GROUND-WATER QUALITY IN NORTH IDAHO

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CECIL D. ANDRUS, Secretary

GEOLOGICAL SURVEY

H. William Menard, Director

Water-Resources Investigations/Open-File Report 80-596

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CONVERSION FACTORS

For the convenience of those who prefer SI (International System of Units) rather than the inch-pound system of units, conversion factors for terms used in this report are listed below.

Multiply inch-pound unit	<u>By</u>	To obtain SI unit
	Length	
<pre>inch (in.) foot (ft) mile (m1)</pre>	25.4 0.3048 1.609	millimeter meter kilometer
	<u>Area</u>	
acre acre-foot (acre-ft) square mile (mi²)	4047 1233 2.590	square meter cubic meter square kilometer
	Flow	
gallon per minute (gal/min)	0.06309	liter per second
	Mass Per Unit Volume	
ton per acre-foot (ton/acre-ft)	0.8236	kilogram per cubic meter
	Temperature	
degrees Fahrenheit (°F)	5/9 (°F - 32)	degrees Celsius (°C)

Concentrations of chemical constituents are given in mg/L (milligrams per liter) or $\mu g/L$ (micrograms per liter). (One milligram equals 1,000 micrograms.) These values, within the range of values presented, are numerically equal to values expressed in parts per million and parts per billion, respectively. Specific conductance is expressed as $\mu mhos/cm$ (micromhos per centimeter at 25 degrees Celsius). SAR (sodium-adsorption-ratio) values, calculated from ion concentrations and expressed in meq/L (milliequivalents per liter), are determined by dividing the milligrams per-liter concentration of a constituent by the atomic weight of the constituent.

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ABSTRACT

From July 1977 to May 1978, water samples were collected from 116 wells north of the Palouse River in Idaho to define water-quality conditions, on a reconnaissance level, in major aquifers. Geologic and hydrologic data were combined with water-quality data to develop an understanding of factors affecting present and future ground-water quality.

Samples were analyzed for 16 major chemical constituents, selected metallic trace elements, pH, specific conductance, water temperature, and total—and fecal—coliform bacteria. Locally, concentrations of dissolved solids, nitrite plus nitrate, iron, and cadmium exceeded mandatory or recommended limits established for public water supplies. Hardness exceeding 300 milligrams per liter may restrict ground—water use esthetically or economically. Ground—water quality is adequate and quantity is sufficient to meet population and economic demands as of 1978.

INTRODUCTION

Use of ground water in Idaho north of the Palouse River (see fig. 1 for map of study area) is increasing rapidly as available surface-water supplies become appropriated. Aquifers (water-yielding formations) are an important source of water for municipal and rural domestic use, irrigation, and manufacturing processes. The increasing use of ground water may affect the quantity and quality of water available for further development.

An understanding of the factors affecting ground-water quality is needed to evaluate effects of development. Prior to this study, little information was available regarding quality of water in major aquifers in north Idaho. Previous reports (most recently, Eisenbarth, 1978) provide some local ground-water quality data, but information was insufficient to adequately define overall current (1978) conditions.

This study was made by the U.S. Geological Survey, in cooperation with the Idaho Department of Water Resources. Similar studies are planned, specifically to obtain groundwater quality data in areas where land and water-resource development are expected or increasing.

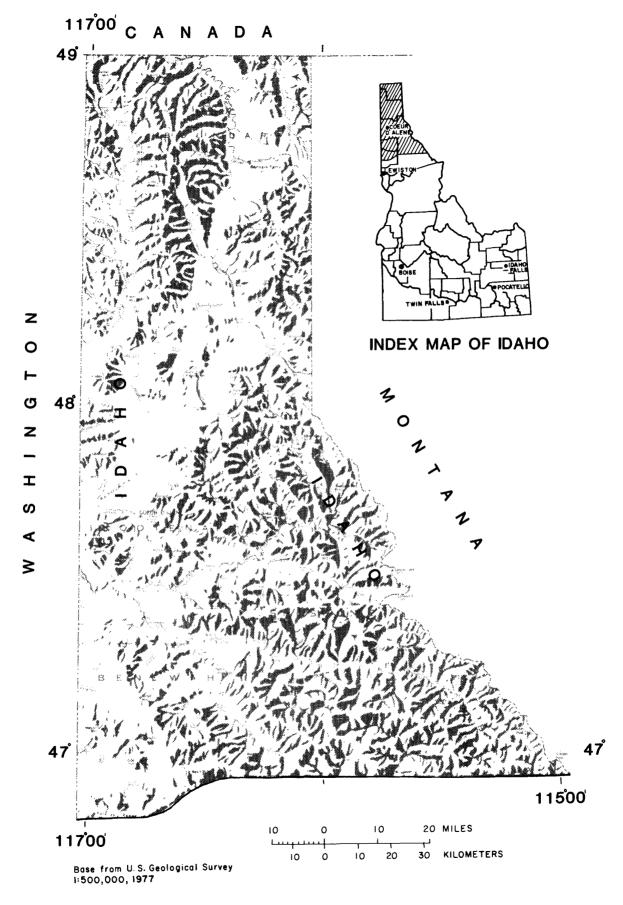


Figure 1.--Shaded relief map of study area.

The authors gratefully acknowledge the many well owners, municipal officials, and private industries who provided well information and allowed collection of water samples on their property.

Purposes

The major purposes of this report are to: (1) Provide water-quality data representative of the water in different aquifers in the study area, and (2) relate these data to natural and manmade influences. Another purpose is to provide a basis for comparing changes in ground-water quality. Understanding the cause-and-effect relations that affect water quality will aid in planning and managing land and water-resource development.

Well-Numbering System

The well-numbering system (fig. 2) used by the U.S. Geological Survey in Idaho indicates the location of wells within the official rectangular subdivision of the public lands, with reference to the Boise base line and meridian. The first two segments of the number designate the township and range. The third segment gives the section number, followed by three letters and a numeral, which indicate the 1/2 section (160-acre tract), the $\frac{1}{4}-\frac{1}{4}$ section (40-acre tract), the $\frac{1}{4}-\frac{1}{4}-\frac{1}{4}$ section (10-acre tract), and the serial number of the well within the tract, respectively. Quarter sections are lettered A, B, C, and D in counterclockwise order from the northeast quarter of each section. Within the quarter sections, 40-acre and 10-acre tracts are lettered in the same manner. Well 56N-2W-10CAB1 is in the NW4NE4SW4 sec. 10, T. 56 N., R. 2 W., and is the first well inventoried in that tract.

DESCRIPTION OF STUDY AREA

North Idaho, as described in this report, comprises Benewah, Bonner, Boundary, Kootenai, and Shoshone Counties, and part of Latah County. The total area is about 8,000 mi², including about 250 mi² of water surface. Topography is dominated by glacially scoured valleys and rugged northwest-trending mountain chains. Major hydrologic features include the Priest, Pend Oreille, Coeur d'Alene, St. Joe, and St. Maries River drainage basins; parts of the Kootenai, Spokane, and Palouse River drainage basins; and several large lakes, including Priest, Pend Oreille, and Coeur d'Alene Lakes (pl. 1).

