UNITED STATES DEPARTMENT OF THE INTERIOR

GEOLOGICAL SURVEY

Audio-magnetotelluric data log for Cedarville, California, 15' quadrangle. Supplement to Open-File Report 75-102.

By

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Cedarville, Calif., 15' quadrangle, 1975

U.S. GEOLOGICAL SURVEY A.M.T. DATA LOG

ρa = observed apparent resistivity in ohm-metres
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– = no data

"NOTE" - Telluric line orientation indicated with station numbers.

Sta. No.		FREQUENCY 7.5	10	14	27	76	285	685	1.2K	3.3K	6.7K	10.2K	18.6K
1NS	ρa	1.3	–	2.1	7.6	13.8	19.5	–	–	–	95.	130	46
	N	3		7	11	11	9				8	1	1
	Er	.2		.5	1.2	0.6	0.8				2.7	–	–
1EW	ρa	1.2	–	3.7	8.0	18.9	24.1	–	–	–	117.	178	62
	N	4		7	10	10	5				10	1	1
	Er	.4		.2	.4	1.1	4.7				2.6	–	–
2NS	ρa	1.3	–	1.6	5.1	10.3	15.5	–	–	–	74	113	31
	N	8		10	10	10	11				10	1	1
	Er	.3		.4	.7	.4	1.2				4.4	–	–
2EW	ρa	1.6	–	1.9	6.5	14.9	28.	–	–	–	93	158	29
	N	6		7	10	10	5				10	1	1
	Er	.3		.2	.9	1.2	4.0				3.3		
3NS	ρa	1.5	–	.8	3.1	5.5	11	–	–	–	45	138	16
	N	4		6	10	10	10				10	1	1
	Er	.6		.1	.3	.2	.8				2.5	–	–
3EW	ρa	1.9	–	12.	11.6	25.	8.5	–	–	–	142	–	23.
	N	5		5	10	10	8				10	1	1
	Er	.3		2.8	1.1	2.5	1.1				11.	–	–
4NS	ρa	1.6	–	1.5	2.0	2.7	10	–	–	–	37	29	6.5
	N	3		5	10	10	7				10	1	1
	Er	.3		1.3	.2	.4	1.8				4.2	–	–
4EW	ρa	.6	–	.95	1.6	4.4	11.	–	–	–	39.	17.	8.1
	N	4		6	10	10	7				8	1	1
	Er	.1		.3	.2	.3	.1				4.4	–	–

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5NS	ρa	2.1	—	5.2	11.3	12.6	8.7	—	—	—	10.5	12.0	4.0
	N	5		6	10	10	9				10	1	1
	Er	.4		1.0	1.4	1.8	1.2				.3		
5EW	ρa	1.6	—	3.0	9.2	6.4	3.7	—	—	—	9.5	11.9	5.9
	N	5		5	10	10	10				11	1	1
	Er	.3		.2	1.4	.5	.4				.2		
6NS	ρa	1.0	—	0.4	0.6	0.4	1.3	—	—	—	0.8	0.8	—
	N	3		6	10	10	8				7	1	1
	Er	.3		.1	.1	.02	.05				.04		
6EW	ρa	0.8	—	0.2	0.4	0.7	2.8	—	—	—	0.6	0.8	0.3
	N	3		3	9	9	7				10	1	1
	Er	.2		.03	.04	.08	.3				.03		
7NS	ρa	3.0	—	1.6	1.0	3.0	10.2	—	—	—	11.6	28.	4.2
	N	2		5	10	10	10				11	1	1
	Er	.2		.9	.1	.3	1.4				.7		
7EW	ρa	0.9	—	1.3	0.7	3.6	3.4	—	—	—	9.5	9.4	4.5
	N	1		5	10	10	8				8	1	1
	Er			.2	.7	.2	.3				1.2		
8NS	ρa	1.6	—	3.9	9.4	18.	17	—	—	—	20.	4.4	11.4
	N	5		6	7	10	10				10	1	1
	Er	.3		.6	2.0	1.4	2.2				3.2		
8EW	ρa	4.9	—	5.0	17.	15.	139	—	—	—	48	—	3.7
	N	4		5	10	8	7				10		1
	Er	.4		1.7	5.4	2.2	29				3.2		

