swfwmd024	27.59220	-82.30930	unk	FL	MANATEE	91,310	0.0004	No additional data available.	503	1264	UFA
sfwmd790	27.46700	-82.68400	unk	FL	MANATEE	280,749		T value was from a step-drawdown test (4 steps increasing from 2,000 to 11,800 gpm); drawdown was corrected for friction and formation losses.:Tested Formation -AP	1067	1659	UFA

sjrwmd277	27.46955	-82.68535	unk	FL	MANATEE	8		Low T representative of tight zone between lower Ocala & upper Avon Park Fmns.; T value is avg. of 4 packer tests @ various intervals between 820' & 1017'; pumping rate varied between 1.5 & 40 gpm.	0	1017	UFA
sfwmd774	27.58861	-82.25139	unk	FL	MANATEE	12,000	0.00016	:Tested Formation -S	520	714	UFA
swfwmd067	27.43790	-82.29520	unk	FL	MANATEE	45,455	0.001	Rain occurred several times during test; depth of OB wells unknown but assumed same a s pumped well; no data corrections applied; used Chow's (Kruseman & DeRidder, 1976) leaky aquifer method for analysis.	250	1250	UFA
swfwmd080	27.37610	-82.17890	unk	FL	MANATEE	133,690		No additional data available.	600	1500	UFA
swfwmd034	27.40410	-82.09630	unk	FL	MANATEE	74,465	0.000917	T & S values are averages; background water levels monitored prior to test; observed abnormal water level decline in pumping well data 1.5 min. & 10 min. into test; used Cooper-Jacob's (1946) & Hantush's (1960) modified methods for analysis.	632	1405	UFA
sjrwmd278	27.46955	-82.68535	unk	FL	MANATEE	280,729		T value from step-drawdown test (4 steps increasing from 2000 to 11,800 gpm); drawdown corrected for friction & formation losses.	1067	1659	UFA
swfwmd026	27.49080	-82.36040	unk	FL	MANATEE	42,781	0.00016	No correction applied; monitored lower Floridan & upper artesian zones; wells open only to Suwannee LS.; results are accurate.	400	700	UFA
swfwmd035	27.63831	-82.34228	unk	FL	MANATEE	10,695	0.0027	Background monitoring for 5 days prior to testing; corrections applied for regional trends; used Cooper-Jacob (1946) & Theis time-drawdown curve for analysis; L value log. avg. of reported range of values.			UFA
swfwmd224	27.39020	-82.19470	unk	FL	MANATEE	260,695	0.00072	No additional data available.	522	1200	UFA
swfwmd014	27.62410	-82.42590	unk	FL	MANATEE	133,690		Background water levels monitored prior to test; water level trend affected by recovery from freeze protection pumping prior to APT had negligible effect on effect on data; recovery data used to estimate T value; used Jacob's (1963) straight-line method f	200	900	UFA
swfwmd132	27.45775	-82.25708	NAD83	FL	MANATEE	3,945		T value estimated to be 20,685 gpd/ft during recovery (could not be confirmed); Q value could not be confirmed either; used Jacob's straight-line method for analysis.	404	750	UFA
swfwmd155	27.46850	-82.50610	unk	FL	MANATEE	4,947	0.00022	Unusually high leakance coefficicent due to partial penetration of Suwannee LS.; regional trends monitored; parameters averaged.	350	606	UFA
swfwmd227	27.50840	-82.14590	unk	FL	MANATEE	61,497	0.0004	All upper zones monitored; regionla trends monitored; data corrections applied for barometric & regional trends; good recovery data; good overall coverage.	750	1225	UFA

swfwmd240	27.58170	-82.15270	unk	FL	MANATEE	14,637	0.000288	Used Stallman, 1952 Image Well Analysis (Brandon Carst Terrain); Corrected for regional trends	133	400	UFA
swfwmd153	27.50510	-82.34360	unk	FL	MANATEE	44,385	0.002	Depths of monitor wells unknown; two pumping wells actually used; interference affected recovery data; no corrections applied; used Hantush's (1960, 1964) inflection point method & Chow's (Kruseman & DeRidder 1976) leaky aquifer methods for analysis.	250	1180	UFA
usgs031	27.46950	-82.58650	unk	FL	MANATEE	17,500	0.0383	Fully penetrating; used Jacob's straight-line for analysis.	358	700	UFA
swfwmd232	27.46680	-82.68400	unk	FL	MANATEE	8		Low T representative of tight zone between lower Ocala & upper Avon Park Fmns.; T value is avg. of 4 packer tests @ various intervals between 820' & 1017'; pumping rate varied between 1.5 & 40 gpm.		1017	UFA
swfwmd231	27.46680	-82.68400	unk	FL	MANATEE	280,749		T value from step-drawdown test (4 steps increasing from 2000 to 11,800 gpm); drawdown corrected for friction & formation losses.	1067	1659	UFA
swfwmd001	27.63770	-82.32520	unk	FL	MANATEE	116,310	0.001	Injection test; construction details of OB well unknown; little observable drawdown.	346	1568	UFA
swfwmd149	27.57840	-82.53810	unk	FL	MANATEE	2,941		Pump ceased at 53.15 minutes; tidal effects assumed negligible due to short duration of test; T & Q values could not be confirmed.	462	1260	UFA
swfwmd209	28.97294	-82.03741	unk	FL	MARION	338,770	0.000356	1st 14-day test	509	930	FAS
swfwmd097	29.08028	-82.26973	unk	FL	MARION	1,516,500		Step draw down test	125	215	UFA
swfwmd229	29.01883	-82.32000	unk	FL	MARION	701,611		Step drawdown test	63	120	UFA
swfwmd248	29.08430	-82.29440	unk	FL	MARION	62,166	0.0062	Partially penetrating (did not penetrate dolomitic zone of AP limestone).	115	200	UFA
swfwmd036	28.98140	-82.19330	unk	FL	MARION	53,475	0.0005	Partially penetrating (not in AP Fmn.); T value est. from step-drawdown test w/ approximated value for S; Q ranged from 460-750 gpm.	107	300	UFA
swfwmd228	29.01852	-82.32028	unk	FL	MARION	400,059		Step draw down test	75	113	UFA
swfwmd094	29.07971	-82.27071	unk	FL	MARION	2,251,900		Step drawdown test	147	200	UFA
usgs252	28.98140	-82.19330	unk	FL	MARION	67,000		SWFWMD (2000)	107	300	UFA
swfwmd096	29.08422	-82.28702	unk	FL	MARION	77,500		Step drawdown test	116	200	UFA
swfwmd098	29.09902	-82.29058	unk	FL	MARION	1,856,000		Step draw down test	110	553	UFA
swfwmd099	29.07987	-82.26934	unk	FL	MARION	645,600		Step drawdown test	72	118	UFA
swfwmd022	29.09506	-82.21945	unk	FL	MARION	6,999		24 hour test	91	240	UFA
swfwmd021	29.09507	-82.22005	unk	FL	MARION	1,600		24 hour test	120	225	UFA
swfwmd020	29.09507	-82.22032	unk	FL	MARION	5,110		24 hour test	93	240	UFA
sjrwmd284	29.21609	-82.05287	unk	FL	MARION	33,420			105	225	UFA
swfwmd163	29.21500	-82.04500	unk	FL	MARION	2,085,561		Special case: site is a spring; T determined by flow-net analysis using May 1968 potentiometric surface map; one flow cell contained a T value of 1.896 x 108.			UFA

sjrwmd116	29.08733	-82.00028	unk	FL	MARION	66,840			126	222	UFA
swfwmd109	29.12647	-82.26964	unk	FL	MARION	16,800		Step drawdown test	103	342	UFA
swfwmd095	29.09398	-82.26475	unk	FL	MARION	2,048,000		Step draw down test	71	245	UFA
sfwmd073	27.18005	-80.16755	unk	FL	MARTIN	1,721	0.0005		630	1525	FAS
sfwmd066	27.07461	-80.56336	unk	FL	MARTIN	9,959		SINGLE WELL RECOVERY TEST	456	1119	FAS
sfwmd062	27.17089	-80.46869	unk	FL	MARTIN	14,133		SINGLE WELL RECOVERY TEST	342	880	FAS
sfwmd064	27.16116	-80.58311	unk	FL	MARTIN	14,214		SINGLE WELL RECOVERY TEST	400	1052	FAS
sfwmd076	27.03969	-80.51419	unk	FL	MARTIN	27,406	0.0003	IPW-2 WAS TESTED AT TWO ZONES DURING CONSTRUCTION	738.7	1262.8	FAS
sfwmd081	27.05179	-80.12312	unk	FL	MARTIN	80,748	0.00000039	MAX DRAWDOWN: PRODUCTION WELL = 3.66, RO-1 = 0.69. WATER QUALITY SAMPLED DURING TEST (CL = 1,440 MG/L, SPECIFIC CONDUCTANCE = 5,090 MMHOS/CM). TRANSMISSIVITY WAS DERIVED FROM A THEIS CURVE-MATCHING ANALYSIS.	1222	1495	LFA
sfwmd080	27.09194	-80.25639	unk	FL	MARTIN	133,933	0.00000008	BETWEEN 100 MINUTES AND 1440 MINUTES INTO TEST, A STEADY TIDAL WATER LEVEL FLUCUATION OF APPROXIMATELY 0.2 FT. WAS APPARENT. MAX DRAWDOWN FOR PUMPED WELL TFRO-4 WAS 47.221. MAX DRAWDOWN FOR TFRO-3 WAS 0.516 AND MAX DRAWDOWN FOR TFRO-5 WAS 0.679.	1108	1345	MCU
sfwmd082	27.03969	-80.51419	unk	FL	MARTIN	307,487	0.0013	LEAKANCE IS FOR MC1 - UNIT BETWEEN UPPER AND MIDDLE FLORIDAN	1482	1660	MCU
sfwmd077	26.98806	-80.60556	unk	FL	MARTIN	12,873		THIS WAS A SINGLE WELL RECOVERY TEST. FLOW RATES VARIED ABOUT 6% DURING THE TEST. ANALYSIS BASED ON THEIS RESIDUAL DRAWDOWN ANALYTICAL SOLUTION OF RECOVERY DATA ONLY.	800	1040	UFA
sfwmd078	27.24328	-80.26257	unk	FL	MARTIN	59,218	0.000375	VALUES ARE AVERAGES OF HANTUSH (1956) & WALTON (1960) METHODS SUWANNEE LS, OCALA LS & UPPER AVON PARK FM.	967	1260	UFA
sfwmd079	27.24005	-80.26144	unk	FL	MARTIN	77,723	0.0004	VALUES ARE AVERAGES OF HANTUSH (1956) & WALTON (1960) METHODS SUWANNEE LS, OCALA LS & UPPER AVON PARK FM.	1063	1289	UFA
sfwmd039	24.71125	-81.09368	unk	FL	MONROE	2,327	0.0004	LEAKANCE USING WALTON (1962) METHOD NOT DETERMINED RECOMMENDED PARAMETERS ARE AVERAGE OF WALTON AND C-J VALUES FROM BOTH OBSERVATION WELLS. (NATIVE WATER = 37,300 MG/L TDS; INJECTIED WATER = 212 MG/L TDS)	387	432	IA
sfwmd040	24.55833	-81.73389	unk	FL	MONROE	256		T VALUE IS AVERAGE OF METHODS USED, SEE ANALYSIS	680	716	UFA
usgs057	30.65996	-81.47676	NAD27	FL	NASSAU	30,000	0.00025	observation well for aquifer test; additional obs well yields T=31000 ft2/day and S=0.0004.	513	1070	UFA
usgs281	30.66150	-81.48500	NAD83	FL	NASSAU	21,000	0.0003	Cooper and Warren (1945). Thickness of aquifer tested, 500 ft.			UFA

sjrwmd118	30.62278	-81.53361	unk	FL	NASSAU	17,300	0.000317	Average of Hantush type curve and time recovery analysis	490	900	UFA
sjrwmd117	30.66135	-81.47148	NAD27	FL	NASSAU	30,000	0.000325	Average of modified Cooper and Jacob (1946) generalized graphical method	560	1100	UFA
sjrwmd119	30.66083	-81.52389	unk	FL	NASSAU	170,000	0.0024	Nonleaky aquifer analysis		567	UFA
nwfwmd022	30.62936	-86.73912	NAD27	FL	OKALOOSA	25,703	0.00013		527	690	FAS
nwfwmd023	30.40548	-86.61079	NAD27	FL	OKALOOSA	1,800	0.000022	Test data and plots unvailable.	508	726	FAS
nwfwmd019	30.73318	-86.55989	unk	FL	OKALOOSA	9,870	0.0002		505	735	FAS
nwfwmd020	30.57547	-86.44578	NAD27	FL	OKALOOSA	1,900	0.00019		436	585	FAS
nwfwmd024	30.46103	-86.61329	NAD27	FL	OKALOOSA	11,700	0.00057	Test data and plots unvailable.	500	750	FAS
nwfwmd025	30.39631	-86.58995	NAD27	FL	OKALOOSA	1,300	0.000176		460	850	FAS
nwfwmd026	30.77200	-86.61000	unk	FL	OKALOOSA	16,511		Lat/long estimated from Google Earth. Value is average from 3 observation wells (reported in gpd/ft - converted to ft2/d).	420	710	FAS
nwfwmd021	30.58825	-86.63356	NAD27	FL	OKALOOSA	11,183	0.00017		528	680	FAS
nwfwmd027	30.39509	-86.58334	unk	FL	OKALOOSA	642	0.0004	John Beasley State Park	513	864	FAS
usgs001	30.67217	-86.72183	NAD83	FL	OKALOOSA	26,000	0.0001	Barr and others (1981). Thickness of aquifer tested, 163 ft.			UFA
sfwmd109	27.23744	-80.78573	unk	FL	OKEECHOBEE	586,000	0.00125	LEAKANCE OF .01-.001 DERIVED BY EXTRAPOLATION; LONGER PUMPING PERIOD REQUIRED FOR MORE ACCURATE VALUE. RECOMMENDED PARAMETERS METHOD H-J.	1268	1710	LFA
sfwmd049	27.31560	-80.80672	unk	FL	OKEECHOBEE	46,294		CORRECTED SPECIFIC CAPACITY = 172.5 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 1.02 FT SINGLE WELL RECOVERY TEST	440	1181	UFA
sfwmd106	27.23788	-80.78556	unk	FL	OKEECHOBEE	5,924		T CALCULATED USING COOPER-JACOB NONEQUILIBRIUM EQUATION	717	800	UFA
sfwmd104	27.23788	-80.78556	unk	FL	OKEECHOBEE	1,891		T = 307 GPM / 44' * 2000	717	800	UFA
sfwmd058	27.23788	-80.78556	unk	FL	OKEECHOBEE	1,953		T = 173 GPM / 24' * 2000	717	800	UFA
sfwmd057	27.18394	-80.70867	unk	FL	OKEECHOBEE	5,638	0.00006952	TRANSMISSIVITY AND STORATIVITY AVG. FROM 5 MODELS USING HANTUSH (W/STOR), MOENCH, THEIS, HANTUSH (NO STOR.), AND PAPADOPULOS-COOPER SOLUTION METHODS.	680	882	UFA
sfwmd052	27.33004	-80.98118	unk	FL	OKEECHOBEE	6,900		TRANSMISSIVITY ESTIMATED USING THEIS RECOVERY EQUATION	466	1125	UFA
sfwmd051	27.33643	-80.91867	NAD27	FL	OKEECHOBEE	240		Specific capacity = 2 gal/min/d. Single well recovery test. Bradner well #36.	536	986	UFA
sfwmd291	27.43476	-80.67756	NAD27	FL	OKEECHOBEE	11,043		SINGLE WELL RECOVERY TEST	311	896	UFA
sfwmd050	27.33643	-80.91867	unk	FL	OKEECHOBEE	246		CORRECTED SPECIFIC CAPACITY = 2.81 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 24.94 FT SINGLE WELL RECOVERY TEST	448	983	UFA

sfwmd105	27.23788	-80.78556	unk	FL	OKEECHOBEE	1,792		T = 400 GPM / 60.5' * 2000	717	800	UFA
sfwmd048	27.41282	-80.92784	NAD27	FL	OKEECHOBEE	3,700		Average of 4 values from USGS single-well recovery test. Pumped well is Bradner well #48.	482	972	UFA
sfwmd047	27.36643	-80.78562	NAD27	FL	OKEECHOBEE	3,689		CORRECTED SPECIFIC CAPACITY = 11.63 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 22.78 FT SINGLE WELL RECOVERY TEST	412	927	UFA
sfwmd045	27.40115	-81.11590	NAD27	FL	OKEECHOBEE	2,875		CORRECTED SPECIFIC CAPACITY = 7.75 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 5.55 FT SINGLE WELL RECOVERY TEST	370	1152	UFA
sjrwmd026	27.31560	-80.80673	NAD27	FL	OKEECHOBEE	2,600		RADNER, L.A. GROUND-WATER RESOURCES OF OKEECHOBEE COUNTY, FLORIDA. USGS. WRIR 92-4166.	425	1098	UFA
sfwmd107	27.30310	-80.71644	unk	FL	OKEECHOBEE	4,278	0.001376	TRANSMISSIVITY AND STORATIVITY AVG. OF 3 MODELS USING MOENCH, HANTUSH (NO STOR.), AND COOPER-JACOB SOLUTION METHODS. AQUIFER THICKNESS REPORTED AS 1225 FT BY J HERR (UNABLE TO UPDATE DATABASE -CB)	742	942	UFA
sfwmd041	27.54420	-80.71145	NAD27	FL	OKEECHOBEE	20,786		SINGLE WELL RECOVERY TEST	218	666	UFA
sfwmd134	28.37880	-81.58774	unk	FL	ORANGE	18,428		INTERVAL TEST #2 OF 2 SPECIFIC CAPACITY: 68 GPM/FT TDS: 160 MG/L	1170	1280	FAS
sjrwmd122	28.51891	-81.21017	unk	FL	ORANGE	135,993		Distance-Drawdown Method	1045	1190	FAS
sjrwmd291	28.37112	-81.38313	unk	FL	ORANGE	412,500		Data compiled in USGS WRIR 02-4036, data originally from, BOYLE ENGINEERING CORP	1100	1690	FAS
sjrwmd072	28.56500	-81.37313	unk	FL	ORANGE	668,000	0.002	Data compiled in USGS WRIR 02-4036, data originally from, SZELL	947	1445	FAS
sjrwmd022	28.38195	-81.28229	unk	FL	ORANGE	89,000		Data compiled in USGS WRIR 02-4036, data originally from, BARNES, FERLAND & ASSOC, INC	1045	1450	FAS
sfwmd129	28.37880	-81.58774	unk	FL	ORANGE	63,686		INTERVAL TEST #1 OF 2 SPECIFIC CAPACITY: 235 GPM/FT TDS: 134 MG/L	220	715	FAS
sjrwmd067	28.73555	-81.53757	unk	FL	ORANGE	460,000		Data compiled in USGS WRIR 02-4036, data originally from, BOYLE ENGINEERING CORP	859	1303	FAS
sjrwmd069	28.63722	-81.49091	unk	FL	ORANGE	625,000		Data compiled in USGS WRIR 02-4036, data originally from, POST, BUCKLEY, SHUH & JERNIGAN, INC	1037	1455	FAS
sjrwmd070	28.45639	-81.47757	unk	FL	ORANGE	322,500		Data compiled in USGS WRIR 02-4036, data originally from, LEGGETTE, BRASHEARS & GRAHAM, IN	997	1742	FAS
sjrwmd071	28.62861	-81.39896	unk	FL	ORANGE	82,000		Data compiled in USGS WRIR 02-4036, data originally from, BARNES, FERLAND & ASSOC, INC	850	1350	FAS
sjrwmd074	28.51417	-81.32840	unk	FL	ORANGE	650,000		Data compiled in USGS WRIR 02-4036, data originally from, BARNES, FERLAND & ASSOC, INC	1060	1462	FAS
sfwmd131	28.39612	-81.54146	unk	FL	ORANGE	78,866	0.0016	WELL C	237	910	FAS

