

Nonplastic sandy soil derived from fluvial deposits of Pleistocene age

AM24

Nonplastic to slightly plastic sandy and silty soil derived from fluvial deposits of Pleistocene age

Z

Poorly drained organic swamp soil

AR/Z

Flood-plain deposits associated with swamp deposits

AM2/Z3

Nonplastic to slightly plastic sandy soil derived from fluvial deposits of Pleistocene age associated with AM23 soil

AM2/Z2A

Nonplastic to slightly plastic sandy soil derived from fluvial deposits of Pleistocene age associated with AM24 soil

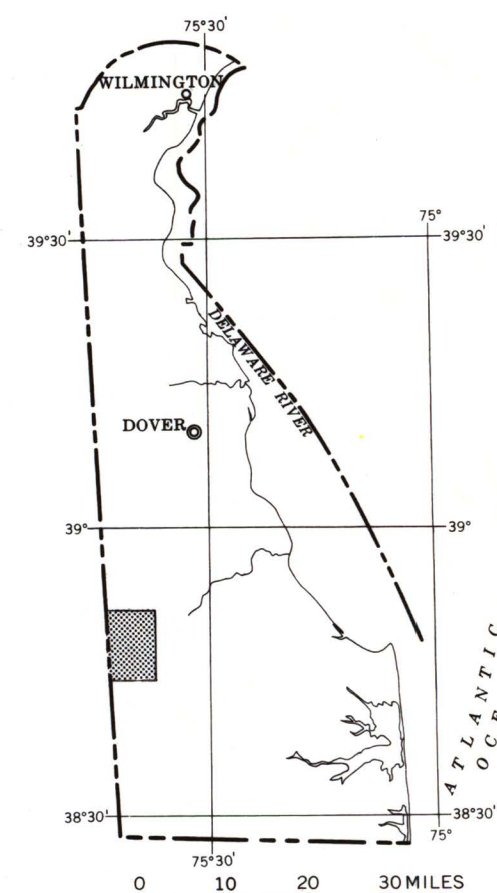


FIGURE 1.—Index map of Delaware showing location of the Hickman Area

TABLE 1.—*Explanation of letter symbols*

Symbol	Explanation
AM	Surficial alluvial mantle, Pleistocene age
AR	Recent alluvial deposit.
Z	Swamp deposit.

The map symbols used in this report to designate the various types of soils are a modification of the system used in the engineering soil survey of New Jersey (Rogers, 1956). The first part of the symbol is a letter, or group of letters, which identifies the soil type. The second part of the symbol is a number developed by Lueder (1950) (see table 1). The second part of the symbol is a number which identifies the soil group according to the classification system adopted by the Highway Research Board (American Association of Highway Engineers, 1945) and the Delaware State Highway Department (see table 2). A two-digit number indicates that two soil types are present within the same soil profile; for example, the symbol A-2B-1 implies that both A-2 and A-1 soils occur together in the same soil profile, but usually in different horizons.

Two different soil symbols may be combined by a diagonal bar (AM2/A4). A diagonal bar indicates that two soil types (AM2 and A4) are present in the same soil profile, but are not necessarily within the same profile. The two soils are so frequently intermixed that they cannot be mapped separately.

Allen, Harold, and others, 1945, Report of committee on classification of materials for subgrades and granular type roads: Highway Research Board, 25th Ann. Mtg. Oklahoma City, 1946, Highway Research Board Proc., v. 25, p. 375-388, Washington.

Lueder, D. R., 1950, A system for designating map-units on engineering soil-maps in soil exploration and mapping: Highway Research Board Bull. 28, p. 17-35, Washington.

Rogers, F. C., 1955, Engineering soil survey of New Jersey. Report No. 1: Rutgers Univ. Eng. Research Bull. 15, 114 p., New Brunswick, N. J.

FIGURE 2.—Hydrograph showing average depth to water in 13 water-table wells in Delaware. November 1955, period of measurement in Kent County; October 1960, period of measurement in Sussex County