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Sta. No.		FREQUENCY 7.5	10	14	27	76	285	685	1.2K	3.3K	6.7K	10.2K	18.6K
13N	ρa	4.3	—	3.0	8.0	17.	18	—	—	—	80	56	—
	N	6		5	10	10	2				10	1	
	Er	1.6		1.1	.9	1.8	.1				3.5		
13E	ρa	4.4	—	5.3	19.	28	24.	—	—	—	61.	65	—
	N	5		5	10	10	10				10	1	
	Er	.7		.6	2.0	1.8	2.7				5.		
14N	ρa	1.0	—	3.5	4.2	9.0	15.	—	—	—	27	15	3.1
	N	3		6	10	10	8				10		
	Er	.1		1.3	.3	.5	1.2				1.3		
14E	ρa	1.2	—	3.0	5.9	11.	11	—	—	—	25	14	4.9
	N	4		5	10	10	8				10		
	Er	.2		.6	.7	.4	.8				.6		
15N	ρa	1.4	—	.5	1.5	1.6	1.1	—	—	—	4.5	1.9	1.6
	N	4		5	10	10	5				10	1	1
	Er	.6		.2	.2	.1	.2				.08		
15E	ρa	1.7	—	.9	1.6	2.4	2.7	—	—	—	1.6	2.6	.9
	N	3		6	10	10	5				10	1	1
	Er	.5		.1	.2	.3	.2				.1		
16N	ρa	1.0	—	.24	.42	.38	.45	—	—	—	.66	.57	.33
	N	4		3	8	10	2				10	1	1
	Er	.45		.09	.06	.04	.07				.01		
16E	ρa	.45	—	.20	.37	.45	.86	—	—	—	.65	1.0	.34
	N	5		5	6	10	2				10	1	1
	Er	.05		.04	.07	.04	.15				.02		

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9NS	ρa	1.0	-	0.9	1.3	1.5	2.0	-	-	-	55	18	-
	N	4		3	10	10	8				5	1	1
	Er	.3		.1	.1	.1	.2				6.		
9EW	ρa	1.3	-	1.6	1.2	2.6	2.0	-	-	-	46	8.0	11.6
	N	5		7	10	10	5				8	1	1
	Er	.1		.6	.1	.2	.2				6.7		
10NS	ρa	.9	-	1.0	5.4	10	18	-	-	-	25	28	7.2
	N	5		5	10	10	7				11	1	1
	Er	.1		.3	.7	.9	1.2				.9		
10EW	ρa	4.2	-	7.9	14	28	16	-	-	-	18	13	5.0
	N	5		6	10	10	7				10	1	1
	Er	.7		1.5	1.1	2.4	1.2				.8		
11NS	ρa	.6	-	.5	.3	.5	.7	-	-	-	3.2	4.0	5.9
	N	4		2	8	11	2				10	1	1
	Er	.2		.05	.07	.07	.06				.1		
11EW	ρa	.7	-	.3	.7	2.1	5.3	-	-	-	4.3	4.0	6.2
	N	4		4	10	10	3				11	1	1
	Er	.2		.1	.05	.06	.3				.2		
12NS	ρa	9.1	-	2.7	9.3	13	13	-	-	-	14	5	1.4
	N	5		5	10	10	2				3	1	1
	Er	5.2		.5	1.3	.6	1.1				1.8		
12EW	ρa	2.1	-	2.9	3.9	6.2	10.0	-	-	-	-	8	2.2
	N	5		7	10	7	5					1	1
	Er	.6		.8	.5	.9	.6						

