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A PROGRAM TO COMPUTE AQUIFER-RESPONSE COEFFICIENTS

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A PROGRAM TO COMPUTE AQUIFER-RESPONSE COEFFICIENTS

BY

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ABSTRACT

An alternating direction technique is used to solve finite difference equations approximating the flow of water in an aquifer. The solutions produce response coefficients relating pumping from wells to drawdowns within those wells. The product of the response coefficient with the pumping values produces a linear algebraic technological function that can be used for integrating hydrologic phenomena into planning and management models.

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Introduction

This program, written in FORTRAN IV for the IBM 360 or 370 series computers, calculates the response coefficients for one or more wells over a set of specified time periods called the design horizon. For convenience the time period selected represents the length of time during which the rate of pumping of a well remains constant. The program may simulate 1) a confined aquifer or 2) an unconfined aquifer providing the drawdown is small in relation to the saturated thickness (transmissivity is thus independent of the drawdown). The aquifer may have irregular shaped boundaries and non-homogeneous transmissivity. Vertical components of flow in the aquifer should be negligible compared to the horizontal components of flow. The response functions calculated for the wells are used to determine drawdown averaged over the area represented by a node. No well bore correction term is present in this version of the program.

Application

This program may be used to calculate response coefficients relating pumping to drawdown. The response coefficients are valid only if the following characteristic behavior and restrictions are followed.

1. The region of interest is underlain by a single aquifer.
2. The aquifer may be treated as a two-dimensional flow system.
3. Drawdowns relative to the saturated thickness are always small (transmissivity is essentially independent of drawdown).
4. The storage coefficient throughout the aquifer may be treated as a constant.
5. There is no land subsidence and water is instantly released from storage.

6. The boundaries may be regular or irregular in shape.
7. The transmissivity may be nonhomogeneous but isotropic.
8. The aquifer may have constant head boundaries.
9. Time is broken up into equal intervals called pumping periods. Within a pumping period, the well must pump at a constant rate. Any period of time up to 2 years is allowable as a pumping period.
10. A well may occupy any node position of the grid imposed on the plan view of the aquifer. The node point represents an area. The response coefficient calculated for a node may represent the effect of more than one well. The number of wells at a node does not vary over the design horizon.
11. The natural recharge and discharge to and from the aquifer are not disrupted by the pumping from wells.
12. Wells may be assumed to fully penetrate the aquifer.

Theory

The satisfying of the above conditions is sufficient to insure that the aquifer's response to pumping stress can be modeled with a linear ground water model. It is therefore possible to construct response coefficients that relate pumping at wells to the drawdown in those wells (Maddock, 1972). The coefficients exist even if the aquifer has irregularly shaped boundaries or nonhomogeneous flow parameters, such as transmissivity and storage coefficient.

The coefficients for an aquifer penetrated by M wells is derived as follows. When the previous stated conditions hold, flow within the aquifer is modeled by the partial differential equation (Maddock, 1972):

$$\nabla \cdot [T(\hat{x}) \nabla s(\hat{x}, t)] = S(\hat{x}) \frac{\partial s}{\partial t}(\hat{x}, t) - \sum_{j=1}^M Q'(\hat{x}_j, t) \delta(\hat{x} - \hat{x}_j) \quad (1)$$

where \hat{x} is the point (x, y) of observation, $T(\hat{x})$ is nonhomogeneous transmissivity, $S(\hat{x})$ is nonhomogeneous coefficient of storage for a confined aquifer or specific yield for an unconfined aquifer, $s(\hat{x}, t)$ is the drawdown at point \hat{x} at time t , $Q'(\hat{x}_k, t)$ is the instantaneous discharge at the k^{th} well at time t , and $\delta(\hat{x} - \hat{x}_j)$ is a Dirac delta function. Assuming no previous development, the initial condition on drawdown is

$$s(\hat{x}, 0) = 0 \quad \hat{x} \text{ within and on boundary} \quad (2)$$

If there are not rivers or streams present and if the pumping does not interfere with the natural recharge and discharge from the aquifer, the boundary conditions are

$$\frac{\partial s}{\partial n}(\lambda) = 0 \quad (3)$$

where λ is a parameter indicating that $\partial s / \partial n$ is evaluated on the boundary. The boundary is irregular in shape, n is the normal direction and $\partial s / \partial n(\lambda)$ is the gradient of the drawdown for the normal to the boundary. If there are constant head conditions on portions of the boundary λ' , the boundary conditions on that portion are

$$s(\lambda') = 0 \quad (4)$$

Equation (1) and its initial and boundary conditions are linear, hence there exists a Green's function such that

$$s(\hat{x}, t) = \int_{\forall \hat{x}} \int_0^t G(\hat{x}, \hat{x}', t-\tau) F(\hat{x}', \tau) d\hat{x}' d\tau \quad (5)$$

where

$$F(\hat{x}', \tau) = \sum_{j=1}^M Q'(\hat{x}_j, \tau) \delta(\hat{x}' - \hat{x}_j) \quad (6)$$

Let the design period consist of N equal duration time periods of length η . When $Q'(\hat{x}_j, \tau)$, $j=1, \dots, M$, are constants between the i^{th} and $i-1^{\text{th}}$ time periods, $i=1, \dots, N$ the drawdown at the k^{th} well at the end of the n^{th} time period, rewritten $s(k, n)$, is given by the equation

$$s(k, n) = \sum_{j=1}^M \sum_{i=1}^n Q(j, i) \int_{(i-1)\eta}^{i\eta} G(\hat{x}_k, \hat{x}_j, n\eta - \tau) d\tau \quad (7)$$

where

$$Q(j, i) = Q'(\hat{x}_j, i\eta)\eta \quad (8)$$

is the quantity of water withdrawn from the j^{th} well in the i^{th} time period. Define

$$\beta(k, j, n-i+1) = \int_{(i-1)\eta}^{i\eta} G(\hat{x}_k, \hat{x}_j, n\eta - \tau) d\tau \quad (9)$$

and equation (7) becomes

$$s(k, n) = \sum_{j=1}^M \sum_{i=1}^n Q(j, i) \beta(k, j, n-i+1) \quad (10)$$

The β 's are the response coefficients and are constants independent of pumping and drawdown. $\beta(k, j, n-i+1)$ measures the increment of drawdown

at the k^{th} well at the n^{th} time period due to pumping at the j^{th} well during the i^{th} time period. The coefficients β 's are related to the well hydraulics, being functions of the distances between wells, the well radii (grid size), the transmissivity of the aquifer, the storage coefficient when the aquifer is confined and the specific yield when the aquifer is unconfined, the boundary conditions, the initial conditions, and the type of partial differential equation chosen to emulate the flow phenomena. In practice the β 's are determined by a simulation model because the irregularly shaped boundaries and nonhomogeneous parameters make analytical determination impossible. Maddock (1972) does determine a set of β 's for an aquifer of infinite extent and homogeneous parameter by analytical methods. Equation 9 forms a linear algebraic technological function (LATF).

