(200) R290 No.79-931

UNITED STATES

3 1818 00073385 5

DEPARTMENT OF THE INTERIOR

GEOLOGICAL SURVEY

TH comentary

PRELIMINARY CATALOG OF EARTHQUAKES

IN NORTHERN IMPERIAL VALLEY, CALIFORNIA

JULY 1978 - SEPTEMBER 1978

Ву

V. Lamanuzzi and C. E. Johnson
U.S. Geological Survey
Seismological Laboratory
California Institute of Technology
Pasadena, California 91125

OPEN-FILE REPORT

79-931

This report is preliminary and has not been edited or reviewed for conformity with Geological Survey standards and nomenclature.

297700



# PRELIMINARY CATALOG OF EARTHQUAKES IN NORTHERN IMPERIAL VALLEY, CALIFORNIA JULY 1978 - SEPTEMBER 1978

						CO	NT	EN'	rs												
																					Page
Introduction				•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	1
Area Covered	and	Ins	str	um	en	tai	ti	on													1
Data Analysis																					2
Discussion .																					3
References .																					5
					ILI	LUS	STE	RAT	CIC	ONS	3										
Figure 1.	Bas	e M	lap	0	f	Sou	ıtl	nei	cn	Ca	a1:	if	ori	nia	a						6
Figure 2.		the	•																		7
	and	SE	:15	mO	gra	арі	1 .	3 La	ı.	LOI	15	•	•	•	•	•	•	•	•	•	7
Table 1.	Sta	tic	n	Dat	ta				•							•	•		•		8
Table 2.	for	lin Ea	rt	hqi	ual	ces	5	Erc	om	Ju	113	y ]	1,1	197	78						
	cnr	oug	n	per	DIE	emi	)ei		U,		19	10									9

## INTRODUCTION

The northern section of the Imperial Valley region in southern California is an area of known geothermal resources and high seismicity. To investigate the relationship between geothermal areas and earthquakes in the Imperial Valley, a 16-station seismic network was established in early 1973 by the U. S. Geological Survey. Six more stations were added to the network in November 1976. This catalog contains a description of the network and a list of preliminary data on earthquakes detected and recorded by the network from July 1978 through September 1978.

#### AREA COVERED AND INSTRUMENTATION

Earthquakes reported in this catalog are located in the area indicated in Figure 1. Locations of most of the seismographic stations used to locate the earthquakes reported here are listed in Table 1 and many of these are shown in Figure 2.

The telemetered seismographic network in the Imperial Valley employs the same type of instrumentation developed by the U. S. Geological Survey for use in the central California network. (See Wesson and others, 1974, or Hill and others, 1975, for more details.) Seismometers are mostly vertical-

component Mark Products instruments (Model L-4C)  $\frac{1}{}$  (T<sub>seis</sub> = 1 sec.). Horizontal component instruments are present only at stations SNR and DHS. Signals from these instruments are filtered in the field (T<sub>amplifier</sub> = 0.1 sec.), multiplexed, and telemetered to the California Institute of Technology in Pasadena, California. At Caltech, the signals are discriminated and filtered again (T<sub>discriminator</sub>  $\approx$  0.3 sec.). The signals are digitally recorded by the Caltech Earthquake Detection and Recording System (CEDAR) (Johnson, 1978a) and are also recorded on 16mm films using Develocorders  $\frac{1}{}$  (T<sub>galvo</sub> = 0.06 sec.). When a Geotech  $\frac{1}{}$  film viewer is used, peak magnification ranges from 10 $^5$  to 10 $^6$  and occurs at T<sub>peak</sub>  $\approx$  0.3 sec. An earthquake detection algorithm is used in CEDAR, and only "detected" earthquakes are saved.

#### DATA ANALYSIS

During this quarter, all analysis has been based on the digital recordings made by CEDAR. (For a description of the CEDAR data reduction procedure, see Johnson, 1978a, or Fuis, Johnson, and Richter, 1978.) To locate each earthquake, P and S wave arrival time data were processed using an abbreviated and modified version of the computer program HYPO71 (Lee and Lahr, 1975). During this step, no station delays were used and a simple velocity structure was imposed (see Discussion).

The geographic areas in which the resulting preliminary epicenters are located determine which velocity structures and associated station delays should be used for subsequent refinement of the locations. These ultimate locations will appear in the final catalog and will be based on the use of new, improved, and regionalized velocity models to be obtained from upcoming

<sup>1/</sup> Any use of trade names and trademarks in this publication is for descriptive purposes only and does not constitute endorsement by the U. S. Geological Survey.

refraction-calibration explosions in the Imperial Valley.

This catalog lists only the preliminary location parameters for all well-located earthquakes in northern Imperial Valley for this quarter. These preliminary parameters appear in Table 2. The epicenters are plotted in Figure 2.

#### DISCUSSION

The velocity model used for the earthquake locations in this catalog is taken from Kanamori and Hadley (1975):

VELOCITY	DEPTH TO						
(km/sec)	TOP OF LAYER (km)						
5.5	0.0						
6.3	5.5						
6.7	16.0						
7.8	37.0						

This model was obtained from refraction studies in the western Mojave

Desert, Transverse Ranges, and Peninsular Ranges of southern California.

For a discussion of the differences in earthquake location that result from using this model rather than a more appropriate model for Imperial Valley

(Biehler and others, 1964), refer to Fuis, Johnson, and Jenkins (1978).

Richter magnitudes have been calculated for all events in this catalog with  $M_L \geq 3.0$  and for some earthquakes with smaller magnitudes. Magnitudes appearing in the final catalog will be based on values of  $M_L$ ,  $M_{CA}$  (coda-amplitude magnitudes calculated from the digital CEDAR recordings), and other data where possible. (For a description of  $M_{CA}$ , see Johnson, 1978b.)