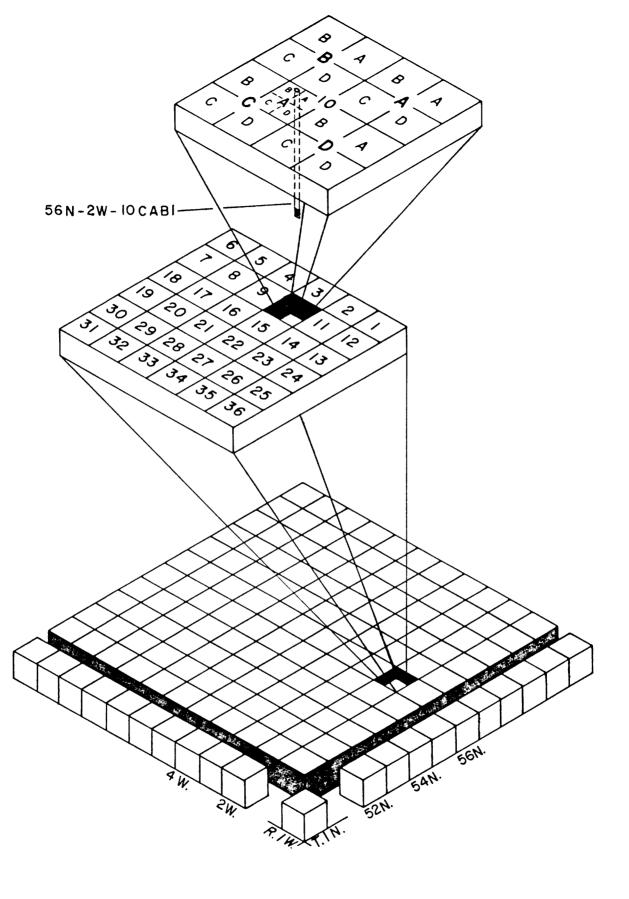


Figure 2.--Well-numbering system.

Population, based on census estimates (Idaho Department of Water Resources and Boise State University, 1978), was 90,450 in 1975. About one-half of the population lives in rural areas or small towns of 1,200 or fewer inhabitants.

The economy of north Idaho is based largely on wood-products industries, local wholesale-retail trade, and State and local government. Six percent of the land is used for agriculture. Mining is locally important, especially along the South Fork Coeur d'Alene River.

Increases in urban population and industrial development are predicted, particularly in the Coeur d'Alene and Sandpoint areas. These increases, together with probable increases in farmland irrigated by ground water, are expected to affect the ground-water resources of north Idaho, both in quality and quantity.

Generalized Geology

Geologic formations ranging in age from Precambrian to Quaternary occur in north Idaho (Bond, 1978). The formations are grouped, for hydrologic purposes, into four major units: (1) Cambrian and Precambrian, (2) Tertiary and Cretaceous, (3) Tertiary, and (4) Quaternary. Generalized geology of north Idaho and correlation, description, and water-yielding characteristics of geologic units are shown on plate 2.

Rocks of Precambrian age consist of metamorphosed sediments and igneous intrusives. The metamorphic rocks are folded, faulted, and uplifted and constitute one of the major rock types in the mountainous areas of north Idaho. Rocks of Cambrian age consist of limestone and claystone, which crop out in the mountains along the east side of Pend Oreille Lake and in areas north and east of Bayview. Together, the undifferentiated sedimentary, igneous, and metamorphic rocks compose the basement complex in north Idaho.

Granitic rocks of Tertiary and Cretaceous age, principally associated with the Idaho batholith, occur north and west of Pend Oreille Lake. Many fault-related mineral and ore deposits of economic importance occur in these rocks.

Rocks of Tertiary age, consisting of basalt flows and interbedded sediments of the Columbia River Basalt Group, crop out in the St. Joe, St. Maries, and Coeur d'Alene River valleys and around Coeur d'Alene Lake. These rocks are mantled by loess (windblown silt) of Quaternary age in western Latah, Benewah, and Kootenai Counties.

Alluvium, colluvium, and glacial deposits of Quaternary age are the predominant valley fill throughout north Idaho. Alluvium and colluvium, hereafter referred to as alluvium, include unconsolidated to well-consolidated beds of poorly sorted to well-sorted stream and lake deposits. Most of the valley fill, however, is of glacial origin.

Glacial deposits include unconsolidated to well-consolidated, poorly sorted to well-sorted beds. They are mineralogically similar and are difficult to distinguish from alluvium. Surficial distinctions between alluvial and glacial deposits in this report are based solely on the State Geologic Map (Bond, 1978). These deposits are hydrologically significant because: (1) A majority of the population centers are located on or near them; and (2) future agricultural, industrial, and urban development will directly affect the quality of water in them.

Hydrology

Hydrologic, geologic, and well-construction data were collected for 116 wells in the study area during the period May 1977 to May 1978 (table 1). Hydrologic data included onsite water-level measurement, discharge estimation, and well-use information. Hydrologic data from well drillers' logs included pump-test information where available. Geologic data from drillers' logs included lithologic description and thickness of geologic units penetrated. Well-construction information from drillers' logs included diameter of borehole, diameter and depth of well casing(s), type and depth of surface seal, and manner of well completion, such as screen or open hole.

Aquifer Recharge and Ground-Water Movement

Aquifers in the study area are recharged largely by infiltration of precipitation, seepage from rivers and tributary streams, and leakage from large lakes. For example, aquifers that underlie Rathdrum Prairie are recharged by precipitation, seepage from streams, and leakage from Pend Oreille, Coeur d'Alene, Hayden, Twin, and Spirit Lakes. Basalt aquifers of the Coeur d'Alene Lake valley are mainly recharged by leakage from Coeur d'Alene Lake and percolation of precipitation through overlying loess deposits.

The altitude of the water table is depicted in figure 3 on the basis of water-level measurements in wells (table 1). Ground water moves approximately at right angles to

Table 1. Well data

 $\frac{\text{Aquifer(s)}\colon}{\text{Qgl - Glacial deposits}} : \quad \text{Qal - Alluvium and colluvium}$

map

Altitude: From U.S. Geological Survey quadrangle

Tcr - Columbia River Basalt Group TKi - Granitic rocks, undifferentiated

Ep6 - Sedimentary, igneous, and meta-morphic rocks, undifferentiated

 $\frac{\text{Well finish};}{\text{P - Perforated casing}} \cdot \frac{\text{O - Open end}}{\text{P - Perforated casing}}$