The Green's function $G(\hat{x}, \hat{x}', t)$ is determined by solving the equation

$$\nabla \cdot [T(\hat{x}) \nabla G(\hat{x}, \hat{x}', t)] = S(\hat{x}) \frac{\partial G}{\partial t}(\hat{x}, \hat{x}', t) - \delta(\hat{x}, \hat{x}') \delta(t) \quad (11)$$

numerically subject to the causality condition

$$G(\hat{x}, \hat{x}', t - \tau) = 0 \quad t < \tau \quad (12)$$

and the boundary conditions

$$\frac{\partial G(\hat{\lambda}, t)}{\partial \eta} = 0 \quad \text{and/or} \quad G(\hat{\lambda}', t) = 0 \quad (13)$$

Applying finite difference techniques to equation (11) leads to a discrete form of the equation

$$\begin{aligned}
& \frac{T_{i-\frac{1}{2}j}}{\Delta x^2} (G_{i-1jk} - G_{ijk}) + \frac{T_{i+\frac{1}{2}j}}{\Delta x^2} (G_{i+1jk} - G_{ijk}) \\
& + \frac{T_{ij-\frac{1}{2}}}{\Delta x^2} (G_{ij-1k} - G_{ijk}) + \frac{T_{ij+\frac{1}{2}}}{\Delta x^2} (G_{ij+1k} - G_{ijk}) - \frac{S}{\Delta t} G_{ijk} \\
& = - \begin{cases} \frac{S}{\Delta t} G_{ijk-1} + 1 & \text{if } k = 1 \\ \frac{S}{\Delta t} G_{ijk-1} & \text{if } k > 1 \end{cases} \quad (14)
\end{aligned}$$

A square grid has been used. The index k represents the k^{th} time step and i and j represent row and column number respectively of the square grid imposed to produce the discretized form. The i index represents the discrete form of y and j represents the discrete form of x . The half node expansions of transmissibility variable are defined as (Saul'yev, 1964).

$$T_{i-\frac{1}{2}j} = \frac{T_{i-1j} + T_{ij}}{2} \quad (15)$$

$$T_{i+\frac{1}{2}j} = \frac{T_{i+1j} + T_{ij}}{2} \quad (16)$$

$$T_{ij-\frac{1}{2}} = \frac{T_{ij-1} + T_{ij}}{2} \quad (17)$$

$$T_{ij+\frac{1}{2}} = \frac{T_{ij+1} + T_{ij}}{2} \quad (18)$$

An alternating-direction-implicit method is used to solve equation (14). In addition an iterative procedure is used to increase the speed and accuracy of the method (Rubin, 1968). Application of these techniques to equation (14) leads to two new equations

$$\begin{aligned}
& T_{ij-\frac{1}{2}} G_{ij-1k+1}^{n+\frac{1}{2}} - [T_{ij-\frac{1}{2}} + T_{ij+\frac{1}{2}} + \rho + I_{ij}^{n+\frac{1}{2}}] G_{ijk+1}^{n+\frac{1}{2}} + T_{y+\frac{1}{2}} G_{ijk+1}^{n+\frac{1}{2}} \\
& = -T_{i-\frac{1}{2}j} G_{i-1jk+1}^n - \rho G_{ijk}^n + [T_{i-\frac{1}{2}j} + T_{i+\frac{1}{2}j} - I_{ij}^{n+\frac{1}{2}}] G_{ijk+1}^n \\
& \quad - T_{i+\frac{1}{2}j} G_{i+1jk+1}^n + \Delta x^2 \delta(k-1)
\end{aligned} \tag{19}$$

and

$$\begin{aligned}
& T_{i-\frac{1}{2}j} G_{i-1jk+1}^{n+1} - [T_{i-\frac{1}{2}j} + T_{i+\frac{1}{2}j} + \rho + I_{ij}^{n+1}] G_{ijk+1}^{n+1} + T_{i+\frac{1}{2}j} G_{i+1jk+1}^{n+1} \\
& = -T_{ij-\frac{1}{2}} G_{ij-1k+1}^{n+\frac{1}{2}} - \rho G_{ijk}^{n+\frac{1}{2}} + [T_{ij-\frac{1}{2}} + T_{ij+\frac{1}{2}} - I_{ij}^{n+1}] G_{ijk+1}^{n+\frac{1}{2}} \\
& \quad - T_{ij+\frac{1}{2}} G_{ij+1k+1}^{n+\frac{1}{2}} + \Delta x^2 \delta(k-1)
\end{aligned} \tag{20}$$

where n is the iteration index,

$$\rho = \frac{\Delta x^2 S}{\Delta t}, \tag{21}$$

I_{ij}^n denotes the iteration parameter at the (i,j) node and is defined

$$I_{ij}^n = I_{ij}^{n-1} \exp \left\{ \frac{\ln \frac{2x_m}{\lambda-1}}{\lambda-1} \right\} \tag{22}$$

with

λ -- the number of iteration parameters desired,

x_m -- the larger of the total number of rows or total of columns for the grid

initially

$$I_{ij}^1 = \frac{\pi^2}{2x_m} [T_{i-\frac{1}{2}j} + T_{i+\frac{1}{2}j} + T_{ij-\frac{1}{2}} + T_{ij+\frac{1}{2}}], \tag{23}$$

and

$$\delta(k-1) = \begin{cases} 1 & k = 1 \\ 0 & k \neq 1 \end{cases} \tag{24}$$

Equations (19) and (20) form two systems of linear equations. The first set represents the row values with column values held fixed, and the second set represents the column values with row values held fixed. The values of G_{ijk+1}^n and G_{ijk+1}^{n+1} are compared for all i's and j's. If the absolute value of their difference is less than some convergence factor, ϵ , the time increment counter, k , is advanced to $k + 1$, if not, the iteration parameter index, n , is advanced and the k index remains fixed. The row and column solutions are repeated for fixed index k , but advancing iteration parameter index until convergence is achieved. The parameters are cycled if more than the λ iterations are required. The time duration, Δt , represented by the index advance from k to $k + 1$, may be quite large. Values of up to two years have been used for Δt . As Δt increases more iterations with the iteration parameter are needed to achieve convergence.

Preliminary Operation

Values for transmissivity are given at each node of a grid superimposed on the plan view of the aquifer. The element of lengths x and y are equal. The nodal array of the grid is pictured as follows:

$$\begin{array}{ccccc}
 & & \Delta x & & \\
 & i-1, j-1 & & i-1, j & & i-1, j+1 \\
 \Delta y & i, j-1 & & i, j & & i, j+1 \\
 & i+1, j-1 & & i+1, j & & i+1, j+1
 \end{array}$$

The rules for assigning the values of the hydrologic variables and parameters are:

1. If a node point lies outside the boundary of aquifer, the transmissivity value for that node is set equal to zero.
2. Values of transmissivity within the boundaries of the aquifer should have values whose dimensions are in square feet per second. The dimensions of the matrix of the transmissivity values, zero or non-zero may not exceed 50 by 50 unless the dimension statements in the program are changed.
3. Storage coefficient is a dimensionless constant everywhere including those areas outside the boundaries of aquifer.
4. Those node points that have a constant head value are flagged.
(See section of Constant Head Boundary cards.)
5. Those node points that have wells are flagged.

When all the input data have been amassed, formatted, and punched onto cards as outlined in the Input Requirements and Data Description section, the program is ready to go.

Structure

The program consists of a main program and seven subroutines. The functions of the subroutines are as follows:

1. INF provides information as to type of boundary, type of output desired, initial values of variables, and the transmissivity values for the aquifer. These variables are unaffected by locations of wells.

