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UNITED STATES DEPARTMENT OF INTERIOR

GEOLOGICAL SURVEY



Texas Instruments Model 59 Hand-Calculator Program
to Calculate Theoretical MT Planewave Soundings
over a Structure of up to 10 Horizontal Layers

By ✓ VGS

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300953

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Although this program has been extensively tested, the U.S. Geological Survey cannot guarantee that it will give correct results in any or all particular applications.

(Standard partitioning)

PROGRAM DESCRIPTION

Given an input conductivity structure of ≤ 10 horizontal "layers" (≤ 9 true layers plus underlying half-space), this program calculates magnetotelluric plane-wave apparent conductivity σ_a and phase angle $\angle E^H$ at arbitrary frequencies input by user. Alternately, an MT sounding from frequencies f_{min} to f_{max} , having n points per log cycle may be calculated. This program is a translation of Ray Watt's HP67 program.

USER INSTRUCTIONS

STEP	PROCEDURE	ENTER	PRESS	DISPLAY
1	Load side 1 and side 2, then initialize:		f_i	
2	To work with resistivities... (In this case, all symbols σ below are to be interpreted as resistivity values, not conductivities. If flag 1 not set, default case of conductivity is assumed.)		2 nd St flg 1	
3	Input layers, working from shallow to deep. Last layer entered is taken to be half-space, and program does not use h value for it.	σ_i [$\frac{m\Omega}{m}$] h_i [m]	X↔T B	
4	To calculate $\sigma_a, \angle E^H$ at frequency f (Use this option when printer not available)	f (Hz)	C X↔T	$\sigma_a, \angle E^H$
5	To calculate an MT sounding with n points per log cycle... (Use this option only with PC-100A printer.)	n f_{min} f_{max}	STO 35 X↔T E	$\sigma_a, \angle E^H$
6	For next case, press "2 nd CMS" and go to step 2.			

USER DEFINED KEYS	DATA REGISTERS (INV INT)	LABELS (Op 08)
A START	0 $w\mu_0$	INV <input type="checkbox"/> INX <input type="checkbox"/> CE <input type="checkbox"/> CLR <input type="checkbox"/> x:1 <input type="checkbox"/> x:2 <input type="checkbox"/>
B σ, h	1 Re E↑ } Used	<input checked="" type="checkbox"/> \sqrt{x} <input checked="" type="checkbox"/> STO <input type="checkbox"/> RCL <input type="checkbox"/> SUM <input type="checkbox"/> Y*
C f	2 $\text{Im } E\downarrow$ } with	EE <input type="checkbox"/> (<input type="checkbox"/>) <input type="checkbox"/> \div <input checked="" type="checkbox"/> GTO <input type="checkbox"/> X
D —	3 — } ML-4	SBR <input type="checkbox"/> - <input type="checkbox"/> RST <input type="checkbox"/> + <input type="checkbox"/> R/S <input type="checkbox"/> 0
E f_{min}, f_{max}	4 — } ML-5	+/- <input type="checkbox"/> = <input type="checkbox"/> CLR <input type="checkbox"/> INV <input type="checkbox"/> LOG <input type="checkbox"/> 0
A' —	5 Re E↓	EXP <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
B' —	6 $\text{Im } E\downarrow$	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
C' —	7 i = layer no.	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
D' —	8 σ index	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
E' —	9 h index	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
FLAGS	0 Resistivity	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	2	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	3	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	4	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	5	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	6	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	7	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	8	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS
	9	EE <input checked="" type="checkbox"/> P/m <input type="checkbox"/> P=1 <input type="checkbox"/> $\sqrt{\square}$ <input checked="" type="checkbox"/> CAS <input checked="" type="checkbox"/> CDS

Comments

1. Error conditions:
 - a. At Step 4, a flashing "-1.00 00" in display means no layers were entered.
 - b. At Step 3, a flashing "11." in display means an attempt was made to enter too many (≥ 11) layers.
 - c. If only a single layer has been entered, the program stops at Step 4 with "0.00 00" in display. (To calculate soundings over an infinite half-space, fool the program by entering 2 layers with identical conductivities.)
2. This program is a translation by Dave Campbell of Ray Watts' HP program (Campbell and Watts, 1978). The algorithm used involves the special case of equations (2) through (15) in which k_x vanishes (Watts, 1978). For an alternate treatment, see Ward (1967).
3. Users who don't have access to a PC-100 print cradle may omit quite a few steps in this program which merely handle print-out. These steps are marked by a double vertical bar on the listing on pages 3, 4, and 5.