Notations: > - Greater than

< - Less than
-- No data available</pre>

E - Estimated

S - Screen X - Open hole

Water level: F - Flowing

Use of water: C - Commercial H - Domestic I - Irrigation N - Industrial

P - Public supply

				C	asing						
		Altitude of land surface (ft,	Reported depth		Depth to first perforation		Water	level			
Well number	Aquifer(s)	National Geodetic Vertical Datum of 1929)	of well (ft below land surface)	Diameter (in.)	or bottom of casing (ft below land surface)	Well finish	Depth (ft below land surface)	Date measured	Reported discharge (gal/min)	Use of water	Date of well completion
					BENEWAH COUN	TY					
44N-2W-33BAA1	Qa1	2,830	76	6	62	P	15.0	9- 3-75	< 5	Н	1975
44N-5W-11CCC1	Ter	2,560	190	6	92	X	F	5-18-78	E15	H	1974
46N-2W-16BBD1	Ter	2,200	80	6	79	X	41.65	5-16-78	E15	Н	1975
46N-2W-20BDA1	Qg1	2,210	125	6	108	X	66.87	5-16-78	> 5	H	1973
46N-2W-36DDA1	Ter	2,320	214	6	93	X	63.61	5-16-78	E10	Н	1958
46N-4W-7CDB1	Ter	1,610	100	10	66.5	X	28.40	5-16-78	E15	Н	1974
46N-4W-11ACC1		2,800	600	6	56	X	51.65	5-16-78	E10	Н	1974
40N-4W-IIACCI	€р€	2,800	000	Ü			32.03				
					BONNER COU	NTY					
54N-2W-19CBA1	Qg1	2,440	125	6	121	X	98.74	7-28-77	E10	H	1975
54N-3W-25BCB1	TKi	2,360	375	6	70	X	149.29	8-10-77	E20	Н	1971
54N-3W-27DDC1	Qg1	2,240	90	8	79	S	69.95	8-18-77	E20	P	1967
54N-4W-17CAD1	Qg1	2,312	195	6	187	P	166.50	8-11-77	E10	H	1971
54N-4W-19BCD1	Qg1	2,300	200	6	200	0	142.13	7-19-77	E20	H	1975
J4N-4W-19DOD1	481	2,500	200	ű							
54N-4W-31DDD1	Qg1	2,565	538	6	538	0	515.00	7- 1 - 76	> 20	Н	1976
54N-5W-18AAA1	Qg1	2,280	146	8	138	P	109.60	8-23-77	> 25	H	1973
54N-5W-30ABD1	€p€(?)	2,415	252	6	77	х	124.49	8- 9-77	E5	H	1973
54N-5W-36AAD1	TK1	2,360	325	6	115	X	276.34	8- 8-77	E25	H	1972
55N-3E-19CAD1	Qg1	2,160	110	6	106	P	93.86	11-15-77	< 15	H	1974
55W 2E 202021	0-1	2 200	239	6	239	0	213.55	11-15-77	< 15	Н	1967
55N-3E-29DDD1	Qg1	2,280 2,280	189	14	138	P	130.05	8-23-77	>60	I	1967
55N-5W-19CBD1	Qa1		210	6	207	X	174.24	8-11-77	6.0	Н	
55N-6W-1DDD1	Qg1	2,360	75	6	70	P	60.55	11-16-77	< 15	Н	1971
56N-2E-6CCC1	Qg1	2,160 2,160	75 70	6	65	P	33.82	11-16-77	<15	H	1969
56N-2E-19ADD1	Qg1	2,100	70	U							1070
56N-1W-10CCD1	Qg1	2,280	73	6	32	X	21.80	12- 1-77	< 15	Н	1970
56N-2W-10CAB1	TKi	2,200	50	6	45	P	49.07	11-30-77	E15	Н	1973
56N-2W-15CCB1	Qg1	2,180	182	6	182	0	28.17	12- 1-77	E15	H	1971
56N-3W-4AAA1	TK1	2,086	162	6	142	P	F	11-29-77	E15	H	1975
56N-3W-4ADB1	Qg1	2,120	53	6	47	P	12.96	11-30-77	E15	H	1972

