

GEOPHYSICS BRANCH

Geophysics Branch Copy

AUG 17 1955

U. S. DEPARTMENT OF THE INTERIOR

GEOLOGICAL SURVEY

ELECTRICAL RESISTIVITY MEASUREMENTS IN THE NEILLSVILLE AREA, WISCONSIN

By

H. Cecil Spicer and George J. Edwards

Prepared in cooperation with the Wisconsin Geological Survey

GEOPHYSICS BRANCH REPORT 55-2

Released to Open Files AUG SI 1955

This report and accompanying illustrations are preliminary and have not been edited or reviewed for conformity with Geological Survey standards and nomenclature.

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ELECTRICAL RESISTIVITY MEASUREMENTS

IN THE NEILLSVILLE AREA, WISCONSIN

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ABSTRACT

Sixty-eight electrical depth profiles were completed in the vicinity of Neillsville, Wis. to obtain information on the water-bearing beds in the glacial moraine and consolidated sedimentary rocks in the area. No productive aquifers were found but the best areas for test drilling are described. The basic theory and interpretation procedures, together with a short description of field methods on electrical resistivity measurements are also presented.

INTRODUCTION

The Neillsville area, in west-central Wisconsin, has long been deficient in water. Most of the wells drilled so far in the area are either dry or yield insufficient water. As a part of 'the investigation of the ground-water resources of Wisconsin being made in cooperation with the Wisconsin Geological Slrrvey, University of Wisconsin, a ground-water study of that area was undertaken. In connection with that study, an electrical resistivity investigation was made.

The primary purpose of the project was to obtain information on the occurrence of aquifers in the thick sandstone deposits of the area or in the terminal moraine southeast of Neillsville. Other objectives were to

locate any gravel deposits present; to determine the character, depth, and thickness of such material beneath the surface; and to select promising sites for drilling test holes.
Neillsville is in the south-central part of Clark County, in west-

central Wisconsin. The resistivity measurements were made in T.24 N., R. 2 W., of the 4th principal meridian, mainly in the northeastern part of the township (fig. 1).

Work on the project started July 23, 1950 and continued over a period of three weeks, ending August 11 . The field measurements were made by George J. Edwards assisted by Herbert C. Spicer, Jr., and employees of the city of Neillsville. Preliminary interpretations of the apparent resistivity curves were made in the field to make it possible to choose the most favorable sites for drilling tests holes. The final interpretations were made and the report prepared by H. Cecil Spicer.

The assistance and cooperation extended to us by the city of Neillsville are gratefully acknowledged.

GEOLOGY OF THE AREA

The underlying rock of the area near Neillsville is either gneiss, gneissic granite, granite, or diorite. On the uneven, eroded surface of these crystalline rocks there was deposited marine sandstone to a depth of several hundred feet. Afterrthe area was uplifted from the sea, erosion removed much of the sandstone and valleys were cut which probably

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extended through the sandstone and into the crystalline rocks. The topography was again modified by glaciation and the surface vas covered with drift varying in thickness from a few feet to more than 125 feet. Some of the hills of the area owe their relief to a rock cora covered with thick terminal moraine. Numerous out-crops of crystalline rocks occur along both Black River and O'Neill Creek.

The ground water of this area has been found in only small quantities, inadequate for the growing needs of the area. The crystalline rocks of the area cannot be considered as possible aquifers. The sandstone above the granitic rocks was considered a possible aquifer because of its extent and thickness as well as the large amount of recharge possible from a considerable area of near-surface rock .. The glacial drift is not a very promising source for an aquifer because of the large amount of clay contained therein. The best source for ground-water supplies would be in a deposit of outwash sand and gravel in a buried stream valley, if such could be located in the area.