usgs258	28.53333	-81.33333	unk	FL	ORANGE	575,000	0.00000007		1063	1247	LFA
sjrwmd068	28.59889	-81.50202	unk	FL	ORANGE	197,500		Data compiled in USGS WRIR 02-4036, data originally from, YOVAISH ENGINEERING SCIENCES, INC	1192	1450	LFA
usgs296	28.41367	-81.58500	NAD83	FL	ORANGE	120,000		USGS files (Orlando, FL). Thickness of aquifer tested, 212 ft.			UFA
sjrwmd024	28.34778	-81.22534	unk	FL	ORANGE	7,859		SHAW, J.E. AND S.M. TROST. 1984. HYDROGEOLOGY OF THE KISSIMMEE PLANNING AREA, SFWMD TP 84-1. TRANSMISSIVITY ESTIMATED FROM CORRECTED SPECIFIC CAPACITY = 30.22 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 10.59 FT	373	463	UFA
sfwmd132	28.42556	-81.13201	NAD27	FL	ORANGE	64,400	0.01	TRANSMISSIVITY, STORATIVITY, AND LEAKANCE OBTAINED FROM AVERAGE OF 3 OBSERVATION WELLS; ALL LISTED IN ANALYSIS INFO	244	509	UFA
sjrwmd121	28.42528	-81.09479	NAD27	FL	ORANGE	750,000	0.00007	Transmissivity value taken from observation well.	285	490	UFA
sfwmd130	28.42556	-81.16562	unk	FL	ORANGE	59,484	0.00063	WELL B	226	300	UFA
sjrwmd079	28.47176	-81.53471	unk	FL	ORANGE	40,651	0.0024		106	650	UFA
usgs293	28.44767	-81.11178	NAD83	FL	ORANGE	210,000	0.00007	Tibbals and Frazee (1976). Thickness of aquifer tested, 205 ft.			UFA
usgs291	28.59933	-81.49900	NAD83	FL	ORANGE	61,000	0.0007	Lichtler and others (1968). Thickness of aquifer tested, 262 ft.			UFA
sfwmd133	28.40362	-81.07951	NAD27	FL	ORANGE	550,000	0.0009	TRANSMISSIVITY FROM PW = 3814800 GAL/D FT	275	600	UFA
usgs292	28.53467	-81.38267	NAD83	FL	ORANGE	55,000	0.0007	Lichtler and others (1968). Thickness of aquifer tested, 212 ft.			UFA
sjrwmd073	28.53195	-81.36840	NAD27	FL	ORANGE	80,000	0.0014	SFWMD TECHPUB 84-1	77	364	UFA
usgs295	28.42167	-81.14900	NAD83	FL	ORANGE	74,000	0.0003	Lichtler and others (1968). Thickness of aquifer tested, 509 ft.			UFA
usgs294	28.39900	-81.10738	NAD83	FL	ORANGE	510,000		Tibbals and Frazee (1976). Thickness of aquifer tested, 328 ft.			UFA
sfwmd155	28.25656	-81.50380	unk	FL	OSCEOLA	69,106	0.000022		370	680	FAS
sjrwmd020	28.09446	-81.29121	unk	FL	OSCEOLA	137,990	0.0007	Leakance calculated using the Hantush-Jacob method	1020	1500	FAS
sjrwmd298	28.27973	-81.59841	NAD27	FL	OSCEOLA	16,000	0.011	Penetrates 360 ft of FAS. No additional data available.			FAS
sfwmd159	28.25656	-81.50380	unk	FL	OSCEOLA	200,535	0.000012		1210	1500	LFA
sfwmd158	27.65833	-81.13300	unk	FL	OSCEOLA	78,877		THIS TEST WAS CONDUCTED IN A HIGHLY FRACTURED INTERVAL. THE MAXIIMUM AVAILABLE PUMPING RATE WAS INADEQUATE TO PRODUCE SIGNIFICANT DRAWDOWN IN THE PRODUCTION ZONE MONITOR WELL, AND THE RECOVERY DATA FROM THE PRODUCTION WELL WAS OSCILLATORY AND NEAR INSTAN	930	1202	MCU
sjrwmd025	28.02835	-81.19062	NAD27	FL	OSCEOLA	13,725	0.00023	SFWMD David Butler APT	343	670	UFA

sfwmd144	27.80305	-81.19828	unk	FL	OSCEOLA	5,688		CORRECTED SPECIFIC CAPACITY = 23.34 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 20.35 FT SINGLE WELL RECOVERY TEST	172	880	UFA
sfwmd145	28.09446	-81.29121	unk	FL	OSCEOLA	52,525	0.0006	RECOMMENDED PARAMETERS OF AVERAGES GIVEN IN REPORT REFERENCED ABOVE. TRANSMISSIVITY RANGED BETWEEN 48,375 AND 56,674; STORATIVITY RANGED BETWEEN .0003 AND .0009; LEAKANCE RANGED BETWEEN .000003 AND .000038	185.89	533.89	UFA
sfwmd149	27.74098	-81.06330	unk	FL	OSCEOLA	53,590		DISCHARGE IS AVERAGE OF 500, 900, 1300, AND 1833 GPM DISCHARGE RATES, TRANSMISSIVITY IF BASED ON SPECFIC CAPACITY AND AVERAGED	289	844	UFA
sfwmd150	27.74098	-81.06330	unk	FL	OSCEOLA	242,000	0.00101	VALUES BASED ON TWO APT TESTS USING HANTUSH-JACOB TYPE CURVE SOLUTION (1955) AND DISTANCE-DRAWDOWN (COOPER-JACOB 1946) TRANSMISSIVITY AVERAGE OF 172,500 FT2/D AND 311,500 FT2/D STORATIVITY AVERAGE OF 1.18 E-03 AND 8.31 E-04 LEAKANCE AVERAGE OF 1.59 E-02 A	289	844	UFA
sjrwmd078	27.69725	-80.89645	NAD27	FL	OSCEOLA	16,929	0.00023	SFWMD David Butler	325	590	UFA
sfwmd142	28.25656	-81.50380	unk	FL	OSCEOLA	15,583	0.000022		110	260	UFA
sfwmd139	28.33419	-81.63358	unk	FL	OSCEOLA	24,350	0.0007545	HANTUSH-JACOB ANALYSIS METHOD USED FOR PARAMETER. WELLS OSF-103,OSS-101, & OSS-102 WERE USED AS MONITOR WELLS DURING THE TEST	67	150	UFA
sjrwmd077	27.90070	-81.04486	NAD83	FL	OSCEOLA	17,044	0.00013	SFWMD David Butler APT	260	630	UFA
sfwmd143	28.14001	-81.35062	unk	FL	OSCEOLA	43,695		CORRECTED SPECIFIC CAPACITY = 119.4 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 7.01 FT SINGLE WELL RECOVERY TEST	160	980	UFA
swfwmd012	28.28150	-81.58260	unk	FL	OSCEOLA	16,040	0.011	No additional data available.			UFA
sfwmd153	27.65833	-81.13300	unk	FL	OSCEOLA	11,424	0.0055		330	550	UFA
sfwmd157	28.11557	-81.00784	unk	FL	OSCEOLA	274,950	0.002	APT	700	900	UFA
sjrwmd021	28.09446	-81.29121	unk	FL	OSCEOLA	53,857	0.000235	Transmissivity :Average of Cooper-Jacob Time drawdown method and Hantush-Jacob Leaky Aquifer Method; Storativity: Average of Cooper-Jacob Time drawdown method and Hantush Jacob Leaky Aquifer Method; Leakance: Average of Hantush-Jacob Leaky Aquifer Method	252	640	UFA
sjrwmd019	28.25236	-81.32820	NAD83	FL	OSCEOLA	159,681	0.0404	SFWMD David Butler APT	130	470	UFA
sfwmd152	28.17335	-81.13145	unk	FL	OSCEOLA	3,708	0.00006	APT	330	630	UFA
sjrwmd023	28.07196	-81.26757	NAD27	FL	OSCEOLA	10,000	0.00033	SFWMD David Butler APT	310	610	UFA

sfwmd196	26.67610	-80.10286	unk	FL	PALM BEACH	198,500	0.00085	SITE MAP IS ON SERVER B1HOME1\LYTAL SITE MAP*.TIF PUMPED WELL WAS PBF-6 ULTIMATELY COMPLETED IN THIS MIDDLE FLORIDAN FLOW ZONE. PBF-6 ALSO USE TO PUMP UPPER FLORIAN INTERVAL IN APT-1	1360	1510	FAS
sfwmd187	26.74826	-80.68232	unk	FL	PALM BEACH	15,854	0.00011	TEST WAS CONDUCTED POST ACIDIFICATION OF THE WELLS. THE MONITOR WELL, TP-2, WAS ALSO PUMPED AT A CONSTANT RATE OF 50 GPM DURING THE TEST. RESULTS ARE BASED ON HANTUSH & JACOB (1955) METHOD FOR A LEAKY CONFINED AQUIFER. SALINITY FROM THE TESTED INTERVAL	1150	1450	FAS
sfwmd183	26.93284	-80.13393	unk	FL	PALM BEACH	6,436	0.0004	RECOMMENDED VALUE BASED ON HANTUSH-JACOB METNOD FOR WELLS RO-2 & RO-4. REPORT DATE USED FOR DATE OF TEST.	1073	1500	FAS
sfwmd181	26.70056	-80.37641	unk	FL	PALM BEACH	221,925	0.0004	COMPOSITE TEST OF UF AND AVON PARK PERMEABLE ZONE OF THE FLORIDAN AQUIFER SYSTEM. RECOMMENDED PARAMETERS ARE AVERAGE OF HANTUSH-JACOB RESULTS FROM MONITOR WELLS FPL_FAW1 & FPL_FAW3. HIGH LEAKANCE IS PROBABLY DUE TO MULTIPLE AQUIFER PENETRATION.	1063	1490	FAS
sfwmd218	26.69958	-80.71594	unk	FL	PALM BEACH	68,306	0.000026	DUAL ZONE PUMPING WELL PBF-9 USED AS PRODUCTION WELL HERE. FINAL COMPLETION OF PBF-9 LEFT AS STATED HERE AND USED AS MONITOR WELL WITH DATALOGGER.	1960	2040	LFA
sfwmd197	26.92339	-80.15616	unk	FL	PALM BEACH	37,940	0.0001	HIGHER CHLORIDE CONCENTRATIONS FOUND IN UPPER FAS HIGHER PRODUCTIVITY AND BETTER WATER QUALITY IN DEEPER FAS	1451	1665	MCU
sfwmd193	26.86053	-80.09991	unk	FL	PALM BEACH	22,730		T FROM RECOVERY DATA 37000 FT2/D CONSIDERED TOO HIGH. SPECIFIC CAPACITY IN RANGE 22 TO 43 GPD/FT	1300	1600	MCU
sfwmd189	26.61424	-80.06973	unk	FL	PALM BEACH	87,414	0.0002	RECOMMENDED VALUES FROM HANTUSH-JACOB LEAKY AQUIFER METHOD	1220	1484	MCU
sfwmd188	26.69958	-80.71594	unk	FL	PALM BEACH	9,634	0.00029	TWO MONITOR WELLS, ONE IN UPPER THE OTHER IN LOWER FLORIDAN FLOW ZONES. PBF-7 WAS PUMPING WELL FOR 2 APT'S. FIRST DRILLED AND PUMPED IN UPPER FLORIDAN FLOW ZONE THEN DRILLED DOWN TO LOWER FLORIDAN, COMPLETED AND PUMPED FOR APT2. THUS THE SAME PRODUCTION W	1202	1447	MCU

sfwmd178	26.69680	-80.03618	unk	FL	PALM BEACH	2,811		SPECIFIC CAPACITY = 56.82 GPM/FT AT 60 MIN. TRANSMISSIVITY ESTIMATED FROM COOPER-JACOB ANALYSIS METHOD DERIVED FROM SPECIFIC CAPACITY.	1052	1267	UFA
sfwmd179	26.69680	-80.03618	unk	FL	PALM BEACH	1,878		SPECIFIC CAPACITY = 42.20 GPM/FT FOR 60 MIN. TRANSMISSIVITY ESTIMATED FROM COOPER-JACOB ANALYSIS METHOD DERIVED FROM SPECIFIC CAPACITY.	1052	1267	UFA
sfwmd177	26.67610	-80.10286	unk	FL	PALM BEACH	34,300	0.0036	SITE MAP STORED ON DISTRICT SERVER B1 HOME1\LYTAL SITE MAP*.TIF R/B = 0.248 USING THE HANTUSH (1956) METHOD	1050	1250	UFA
sfwmd175	26.57300	-80.05335	unk	FL	PALM BEACH	2,202		DATE OF TEST IS DATE OF REPORT DISCHARGE RATE IS AVERAGE OF 842 GPM, 1542 GPM, 2275 GPM TRANSMISSIVITY IF AVERAGE OF DRAWDOWN AND RECOVERY DATA AT DIFFERENT DISCHARGE RATES	1035	1200	UFA
sfwmd174	26.41007	-80.06698	unk	FL	PALM BEACH	13,182		VALUES ARE AVERAGE OF PUMPED AND RECOVERY DATA ANALYSIS METHOD: COOPER-JACOB TDS: 6600 MG/L	1027	1200	UFA
sfwmd172	26.35531	-80.29509	unk	FL	PALM BEACH	8,214	0.000098	TRANSMISSIVITY AND STORATIVITY ESTIMATED USING HANTUSH (1960). OTHER ANALYTIC METHODS USED WERE THEIS (1935) WHICH YIELDED T=83470 GPD/FT AND ST=.00009776 AND MOENCH (1985) WHICH YIELDED T=75830 AND ST=.0001147 BUT HANTUSH WAS THE METHOD THAT APPEARS TO B	1015	1225	UFA
sfwmd169	26.41043	-80.06560	unk	FL	PALM BEACH	17,769	0.0598	RECOMMENDED T IS AN AVERAGE OF VALUES CALCULATED FROM THE PUMPING AND RECOVERY DATA (RANGE: 14,547 F2/D - 21,540 FT2/D). TDS = 7,280 MG/L. SPECIFIC CAPACITY = 112 GPM/FT.	1010	1200	UFA
sfwmd166	26.57268	-80.05269	unk	FL	PALM BEACH	1,437		DATE OF TEST IS DATE OF REPORT DISCHARGE RATE IS AVERAGE OF 842 GPM, 1542 GPM, 2275 GPM TRANSMISSIVITY IF AVERAGE OF DRAWDOWN AND RECOVERY DATA AT DIFFERENT DISCHARGE RATES	990	1293	UFA
sfwmd165	26.71673	-80.06338	unk	FL	PALM BEACH	108,000	0.0008	RECOVERY WAS ALLOWED FOLLOWING STEP TEST OF ASR-1, PRIOR TO INITIAION OF MULTI-WELL TEST. LARGE DEVIATION FROM THEIS CURVE DURING LATE TIME, BUT LEAKY AQUIFER SOLUTION NOT USED.	985	1200	UFA
sfwmd161	26.51424	-80.06254	unk	FL	PALM BEACH	9,900		TRANSMISSIVITY VALUE 6800-13000, AVERAGE LISTED ABOVE	804	900	UFA