Act Color					Ca	asing						
Disput			of land surface			to first		Water	level			
S68-B-9-7ABA Gal 2,149 80 6 59 P 48,15 11-20-77 E15 H 1932 1568-B-9-7ABA Gal 2,240 67 6 67 P 48.74 B-23-77 20 H 1946 1958-B-9-7ABA Gal 2,120 54 6 650 P 27.30 11-17-77 15 H 1996 1975-B-18-1384 Gal 2,120 54 6 50 P 27.30 11-17-77 15 H 1973 1978-B-18-1384 Gal 2,120 175 6 50 P 27.30 11-17-77 15 H 1973 1978-B-18-1384 Gal 2,140 118 6 111 X F 11-29-77 E15 H 1995 1978-B-18-1384 Gal 2,140 118 6 111 X F 11-29-77 E15 H 1995 1978-B-18-1384 Gal 2,140 118 6 111 X F 115-29-77 E15 H 1995 1978-B-14-1384 Gal 2,140 118 6 170 X 170	Well number	Aquifer(s)	Geodetic Vertical Datum of	(ft below land		of casing (ft below land		below land		discharge	of	of well
Sob-19-27AAB1		····			BONT	NER COUNTY (CO	NTINUED)					
586-9-7-7AAB.	56N-3W-30BAC1	Qa1	2,149	80	6	59	P	48.35	11-30-77	E15	н	1972
5781—18-218481			2,260		6	226	P	202.57	8-23-77	20	H	1961
\$7878-1808.1 Qg1 2,132 28 24 18 P 8.4.5 11-29-77 E15 H 1973 \$7878-1808.1 Qg1 2,140 175 6 21 X 47.13 11-29-77 E15 H 1973 \$7878-1808.1 Qg1 2,140 175 6 21 X F P 11-13-29-77 E15 H 1975 \$7878-1808.1 T4 2,140 175 6 111 X F P 11-13-29-77 E15 H 1975 \$7878-1808.1 Qg1 2,280 105 6 70 P 115.01 8-24-77 E15 H 1975 \$7878-1400.1 Qg1 2,380 178 6 87 P 115.01 8-24-77 E15 H 1975 \$7878-1400.1 Qg1 2,280 178 6 87 P 115.01 8-24-77 E15 H 1975 \$788-11-240.1 Qg1 2,280 178 6 87 P 115.01 8-24-77 E15 H 1970 \$588-11-240.1 Qg1 2,280 178 8 15 F 7 1.40 11-17-77 e15 H 1970 \$588-11-240.1 Qg1 2,280 178 8 15 F 7 1.40 11-17-77 e15 H 1970 \$588-11-240.1 Qg1 2,460 16 6 5 S X 11-18-27 e15 H 1975 \$608-38-240.1 Qg1 2,460 10 6 6 70 0 F 20.78 8-25-77 E15 H 1975 \$608-38-240.1 Qg1 2,460 10 6 6 70 0 F 20.78 8-25-77 E15 H 1975 \$608-38-240.1 Qg1 2,460 10 6 6 70 0 F 20.78 8-25-77 E15 H 1976 \$618-18-240.1 Qg1 2,460 10 6 6 5 5 F 14 11-19-77 E15 H 1976 \$618-18-240.1 Qg1 2,460 10 6 6 5 5 F 14 11-19-78 E15 H 1976 \$618-18-240.1 Qg1 2,460 10 6 6 5 5 F 14 11-19-78 E15 H 1973 \$628-22-104.1 Qg1 2,250 20 6 85 F 2 34.58 1-19-78 E15 H 1973 \$628-22-104.1 Qg1 2,250 20 6 85 F 2 34.58 1-19-78 E15 H 1973 \$628-22-104.1 Qg1 2,250 20 6 85 F 2 34.58 1-19-78 E15 H 1973 \$638-18-240.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E15 H 1973 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 30 F 2.28 1 1-18-78 E10 H 1975 \$638-18-340.1 Qg1 1,785 45 6 6 30 F 2.28 1 1-18-78 E10 H 1976 \$638-18-340.1 Qg1 1,785 45 6 6 30 F 2.28 1 1-18-78 E10 H 1976 \$638-18-340.1 Qg1 1,785 45 6 6 30 F 2.28 1 1 1-1												
S78-24-16ACC2												
578-A-1-68AA1			-									
578-SP-19CAD1												
578-9-1-40CC1												
S8H-IN-2AMCH Qs1 2,200 105 6 76 P 34.41 11-17-77 <15 H 1970												
1881-14-30A818 6pc 2,200 151 6 65 X 16.29 11-18-77 15 H 1975	58N-1W-2ADC1											
1881-14-30A818 6pc 2,200 151 6 65 X 16.29 11-18-77 15 H 1975	FON 111 O/ADDI	0.1	2 222			1.0	_	7 40		.15		1074
60N-44-31CBD1 Qg1 2,540 46 6 42 P 44.26 8-25-77 ED0 H 1962 60N-34-24A6C1 Qg1 2,440 70 6 70 0 F 44.26 8-25-77 60 P 1963 61N-44-16BCA1 Qg1 2,460 40 6 40 0 23.78 8-25-77 ED5 H 1963 61N-44-16BCA1 Qg1 2,460 40 6 40 0 23.78 8-25-77 ED5 H 1963 61N-44-16BCA1 Qg1 1,465 118 8 113 P 40.04 1-16-78 ED5 H 1960 61N-14-34A0B1 Qg1 1,485 118 8 113 P 40.04 1-16-78 ED5 H 1970 61N-14-34A0B1 Qg1 1,245 118 8 113 P 40.04 1-16-78 ED5 H 1973 62N-2E-70A01 Qg1 2,250 200 6 85 P 34.58 1-18-78 ED0 H 1973 62N-2E-70A01 Qg1 2,250 270 6 190 X 115.96 1-19-78 ED5 H 1973 62N-2E-2GCC1 Qg1 2,250 270 6 190 X 115.96 1-19-78 ED5 H 1973 62N-2E-2GCC1 Qg1 1,780 60 6 6 60 0 27.20 1-18-78 ED5 H 1973 65N-14-24A0B1 Qg1 2,250 260 6 257 X 100.00 7-25-75 ED0 H 1975 65N-14-34A0D1 Qg1 1,785 45 6 30 P 22.81 1-18-78 ED0 H 1975 65N-14-34A0D1 Qg1 1,785 45 6 30 P 22.81 1-18-78 ED0 H 1975 65N-14-34A0D1 Qg1 2,740 102 6 98 P 58.80 1-17-78 ED0 H 1975 65N-14-34A0D1 Qg1 2,740 102 6 98 P 58.80 1-17-78 ED0 H 1975 65N-3A-1-BADA1 Qg1 2,146 153 8 0 17.8 ED0 H 1976 65N-14-34A0D1 Qg1 2,146 153 8 0 17.8 ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.8 ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.8 ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.8 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,146 153 8 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,140 10 6 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,120 110 6 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,120 110 6 0 17.9 R ED0 H 1976 50N-3A-BADA1 Qg1 2,120 110 6 0 17.9 R ED0 H 1977 50N-3A-BADA1 Qg1 2,258 305 6 292 P 24.7 P 27.7 P 20												
60N-SH-24ABC1 Qg1 2,460 40 6 40 0 23.78 8-25-77 60 P 1963												
BOUNDARY COUNTY							0	F				
CON-1W-34ADB1 OR1	61N-4W-16BCA1	Qg1	2,460	40	6	40	0	23.78	8-25-77	E15	H	1967
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Can-ze-29CDC1												
63N-IR-4AABI QE	62N-2E-1/BCC1	QgI	2,250	270	6	190	Х	1.15.96	1-19-78	E15	Н	19/3
63N-1R-4AAB1 Qg1 2,210 260 6 257 X 100.00 7-25-75 E10 H 1975 63N-1R-4CACI Qg1 1,785 45 6 30 P 22.81 1-18-78 E20 H 1962 65N-2R-26BCD1 Qg1 2,740 102 6 98 P 58.80 1-17-78 E10 H 1971 65N-1W-3AADD1 Qg1 1,750 172 6 133 S 10.43 1-17-78 E10 H 1971 65N-1W-3ADD1 Qg1 1,750 172 6 133 S 10.43 1-17-78 E10 H 1971 65N-1W-3ADD1 Qg1 1,750 172 6 133 S 10.43 1-17-78 E10 P 1972 49N-1W-15DAC1 CPC 2,160 125 6 80 X 26.12 3-2-78 E10 P 1972 49N-1W-15DAC1 CPC 2,300 150 6 73 X 13.37 3-1-78 E10 H 1968 49N-1W-2DDC1 Qg1 2,200 135 6 116 P 22.70 3-2-78 E20 P 1975 50N-4W-5DDA1 Qg1 2,146 153 8 0 127.80 8-3-77 >5 H 1950 50N-5W-1AAD1 Qg1(?) 2,193 <230 30 199.04 8-17-77 700 P 1976 50N-5W-1AAD1 Qg1(?) 2,193 <230 30 199.04 8-17-77 700 P 1976 50N-5W-1ADD1 Qg1 2,112 152 26 125 P 140.99 7-21-77 >3,000 I 1957 50N-5W-ADD1 Qg1 2,112 152 26 125 P 140.99 7-21-77 >3,000 I 1957 50N-5W-ADD1 Qg1 2,120 110 6 0 91.72 8 1-77 E10 H 1969 51N-3W-19Bal Qg1 2,244 277 18 249 P 245.51 7-12-77 >1,000 I 1965 51N-4W-15DAB1 Qg1 2,244 277 18 249 P 245.51 7-12-77 >1,000 I 1965 51N-4W-15DAB1 Qg1 2,300 348 10 328 S 301.55 7-13-77 >100 P 1968 51N-4W-15DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-15DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-15DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 51N-4W-25DAB1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1968 51N-4W-25DAB1 Qg1 2,258 306 E20 220 P 267.93 7-27-77 E20 H 1968 51N-4W-25DAB1 Qg1 2,250 248 6 20 237 P 237.69 7-12-77 > 100 P 1971 1968 51N-5W-12BAB1 Qg1 2,207 264 16 244 S 217.13 7-13-77 > 100	62N-2E-29CDC1	Qg1	1,780	60	6	60	0	27.20	1-18-78	E10	н	1967
65N-2E-26BCD1 Qg1 2,740 102 6 98 P 58.80 1-17-78 E10 H 1971 65N-1W-34ADD1 Qg1 1,750 172 6 133 S 10.43 1-17-78 E10 H 1972 **ROOTENAL COUNTY** **ROOTENAL		Qg1										
Continue												
## A8N-IW-18BBB1 CPC 2,160 125 6 80 X 26.12 3-2-78 E10 P 1972 ## A9N-IW-15DAC1 CPC 2,300 150 6 73 X 13.37 3-1-78 E10 H 1968 ## A9N-IW-12DDC1 Qa1 2,200 135 6 116 P 22.70 3-2-78 E20 P 1975 ## SON-AW-5DDA1 Qg1 2,146 153 8 0 127.80 8-3-77 >5 H 1950 ## SON-SW-1AAD1 Qg1(?) 2,193 <230 30 199.04 8-17-77 700 P 1976 ## SON-SW-1CBB1 Qg1 2,194 275 16 235 S 195.85 7-20-77 1,400 P 1974 ## SON-SW-6DC1 Qg1 2,112 152 26 125 P 140.99 7-21-77 >3,000 I 1957 ## SON-SW-7ADD1 Qg1 2,120 110 6 0 91.72 8-1-77 E10 H 1969 ## SIN-3W-19BAB1 Qg1 2,293 221 6 220 X 162.70 7-28-77 E10 H 1976 ## SIN-4W-6ADA1 Qg1 2,244 277 18 249 P 245.51 7-12-77 >1,000 I 1965 ## SIN-4W-15ABA1 Qg1 2,300 348 10 328 S 301.55 7-13-77 >100 P 1968 ## SIN-4W-15ABA1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 ## SIN-4W-15ABA1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 ## SIN-4W-15ABA1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 ## SIN-4W-15ABA1 Qg1 2,258 305 6 292 P 267.93 7-27-77 E20 H 1967 ## SIN-4W-15ABA1 Qg1 2,258 305 8 307 P 257.22 7-21-77 >1,000 I 1968 ## SIN-4W-2DBB1 Qg1 2,258 330 8 307 P 257.22 7-21-77 >1,000 I 1963 ## SIN-4W-2DBB1 Qg1 2,250 217 6 210 P 186.41 7-26-77 E20 H 1967 ## SIN-4W-2DBB1 Qg1 2,276 330 8 307 P 267.14 7-12-77 >500 I 1966 ## SIN-4W-2DBB1 Qg1 2,276 330 8 307 P 267.14 7-12-77 >500 I 1965 ## SIN-4W-2DBB1 Qg1 2,276 330 8 307 P 266.73 7-28-77 >500 I 1966 ## SIN-4W-2DBB1 Qg1 2,276 330 8 307 P 266.73 7-26-77 >500 I 1966 ## SIN-5W-12DB1 Qg1 2,274 310 18 255 P 266.73 7-26-77 >500 I 1966												
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51N-5W-19CAD1 Qg1 2,129 208 12 188 S 149.90 7-21-77 >500 P 1967		Qg1	2,207									