Instrumentation and Field Methods

The Gish-Rooney type earth resistivity apparatus, with modifications by H. Cecil Spicer, was used to make the resistivity measurements. Vertical depth profiling was used throughout the study in order to obtain

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all the information possible about the materials beneath the surface. E lectrodes were set in the earth according to the modification of the Wenner arrangement as proposed by $F.$ W. Lee (1929). Measurements of potential were made by both the Wenner (1915) and Lee (1929) techniques thus giving three measurements at each interval. The apparent resistivities were computed by the Wenner (1915) formula $\beta_{a}^{a} = 2\pi a \frac{E}{I}$ for all the observations, thus giving three apparent resistivity curves which when plotted are spread on the chart thus making them more accessible for interpretation; however, the curve form remains the same. The three resistivity curves thus obtained are termed Full, P-1 and P-2. Bearings for the depth profiles are referred to true north and are given for the P-1 direction. Altitudes are expressed as heights above mean sea level. ..

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INTERPRETATION OF THE RESISTIVITY CURVES

An apparent resistivity curve expresses graphically the behavior of an electrical field impressed on the earth. The curve by means of its slope, inflections, and other characteristics enables a determination to be made of the material beneath the surface of the earth.

The method of interpretation applies to resistivity curves of two,
three, and more layers. The theory of images, as given by Jeans (1925) and others, is fundamental. Theoretical aspects relating to the application of images to resistivity curves are given by Hummel (1931). Two

layer resistivity curves and as many methods of interpreting them will be found in papers by Roman (1931) . Three layer resistivity curves will be found in an article by Wetzel and McMurry (1937) , and the use of two-layer curves and Wetzel and McMurry three-layer curves to aid in the interpretation of three and more curves is completely explained by Watson and Johnson (1938) . Assistance in understanding their t atment of image theory will be found in an article by Watson (1934), The method described by Tagg (1937) is useful at times for certain types of resistivity curves. Examples of its application will be found in the reference cited and in Heiland (1940) and in the present paper.

SUMMARY OF FIELD MEASUREMENTS AND INTERPRETATIONS

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Sixty-eight depth profiles were completed in the Neillaville area. A few depth profiles were repeated in an attempt to get satisfactory measurements, but the cause of the erratic behavior was not always located. The centers of the depth profiles and the directions of the electrode lines are shown on figure 1, the circle representing the center and the line through the circle the direction. The filled circles on this figure indicate the location of wells or drill holes which were used in trying to correlate the resistivity interpretations with the geologic materials. Except for a few wells, the information is of little assistance because the descriptions on the well logs or drill logs were

inadequate or missing. The complete listing of locations and descriptions of the drilling information is given in the appendix. Surface contours from a map by the Wisconsin Geological Survey are also given on figure 1.

Short depth profiles were completed on or just above outcrops of the rocks in the area. These are indicated by concentric circles designated T-1 to T-5 on figure 1. The computed resistivities obtained from these tests were used in correlating the interpretations obtained from the apparent resistivity curves with the geological materials. The following resistivities were obtained from measurements on the granite in a quarry: on the weathered surface, 55,800 ohm cms; weathered at shellow depth, 18,600 ohm cms; depth greater than 12 feet, 137,200 chm oms; unweathered surface, $1,249,350$ ohm cms. Tests on the sandstone gave the following resistivities: weathered surface, 21,200 ohm oms; depth greater than 10 feet, $212,000$ ohm cms; unweathered surface, $105,200$ ohm oms.

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Interpretations of the resistivity curves giving a description of the materials and depths to each material will be found in the appendix. Altitudes on the surfaces of the sandstone and granite along with their thicknesses are given in Table 1. The altitudes on the sandstone surface are shown also on figure 2 for each resistivity depth profile; these altitudes are from table 1, colunm 3. Shown also on figure 2 are the wells and drill holes in which sandstone was reported.

TABLE 1

ALTITUDES ON SURFACE, SANDSTONE, AND GRANITE WITH THICKNESSES.

TABLE 1
(Cont.)

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The thickness of the sandstone from the drilling information and the resistivity interpretations is shown on figure 3. These thicknesses are from table 1, column 6. It is evident from figure 3 that there are two areas where the sandstone has greater thickness than elsewhere and these areas are shown encompassed by dotted lines on this figure. Only four drill holes are reported to have penetrated through the sandstone to the granite in these areas.