2. PARAM provides calculations of the iteration parameters for the implicit iterative method
3. BOUND reads location signals for constant head boundary nodes and well nodes
4. INF2 assigns the producing well - INF2 is called for each well node
5. ITRATE provides control over the iteration procedures
6. MATCAL MATCAL is three subroutines; INITL, ROW, and COLUMN and they are entered by multiple entry procedures. The three subroutines initialize the variable used in the solution technique (INITL), calculate a solution with column values fixed, (ROW) and then calculate a solution with the row values fixed (COLUMN).
7. BETA calculates the response coefficients

Input Requirements and Data Description

Input to the program consists of control cards and data cards

Control Cards

There are two control cards read at the beginning of the program: the first is called a suppression card and the second is called a format card.

Suppression Card.-- This card indicates whether or not constant head boundaries are present, punched output is required, write out on a file is required, or normal printout is desired. The suppression card variables are all integers

<u>Column</u>	<u>Variable Name</u>	
1 - 2	IBOUND	Constant head boundary signal: If IBOUND=1, then there exists somewhere in the aquifer a constant head boundary and that constant

<u>Column</u>	<u>Variable Name</u>	
		Head boundary location cards to be read. If there is no constant head boundary present, leave the field of IBOUND blank.
3 - 4	IDISK	File write out signal: If IDISK=1 then the β 's are written out and stored unformatted on a file with unit number 10. If no file storage is required leave the field IDISK blank.
5 - 6	IPUNCH	Punched output signal: If IPUNCH=1 the β 's are punched out on cards. The format for the punched output is provided by FBETA. If no punched output is required leave the field IPUNCH blank.
7 - 8	IWRITE	Printer output signal: If IWRITE=1 the β 's are printed on the online printed. If no printout is required leave the field IWRITE blank.

Format Cards -- The format cards provide the format for reading in the transmissivity values and for punching out the β values (if required). This card is read at the time the program is executed so that the format of the data is dynamic. The card contains two 16 character fields. For a detailed explanation of preparing format cards see FORTRAN IV Language, an IBM publication (IBM C28-6515).

<u>Column</u>	<u>Variable Name</u>	
1 - 16	FTRAN	Transmissivity data format containing up to 16 characters.
17 - 32	FBETA	β punchout format of up to 16 characters. To avoid a syntax error a dummy format should be supplied even if no punched output is required.

Data Cards

There are two types of data cards: those that contain integer values and those that contain real values.

Integer Parameter Card. -- The integer parameter card provides the values for the grid dimension (both length and width), the number of well nodes, the number of time periods in the design horizon, and the number of iteration parameters desired. Each value must be right-justified.

<u>Column</u>	<u>Variable Name</u>	
1 - 8	IDIM	the total number of rows
9 - 16	JDIM	the total number of columns
17 - 24	NWEL	the number of well nodes
25 - 32	NUMKIT	the number of time periods in the design horizon. Up to 50 time periods are allowed as the program is now dimensioned
33 - 40	LENG	the number of iteration parameters

Real Parameter Card -- The real parameter card provides the values for the distance between node points, the constant storage coefficient, a scaling parameter for transmissivity (in case the user wishes to read the transmissivities in as integers), the duration of a pumping period, and a convergence factor to determine if the β 's have been calculated to sufficient accuracy. Each value must be right-justified unless the decimal point is punched.

<u>Card #</u>	<u>Column</u>	<u>Variable Name</u>	
1	1-20	DX	the distance in feet represented by consecutive grid nodes
1	21-40	S	the coefficient of storage (dimensionless)

<u>Card #</u>	<u>Column</u>	<u>Variable Name</u>	
1	41-60	SCALE2	Scales integer transmissivity values to feet squared per second. Set SCALE2=1 if no scaling is required
1	61-80	DT	the duration of the pumping period in seconds
2	1 -20	EPS	If two consecutive iterations produce head values with a difference less than EPS, β 's are calculated and the program proceeds to the next time step. EPS is thus a convergence factor.

Transmissivity Cards -- Transmissivity data should be read in a row at a time. This somewhat restricts the allowable format statements for FTRAN. The row number occupies the first field of the first card of a row.

Transmissivity values for the row are then read from the remaining fields of the card. Cards will continue to be read until all the transmissivity values for the rows are in. Then a new row of transmissivity values along with its row number are read. The process continues until all the rows have been entered. The format for the transmissivity cards is specified in FTRAN. An example is (20I4), twenty 4-digit fields. The last card of the set of transmissivity cards is a check card. In columns 2 through 25 of the checkcard the words

TRANSMISSIVITY READ IN

should be punched. This card is read and is printed out. If the above words appear in the output, the transmissivity values probably have read in properly.

Constant Head Boundary Cards -- Those node points which lie on the constant head boundary are read one node point per card. If no constant head boundary is present (IBOUND=0 or blank on the suppression card), no node points are read. If IBOUND=1 there is a constant head boundary. Each of the cards provides the row and column number of the node and a signal flag which determines if another constant boundary node card is to be read. Each value must be right justified.

<u>Column</u>	<u>Variable Name</u>	
1-4	I	The row number for the constant head node
5-8	J	The column number for the constant head node
9-12	JSIG	A signal flag. If JSIG=0 another node card is read. If JSIG=1 no more node cards are read.

Well Cards -- The well cards read in the row and column number of the well nodes. A node may be representative of more than one well. As the program is now dimensioned, up to 100 well nodes are allowed.

The row number is followed by a column number. The format for the card is 20I4 thus there are ten well nodes per card (10 row numbers and 10 column numbers). For example, if $I(k)$ is the row number of k^{th} well and $J(k)$ is the column number of the k^{th} well, then for 2 wells the card would be as follows:

<u>Column</u>	<u>Variable</u>	
1-4	I(1)	row number of first well
5-8	J(1)	column number of first well
9-12	I(2)	row number of second well
13-16	J(2)	column number of second well

Each value must be right-justified. Once the well cards are read in, the input data requirements have been completed.