				С	asing						
		Altitude of land surface (ft,	Reported depth		Depth to first perforation		Water	level			
Well number	Aquifer(s)	National Geodetic Vertical Datum of 1929)	of well (ft below land surface)	Diameter (in.)	or bottom of casing (ft below land surface)	Well finish	Depth (ft below land surface)	Date measured	Reported discharge (gal/min)	Use of water	Date of well completion
				KOOT	ENAI COUNTY (C	ONTINUED)					
51N-5W-26BCA1	Qg1	2,241	274	30	242	P	254.34	7-20-77	> 1,000	I	1963
51N-5W-27BBB1	Qg1	2,143	184	6	184	X	157.86	7-21-77	E10	H	1969
51N-5W-31ACA1	Qg1	2,105	189	16	167	S	129.95	7-21-77	> 1,500	I	1975
51N-5W-35BDC1	Qg1	2,206	242	20	212	P	218.41	7-20-77	> 1,000	I	1965
52N-3W-7DAC1	Qg1	2,300	117	8	95	P	92.20	8- 4-77	> 5	Н	1975
52N-3W-7DCA1	Qg1	2,308	270	12	106	P	95.86	8- 2-77	> 200	N	1969
52N-3W-19AAB1	Qg1	2,360	310	6	245	S	193.34	8- 2-77	E5	Н	1972
52N-4W-10DBA1	TKi	2,305	432	6	280	X	327.22	8- 2-77	E2	Н	1969
52N-4W-14DCD1	Qg1	2,305	365	6		P	217.26	8- 2-77	E10	Н	1974
52N-4W-17DDD1	Qg1	2,298	350	8	331	P	272.09	8- 9-77	150	P	1974
52N-4W-20CCB1	Qgl & TKi	2,266	500	8	225	P	219.32	7-14-77	<15	Н	1973
52N-4W-27DCD1	Qg1	2,260	306	8	265	P	258.22	7-14-77	>20	P	1970
52N-4W-31DAB1	Qg1	2,197	220	8	210	S	198.04	7-13-77	E30	P	1970
52N-4W-32ABC1	Qg1	2,217	234	30	204	P	216.64	7-13-77	>1,000	I	1964
52N-4W-35DCB1	Qg1(?)	2,310					320.68	7-12-77	>1,000	I	
53N-2W-7CAA1	Qg1	2,432	404	6	404	0	381.37	7-19-77	E10	Н	1974
53N-2W-19ADD1	TKi	2,520	401	6	126	Х	127.78	7-19-77	>8	H	1970
53N-3W-3BAB1	Qg1	2,400	369	8	369	0	351.46	7-19-77	>5	К	1976
53N-3W-9CDD1 53N-3W-21CDC1	Qgl TKi & Qgl	2,384 2,369	357 198	6 8	 156	P P	336.96 156.98	8- 2-77 7-27-77	70 E20	P H	 1971
53N-3W-22DAB1	TKi	2,424	410	8		х	191.50	7-14-77	>20	н	1966
53N-4W-6DDB2	Qg1	2,424	328	8			302.10	7-19-77	>500	P	1963
53N-4W-22CDD1	Qg1 Qg1	2,434	441	6			427.23	8- 2-77	E10	H	1970
53N-4W-24BBA1	Qg1	2,487	485	25	449	P	468.05	8- 2-77	>500	I	pre-1929
53N-4W-33CBB1	Qg1(3)	2,422					415.05	7-28-77	E20	H	1972
53N-4W-36BBA1	Qg1	2,419	426	6	421	S	403.26	7-27-77	E20	Н	1970
54N-2W-34CCB1	Qg1	2,180	144	6	144	0	131.32	8-22-77	>5	Н	1964
					LATAH COUNT	Y					
41N-3W-3BCB1	$\epsilon_{ m p}\epsilon$	2,640	98	8	71	X	15.71	5-17-78	E10	Н	1971
41N-3W-9BBD1	€p€	2,600	170	8			67.82	5-17-78	E10	P	1971
41N-4W-6BAC1	Tcr	2,620	51	8	180.5	Х	148.79	5-18-78	E20	P	1971
41N-4W-9BAD1	Tcr	2,520	261	6	257	X	27.00	10-16-62	E10	H	1962
41N-5W-3DBC1	Ter	2,520	41	8	34	Х	21.97	5-18-78	E10	Н	1972
					SHOSHONE COU	NTY					
48N-2E-3ABC1	$\epsilon_{ m p}\epsilon$	2,060	200	6	35	Х	14.21	2-28-78	E10	P	1974
48N-2E-5BDA1	Qa1	2,230	95	8	85	P	0.0	2-28-78	E20	С	1975
48N-3E-6ADA1	€p€ & Qal	2,300	152	8	57	P	40.00	5-21-75	E10	P	1975
48N-3E-11DDD1	Qg1 & €p€	2,450	75	6	30	P	11.16	2-28-78	E10	H	1973
48N-5E-36BBB1	Qg1(?)	3,460					8.98	3- 2-78	E5	I	
49N-1E-34BCD1	Qa1	2,140	83	12	30	S	10.00	8- 5-71	E200	P H	1971
49N-2E-8CAA1	€р€	2,330	197	6	12	X	56.30	3- 1-78	E10	п	1967

the contours, from areas of recharge in the mountains to areas of discharge in the valley lowlands. Arrows in figure 3 indicate direction of ground-water movement only in the water-table aquifers. Where data are sparse, direction of flow arrows are based on topography, geology, and hydrography. In figure 3, a water level is shown for each well measured, except for those completed in the water-table aquifer underlying Rathdrum Prairie, where water-table contours indicate the water level in wells.

Yields From Wells

Yields from wells completed in alluvium range generally from 5 to 200 gal/min (table 1). Wells completed in thick (more than 400 ft) glacial deposits underlying the Rathdrum Prairie have yields ranging from 5 to as much as 3,000 gal/min. In relatively thin (less than 200 ft) glacial deposits in mountain valleys, however, yields from wells range generally from 1 to 60 gal/min. Percolation rates and ground-water movement through alluvial and glacial deposits vary with particle size and sorting, degree of compaction of deposits, and clay-lens interbedding. Yields from wells completed in these aquifers are generally adequate for most uses.

Yields from wells completed in basalt, granite, or the basement complex range generally from 2 to 25 gal/min and average 13 gal/min. Fractures, joints, deeply weathered sections, and permeable sedimentary interbeds locally increase the ability of these rocks to transmit water. Percolation rates and ground-water movement are relatively slow. Yields of wells completed in these aquifers are generally sufficient for domestic use only.

Wells open to more than one aquifer, such as alluvial or glacial deposits and basement complex, are relatively common; because these wells tap more than one aquifer, water-quality and well-yield information obtained are not representative of any one aquifer. Four multiaquifer wells were measured and sampled in this study. Data for these wells are included for comparative purposes only.