A filter was applied to the events in this catalog to eliminate very bad hypocenter solutions. A location was not listed or plotted unless its solution quality, Q (slightly different from that of Lee and Lahr, 1975), was either A, B, or C (see below). No arrival times have been reread to improve the preliminary locations.

-Coordinated Universal Time

The hypocentral parameters listed in Table 2 are the following:

- 1) Y, year of occurrence
- 2) M, month of occurrence
- 3) D. day of occurrence
- 4) H, hour of occurrence
- 5) M. minute of occurrence
- 6) SEC, second of occurrence
- 7) LAT, north latitude of epicenter, in degrees and minutes
- 8) LONG, west longitude of epicenter, in degrees and minutes
- 9) DEP, depth of hypocenter, in kilometers
- 10) MAG, magnitude
- 11) N, number of P and S arrivals used in locating the earthquake
- 12) GAP, maximum azimuthal gap, in degrees, between stations contributing P or S arrivals
- 13) DM, distance from epicenter to nearest station used in locating the earthquake, in kilometers
- 14) RMS, root mean square of travel time residuals, R<sub>i</sub>, in seconds

$$RMS = \sqrt{\sum_{i=1}^{N} R_i^2 / N}$$

- 15) ERH, standard error of the epicenter, in kilometers
- 16) ERZ, standard error of the focal depth, in kilometers
- 17) Q, solution quality of the hypocenter:

2	RMS	ERH	ERZ
A	< 0.15	< 1.0	≤ 2.0
В	< 0.30	≤ 2.5	< 5.0
C	< 0.50	< 5.0	_
D	others	-	

### REFERENCES CITED

- Biehler, S., R. L. Kovach, and C. R. Allen, 1964, Geophysical framework of the northern end of the Gulf of California structural province, in Marine Geology of the Gulf of California (T. J. van Andel and G. G. Shor, Jr., eds.): Am. Assoc. Pet. Geol. Memoir, 3, p. 126-156.
- Fuis, C. S., C. E. Johnson, and D. J. Jenkins, 1978, Preliminary catalog of earthquakes in northern Imperial Valley, California, October 1977 December 1977: U.S. Geol Survey, Open-file Rept. 78-673, 144p.
- Fuis, C. S., C. E. Johnson, and K. J. Richter, 1978, Preliminary catalog of earthquakes in northern Imperial Valley, California, April 1978 June 1978: U.S. Geol. Survey, Open-file Rept. (in review), 20p.
- Hill, D. P., P. Mowinckel, and K. M. Lahr, 1975, Catalog of earthquakes in the Imperial Valley, California, June 1973 May 1974: <u>U.S. Geol.</u>

  <u>Survey, Open-file Rept. 75-401</u>, 25p.
- Johnson, C. E., 1978a, CEDAR an approach to the computer automation of short-period, local seismic networks: <u>EOS</u>, v.59, p. 316.
- Johnson, C. E., 1978b, Ph.D. Thesis, California Institute of Technology, (in preparation).
- Kanamori, H., and D. M. Hadley, 1975, Crustal structure and temporal velocity change in southern California: <u>Pure Appl. Geophys.</u>, v.113, pp. 257-280.
- Lee, W. H. K. and J. C. Lahr, 1975, HYPO71 (Revised): A computer program for determining hypocenter, magnitude, and first-motion pattern of local earthquakes: U.S. Geol. Survey, Open-file Rept. 75-311, 113p.
- Wesson, R. L., F. W. Lester, and K. M. Meagher, 1974, Catalog of earthquakes along the San Andreas fault system in central California, October December 1972: U.S. Geol. Survey, Open-file Rept., 46p.

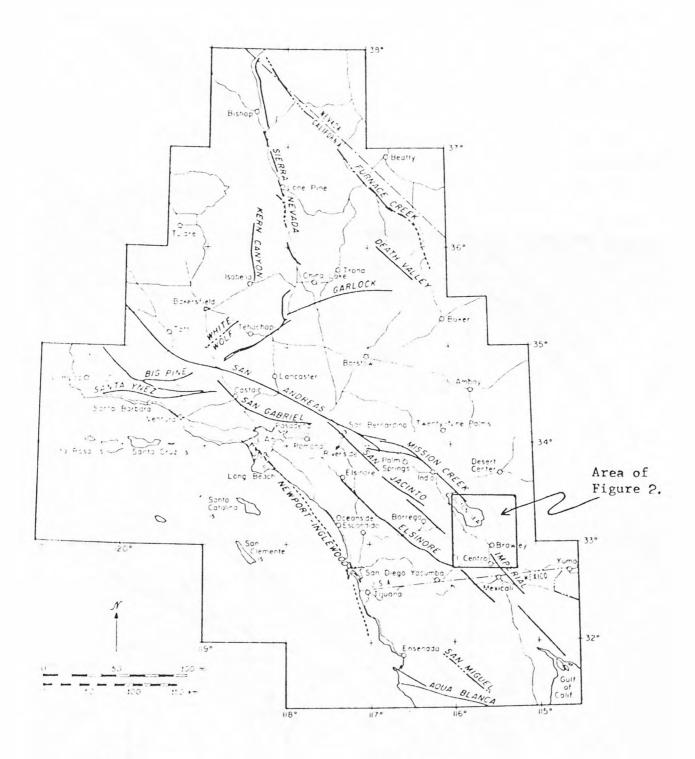


Figure 1. Base map of southern California region with major faults.