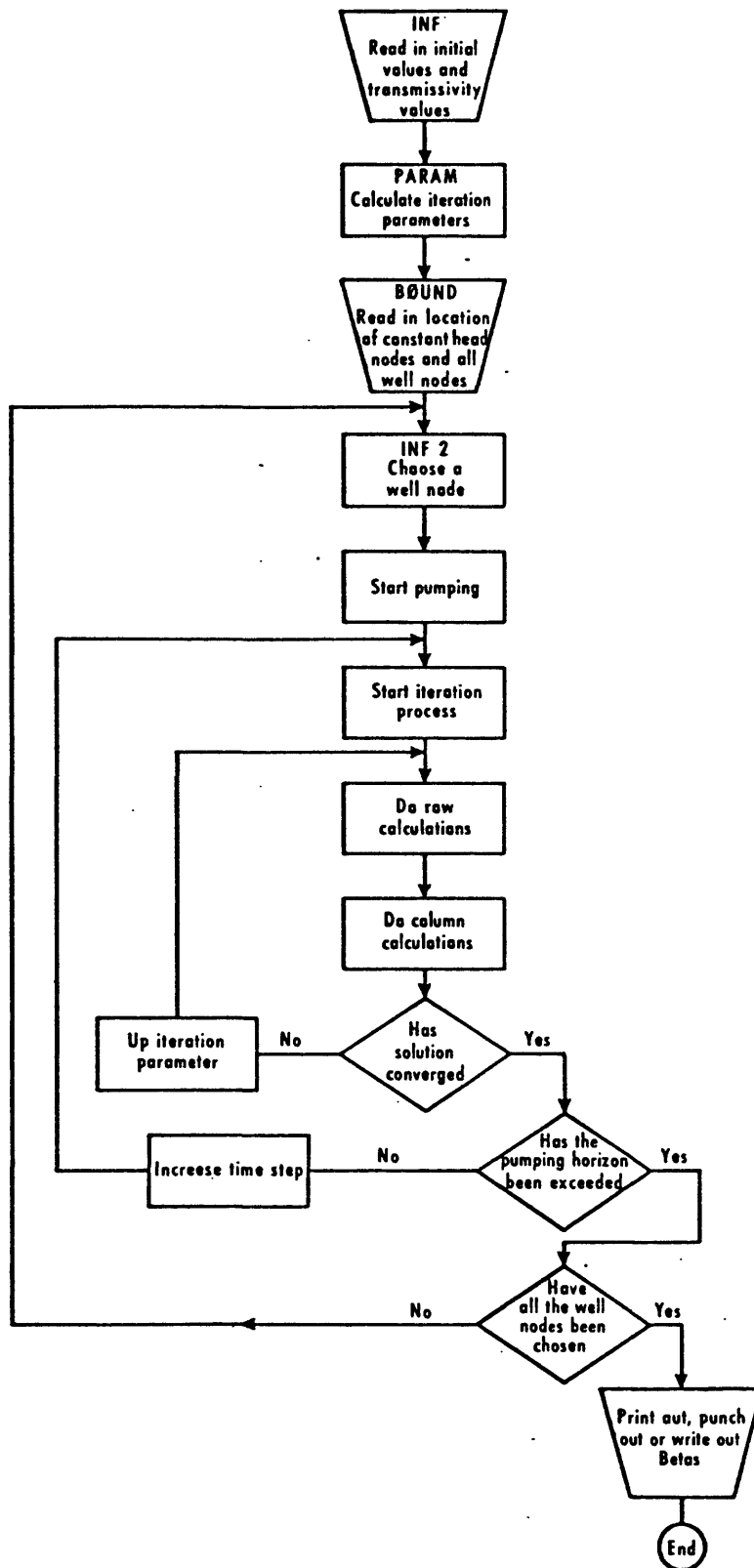
Output

The program output consists of 1) printing the integer and real variable inputs, 2) listing well nodes by row and column number, and 3) the option to print-out, punch-out, or write out (on a file) the response coefficient, β 's.

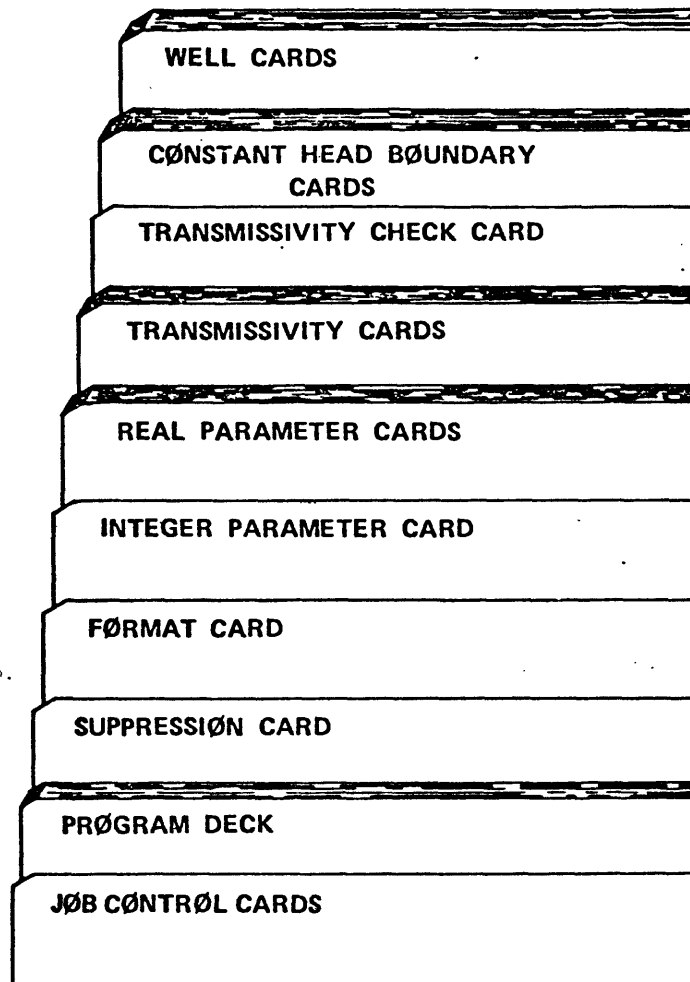
Core Requirements and Time Estimates

The program as it is now written and when it is run on an IBM 370-155 requires 248 K bytes of storage, 9 sec to compile, and averages 2 minutes per well node calculation (based on a design horizon of 20 one-year time periods). The calculating of the response coefficient for 30 well nodes over 20 one-year time periods takes about 60 minutes of compute time on an IBM 370-155. On an IBM 360-91 the same problem requires less than 10 minutes of computer time.

FLOW CHART



LOADING PROCEDURE



References

- Maddock, T, III, 1972, Algebraic technological function from a simulation model: Water Resources Research, vol. 8, no. 1, p. 129,134.
- Rubin, J., 1968, Theoretical analysis of two dimensional transient flow of water in unsaturated and partly unsaturated soils: Proc. Soil Sci. Soc. Am., vol. 32, no. 5, p. 607-615.
- Saul'yev, V.K., 1964, Integration of equations of parabolic type by the methods of nets: Pergamon Press, Oxford, England, 364 p.

APPENDIX A

Input Data to Program

APPENDIX B

Program Listing

```

COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=0000K,
                   SOURCE=ERBCDIC,INCLIST=NODECK,LOAD=MAP,...,EDIT,IO,NOXREF
C ACIP-ITERATIVE
C BETA CALCULATIONS
C ACQUIFER MODEL
C UNCONFINED ACQUIFER OR UNCONFINED ACQUIFER WITH CONSTANT
C TRANSMISSIBILITY IN TIME
C
C THIS PROGRAM USES AN IMPLICIT ALTERNATING DIRECTION SCHEME.
C
C CCMON /C8/ KT
C CCMON /C10/ NUKT,NMEL
C CCMON /C23/ IDIVG,KOUNT
C CCMON /C24/ LENG
C
C CALL INF
C CALL PARAP
C CALL BOUND
C DC 3 KREL=1,NMEL
C CALL INF2(KREL)
C C 2 KT=1,NUKKT
C 1 CALL ITRATE
C CALL ROW
C CALL CCLUPN
C IF (KCLNT.LE.5*LENG.AND.IDIVG.EQ.1) GO TO 1
C IF (KCLNT.GT.5*LENG) WRITE (6,4)
C IF (KOUNT.GT.5*LENG) GO TO 3
C IF (IDIVG.EQ.0) CALL BETA(KREL)
C 2 CONTINUE
C 3 CONTINUE
C STOP
C
C 4 FORMAT (' THE SOLUTION FAILED TO CONVERGE.')
C END