sfwmd180	26.69680	-80.03618	unk	FL	PALM BEACH	2,292		SPECIFIC CAPACITY = 42.02 GPM/FT FOR 60 MIN. TRANSMISSIVITY ESTIMATED FROM COOPER-JACOB ANALYSIS METHOD DERIVED FROM SPECIFIC CAPACITY.	1052	1267	UFA
sfwmd238	26.48341	-80.13616	unk	FL	PALM BEACH	8,943		TRANSMISSIVITY WAS ESTIMATED DUE TO LIMITED AMOUNT OF DATA FOR ASR ZONE. THE 72-HOUR APT WAS ABSENT. THE SPECIFIC CAPACITY RATES RANGED FROM 25.2 GPM/FT AT 2100 GPM TO 47.8GPM/FT AT 530 GPM. WELL WAS PUMPED FOR 1.5 HOURS AT EACH RESPECTIVE PUMPING RAT		1155	UFA
sfwmd185	26.86459	-80.05413	unk	FL	PALM BEACH	27,138			1075	1237	UFA
sfwmd186	26.86459	-80.05413	unk	FL	PALM BEACH	21,715			1075	1237	UFA
sfwmd184	26.86459	-80.05413	unk	FL	PALM BEACH	37,049			1075	1237	UFA
sfwmd239	28.41118	-82.44473	unk	FL	PASCO	50,267	0.0003	2 tests were made for confirmation; rain hindered the test and the data were not corrected for regional fluctuations:Tested Formation -Tp-S-Oc-AP	72	625	UFA
swfwmd181	28.25430	-82.59310	unk	FL	PASCO	38,770	0.00026	No apparent corrections were made to background barometric or tidal flux; surf. aquifer also monitored; total test ran for 120 hrs, but last 10 hrs of test invalid due to pump failure; Jacob-Hantush leaky aquifer method used (1955); L value could not be c	181	905	UFA
usgs299	28.44767	-82.22600	NAD83	FL	PASCO	40,000		Pride and others (1966). Thickness of aquifer tested, 190 ft.			UFA
swfwmd049	28.36880	-82.19680	unk	FL	PASCO	300,000		Partial penetration; estimation based on 16 production wells (indiv. pumpage unknown); pumpage increased from 3mgd to 25mgd & T was calculated from this increase in an ob. Well near center of pumpage. Value is average of low and high estimates.			UFA
swfwmd048	28.28050	-82.41130	unk	FL	PASCO	49,500	0.0012	T, S & L values are log. avgs.; aquifer coefficients are avgs. based on 7 diff. pumping tests on wells C-1, C-2 (data presented), C-3, C-8, C-9 & C-10 (incl. combinations); testing on C-2 considered the best; all corrections made; obs. wells open to same	118	700	UFA
usgs024	28.40306	-82.45343	NAD27	FL	PASCO	115,000	0.0004	Data adjusted for regional trends; 2 tests made for confirmation; rain hindered test.	152	700	UFA
swfwmd046	28.22070	-82.37800	unk	FL	PASCO	27,126	0.001	Drawdowns corrected for barometric & regional fluctuations; typical dry season water level trend; minor precipitation occurred during test.	174	608	UFA
usgs304	28.29967	-82.38617	NAD83	FL	PASCO	39,000	0.0012	USGS files (Tampa, FL). Thickness of aquifer tested, 610 ft.			UFA
swfwmd027	28.23570	-82.44330	unk	FL	PASCO	28,342	0.001	No data available; values obtained from Plate 12 following pg. C-22, Vol. II of referenced report.			UFA

swfwmd018	28.28070	-82.06360	unk	FL	PASCO	21,390	0.00013	No additional data available.			UFA
usgs025	28.36195	-82.47676	NAD27	FL	PASCO	50,000	0.0003	Data adjusted for regional trends; 2 tests made for confirmation; rain hindered test.	152	700	UFA
swfwmd047	28.20870	-82.37780	unk	FL	PASCO	56,530	0.00068	Drawdowns corrected for barometric & regional fluctuations; typical dry season water level trend; minor precipitation occurred during test; ROMP 85 used to monitor background levels.	130	715	UFA
swfwmd180	28.25470	-82.55980	unk	FL	PASCO	60,695	0.0024	Aquifer penetration depth averaged from 2 values reported; no significant interferences; avg. T value from 2 ob. wells; tidal & regional effects NOT accounted for; surf. aquifer also monitored.	185		UFA
sjrwmd297	28.22287	-82.49348	unk	FL	PASCO	70,000	0.0057	Penetrates 510 ft of FAS. No additional data available.			UFA
swfwmd173	28.18515	-82.52196	unk	FL	PASCO	73,000	0.0014	Drawdown & recovery analyzed using Walton curve-matching, Hantush inflection-point, Theis's recovery methods.	126	703	UFA
swfwmd172	28.17844	-82.51195	unk	FL	PASCO	68,000	0.0018	Drawdown & recovery analyzed using Walton curve-matching, Hantush inflection-point, Theis's recovery methods.	89	703	UFA
swfwmd171	28.19330	-82.51030	unk	FL	PASCO	47,000	0.00515	T & S values represent log. avg.; L value could not be confirmed.			UFA
swfwmd062	28.38298	-82.47729	unk	FL	PASCO	47,459	0.0005	Data adjusted for regional trends; 2 tests made for confirmation; rain hindered test.	154	485	UFA
swfwmd064	28.22210	-82.36210	unk	FL	PASCO	52,353	0.00061	Drawdowns corrected for barometric & regional fluctuations; initial test aborted due to mounding caused by discharge of water near APT; discharge subsequently routed farther away from test site.	186	715	UFA
swfwmd170	28.18580	-82.53210	unk	FL	PASCO	85,300	0.00078	Drawdown and Recover monitoried in eleven wells; Analysis of anisotropy performed - Major axis of T N 4.1 degrees W; Te = 85,300 ft2/day, T (major) = 143,000 ft2/day, T(minor) = 51,200 ft2/day; T ratio is 2.79.	89	703	UFA
swfwmd079	28.25100	-82.32920	unk	FL	PASCO	18,717	0.0013	Ob. well depth represents avg. value of estimated values reported (600-900'); mon. well construction unknown; surf. aquifer also monitored; background trends were corrected.	82	698	UFA
swfwmd100	28.17910	-82.50930	unk	FL	PASCO	71,000	0.001	No data correction applied due to lack of control wells in area; anisotropic aquifer; T value represents eff. T (Tx/Ty = 2.5); no L value determined from short duration test; other 2 OB wells located at 3710' & 4310' rad.	45	707	UFA

swfwmd101	28.17910	-82.50930	unk	FL	PASCO	68,000	0.0008	No data correction applied due to absence of control wells in area; anisotropic aquifer indicated by variation in OB well drawdown data; T value represents eff. T (Tx/Ty = 2.1); no L value calculated due to short duration of test; 3 other OB wells at 4730	78	704	UFA
swfwmd102	28.19330	-82.51030	unk	FL	PASCO	51,000	0.0006	Total duration incl. recovery time; no data correction applied due to absence of control wells in area; anisotropic aquifer indicated by variation in OB well drawdown; T value represents eff. T (Tx/Ty = 3.5); other 2 ob. wells at 1794' & 2751' rad.	59	702	UFA
usgs305	28.26500	-82.40800	NAD83	FL	PASCO	49,000	0.0012	USGS files (Tampa, FL). Thickness of aquifer tested, 490 ft.			UFA
usgs307	28.25500	-82.65883	NAD83	FL	PASCO	33,000	0.0004	USGS files (Tampa, FL). Thickness of aquifer tested, 210 ft.			UFA
usgs303	28.41350	-82.45067	NAD83	FL	PASCO	130,000		USGS files (Tampa, FL). Thickness of aquifer tested, 410 ft.			UFA
sjrwmd080	28.10762	-82.69052	unk	FL	PINELLAS	40,000	0.0009	No additional data available.			FAS
sfwmd240	27.87975	-82.80527	unk	FL	PINELLAS	0	0.00031	TRANSMISSIVITY ESTIMATED FROM HORIZONTAL CONDUCTIVITY (K) AND TESTED INTERVAL. VALUES ARE FROM NUMERICAL MODEL USING USGS COMPUTER MODEL CODE HST3D (KIPP 1987).	35	135	IC
sfwmd254	27.82530	-82.74346	unk	FL	PINELLAS	2,500			2000	2260	LFA
swfwmd258	27.98880	-82.75420	unk	FL	PINELLAS	33,400	0.0004	No data available; values obtained from Plate 12 following pg. C-22, Vol. II of referenced report.			UFA
swfwmd052	28.10700	-82.67460	unk	FL	PINELLAS	47,193	0.00019	Regional water level & barometric flux were monitored prior to test start; correction applied to regional pot. surface due to pretest precipitation conditions; Jacob-Hantush leaky artesian aquifer analytical method (1955) as modified by Cooper (1963), & J	250	450	UFA
swfwmd195	27.92860	-82.80470	unk	FL	PINELLAS	28,449	0.00094	Data corrected for regional trends, barometric changes & tidal effects; hydraulic parameters reported could not be confirmed.	58	303	UFA
sfwmd250	27.87975	-82.80527	unk	FL	PINELLAS	37,500	0.000086	TRANSMISSIVITY ESTIMATED FROM HORIZONTAL CONDUCTIVITY (K) AND TESTED INTERVAL. VALUES ARE FROM NUMERICAL MODEL USING USGS COMPUTER MODEL CODE HST3D (KIPP 1987). FROM LOWER ZONE A - INPUT PARAMETERS VARIED BETWEEN THE TWO OUTPUTS REPRESENTING LOWER ZONE A.	300	350	UFA

sfwmd248	27.87975	-82.80527	unk	FL	PINELLAS	250	0.000043	TRANSMISSIVITY ESTIMATED FROM HORIZONTAL CONDUCTIVITY (K) AND TESTED INTERVAL. VALUES ARE FROM NUMERICAL MODEL USING USGS COMPUTER MODEL CODE HST3D (KIPP 1987).	275	300	UFA
sfwmd245	27.87975	-82.80594	unk	FL	PINELLAS	1,350		SPECIFIC CAPACITY = 5.1 GPM/FT	205	235	UFA
sjrwmd280	27.82503	-82.74288	NAD27	FL	PINELLAS	1,200,000	0.00022	Penetrates only AP limestone (non-potable in this area); monitored both upper & lower zones; no corrections applied; deep well injection site; used Hantush-Jacob type curve (1955) for analysis.	953	1072	UFA
sfwmd243	27.87975	-82.80594	unk	FL	PINELLAS	1,870		SPECIFIC CAPACITY = 7.0 GPM/FT.	135	235	UFA
swfwmd177	27.79810	-82.68820	unk	FL	PINELLAS	1,203,210	0.0002	Wells penetrate only AP fmn. (non-potable in this area); monitored both upper & lower zones; no corrections applied; deep well injection site.	921	1121	UFA
sfwmd242	27.87975	-82.80594	unk	FL	PINELLAS	1,675		SPECIFIC CAPACITY = 6.3 GPM/FT.	135	185	UFA
sfwmd241	27.87975	-82.80527	unk	FL	PINELLAS	2,520	0.00026	TRANSMISSIVITY ESTIMATED FROM HORIZONTAL CONDUCTIVITY (K) AND TESTED INTERVAL. VALUES ARE FROM NUMERICAL MODEL USING USGS COMPUTER MODEL CODE HST3D (KIPP 1987).	135	275	UFA
swfwmd028	28.08230	-82.70290	unk	FL	PINELLAS	6,465	0.0000872	Short term test (6 hours), No data correction. Data analysis included Cooper-Jacob and Theis solutions	190	240	UFA
swfwmd066	28.15120	-82.65790	unk	FL	PINELLAS	58,800	0.0014	Short duration test; no data corrections applied; moderate regional water-level flux; partial penetration; lower zones also monitored; test duration incl. recovery time; L value is assumed to be less than value reported.	59	300	UFA
sjrwmd281	27.87836	-82.84399	NAD27	FL	PINELLAS	900,000	0.0008	Penetrates only AP limestone (non-potable in this area); monitored both upper & lower zones; no corrections applied; deep well injection site; used Hantush-Jacob type curve (1955) for analysis.	940	1028	UFA
swfwmd188	28.15120	-82.65790	unk	FL	PINELLAS	40,107	0.00037	Regional water level & barometric flux were monitored prior to test start; correction made for regional pot. surface decline from APT drawdown data; Jacob-Hantush leaky aquifer analytical method (1955) as modified by Cooper (1963), & Jacob's & Chow's stra	74	210	UFA
sfwmd252	27.87975	-82.80527	unk	FL	PINELLAS	200	0.000026	TRANSMISSIVITY ESTIMATED FROM HORIZONTAL CONDUCTIVITY (K) AND TESTED INTERVAL. VALUES ARE FROM NUMERICAL MODEL USING USGS COMPUTER MODEL CODE HST3D (KIPP 1987).	350	550	UFA

swfwmd241	28.16580	-82.65950	unk	FL	PINELLAS	108,957	0.0033	Regional water level & barometric flux were monitored prior to test start; correction made for regional pot. surface decline from APT drawdown data; Jacob-Hantush leaky aquifer analytical method (1955) as modified by Cooper (1963), & Jacob's & Chow's stra	183	647	UFA
swfwmd250	27.97361	-82.76611	unk	FL	PINELLAS	4,680	0.00011	Upper & lower zones also monitored; drawdown & recovery data analyzed using Cooper & Jacob methods.	234	302	UFA
swfwmd251	28.02890	-82.70370	unk	FL	PINELLAS	27,059		Short term Packer Secific Capacity tests/ Recovery data used in estimations	208	275	UFA
swfwmd252	27.97417	-82.76611	unk	FL	PINELLAS	9,358	0.00019	Upper & lower zones also monitored; drawdown & recovery data analyzed using Cooper & Jacob methods.	76	152	UFA
swfwmd078	27.86111	-82.77500	unk	FL	PINELLAS	25,401		Data analyzed using Walton (1973) method; Estimated values of T only.	225	300	UFA
swfwmd077	27.84111	-82.77056	unk	FL	PINELLAS	16,042		Data analyzed using Walton (1973) method; Estimated values of T only.	220	300	UFA
swfwmd179	27.71270	-82.70340	unk	FL	PINELLAS	29,000	0.0004	T value obtained from analysis of OB well; Hantush-Jacob type curve method used for analysis; analysis of pumped well data from 6 to 270 min. using Jacob's semi-log straight line method confirms T value; S value was calculated from compressibility of core	250	400	UFA
swfwmd075	27.88944	-82.72111	unk	FL	PINELLAS	22,727		Data analyzed using Walton (1973) method; Estimated values of T only.	195	300	UFA
swfwmd178	27.71270	-82.70340	unk	FL	PINELLAS	1,200,000	0.00033	Hydraulic properties, T, S & L values were estimated from test results using the Hantush-Jacob type curve method; S value compares favorably to storativity calc. from avg. rock compressibility data of core samples.	921	1121	UFA
swfwmd156	28.01939	-82.77150	unk	FL	PINELLAS	26,070	0.008	T is log. avg.; monitored tide & regional water level changes before & during test; leakance for upper confining layer = 0.0034 gpd/ft3, lower confining layer = 0.047 gpd/ft3.	51	342	UFA
swfwmd065	28.15160	-82.67650	unk	FL	PINELLAS	34,400	0.0015	Regional trends believed to be minimal; no corrections applied; partial penetration; test duration incl. recovery time; highly permeable dolomite stratum in AP Ls not penetrated by pumping well.	173	380	UFA
swfwmd253	28.00570	-82.76970	unk	FL	PINELLAS	19,415	0.00075	Data corrected for tidal effects; L value represents combined upper & lower confining; used Walton's (1962) & Hantush's (1956(inflection point methods for analysis.	50	180	UFA

swfwmd254	27.86556	-82.73529	unk	FL	PINELLAS	32,620	0.00053	Upper & lower zones also monitored; drawdown & recovery data analyzed using Cooper & Jacob methods.	200	281	UFA
swfwmd255	27.86556	-82.73556	unk	FL	PINELLAS	32,620	0.00042	Upper & lower zones also monitored; drawdown & recovery data analyzed using Cooper & Jacob methods.	100	150	UFA
swfwmd256	28.16390	-82.75490	unk	FL	PINELLAS	34,600	0.0049	Drawdown monitored at four Upper Floridan aquifer wells and one surficial aquifer well; Upper Floridan aquifer monitoring interval within and below the production interval, no apparent regional trend correction; failed attempt for drawdown correction due	67	105	UFA
sfwmd244	27.87975	-82.80594	unk	FL	PINELLAS	1,400		SPECIFIC CAPACITY = 5.2 GPM/FT.	135	235	UFA
swfwmd076	27.85556	-82.71611	unk	FL	PINELLAS	24,064		Data analyzed using Walton (1973) method; Estimated values of T only.	179	316	UFA
sfwmd260	27.78400	-81.95000	unk	FL	POLK	116,310	0.00044	Leakance result is questionable; well pumped for 24 hours, one day before test began; zones above were monitored.:Tested Formation -S-Oc-AP	359	855	FAS
sfwmd258	27.65805	-81.13421	unk	FL	POLK	8,979		CORRECTED SPECIFIC CAPACITY = 33.78 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 13.2 FT SINGLE WELL RECOVERY TEST	260	1000	FAS
sfwmd255	27.78778	-81.55139	unk	FL	POLK	5,014	0.00013	TRANMISSIVITY IS THE AVERAGE OF THE RANGE 18,000-56,000 GPD/FT LEAKANCE IS AN AVERAGE BETWEEN THE RANGES FOR THE LOWERMOST & UPPERMOST REGIONS. K-VALUE WAS AN AVERAGE THAT WAS ASSUMED TO BE HORIZONTAL.	109	205	IA
sjrwmd287	28.15721	-81.56536	unk	FL	POLK	17,492		Variable Rate on APT discharge, Only used first 30 min. of drawdown data (@ 1080 GPM) for analysis; No potentiometric trend data leading into the test period due to transducer removal.	1250	1400	LFA
swfwmd016	28.31340	-81.66450	unk	FL	POLK	193,400		Specific capacity test, Jacob's equation. No recovery analysis.	1685	2230	LFA
swfwmd144	28.15720	-81.56530	unk	FL	POLK	17,493		Variable Rate on APT discharge, Only used first 30 min. of drawdown data (@ 1080 GPM) for analysis; No potentiometric trend data leading into the test period due to transducer removal.	1250	1400	LFA
swfwmd011	28.12110	-81.89750	unk	FL	POLK	96,250	0.0036	Well construction data not presented. T & S are log. avgs. of 2 tests; analytical methods used are Theis' type-curve (1935) and Jacob's semi-log (1950).			UFA
usgs310	27.78333	-81.94833	NAD83	FL	POLK	108,000	0.0008	Wilson and Gerhart (1980). Thickness of aquifer tested, 510 ft.			UFA
usgs300	28.25017	-81.61083	NAD83	FL	POLK	16,000	0.01	Pride and others (1966). Thickness of aquifer tested, 360 ft.			UFA