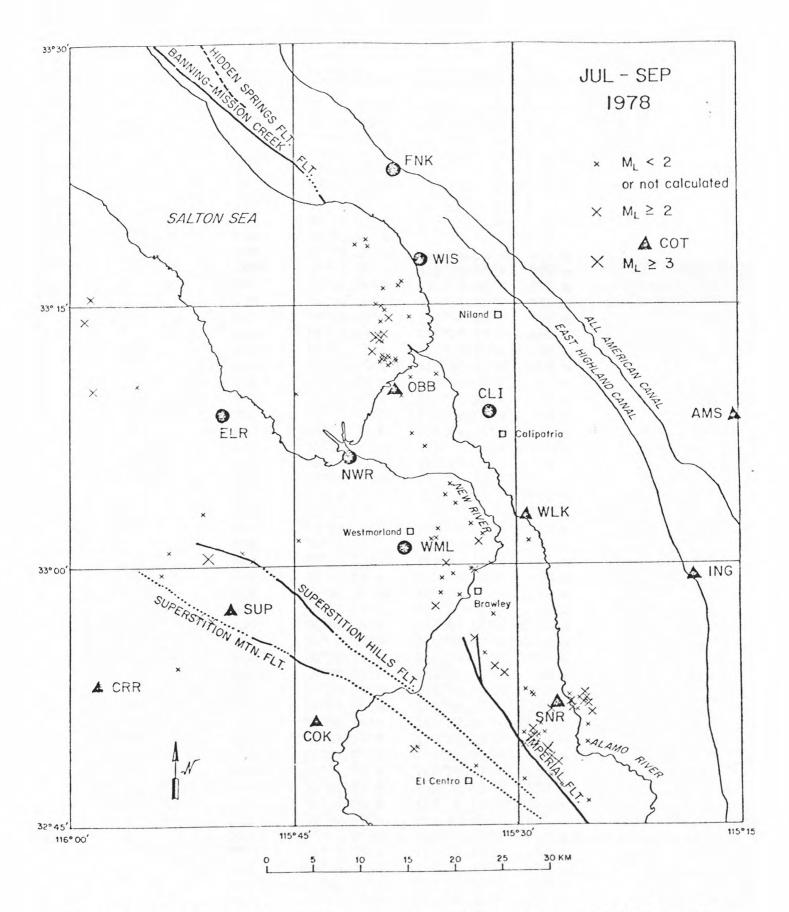


Figure 2. Locations of earthquake epicenters (X's) in the Imperial Valley with respect to major faults for the period July 1, 1978 through September 30, 1978. Solid triangles are seismograph stations in the Imperial Valley installed in 1973; solid circles are the seismograph stations installed in November 1976.

STATION	LATITUDE	LONGITUDE	ELEV.
AMS	33° 8.48' N	115°15.25'W	140 m
BAR	32°40.80'N	116°40.30'W	549 m
BC2	33°39.42'N	115°27.67'W	1185 m
BON	32°41.67'N	115°16.11'W	14 m
BSC	32°43.49'N	115° 2.64'W	43 m
CH2	33°17.77'N	115°20.17'W	347 m
CLI	33° 8.45' N	115°31.64'W 115° 7.36'W	-59 m
COA	32°51.81'N	115° 7.36'W	34 m
COK	32°50.95'N	115°43.61'W	-15 m
COY	32°50.95'N 33°21.63'N	116°18.56'W	232 m
C02	33°50.83'N	115°20.68'W	276 m
CPE	32°52.80'N	117° 6.00'W	213 m
CPM	34° 9.24'N	116°11.80'W	937 m
CRR	32°53.18'N	115°58.10'W	98 m
DHS	33°55.58'N	116°23.13'W	442 m
DHSE	33°55.58'N	116°23.13'W	442 m
DHSN	33°55.58'N	116°23.13'W	442 m
ELR	33° 8.84'N	115°49.95'W	-63 m
FNK	33°22.98'N	115°38.26'W	
GLA	33° 3.10'N	114°49.60'W	/
HOT	33°18.85'N		
IKP		116°34.90'W 116° 6.48'W	1963 m
	32°38.93'N		957 m
ING	32°59.30'N	115°18.61'W	2 m
INS	33°56.14'N	116°11.66'W	1700 m
JUL	33° 2.90'N	116°36.77'W	1292 m
KEE	33°38.30'N	116°39.19'W	1366 m
LTC	33°29.34'N	115° 4.20'W	458 m
MOV	34° 9.35' N	116°30.10'W	1239 m
WAS	33° 5.43'N	115°41.54'W	-68 m
OBB	33°10.04'N	115°38.20'W	-69 m
PLM	33°21.20'N	116°51.70'W	1692 m
PLT	32°43.87'N	114°43.76'W	61 m
PNM	33°58.64'N	115°48.05'W	1146 m
RAY	34° 2.18'N	116°48.67'W	2342 m
RMR	34°12.77'N	116°34.52'W	1702 m
RUN	32°58.33'N	114°58.63'W	152 m
SGL	32°38.95'N	115°43.52'W	110 m
SHH	34°11.26'N	115°39.27'W	1122 m
SMO	33°32.15'N	116°27.70'W	2437 m
SNR	32°51.71'N	115°26.21'W	-30 m
SNRE	32°51.71'N	115°26.21'W	-30 m
SNRN	32°51.71'N	115°26.21'W	-30 m
SUP	32°57.31'N	115°49.43'W	219 m
TPC	34° 6.35'N	116° 2.92'W	761 m
VG2	33°49.91'N	116°48.55'W	1484 m
WIS	33°16.56'N	115°35.58'W	-68 m
WLK	33° 3.08'N	115°29.44'W	-48 m
WML	33° 0.91'N	115°37.35'W	-44 m
WWR	33°59.51'N	116°39.36'W	702 m
YMD	32°33.28'N	114°32.68'W	76 m
1000			1

# Table 2.

Preliminary hypocenter solutions for earthquakes July 1, 1978 through September 30, 1978. Note that "N" and "DM" have not been calculated for this preliminary report.