```

```

A 10
A 20-
A 30
A 40
A 50
A 60
A 70
A 80
A 90
A 100
A 110
A 120
A 130
A 140
A 150
A 160
A 170
A 180
A 190
A 200
A 210
A 220
A 230
A 240
A 250
A 260
A 270
A 280
A 290
A 300
A 310
A 320
A 330-

```

COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=0700K,
SOURCE=EBCDIC,NOLIST,NODECK,LOAD,VAP,NODEIT,ID,NXREF

```

15N 0002      C      SLROUTINE INF
15N 0003      C      IMPLICIT REAL*8(A-H,O-Z)
15N 0004      C      COMMON /C1/ IDIM,JDIM
15N 0005      C      COMMON /C2/ T(50,50)
15N 0006      C      COMMON /C3/ M(50,50),STRTM
15N 0007      C      COMMON /C4/ DT
15N 0008      C      COMMON /C6/ PI
15N 0009      C      COMMON /C9/ S
15N 0010      C      COMMON /C10/ NUPKT,NMEL
15N 0011      C      COMMON /C11/ IROUND,IDISK,IPUNCH,IWRITE
15N 0012      C      COMMON /C13/ DX
15N 0013      C      COMMON /C18/ SCALE2
15N 0014      C      COMMON /C19/ FTRAN(4),FBETA(4)
15N 0015      C      COMMON /C21/ PARAM,PREVM(50,50),EPS
15N 0016      C      COMMON /C24/ LENG
15N 0017      C      INTEGER T,FTRAN,FBETA
15N 0018      C      NAMELIST /N1/ IROUND,IDISK,IPUNCH,IWRITE/N2/ LENG/N3/SCALE2,EPS
15N 0019      C      READ IN SIGNALS FOR SUPPRESSION OR OPERATION OF SUBROUTINES
15N 0020      C      READ (5,7) IROUND,IDISK,IPUNCH,IWRITE
15N 0021      C      WRITE (6,N1)
15N 0022      C      READ IN FORMATS FOR TRANSMISSIVITY AND PUMPING CARDS.
15N 0023      C      READ (5,3) IDIM,JDIM,NMEL,NUPKT,LENG
15N 0024      C      WRITE (6,N2)
15N 0025      C      READ IN REAL VARIABLES
15N 0026      C      STRTM=1000.
15N 0027      C      READ (5,4) DX,S,SCALE2,DT,EPS
15N 0028      C      WRITE (6,N3)
15N 0029      C      PI=3.14159265359
15N 0030      C      CALL INITL
15N 0031      C      READ IN TRANSMISSIBILITY MATRIX
15N 0032      C      DO 1 I=1,IDIM
15N 0033      C      1 READ (5,FTRAN) I,(T(I,J),J=1,JDIM)

```

```

      B 10
      B 20
      B 30
      B 40
      B 50
      B 60
      B 70
      B 80
      B 90
      B 100
      B 110
      B 120
      B 130
      B 140
      B 150
      B 160
      B 170
      B 180
      B 190
      B 200
      B 210
      B 220
      B 230
      B 240
      B 250
      B 260
      B 270
      B 280
      B 290
      B 300
      B 310
      B 320
      B 330
      B 340
      B 350
      B 360
      B 370
      B 380
      B 390
      B 400
      B 410
      B 420
      B 430
      B 440
      B 450
      B 460
      B 470
      B 480
      B 490
      B 500

```

```

1SN 0032      READ (5,2)
1SN 0033      WHITE (6,2)
C
1SN 0034      WHITE (6,5) DT,DX,S,NUMKT,101W,JD1W,NWEL
C
1SN 0035      RETURN
C
1
1SN 0036      2 FCRWAT (1
1SN 0037      3 FCRWAT (101R)
1SN 0038      4 FCRWAT (4F20,5)
1SN 0039      5 FCRWAT (1M),1X,29HLENGTH OF INITIAL TIME STEP =,016.4//1X,27HGRID
1SPACING OF PROTOTYPE =,F16.4//1X,21HSTORAGE COEFFICIENT =,F16.8//1
2X,30HMAXIMUM NUMBER OF TIME STEPS =,14//1X,24HNUMBER OF LENGTH MOD
3ES =,14//1X,23HNUMBER OF WIDTH NODES =,14//1X,19HNUMBER OF WELLS =,1
414//
6 FCRWAT (2(444))
7 FCRWAT (1012)
END
1SN 0040
1SN 0041
1SN 0042

```

```

B 510
B 520
B 530
B 540
B 550
B 560
B 570
B 580
B 590
B 600
B 610
B 620
B 630
B 640
B 650
B 660
B 670
B 680
B 690
B 700-

```

```

COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=0C00K,
SOURCE,ERCDIC,NCLIST,NODECK,LOAD,MAP,NJEDIT,IO,NOXREF
SUBROUTINE PARAP
ISN 0002 C 10
C 20
C 30
C 40
C 50
C 60
C 70
C 80
C 90
C 100
C 110
C 120
C 130
C 140
C 150
C 160
C 170
C 180
C 190
C 200-

ISN 0003 C
C
IMPLICIT REAL*8(A-H,O-Z)

ISN 0004 C 70
ISN 0005 C 80
ISN 0006 C 90
ISN 0007 C 100
C 110
C 120
C 130
C 140
C 150
C 160
C 170
C 180
C 190
C 200-

C
XMAX=MAX0(1DIM,JDIM)
CM1A=D1*2/(2.0*XMAX)
BETA=DEXP(DLOG(1.0/OMIN)/IDFLOAT(LENG)-1.0))
OMEGA(1)=CM1A
DC 1 I=2,LENG
1 OMEGA(I)=OMEGA(I-1)*BETA
RETURN

ISN 0015 C
END

```

```

      COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=(000K,
        SOURCE,EBDCIC,NOLIST,NODECK,LOAD,MAF,,NOEDIT, ID,NOXREF
      SUBROUTINE BOUND
      ISN 0002
      C
      C T-15 SUBROUTINE READS IN POINTS OF CONSTANT HEAD AND READS IN
      C WELL NODES
      C
      C IMPLICIT REAL*8(A-H,O-Z)
      ISN 0003
      C
      C CCMON /C1/ IDIM,JDIM
      C CCMON /C5/ P(50,50)
      C CCMON /C10/ NUWKT,NWEL
      C CCMON /C11/ IROUND,IDISK,IPUNCH,IWRITE
      C CCMON /C14/ II(70),JJ(70)
      ISN 0004
      C
      C INTEGER P,FTNAN,FPUMP
      ISN 0009
      C
      C DC 1 I=1,IDIM
      C DC 1 J=1,JDIM
      C 1 P(I,J)=0
      ISN 0010
      C
      C READ IN CONSTANT HEAD POINTS IF ANY
      ISN 0011
      C
      C IF (IROUND.EQ.0) GO TO 3
      C 2 READ (5,5) I,J,USIG
      C P(I,J)=2
      C IF (USIG.EQ.0) GO TO 2
      C 3 CONTINUE
      ISN 0013
      C
      C READ IN WELL POINTS
      ISN 0015
      C
      C READ (5,5) (I(K),JJ(K),K=1,NWEL)
      C WRITE (6,4) (K,II(K),JJ(K),K=1,NWEL)
      C RETURN
      ISN 0016
      C
      C 4 FCMAT (1X,'WELL POINTS',5X,'I',4X,'J'/(5X,12,9X,12,3X,12))
      ISN 0017
      C
      C 5 FCMAT (20A)
      ISN 0019
      C
      C END
      ISN 0020
      C
      C
      ISN 0021
      C
      C
      ISN 0022
      C
      C
      ISN 0023
      C
      C
      ISN 0024
      C
      C
      ISN 0025
      C