Figure 4 shows the altitudes on the crystalline rocks and was prepared from the values of table 1, column 4. Information from twelve drill holes having no sandstone but giving the depths to granite is also included on the figure. It is apparent that the thick area of sandstone, particularly the easterly one shown on figure 3, is directly related to the depression in the granitic rocks, shown on figure $4.$ The shape of the thick sandstone mass of the westerly area is similar to that of the depression in the granite and, had there been more information about the depth to granite available, the two probably would have had the same appearance on both figures thus more completely establishing the same relationship which was found in the easterly area.

The appearance of the contours drawn on the bedrock surface and thickness of the sandstone above the bedrock are altered somewhat in the complete interpretations of the resistivity curves from those obtained by the preliminary ones which were made during the progress of the field observations.

On the basis of the preliminary estimates of the resistivity curves, two areas were selected as most promising for test drilling. One is in what appeared to be the area of thick sandstone and the other is in the moraine southeast of Neillsville. Such drilling would give much better information to correlate the geologic materials and. the interpretations from resistivity measurements, and, furthermore, the areas chosen also appeared to be the most likely ones for obtaining water, but it was emphasized that they held little promise as adequate water-bearing areas •

Drill hole 48 was completed in the autumn of 1950. According to the sample log, see appendix, it had 32 feet of sandstone and the amount of water produced was unreported so it is presumed to be too small to be useful for a large-capacity well. This drill hole was put down near re sistivity depth profile D-2. It was estimated, in the preliminary interpretations, that the sandstone would have a thickness of more than 200 feet there. The correlation between the drill log and the resistivity interpretations is definitely negative. No explanation for this situation can be offered other than the observer must have taken the measurements of resistivity over or alongside an apparently unnoticed and unreported buried conductor.

Drill hole 49 was completed in 1951 and was located near resistivity depth profile L-3. The correlation between the two sets of observations here is considered only fair. Interpretations of the resistivity

observations show no evidence of sandstone, but the depth to granite is very close; 150 feet by resistivity and 152 1/2 feet by drilling. No water is reported in this well, but a well less than $1/4$ mile NNW. from this drill hole, number 47 , is stated to have water with a probable capacity of 100 gpm and, apparently, this water comes from a sand at a depth of 106 to 171 feet.

Well number 47 is located approximately midway between resistivity depth profiles $K-3$ and $L-3$ and only a short distance from drill hole number 44 . The depth to granite at K-3 was 125 feet, at L-3 was 150 feet, and at number 44 was 154 feet, but at number 47 the granite was not reached at 171 feet. Consequently, it seems probable that a buried channel may be present near this drill hole and further exploration near it might discover a useful aquifer.

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Another area appears in the completed interpretation to be a possible area for drilling to discover an aquifer. It is located in the northeastern part of section 1 near resistivity depth profiles I-1 and I-2. Unfortunately, these observations are at the northern most limits of the area investigated so it is not possible to estimate the extent of the gravels found there. These gravels may be associated with those known to be present in the gravel pit of SE $1/4$ NW $1/4$ section 1, and, if they are, a sizeable aquifer might be present.

The electrical-resistivity measurements made in this area were not successful in locating a productive aquifer in either the sandstone or the glacial moraine. Three areas, though, are pointed out as possibilities for drilling to discover an aquifer; one in gravels, one in sandstone, and one in the glacial moraine. However, the area is one where little ground water can be expected because the sandstone is of low porosity and in most places interbedded with shales; the gravel deposits are scarce and, insofar as found, mostly near the surface; and the moraine is largely composed of clay which makes it a poor to valueless material for an adequate aquifer.

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APPENDIX

Well Records in T. 24 N. R. 2 W.

See map for location

Well records continued

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Well Logs

Well 44· 552 feet N., 12.5 feet E. of SW. corner sec. 13, T.24 N., R.2 W.

Well 45. SE corner NE 1/4 NE 1/4 sec. 23, T. 24 N., R.2 W. SE. corner Clark County Fair Grounds.

Description Depth in feet

Clay and "hardpan"; red brown Li1 0 - 27

Well 46 . At house $1/5$ mile west of N. $1/4$ cor. section 24.

Well 47. East of Neillsville on U. S. Highway 10 across road from Fair Ground.