GROUND-WATER QUALITY Obtaining Samples for Ground-Water Quality Analyses

The most representative water samples are obtained from municipal, irrigation, and industrial wells. These wells generally are pumped frequently, thereby yielding water recently obtained from the aquifers in which they are com-

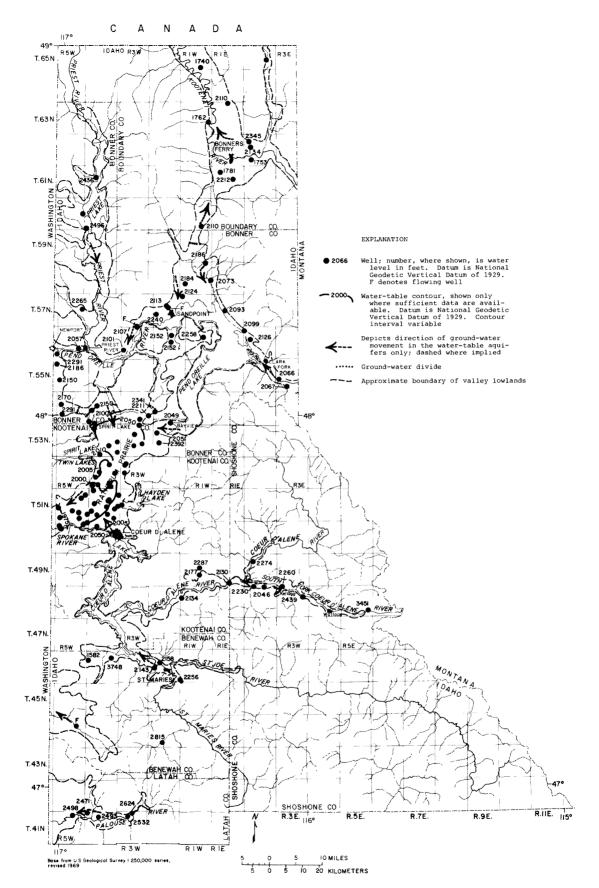


Figure 3.--Altitudes of water levels in wells and contours of the water table, summer 1977.

pleted. When obtaining water samples from domestic wells equipped with pressure systems, the wells were pumped long enough to insure that water was obtained from the aquifer without being stored in the pressure tank for a significant period of time. Also, some wells may provide nonrepresentative samples if surface seals are absent, allowing contamination from surface sources. Old well casings may be cracked or corroded, allowing surface or subsurface leakage into the well.

Certain physical properties and chemical constituents, as well as bacterial concentrations, may change with time after sample collection. Therefore, determinations of water temperature, pH, specific conductance, alkalinity (carbonate and bicarbonate), total coliform bacteria, and fecal coliform bacteria are made at the well site.

Suitability of Water For Use

Factors such as geologic environment, contact time with aquifer materials, source of recharge, and activities of man affect the physical, chemical, and bacteriological quality of water in an aquifer. Although man's activities may cause dramatic changes in water quality, the geologic environment has the greatest effect in north Idaho.

Generally, water becomes more mineralized with depth below land surface. As percolating water passes through rock or sediment, the water accumulates increasingly greater concentrations of dissolved solids as a function of contact time with, and solubility of, the rock or sediment minerals.

Bacterial concentrations usually decrease with depth, owing to the filtering effects of fine-grained sediments or organic material that build up near the source of bacterial contamination (Vecchioli and others, 1972). Water containing bacteria may enter an aquifer, however, where overlying sediments are thin or where water moves through fractured and faulted rocks, which have little filtering action.

Whatever factors determine its quality, the water's suitability for use is the important consideration. In relation to human needs, water-quality criteria (U.S. Environmental Protection Agency, hereafter referred to as EPA, 1976), designate maximum chemical concentrations, physical properties, and bacterial concentrations that, when not exceeded, will cause no harm to water users.

In contrast, water-quality regulations (EPA, 1977a and 1977b), which use criteria as a basis, describe legally established recommended (secondary) and mandatory (primary) limits for constituents and properties and bacterial con-

centrations. Local natural conditions, esthetic or economic considerations, and resource protection considerations may result in variations of regulations in different places. Also, Federal drinking-water quality regulations legally apply only to public water supplies, not to domestic, agricultural, or industrial supplies for nonpublic use. Regulation limits do, however, provide a comparative base for all water-quality discussion.

A list of constituents and properties commonly important to water users is presented in table 2. Current (1978) water-quality criteria and regulations are given where possible. Water-quality analyses for wells sampled in north Idaho in 1977 and 1978 are shown in table 3.

Hardness

Water hardness is caused principally by calcium and magnesium dissolved in water. Hardness is expressed in milligrams per liter of calcium carbonate (CaCO₃). Other ions, such as iron, strontium, and manganese, can contribute to hardness if the concentrations are exceptionally large.

Hardness is a measure of the soap-consuming potential of a water. Calcium and magnesium react with soap, forming precipitates of calcium and magnesium, or soap scum. After the reaction is complete, the remaining soap is available to produce lather. When hard water is heated and evaporated, calcium and magnesium react with bicarbonate, carbonate, sulfate, and silica to form heat-retarding, pipe-clogging scale. This scale is commonly seen as white crust inside teakettles and plumbing and as rings in bathtubs.

High concentrations of hardness generally are not a health problem but may create an economic problem. The costs of softening some natural water may be considerable before the water is suitable for domestic use, and especially for some industrial uses. Hardness in domestic water supplies probably is not objectionable at concentrations less than 100 mg/L.

Most water in north Idaho has less than 150 mg/L hardness (table 3). Geographical differences in hardness were evident; the hardest water, as much as 610 mg/L, occurred in unconsolidated deposits of the Kootenai River valley.

Hardness in ground water in north Idaho is shown in figure 4. The table in figure 4 shows the range and median concentration of hardness in water from each of the various geologic units.

Table 2. Source or cause and significance of physical properties and chemical constituents of water