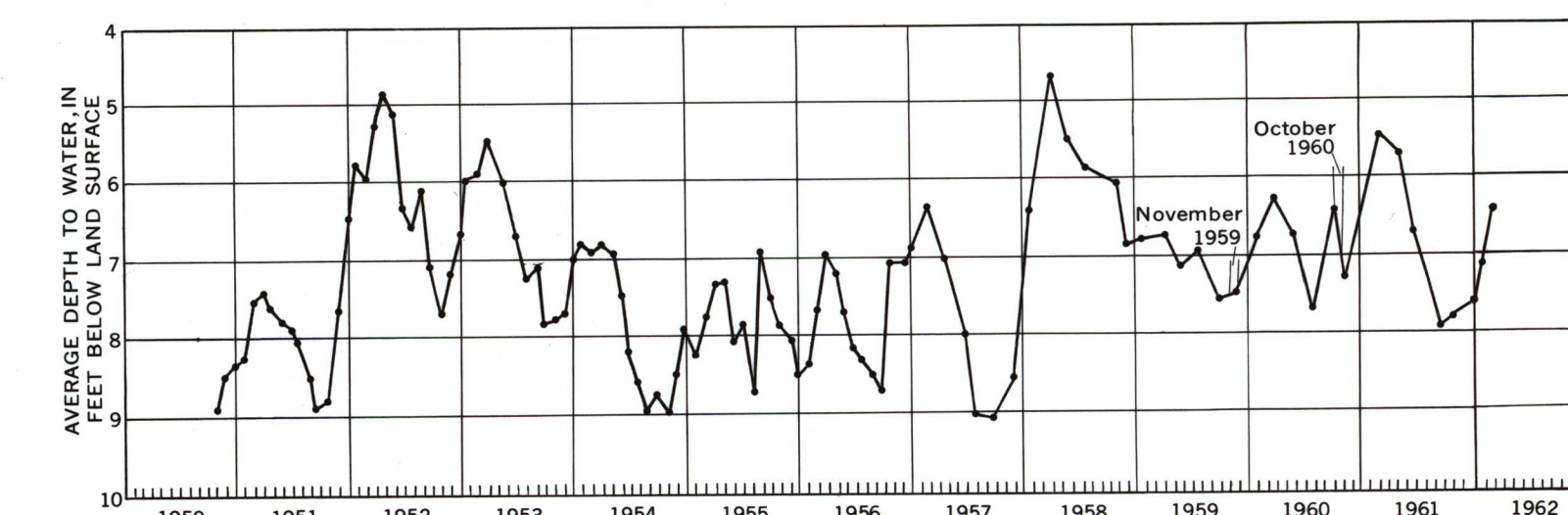


FIGURE 2.—Hydrograph showing average depth to water in 13 water-table wells in Delaware. November 1955, period of measurement in Kent County; October 1960, period of measurement in Sussex County

TABLE 2.—Soils classification

General classification	Granular materials (35 percent or less passing a No. 200 sieve)							Silt-clay materials (more than 35 percent passing a No. 200 sieve)				
Group classification	A-1		A-3	A-2				A-4	A-5	A-7		A-8
	a	b		4	5	6	7			1	2	
Sieve analysis Percent passing No. 10 sieve No. 40 sieve No. 200 sieve	50 max 10 min	10 max 5 min	10 max 5 min	35 max 10 min	35 max 10 min	35 max 10 min	35 max 10 min	35 max 10 min	38 min 5 max	38 min 5 max	38 min 5 max	38 min 5 max
Characteristics of fraction passing No. 10 sieve Liquid limit Plasticity index	6 max	6 max	Nonplastic	40 max 10 min	41 max 10 min	40 max 11 min	41 max 11 min	40 max 11 min	40 max 11 min	41 max 11 min	41 max 11 min	41 max 11 min
Group index ^a	0	0	0	0	0	4 max		8 max	12 max	10 max	20 max	
General subgrade rating	Excellent		Good	Good				Poor	Poor	Poor	Poor	Unsatisfactory
Material	Well-graded gravel and sand		Clean sand and gravel	Poorly graded, silty or clayey sand and gravel				Silty sand	Plastic clay	Plastic clay	Nonplastic clay	Most plastic

The group index is calculated according to the following formula: Group index = $0.2a + 0.006ac + 0.013d$

In which: a = That portion of the percentage passing No. 200 sieve greater than 15 percent and not exceeding 75 percent, expressed as a positive whole number (1 to 40);

b = That portion of the percentage passing No. 200 sieve greater than 15 percent and not exceeding 55 percent, expressed as a positive whole number (1 to 40);

c = That portion of the numerical liquid limit greater than 40 and not exceeding 60, expressed as a positive whole number (1 to 20);

d = That portion of the numerical plasticity index greater than 10 and not exceeding 30, expressed as a positive whole number (1 to 20).