Well 48. SW. of center NW 1/4 sec. 12, T. 24 N., R. 2 W, 1950.

Well 49. NW $1/4$ NW $1/4$ sec. 24, T. 24 N., R. 2 W. 1951.

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Geologic Materials as Determined

from Resistivity Curve Interpretations

in T. 24 N., R. 2 W.

Line A-1. 550 feet E. of $1/4$ line, 390 feet S. of NW. cor. SE $1/4$ SW $1/4$ sec. 12. Altitude 1,100 feet. P-1 N. 880 E.

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Line B-1. SE. cor. NW 1/4 SE 1/4 sec. 12. Altitude 1,100 feet. $P-1$ N. 770 E.

Line B-2E. 67 feet E. of SW. cor. NE $1/4$ SW $1/4$ sec. 12. Altitude 1,100. P-1 N. 88° E.

Abandoned; interference from surface conductor.

Line B-2. NW cor. SW 1/4 SW 1/4 sec. 12. Altitude 1,075 feet. P-1 N. 870E.

Line B-3. NE cor. SW $1/4$ SE $1/4$, 40 feet S. and 0.05 mi. W. of cor. sec. 11. Altitude 1,050 feet. P-1 N. 900 E.

 $Line B-4.$ SE. cor. SW $1/4$ NW $1/4$ SE $1/4$ sec. 10. P-1 N. 0° E. Altitude 1,020 feet.

NE. cor. SE $1/4$ SE $1/4$ sec. 9. Altitude 1,066 feet. P-1 N. Line B-5.
 $\frac{\text{Line B-5}}{\text{O}^{\text{O}}$ E.

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Line B-6. NE. cor. SW $1/4$ SE $1/4$ sec. 9. Altitude 1,100 feet. P-1 S. 45° E.

Line C-1. NW. cor. *NW 1/4 SE 1/4 sec. 12.* Altitude 1,075 feet. P-1 N. 86^OE.

Line C-2. NW. cor. NE 1/4 NE 1/4 SE 1/4 sec. 11. Altitude 1,038 feet. $P-1$ N. 90^o E.

<u>Line C-3</u>. 150 feet N. of SW. cor. SW 1/4 NE 1/4 sec. 11. Altitude 1,030 feet. P-1 N. 63⁰ E.

<u>Line C-4</u>. 57 feet W. of SE. cor. SW $1/4$ NE 1/4 sec. 10. Altitude, 1,042 feet. P-1 N. 90⁰ E.

<u>Line C-5</u>. NW. cor. SE $1/4$ NW $1/4$ SE $1/4$ sec. 9. Altitude 1,082 feet.
P-1 N. 72^o E.

Line D-1. SE $1/4$ SW $1/4$ NE $1/4$ sec. 12, 800 feet N. of $1/2$ line. Altitude $1,100$ feet. P-1 N. 0° E.

Line $D-1W$. 216 feet E. of $1/4$ line, 0.275 mile S. of road, NW. cor. SW $1/4$ NE $1/4$ sec. 12. Altitude 1,090 feet. P-1 N. 0° E.

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Line D-2. *NW.* cor. SE 1/4 sec. 12. Altitude 1,040 feet. P-1 N. O^o E. Interference from buried conductor evident on curve; interpretation impossible to correlate with log of well 48.

Line D-3. NW cor. SE $1/4$ NE $1/4$ sec. 12. Altitude 1,075 feet. P-1 N. 90[°] E.

Line D-3W. 76 feet W. of SE. cor. NE 1/4 NW 1/4 sec. 11. Altitude 1,033 feet. \overline{P} -1 N. 90⁰ E. **有部分路** Seria.

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Line D-3W2.

Line D-3N. 702 feet E. and 590 feet N. 22^o W. of SW. cor. NE $1/4$ NE $1/4$ sec. 11. Altitude 1,075 feet. P-1 N. 220 W. \mathcal{L}_{max}

Line $D-4$. 384 feet W. of SE. cor. NE $1/4$ NE $1/4$ sec. 10. Altitude 1,045. $\overline{\text{feet}}$. $\overline{\text{P}}$ -1 S. 87⁰ E.