```

```

      D 10
      D 20
      D 30
      D 40
      D 50
      D 60
      D 70
      D 80
      D 90
      D 100
      D 110
      D 120
      D 130
      D 140
      D 150
      D 160
      D 170
      D 180
      D 190
      D 200
      D 210
      D 220
      D 230
      D 240
      D 250
      D 260
      D 270
      D 280
      D 290
      D 300
      D 310
      D 320
      D 330
      D 340
      D 350
      D 360
      D 370-

```

COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=0)(OK,
SOURCE,FRCD)C,NCLIST,NODECK,LOAD,MAP,NODEIT,ID,NXREF

```

15N 0002      C      SLROUTINE INF2(KNEL)
15N 0003      C      I*PLICIT REAL*8(A-H,O-Z)
15N 0004      C      COMMON /C1/ IDIM,JDIM
15N 0005      C      COMMON /C3/ H(50,50),STRTH
15N 0006      C      COMMON /C5/ P(50,50)
15N 0007      C      COMMON /C11/ IROUND,IOISK,IPUNCH,IWRITE
15N 0008      C      COMMON /C14/ II(70),JJ(70)
15N 0009      C      COMMON /C23/ IDIVG,KOUNT
15N 0010      C      INTEGER P
15N 0011      C      INITIALIZE CONSTANTS
15N 0012      C      IDIVG=0
15N 0013      C      SET INITIAL VALUE OF HEAD AND ZERO PUMPING
15N 0014      C      DC 1, I=1, IDIM
15N 0015      C      DC 1, J=1, JDIM
15N 0016      C      IF (P(I,J).NE.2) P(I,J)=0
15N 0017      C      1 H(I,J)=STATH
15N 0018      C      SET UP PUMPING WELL
15N 0019      C      I=1(KNEL)
15N 0020      C      J=J(KNEL)
15N 0021      C      P(I,J)=1
15N 0022      C      IF (IWRITE.EQ.1) WRITE (6,2)
15N 0023      C      RETURN
15N 0024      C      2 FORMAT (1H1)
15N 0025      C      END

```

```

E 10
E 20
E 30
E 40
E 50
E 60
E 70
E 80
E 90
E 100
E 110
E 120
E 130
E 140
E 150
E 160
E 170
E 180
E 190
E 200
E 210
E 220
E 230
E 240
E 250
E 260
E 270
E 280
E 290
E 300
E 310
E 320
E 330
E 340
E 350
E 360-

```


COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=00,OK,
SOURCE,EBGCDIC,NCLIST,NODECK,LOAD,MAP,POEDIT,10,NOXREF
SLROUTINE ITHATE

ISA 0002	C			F 10
ISA 0003	C	IMPLICIT REAL*8(A-H,O-Z)		F 20
ISA 0004				F 30
ISA 0005		COMMON /C1/ IDIM,JDIM		F 40
ISA 0006		COMMON /C3/ H(50,50),STATB		F 50
ISA 0007		COMMON /C4/ DT		F 60
ISA 0008		COMMON /C10/ NUKKT,NWEL		F 70
ISA 0009		COMMON /C21/ PARM,PHEVH(50,50),EPS		F 80
ISA 0010		COMMON /C22/ OMEGA(10)		F 90
ISA 0011		COMMON /C23/ IDIVG,KOUNT		F 100
		COMMON /C24/ LENG		F 110
	C			F 120
ISA 0012		IF (IDIVG.EQ.1) GO TO 2		F 130
ISA 0014		NT=0		F 140
ISA 0015		KOUNT=0		F 150
ISA 0016		PARM=U,0		F 160
ISA 0017		DC 1 I=1, IDIM		F 170
ISA 0019		DC 1 J=1, JDIM		F 180
ISA 0020		1 PHEVH(I,J)=H(I,J)		F 190
ISA 0021		RETURN		F 200
ISA 0022		2 KOUNT=KOUNT+1		F 210
ISA 0023		3 IF (MOD(KOUNT,LENG)) 3,3,4		F 220
ISA 0024		4 NT=NT+1		F 230
ISA 0025		PARM=OMEGA(NT)		F 240
ISA 0026		RETURN		F 250
ISA 0027		END		F 260
				F 270
				F 280

```

15A 0002 C SLROUTINE MATCAL
15A 0003 C
15A 0004 C IMPLICIT REAL*8(A-H,O-Z)
15A 0005 C
15A 0006 C COMMON /C1/ ID1*,JD1*
15A 0007 C COMMON /C2/ T(50,50)
15A 0008 C COMMON /C3/ M(50,50),STRM
15A 0009 C COMMON /C4/ DT
15A 0010 C COMMON /C5/ P(50,50)
15A 0011 C COMMON /C6/ KT
15A 0012 C COMMON /C7/ S
15A 0013 C COMMON /C8/ DX
15A 0014 C COMMON /C9/ DY
15A 0015 C COMMON /C10/ SCALE2
15A 0016 C COMMON /C11/ PARM,PREVH(50,50),EPS
15A 0017 C COMMON /C12/ IDIVG,KOUNT
15A 0018 C
15A 0019 C INTEGER T,P
15A 0020 C DIMENSION BE(50), G(50), TEMP(50)
15A 0021 C
15A 0022 C ENTRY INITL
15A 0023 C
15A 0024 C
15A 0025 C DIV=2.0*SCALE2
15A 0026 C JLESS1=JD1M-1
15A 0027 C JLESS2=JD1M-2
15A 0028 C ILESS1=ID1M-1
15A 0029 C ILESS2=ID1M-2
15A 0030 C RETURN
15A 0031 C
15A 0032 C ENTRY POW
15A 0033 C
15A 0034 C RHO=DX**2*S/DY
15A 0035 C RE(1)=0.0
15A 0036 C G(1)=0.0
15A 0037 C DC 9 I=2,JD1*
15A 0038 C DO 1 J=2,ID1*
15A 0039 C
15A 0040 C DETERMINE WHETHER NODE IS OUTSIDE AQUIFER BOUNDARY
15A 0041 C
15A 0042 C IF (T(I,J).EQ.0) GO TO 1
15A 0043 C
15A 0044 C CALCULATE AVERAGE VALUES CF T BETWEEN ADJACENT NODES.
15A 0045 C
15A 0046 C NCDE. T1=LEFT, T2=RIGHT, T3=UPPER, T4=LOWER
15A 0047 C
15A 0048 C T1=DFLOAT(T(I,J-1)+T(I,J))/DIV
15A 0049 C T2=DFLOAT(T(I,J-1)+T(I,J))/DIV
15A 0050 C T3=DFLOAT(T(I-1,J)+T(I,J))/DIV
15A 0051 C T4=DFLOAT(T(I-1,J)+T(I,J))/DIV
15A 0052 C IF (T1+T2+T3+T4)/4.0 T1=0.0
15A 0053 C IF (T1+T2+T3+T4)/4.0 T2=0.0
15A 0054 C IF (T1+T2+T3+T4)/4.0 T3=0.0
15A 0055 C IF (T1+T2+T3+T4)/4.0 T4=0.0
15A 0056 C
15A 0057 C
15A 0058 C
15A 0059 C
15A 0060 C
15A 0061 C
15A 0062 C
15A 0063 C
15A 0064 C
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15A 0358 C
15A 0359 C
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15A 0363 C
15
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15A 0040      IF (T(I-1,J).EQ.0) T3=0.0      G 510
15A 0042      IF (T(I+1,J).EQ.0) T4=0.0      G 520
15A 0044      MINCR=PARAM*(T1+T2+T3+T4)      G 530
C              G 540
C              G 550
C              G 560
C              G 570
C              G 580
C              G 590
C              G 600
C              G 610
C              G 620
C              G 630
C              G 640
C              G 650
C              G 660
C              G 670
C              G 680
C              G 690
C              G 700
C              G 710
C              G 720
C              G 730
C              G 740
C              G 750
C              G 760
C              G 770
C              G 780
C              G 790
C              G 800
C              G 810
C              G 820
C              G 830
C              G 840
C              G 850
C              G 860
C              G 870
C              G 880
C              G 890
C              G 900
C              G 910
C              G 920
C              G 930
C              G 940
C              G 950
C              G 960
C              G 970
C              G 980
C              G 990
C              G1000
C              G1010
C              G1020

15A 0054      CALCULATE VALUES FOR PARAMETERS A,B,C,D
15A 0055      G=0.0
15A 0056      ZK=0.0
15A 0057      IF (P(I,J).EQ.1.AND.KT.EQ.1) Q=1.0
15A 0058      IF (P(I,J).EQ.2) ZK=10.0D+50
15A 0059      A=11
15A 0060      R=-T1-T2-RHO-ZK*DX**2-MINCR
15A 0061      C=T2
15A 0062      D=-T3*M(I-1,J)-RHU*PREV(I,J)*(T3+T4-MINCR)*M(I,J)-T4*M(I+1,J)+Q-(
15A 0063      W=B-A*RE(J-1)
15A 0064      RE(J)=C/W
15A 0065      G(J)=(D-A*G(J-1))/W
15A 0066      1 CONTINUE
15A 0067      G 740
15A 0068      G 750
15A 0069      G 760
15A 0070      G 770
15A 0071      G 780
15A 0072      G 790
15A 0073      G 800
15A 0074      G 810
15A 0075      G 820
15A 0076      G 830
15A 0077      G 840
15A 0078      G 850
15A 0079      G 860
15A 0080      G 870
15A 0081      G 880
15A 0082      G 890
15A 0083      G 900
15A 0084      G 910
15A 0085      G 920
15A 0086      G 930
15A 0087      G 940
15A 0088      G 950
15A 0089      G 960
15A 0090      G 970
15A 0091      G 980
15A 0092      G 990
15A 0093      G1000
15A 0094      G1010
15A 0095      G1020