Constituent or property	Source or cause	Range of concentrations in sampled wells	Significance
Silica (SiO ₂)	Dissolved from practically all rocks and soils.	8.0-52.0 mg/L SiO ₂	Together with calcium and magnesium, silica forms a low heat-conducting, hard, glassy scale in boilers and turbines. Silica inhibits deterioration of zeolite-type water softeners and corrosion of iron pipes by soft (0-75 mg/L CaCO ₃) water
Iron (Fe)	Dissolved from practically all rocks and soils. Present in some industri- al wastes. Also caused by corrosion of iron pipes, pumps, and other equip- ment.	O-13 mg/L Fe (O-13,000 μg/L) Fe	When concentrations are more than 0.1 mg/L (more than 100 μ g/L), iron commonly precipitates on exposure to air, causing turbidity, staining of plumbing fixtures and laundry, and tastes and colors that are objectionable in food, beverages, textile processes, and ice manufacture. Recommended maximum limit for public water supplies is 0.3 mg/L, or 300 μ g/L.
Sodium-adsorption- ratio ² (SAR)	Dissolved calcium, magnesium, and sodium from rocks and soils.	0.1-3.2	Estimates the degree to which sodium in irrigation water tends to enter into cation-exchange reactions in soil. High values indicate that sodium replaces adsorbed calcium and magnesium. This replacement damages soil structure and decreases permeability.
Calcium (Ca), Magnesium (Mg)	Dissolved from practically all soils and rocks, but especially from limestone, dolomite, and gypsum.	4.4-180 mg/L Ca 0.7-38 mg/L Mg	Causes most of the hardness and scale-forming properties of water; soap consuming (see hardness). Water having small amounts of calcium and magnesium is desired in electroplating, tanning, dyeing, and textile manufacturing. Small amounts are desirable to prevent corrosion.
Sodium (Na), Potassium (K)	Dissolved from practically all rocks and soils. Present in industrial wastes, sewage, and commercial fertilizers.	1.1-110 mg/L Na 0.4-10 mg/L K	More than 50 mg/L sodium and potassium in the presence of suspended matter causes foam in boilers, which accelerates scale formation and corrosion.
Bicarbonate (HCO_3), Carbonate (CO_3)	Action of carbon dioxide in water on carbonate cementing material and rocks, such as limestone, dolomite, and travertine.	11-530 mg/L HCO ₃ 0 mg/L CO ₃	Produce alkalinity. When heated in the presence of calcium and magnesium, can form scales in pipes and release corrosive carbon-dioxide gas. Aid in coagulation for the removal of suspended matter from water.
Sulfate (SO ₄)	Dissolved from rocks and soils containing gypsum, sulfides, and other sulfur compounds. May be derived from industrial wastes, both liquid and atmospheric.	0.7-140 mg/L SO ₄	Sulfate in water containing calcium forms hard scale in steam boilers. In large amounts, sulfate, in combination with other ions, imparts bitter taste to water. Some calcium sulfate is considered beneficial in brewing processes. Recommended maximum limit for public water supplies is 250 mg/L.
Chloride (C1)	Dissolved from rocks and soils. Present in sewage and industrial wastes.	0.1-100 mg/L C1	A salty taste can be detected when concentrations exceed 100 mg/L. In large quantities, increases the corrosiveness of water. Present available removal methods not generally economical for most uses. Recommended maximum limit for public water supplies is 250 mg/L.
Fluoride (F)	Dissolved in small quantities from most rocks and soils. Added to many public supplies.	0.00-1.4 mg/L F	Fluoride concentrations in limited amounts have beneficial effect on the structure and resistance to decay of children's teeth. Excessive concentrations produce objectionable dental fluorosis (tooth mottling). Optimum recommended limits for public water supplies range from 0.7 to 1.2 mg/L and are based on annual average maximum daily air temperatures. ³

Table 2. Source or cause and significance of physical properties and chemical constituents of water (Continued)

Constituent or property	Source or cause	Range of concentrations in sampled wells	Significance
Nitrite (NO_2) -plus- nitrate (NO_3) as nitrogen (N)	Decaying organic matter, sewage, fertilizers, and nitrates in soils.	0.00-25 mg/L N	Small amounts help reduce cracking of high-pressure boiler steel. Encourages growth of algae and other organisms that produce undesirable taste and odors. Concentrations in excess of 10 mg/L are suspected as cause of methemoglobinemia (bluebaby disease) in infants. Mandatory maximum limit for public water supplies is 10 mg/L. ³
Dissolved solids (calculated sum)	Mineral constituents dissolved from rocks and soils.	28-773 mg/L	Recommended maximum $limit$ for public water supplies is 500 mg/L. Water containing more than 1,000 mg/L of dissolved solids is unsuitable for many purposes.
${\tt Hardness\ as\ CaCO}_3$	In most waters, nearly all hardness is due to calcium and magnesium.	14-610 mg/L	Soap consuming capacity of a water. Forms white scale on teakettles and plumbing and rings in bathtubs. Although hardness is less of a factor with synthetic detergents than with soap, it is still desirable to soften hard water for esthetic as well as economic reasons.
Specific conductance	Mineral content of water.	32-1,050 μmhos/cm	Indicator of mineral content. A measure of the capacity of the water to conduct a current of electricity, and varies with the concentration and degree of ionization of the different minerals in solution; the more minerals, the larger the specific conductance.
рН	Hydrogen-ion concentration.	рН 6 - рН 8.2	A pH of 7.0 indicates neutrality of a solution. Values higher than 7.0 denote increased alkalinity; values lower than 7.0 indicate increased acidity. Corrosiveness of water generally increases with decreasing pH, but excessively alkaline water also may be corrosive. Recommended level for public water supplies ranges from 6.5 to 8.5.
Fecal coliform bacteria	Derived from fecal matter of humans and other warm-blooded animals. Indi- cators of potential presence of patho- genic bacteria.	<1-19 col./100 mL	Indicates contamination from human or animal wastes. Mandatory maximum contaminant limits for public water supplies vary with sample method and frequency. ³

 $^{^{1}\}text{U.S.}$ Environmental Protection Agency (1977b)

²U.S. Salinity Laboratory Staff (1954) SAR = $\frac{\text{(Na+)}}{\text{(Ca}^{+2}) + (\text{Mg}^{+2})}, \text{ in meq/L}$

³U.S. Environmental Protection Agency (1977a)

Local identifier: Well number

Well yield: GAL/MIN - gallons per minute E - estimated or reported

Coliform bacteria: Cols./100 ML - Colonies per 100 milliliters K - Less than ideal colony count

Aquifer(s): Qal - Alluvium and colluvium; Qgl - Glacial deposits; TCr - Columbia River Basalt Group; TKi - Granitic rocks, undifferentiated; EpE - Sedimentary, igneous, and metamorphic rocks, undifferentiated