SW. cor. NW $1/4$ NE $1/4$ sec. 10. Altitude 1,060 feet. P-1 S. Line $D-5$.
770 E.

<u>Line D-6</u>. SW. cor. NW 1/4 NW 1/4 sec. 10. Altitude 1,055 feet. P-1 N. 0° E.

<u>Line D-7</u>. NW. cor. SW 1/4 NE 1/4 sec. 9, 120 feet S. of creek. Altitude $1,055$ feet. P-1 N. O^O E.

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Line E-1. NE. cor. SE $1/4$ SW $1/4$ sec. 1, 0.175 mile N. of road. Altitude 1,110 feet.

Line E-2. NW. cor. NW $1/4$ NW $1/4$ sec. 12, 420 feet E. of $1/4$ line and 0.05 mi. S. of road. Altitude 1,090 feet. P_T1 N. 88⁰ E.

Line E-3. SE. cor. SW $1/4$ SW $1/4$ sec. 1, 100 feet N. and 27 feet E. of corner. Altitude 1,050 feet. P-1 N. OO E. ~ 6

Line E-4. NE. cor. NW 1/4 NE 1/4 sec. 2. Altitude 1,058 feet. P-1 N. 90° E.

Line E-5. SW. cor. SE $1/4$ SW $1/4$ sec. 3, 255 feet N. of corner. Altitude 1,090 feet. P-1 N. 90° E.

SE. cor. SW $1/4$ SW $1/4$ sec. 3. Altitude 1,088 feet. P-1 N. Line E-6.
90⁰ E.

• <u>Line E-7</u>. 390 feet S₂ of road and NW. cor. NE $1/4$ NW $1/4$ sec. 9. Altitude 1078 feet. $P-1 N \cdot 90^{\circ} E$.

 $Line E-8.$ 400 feet S. of NE. cor. NW $1/4$ NW $1/4$ seo. 9. Altitude 1,060 feet. P-1 N. 88° E.

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● <u>Line F-1</u>. NE. cor. SW $1/4$ SE $1/4$ sec. 1. Altitude 1,090 feet. P-1 N. 900 E. Abandoned because of interference from buried conductor ..

Line F-1W. 200 feet W. of NE. cor. SW $1/4$ SE $1/4$ sec. 1. Altitude 1,095 feet. P-1 N . 90⁰ E.

Line F-2. 284 feet S. of NE. cor. SW $1/4$ SW $1/4$ sec. 1. Altitude 1,110 feet. $P-I$ N. O^O E.

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Line F-3. SE cor. NW $1/4$ SE $1/4$ sec. 2. Altitude 1,040 feet. P-1 N 0[°] E.

Line F-4. 376 feet E. of road, 0.15 mile to SW cor. sec. 2. Altitude 1,040 feet. P-1 N. 88º E.

Line F-5. NE. cor. SE 1/4 SE 1/4 sec. 3. Altitude 1,080. P-1 N. 90° E.

<u>Line F-6</u>. 15 feet N. of SW. cor. NW $1/4$ SW $1/4$ sec. 3. Altitude 1,120 feet. P-1 N. 90⁰ E.

<u>Line F-7</u>. 397 feet E. of SW. cor. NW 1/4 SE 1/4 sec. 4. Altitude 1,093 feet. P-1 N. 90^o E.

Line $F-8$.
90⁰ E. SE. cor. NE $1/4$ SE $1/4$ sec. 5. Altitude 1,075 feet. P-1 N.

 $P-1 N. 0^0 E.$ Line G-1. 0.5 mile N. SE cor. sec. 1. Altitude 1,100 feet.

Line G-2. NE. con. NE $1/4$ SW $1/4$ sec. 1. Altitude 1,100 feet. P-1 N. 90⁰ E.

Line G-3. SE $1/4$ NE $1/4$ sec. 2. Altitude 1,080 feet. P-1 N. 20^o E.

<u>Line G-4</u>. 195 feet S. of $1/4$ line, 350 feet W. of NE. cor. NW $1/4$ SE $1/4$ sec. 2. Altitude 1,025 feet. P-1 N. 850 E.