```

```

ISA 00P2          DC 10 I=2,ILESS1          61030
C
C DETERMINE WHETHER NODE IS OUTSIDE AQUIFER BOUNDARY          61040
C IF (T(I,J).EQ.0) GO TO 10          61050
ISA 00E3          61060
C          61070
C          61080
C          61090
C          61100
C          61110
C          61120
C          61130
C          61140
C          61150
C          61160
C          61170
C          61180
C          61190
C          61200
C          61210
C          61220
C          61230
C          61240
C          61250
C          61260
C          61270
C          61280
C          61290
C          61300
C          61310
C          61320
C          61330
C          61340
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C          61370
C          61380
C          61390
C          61400
C          61410
C          61420
C          61430
C          61440
C          61450
C          61460
C          61470
C          61480
C          61490
C          61500
C          61510
C          61520
C          61530
C          61540

ISA 00G5          T1=DFLCAT(T(I,J-1)+T(I,J))/DIV          61230
ISA 00E6          T2=DFLCAT(T(I,J+1)+T(I,J))/DIV          61240
ISA 00E7          T3=DFLCAT(T(I-1,J)+T(I,J))/DIV          61250
ISA 00E8          T4=DFLCAT(T(I+1,J)+T(I,J))/DIV          61260
ISA 00E9          IF (T(I,J-1).EQ.0) T1=0.0          61270
ISA 00F1          IF (T(I,J+1).EQ.0) T2=0.0          61280
ISA 00F3          IF (T(I-1,J).EQ.0) T3=0.0          61290
ISA 00F5          IF (T(I+1,J).EQ.0) T4=0.0          61300
ISA 00F7          H1NCH=PARP*(T1+T2+T3+T4)          61310
C          61320
C          61230
C          61240
C          61250
C          61260
C          61270
C          61280
C          61290
C          61300
C          61310
C          61320
C          61330
C          61340
C          61350
C          61360
C          61370
C          61380
C          61390
C          61400
C          61410
C          61420
C          61430
C          61440
C          61450
C          61460
C          61470
C          61480
C          61490
C          61500
C          61510
C          61520
C          61530
C          61540

ISA 00G9          Q=0.0          61030
ISA 00S9          ZK=0.0          61040
ISA 0100          IF (P(I,J).EQ.1.AND.KT.EQ.1) Q=1.0          61050
ISA 0102          IF (P(I,J).EQ.2) ZK=10.00*50          61060
ISA 0104          A=T3          61070
ISA 0105          H=-T3-T4-RHO-ZK*DX**2-HINCH          61080
ISA 0106          C=T4          61090
ISA 0107          D=-T1*(I,J-1)-RHO*PREVH(I,J)+(T1+T2-HINCH)*h(I,J)-T2*(I,J+1)+D-(          61100
          1ZK*DX**2)*(STRM-H(I,J))/2.0)          61110
ISA 0108          h=R-A*RE(1-1)          61120
ISA 0109          BE(I)=C/W          61130
ISA 0110          G(I)=D-A*G(1-1)/W          61140
ISA 0111          10 CONTINUE          61150
C          61160
C          61170
C          61180
C          61190
C          61200
C          61210
C          61220
C          61230
C          61240
C          61250
C          61260
C          61270
C          61280
C          61290
C          61300
C          61310
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C          61100
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C          61120
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C          61200
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C          61480
C          61490
C          61500
C          61510
C          61520
C          61530
C          61540

ISA 0112          IF (J.GT.2) GO TO 14          61030
ISA 0114          DC 13 K=1,ILESS2          61040
ISA 0115          n=IDIV-K          61050
ISA 0116          IF (T(n,J)) 12,11,12          61060
ISA 0117          11 TEMP(n)=STRM          61070
ISA 0118          GC TO 13          61080
ISA 0119          12 TEMP(n)=G(n)-RE(n)*TEMP(n+1)          61090
ISA 0120          13 IF (DABS(TEMP(n)-h(n,J)).GT.EPS) IDIVG=1          61100
ISA 0122          13 CONTINUE          61110
ISA 0123          GC TO 14          61120
ISA 0124          14 DC 17 K=1,ILESS2          61130
ISA 0125          n=IDIV-K          61140
          61150
          61160
          61170
          61180
          61190
          61200
          61210
          61220
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          61490
          61500
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          61520
          61530
          61540