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17N	ρa	.9	—	1.0	1.1	1.5	1.5	—	—	—	2.5	5.4	.5
	N	4		5	10	10	4				10	1	1
	Er	.2		.2	.1	.1	.2				.1		
17E	ρa	.3	—	.4	.8	1.6	1.7	—	—	—	2.8	3.7	1.5
	N	4		4	10	10	4				9	1	1
	Er	.03		.1	.1	.1	.1				.1		
18N	ρa	1.2	—	1.3	3.5	6.8	28	—	—	—	50	94	26
	N	4		6	10	10	10				10	1	1
	Er	.3		.1	.4	.3	.6				1.2		
18E	ρa	.9	—	.6	3.4	4.3	12	—	—	—	22	26	—
	N	3		4	10	10	3				10	1	1
	Er	.2		.2	.4	.4	1.0				.6		
19N	ρa	1.0	—	3.3	34.	62	47	—	—	—	89	—	33
	N	5		4	10	10	2				10	1	1
	Er	.3		.3	4.7	7.7	6.7				4.5		
19E	ρa	3.6	—	2.8	29.	23	—	—	—	—	79	—	17
	N	5		5	10	10					11	1	1
	Er	.4		.2	2.6	2.0					4.3		
20N	ρa	1.1	—	2.0	5.0	9.8	—	—	—	—	19	15	9.9
	N	3		4	10	10					10	1	1
	Er	.3		.6	.5	.5					.9		
20E	ρa	1.8	—	1.6	6.0	11.	49	—	—	—	19	13	14
	N	3		5	10	10	3				10	1	1
	Er	.4		.4	.9	.6	.2				1.5		

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21N	ρa	.6	—	1.4	1.9	3.5	8.2	—	—	—	1.0	1.1	.7
	N	3		6	8	10	5				10	1	1
	Er	.2		.6	.3	.5	.4				.03		
21E	ρa	1.2	—	1.4	2.3	3.4	3.4	—	—	—	1.5	2.4	.5
	N	3		5	9	10	3				10	1	1
	Er	.1		.3	.2	.2	.3				.05		
22N	ρa	2.4	—	2.6	7.2	8.6	6.4	—	—	—	13	7.3	5.0
	N	2		5	10	10	5				10	1	1
	Er	1.4		.3	.6	.3	1.6				.3		
22E	ρa	1.5	—	1.8	5.5	8.0	6.0	—	—	—	9.8	10.1	7.5
	N	4		4	10	10	5				11	1	1
	Er	.5		.5	.3	.8	.7				1.2		
23N	ρa	5.4	—	9.	25	59	78	—	—	—	162	121	92.
	N	5		7	10	10	5				10	1	1
	Er	1.0		1.4	2.6	13.	28				3.7		
23E	ρa	14	—	26	60	105	76	—	—	—	171	262	200
	N	3		5	10	10	5				10	1	1
	Er	3.0		5.5	4.5	36.	14.				5.8		
24N	ρa	1.4	—	3.1	8.8	12	11	—	—	—	17	17	9.5
	N	5		5	10	10	5				10	1	1
	Er	.5		.7	1.3	.5	.8				1.1		
24E	ρa	1.2	—	1.0	4.2	7.9	13	—	—	—	14	20	5.8
	N	3		4	10	10	5				11	1	1
	Er	.2		.2	.3	.3	.5				.6		

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25N	ρa	—	—	—	—	—	—	—	—	—	—	—	—
	N												
	Er												
25E	ρa	2.3	—	11.7	18.	31.	26.	—	—	—	51	33	102
	N	3		6	10	10	6				10	1	1
	Er	.4		2.0	1.5	1.1	1.5				1.9		
26N	ρa	.86	—	2.8	6.4	15	13	—	—	—	29	8	13
	N	4		6	10	10	1				9	1	1
	Er	.04		1.0	1.2	1.4					2.8		
26	ρa	2.1	—	2.6	6.7	11	15	—	—	—	31	15	16
	N	5		5	10	10	5				10	1	1
	Er	.4		.6	.7	.6	1.6				1.8		
	ρa												
	N												
	Er												
	ρa												
	N												
	Er												
	ρa												
	N												
	Er												
	ρa												
	N												
	Er												