References:

- Campbell, D. L., and Watts, R. D., 1978, Exploration geophysics calculator programs for use on Hewlett-Packard models 67 and 97 programmable calculators: U.S. Geological Survey Open-File Report 78-815, p. 56-60.
- Nekut, A., Connerney, J. E. P., and Kuckes, A. F., 1977, Deep crustal electric conductivity: evidence for water in the lower crust: Geophysical Research Letters, v. 4, no. 6, p. 239-242.
- Ward, S. H., 1967, Electromagnetic theory for geophysical application, in Ward, S. H., ed.: Mining Geophysics II, Society of Exploration Geophysicists, Tulsa, p. 107-124.
- Watts, R. D., 1978, Electromagnetic scattering from buried wires: Geophysics, v. 43, p. 767-781.



LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS
000	76	LBL	A: START	055	05	05		110	76	LBL	C:
001	11	R		056	98	ADV		111	13	C	
002	47	CMS	Clear Mem.	057	00	0		112	70	RAD	
003	01	1		058	92	RTN		113	22	INV	
004	00	0	set layer	059	76	LBL	B:	114	52	EE	
005	42	STO	indexing.	060	12	B		115	22	INV	
006	08	08		061	69	OP		116	58	FIX	
007	42	STO		062	27	27	Increment	117	42	STO	
008	35	35		063	69	OP	layer	118	00	00	
009	02	2		064	28	28	indexes.	119	02	2	
010	00	0		065	69	OP		120	03	3	"H?"
011	42	STO		066	29	29		121	04	4	
012	09	09		067	32	XIT	σ	122	06	6	
013	52	EE		068	87	IFF	Resistivity?	123	69	OP	
014	22	INV		069	01	01		124	04	04	
015	52	EE		070	35	1/X		125	43	RCL	
016	69	OP		071	71	SBR		126	00	00	
017	00	00		072	76	LBL		127	57	ENG	
018	03	3		073	76	LBL		128	58	FIX	
019	00	0		074	34	FX	\sqrt{x} :	129	02	02	
020	03	3		075	72	ST*	Store σ	130	69	OP	
021	07	7		076	08	08		131	06	06	
022	00	0		077	22	INV		132	89	r	
023	00	0	"MT_PL"	078	52	EE		133	33	X ²	
024	03	3		079	32	XIT	Thickness h	134	65	x	
025	03	3		080	42	STO	store h	135	08	8	
026	02	2		081	32	32	"M"	136	52	EE	
027	07	7		082	03	3		137	94	+/-	
028	69	OP		083	00	0		138	07	7	
029	01	01		084	69	OP		139	95	=	
030	01	1		085	04	04		140	49	PRD	Now
031	03	3		086	43	RCL		141	00	00	
032	03	3		087	32	32		142	00	0	Zero:
033	01	1	"ANEWA"	088	69	OP		143	42	STO	Re E↑
034	01	1		089	06	06		144	01	01	
035	07	7		090	72	ST*	Store h	145	42	STO	Im E↑
036	04	4		091	09	09		146	02	02	
037	03	3		092	01	1		147	42	STO	Im E↓
038	01	1		093	01	1		148	06	06	
039	03	3		094	32	XIT		149	32	XIT	
040	69	OP		095	43	RCL	too many	150	01	1	
041	02	02		096	07	07	layers?]	151	42	STO	Re E↓ = 1
042	04	4		097	77	GE		152	05	05	
043	02	2	"VE..."	098	10	E'		153	43	RCL	
044	01	1		099	42	STO		154	10	10	
045	07	7		100	10	10		155	75	-	
046	00	0		101	98	ADV		156	01	1	
047	00	0		102	92	RTN		157	95	=	
048	00	0		103	76	LBL	1/x:	158	22	INV	n-1 < 1, GTO INT
049	00	0		104	35	1/X		159	77	GE	
050	00	0		105	71	SBR					
051	00	0		106	88	DMS					
052	69	OP		107	35	1/X					
053	03	03		108	61	GTO					
054	69	OP		109	34	FX					