Y	M D	Н	М	SEC	LAT	LONG	DEP	MAG	N	GAP	DM	RMS	ERH	ERZ Q
7 8	7 1	3	44	32.98	32-52.06	115-25.54	3.58	2.40		86		0.21	1.2	1.0 B
78	7 1	6	16	59.89	32-50,82	115-28.43	10.17	0.0		140		0.10	0.9	
78	7 1	18	13	24.85		115-32.28				83		0.24	1.3	1.3 B
78	7 3	2	28	15.38	33- 3.04	115-51.10	5 . CO	0.0		92		0.17	1.6	1.4 B
78	7 4	21	13	58.34	33-10.38	115-55.43	10.14	0.0		71		0.15	1.6	3.0 B
78	7 5	21	37	20.22	32-57.93	115-43.27	5.58	0.0		03		C.15	0.9	7.5 C
78	7 6	7	21	22.70	32-47.82	115-27.71	13,25	C.C		115		0.15	0.8	U.8 B
78	7 6	10	4()	39.11	33- 4.67	115-34.47	8.14	0.0		54		0.24	1.7	3.1 8
78	7 7	4	57	25.10	33- 0.78	115-48.48	5.28	0.0		64		0.22	1.4	1.4 B
78	7 8	6			33- 5.93	115-44.86				95		0.03	0.6	1.0 A
178		9	9		32-47.20	115-27.011				119		C.20	1.5	2.0 B
178		16	15				7.40			104		() = ()4	0.6	1.5 A
78	712	7	13	15.93		115-47.79	5.01			58		0.06	0.5	0.5 A
178	712	3	36	35.52		115-38.95				83		0.19	2.2	1.3 B
78	712	12	24		33-14.08	115-35.14		1.80		52		0.12	1,3	21.4 C
78	712	15	8	23.69	32-49.37	115-36.961				54		0.34	2.5	4.8 C
78	714	2 C	55	50.08		115-27.041				117		0.23	1.2	1.6 B
178	714	21	22	59,36		115-37.72		0 0		122		0,05	0.7	U.5 A
78	716	19	31			115-37.02	5.83			115		0.15	1.8	3.3 B
78	717	3	11	20.34		115-29.501		0.0		116		0.08	8.0	1.1 A
1.78	720	3	19	24.59	32-57,10	115-51.35	35.2	2.60		55		0.24	0.9	0.9 B
1 78	723	8	39	56.35	32-50.30	115-29.551				141		0.25	2.4	2.88
78	723	23	12	15.47	33-10.82		1,22			143		0.26	3,9	5.8 C
78	724	0	26	56.64			7.85			3.5		0.12	1.4	2.5 B
78	725	3	54	15.37	33- 2.38	115-33.06	8.83			65		0.14	1.0	1.7 A
78	725	5	3	55,06	32-58.27 32-57.62	115-33.84	6.72 4.51	2.30		57 111		0.07	0,6	1.4 A
E 78	727	6	24	24.54	32-58.38	115-35.121				68		0.03	0.5	0.6 A
78	727	22	26	43.35	33-14,15	115-58.92		2,50		73		0.21	1.2	1.9 B 99.0 C
78	728	17	3	5.59	32-52.30	115-25.83	3.18			117		0.08	1.0	0.5 A
178	728	18	7	25.51	32-51.47	115-24.98	3.68			88		0.26	1.3	0.7 B
2 78	729	16	20	18,83	32-48.39	115-32.79	5.54			109		0.22	2.4	
	731	23				115-25.35				85		C.22	1.1	U. 7 B
	8 2					115-50.74				48		0.24	0.9	1.2 8
	8 3					115-37.76				114		0.06	0.8	0.8 A
	8 4					115-38.91				53		0.08	1.0	0.7 A
	8 4					115-44.71				95		0.10	2,1	2.1 B
	8 5					115-25.22				107		0.25	2.0	1.3 B
	8 5		14	21.35	32-52.11	115-26.43	4.56	2.50		93		0.20	1.8	0.8 B
	8 5		9	48.62	32-51.64	115-27.70	4.45	2.5C		218		0.12	3.1	U.6 C
	8 5		40	6.49	32-52.49	115-26.51	3.95	0.0	4	209		0.05	2.5	1.4 C
2 78	8 6	0	23	2.65	32-52.CE	115-26.44	5.00	2.70		95		0.26	0.0	0.0 B
3 78	8 6	0	36	34.61	32-50.31	115-28.15	4.65	0.0		302		0.04	3.7	0.5 C
4 78	6 3	5	22	52.50	32-51.74	115-26.28	5.00	2.00		232		0.26	2.0	2.0 B
5 78	8 7	18	35	46,50	33-10.12	115-58.37	6,23	2,30		158		0.17	3,2	24.6 C
6 78						115-25.46				111		0.30	2.3	1.2 C
178						115-25.38				127		0.30	1.5	0.8 C
8 78						115-37.22				187		0.04	3.3	1.5 C
9 78						115-31.58				159		C.17		20.5 C
178	812	4	10	55.84	32-59.25	115-35.04	5.42	0.0		138		0.04	0.7	0.4 4

