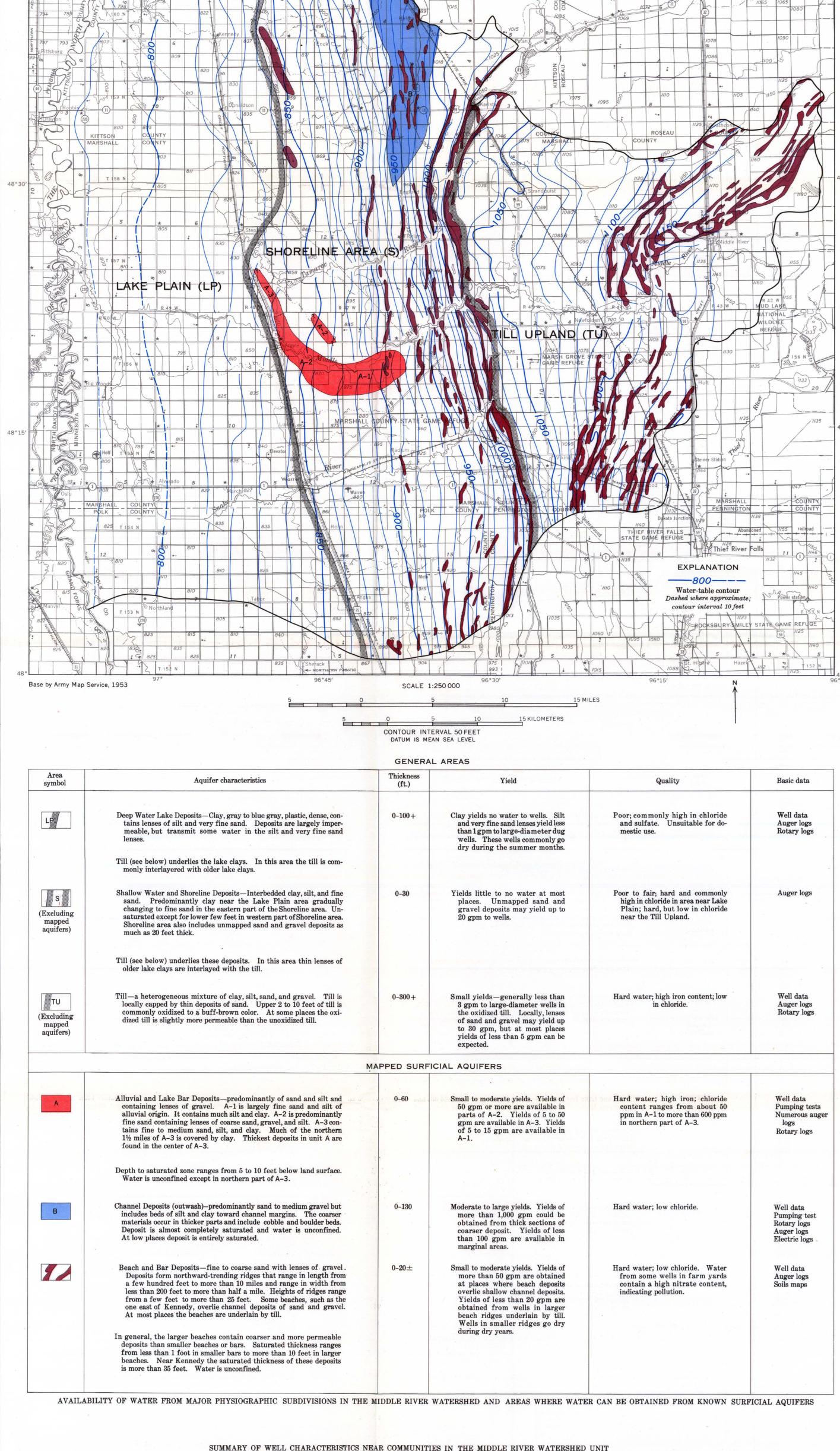


						AR	EAS IN THE MIDDI	LE RIVER WATERSH	HED WHERE WATE	ER CAN	BE O	BTAINED FROM KN	IOW:	N SUBSURFACE AQ	UIFI	ERS			
e e								APPRAISALS O	F MAJOR AQUIFER	RS									
					Source			Hydra	nulic coefficients										
				Natural Precipitation	Underflow		Potential sources of replenishment due to development			Average coefficient of aquifer				Storage		Use ir		ions of gallons r year	
						Undernow													8
Area	Map key	Areal extent (square miles)	Estimated infiltration of precipitation to aquifer (in./sq. mi.)	Remarks	Water moving into and out of aquifer (acre-ft/year)	Remarks	Derived from storage in confining beds	Diversion from surface water	Salvage from evapotranspiration	T (gpd/ft)	S	Remarks	Total (billions of gallons)	Remarks	Municipal and domestic	Industrial and	Commercial	Total	Water potential
Argyle- Stephen	Alluvial and lake-bai deposits (Area A or map showing water availability in sur- ficial aquifers.)		2 to 4	Estimated on basis of high infiltration capacity of soils. Annual recharge ranges from 2,350 to 4,700 acre-feet depending upon climatic conditions.		Computed by Darcy's Law using estimated coefficient of transmissibility for contributing water-bearing formations.	Pr pro	It is possible to divert sur- face water into aquifer by maintaining surface storage in channel of the Middle River east of Argyle. Water could seep into the aquifer when cone of depression reaches surface storage.	Pumpage near Middle River east of Argyle will salvage some water dis- charge to springs or loss by evapotranspiration within the channel.) 0.1 (est.)		acre-ft.)	Only a small part of water storage is economically available.	9.0	3.0	2.0	5 12.5 (38 acre-ft.)	Based on aquifer replenishment, more than twice the annual rate of pumpage could be developed from aquifer. The most favorable area for development is A-2. Natural discharge is largely by evapotranspiration.