MERGED CODES

62	PRD	IND	72	STO	IND	83	GTO	IND
63	EE	IND	73	RCL	IND	84	OP	IND
64	OP	IND	74	SUM	IND	92	INV	SBR

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LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS
000	76	LBL	Pgm <u>A</u> : Start Clear mem. & set layer indexes.	055	05	05	Pgm <u>B</u> : Increment layer indexes. σ_i Resistivity? \bar{x} : Store σ_i Store h_i in temp. location "H" for print-out Store h_i Too many layers? Sub $1/x$: Invert σ to get ρ .	110	61	GTO	Pgm <u>C</u> : "HZ": Prepare for iteration, downward thru layers. Now Zero: ReET ImET ImEv ReEL ← 1 if $n-1 < 1$ GTO Int
001	11	A		056	98	ADV		111	34	FX	
002	47	CMS		057	00	0		112	76	LBL	
003	01	1		058	92	RTN		113	13	C	
004	00	0		059	76	LBL		114	70	RAD	
005	42	STO		060	12	B		115	22	INV	
006	08	08		061	69	DP		116	52	EE	
007	42	STO		062	27	27		117	22	INV	
008	35	35		063	69	DP		118	58	FIX	
009	02	2		064	28	28		119	42	STO	
010	00	0	065	69	DP	120	00	00			
011	42	STO	066	29	29	121	02	2			
012	09	09	067	32	X↑T	122	03	3			
013	52	EE	068	87	IFF	123	04	4			
014	22	INV	069	01	01	124	06	6			
015	52	EE	070	35	1/X	125	69	DP			
016	69	DP	071	71	SBR	126	04	04			
017	00	00	072	76	LBL	127	43	RCL			
018	03	3	073	76	LBL	128	00	00			
019	00	0	074	34	FX	129	57	ENG			
020	03	3	075	72	ST*	130	58	FIX			
021	07	7	076	08	08	131	02	02			
022	00	0	077	22	INV	132	69	DP			
023	00	0	078	52	EE	133	06	06			
024	03	3	079	32	X↑T	134	89	↑			
025	03	3	080	42	STO	135	33	X ²			
026	02	2	081	32	32	136	65	X			
027	07	7	082	03	3	137	08	8			
028	69	DP	083	00	0	138	52	EE			
029	01	01	084	69	DP	139	94	+/-			
030	01	1	085	04	04	140	07	7			
031	03	3	086	43	RCL	141	95	=			
032	03	3	087	32	32	142	49	PRD			
033	01	1	088	69	DP	143	00	00			
034	01	1	089	06	06	144	00	0			
035	07	7	090	22	INV	145	42	STO			
036	04	4	091	58	FIX	146	01	01			
037	03	3	092	72	ST*	147	42	STO			
038	01	1	093	09	09	148	02	02			
039	03	3	094	01	1	149	42	STO			
040	69	DP	095	01	1	150	06	06			
041	02	02	096	32	X↑T	151	32	X↑T			
042	04	4	097	43	RCL	152	01	1			
043	02	2	098	07	07	153	42	STO			
044	01	1	099	77	GE	154	05	05			
045	07	7	100	10	E'	155	43	RCL			
046	00	0	101	42	STO	156	10	10			
047	00	0	102	10	10	157	75	-			
048	00	0	103	98	ADV	158	01	1			
049	00	0	104	92	RTN	159	95	=			
050	00	0	105	76	LBL	MERGED CODES 62 Pgm Ind 72 STO Ind 83 GTO Ind 63 Exp Ind 73 RCL Ind 84 LBL Ind 64 DP Ind 74 SUM Ind 92 INV SBR					
051	00	0	106	35	1/X						
052	69	DP	107	71	SBR						
053	03	03	108	88	DMS						
054	69	DP	109	35	1/X	TEXAS INSTRUMENTS INCORPORATED					



LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS			
160	22	INV		215	42	STO		270	01	01				
161	77	GE		216	04	04	$\sqrt{2\sigma_{\mu 0}}$	271	39	CDS				
162	24	CE		217	94	+/-		272	71	SBR				
163	76	LBL		218	22	INV		273	76	LBL				
164	30	TAN	Lbl <u>tan</u> :	219	23	LNx	e^x	274	76	LBL	Lbl <u>sin</u> :			
165	67	EQ		220	32	X↑T		275	38	SIN				
166	10	E'	Error exit.	221	43	RCL		276	32	X↑T				
167	42	STO		222	04	04		277	65	x				
168	07	07	<u>i</u>	223	37	P/R		278	01	1				
169	85	+		224	42	STO		279	08	8				
170	01	1		225	04	04		280	00	0				
171	00	0		226	32	X↑T		281	55	÷				
172	95	=		227	42	STO		282	89	π				
173	42	STO		228	03	03		283	95	=				
174	08	08	σ index	229	36	PGM		284	75	-				
175	85	+		230	04	04	Cx mult.	285	01	1				
176	01	1		231	13	C		286	03	3				
177	00	0		232	69	DP		287	05	5				
178	95	=		233	37	37	Decrement	288	95	=				
179	42	STO		234	69	DP	all	289	42	STO				
180	09	09	h index	235	38	38	indexes	290	33	33				
181	76	LBL		236	69	DP		291	22	INV				
182	78	Σ+	Lbl <u>Σ+</u> :	237	39	39		292	57	ENG				
183	71	SBR	loop entry	238	01	1		293	22	INV				
184	59	INT		239	32	X↑T		294	58	FIX				
185	69	DP		240	43	RCL		295	01	1				
186	28	28		241	07	07		296	06	6				
187	73	RC*		242	77	GE		297	01	1	"DEG"			
188	08	08	σ_{i+1}	243	78	Σ+		298	07	7				
189	69	DP		244	71	SBR		299	02	2				
190	38	38		245	59	INT		300	02	2				
191	55	÷		246	43	RCL		301	69	DP				
192	73	RC*		247	05	05		302	04	04				
193	08	08	σ_i	248	48	EXC		303	58	FIX				
194	95	=		249	01	01		304	01	01				
195	34	FX	$\sqrt{\sigma_{i+1}/\sigma_i}$	250	42	STO		305	43	RCL				
196	49	PRD		251	03	03		306	33	33				
197	05	05	New Re Et	252	43	RCL		307	32	X↑T				
198	49	PRD		253	06	06		308	00	0				
199	06	06	New Im Et	254	48	EXC		309	77	GE				
200	71	SBR		255	02	02		310	50	IXI				
201	59	INT		256	42	STO		311	32	X↑T				
202	73	RC*		257	04	04		312	76	LBL				
203	08	08	σ_i	258	36	PGM		313	55	÷	Lbl <u>÷</u> :			
204	65	x		259	04	04		314	69	DP				
205	43	RCL		260	18	C'	Complex	315	06	06				
206	00	00	$\omega_{\mu 0}$	261	36	PGM	divide	316	22	INV				
207	65	x		262	05	05		317	58	FIX				
208	02	2		263	12	B	→ Polar	318	32	X↑T				
209	95	=		264	33	X²		319	43	RCL				
210	34	FX		265	65	x		MERGED CODES						
211	65	x		266	43	RCL		62	77	INV	72	STO	83	GTO
212	73	RC*		267	11	11		63	77	INV	73	RCL	84	77
213	09	09	h_i	268	95	=		64	77	INV	74	SUM	92	INV
214	95	=		269	87	IFF		TEXAS INSTRUMENTS INCORPORATED						



