

The geologic framework and hydrologic characteristics of aquifers are important components for studying the nation's subsurface heterogeneity and predicting its hydraulic budgets. Detailed study of an aquifer's subsurface hydrostratigraphy is needed to understand both its geologic and hydrologic frameworks. Surface hydrostratigraphic mapping can also help characterize the spatial distribution and hydraulic connectivity of an aquifer's permeable zones. Advances in three-dimensional (3-D) mapping and modeling have also enabled geoscientists to visualize the spatial relations between the saturated and unsaturated lithologies.

This detailed study of two borehole cores, collected in 2001 on the Camp Stanley Storage Activity (CSSA) area (fig. 1), provided the foundation for revising a number of hydrostratigraphic units (HSUs) representing the middle zone of the Trinity aquifer (fig. 2). The CSSA area is a restricted facility that encompasses approximately 1,000 acres and is located in Borden, Texas, northwest of the city of San Antonio (fig. 1). Studying both the surface (fig. 3) and subsurface geology of the CSSA area are integral parts of a U.S. Geological Survey (USGS) project funded through the National Cooperative Geologic Mapping Program (NCGMP). This modification of hydrostratigraphic units is being applied to all subsurface data used to construct a proposed 3-D EarthVision (EV) model of the CSSA area and areas to the south and west (fig. 4).

There are multiple, and sometimes contrasting, meanings for HSUs. A HSU may imply a part of an aquifer, a select part of a groundwater or assessment model, or a geologic unit with distinct hydraulic properties. One of the reasons for this ambiguity is that a hydrostratigraphic unit is a term that never gained formal status within the stratigraphic community. The usage of hydrostratigraphic terminology is also inconsistent within the geologic community and its meanings can diverge depending on whether surficial or bedrock geology is involved. Hydrostratigraphic unit boundaries can also be indistinct because they are not true stratigraphic contacts and may reflect lateral facies changes. For this report, a HSU is defined as a body of rock with distinct hydrologic properties (such as porosity) that is mappable (traceable) over considerable distance.

Two well sites, MW9-C5 and 5S-1/G9, were cored by the CSSA and logged by the USGS to depths of more than 470 and 450 feet, respectively (figs. 5 and 6). Close examination of the geophysical log for MW9-C5 designated the study type log, fig. 5, and detailed descriptions of the core (table 1) has helped refine the hydrostratigraphy developed for the middle Trinity aquifer by Parsons Corporation, Austin, Texas. Parsons' original designations for all HSU units are labeled in black and are used in this report. The designations for the two HSU units in the middle Trinity aquifer are the MW9-C5 log (fig. 5). Both in this report and in Parsons' designations, the lower member of the Glen Rose Limestone is divided into six HSUs, designated units "A" through "F". Although Parsons divided the Bear Shale and the Cow Creek Limestone Members of the Permian Formation into two HSUs, designated "A" and "B" (figs. 6 and 6), the authors saw little or no difference in lithology between these two units; therefore, we treat the Bear Shale and Cow Creek Limestone Members as single, undivided hydrostratigraphic units.

The core from site MW9-CC (fig. 5) contains hydrostratigraphic units assignable to the lower part of the Glen Rose Limestone (from about 15 to 326 feet). The core also includes the Bexar Shale and Cow Creek Limestone Members of the Pearsall Formation as well as the uppermost part of the Hammatt Shale Member of the Pearsall Formation (fig. 2). Core from MW9-CC was slabbbed, photographed, and described in detail (see table 1), and more than 100 thin-section samples were collected throughout its length. The core from site MW5-LGR contains HSUs assignable to the lower member of the Glen Rose as well as the uppermost part of the Bexar Shale (fig. 6).

In addition to identifying hydrostratigraphic units for the lower member of the Glen Rose in well MWS-LGR, 52 one-by-two-inch core plugs were collected throughout its core and sent to Weatherford Laboratories (Golden, Colorado) for helium-gas injection porosity analyses (fig. 6 and table 2). Porosity values for the lower Glen Rose range from as low as 6.0 percent to as high as 30.2 percent with a mean porosity value of 17.8 percent. The helium-injection porosity values and porosity estimates from neutron geophysical logs (table 3) can be used to construct a future 3-D EV property model for the area encompassed by figure 4.