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Line G-5. 325 feet S. of road and NE. cor. NW $1/4$ SE $1/4$ sec. 3. Altitude 1,100 feet. P-1 N• 0° E. •

Line G-6. 550 feet N. of SW. cor. SE $1/4$ NW $1/4$ sec. 3. Altitude 1,130 feet. $P-1 N. 0^{\circ} E.$

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<u>Line G-7</u>. 566 feet S. and 173 feet E. of NW. cor. NE $1/4$ SE $1/4$ sec. $4.$ Altitude 1,120 feet. P-1 N. oo E.

Line $G-8$. 219 feet S. of road and NW. cor. NE $1/4$ SW $1/4$ sec. 4. Altitude 1,100 feet. P-1 N. 90° E.

Line H-1. 0.15 mile W. of road and NE. cor. $\frac{W}{1/4}$ SE 1/4 NE 1/4 sec. 1. Altitude 1,100 feet. P-1 N. 90^o E.

Line H-2. SE. cor. NW 1/4 NW 1/4 sec. 1. Altitude 1,100 feet. P-1 N. O E.

<u>Line H-3</u>. NE. cor. NW 1/4 SW 1/4 NE 1/4 sec. 2. Altitude 1,022 feet
P-1 S. 50^o E.

<u>Line I-1</u>. NE. cor. NE $1/4$ on N. side of road. Altitude 1,100 feet. $P-1$ N. 90^o E.

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Line I-2. NE cor. NE $1/4$ NW $1/4$ sec. 1, N. side of road. Altitude 1,125 feet. $P-1$ N. 90 $^{\circ}$ E.

Line I-3. *300* feet S. of NW. cor. NW 1/4 NW 1/4 sec. 1. Altitude *1,nqn* f eet. $P-1$ S-87⁰ E.

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<u>Line I-4</u>. Opposite NW. cor. NE 1/4 NW 1/4 sec. 3. Altitude 1,055 feet. $P-1 N. O^O E.$

 $\begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$ <u>Line I-5</u>. 305 feet W. and 196 feet S. of NE. cor. NW $1/4$ NE $1/4$ sec. 4 . Altitude 1,100 feet. P-1 N. 85° E.

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Line I-6. 218 feet N. of NE. cor. NW 1/4 NW 1/4 sec. 4. Altitude 1,060 feet. $P-1 S. 80⁰ E.$ $\lambda \sim \sqrt{2}$

Line J-1. 0.35 mile W. of NE. cor. SE 1/4 sec. 13. Altitude 1,050 feet $P-1 N.90^{\circ} E.$

<u>Line J-2</u>. 0.85 mile W. of NE. cor. SE $1/4$ sec. 13. Altitude 1,038 feet.
P-1 N. 90⁰ E.

Line K-1. NW. cor. SE $1/4$ SE $1/4$ sec. 13. Altitude 1,110 feet. P-1 N. 90⁰ E.

Line K-1N. 486 feet S. of road and NE.
Altitude 1,090 feet. P-1 N. 2⁰ W.

Line K-2. NW. cor. SW $1/4$ SE $1/4$ sec. 13. Altitude 1,105 feet. P-1 N. 0° E.

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<u>Line K-2W</u>. 90 feet E. of SW. cor. NE $1/4$ SW $1/4$ sec. 13. Altitude 1,105 feet. P-1 N. 90° *E.*

<u>Line K-3</u>. 210 feet N. 45° W. of SE. cor. NE 1/4 SE 1/4 1,100 feet. P-1 S. 45° E. sec. Altitude

<u>Line L-1</u>. SE. cor. SE 1/4 SE 1/4 sec. 13. Altitude 1,135 feet. P-1 N.
90⁰ E.

<u>Line L-2</u>. NE. cor. NE 1/4 NW 1/4 sec. 24. Altitude 1,130 feet. P-1 N.
90⁰ E.

<u>Line L-3</u>. 685 feet S. of road and NW. cor. NW 1/4 NW 1/4 sec. 24 Altitude 1,162 feet. P-1 N. 0⁰ E.