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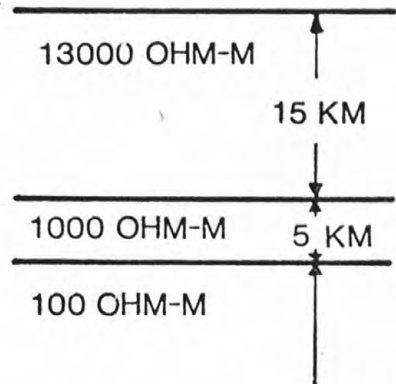
LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS	LOC	CODE	KEY	COMMENTS
320	32	32		375	32	X:IT		430	03	3	
321	98	ADV		376	76	LBL		431	02	2	
322	92	RTN		377	48	EXC		432	02	2	"OHM"
323	76	LBL	<u>Lbl Int:</u>	378	42	STO		433	03	3	
324	59	INT		379	31	31		434	03	3	
325	43	RCL	B	380	71	SBR		435	00	0	
326	01	01		381	13	C		436	69	DP	
327	85	+		382	01	1		437	04	04	
328	43	RCL		383	00	0		438	43	RCL	
329	05	05	D	384	45	YX		439	32	32	
330	95	=		385	43	RCL		440	57	ENG	
331	48	EXC		386	35	35		441	58	FIX	
332	01	01	B+D→B	387	35	1/X		442	02	02	
333	75	-		388	95	=		443	69	DP	
334	43	RCL		389	49	PRD		444	06	06	
335	05	05		390	31	31		445	22	INV	
336	95	=		391	43	RCL		446	57	ENG	
337	42	STO	B-D→D	392	34	34		447	92	RTN	
338	05	05		393	32	X:IT		448	76	LBL	Sub E: Error
339	43	RCL		394	43	RCL		449	10	E'	
340	02	02		395	31	31		450	33	X²	
341	85	+		396	22	INV		451	94	+/-	
342	43	RCL		397	77	GE		452	34	FX	
343	06	06		398	48	EXC		453	91	R/S	
344	95	=		399	92	RTN		454	00	0	
345	48	EXC	C+E→C	400	76	LBL	<u>Lbl Lbl:</u>	455	00	0	
346	02	02		401	76	LBL		456	00	0	
347	75	-		402	42	STO		457	00	0	
348	43	RCL		403	32	32	<u>Print-out</u>	458	00	0	
349	06	06		404	22	INV	<u>subroutine</u>	459	00	0	
350	95	=		405	58	FIX		460	00	0	
351	42	STO	C-E→E	406	03	3		461	00	0	
352	06	06		407	00	0		462	00	0	
353	92	RTN		408	02	2		463	00	0	
354	76	LBL	<u>Lbl cos:</u>	409	03	3	"MHO"	464	00	0	
355	39	COS		410	03	3		465	00	0	
356	35	1/X	<u>Invert</u>	411	02	2		466	00	0	
357	71	SBR		412	69	DP		467	00	0	
358	88	DMS		413	04	04		468	00	0	
359	61	GTO		414	52	EE		469	00	0	
360	38	SIN		415	58	FIX		470	00	0	
361	76	LBL	<u>Lbl 1/x:</u>	416	02	02		471	00	0	
362	50	I×I		417	43	RCL		472	00	0	
363	32	X:IT		418	32	32		473	00	0	
364	85	+		419	69	DP		474	00	0	
365	03	3		420	06	06		475	00	0	
366	06	6		421	92	RTN		476	00	0	
367	00	0		422	76	LBL	<u>Lbl DMS:</u>				
368	95	=		423	88	DMS					
369	61	GTO		424	42	STO	<u>Print-out</u>				
370	55	+		425	32	32	<u>subroutine</u>				
371	76	LBL		426	22	INV					
372	15	E		427	57	ENG					
373	42	STO		428	22	INV					
374	34	34		429	58	FIX					

MERGED CODES

62	Prn	Ind	72	STO	Ind	83	GTO	Ind
63	Int	Ind	73	RCL	Ind	84	Sub	Ind
64	Pd	Ind	74	SUM	Ind	92	INV	SBR

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EXAMPLE: NEKUT AND OTHERS (1977) GIVE THE SOLUTION SKETCHED AT RIGHT FOR RESISTIVITY STRUCTURE UNDER THE ADIRONDACK DOME. CALCULATE A 3-POINT-PER-DECADE MT SOUNDING WHICH WOULD BE SEEN OVER SUCH A STRUCTURE FOR FREQUENCIES FROM 0.001 HZ TO 1 HZ.