Barker, R.A., and Ardis, A.F., 1996, Hydrogeologic framework of the Edwards-Trinity aquifer system, west-central Texas: U.S. Geological Survey Professional Paper 1421-B, 61 p.

Clark, A.R., Blome, C.D., and Faith, J.R., 2009, Map showing the geology and hydrostratigraphy of the Edwards aquifer catchment area, northern Bexar County, south-central Texas: U.S. Geological Survey Open-File Report 2009-1008, 24 p., 1 pl.

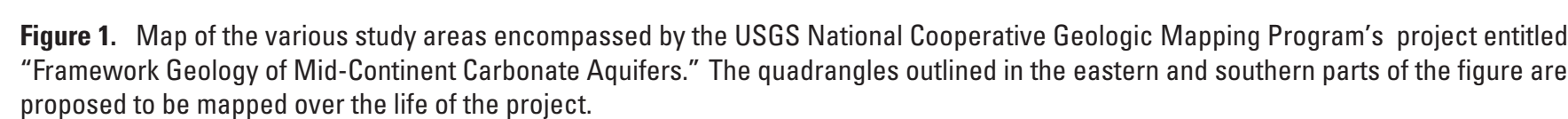
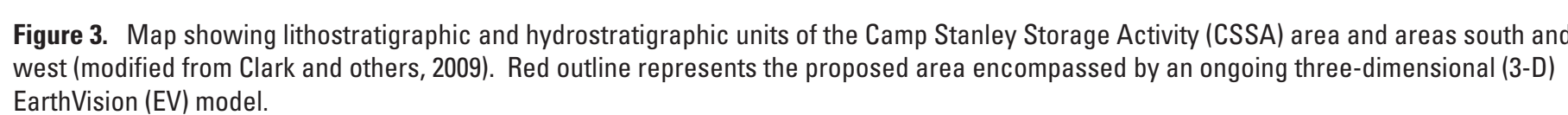
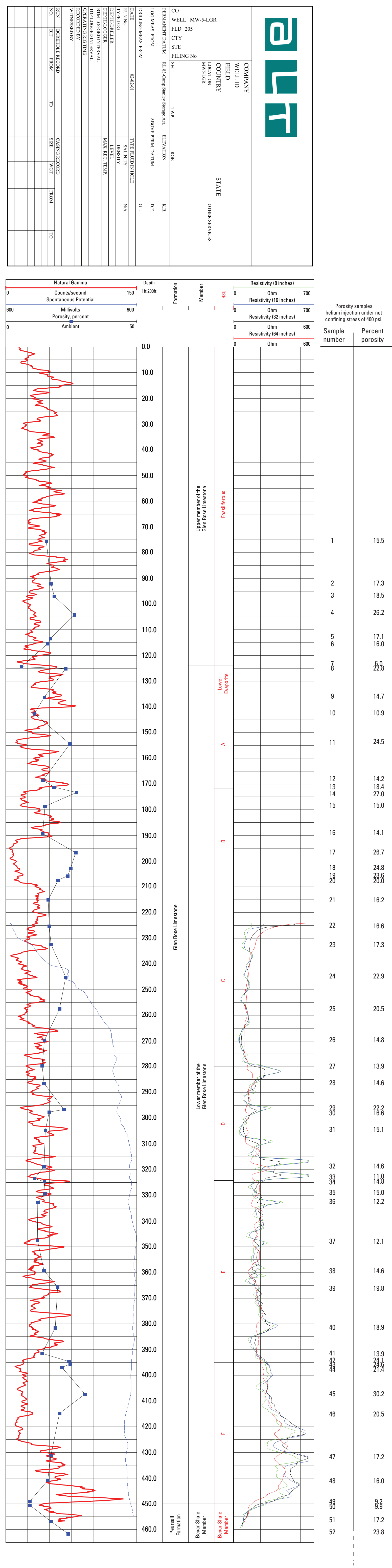
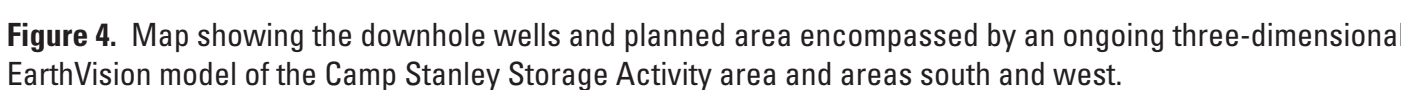