Beach Ridge area about 4 miles east of Kennedy	Beach Ridge (see map showing water availability in sur- ficial aquifers.)		2 to 4	Estimated on basis of high infiltration capacity of sandy soils and low surface runoff. Annual recharge ranges from 320 to 640 acre-feet depending upon climatic conditions.		Computed by Darcy's Law using estimated coeffi- cient of transmissibility for contributing water- bearing formations.			Pumpage will decrease natural discharge by evapotranspiration.) 0.1 (est.)		0 acre-ft.)	Only a small part of storage can be utilized economically.		2.4	0.2	10.9 (33 acre-ft.)	Aquifer is largely undeveloped. It could sustain yields at more than double the present usage.
Halma-Lake Bronson	Channel Deposit (see Area B on map showing water availability in sur- ficial aquifers.)		1 to 4	Estimated on basis of moderate to high infiltration capacity. Watertable aquifer throughout most of area. It is confined toward the western edge. Recharge ranges from 2,100 to 8,400 acre-feet per year.		Computed by Darcy's Law using estimated coefficient of transmissibility for contributing water-bearing formations.	Potential sources near the western border.	Lake Bronson and South Branch of Two Rivers are a potential source of significant recharge to ground-water reservoir. Usable storage in Lake Bronson is 3,700 acre- feet. Average flow of South Branch of Two Rivers is 65.6 cfs. Low flow of 5 cfs or less is common during August and September. Amount of diversion possible cannot be determined from available data.	Pumpage near Lake Bronson or in northern part of aquifer could reduce evapotranspiration losses.	100,000 +	0.1	Largest transmissibility occurs in the thicker part of the aquifer.	(2,800,000 acre-ft.) 66	Storage within the Middle River Watershed Unit.	1.2			3.1 (9.5 acre-ft.)	Aquifer is undeveloped and has the largest potential capacity. It is a potential source of water for irrigation and industrial purposes.
Newfolden	Sand bed within till (Area D on map showing water availability in sub- surface aquifers.)		to 2	Estimated on infiltration capacity of soil. Aquifer is confined in western half. Natural recharge from precipitation occurs in eastern half of aquifer.		Computed by Darcy's Law using estimated coefficient of transmissibility for contributing water-bearing formations.	Leakage of water stored in overlying confining beds is a potential source of recharge in the western half of the aquifer.	Diversion potential from surface to ground water is low because of low permeability of till with- in the channel of the Middle River.							8.4	6.8	3.9	9 19.1 (58.5 acre-ft.)	Not feasible to estimate water potential from available data. No declines in well yields are reported at present rate of pumpage. Nearly all well owners report plenty of water for their uses.
Alvarado	Sand bed within till (Area F on map showing water avail- ability in subsurface aquifers.)					Computed by Darcy's Law using estimated coefficient of transmissibility for contributing water-bearing formations.	A small amount of water could leak into the aquifer from overlying glacial till. Lake clay would yield practically no water.					***	Unknown		6.0	2.5	5 5.3	2 13.7 (42 acre-ft.)	Adequate supplies for present rate of use. Owners report decline in flows of many older wells.