TABLE 3.—Results of laboratory analyses of soil samples

		Liquid limit: N_L , nonliquid										Plasticity index: N_P , nonplastic													
		Mechanical analyses																						Classification	
Sample no.	Depth of test, ft.	Cumulative percent by weight passing chart (sampled)	No. 40 (d_{40})					No. 60 (d_{60})					SH (0.002 to 0.0075 mm)	Clay (<0.00075 mm)	Liquid limit	Plas- ticity index	Maximum liquid limit (w_{Lmax} , per cu. ft.)	Optimum moisture content (w_{opt} , percent by weight)	Classification	Remarks					
			7/4	4.75	0.075	0.0475	0.025	SH	CH	SH	CH	SH									CH	SH	CH		
100	0-35	100	100	100	100	100	6.7							NI	NP	117	indefinite	A-3	(3)						
	15-40	100	100	100	100	100	8.1	2						4	NI	NP	111	indefinite	A-3	(3)					
101	30-46	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	30-46	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	10-26	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	10-26	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	10-26	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	10-26	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
	10-26	100	100	100	100	100	8.1	3						2	NI	NP	109	6	A-3	(3)					
104	0-31	100	100	100	100	100	8.1	3						2	NI	NP	122	6	A-4	(3)					
	0-31	100	100	100	100	100	8.1	3						2	NI	NP	122	6	A-4	(3)					
1A	0-12	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	0-12	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
1B	10-10	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	10-10	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
1C	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
1D	0-14	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	0-14	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2A	13-72	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	13-72	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2B	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2C	36-60	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	36-60	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2D	0-13	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	0-13	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	30-73	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2A	6-42	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	6-42	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
2C	13-45	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
	13-45	99.3	100	100	100	100	14.0	2.4						<40	<10	118		A-4	(3)						
4A	0-15	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	0-15	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	30-73	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
4B	30-73	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	30-73	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
4C	30-73	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	30-73	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
4D	0-8	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	0-8	100	100	100	100	100	8.7	3						<40	<10	118		A-4	(3)						
	10-73	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
1C	13-48	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
	13-48	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
	13-48	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
	13-48	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
	13-48	100	100	100	100	100	8.7	3						9	NP	NP	109	A-3	(3)						
1D	14-44	100	100	100	100	100	8.7	3						<10	<10	118		A-4	(3)						
	14-44	100	100	100	100	100	8.7	3						<10	<10	118		A-4	(3)						
	14-44	100	100	100	100	100	8.7	3						<10	<10	118		A-4	(3)						
	14-44	100	100	100	100	100	8.7	3						<10	<10	118		A-4	(3)						
	14-44	100	100	100	100	100	8.7	3						<10	<10	118		A-4	(3)						

¹Based on AASHTO (American Association of State Highway Officials) Designation: T319-41.

TABLE 4.—Characteristics of the engineering soil types in the Hickman Area

Soil Type ^a	Description	Origin	Engineering properties				Suitable compaction equipment
			In place Suitability as a subgrade ^b	In place Suitability as a wearing surface ^b	Removable ^c Suitability as embankment material ^b	Removable ^c Compaction characteristics	
A M2	Nonplastic to slightly plastic sandy soil	Fluvial deposits of Pleistocene age	Good	Excellent to good depending on binder present.	Good	Good	Rubber-tired equipment.
A M3	Nonplastic, generally poorly graded sandy soil	Fluvial deposits of Pleistocene age	Good to fair	Excellent to good depending on binder present if surface is A-2. Poor if surface is A-3.	Good if predominant material is A-2. Fair if predominant material is A-3.	Good if predominant material is A-2. Poor if predominant material is A-3.	Rubber-tired equipment for soils which are predominantly A-2. Vibratory equipment for soils which are predominantly A-3.
A M4	Nonplastic to slightly plastic, sandy and silty soil	Fluvial deposits of Pleistocene age	Good if material left after grading is predominantly A-2. Poor if material left after grading is predominantly A-4.	Excellent to good depending on binder present if surface is A-2. Poor if surface is A-4.	Good if predominant material is A-2. Fair if predominant material is A-4.	Good if predominant material is A-2. Poor if predominant material is A-4.	Rubber-tired equipment.
A M5	Nonplastic to highly plastic, sandy and clayey soils	Fluvial deposits of Pleistocene age	Good if material left after grading is predominantly A-2. Poor if material left after grading is predominantly A-4 or if poorly drained A-6.	Good if surface is A-2. Poor if surface is A-4. Varied A-6.	Fair if predominant material is A-2. Poor if predominant material is A-4.	Fair if predominant material is A-2. Poor if predominant material is A-4.	Rubber-tired equipment for soils which are predominantly A-2. Poor rollers for soils which are predominantly A-4.
A M6	Nonplastic to highly plastic, sandy and silty soil	Fluvial deposits of Pleistocene age	Pair	Fair if surface is A-2. Fair to poor if surface is A-4.	Pair. Good if A-2 and A-4 are combined as well graded materials. Poor if predominant material is A-4.	Good if A-2 and A-4 are combined as well graded materials. Poor if predominant material is A-4.	Vibratory equipment for soils which are predominantly A-2. Rubber-tired equipment for soils which are predominantly A-4.
A M7	Slightly plastic to highly plastic, silty and clayey	Fluvial, glacial, and lacustrine deposits of Pleistocene age	Poor if material left after grading is predominantly A-4. Poor if material left after grading is predominantly A-6.	Fair if surface is A-4. Very poor if surface is A-6.	Poor if predominant material is A-4. Very poor if predominant material is A-6.	Poor	Shoe's foot rollers.
A R	Alluvial gravel, sand, silt and clay	Alluvium of Recent age	Variable	Variable	Variable	Variable	Variable.
Z	Soil rich in organic material and frequently poorly drained. May be unstable as shallow depths by gravel, sand or clay.	Swamp deposits of Recent age	Variable	Variable	Variable	Variable	Variable.

³For soil types designated by two-digit numbers, these columns refer to the composite soil.

INTERIOR—GEOLOGICAL SURVEY, WASHINGTON, D. C.—1964—W 63316