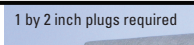


Figure 2. Lithostratigraphy of the Trinity aquifer in northern Bexar County, Texas (modified from Barker and Ardis, 1996).

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SUMMARY OF ROUTINE CORE ANALYSES RESULTS					
USGS WISDOM USGS LHA 014 Undershot/Left				Undershot Location US: CA 02400 Core: 0502011	
Sample Number	Depth, Feet	Permeability, mD		Porosity, %	Core Density, g/cc
		in situ	Coreface		
1	70.55	0.048	0.048	15.5	16.4
2	72.15	0.081	0.082	15.1	17.2
3	90.95	0.157	0.161	16.0	16.9
4	104.50	408	378	20.7	26.1
5	113.25	0.058	0.058	16.1	16.9
6	114.00	0.022	0.031	16.0	15.9
7	124.25	0.043	0.038	16.4	17.5
8	124.15	0.054	0.054	22.8	27.2
9	138.50	0.019	0.018	14.7	14.8
10	145.05	0.137	0.066	10.8	10.8
11	154.50	0.448	0.462	24.5	24.8
12	185.20	0.037	0.043	14.2	14.1
13	171.25	0.096	0.084	16.8	17.2
14	172.35	1.28	1.01	24.1	26.9
15	178.75	0.082	0.055	15.8	16.9
16	186.05	0.013	0.041	14.5	17.1
17	200.75	561	561	26.6	27.1
18	205.15	261	261	25.6	27.1
19	207.40	0.038	0.034	20.6	20.7
20	215.00	0.422	0.202	16.2	16.8
21	232.25	0.094	0.094	16.2	16.8
22	234.40	0.048	0.047	11.9	11.2
23	240.10	0.483	0.483	20.5	20.6
24	257.20	0.195	0.139	20.5	20.4
25	260.55	0.022	0.015	14.6	14.6
26	272.55	1.15	0.878	14.6	15.9
27	286.40	0.096	0.096	14.6	14.6
28	296.05	8.12	6.57	22.2	27.1
29	307.60	0.162	0.168	18.5	19.0
30	348.65	0.081	0.040	15.1	15.0
31	378.60	0.040	0.040	14.6	14.6
32	322.40	0.085	0.10	17.1	17.1
33	324.30	0.277	0.354	16.7	16.9
34	307.15	0.075	0.075	16.8	16.8
35	307.30	0.075	0.075	16.8	16.8
36	299.20	0.167	0.167	16.8	16.8
37	299.20	0.167	0.167	16.8	16.8
38	299.20	0.167	0.167	16.8	16.8
39	281.50	3.75	3.19	18.8	21.1
40	281.50	3.75	3.19	18.8	21.1
41	281.50	3.75	3.19	18.8	21.1
42	286.00	4.14	3.31	24.1	24.1
43	286.00	4.14	3.31	24.1	24.1
44	286.00	3.15	2.21	21.4	21.2
45	407.35	9.15	8.73	21.5	28.1
46	414.80			28.5	27.1
47	403.35			28.5	27.1
48	408.90			28.5	27.1
49	408.90			28.5	27.1
50	402.90			28.5	27.1
51	408.80	0.801	0.622	17.1	18.3
52	408.80	14.4	11.8	22.8	27.1
Average average:					
		14.7	13.3	17.8	18.2

* Indicates the sample is unusable due to this type of measurement

Table 2. Helium injection porosity analyses from well MW5-LGR, Weatherford Labs, Golden, Colorado. psi, pounds per square inch; NCS, Net Confined Stress; gm/cc, grams per cubic centimeter.

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