	Well owner	Well location				×					Hydraulic				Quality				35	
Community		5 <u></u> 흥			Rate of pumping (gpm)	Duration of tests (hours)	Drawdown (ft)	Specific capacity (gpm/ft)	Method of analysis for hydraulic coefficients	Available drawdown (ft)	coeffici T (gpd/ft)	ents ₁	Well depth (ft)	Size	Fe (ppm)	CI (ppm)	Hardness as CaCO ₃ (ppm)	рН	Remarks	Aquifer texture and range in depth, in feet below land surface
Warren YSD 13Q	U.S.G.S test well	NE		55 47		48	35	6.25	Time, drawdown, recovery	56	16,000	0.0001	110	8 in.	0.68	252	132	7.6		Sand and gravel; 65-103'
	Municipal	NE	11 1	55 47	250	24	47	5.3	• >	70			112	10 in.					80.5 ft. casing, 30 ft. screen.	Sand and gravel; 65-103'
	Municipal	NW	1 1	54 48	60	14			P.		The second secon		151	8 in.	y = 16			1 14	15 ft. of 8-inch screen. Pumped about 29,000 gallons per day	White, fine sand; 133-151'
	Municipal (standby)	SW	36 1	55 48	75	3	y-1			*		*	158	8 in.			36	1	Stand-by well	Gravel; 150-158'
Stephen	U.S.G.S test well	NW	27 1	57 48	45	25	31	1.5	Time-drawdown, recovery	38	5,000	0.05	70	4 in.		59	357	7.6	Sand packed well, 4-inch screen from 50-70 feet	Fine sand; 10-70'
a 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Test well	SE	21 1	57 48	45	24	10.7	4.2	Time-drawdown, recovery	11	8,000	0.0001	46	4 in.		870	2,920	7.4	Sand packed well, 4-inch screen from 21-46 feet	Fine to medium sand; 21-46'
Argyle	Village well, north	SE	10 1	56 48	31 (est.)	1	3	30	Specific capacity	3	6,000	0.1 (est.)	16	10 feet square	3.2	20	370	8.4	WPA dug well	Medium sand and gravel;10-26'
7.18310	Village well, south	NE	15 1	56 48	30		in the state of th						18	6 feet diam.					Well will pump dry	Sand, fine; 12-22'
Kennedy	Village	SE	27 1	60 48	62 (rept.)	7	2.2	28	Specific capacity	4			24	6.5 feet square	0.04	47	340	8.7	WPA dug well	Sand and gravel; 0-24'
Alvarado	Village	NW	5 1	54 49	145 (rept.)	12	35 (rept.)	4.1					158	8 in.	1.0	600	490	7.8	7 feet of 8-inch screen. Well flowed for a period after com- pletion	Sand and gravel 151-158'
	School		_	54 49			150+		. 1				162	6 in.					Flowing well in 1955	Gravel
Strandquist	Village	SW	22 1	58 45	20 (rept.)	24	100 (rept.)	0.2		358			362		0.63	62	50	7.9	4 feet of 40-slot screen	Fine sand; 358'-362'
otianuquist	School	SW	22 1	58 45	10	2	44	0.25	Time-drawdown, recovery	300	Less than 500	0.0001 (est.)	308	6 in.						Sand
liddle River	Village	NW	11 1	57 43	100			3		229			244	6 in.	0.42	13	230	7.6	10 feet of 6-inch screen—50 slot 5 feet of 6-inch screen—40 slot	Gravel; 230'-244'
	School	NW	11 1	57 43	36	61		0.6	Specific capacity	204	1,000		227	6 in.					Not used. 4 feet of screen	Gravel; 210'-227'
11.11	Co-op Creamery	SE	32 1	56 43	15	1/4	12	1.3	Specific capacity	265	2,000		290	6 in.	0.93	10	265		No screen	Sand and gravel
Holt	Village	SW	33 1	56 43		er e	110						240	6 in.			1.0		Well not connected to distribution system. Adequate yield	
Newfolden	Village		-	56 44	(rept.)	1	60	1.7	Specific capacity	95			121	8 in.	0.28	10	210	7.8	10 feet of screen	Sand
	Co-op Creamery	NW	8 1	56 44	30	12		v I		90			100	6 in.	*	4 8			Adequate	Sand
Viking	Village	NW	26 1	55 45	40 (rept.)								180	6 in.					Pumps into a pressure tank of 850-gallon capacity	Sand
	Co-op Creamery	SW	26 1	55 45	12	1/2	3.3	3.65	7.1	130	-		158	6 in.					Adequate	Sand

restriction of the aquifer increases drawdown and leakage into aquifer decreases drawdown. Pumping of nearby well increases drawdown.

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