78	ER Z 1.5 1.1	Q
TR   815   O   22   50.90   32-49.35   115-27.9713.86   3.30   104   C.32   1.1     TR   E15   C   31   55.0E   32-52.55   115-29.01   1.51   0.0   180   0.08   1.2     TR   815   O   37   43.92   32-49.67   115-29.49   5.12   2.40   145   0.21   2.7     TR   815   C   38   36.55   32-52.47   115-28.92   7.44   0.0   164   0.03   0.7     TR   815   C   38   36.55   32-52.62   115-29.45   5.00   0.0   0.24   1.6     TR   815   O   39   31.36   32-50.51   115-28.9611.35   2.60   58   0.24   1.4     TR   815   C   40   12.93   32-50.16   115-28.9611.35   2.60   58   0.24   1.4     TR   815   C   40   12.93   32-50.16   115-28.7611.23   0.0   103   0.24   1.6     TR   817   D   18.84   32-49.62   115-28.7611.23   0.0   103   0.29   1.7     TR   817   D   18.84   32-49.62   115-28.7611.23   0.0   103   0.29   1.7     TR   817   D   2   44.60   33-   0.12   115-34.77   8.51   2.40   89   0.19   1.2     TR   818   15   29   27.74   22-48.92   115-27.7013.22   2.60   107   0.27   1.5     TR   818   15   49   25.81   32-45.37   115-27.9613.35   2.80   105   0.24   1.4     TR   818   16   30.31   32-50.20   115-28.79   5.00   0.0   0.25   1.4     TR   818   18   16   30.31   32-50.20   115-28.79   5.00   0.0   0.25   1.4     TR   819   10   33   47.95   32-49.97   115-28.6110.51   0.0   0.0   0.25   1.4     TR   819   10   33   47.95   32-49.97   115-28.9512.10   0.0   0.0   0.16   1.8     TR   819   12   20   55.02   32-50.14   115-28.9610.24   0.0   0.0   0.16   2.1     TR   823   6   34   24.23   32-50.21   115-28.9512.10   0.0   0.16   2.1     TR   823   6   34   24.23   32-55.52   115-53.85   5.26   1.60   0.0   0.16   2.1     TR   823   14   59   56.28   32-55.52   115-32.8814.04   2.30   106   0.11   0.7     R   824   2 2 2 27.30   32-45.45   115-32.8814.04   2.30   106   0.16   2.5     TR   827   2 48   16.55   33-0.07   115-31.7411.05   0.0   93   0.16   3.5     TR   827   2 48   16.55   33-0.07   115-31.7411.05   0.0   93   0.16   3.5     TR   827   2 48   16.55   33-0.07   115-31.7411.05   0.0   0.0   0.16		
78 815         0 22 50.90         32-49.35         115-27.9713.86         3.30         104         0.32         1.1           78 815         0 31 55.08         32-52.55         115-29.01         1.51 0.0         180         0.08         1.2           78 815         0 37 43.93         32-52.55         115-29.49         5.12 2.40         145         0.21 2.7           78 815         0 38 50.86         32-52.47         115-28.92         7.44 0.0         164         0.03         0.7           78 815         0 38 50.86         32-52.62         115-28.96         1.0         164         0.03         0.7           78 815         0 39 31.36         32-50.51         115-28.9611.35         2.60         58         0.24         1.4           78 815         0 39 31.36         32-50.16         115-28.9611.35         2.60         58         0.24         1.4           78 815         1 29 18.84         32-49.62         115-28.7611.32         0.0         103         0.29         1.7           78 817         5 5         0.25         32-56.84         115-30.71         2.40         78         0.25         1.3           78 818         15 2 9 2.74         32-46.57         115-27.7013.22		Δ
TRE 615		
78 815       0 27 42.92       32-45.67       115-29.49       5.12       2.40       145       0.21       2.7         76 815       C 38 36.59       32-52.47       115-28.92       7.44       0.0       164       0.03       0.7         78 815       C 38 50.69       32-52.62       115-28.961.32       2.60       52       0.28       1.5         78 815       O 39       31.36       32-50.16       115-28.9611.35       2.60       58       0.24       1.4         78 815       O 40       12.93       32-50.16       115-28.9611.35       2.60       58       0.24       1.4         78 815       1 29       18.84       32-49.62       115-28.7011.23       0.0       103       0.24       1.6         78 817       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78 817       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78 818       15       29       27.74       32-46.57       115-27.7013.22       2.60       107       0.27       1.5         78 818       16       46       55.37	6.9	
76       815       C       38       36.59       32-52.47       115-28.92       7.44       0.0       164       0.03       0.7         78       815       C       38       50.69       32-52.62       115-29.45       5.00       0.0       92       0.28       1.5         78       815       O       39       31.36       32-50.51       115-28.8710.77       2.50       100       0.24       1.6         78       815       C       40       12.93       32-50.16       115-28.8710.77       2.50       100       0.24       1.6         78       815       C       40       12.93       32-56.84       115-28.8710.77       2.50       100       0.24       1.6         78       817       5       0.25       32-56.84       115-20.7511.33       0.0       103       0.29       1.7         78       817       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78       817       29       27.74       32-46.92       115-27.7013.22       2.60       107       0.27       1.5         78       818       15       49       35.81	3.0	
78 815       C 38 5C, E9 32-52. E2 115-29.45 5.0C 0.0       92       0.28 1.5         78 815       O 39 31.36 32-50.51 115-28.9611.39 2.6C       98       0.24 1.4         78 815       C 40 12.93 32-50.16 115-28.8710.77 2.90 100 0.24 1.6       0.24 1.6         78 815       1 29 18.84 32-49.63 115-28.7011.23 0.0 103 0.29 1.7       0.29 1.7         78 817       5 5 0.25 32-56.84 115-50.51 5.43 2.40 78 0.25 1.3       0.29 1.7         78 818 15 29 27.74 32-46.92 115-27.7013.22 2.60 107 0.27 1.5       0.19 1.2         78 818 15 29 27.74 32-46.92 115-27.7013.22 2.60 107 0.27 1.5       0.60 0.4         78 818 16 46 55.37 32-46.57 115-27.2412.67 2.70 138 0.06 0.4       0.60 0.4         78 818 18 16 30.31 32-50.20 115-28.79 5.00 0.0 105 0.24 1.4       0.24 1.4         78 818 18 16 30.31 32-50.20 115-28.79 5.00 0.0 100 0.25 1.4       0.22 1.8         78 819 10 33 47.95 32-49.97 115-28.6110.10 0.0 100 0.25 1.4       0.22 1.8         78 819 10 33 47.95 32-49.97 115-28.9512.10 0.0 100 0.16 1.8       0.16 1.8         78 823 6 34 24.23 32-45.74 115-25.29 4.44 0.0 136 0.16 2.1       0.16 2.2         78 823 17 10 24.54 32-55.76 115-32.8814.04 2.30 106 0.1       0.16 0.11 1.2         78 823 17 10 24.54 32-55.76 115-32.8814.04 2.30 106 0.1       0.11 1.2         78 824 2 25 27.30 32-45.45 115-36.7214.28 0.0 0.1       105 0.16 3.5         78 827 2 2 48 18.55 33- 0.07 115-31.7411.05 0.0 93 0	U. 9	
78       815       0       39       31.36       32-50.51       115-28.9611.35       2.60       \$8       0.24       1.4         78       815       0       12.93       32-50.16       115-28.8710.77       2.50       100       0.24       1.6         78       815       1       29       18.84       32-45.62       115-28.7611.33       0.0       103       0.29       1.7         78       817       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78       817       2       8       44.50       32-66.92       115-27.7013.22       2.40       89       0.19       1.2         78       818       15       29       27.74       32-46.92       115-27.7013.22       2.40       89       0.19       1.2         78       818       15       29       27.74       32-46.92       115-27.7013.22       2.60       107       0.27       1.5         78       818       16       46.55.37       32-45.34       115-27.913.39       2.80       105       0.24       1.4         78       818       18       16       30.31       32-50.20 </td <td></td> <td></td>		