swfwmd039	27.66730	-81.76810	unk	FL	POLK	149,732	0.0001	Upper zones were also monitored; corrections applied for barometric & regional trends; values represent weighted avg. of all 5 OB wells, all have similar construction.	316	1002	UFA
swfwmd015	27.78990	-81.86740	unk	FL	POLK	595,187	0.0059	Regional trend correction made. Analysis using Hantush - Jacob.	335	834	UFA
swfwmd009	27.78420	-81.94950	unk	FL	POLK	76,070	0.003	T value is log. avg.of 4.9x105 gpd/ft & 6.6x105 gpd/ft; L value is questionable; well pumped for 24 hrs prior to start of test; zones above were monitored.	355	829	UFA
sjrwmd271	28.24166	-81.57499	unk	FL	POLK	5,000		Data were analyzed by the Theis (1935) method, by the family of leaky aquifer type-curves by Cooper (1963), and by the Jacob (1950) recovery method	85	250	UFA
swfwmd176	27.75590	-81.93050	unk	FL	POLK	96,257		No additional data available.			UFA
sjrwmd272	28.25833	-81.82499	unk	FL	POLK	3,900		Data were analyzed by the Theis (1935) method, by the family of leaky aquifer type-curves by Cooper (1963), and by the Jacob (1950) recovery method			UFA
swfwmd032	28.06250	-81.94860	unk	FL	POLK	100,000	0.0009	Data analyzed using composite plot of (r2/t) vs. drawdown; test duration and Q could not be confirmed;T & S values based on values obtained from Lake Parker test.	198	660	UFA
swfwmd031	28.16282	-81.88899	unk	FL	POLK	89,800	0.000137	Drawdown and recovery monitored at seven wells including the production well; data corrected for regional trends; analysis performed using Theis (1935) drawdwon / recovery, Hantush-Jacob (1955), Dennis and Motz (1998)	123	780	UFA
swfwmd030	28.07680	-81.98230	unk	FL	POLK	98,796	0.0015	Ob. well construction similar to prod. well; barometric & regional trends corrected; monitored zones both above & below prod. zone.	250	702	UFA
sjrwmd270	28.22500	-81.82499	unk	FL	POLK	5,300		Jacob (1950) recovery	78	217	UFA
usgs301	28.25167	-81.94017	NAD83	FL	POLK	60,000	0.01	USGS files (Orlando, FL). Thickness of aquifer tested, 142 ft.			UFA
swfwmd029	27.88580	-81.57350	unk	FL	POLK	51,471	0.0047	No recovery data; well open only to lower Floridan; interference from irrigation wells; no correction applied; Q is rough estimate.	800	1063	UFA
swfwmd056	28.10600	-81.91040	unk	FL	POLK	77,300	0.00022	Drawdown and recovery monitored at six wells including the production well; data corrected for regional trends; analysis performed using Theis (1935) drawdwon / recovery, Hantush-Jacob (1955)	300	581	UFA
usgs322	27.89333	-81.81222	NAD83	FL	POLK	60,000	0.0025	Cooper-Jacob (1946) and Hantush-Jacob (1955). L = 1.6e-2/d	95	235	UFA

swfwmd142	27.78510	-81.55570	unk	FL	POLK	49,732	0.0023	Accounted for water-level fluctuations, barometric pressure changes & precipitation effects; used Cooper-Jacob straight-line & Walton curve matching (Kruseman & DeRidder, 1983) for analysis; hydraulic parameters could not be verified.	210	1200	UFA
swfwmd141	27.78494	-81.55583	unk	FL	POLK	4,250	0.00013	Shallower zones monitored; due to interference from surrounding irrigation wells; L value could not be determined; T value represents log. avg. of reported range between 18,000 & 56,000 gpd/ft.	210	250	UFA
usgs321	27.84278	-81.81092	NAD83	FL	POLK	13,000	0.0001	Cooper-Jacob (1946) and Hantush-Jacob (1955). L = 5.4e-5/d	150	310	UFA
swfwmd139	27.82710	-81.60460	unk	FL	POLK	1,300	0.0002	Accounted for regional groundwater level changes; data adjusted for precipitation effects; monitored upper zones; T value is log. avg. of reported end values.	232	402	UFA
swfwmd085	28.16500	-81.88100	unk	FL	POLK	179,144		No data available.	122	780	UFA
swfwmd086	28.25200	-81.65140	unk	FL	POLK	19,900	0.00089	Drawdown monitored at four Floridan Aquifer wells and two surficial aquifer wells; data corrected for regional trends; analysis performed using Hantush-Jacob and DeGlee.	380	520	UFA
swfwmd087	28.34330	-81.66510	unk	FL	POLK	14,243	0.0004	Drawdown monitored at two Floridan Aquifer wells and two surficial aquifer wells; data corrected for regional trends; analysis performed using Hantush-Jacob.	261	502	UFA
sfwmd257	28.03168	-81.46118	unk	FL	POLK	16,575		CORRECTED SPECIFIC CAPACITY = 35.06 GPM/FT DRAWDOWN CORRECTED FOR FRICTION = 9.89 FT SINGLE WELL RECOVERY TEST	178	411	UFA
sfwmd261	28.15678	-81.56525	unk	FL	POLK	16,167	0.00017	AQTESOLV? sofware using Hantush-Jacob (1955) and Theis (1935); No regional correction was made; Low T resulting from sediment infilling of secondary porosity.	450	740	UFA
usgs302	28.17300	-81.91183	NAD83	FL	POLK	70,000	0.006	Pride and others (1966). Thickness of aquifer tested, 510 ft.			UFA
sjrwmd288	28.15721	-81.56536	unk	FL	POLK	16,166	0.00017	AQTESOLV« sofware using Hantush-Jacob (1955) and Theis (1935); No reginal correction was made; Low T resulting from sediment infilling of secondary porosity.	450	740	UFA
swfwmd222	28.04620	-81.76830	unk	FL	POLK	106,951	0.0015	Recovery measured; regional trends not corrected.	105	666	UFA
sjrwmd128	28.24001	-81.66118	unk	FL	POLK	16,000		Average, Data were analyzed by the Theis (1935) method, by the family of leaky aquifer type-curves by Cooper (1963), and by the Jacob (1950) recovery method			UFA
sjrwmd127	28.15862	-81.70590	unk	FL	POLK	14,700		Jacob (1950) recovery	101	425	UFA

sjrwmd130	29.67583	-81.58389	unk	FL	PUTNAM	24,000	0.0008	Hantush and Jacob (1955) leaky-artesian aquifer type-curve matching method modified by Cooper	120	250	UFA
sjrwmd131	29.71583	-81.54639	unk	FL	PUTNAM	59,996	0.001	Leakance expressed as units per day. Thickness of aquifer is 150 ft.		300	UFA
sjrwmd133	29.54303	-81.71119	NAD27	FL	PUTNAM	41,000		Thickness of aquifer is 240 ft.	55	295	UFA
sjrwmd134	29.71774	-81.73925	unk	FL	PUTNAM	37,000	0.00094	Cooper (1963) leaky-aquifer type-curve matching method for nonsteady flow in an infinite leaky aquifer	178	564	UFA
sjrwmd132	29.76111	-81.64250	unk	FL	PUTNAM	17,000		Jacob recovery test	190	260	UFA
sjrwmd135	29.67361	-81.56666	unk	FL	PUTNAM	37,000		Theis recovery	150	452	UFA
sjrwmd136	29.65916	-81.57444	unk	FL	PUTNAM	48,000		Theis recovery	113	547	UFA
sjrwmd137	29.71495	-82.02916	unk	FL	PUTNAM	106,298		Average of data analyzed by Hantush's inflection point method	95	167	UFA
usgs287	29.70650	-81.54867	NAD83	FL	PUTNAM	55,000	0.001	Bently (1977). Thickness of aquifer tested, 430 ft.			UFA
sjrwmd138	29.38250	-81.59222	unk	FL	PUTNAM	17,000	0.00035	Average of Modified Hantush (1960) leaky artesian aquifer solution	96	187	UFA
nwfwmd028	30.44789	-86.86725	unk	FL	SANTA ROSA	7,823		Plot and data only, no analysis or other well documentation.			FAS
nwfwmd029	30.43248	-86.90085	unk	FL	SANTA ROSA	18,716		Plot and data only, no analysis or other well documentation.			FAS
sfwmd018	27.30500	-82.34400	unk	FL	SARASOTA	247,000		TESTED INTERVAL EXTENDS SEVERAL HUNDRED FEET INTO LOWER CONFINING UNIT	950	1800	FAS
sfwmd266	27.30500	-82.34400	unk	FL	SARASOTA	310		TEST CONDUCTED WITHIN THE LOWER IAS. HORIZONTAL K-VALUE WAS CALCULATED AND BASED ON THE RESULTS OF THE DRAWDOWN	230	290	IA
sfwmd265	27.07589	-82.14898	unk	FL	SARASOTA	6,374	0.00028	NO DATA CORRECTION FOR REGIONAL TRENDS. MULTIPLE AQUIFERS MONITORED WITH NO SIGNIFICANT WATER LEVEL CHANGES INDICATING AQUIFERS HYDRAULICALLY DISCONNECTED. PRODUCING ZONE 3 OF THE INTERMEDIATE AQUIFER SYSTEM.	190	320	IA
sfwmd264	27.18900	-82.47200	unk	FL	SARASOTA	14,325	0.000058	UPPER IAS. THE TRANSMISSIVITY AND STORATIVITY ARE AVERAGES BETWEEN THE THEIS AND JACOB-HANTUSH METHODS. THE REPORT DID NOT DISCLOSE ANY KNOWN HORIZONTAL OR VERTICAL HYDRAULIC K-VALUES.	75	125	IA
swfwmd257	27.10106	-82.44183	unk	FL	SARASOTA	15,374	0.00064	No data corrections applied due to minimal regional water level changes; response in OB well slow & insignificant; 2 of city's RO wells caused interference; hydraulic parameters represent log. avgs. of 4 analytical methods.	221	456	IA

sfwmd267	27.18900	-82.47200	unk	FL	SARASOTA	11,254	0.0000702	LOWER IAS. THE TRANSMISSIVITY AND STORATIVITY ARE AVERAGES OF THE JACOB-COOPER METHOD. THE K-VALUE IS AN AVERAGE THAT IS ASSUMED TO BE VERTICAL.	250	370	IA
usgs149	27.38310	-82.33120	NAD27	FL	SARASOTA	1,900	0.0014	Partial penetration; wells opened to both Intermediate & Floridan aquifers; little data available.	91	440	IA-UFA
swfwmd199	27.09283	-82.43593	NAD27	FL	SARASOTA	17,900	0.00013	Test duration incl. recovery; no data correction applied fro regional trends, however test duration was short; pumped well tapped both Intermediate & Floridan Aquifers; Floridan highly stratified; OB well monitored shallower zone; T, S & L values are repr	200	650	IA-UFA
swfwmd125	27.18910	-82.47230	unk	FL	SARASOTA	20,456	0.0001426	Used distance-drawdown, Theis' type-curve & Hantush-Jacob methods for analysis; T, S & L values are log. avgs. of several analyses' results.	500	840	UFA
swfwmd154	27.36520	-82.55680	unk	FL	SARASOTA	35,428	0.00065	Construction details of OB well unknown but reported similar to pumped well; no measurements in test well; good recovery data; no data corrections applied; results may be low due to small OB well radius & partial penetration.	246	649	UFA
usgs019	26.95478	-82.34732	NAD27	FL	SARASOTA	4,581	0.0000695	PARAMETERS DETERMINED USING AUTOMATED THEIS CURVE MATCHING PROGRAM	450	850	UFA
usgs021	27.07634	-82.14901	NAD83	FL	SARASOTA	7,260	0.000276	DRAWDOWN ONLY. NO CORRECTIONS FOR REGIONAL TRENDS.:TESTED FORMATION -S	545	860	UFA
swfwmd124	27.18660	-82.13070	unk	FL	SARASOTA	23,100	0.00057	Results low poss. due to small OB well radius; results are combination of 3 indiv. zone tests; upper zone monitored; partial penetration; L value not calculated from this test, used from previous test in the area by Geraghty & Miller, 1978.	57	520	UFA
swfwmd148	27.15820	-82.39310	unk	FL	SARASOTA	13,300		Corrections applied for prevailing tidal effects, local pumping, barometric pressure changes & test well development.	510	700	UFA
usgs026	26.95478	-82.34732	NAD27	FL	SARASOTA	78,604	0.0000007	No additional data available.	1040	1800	UFA
swfwmd108	27.06867	-82.36676	NAD27	FL	SARASOTA	67,000		No additional data available.	1102	1605	UFA
swfwmd126	27.31211	-82.33658	NAD83	FL	SARASOTA	247,000	0.000012	L value from ROMP intranet site; S value could not be confirmed; aquifer thickness calculated by dividing reported T by reported horiz. conductivity (343 ft/day); used Cooper-Jacob & Hantush-Jacob methods for analysis; corrections made for local pumping,	940	1685	UFA

swfwmd127	27.31211	-82.33658	NAD83	FL	SARASOTA	7,517	0.0003	L value from ROMP intranet site; S value could not be confirmed; T value calculated by multiplying open interval (226') by reported kh (33.26 ft/day); used Cooper-Jacob & Hantush-Jacob methods for analysis; corrections made for local	409	635	UFA
usgs018	26.95478	-82.34732	NAD27	FL	SARASOTA	1,016	0.0062	PARAMETERS DETERMINED USING AUTOMATED THEIS CURVE MATCHING PROGRAM	450	700	UFA
swfwmd194	27.20350	-82.48990	unk	FL	SARASOTA	29,238	0.0009	T & S values represent avg. of 3 analytical methods; L value calculated using Cooper (1963) curve matching method; background water levels were monitored; no data corrections applied.	330	660	UFA
sfwmd268	27.30500	-82.34400	unk	FL	SARASOTA	4,324			390	620	UFA
usgs020	26.95478	-82.34732	NAD27	FL	SARASOTA	41,441	0.0000036	PARAMETERS DETERMINED USING AUTOMATED THEIS CURVE MATCHING PROGRAM	450	1600	UFA
swfwmd198	27.07256	-82.38454	NAD27	FL	SARASOTA	24,000		No additional data available.	1388	1705	UFA
swfwmd023	27.16033	-82.40232	NAD27	FL	SARASOTA	300,000		No additional data available.	1599	1915	UFA
sfwmd269	27.31227	-82.33620	unk	FL	SARASOTA	9,626	0.0003	ANALYSIS METHOD: COOPER-JACOB AND JACOB-HANTUSH ACCOUNTED FOR WATER LEVEL CHANGES CAUSED BY RAIN, BAROMETRIC PRESSURE FLUCTUATION, AND LOCAL PUMPING; MONITORED UPPER ZONES.:TESTED FORMATION -S	409	635	UFA
swfwmd226	27.31505	-82.46898	NAD27	FL	SARASOTA	5,000		No additional data available.	1480	1902	UFA
usgs027	26.95478	-82.34732	NAD27	FL	SARASOTA	48,000		No additional data available.	1040	1600	UFA
sjrwmd005	28.80833	-81.32500	unk	FL	SEMINOLE	13,468		Step drawdown test (Walton, 1970); average of 4	400	700	FAS
sjrwmd008	28.82305	-81.31645	NAD27	FL	SEMINOLE	18,000		Cooper and Jacob (1946) recovery test	144	200	UFA
sjrwmd007	28.72722	-81.31201	NAD27	FL	SEMINOLE	42,000		Cooper and Jacob (1946) recovery test	120	163	UFA
sfwmd282	28.64840	-81.11669	unk	FL	SEMINOLE	8,528	0.0045	PARAMETER VALUES ARE AVERAGE FROM HANTUSH & JACOB DRAWDOWN AND RECOVERY AND COMPUTER SIMULATED AUTOMATCH METHOD FOR DRAWDOWN AND RECOVERY.	122	218	UFA
sjrwmd084	28.64222	-81.24507	NAD27	FL	SEMINOLE	34,000		Cooper and Jacob (1946) recovery test			UFA
sjrwmd220	28.71555	-81.17312	NAD27	FL	SEMINOLE	30,000		Cooper and Jacob (1946) recovery test		116	UFA
sjrwmd203	28.77500	-81.39166	unk	FL	SEMINOLE	160,417	0.005	Cooper (1963) unsteady flow in leaky confined aquifers	290	520	UFA
sfwmd279	28.78694	-81.07839	NAD27	FL	SEMINOLE	3,700		ADD. REF: TIBBALS, C.H. 1975. AQUIFER TESTS IN THE SUMMIT REACH OF THE PROPOSED CROSS-FL BARGE CANAL NEAR OCALA, FL. WRIR 28-75, WASHINGTON D.C.: USGS. ANALYTICAL METHOD: RECOVERY	70	141	UFA