```

ISA 0126	H(N,J-1)=TEMP(N)	G1550
ISA 0127	IF (T(N,J)) 16,15,16	G1560
ISA 0128	15 TEMP(N)=STRT	G1570
ISA 0129	GC TO 17	G1580
ISA 0130	16 TEMP(N)=G(N)-BE(N)*TEMP(N+1)	G1590
ISA 0131	IF (DABS(TEMP(N)-H(N,J))*GT.EPS) IDIVG=1	G1600
ISA 0132	17 CONTINUE	G1610
ISA 0133	18 CONTINUE	G1620
ISA 0134		G1630
ISA 0135	RETURN	G1640
ISA 0136	END	G1650
		G1660-

```

COMPILER OPTIONS - NAME= MAIN,OPT=00,LINECNT=54,SIZE=0000K,
SOURCE,EBCDIC,NGLIST,NODECK,LOAD,MAP,NODEDIT,IO,NXREF
ISN 0002      SLRROUTINE RETA(KWEL)
C
C      THIS SUBROUTINE CALCULATES BETAS
ISN 0003      IMPLICIT REAL*8(A-M,O-Z)
C
ISN 0004      CCMON /C1/ INIM,UDIM
ISN 0005      CCMON /C3/ M(50,50),STRMTH
ISN 0006      CCMON /C8/ KT
ISN 0007      CCMON /C10/ NUPKT,NWEL
ISN 0008      CCMON /C11/ IRCUND,IDISK,IPUNCH,IWRITE
ISN 0009      CCMON /C14/ I(70),J(70)
ISN 0010      CCMON /C19/ FTRAN(4),FBETA(4)
C
ISN 0011      IATEGER FTRAN,FBETA
ISN 0012      REAL *4B(100,20)
C
C      CALCULATE BETAS
ISN 0013      DC 1 KCLNT=1,NWEL
ISN 0014      I=1(KCLNT)
ISN 0015      J=J(KCLNT)
ISN 0016      1 R(KOUNT,KT)=STRM-H(I,J)
C
C      WRITE OUT BETAS
ISN 0017      IF (IDISK.EQ.1) WRITE (10) (R(KOUNT,KT),KOUNT=1,NWEL)
ISN 0019      IF (IPUNCH.EQ.1) WRITE (7,FBETA) KWEL,KT,(R(KOUNT,KT),KOUNT=1,NWEL
1)
ISN 0021      IF (IWRITE.EQ.1) WRITE (6,2) KWEL,KT,(R(KOUNT,KT),KOUNT=1,NWEL)
ISN 0023      RETURN
C
C
ISN 0024      2 FCRMAT (1X,BETA('12','J','12',''),4X,(15F7.3))
ISN 0025      END
C

```

APPENDIX C

Program Output from Printe

```

AN1
INCLNO= 0.0DISK= 0.0PUNCH= 1.0WRITE= 1
KENC (2014) (213/(10FB,4))
AN2
LENG= 10
KENC
AN3
SCALE2= 1000.000000000000 EPS= 0.9999999999999999D-03
KENC
TRANSMISSIVITY READ IN

```


LENGTH OF INITIAL TIME STEP = 0.31560 08
 GAIC SPACING OF PROTOTYPE = 2640.0000
 STORAGE COEFFICIENT = 0.01000000
 MAXIMUM NUMBER OF TIME STEPS = 10
 NUMBER OF LENGTH NODES = 49
 NUMBER OF WIDTH NODES = 41
 NUMBER OF WELLS = 3
 WELL POINTS 1 J
 1 8 17
 2 8 19
 3 12 17

PETA(1.0, 1)	15.135	5.512	2.451
PETA(1.0, 2)	4.531	3.536	2.236
PETA(1.0, 3)	2.026	2.745	1.894
BETA(1.0, 4)	2.476	2.321	1.657
BETA(1.0, 5)	2.126	2.021	1.486
BETA(1.0, 6)	1.864	1.795	1.354
BETA(1.0, 7)	1.656	1.555	1.245
PETA(1.0, 8)	1.448	1.439	1.155
BETA(1.0, 9)	1.350	1.310	1.078
BETA(1.0, 10)	1.237	1.203	1.012

BETA(2.0, 1)	5.510	17.943	2.166
BETA(2.0, 2)	3.535	4.139	2.082
BETA(2.0, 3)	2.745	2.765	1.610
BETA(2.0, 4)	2.321	2.270	1.601
BETA(2.0, 5)	2.020	1.959	1.443
BETA(2.0, 6)	1.785	1.727	1.317
BETA(2.0, 7)	1.594	1.544	1.214
BETA(2.0, 8)	1.438	1.356	1.127
BETA(2.0, 9)	1.310	1.274	1.054
BETA(2.0, 10)	1.203	1.174	0.992

BETA(3.0, 1)	2.435	2.154	14.471
BETA(3.0, 2)	2.231	2.076	3.018
BETA(3.0, 3)	1.697	1.811	1.236
BETA(3.0, 4)	1.661	1.605	1.456
BETA(3.0, 5)	1.630	1.447	1.254
BETA(3.0, 6)	1.357	1.320	1.145
BETA(3.0, 7)	1.248	1.216	1.059
BETA(3.0, 8)	1.157	1.130	0.992
BETA(3.0, 9)	1.080	1.056	0.938
BETA(3.0, 10)	1.014	0.954	0.892

APPENDIX D

Programs Punched Output

1	19.1353	5.5124	2.4509
1 2			
1 3	4.5312	3.5382	2.2356
1 4	3.0258	2.7447	1.8942
1 5	2.4755	2.3208	1.6570
1 6	2.1259	2.0206	1.4864
1 7	1.8536	1.7849	1.3535
1 8	1.6561	1.5945	1.2452
1 9	1.4879	1.4387	1.1545
1 10	1.3503	1.3101	1.0778
2 1	1.2346	1.2035	1.0125
2 2	5.5100	17.9428	2.1663
2 3	3.5386	4.1390	2.0821
2 4	2.7451	2.7653	1.8098
2 5	2.3210	2.2703	1.6015
2 6	2.0203	1.9592	1.4432
2 7	1.7846	1.7274	1.3173
2 8	1.5944	1.5444	1.2140
2 9	1.4385	1.3962	1.1275
2 10	1.3100	1.2744	1.0545
3 1	1.2034	1.1736	0.9923
3 2	2.4349	2.1543	14.4712
3 3	2.2305	2.0764	3.0180
3 4	1.8555	1.8113	1.8362
3 5	1.6410	1.6046	1.4556
3 6	1.4503	1.4467	1.2643
3 7	1.3570	1.3203	1.1447
3 8	1.2481	1.2165	1.0590
3 9	1.1549	1.1296	0.9923
3 10	1.0797	1.0562	0.9377
4 1	1.0140	0.9937	0.8919