78       815       C       40       12.93       32-50.16       115-28.8710.77       2.90       100       0.24       1.6         78       815       1       29       18.84       32-49.62       115-28.7011.22       0.0       103       0.29       1.7         78       817       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78       817       2       8       44.90       33-       0.12       115-34.77       8.51       2.40       89       0.19       1.2         78       818       15       29       27.74       22-46.92       115-27.7013.22       2.60       107       0.27       1.5         78       818       15       29       23.74       32-46.57       115-27.7013.22       2.60       107       0.27       1.5         78       818       16       40       35.81       32-46.57       115-27.7013.22       2.60       107       0.27       1.5         78       818       16       40       35.81       115-27.7013.22       2.60       105       0.24       1.4         78       818       16       63.031	1.6	
78       815       1       29       18.84       32-49.62       115-28.7611.23       0. C       103       0.29       1.7         78       817       5       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78       817       22       8       44.90       33- C.12       115-34.77       8.51       2.40       89       0.19       1.2         78       818       15       29       27.74       32-48.92       115-27.7013.22       2.60       107       0.27       1.5         78       818       15       49       35.81       32-48.52       115-27.2412.67       2.70       128       0.06       0.4         78       818       16       46       55.37       32-45.34       115-27.9613.39       2.80       105       0.24       1.4         78       818       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.0       4         78       819       10       33       47.95       32-49.81       115-28.6110.11       0.0       100       0.16       1.8         78       81	1.5	
78       817       5       5       0.25       32-56.84       115-50.51       5.43       2.40       78       0.25       1.3         78       817       22       8       44.90       33-       C.12       115-34.77       8.51       2.40       89       0.19       1.2         78       818       15       29       27.74       32-48.92       115-27.7013.22       2.60       107       0.27       1.5         78       818       15       49       35.81       32-48.57       115-27.2412.67       2.70       138       0.06       0.4         78       818       16       46       55.37       32-45.34       115-27.9613.35       2.80       105       0.24       1.4         78       818       18       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.0       4         78       818       18       16       30.31       32-50.20       115-28.5610.96       0.0       100       0.25       1.4         78       819       10       33       47.95       32-49.97       115-28.56110.91       0.0       100       0.16       1.8      <	1.8	
78       817       22       8       44.50       33-       C.12       115-34.77       8.51       2.40       89       0.19       1.2         78       818       15       29       27.74       32-46.92       115-27.7012.22       2.60       107       C.27       1.5         78       818       15       49       35.81       32-46.57       115-27.2412.67       2.70       128       0.06       0.4         78       818       16       46       55.37       32-45.34       115-27.9613.39       2.80       105       0.24       1.4         78       818       18       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.0       4         78       818       18       16       30.31       32-50.20       115-28.5610.56       0.0       100       0.25       1.4         78       818       12       52.30       32-45.81       115-28.5610.56       0.0       101       0.22       1.8         78       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       129       0.16       1.8         78 <t< td=""><td>1.1</td><td></td></t<>	1.1	
78       818       15       29       27.74       22-46.92       115-27.7013.22       2.60       107       0.27       1.5         78       616       15       49       35.81       32-46.57       115-27.2412.67       2.70       128       0.06       0.4         76       818       16       46       55.37       32-45.34       115-27.9613.39       2.60       105       0.24       1.4         76       818       18       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.0       4         76       818       12       52.30       32-50.17       115-28.5610.96       0.0       100       0.25       1.4         76       819       22       8       48.15       32-50.17       115-28.5610.96       0.0       100       0.22       1.8         76       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       129       0.16       1.8         78       819       10       33       47.95       32-49.97       115-28.9512.10       0.0       100       0.16       1.8         78       819       12	1.7	
7E       E18       15       49       35.81       32-48.57       115-27.2412.67       2.70       128       0.06       0.4         7E       818       16       46       55.37       32-45.34       115-27.9613.39       2.80       105       0.24       1.4         7E       818       18       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.0       4         7E       818       22       8       48.15       32-50.21       115-28.5610.96       0.0       100       0.25       1.4         7E       819       23       32-45.81       115-28.6110.11       0.0       101       0.22       1.8         7E       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       125       0.18       1.5         7E       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       129       0.16       1.8         7E       819       12       39       15.47       32-50.21       115-28.9512.10       0.0       0.0       0.16       1.8         7E       823       7       4	1.3	
7E       818       16       46       55.37       32-45.34       115-27.9613.35       2.86       105       0.24       1.4         7E       818       18       16       30.31       32-50.20       115-28.75       5.00       0.0       100       0.21       4.0       4         7E       818       22       8       48.15       32-50.17       115-28.5610.96       0.0       100       0.25       1.4         7E       819       2       52.30       32-49.81       115-28.66110.11       0.0       101       0.22       1.8         7E       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       125       0.18       1.5         7E       819       10       33       47.95       32-49.97       115-29.0310.61       2.40       125       0.18       1.5         7E       819       10       33       47.95       32-49.97       115-28.9512.10       0.0       0.0       0.16       1.8         7E       819       12       20       55.02       32-50.14       115-28.9512.10       0.0       0.0       0.16       0.16       0.16       0.16       0.16       0.16<	0.5	
76       818       18       16       30.31       32-50.20       115-28.79       5.00       0.0       100       0.21       4.04       4         76       818       22       8       48.15       32-50.17       115-28.5610.96       0.0       100       0.25       1.4         76       819       819       52.30       32-49.81       115-28.6110.11       0.0       101       0.22       1.8         78       819       10       33       47.95       32-49.97       115-29.0210.61       2.40       129       0.16       1.8         76       819       10       33       47.95       32-49.97       115-29.0210.61       2.40       129       0.16       1.8         78       819       12       20       55.02       32-50.21       115-28.9512.10       0.0       100       0.16       1.8         78       819       12       20       55.02       32-50.14       115-28.9512.10       0.0       100       0.16       1.8         78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       126       0.16       0.2       1         78 <t< td=""><td>1.5</td><td></td></t<>	1.5	