sfwmd281	28.78527	-81.11867	NAD27	FL	SEMINOLE	1,700		ADD REF: TIBBALS, C.H. 1975. AQUIFER TESTS IN THE SUMMIT REACH OF THE PROPOSED CROSS-FL BARGE CANAL NEAR OCALA, FL. WRIR 28-75, WASHINGTON D.C.: USGS. ANALYTICAL METHOD: RECOVERY	99	178	UFA
sjrwmd219	28.69583	-81.17784	NAD27	FL	SEMINOLE	1,200		Cooper and Jacob (1946) recovery test	53	156	UFA
sjrwmd211	28.75638	-81.21812	NAD27	FL	SEMINOLE	8,900	0.000004	Average of two values.	111	228	UFA
sjrwmd210	28.75638	-81.21784	NAD27	FL	SEMINOLE	11,000		Cooper and Jacob (1946) recovery test	100	145	UFA
sfwmd280	28.76416	-81.12062	NAD27	FL	SEMINOLE	17,000		ADD REF: TIBBALS, C.H. 1975. AQUIFER TESTS IN THE SUMMIT REACH OF THE PROPOSED CROSS-FL BARGE CANAL NEAR OCALA, FL. WRIR 28-75, WASHINGTON D.C.: USGS. ANALYTICAL METHOD: RECOVERY	77	126	UFA
sjrwmd209	28.69055	-81.22451	NAD27	FL	SEMINOLE	13,000		Cooper and Jacob (1946) recovery test	80	98	UFA
sjrwmd216	28.78666	-81.20340	NAD27	FL	SEMINOLE	26,000		Cooper and Jacob (1946) recovery test		147	UFA
sjrwmd142	30.06639	-81.53250	unk	FL	ST JOHNS	51,547	0.0014	Average of Theis curve matching and residual drawdown	300	400	UFA
sjrwmd204	29.97583	-81.39555	unk	FL	ST JOHNS	19,655	0.0001	average Jacob straight line drawdown and modified Cooper-Jacob	256	325	UFA
sjrwmd149	29.68028	-81.49555	unk	FL	ST JOHNS	56,000	0.0006	Leakance expressed as units per day. Thickness of aquifer is 430 ft.		550	UFA
sjrwmd141	30.08389	-81.59694	unk	FL	ST JOHNS	28,082	0.0031	Jacob straight-line method	250	550	UFA
sjrwmd155	29.97583	-81.39555	unk	FL	ST JOHNS	18,950	0.0001	Average of Jacob straight-line, Hantush-Jacob drawdown, Jacob straight-line recovery, and Hantush-Jacob recovery	256	325	UFA
sjrwmd154	29.97583	-81.39555	unk	FL	ST JOHNS	22,021	0.000225	Average of Jacob straight-line, Hantush-Jacob drawdown, Jacob straight-line recovery, and Hantush-Jacob recovery	256	325	UFA
sjrwmd150	29.79250	-81.48500	unk	FL	ST JOHNS	23,000	0.000157	Hantush and Jacob	147	310	UFA
sjrwmd151	29.79250	-81.48277	unk	FL	ST JOHNS	39,000	0.00059	Hantush and Jacob	147	500	UFA
sjrwmd157	29.97583	-81.39555	unk	FL	ST JOHNS	21,995	0.000180818	Average of Jacob straight-line drawdown, Hantush-Jacob drawdown, Jacob straight-line recovery, and Hantush-Jacob recovery	256	325	UFA
sjrwmd143	29.96389	-81.49527	unk	FL	ST JOHNS	71,426	0.0017	modified Hantush	270	605	UFA
sjrwmd144	30.04500	-81.44944	unk	FL	ST JOHNS	15,329	0.0003407	Theis	275	681	UFA
sjrwmd145	30.04500	-81.44944	unk	FL	ST JOHNS	14,260	0.0004031	Hantush-Jacob	275	681	UFA
sjrwmd146	30.04500	-81.44944	unk	FL	ST JOHNS	13,559	0.000297	Hantush	275	681	UFA
sjrwmd201	29.77000	-81.42611	unk	FL	ST JOHNS	15,000	0.00015	average Jacob straight line recovery and matchpoint recovery	156	306	UFA
sjrwmd186	29.79666	-81.48500	unk	FL	ST JOHNS	25,000	0.0001	Hantush and Jacob	172	302	UFA
sjrwmd153	29.95695	-81.48549	unk	FL	ST JOHNS	54,000	0.0002	Hantush and Jacob	200	525	UFA
sjrwmd178	29.84111	-81.55250	unk	FL	ST JOHNS	8,700		Hantush and Jacob	230	300	UFA
sjrwmd176	30.08389	-81.59694	unk	FL	ST JOHNS	21,524	0.0011	average Jacob straight line, Jacob straight line recovery, and Hantush Jacob recovery	250	550	UFA

sjrwmd152	29.85914	-81.27979	NAD27	FL	ST JOHNS	12,999		Jacob straight-line	193	248	UFA
sjrwmd156	29.97583	-81.39555	unk	FL	ST JOHNS	25,015	0.00022225	Average of Jacob straight-line, Hantush-Jacob drawdown, Jacob straight-line recovery, and Hantush-Jacob recovery	256	325	UFA
sjrwmd206	29.97583	-81.39555	unk	FL	ST JOHNS	25,269	0.00025	average Jacob straight line drawdown	256	325	UFA
sjrwmd181	30.06524	-81.50314	NAD27	FL	ST JOHNS	6,800	0.000105	average Jacob straight line recovery and matchpoint recovery	322	362	UFA
sjrwmd205	29.97583	-81.39555	unk	FL	ST JOHNS	21,809	0.00025	average Jacob straight line drawdown	256	325	UFA
sjrwmd192	29.72802	-81.48174	unk	FL	ST JOHNS	29,000	0.0003	Hantush and Jacob	180	280	UFA
sjrwmd177	30.11805	-81.59444	unk	FL	ST JOHNS	30,747	0.0002	Hantush Jacob type-curve	335	610	UFA
sjrwmd139	29.94750	-81.51389	unk	FL	ST JOHNS	85,689	0.001245	average modified Hantush	270	605	UFA
sjrwmd140	29.97083	-81.31083	unk	FL	ST JOHNS	17,980	0.000235	Average of modified Hantush drawdown and modified Hantush recovery			UFA
sjrwmd148	29.66639	-81.47833	unk	FL	ST JOHNS	88,000	0.0006	Average of Hantush and Jacob	160	200	UFA
sjrwmd207	30.01358	-81.39230	NAD27	FL	ST JOHNS	1,600	0.00045	average Jacob straight line recovery and matchpoint recovery	248	258	UFA
sjrwmd180	30.06639	-81.53250	unk	FL	ST JOHNS	36,964	0.0014	average Theis curve matching, straight line, and specific capacity	300	400	UFA
sfwmd292	27.33778	-80.57142	unk	FL	ST LUCIE	55,935		SINGLE WELL RECOVERY TEST	318	1286	FAS
sfwmd308	27.33777	-80.48967	unk	FL	ST LUCIE	65,745	0.00018	SLF-74 (PUMPED) PAIRED WITH SLF-73 (OBS) ALSO NAMED W-16543 6 TOTAL FLORIDAN WELLS ON THIS C24 SITE. 1PAIR OF WELLS COMPLETED TO EACH OF 3 MAJOR FLOW ZONES. GEOPHYSICAL LOGS BY SCHLUMBERGER IN 1990. SLF-73 DRILLED, TESTED AND CONSTRUCTED UNDER CONTRACT W	1070	1450	FAS
sfwmd304	27.52948	-80.31643	unk	FL	ST LUCIE	34		SINGLE WELL RECOVERY TEST	640	1730	FAS
sfwmd305	27.30764	-80.34308	unk	FL	ST LUCIE	51,768	0.00058	THE PORT ST LUCIE WELLFIELD IS OPEN TO BOTH THE UPPER FLORIDAN AND MIDDLE FLORIDAN (OFTEN CALLED THE FIRST FLOW ZONE OF THE LOWER FLORIDAN) AQUIFERS. THE CONSULTANT ASSUMED A 70:30 SPLIT OF TRANSMISSIVITY (UPPER:LOWER), BUT DID NOT PROVIDE EXPLANATION FO	650	1350	FAS
sfwmd294	27.40365	-80.61311	unk	FL	ST LUCIE	75,037		SINGLE WELL RECOVERY TEST.	344	1238	FAS
sfwmd293	27.32449	-80.57061	unk	FL	ST LUCIE	22,575		SINGLE WELL RECOVERY TEST	320	1286	FAS
sfwmd363	27.33365	-80.57144	unk	FL	ST LUCIE	85,257		MONITOR WELL RECOVERY TEST		1246	FAS
sfwmd283	27.34831	-80.24366	unk	FL	ST LUCIE	6,000	0.002	DRAWDOWN ANALYSIS: COOPER-JACOBS METHODS VIA AQTESOLVE SOFTWARE	20	60	IA
sjrwmd163	27.37032	-80.40089	unk	FL	ST LUCIE	47,590	0.000836	Hantush and Jacob, 1955	100	350	IA
sjrwmd028	27.37032	-80.40089	unk	FL	ST LUCIE	12,737		ARCADIS. 2003. OPERATIONAL TESTING REQUEST. CITY OF PORT ST. LUCIE CLASS I INJECTION WELL SYSTEM.	2160	2264	LFA
sfwmd295	27.22005	-80.46949	unk	FL	ST LUCIE	14,458		SINGLE WELL RECOVERY TEST.	350	894	UFA
sfwmd286	27.34143	-80.27616	unk	FL	ST LUCIE	3,333		SINGLE WELL RECOVERY TEST	200	883	UFA

sfwmd285	27.42833	-80.40194	unk	FL	ST LUCIE	6,640		SINGLE WELL RECOVERY TEST.	156	707	UFA
sjrwmd262	27.20611	-80.47611	unk	FL	ST LUCIE	254,982	0.0047	Hantush and Jacob (1955)	790	970	UFA
sjrwmd263	27.20611	-80.47611	unk	FL	ST LUCIE	1,106,928	0.0037	Hantush and Jacob (1955)	1100	1200	UFA
sfwmd302	27.33838	-80.49783	unk	FL	ST LUCIE	6,170	0.00022	RECOMMENDED VALUES AVERAGE OF DRAWDOWN AND RECOVERY. ANALYSIS METHOD HANTUSH-JACOB.	600	775	UFA
sfwmd300	27.47361	-80.48389	unk	FL	ST LUCIE	62,561		SINGLE WELL RECOVERY TEST	482	993	UFA
sfwmd298	27.33775	-80.48972	unk	FL	ST LUCIE	23,748	0.00089	6 FLORIDAN WELLS ON SITE. 3 PAIRS IN EACH OF 3 FLOW ZONES. SLF-75 IS THE MIDDLE ZONE. CONSTRUCTED BY DISTRICT DRILLERS AND RIG	480	700	UFA
sfwmd287	27.44722	-80.59028	unk	FL	ST LUCIE	72,022		SINGLE WELL RECOVERY TEST	256	1058	UFA
sfwmd307	27.33777	-80.48967	unk	FL	ST LUCIE	14,905	0.00064		790	860	UFA
sfwmd306	27.33777	-80.48967	unk	FL	ST LUCIE	29,953	0.00016	6 TOTAL WELLS ON SITE, ONE PAIR FOR EACH OF THREE FLOW ZONES.	790	860	UFA
sfwmd303	27.33838	-80.49783	unk	FL	ST LUCIE	14,509	0.00027	ANALYSIS METHOD IS WALTON TYPE CURVE MATCHING	600	1000	UFA
swfwmd212	28.85531	-82.01129	unk	FL	SUMTER	43,850		Step draw down test	570	1080	FAS
swfwmd211	28.88290	-82.01310	unk	FL	SUMTER	604,000		Step drawdown test	600	1100	FAS
swfwmd208	28.87530	-81.99130	unk	FL	SUMTER	219,000		Step drawdown test	600	1100	FAS
swfwmd218	28.84294	-81.96396	unk	FL	SUMTER	1,236,584		Step drawdown test	612	1006	FAS
swfwmd216	28.89482	-81.97514	unk	FL	SUMTER	48,797		Step drawdown test	600	1060	FAS
swfwmd210	28.86457	-82.00759	unk	FL	SUMTER	68,182		Step drawdown test	633	1006	FAS
swfwmd214	28.85072	-81.98015	unk	FL	SUMTER	1,733,783	0.029	14-day test	595	890	LFA
swfwmd215	28.86628	-81.95394	unk	FL	SUMTER	4,515,374		Step draw down test	595	756	LFA
swfwmd213	28.85072	-81.98015	unk	FL	SUMTER	413,837		Step drawdown test	595	890	LFA
swfwmd202	28.92246	-82.00242	unk	FL	SUMTER	31,640		Step draw down test, results before air pressure fracturing	97	303	UFA
swfwmd200	28.93210	-81.99675	unk	FL	SUMTER	27,798		Step draw down test	143	350	UFA
swfwmd115	28.77760	-82.06100	unk	FL	SUMTER	9,091	0.000443	Abrupt pump shutoff 12 hrs into test caused loss of early recovery data; Theis non-eq & type curve and Jacob approx. of Theis analytical methods used (Lohman 1972).	63	184	UFA
swfwmd201	28.92246	-82.00242	unk	FL	SUMTER	184,404		Constant rate 48 hr test,water discharge 500' to east of well,results after air pressure fracturing	97	303	UFA
swfwmd221	28.87670	-82.10050	unk	FL	SUMTER	247,000	0.04	Partial penetration test, Ocala limestone production interval. Production well inefficiency (well screen / gravel pack issues)	80	105	UFA
swfwmd207	28.87971	-81.96646	unk	FL	SUMTER	1,847,126		Step drawdown test, fractured zone/cavity approx. 255' to 269' btoc	135	280	UFA
swfwmd249	28.73680	-82.05800	unk	FL	SUMTER	50,000		48 hr constant rate following specific capacity testing. Analysis of pumping data via specific capacity. Theis recovery analysis on monitor well.	100	335	UFA

swfwmd206	28.87971	-81.96646	unk	FL	SUMTER	1,234,757	0.00676	48 hr test, water discharge 500' to east of well, fractured zone/cavity approx. 255' to 269' btoc	135	280	UFA
swfwmd205	28.87966	-81.96644	unk	FL	SUMTER	1,076,203		Step draw down test	139	280	UFA
swfwmd204	28.92240	-82.00328	unk	FL	SUMTER	438,108		Constant rate 48 hr test,water discharge 500' to east of well,results after air pressure fracturing	152	327	UFA
swfwmd203	28.92240	-82.00328	unk	FL	SUMTER	88,971		Step draw down test, results before air pressure fracturing	152	327	UFA
usgs245	30.02433	-82.95060	unk	FL	SUWANNEE	450,000		SRWMD files in Live Oak	85	160	UFA
usgs244	30.12611	-83.08528	unk	FL	SUWANNEE	300,000		SRWMD files in Live Oak	71	273	UFA
usgs012	30.07072	-83.53183	NAD83	FL	TAYLOR	125,000	0.0008	USGS files (Tallahassee, FL). Thickness of aquifer tested, 143 ft.			UFA
sjrwmd191	29.24470	-81.47424	NAD27	FL	VOLUSIA	22,000	0.0006	average of curve matching and straight line method			FAS
sjrwmd295	29.09248	-81.35951	NAD27	FL	VOLUSIA	88,500	0.0007	average of curve matching and straight line method			FAS
sjrwmd224	29.25833	-81.15833	unk	FL	VOLUSIA	41,976	0.0006	Step-drawdown pump test; Jacob-Rorabaugh; the Walton formula	90	260	UFA
sjrwmd228	29.09166	-81.14166	unk	FL	VOLUSIA	4,445	0.000121	average Theis non-equilibrium formula and Jacob non-equilibrium formula	125	250	UFA
sjrwmd229	29.10833	-81.14166	unk	FL	VOLUSIA	5,526	0.0002045	average curve matching and straight line (All three obervation well data combined)	125	300	UFA
sjrwmd248	28.99166	-80.92222	unk	FL	VOLUSIA	7,400	0.00034	Theis non-equilibrium	90	177	UFA
sjrwmd221	28.88241	-81.16050	unk	FL	VOLUSIA	11,229		recovery	147	400	UFA
sjrwmd208	29.09166	-81.24166	unk	FL	VOLUSIA	3,837		Not published	81	500	UFA
sjrwmd249	28.99166	-80.91944	unk	FL	VOLUSIA	6,100	0.0002	Cooper and Jacob (1946) semilog	143	231	UFA
sjrwmd222	29.12500	-81.15833	unk	FL	VOLUSIA	6,417		Not published	105	300	UFA
sjrwmd239	29.19278	-81.06639	unk	FL	VOLUSIA	44,000	0.00022	Theis non-equilibrium	110	205	UFA
sjrwmd245	28.78775	-80.94033	unk	FL	VOLUSIA	7,513	0.000285	average Cooper and Jacob (1946) and Hantush	106	255	UFA
sjrwmd244	28.95833	-80.94166	unk	FL	VOLUSIA	18,983	0.0025	Theis graphical method with type-curve matching (composite analysis)	108	206	UFA
sfwmd364	29.10721	-81.02700	unk	FL	VOLUSIA	8,000	0.0003	6 MONITOR WELL: MW-1, MW-2, MW-3, MW-4, MW-5, MW-6 (MW-4, MW-5, MW-6 USED TO TEST THE SURFICIAL AQUIFER). TRANSMISSIVITY ESTIMATED USING THEIS CURVE-MATCHING AND COOPER AND JACOB (1946).	107	250	UFA
sfwmd366	29.16804	-81.17034	NAD27	FL	VOLUSIA	12,000		ANALYTICAL METHOD: CURVE-MATCHING OTHER: NO DATA AVAILABLE FROMT HE PUBLICATION ABOUT THE OBSERVATION WELLS.	119	220	UFA
sfwmd367	29.01082	-81.10422	unk	FL	VOLUSIA	7,600	0.00027	TRANSMISSIVITY, STORATIVITY AND LEAKANCE FROM OBSERVATION WELL. ANALYTICAL METHOD: HANTUSH AND JACOB (1955) FLOW EQUATIONS		200	UFA
sjrwmd243	28.95833	-80.97500	unk	FL	VOLUSIA	10,168	0.00049725	average Hantush-Jacob matchpoint and Cooper-Jacob (1946)	240	158	UFA
sjrwmd242	29.02008	-80.99733	unk	FL	VOLUSIA	27,538	0.00027		105	160	UFA