SOLUTION:

VARIABLE	KEY	DISPLAY	PRINT-OUT	MT PLANEWAVE	MT PLANEWAVE ++
	A	0.			
	2 nd St Flg 1	(0.)			
$\rho_1 = 13000 \text{ ohm-m}$	X↔T	(0.)	13.00 03 OHM [†]	7.69-05 MHO	
$h_1 = 15000 \text{ m}$	B	1.	15000.00 M	15000.00 M	
$\rho_2 = 1000 \text{ ohm-m}$	X↔T	(11.)	1.00 03 OHM	1.00-03 MHO	
$h_2 = 5000 \text{ m}$	B	2.	5000.00 M	5000.00 M	
$\rho_3 = 100 \text{ ohm-m}$	X↔T	(11.)	100.00 00 OHM	1.00-02 MHO	
* $h_3 = 100000 \text{ (arbitrary)}$	B	3.	100000.00 M	1000000.00 M	
For display output			1.00-03 HZ	1.00-03 HZ	
$f = .001 \text{ Hz}$	C	$\rho_a = 127.3187294 \text{ ohm-m}$	127.32 00 OHM	7.85-03 MHO	
	X↔T	$\phi = 51.17599521 \text{ deg}$	51.2 DEG	51.2 DEG	
$f = .00215 \text{ Hz}$	C	$\rho_a = 142.0727971 \text{ ohm-m}$	2.15-03 HZ	2.15-03 HZ	
	X↔T	$\phi = 53.57424851 \text{ deg}$	142.12 00 OHM	7.04-03 MHO	
$f = .00464 \text{ Hz}$	C	$\rho_a = 166.1621533 \text{ ohm-m}$	53.6 DEG	53.6 DEG	
	X↔T	$\phi = 56.65565392 \text{ deg}$	4.64-03 HZ	4.64-03 HZ	
$f = .01 \text{ Hz}$	C	$\rho_a = 206.4591395 \text{ ohm-m}$	166.18 00 OHM	6.02-03 MHO	
	X↔T	$\phi = 60.37161281 \text{ deg}$	56.7 DEG	56.7 DEG	
etc....			10.00-03 HZ	10.00-03 HZ	
			206.46 00 OHM	4.84-03 MHO	
			60.4 DEG	60.4 DEG	
For printed output			21.54-03 HZ	21.54-03 HZ	
3 (points/decade) Sto 35		3.	276.22 00 OHM	3.62-03 MHO	
$f_{min} = .001 \text{ Hz}$	X↔T		64.5 DEG	64.5 DEG	
$f_{max} = 1 \text{ Hz}$	E	(Printed output as shown)	46.42-03 HZ	46.42-03 HZ	
			401.23 00 OHM	2.49-03 MHO	
			68.8 DEG	68.8 DEG	
* Note any value of h_3 may be supplied at this step, since the program doesn't actually use the input h value for the bottom half-space.			100.00-03 HZ	100.00-03 HZ	
			632.46 00 OHM	1.58-03 MHO	
			72.7 DEG	72.7 DEG	
† The correct unit is "ohm-m", of course, rather than the abbreviation "ohm" seen on print-out tapes. Similarly, for conductivity calculations, the tag says "MHO" to indicate "mho/m".			215.44-03 HZ	215.44-03 HZ	
			1.07 03 OHM	933.55-06 MHO	
			75.7 DEG	75.7 DEG	
			464.16-03 HZ	464.16-03 HZ	
			1.92 03 OHM	522.12-06 MHO	
			77.3 DEG	77.3 DEG	
++ Similar print-out for conductivity calculations, same problem, is given at right.			1.00 00 HZ	1.00 00 HZ	
			3.52 03 OHM	283.86-06 MHO	
			76.8 DEG	76.8 DEG	

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