78       818       22       8       48.15       32-50.17       115-28.5610.56       0.0       100       0.25       1.4         78       819       6       12       52.30       32-49.81       115-28.6110.11       0.0       101       0.22       1.8         78       819       10       33       47.95       32-49.97       115-29.0210.61       2.40       129       0.18       1.5         78       819       10       39       15.47       22-50.21       115-28.9512.10       0.0       100       0.16       1.8         78       819       13       20       55.02       32-50.14       115-28.9610.24       0.0       100       0.16       1.8         78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       136       0.16       2.2         78       823       6       34       24.23       32-46.32       115-25.29       4.44       0.0       124       0.20       4.7         78       823       14       59       58.28       32-59.52       115-32.88       5.36       1.60       106       0.11       1.2         78       823	1.4	
78       819       8       12       53.20       32-49.81       115-28.611C.11       C. C       101       0.22       1.8         78       819       10       33       47.95       32-49.97       115-29.021C.61       2.4C       129       C.18       1.5         78       819       10       39       15.47       32-50.21       115-28.9512.10       0.0       100       0.16       1.8         78       819       12       20       55.02       32-50.14       115-28.9512.10       0.0       100       0.16       1.8         78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       126       0.16       2.3         78       823       6       34       24.23       32-46.32       115-25.2215.56       0.0       124       0.20       4.7         78       823       14       59       58.28       32-55.52       115-32.8814.04       2.30       106       0.11       1.2         78       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       0.11       0.7         78       824       2	2.4	
78       819       10       33       47.95       32-49.97       115-29.0210.61       2.40       129       0.18       1.5         78       819       10       39       15.47       32-50.21       115-28.9512.10       0.0       100       0.16       1.8         78       819       12       20       55.02       32-50.14       115-28.9610.24       0.0       100       0.16       2.1         78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       126       0.16       2.3         78       823       6       34       24.23       32-46.32       115-25.2215.56       0.0       124       0.20       4.7         78       823       14       59       58.28       32-55.52       115-33.85       5.36       1.60       100       0.11       1.2         78       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       0.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.28       0.0       125       0.15       1.6         78       827       <	1.8	
76       £19       1C       39       15.47       22-5C.21       115-28.9512.10       0.0       100       0.16       1.8         78       819       12       20       55.02       32-5C.14       115-28.961C.24       C.C       100       C.18       2.1         78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       126       C.16       2.3         78       823       6       34       24.23       32-46.32       115-25.2215.56       0.0       124       0.20       4.7         78       823       14       59       58.28       32-55.52       115-53.85       5.36       1.6C       1C0       0.11       1.2         76       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       C.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.28       C.C       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.79       8.14       0.0       105       C.24       1.5         76       827	1.4	
78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       126       C.16       2.3         78       823       6       34       24.23       32-46.32       115-25.2215.56       0.0       124       0.20       4.7         78       823       14       59       58.28       32-55.52       115-53.85       5.36       1.60       106       C.11       1.2         78       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       C.11       0.7         78       824       2       25       27.30       32-49.45       115-36.7214.28       C.C       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.79       8.14       0.0       105       C.24       1.5         78       827       2       48       18.55       33-       0.07       115-31.7411.05       0.0       93       0.16       3.5	2.2	
78       822       7       4       33.09       32-49.74       115-25.29       4.44       0.0       136       C.16       2.3         78       823       6       34       24.23       32-46.32       115-25.2215.56       0.0       124       0.20       4.7         78       823       14       59       56.28       32-55.52       115-53.85       5.36       1.60       100       0.11       1.2         76       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       0.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.26       0.0       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.75       8.14       0.0       105       0.24       1.5         78       827       2       48       18.55       33-0.07       115-31.7411.05       0.0       93       0.16       3.5	2.6	
78       823       14       59       58.28       32-55.52       115-53.85       5.36       1.60       100       0.11       1.2         76       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       0.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.28       0.0       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.75       8.14       0.0       105       0.24       1.5         78       827       22       48       18.55       33-       0.07       115-31.7411.05       0.0       93       0.16       3.5	1.2	
78       823       14       59       58.28       32-55.52       115-53.85       5.36       1.60       100       0.11       1.2         76       823       17       10       24.54       32-55.76       115-32.8814.04       2.30       106       0.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.28       0.0       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.75       8.14       0.0       105       0.24       1.5         78       827       22       48       18.55       33-       0.07       115-31.7411.05       0.0       93       0.16       3.5		
76       823       17       10       24.94       32-55.76       115-32.8814.04       2.30       106       C.11       0.7         78       824       2       25       27.30       32-45.45       115-36.7214.28       C.C       125       0.15       1.6         78       827       4       19       30.52       32-54.14       115-52.75       8.14       0.0       105       C.24       1.5         78       827       22       48       18.55       33-       0.07       115-31.7411.05       0.0       93       0.16       3.5	0.9	
78 827 4 19 30.52 32-54.14 115-52.75 8.14 0.0 105 C.24 1.5 78 827 22 48 18.55 33- 0.07 115-31.7411.05 0.0 93 0.16 3.5	1.3	
78 827 22 48 18.55 33- 0.07 115-31.7411.05 0.0 93 0.16 3.5	3.3	В
78 827 22 48 18.55 33- 0.07 115-31.7411.05 0.0 93 0.16 3.5		
78 828 14 2 35,95 32-51,63 115-25,98 2,56 0,0 141 0.16 1.5	5.6	
- OFF T   F 23412 2F 24412 112 F2412	0.6	9
78 828 21 58 18.65 32-50.71 115-25.26 2.56 0.0 132 0.19 1.5	1.1	В
78 829 13 23 C.79 33-18.51 115-40.84 4.99 O.0 80 O.04 U.3 9	9.0	C
78 830 2 26 40,20 33-12,17 115-39.47 3.88 3.CC 42 0.21 0.7	0.7	8
78 830 2 28 50.55 33-13.24 115-39.26 4.14 2.80 42 C.25 O.6	U. 8	В
78 830 2 35 1.58 33-12.59 115-39.21 4.64 2.00 135 0.23 1.5	1.2	9
78 830 2 50 37.09 33-11.88 115-38.13 4.27 C.C 172 C.O3 O.E	U.7	A
	1.2	В
	2.3	C
	2.7	
78 830 12 48 33.33 32-59.78 115-23.0611.77 0.0 131 0.10 1.2	3.2	9
	9.5	C
78 9 3 3 46 48.73 33-27.49 115-49.38 5.00 0.0 224 0.02 C.6 S		
	0.7	
	5.2	
	0.3	
78 9 6 8 19 58.59 33-18.80 115-40.12 5.00 G.C 124 0.11 3.2 1		
	3.4	
78 913 7 41 34.80 32-54.16 115-31.49 6.18 2.20 118 0.24 1.7 2		
78 913 7 44 27.12 32-54.92 115-32.17 5.00 0.0 118 0.12 1.7 20		
	i. 6	
	2.0	
78 914 10 54 7.77 33-14.27 115-38.58 5.13 2.CC 162 0.03 0.9	0.5	Δ