sjrwmd230	29.15833	-81.14166	unk	FL	VOLUSIA	19,533	0.00059	Average values derived from Theis, Cooper and Jacob (1946), and Walton for leaky aquifers	104	350	UFA
sjrwmd240	29.19500	-81.05861	unk	FL	VOLUSIA	21,000		Cooper and Jacob (1946) semilog	135	280	UFA
sjrwmd254	28.78749	-80.85616	unk	FL	VOLUSIA	40,000	0.0008	Theis graphical method	84	130	UFA
usgs290	29.18750	-81.06597	NAD83	FL	VOLUSIA	40,000	0.0007	Wyrick (1960). Thickness of aquifer tested, 150 ft.			UFA
sjrwmd238	29.19278	-81.06889	unk	FL	VOLUSIA	41,000	0.00018	Theis non-equilibrium method	110	210	UFA
sjrwmd237	29.19111	-81.07139	unk	FL	VOLUSIA	47,000		Theis non-equilibrium	109	201	UFA
sjrwmd236	29.00833	-81.07500	unk	FL	VOLUSIA	12,860	0.000211	average not published	115	152	UFA
sjrwmd235	29.15859	-81.10117	NAD27	FL	VOLUSIA	41,000	0.000735	average Theis graphical method and Hantush and Jacob	102	234	UFA
sjrwmd233	29.35416	-81.13750	unk	FL	VOLUSIA	2,166		recovery	110	160	UFA
sjrwmd232	29.39166	-81.14139	unk	FL	VOLUSIA	1,604		Walton unsteady state	107	145	UFA
sjrwmd231	29.35833	-81.14166	unk	FL	VOLUSIA	1,978	0.00015	average recovery, Hantush and Jacob (1955), Cooper and Jacob (1946)	112	160	UFA
sjrwmd241	29.20833	-81.04166	unk	FL	VOLUSIA	3,800	0.00023	Cooper (1963) type-curve for nonsteady radial flow in an infinite leaky aquifer	94	160	UFA
sjrwmd301	28.84840	-81.31753	unk	FL	VOLUSIA	4,826	0.000149	Hantush and Jacob (1955)	112	163	UFA
sjrwmd162	29.15133	-81.14911	unk	FL	VOLUSIA	26,068	0.001092	Hantush and Jacob, 1955	100	350	UFA
sjrwmd199	29.26053	-81.43035	NAD27	FL	VOLUSIA	8,400	0.00045	average of curve matching and straight line method	110	510	UFA
sjrwmd160	29.22694	-81.18444	unk	FL	VOLUSIA	29,410	0.00046	average pump and recovery of Walton	108	300	UFA
sjrwmd159	28.92132	-81.18264	unk	FL	VOLUSIA	6,007		average Theis recovery and Cooper-Jacob time-drawdown	87.5	215	UFA
sjrwmd158	28.90361	-81.29055	unk	FL	VOLUSIA	35,522	0.0001	average recovery (Driscoll,1986)	125	264	UFA
sjrwmd004	29.11498	-81.33395	NAD27	FL	VOLUSIA	6,700	0.0003	average of curve matching and straight line method	108	450	UFA
sjrwmd305	29.03139	-81.34055	unk	FL	VOLUSIA	134,616	0.0002064	Hantush-Jacob, Theis, and Cooper-Jacob	93	305	UFA
sjrwmd304	28.85107	-81.31433	unk	FL	VOLUSIA	10,975	0.000221	Hantush-Jacob drawdown	130	275	UFA
sjrwmd296	29.15831	-81.35673	NAD27	FL	VOLUSIA	24,000	0.00095	average of curve matching and straight line method	84	253	UFA
sjrwmd302	28.84862	-81.31665	unk	FL	VOLUSIA	6,176	0.000221	Hantush and Jacob drawdown and recovery	130	275	UFA
sjrwmd161	29.14730	-81.14624	unk	FL	VOLUSIA	18,314	0.000046	Hantush and Jacob, 1955	110	350	UFA
sjrwmd018	28.94166	-81.24139	unk	FL	VOLUSIA	6,016		Hantush and Jacob (1955)	95	220	UFA
sjrwmd017	28.94166	-81.24166	unk	FL	VOLUSIA	33,420	0.0008	Hantush and Jacob (1955)	95	140	UFA
sjrwmd016	28.94139	-81.24166	unk	FL	VOLUSIA	3,155		Hantush and Jacob (1955)	95	200	UFA
sjrwmd015	28.89166	-81.24166	unk	FL	VOLUSIA	4,266	0.00071	average Theis and Cooper and Jacob (1946)	126	260	UFA
sjrwmd014	29.17500	-81.25833	unk	FL	VOLUSIA	10,505	0.00022	Curve-matching Hantush and Jacob (1955)	85	300	UFA
sjrwmd013	28.92693	-81.28145	unk	FL	VOLUSIA	20,300	0.00010625	average recovery, Cooper-Jacob time-drawdown, Walton	126	318	UFA
sjrwmd011	28.98666	-81.29333	unk	FL	VOLUSIA	25,000		Cooper and Jacob (1946) semilog	107	340	UFA
sjrwmd009	29.02500	-81.30833	unk	FL	VOLUSIA	47,081	0.3913	average Hantush curve match and Cooper and Jacob (1946)	176	325	UFA
sjrwmd303	28.84862	-81.31665	unk	FL	VOLUSIA	25,266	0.001379	Hantush-Jacob drawdown and recovery (all obs. Wells)	114	270	UFA
sjrwmd276	29.10833	-81.19166	unk	FL	VOLUSIA	10,080		Not published	101	300	UFA
sjrwmd185	29.25192	-81.48229	NAD27	FL	VOLUSIA	26,000	0.00045	average of curve matching and straight line method	120	424	UFA
sjrwmd187	29.33137	-81.48146	NAD27	FL	VOLUSIA	28,500	0.001	average of curve matching and straight line method	147	338	UFA

sjrwmd193	29.29025	-81.46563	NAD27	FL	VOLUSIA	24,500	0.00055	average of curve matching and straight line method	105	476	UFA
sjrwmd247	28.99166	-80.92500	unk	FL	VOLUSIA	7,400	0.00034	Theis non-equilibrium	93	181	UFA
nwfwmd032	30.53992	-85.95105	NAD27	FL	WALTON	14,000	0.0006		193	585	FAS
nwfwmd039	30.38308	-86.38175	unk	FL	WALTON	10,972		Plot and data only, no analysis or other well documentation.			FAS
nwfwmd038	30.38020	-86.34261	unk	FL	WALTON	6,937		Plot and data only, no analysis or other well documentation.			FAS
nwfwmd037	30.60900	-86.11300	unk	FL	WALTON	6,864	0.00016	Lat/long estimated from Google Earth. Re-analysis of J. Stidham & Assoc. original APT . Test #2 - data from only one observation well available.	280	700	FAS
nwfwmd036	30.60900	-86.11300	unk	FL	WALTON	8,433	0.000393	Lat/long estimated from Google Earth. Re-analysis of J. Stidham & Assoc. original APT . Test #1 - value is average of data from three observation wells.	280	550	FAS
nwfwmd033	30.34028	-86.16972	unk	FL	WALTON	6,421		Plot and data only, no analysis or other well documentation. Value is average of drawdown and recovery periods. Appears to be a single-well, specific capacity test.	353	553	FAS
nwfwmd040	30.58133	-86.08496	unk	FL	WALTON	13,415	0.00057	Re-analysis of Baskervill-Donovan, Inc. original APT.	220	512	FAS
nwfwmd031	30.68214	-86.35384	NAD27	FL	WALTON	3,472	0.0002		327	625	FAS
nwfwmd035	30.72549	-86.06994	unk	FL	WALTON	6,918	0.001066	Drawdown in production and observation wells stabilized after 13 hours.	217	560	FAS
nwfwmd034	30.37611	-86.18000	unk	FL	WALTON	20,400		Plot and data only, no analysis or other well documentation. Appears to be a single-well, specific capacity test.	220	683	FAS
usgs289	30.57817	-86.11862	NAD83	FL	WALTON	24,000	0.0003	Pascale (1974). Thickness of aquifer tested, 249 ft.			UFA
usgs306	30.85167	-86.32683	NAD83	FL	WALTON	3,300	0.0004	Pascale (1974). Thickness of aquifer tested, 350 ft.			UFA
usgs016	30.28883	-86.01582	NAD83	FL	WALTON	500		Pascale (1974). Thickness of aquifer tested, 333 ft.			UFA
usgs009	30.40867	-86.01092	NAD83	FL	WALTON	8,000	0.0002	Pascale (1974). Thickness of aquifer tested, 117 ft.			UFA
usgs014	30.54667	-85.98800	NAD83	FL	WALTON	18,000	0.0004	Pascale (1974). Thickness of aquifer tested, 288 ft.			UFA
usgs297	30.69983	-86.35400	NAD83	FL	WALTON	3,800	0.0002	Pascale (1974). Thickness of aquifer tested, 300 ft.			UFA
usgs054	30.97967	-86.29750	NAD83	FL	WALTON	3,700		Pascale (1974). Thickness of aquifer tested, 139 ft.			UFA
usgs002	30.51000	-86.08673	NAD83	FL	WALTON	19,000	0.0003	Pascale (1974). Thickness of aquifer tested, 177 ft.			UFA
usgs013	30.58617	-86.23150	NAD83	FL	WALTON	12,000		Pascale (1974). Thickness of aquifer tested, 162 ft.			UFA
usgs033	31.26833	-84.54517	NAD83	GA	BAKER	42,000	0.02	Hayes and others (1983). Thickness of aquifer tested, 101 ft.			UFA
ggs183	31.24574	-84.53214	NAD27	GA	BAKER	42,000		Principal artesian aquifer	180	180	UFA
usgs043	31.30944	-84.57472	unk	GA	BAKER	13,800		written communication on fig 15, not in table A1	183	250	UFA
usgs044	31.37796	-84.41186	unk	GA	BAKER	7,579		written communication on fig 15, not in table A1	84	210	UFA
scdnr033	32.28076	-80.82150	NAD27	GA	BEAUFORT	8,800		Newcome rates test poor	255	600	UFA
scdnr032	32.28417	-80.81639	unk	GA	BEAUFORT	18,000		Newcome rates test poor	125	192	UFA
usgs272	31.71657	-83.24599	NAD27	GA	BEN HILL	16,000	0.002	All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs058	31.71741	-83.24488	NAD27	GA	BEN HILL	16,000	0.003		260	825	UFA

usgs271	31.38381	-83.22265	NAD27	GA	BERRIEN	32,000		All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs059	31.38381	-83.22265	NAD27	GA	BERRIEN	32,000		T calculated from recovery analysis	368	550	UFA
usgs163	32.70833	-83.65306	unk	GA	BIBB	4,140			106	220	SCP
usgs060	31.91194	-81.31639	NAD83	GA	BRYAN	8,300			1010	1275	LFA
usgs061	31.91194	-81.31639	NAD83	GA	BRYAN	70,000			315	441	UFA
usgs063	32.37796	-81.84456	NAD27	GA	BULLOCH	4,300			398	637	UFA
usgs064	32.37768	-81.84456	NAD27	GA	BULLOCH	4,700	0.00039		405	630	UFA
usgs066	32.37740	-81.84734	NAD27	GA	BULLOCH	5,000	0.00038		383	540	UFA
usgs065	32.38157	-81.83928	NAD27	GA	BULLOCH	5,600	0.00034		420	580	UFA
usgs069	33.09682	-81.65289	NAD27	GA	BURKE	3,500			150	200	LFA
usgs068	33.17904	-81.78567	NAD27	GA	BURKE	180			180	200	LFA
usgs166	33.14126	-81.76206	NAD27	GA	BURKE	21,900	0.00035		523	860	SCP
usgs164	33.14182	-81.76150	NAD27	GA	BURKE	26,200	0.00066		502	883	SCP
usgs165	33.14222	-81.76214	NAD83	GA	BURKE	21,400	0.00033		510	870	SCP
usgs167	33.14098	-81.76261	NAD27	GA	BURKE	20,500	0.000021		520	860	SCP
usgs168	33.14126	-81.76317	NAD27	GA	BURKE	30,600	0.00039		513	850	SCP
usgs169	33.14126	-81.76150	NAD27	GA	BURKE	21,100			505	850	SCP
usgs067	33.23015	-81.87873	NAD27	GA	BURKE	840			80	110	UFA
usgs042	31.44667	-84.68583	unk	GA	CALHOUN	41,829		written communication on fig 15, not in table A1	38	130	UFA
other002	30.79718	-81.56454	NAD27	GA	CAMDEN	43,000			950	1150	LFA
sjrwmd107	30.73500	-81.55139	unk	GA	CAMDEN	13,000		Straight line analytical solution	1360	1500	LFA
sjrwmd032	30.72028	-81.55000	unk	GA	CAMDEN	110,000	0.0014	Nonleaky aquifer analysis	467	575	UFA
usgs070	30.73361	-81.54167	unk	GA	CAMDEN	19,000		Warren cites T range from observation wells as 14000-24000 ft2/day, analyzed by Theim method	516	1060	UFA
usgs072	30.79718	-81.56454	NAD27	GA	CAMDEN	43,000	0.000058		560	750	UFA
sjrwmd108	30.75333	-81.57666	unk	GA	CAMDEN	98,000	0.0017	Nonleaky aquifer analysis	552	760	UFA
sjrwmd109	30.79889	-81.51972	unk	GA	CAMDEN	130,000	0.00099	Nonleaky aquifer analysis	555	990	UFA
usgs087	32.02688	-80.89039	NAD27	GA	CHATHAM	80,208	0.005				FAS
usgs084	32.08382	-81.09595	NAD27	GA	CHATHAM	33,420			250	1003	FAS
usgs081	32.07799	-81.09289	NAD27	GA	CHATHAM	20,052	0.0003		274	695	FAS
usgs080	32.14917	-81.14500	unk	GA	CHATHAM	26,736	0.0002	Average of 7 values.	270	971	FAS
usgs073	32.09965	-81.12956	NAD27	GA	CHATHAM	33,420	0.0003	Average of 6 values from Warren (1944)	237	603	FAS
usgs076	32.02750	-81.22778	NAD83	GA	CHATHAM	8,200			760	1085	FAS
usgs075	32.08882	-81.15067	NAD27	GA	CHATHAM	33,000	0.0004		251	750	FAS
usgs257	32.05778	-81.14187	NAD83	GA	CHATHAM	36,000	0.0004	Warren (1944). Thickness of aquifer tested, 340 ft.			FAS
usgs256	32.11595	-81.14692	NAD83	GA	CHATHAM	30,000	0.0004	Warren (1944). Thickness of aquifer tested, 374 ft.			FAS
usgs077	32.02750	-81.22778	unk	GA	CHATHAM	46,000	0.00009		358	460	FAS
usgs260	32.00132	-81.17257	NAD83	GA	CHATHAM	10,000		Single well test conducted upon completion of Lower Floridan well open from 703 –1,100 feet. Analysis used Theis, 1935, solution. Drawdown was corrected for tidal and other fluctuations prior to analysis.	703	1100	LFA
usgs074	32.09187	-81.14706	NAD27	GA	CHATHAM	32,000	0.00063		250	406	UFA

usgs259	32.00512	-81.16830	NAD83	GA	CHATHAM	40,000	0.0002	Transmissivity and storage calculated from drawdown response in well No. 8 located 2,020 feet away. Used Hantush, 1960, leaky aquifer solution. Drawdown was corrected for tidal and other fluctuations prior to analysis.	295	425	UFA
usgs078	32.15520	-81.16372	NAD27	GA	CHATHAM	33,420			254	650	UFA
usgs082	32.07604	-81.07400	NAD27	GA	CHATHAM	43,000	0.00074		260	500	UFA
usgs083	32.08222	-81.02972	unk	GA	CHATHAM	26,736		Average of 2 values.	205	650	UFA
usgs085	32.10632	-81.11011	NAD27	GA	CHATHAM	32,000	0.0013		274	344	UFA
usgs170	32.35917	-84.97889	unk	GA	CHATTAHOOCHEE	510					SCP
usgs171	32.30111	-84.77278	unk	GA	CHATTAHOOCHEE	690			746	1130	SCP
usgs172	31.60778	-85.05389	unk	GA	CLAY	930			330	445	SCP
usgs269	31.13769	-83.70906	NAD27	GA	COLQUITT	150,000	0.007	All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs267	31.32352	-83.91768	NAD27	GA	COLQUITT	13,000		All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs071	31.18333	-83.79133	NAD83	GA	COLQUITT	150,000	0.007	Zimmerman (1977). Thickness of aquifer tested, 507 ft.			UFA
usgs079	31.31783	-83.92267	NAD83	GA	COLQUITT	13,000		Zimmerman (1977). Thickness of aquifer tested, 289 ft.			UFA
usgs270	31.13797	-83.42599	NAD27	GA	COOK	210,000	0.002	All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs088	31.04603	-83.39433	NAD27	GA	COOK	6,700			214	308	UFA
usgs089	31.14047	-83.42822	NAD27	GA	COOK	210,000	0.002		207	393	UFA
ggs184	31.02296	-84.38713	NAD27	GA	DECATEUR	43,000		Principal artesian aquifer	160	160	UFA
usgs038	30.71806	-84.77944	unk	GA	DECATUR	19,135		written communication on fig 15, not in table A1	310	790	FAS
usgs276	30.98000	-84.63000	NAD27	GA	DECATUR	330,000	0.001	Cooper-Jacob or Theis. Well information from Hayes, L.R., Maslia, M.L., and Meeks, W.C., 1983, Hydrology and model evaluation of the principal artesian aquifer, Dougherty Plain, southwest Georgia: Georgia Geologic Survey Bulletin 97, 93 p.	168	576	FAS
usgs274	30.90000	-84.50000	NAD27	GA	DECATUR	80,000	0.0009	Cooper-Jacob or Theis. Well information from Hayes, L.R., Maslia, M.L., and Meeks, W.C., 1983, Hydrology and model evaluation of the principal artesian aquifer, Dougherty Plain, southwest Georgia: Georgia Geologic Survey Bulletin 97, 93 p.	144	469	FAS
usgs035	31.01855	-84.41467	NAD83	GA	DECATUR	43,000	0.001	Hayes and others (1983). Thickness of aquifer tested, 72 ft.			UFA
usgs091	32.25072	-83.73879	NAD27	GA	DOOLY	6,600			247	307	LFA
usgs315	31.48731	-84.25833	NAD83	GA	DOUGHERTY	29,000		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS

usgs314	31.45129	-84.12102	NAD27	GA	DOUGHERTY	65,500		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs316	31.51407	-84.05379	NAD27	GA	DOUGHERTY	110,900		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs317	31.55323	-84.10796	NAD27	GA	DOUGHERTY	283,400		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs318	31.55323	-84.10824	NAD27	GA	DOUGHERTY	22,500		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs175	31.59129	-84.08102	NAD27	GA	DOUGHERTY	4,140	0.0014		300	932	LFA
usgs179	31.59656	-84.07768	NAD27	GA	DOUGHERTY	5,320			300	550	LFA
usgs178	31.60295	-84.07713	NAD27	GA	DOUGHERTY	3,790			290	540	LFA
usgs176	31.59601	-84.07907	NAD27	GA	DOUGHERTY	3,380	0.00075		300	550	LFA
usgs174	31.57934	-84.11102	NAD27	GA	DOUGHERTY	4,260			300	930	LFA
usgs177	31.60184	-84.07741	NAD27	GA	DOUGHERTY	3,990	0.00099		290	540	LFA
usgs112	31.49767	-84.27100	NAD83	GA	DOUGHERTY	12,000	0.004	Hayes and others (1983). Thickness of aquifer tested, 87 ft.			UFA
usgs036	31.14629	-84.96743	NAD27	GA	EARLY	12,000		written communication on fig 15, not in table A1	70	245	UFA
usgs041	31.28212	-84.73520	unk	GA	EARLY	33,759		written communication on fig 15, not in table A1	83	132	UFA
usgs037	31.26944	-84.95972	unk	GA	EARLY	11,544		written communication on fig 15, not in table A1	50	130	UFA
usgs032	31.36800	-84.64933	NAD83	GA	EARLY	24,000	0.0004	Hayes and others (1983). Thickness of aquifer tested, 64 ft.			UFA
ggs186	31.37740	-84.65464	NAD27	GA	EARLY	24,000		Principal artesian aquifer	125	125	UFA
ggs185	31.27324	-84.75242	NAD27	GA	EARLY	41,000		Principal artesian aquifer. From P.E. Lamoreaux and Associates, written commun., 1980.	148	155	UFA
usgs132	31.19611	-81.33694	unk	GA	GLYNN	64,000		Upper and lower water-bearing zones. Originally from Wait and Gregg, 1973.	584	1040	FAS
usgs126	31.17676	-81.48257	NAD27	GA	GLYNN	59,000	0.0006		580	753	UFA
usgs125	31.17134	-81.49482	NAD27	GA	GLYNN	67,000	0.0003	J & M cite fit as excellent	500	640	UFA
usgs102	31.05440	-81.40954	NAD27	GA	GLYNN	93,000	0.00469	J & M cite fit as fair	523	764	UFA
usgs103	31.11634	-81.41676	NAD27	GA	GLYNN	60,000	0.00305	J & M cite fit as fair	502	715	UFA
usgs122	31.16995	-81.49177	NAD27	GA	GLYNN	67,000	0.00027	J & M cite fit as excellent	550	745	UFA
usgs121	31.17217	-81.48927	NAD27	GA	GLYNN	64,000	0.00021	J & M cite fit as good	548	630	UFA
usgs279	31.18567	-81.35133	NAD83	GA	GLYNN	280,000		Walt and Gregg (1973). Thickness of aquifer tested, 417 ft.			UFA
usgs124	31.17134	-81.48260	NAD27	GA	GLYNN	66,000	0.00029	J & M cite fit as good	550	700	UFA
usgs100	31.16879	-81.50441	NAD27	GA	GLYNN	63,000	0.00036	J & M cite fit as good	520	790	UFA
usgs099	31.19162	-81.50566	NAD27	GA	GLYNN	75,000	0.00042	J & M cite fit as good	540	777	UFA
usgs127	31.17245	-81.49760	NAD27	GA	GLYNN	64,000	0.00032	J & M cite fit as excellent	540	566	UFA
usgs097	31.23495	-81.53705	NAD27	GA	GLYNN	89,000	0.00419	J & M cite fit as fair	560	825	UFA
usgs130	31.18051	-81.35787	NAD27	GA	GLYNN	56,000	0.00258	J & M cite fit as good	514	640	UFA

usgs096	31.20467	-81.56510	NAD27	GA	GLYNN	58,000	0.00684	J & M cite fit as good	550	650	UFA
usgs095	31.13329	-81.59816	NAD27	GA	GLYNN	65,000	0.012	J & M cite fit as good	550	991	UFA
usgs094	31.29356	-81.69066	NAD27	GA	GLYNN	49,000	0.00406	J & M cite fit as fair	700	740	UFA
usgs093	31.18162	-81.63649	NAD27	GA	GLYNN	66,000	0.0046	J & M cite fit as good	292	445	UFA
usgs092	31.15523	-81.66872	NAD27	GA	GLYNN	110,000	0.00286	J & M cite fit as excellent.	214	518	UFA
usgs098	31.21106	-81.52010	NAD27	GA	GLYNN	65,000	0.00126	J & M cite fit as excellent	550	780	UFA
usgs111	31.17245	-81.49760	NAD27	GA	GLYNN	64,000	0.0003	Upper and lower water-bearing zones	540	1200	UFA
usgs120	31.16273	-81.49843	NAD27	GA	GLYNN	85,000	0.00028		525	756	UFA
usgs119	31.18579	-81.48593	NAD27	GA	GLYNN	75,000	0.00037	J & M cite fit as fair	541	660	UFA
usgs118	31.16495	-81.49955	NAD27	GA	GLYNN	41,000	0.00029	J & M cite fit as fair	527	696	UFA
usgs117	31.13859	-81.49338	NAD27	GA	GLYNN	69,000	0.00051	J & M cite fit as fair	606	700	UFA
usgs116	31.16070	-81.48074	NAD27	GA	GLYNN	23,000	0.0003	J & M cite fit as excellent	504	770	UFA
usgs115	31.22217	-81.39121	NAD27	GA	GLYNN	72,000	0.0025	J & M cite fit as good	600	640	UFA
usgs114	31.13384	-81.39343	NAD27	GA	GLYNN	85,000	0.00028	J & M cite fit as excellent	477	608	UFA
usgs128	31.32717	-81.44566	NAD27	GA	GLYNN	110,000	0.00076	J & M cite fit as good			UFA
usgs280	31.14387	-81.50283	NAD83	GA	GLYNN	200,000	0.0006	Walt and Gregg (1973). Thickness of aquifer tested, 300 ft.			UFA
usgs110	31.15179	-81.49166	NAD27	GA	GLYNN	56,000	0.00033	J & M cite fit as excellent	535	604	UFA
usgs109	31.13523	-81.49010	NAD27	GA	GLYNN	33,000	0.00047	J & M cite fit as good	595	786	UFA
usgs108	31.13218	-81.49066	NAD27	GA	GLYNN	160,000	0.0067	J & M cite fit as excellent	584	757	UFA
usgs107	31.15190	-81.47927	NAD27	GA	GLYNN	33,000	0.00057	T from recovery cited as 40000 ft2/day; S as 0.00057	514	623	UFA
usgs106	31.16356	-81.48093	NAD27	GA	GLYNN	56,000	0.000063	J & M cite fit as excellent	545	890	UFA
usgs105	31.16662	-81.48343	NAD27	GA	GLYNN	58,000	0.00015	J & M cite fit as good	480	911	UFA
usgs104	31.16829	-81.47399	NAD27	GA	GLYNN	64,000	0.00019	J & M cite fit as good	554	810	UFA
usgs131	31.14607	-81.37371	NAD27	GA	GLYNN	55,000	0.00529	J & M cite fit as good	580	704	UFA
usgs129	31.30328	-81.44732	NAD27	GA	GLYNN	140,000	0.000685	J & M cite fit as excellent	580	780	UFA
usgs113	31.17662	-81.48260	NAD27	GA	GLYNN	57,000	0.00036	J & M cite fit as good	520	800	UFA
ggs098	30.89335	-84.32477	NAD83	GA	GRADY	650		If duration of test 24 hours or greater and T on map is not between two methods of estimation of T from specific capacity Driscoll, 1986 and USGS WSP 1536-I, 1963--but a reasonable value classed as APT analysis unknown (Eve Kuniansky)	426	604	FAS
usgs273	30.89408	-84.21435	NAD27	GA	GRADY	9,000	0.0003	Cooper-Jacob or Theis.			UFA
usgs186	32.61264	-83.58879	NAD27	GA	HOUSTON	7,840			200	370	SCP
usgs184	32.43876	-83.63629	NAD27	GA	HOUSTON	32,300			295	630	SCP
usgs183	32.53070	-83.68324	NAD27	GA	HOUSTON	28,700			515	615	SCP
usgs185	32.62403	-83.58740	NAD27	GA	HOUSTON	19,600					SCP
usgs187	31.63378	-84.18074	NAD27	GA	LEE	5,100			560	668	SCP
usgs047	31.78972	-84.07417	NAD83	GA	LEE	79,456		written communication on fig 15, not in table A1	60	225	UFA
usgs048	31.89356	-84.03628	unk	GA	LEE	5,850		written communication on fig 15, not in table A1	103	113	UFA
usgs123	31.69817	-84.13722	NAD83	GA	LEE	43,000	0.01	Hayes and others (1983). Thickness of aquifer tested, 126 ft.			UFA
ggs187	31.70989	-84.15408	NAD27	GA	LEE	43,000		Principal artesian aquifer	190	190	UFA
ggs182	31.74327	-81.41066	NAD27	GA	LIBERTY	160,000	0.00021	T=88000, S=0.00054 in recovery analysis	418	810	FAS

ggs181	31.74410	-81.40677	NAD27	GA	LIBERTY	160,000	0.0004	T=88000, S=0.00054 in recovery analysis	427	810	FAS
usgs277	31.73650	-81.43917	NAD83	GA	LIBERTY	130,000	0.0004	Dyar and others (1972). Thickness of aquifer tested, 350 ft.	502	705	FAS
usgs262	31.90953	-81.61294	NAD83	GA	LIBERTY	7,000	0.0015	calibrated radial model to multi-well pumping and recovery data entry simulated as 475.6 ft thick so top is 896 then bottom 1372	896	1372	LFA
usgs263	31.90953	-81.61294	NAD83	GA	LIBERTY	4,000	0.00068	calibrated radial model to multi-well pumping and recovery data entry semi-confining unit simulated between UFA and LFA in model 220 ft thick top 676 bottom 896	676	896	MCU
ggs179	31.74194	-81.42833	unk	GA	LIBERTY	160,000	0.0005	T=130000, S=0.00041 in recovery analysis	200	535	UFA
usgs264	31.90953	-81.61294	NAD83	GA	LIBERTY	90,000	0.00075	calibrated radial model to multi-well pumping and recovery data entry UF 244 ft thick top 460 bottom 216	460	676	UFA
ggs178	31.86299	-81.61345	NAD27	GA	LIBERTY	124,000		As cited in Bush and Johnston (1988)	451	816	UFA
ggs180	31.74522	-81.40927	NAD27	GA	LIBERTY	160,000	0.0003	T=120000, S=0.00047 in recovery analysis	145	445	UFA
usgs261	31.90946	-81.61293	NAD83	GA	LIBERTY	100,000		Cooper-Jacob, straight-line method (1946);Drawdown data between 2.5 hours and 1 day seem to be affected by a recharge boundary or some large-scale aspect of the Upper Floridan aquifer and were not used to determine transmissivity.	460	560	UFA
usgs134	31.64855	-81.60094	NAD27	GA	LONG	250,000	0.00071		538	870	UFA
usgs152	30.83050	-83.28767	NAD83	GA	LOWNDES	37,000	0.0004	Vorhis (1961). Thickness of aquifer tested, 178 ft.			UFA
usgs135	30.91409	-83.25071	NAD27	GA	LOWNDES	94,000			195	450	UFA
usgs189	32.25405	-84.06630	NAD27	GA	MACON	2,580	0.00022		455	612	SCP
usgs188	32.25405	-84.06630	NAD27	GA	MACON	2,860			435	662	SCP
usgs136	31.60244	-81.30732	NAD27	GA	MCINTOSH	6,000			1144	1422	LFA
usgs040	31.09330	-84.78610	unk	GA	MILLER	145,140		written communication on fig 15, not in table A1	71	290	UFA
usgs030	31.10550	-84.66833	NAD83	GA	MILLER	21,000	0.001	Hayes and others (1983). Thickness of aquifer tested, 95 ft.			UFA
usgs312	31.35824	-84.11574	NAD27	GA	MITCHELL	75,000		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs313	31.36712	-84.19268	NAD27	GA	MITCHELL	61,200		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
ggs189	31.42490	-84.13824	NAD27	GA	MITCHELL	112,000		Principal artesian aquifer. From P.E. Lamoreaux and Associates, written commun., 1980.	250	250	UFA
usgs046	31.32250	-84.05333	unk	GA	MITCHELL	52,008		written communication on fig 15, not in table A1	83	497	UFA
usgs101	31.35567	-84.16252	NAD83	GA	MITCHELL	75,000	0.001	Hayes and others (1983). Thickness of aquifer tested, 131 ft.			UFA
usgs090	31.26333	-84.28433	NAD83	GA	MITCHELL	90,000	0.003	Hayes and others (1983). Thickness of aquifer tested, 140 ft.			UFA
ggs188	31.26101	-84.29185	NAD27	GA	MITCHELL	90,000		Principal artesian aquifer	190	190	UFA

usgs191	32.54000	-83.89750	unk	GA	PEACH	33,100			320	470	SCP
usgs190	32.54056	-83.89833	unk	GA	PEACH	35,100			320	490	SCP
usgs192	32.28127	-83.46573	NAD27	GA	PULASKI	9,820			306	361	SCP
usgs193	31.73600	-84.59325	NAD27	GA	RANDOLPH	3,330			320	435	SCP
usgs194	31.71044	-84.62047	NAD27	GA	RANDOLPH	2,420			336.4	426	SCP
usgs195	31.70767	-84.62131	NAD27	GA	RANDOLPH	5,910			338	475	SCP
usgs199	33.27500	-81.93167	unk	GA	RICHMOND	6,550	0.00057		360	613	SCP
usgs196	33.27510	-81.93163	NAD83	GA	RICHMOND	3,420			387	664	SCP
usgs198	33.27194	-81.93583	unk	GA	RICHMOND	7,650	0.00069		380	632	SCP
usgs200	33.39074	-82.00321	NAD83	GA	RICHMOND	3,150			140	170	SCP
usgs201	33.43375	-81.99651	NAD27	GA	RICHMOND	9,260			43	63	SCP
usgs202	33.37709	-82.02431	NAD83	GA	RICHMOND	6,880					SCP
usgs203	33.39251	-81.98945	NAD83	GA	RICHMOND	7,890			146	171	SCP
usgs197	33.27417	-81.93278	unk	GA	RICHMOND	4,950	0.00037		392	625	SCP
usgs204	32.96571	-81.62261	NAD27	GA	SCREVEN	3,500			370	565	SCP
usgs140	32.89044	-81.59511	NAD27	GA	SCREVEN	1,300			225	280	UFA
usgs139	32.89044	-81.59511	NAD27	GA	SCREVEN	5,600			155	205	UFA
usgs138	32.89044	-81.59511	NAD27	GA	SCREVEN	1,900			50	80	UFA
usgs137	32.75294	-81.63650	NAD27	GA	SCREVEN	4,100			150	301	UFA
usgs023	30.94517	-84.93133	NAD83	GA	SEMINOLE	41,000	0.0002	Hayes and others (1983). Thickness of aquifer tested, 107 ft.			UFA
ggs191	30.94685	-84.93298	NAD27	GA	SEMINOLE	41,000		Principal artesian aquifer	225	225	UFA
ggs190	30.89713	-84.89854	NAD27	GA	SEMINOLE	112,000		Principal artesian aquifer	98	150	UFA
ggs192	31.07435	-84.98632	NAD27	GA	SEMINOLE	27,000		Principal artesian aquifer	123	125	UFA
usgs017	31.06888	-85.00550	NAD83	GA	SEMINOLE	27,000	0.003	Hayes and others (1983). Thickness of aquifer tested, 67 ft.			UFA
usgs028	30.85717	-84.90000	NAD83	GA	SEMINOLE	112,000	0.001	Hayes and others (1983). Thickness of aquifer tested, 87 ft.			UFA
usgs275	31.05000	-84.88000	NAD27	GA	SEMINOLE	50,000	0.001	Cooper-Jacob or Theis.			UFA
usgs205	32.04488	-84.37047	NAD27	GA	SUMTER	3,540			185	860	SCP
usgs206	32.56139	-84.25861	unk	GA	TAYLOR	6,160			157.5	262.5	SCP
usgs207	31.77667	-84.44472	unk	GA	TERRELL	2,860			390	640	SCP
usgs045	31.70056	-84.31694	unk	GA	TERRELL	2,009		written communication on fig 15, not in table A1	76	150	UFA
usgs268	31.01158	-83.86850	NAD27	GA	THOMAS	170,000	0.00002	All tests assumed to be non-leaky and labeled as FAS due to lack of well construction data.			FAS
usgs062	31.00722	-83.87617	NAD83	GA	THOMAS	174,000		Sever (1969). Thickness of aquifer tested, 173 ft.			UFA
usgs212	32.68431	-83.47407	NAD27	GA	TWIGGS	34,000	0.00072		0	225	SCP
usgs208	32.69709	-83.55379	NAD27	GA	TWIGGS	8,710			250	430	SCP
usgs213	32.68348	-83.47296	NAD27	GA	TWIGGS	34,400	0.00081		0	225	SCP
usgs211	32.68959	-83.47073	NAD27	GA	TWIGGS	31,800	0.0008		0	225	SCP
usgs210	32.69070	-83.46712	NAD27	GA	TWIGGS	34,000	0.00082		0	225	SCP
usgs209	32.68709	-83.46907	NAD27	GA	TWIGGS	36,900			85	210	SCP
usgs214	32.68681	-83.46879	NAD27	GA	TWIGGS	31,600	0.00011		0	225	SCP
sjrwmd274	31.11828	-82.26540	NAD27	GA	WARE	574,960		Also R.E. Faye, USGS retired, written commun., 2002	636	1785	FAS