														12.	
Y	M D	+	M	SEC	FAT	LCVG	CEP	MAG	N	GAP	Ch	RMS	ESF	ERZ 6	2
7.8	915	6	21	31.10	33- 2.10	115-35.31	5.44	0.0		84		0.17	2.0	1.1 B	3
78	915	$\epsilon$	35	53.61	33- 1.51	115-35.74	5.24	0.0		84		0.13	2,1	1.3 E	
78	915	11	39	29.07	33- 1.56	115-35.42	5.92	C.C		85		0.10	1.0	1.2 4	
78	915	15	39	23.44	32- 1.41	115-29.18	7.51	0.0		236		0.03	5.C	5.4 0	
37	916	3	51	26.70	33-16.14	115-37.95	4046	1.90		78		0.20	2.3	1.1 8	
78	921	5	52	27.69	33-14.57	115-39.11	4.57	O.C		83		0.13	8.0	U. 6 A	1
78	922	3	22	46.64	33-11.88	115-39.05	5.00	0.0		127		0.16	1.9	1.2 8	3
78	522	3	38	5C.75	32-11,56	115-38,78	3.74	0.0		138		C.27	1.6	1.5 E	2
78	922	8	52	55.47	33-11.82	115-38.83	5.03	0.0		100		0.15	1.2	U. 8 E	3
78	922	10	3	21.98	33-11.56	115-38.54	4.36	1.70		99		0.12	3.0	0.6 4	4
78	922	11	25	7.36	33-12,32	115-39.71	5.C2	2.50		30		0.20	0.7	U. 6 E	3
78	922	12	13	27.49	33-11.71	115-39.17	5.19	0.0		181		0.12	2.1	1.0 8	3
78	922	12	18	4.41	33-11.75	115-38.09	4,42	0.0		126		0.12	2.0	1.2 E	3
78	922	16	7	4.24	33-11.51	115-38.62	5.42	0.0		165		0.12	1.9	0.7 A	1
78	923	7	22	51.79	32-12.10	115-39.01	4.89	1.60		103		0.19	1.5	0.9 B	3
78	923	10	32	25.35	33-12°CE	115-38.62	5 , 4 C	0.0		138		C. 16	2,3	1.0 E	2
78	924	15	19	44.87	33-11.63	115-38.41	5.07	G.C		124		C.13	1.9	U. 9 A	1
78	528	4	34	54.01	33- 1.35	115-32.57	9.60	2.40		52		0.26	1.1	1.9 B	3
78	929	21	26	57.67	33- 3.55	115-34.10	5.24	0.0		88		0.11	0.9	1.4 4	1
78	930	12	57	54.61	33-14.73	115-38.88	4.14	1.60		89		0.26	2.2	2.1 8	3
									•						