usgs141	31.11828	-82.26540	NAD27	GA	WARE	150,000		Originally published in Matthews and Krause (1984), who cited a T of 1,000,000 ft2/day. Re-analysis by Faye utilized here. 90% of flow from Upper Floridan.	636	1785	FAS
usgs133	31.09193	-82.26333	NAD83	GA	WARE	1,100,000	0.0001	Matthews and Krause (1984). Thickness of aquifer tested, 1288 ft.	625	1856	FAS
usgs142	33.04348	-82.94681	NAD27	GA	WASHINGTON	2,700		Screen intervals 36-41, 54-69, and 104-114; latter in Cretaceous strata	36	114	LFA
usgs143	33.01710	-82.95125	NAD27	GA	WASHINGTON	720		Screen intervals 33-43, 48-58, 133-138, and 190-200; latter two zones in Cretaceous strata	33	200	LFA
usgs215	33.03099	-82.87597	NAD27	GA	WASHINGTON	7,100			280	362	SCP
usgs216	33.03237	-82.87875	NAD27	GA	WASHINGTON	7,340			278	400	SCP
usgs151	31.65327	-81.83873	NAD27	GA	WAYNE	230,000	0.00041		493	1000	FAS
usgs150	31.65021	-81.83289	NAD27	GA	WAYNE	220,000	0.00018		500	1000	FAS
usgs148	31.65966	-81.83956	NAD27	GA	WAYNE	270,000	0.00049		486	1010	FAS
usgs147	31.66188	-81.84400	NAD27	GA	WAYNE	280,000	0.00048		480	1009	FAS
usgs278	31.65067	-81.83150	NAD83	GA	WAYNE	240,000	0.0005	Originally from Randolph and others, 1985, Comparison of aquifer characteristics derived from local and regional aquifer tests, Ground Water, 1985, v.23, no.3. Thickness of aquifer tested, 518 ft.			FAS
usgs145	31.61716	-81.90928	NAD27	GA	WAYNE	240,000	0.00059		472	584	UFA
usgs144	31.45550	-81.88122	NAD27	GA	WAYNE	270,000	0.00041		662	770	UFA
usgs146	31.51744	-81.87206	NAD27	GA	WAYNE	260,000	0.00035		587	691	UFA
usgs221	32.81459	-83.28433	NAD27	GA	WILKINSON	6,270	0.00043		90	300	SCP
usgs220	32.81237	-83.28238	NAD27	GA	WILKINSON	12,900	0.00077		70	280	SCP
usgs218	32.81403	-83.28238	NAD27	GA	WILKINSON	3,300			115	210	SCP
usgs217	32.82571	-83.07959	NAD27	GA	WILKINSON	10,500			225	302	SCP
usgs219	32.81375	-83.28294	NAD27	GA	WILKINSON	13,500	0.00055		90	300	SCP
usgs319	31.58323	-83.91823	NAD27	GA	WORTH	13,000		Well names taken from plate 1, transmissivity data taken from figure 5, well location data are from NWIS.			FAS
usgs049	31.59056	-83.83833	unk	GA	WORTH	17,589		written communication on fig 15, also K in table A1 matched T	160	520	UFA
usgs051	31.80806	-83.83639	NAD83	GA	WORTH	1,612		written communication on fig 15, not in table A1	96	260	UFA
usgs224	33.33778	-81.73306	unk	SC	AIKEN	8,740			445	690	SCP
usgs223	33.28639	-81.64861	unk	SC	AIKEN	23,500					SCP
usgs222	33.50528	-81.84722	unk	SC	AIKEN	12,200			160	200	SCP
usgs233	33.28722	-81.63944	unk	SC	AIKEN	26,300			660	850	SCP
usgs225	33.28722	-81.66972	unk	SC	AIKEN	33,700	0.00066		575	820	SCP
usgs158	33.11543	-81.56539	NAD27	SC	ALLENDALE	7,100			390	720	LFA
usgs153	33.01694	-81.30194	unk	SC	ALLENDALE	2,900			240	328	LFA
scdnr083	33.01694	-81.30194	unk	SC	ALLENDALE	3,300		Newcome rates test good	240	329	LFA
scdnr082	33.01833	-81.30889	unk	SC	ALLENDALE	3,300		Newcome rates test fair	154	444	LFA

usgs156	33.02500	-81.38417	unk	SC	ALLENDALE	1,200	0.0003		450	575	LFA
scdnr080	33.00750	-81.32083	unk	SC	ALLENDALE	3,900		Newcome rates test fair	290	340	LFA
usgs157	33.03972	-81.48861	unk	SC	ALLENDALE	1,100			460	794	LFA
usgs155	33.02500	-81.38417	unk	SC	ALLENDALE	970	0.00037		453	578	LFA
scdnr081	32.94306	-81.23917	unk	SC	ALLENDALE	500		Newcome rates test poor	257	344	LFA
usgs226	33.11543	-81.56539	NAD27	SC	ALLENDALE	7,100			390	715	SCP
usgs227	33.08833	-81.24139	unk	SC	ALLENDALE	3,920			180	310	SCP
usgs228	33.03972	-81.48861	unk	SC	ALLENDALE	1,100			460	470	SCP
usgs230	33.03972	-81.48861	unk	SC	ALLENDALE	214			556	566	SCP
usgs231	33.03972	-81.48861	unk	SC	ALLENDALE	263			629	639	SCP
scdnr084	33.28766	-81.04093	NAD27	SC	BAMBERG	670		Newcome rates test poor	140	364	LFA
scdnr085	33.19444	-81.05889	unk	SC	BAMBERG	1,700		Newcome rates test fair	46	260	LFA
scdnr086	33.10278	-81.00278	unk	SC	BAMBERG	670		Newcome rates test poor	94	225	LFA
scdnr087	33.32432	-81.14010	NAD27	SC	BAMBERG	1,300		Newcome rates test fair	162	296	LFA
scdnr088	33.31543	-81.13871	NAD27	SC	BAMBERG	800		Newcome rates test poor	162	302	LFA
scdnr097	33.22333	-81.58167	unk	SC	BARNWELL	6,700		Newcome rates test fair	360	605	LFA
scdnr092	33.23528	-81.36639	unk	SC	BARNWELL	11,000		Newcome rates test poor	218	327	LFA
scdnr091	33.26361	-81.25139	unk	SC	BARNWELL	800		Newcome rates test poor	290	345	LFA
scdnr099	33.22222	-81.55194	unk	SC	BARNWELL	1,500		Newcome rates test fair	230	374	LFA
scdnr100	33.22333	-81.61722	unk	SC	BARNWELL	170		Newcome rates test poor	260	270	LFA
scdnr090	33.36111	-81.27500	unk	SC	BARNWELL	4,100		Newcome rates test fair	204	470	LFA
scdnr098	33.22194	-81.55167	unk	SC	BARNWELL	1,100		Newcome rates test fair	262	335	LFA
scdnr093	33.23611	-81.37917	unk	SC	BARNWELL	4,700		Newcome rates test poor	180	320	LFA
scdnr094	33.24167	-81.38611	unk	SC	BARNWELL	5,900		Newcome rates test fair	220	315	LFA
usgs234	33.24959	-81.49205	NAD27	SC	BARNWELL	22,800					SCP
usgs232	33.39681	-81.40177	NAD27	SC	BARNWELL	13,000			490	680	SCP
usgs241	33.24833	-81.48722	unk	SC	BARNWELL	24,300					SCP
usgs235	33.24861	-81.49250	unk	SC	BARNWELL	19,400	0.00019				SCP
usgs237	33.24861	-81.49250	unk	SC	BARNWELL	19,800					SCP
usgs240	33.24833	-81.48722	unk	SC	BARNWELL	25,500	0.000073				SCP
usgs239	33.24833	-81.48722	unk	SC	BARNWELL	24,200					SCP
usgs238	33.24833	-81.48722	unk	SC	BARNWELL	25,500	0.000071				SCP
usgs236	33.24861	-81.49250	unk	SC	BARNWELL	20,300	0.00025				SCP
scdnr051	32.13750	-80.84944	unk	SC	BEAUFORT	40,000		Newcome rates test poor	140	242	FAS
scdnr052	32.13111	-80.84500	unk	SC	BEAUFORT	13,000		Newcome rates test excellent	441	638	FAS
scdnr054	32.13222	-80.86139	unk	SC	BEAUFORT	2,300		Newcome rates test poor	107	140	FAS
scdnr053	32.13139	-80.85250	unk	SC	BEAUFORT	40,000	0.0001	Newcome rates test poor	125	192	FAS
scdnr001	32.46444	-80.74056	unk	SC	BEAUFORT	3,600	0.00004	Newcome rates test poor	83	100	UFA
scdnr009	32.21972	-80.74556	unk	SC	BEAUFORT	110,000		Newcome rates test poor	146	226	UFA
scdnr008	32.23111	-80.75000	unk	SC	BEAUFORT	92,000		Newcome rates test poor	140	220	UFA
scdnr007	32.26770	-80.72261	NAD27	SC	BEAUFORT	6,700		Newcome rates test fair	227	890	UFA
scdnr006	32.31222	-80.68389	unk	SC	BEAUFORT	700		Newcome rates test good	295	632	UFA
scdnr005	32.30575	-80.68955	NAD27	SC	BEAUFORT	1,200		Newcome rates test fair	250	602	UFA
scdnr004	32.30694	-80.68667	unk	SC	BEAUFORT	530		Newcome rates test good	283	603	UFA

scdnr003	32.37389	-80.69306	unk	SC	BEAUFORT	16,000	0.0003	Newcome rates test fair	45	94	UFA
usgs154	32.46650	-80.72167	NAD83	SC	BEAUFORT	3,300	0.000035	Hayes (1979). Thickness of aquifer tested, n/a ft.			UFA
usgs229	32.43750	-80.57556	unk	SC	BEAUFORT	4,300		Newcome rates test fair	59	66	UFA
usgs159	32.41000	-80.77400	NAD83	SC	BEAUFORT	3,200	0.000013	Hayes (1979). Thickness of aquifer tested, 17 ft.			UFA
usgs254	32.26967	-80.83917	NAD83	SC	BEAUFORT	57,000	0.0003	Hayes (1979). Thickness of aquifer tested, 104 ft.			UFA
usgs253	32.31517	-80.47783	NAD83	SC	BEAUFORT	4,000		Hayes (1979). Thickness of aquifer tested, 58 ft.			UFA
scdnr023	32.57444	-80.75167	unk	SC	BEAUFORT	1,100	0.0001	Newcome rates test fair	124	224	UFA
scdnr010	32.22806	-80.72833	unk	SC	BEAUFORT	27,000		Newcome rates test poor	542	630	UFA
scdnr002	32.37444	-80.69361	unk	SC	BEAUFORT	13,000	0.0001	Newcome rates test good	52	88	UFA
scdnr056	32.28583	-80.92139	unk	SC	BEAUFORT	43,000		Newcome rates test fair	139	220	UFA
scdnr040	32.35778	-80.86167	unk	SC	BEAUFORT	4,000		Newcome rates test fair	298	600	UFA
scdnr041	32.33611	-80.91333	unk	SC	BEAUFORT	5,300		Newcome rates test good	314	582	UFA
scdnr042	32.33250	-80.89083	unk	SC	BEAUFORT	4,000		Newcome rates test fair	357	555	UFA
scdnr043	32.33056	-80.90889	unk	SC	BEAUFORT	53,000	0.0003	Newcome rates test fair	130	215	UFA
scdnr044	32.28556	-80.86056	unk	SC	BEAUFORT	8,200		Newcome rates test fair	353	490	UFA
scdnr045	32.29333	-80.86833	unk	SC	BEAUFORT	23,000		Newcome rates test poor	160	200	UFA
scdnr046	32.29778	-80.90278	unk	SC	BEAUFORT	3,500		Newcome rates test good	357	568	UFA
scdnr047	32.28250	-80.88528	unk	SC	BEAUFORT	23,000		Newcome rates test poor	160	200	UFA
scdnr048	32.26528	-80.86306	unk	SC	BEAUFORT	35,000		Newcome rates test good	140	205	UFA
scdnr011	32.22028	-80.70833	unk	SC	BEAUFORT	64,000		Newcome rates test poor	135	200	UFA
scdnr039	32.24833	-80.82861	unk	SC	BEAUFORT	78,000			101	380	UFA
scdnr021	32.16222	-80.73667	unk	SC	BEAUFORT	84,000		Newcome rates test poor	140	198	UFA
scdnr049	32.26250	-80.85472	unk	SC	BEAUFORT	18,000		Newcome rates test good	356	576	UFA
scdnr058	32.28944	-80.95611	unk	SC	BEAUFORT	4,400		Newcome rates test poor	321	523	UFA
scdnr059	32.28694	-80.98167	unk	SC	BEAUFORT	5,300		Newcome rates test fair	336	512	UFA
scdnr060	32.28278	-80.92528	unk	SC	BEAUFORT	7,200		Newcome rates test fair	299	450	UFA
scdnr101	32.32500	-80.46028	unk	SC	BEAUFORT	1,900		Newcome rates test poor	96	150	UFA
scdnr102	32.44111	-80.57556	unk	SC	BEAUFORT	2,900		Newcome rates test good	51	59	UFA
scdnr103	32.43389	-80.58222	unk	SC	BEAUFORT	2,500		Newcome rates test good	50	58	UFA
scdnr104	32.40083	-80.57556	unk	SC	BEAUFORT	5,600	0.0016	Newcome rates test good	73	78	UFA
scdnr105	32.36778	-80.61000	unk	SC	BEAUFORT	20,000	0.0001	Newcome rates test poor	64	66	UFA
scdnr106	32.36639	-80.60278	unk	SC	BEAUFORT	20,000	0.0003	Newcome rates test poor	55	70	UFA
scdnr107	32.33583	-80.62667	unk	SC	BEAUFORT	17,000	0.0001	Newcome rates test good	90	120	UFA
scdnr108	32.45500	-80.71806	unk	SC	BEAUFORT	790		Newcome rates test poor	120	170	UFA
scdnr050	32.24833	-80.84083	unk	SC	BEAUFORT	50,000		Newcome rates test fair	43	205	UFA
scdnr012	32.22722	-80.70222	unk	SC	BEAUFORT	94,000		Newcome rates test poor	131	200	UFA
scdnr019	32.17472	-80.72444	unk	SC	BEAUFORT	72,000	0.0001	Newcome rates test fair	145	200	UFA
scdnr018	32.18861	-80.71694	unk	SC	BEAUFORT	51,000		Newcome rates test poor	126	198	UFA
scdnr017	32.20472	-80.74917	unk	SC	BEAUFORT	11,000		Newcome rates test fair	316	320	UFA
scdnr055	32.10583	-80.86194	unk	SC	BEAUFORT	40,000		Newcome rates test poor	170	240	UFA
scdnr016	32.20194	-80.72556	unk	SC	BEAUFORT	67,000		Newcome rates test fair	118	200	UFA
scdnr038	32.24028	-80.81028	unk	SC	BEAUFORT	27,000		Newcome rates test poor	140	174	UFA
scdnr015	32.21222	-80.71306	unk	SC	BEAUFORT	80,000		Newcome rates test poor	110	200	UFA
scdnr014	32.21028	-80.70111	unk	SC	BEAUFORT	19,000		Newcome rates test good	314	600	UFA

scdnr013	32.23298	-80.67705	NAD27	SC	BEAUFORT	6,700		Newcome rates test poor	276	600	UFA
scdnr020	32.15611	-80.73222	unk	SC	BEAUFORT	80,000		Newcome rates test poor	145	221	UFA
scdnr024	32.51444	-80.81083	unk	SC	BEAUFORT	24,000	0.0002	Newcome rates test poor	83	140	UFA
scdnr025	32.45611	-80.76583	unk	SC	BEAUFORT	1,600		Newcome rates test fair	90	112	UFA
scdnr028	32.32575	-80.82344	NAD27	SC	BEAUFORT	7,000		Newcome rates test good	240	560	UFA
scdnr037	32.23333	-80.80000	unk	SC	BEAUFORT	11,000		Newcome rates test good	357	568	UFA
scdnr036	32.25250	-80.81972	unk	SC	BEAUFORT	24,000		Newcome rates test poor	140	200	UFA
scdnr035	32.25056	-80.82861	unk	SC	BEAUFORT	58,000			100	340	UFA
scdnr034	32.25222	-80.82833	unk	SC	BEAUFORT	56,000	0.0002	Newcome rates test good	97	209	UFA
usgs255	32.14882	-80.80583	NAD83	SC	BEAUFORT	52,000	0.003	Hayes (1979). Thickness of aquifer tested, 67 ft.			UFA
scdnr031	32.29194	-80.79361	unk	SC	BEAUFORT	13,000		Newcome rates test good	393	587	UFA
scdnr022	32.16167	-80.73667	unk	SC	BEAUFORT	99,000		Newcome rates test poor	140	200	UFA
scdnr029	32.30750	-80.82500	unk	SC	BEAUFORT	45,000	0.0004	Newcome rates test good	100	200	UFA
scdnr027	32.43833	-80.76389	unk	SC	BEAUFORT	11,000	0.0001	Newcome rates test fair	80	84	UFA
scdnr026	32.43750	-80.76000	unk	SC	BEAUFORT	4,000	0.0001	Newcome rates test fair	72	95	UFA
scdnr030	32.30444	-80.79583	unk	SC	BEAUFORT	11,000		Newcome rates test fair	397	587	UFA
usgs242	32.60000	-80.10611	unk	SC	CHARLESTON	3,400			2018	2210	SCP
scdnr061	32.82462	-80.69705	NAD27	SC	COLLETON	900		Newcome rates test poor	125	575	FAS
scdnr062	33.06722	-80.95389	unk	SC	COLLETON	2,000		Newcome rates test poor	450	510	LFA
scdnr079	32.75167	-81.24722	unk	SC	HAMPTON	12,000		Newcome rates test excellent	135	140	UFA
scdnr066	32.74778	-81.20889	unk	SC	HAMPTON	12,000	0.0002	Newcome rates test good	131	251	UFA
scdnr067	32.74944	-81.23750	unk	SC	HAMPTON	11,000		Newcome rates test good	125	160	UFA
scdnr063	32.87583	-81.11389	unk	SC	HAMPTON	1,200	0.0001	Newcome rates test fair	50	120	UFA
scdnr064	32.85972	-81.23667	unk	SC	HAMPTON	5,700		Newcome rates test poor		175	UFA
scdnr065	32.85944	-81.24167	unk	SC	HAMPTON	6,100		Newcome rates test fair	102	150	UFA
scdnr068	32.68083	-81.18833	unk	SC	HAMPTON	3,300		Newcome rates test fair	145	280	UFA
usgs086	32.16250	-81.11667	unk	SC	JASPER	39,000			280	971	UFA
scdnr057	32.29083	-80.94944	unk	SC	JASPER	6,000		Newcome rates test excellent	346	520	UFA
usgs034	32.36992	-80.91400	NAD27	SC	JASPER	48,000	0.0003	Newcome rates test good	145	330	UFA
scdnr070	32.53491	-81.07483	NAD27	SC	JASPER	51,000		Newcome rates test good	240	500	UFA
scdnr073	32.48556	-81.03028	unk	SC	JASPER	53,000		Newcome rates test fair	118	220	UFA
scdnr071	32.53000	-81.07306	unk	SC	JASPER	51,000	0.0004	Newcome rates test good	140	300	UFA
scdnr072	32.50194	-81.05889	unk	SC	JASPER	48,000		Newcome rates test poor	115	180	UFA
scdnr078	32.44667	-81.10222	unk	SC	JASPER	35,000		Newcome rates test poor	142	204	UFA
scdnr077	32.54306	-81.13556	unk	SC	JASPER	45,000		Newcome rates test excellent	252	555	UFA
scdnr076	32.54990	-81.13788	NAD27	SC	JASPER	56,000		Newcome rates test fair	252	545	UFA
scdnr075	32.27186	-81.08594	NAD27	SC	JASPER	67,000		Newcome rates test poor	208	400	UFA
scdnr074	32.46472	-81.04583	unk	SC	JASPER	36,000		Newcome rates test good	118	220	UFA
scdnr069	32.46639	-80.99333	unk	SC	JASPER	39,000		Newcome rates test poor	130	220	UFA