LOCAL IDENT- I- FIER	AQUIFER(S)	DATE OF SAMPLE	WELL YIELD (GAL/MIN)	SPE- CIFIC CON- DUCT- ANCE (MICRO- MHOS)	PH (UNITS)	WATER 1 TFMPER-(C	PER	COLI- FORM. FECAL. U.7 UM-MF (COLS./ 100 ML)	HARD- NESS+ DIS- SOLVED (MG/L AS CACO3)	HARD- NESS. NONCAR- BONATE, DIS. (MG/L CACO3)	CALCIUM DIS- SOLVED (MG/L AS CA)	MAGNE- SIUM+ DIS- SOLVED (MG/L AS MG)
											BE	NEWAH
44N 02W 33RAA 44N 05W 11CCC 46N 02W 16RBD 46N 02W 20BDA 46N 02W 36DDA 46N 04W 07CDB	Ter Ter Qgl	78-05-17 78-05-18 78-05-16 78-05-16 78-05-16	<5 E15 E15 >5 E10	133 191 290 227 313	6.9 7.7 6.9 7.0 7.6	9.5 13.0 10.5 9.5 10.0	1 <1 <1 <1 <1	<1 <1 <1 <1 <1	49 74 140 120 140	0 0 0 0	12 14 36 29 30	4.5 9.6 13 12 15
46N 04W 11ACC		78-05-16	Elo	333	7.4	10.0	<1	<i< td=""><td>150</td><td>ő</td><td>19</td><td>26</td></i<>	150	ő	19	26
											ВО	NNER
54N 02W 19CBA 54N 03W 25BCB 54N 03W 27DDC 54N 04W 17CAD 54N 04W 19BCD	l TŘi l Qgl l Qgl	77-07-28 77-08-10 77-08-10 77-08-11 77-07-19	E10 E20 E10 E10	175 246 185 245 246	7.0 7.8 7.0 7.7 7.9	8.5 11.0 13.0 9.5 11.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	92 120 83 140 120	2 0 0 4 0	29 40 25 31 34	4./ 4.1 4.9 14 9.3
54N 04W 31DDD 54N 05W 18AAA 54N 05W 30ABD 54N 05W 36AAD 55N 03E 19CAD	l Qgl l €p€(?) l TKi	77-08-23 77-08-23 77-08-09 77-08-08 77-11-15	>20 >25 E5 E25 <15	43 301 343 205 221	6.6 7.2 7.6 7.0 8.2	20.0 9.5 9.0 10.0 8.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	16 150 190 110 110	0 19 5 12 2	5.0 44 51 30 22	9.8 14 7.9
55N 03E 29DDD 55N 05W 19CBD 55N 06W 01DDD 56N 01W 10CCD 56N 02E 06CCC	l Qal l Qgl l Qgl	77-11-15 77-08-23 77-08-11 77-12-01 77-11-16	<15 >60 6 <15 <15	171 214 341 367 32	7.8 7.3 7.8 7.1 6.1	6.5 8.0 12.0 10.6 12.5	<1 <1 <1 <1 <1	<1 <1 <1 <1	90 110 180 190 14	1 0 0 0	20 32 47 61 4.5	9.8 7.4 14 9.7 .7
56N 02E 18ADD 56N 02W 10CAB 56N 02W 15CCB 56N 03W 04AAA 56N 03W 04ADB	l TKi l Qgl l TKi	77-11-16 77-11-30 77-12-01 77-11-29 77-11-30	<15 E15 E15 E15 E15 E15	639 400 212 110 174	7.2 6.9 7.0 6.3 6.6	10.5 6.0 5.0 5.5 8.4	<1 <1 K19 <1 <1	<1 <1 <1 <1 <1	360 160 98 37 77	10 0 0 0	81 44 23 8•8 18	39 13 9.9 3.7 7.7
56N 03W 30RAC 56N 05W 27AAB 56N 06W 36AAA 57N 01E 21RAB 57N 02W 01RCR	l Qal l Qgl l Qgl	77-11-30 77-08-23 77-08-23 77-11-17 77-11-29	E15 20 25 <15 E15	84 312 249 48 420	6.1 7.4 7.4 6.5 7.5	6.2 12.0 16.5 8.0 8.2	<1 <1 <1 <1 <1	<1 <1 <1 <1	28 150 130 20 220	5 0 0 1 8	7.7 41 34 6.6 64	2.1 12 11 .8 15
57N 02W 16ACC 57N 02W 16RAA 57N 02W 19CAD 57N 05W 14DCC 58N 01W 02ADC	l Qgl l TKi l Qgl	77-11-28 77-11-29 77-11-18 77-08-24 77-11-17	E15 E1 <15 E10 <15	65 107 139 163 155	6.6 6.7 7.0 6.7 6.8	7.6 8.2 10.0 10.0 7.5	<1 0 <1 <1 <1	<1 0 <1 <1 <1	26 44 53 66 69	0 0 0 0 15	6.3 12 15 18 23	2.6 3.4 3.7 5.2 2.8
58N 01W 24ADB 58N 01W 30AAB 60N 04W 31CBD 60N 05W 24ABC 61N 04W 16BCA	l €p€ l Qgl l Qgl	77-11-17 77-11-18 77-08-25 77-08-25 77-08-25	<15 <15 E10 60 E15	56 282 41 48 58	6.4 7.3 6.2 6.5 6.7	7.0 7.0 7.0 6.0 7.0	4 <1 <1 <1 <1	<1 <1 <1 <1 <1	24 150 14 16 26	0 9 0 0	7.8 38 4.4 5.0 7.5	1.0 13 .8 .9 1.7
										•		BOUNDARY
60N 01W 34ADB 61N 01E 08ABC 61N 01E 15ADD 62N 02E 07DAB 62N 02E 17BCC	l Qgl l Qgl l €p€	78-01-16 78-01-19 78-01-19 78-01-18 78-01-19	£15 £15 £10 £5 £15	426 659 1050 471 282	7.5 7.4 7.2 7.6 8.1	3.0 6.0 9.0 7.0 8.5	<1 <1 <1 <1 <1	<1 <1 <1 <1	240 360 610 170 120	7 13 170 21 0	70 84 180 54 39	17 36 38 8.3 5.5
62N 02E 29CDC 63N 01E 04AAB 63N 01W 24CAC 65N 01W 34ADD 65N 02E 26RCD	l Qgl l Qgl l Qal	78-01-18 78-01-17 78-01-18 78-01-17 78-01-17	E10 E10 E20 L10 F10	412 738 43 567 79	7.2 7.7 6.4 7.7 6.1	8.0 6.0 8.0 8.0	K0 <1 <1 <1 <1	<1 <1 <1 <1 <1	190 300 16 250 29	29 0 0 0	56 77 4.9 62 7.4	13 27 .8 22 2.6

Notations: 0 - Analyzed for, but not detected
-- Determination deleted; improper sample
< - Less than
> - Greater than

Units: MICROMHOS - micromhos per centimeter at 25°C
DEG C - degrees Celsius
MG/L - milligrams per liter
UG/L - micrograms per liter

SUDIUM. DIS- SOLVED (MG/L AS NA)	SODIUM AD- SORP- TION RATIO	POTAS- SIUM, DIS- SOLVED (MG/L AS K)	B1CAR- BUNATE (MG/L AS HC03)	CAR- HONATE (MG/L AS CO3)	ALKA- LINITY, TOTAL (MG/L AS CACO3)	SULFATE DIS- SOLVED (MG/L AS SO4)	DIS- SOLVED (MG/L	SOLIDS+ SUM OF CONSTI- TUENTS+ DIS- SOLVED (MG/L)	NITHO- GEN+ NOZ+NO3 DIS- SOLVED (MG/L AS N)	PHOS- PHORUS. TOTAL (MG/L AS P)	IRON+ DIS- SOLVED (UG/L AS FE)	CHLO- MIDE+ DIS- SOLVED (MG/L AS CL)	SILICA. UIS- SOLVED (MG/L AS SIUZ)
COUNT	Y												
9.4 13 9.2 6.2 11	0.6 .7 .3 .2 .4	1.3 2.3 2.4 1.8 10	70 120 200 160 200	0 0 0 0 0	57 98 160 131 160	8.5 2.7 3.1 2.8 3.9	0.1 .3 .2 .4 .2	103 143 208 181 197	0.06 .00 .09 .08	0.00 .07 .05 .13 .05	510 350 60 10 0	1.3 1.6 1.3 1.1 1.0	31 40 44 49 27
14	•5	.6	\$50	Ŏ	180	7.0	.4	199	.04	.00	30	1.2	22
COUNT	Y												
3.1 15 5.3 3.8 4.1	.1 .6 .3 .1	1.6 .5 2.0 1.8 1.7	110 180 110 160 160	0 0 0 0	90 148 90 130 131	7.2 3.3 6.0 8.9 8.7	•1 •2 •1	126 173 120 153 153	.30 .25 .16 .18	.19 .01 .04 .00	10 20 60 10	1.0 .8 .7 .6	24 19 20 13 15
2.0 5.6 5.1 5.2 2.5	•2 •2 •2 •2	2.0 2.0 1.8 .7	29 160 220 120 130	0 0 0 0	24 131 180 98 110	2.3 9.0 6.0 15 9.0	.0 .2 .2	42 178 220 145 123	.10 5.0 5.0 .11	.02 .03 .04 .01	40 10 10 630 20	2.7 .8 .6	16 13 24 24 11
1.8 5.6 6.1 5.6 1.3	•1 •2 •2 •2 •2	.6 1.8 2.2 1.1	110 150 220 200 16	0 0 0 0	90 123 180 160 13	6.8 9.1 11 29 1.5	•1 •1 •1 •2 •0	104 152 201 230 28	.07 .47 .01 .01	.02 .03 .05 .00	30 10 60 160 60	.3 .8 .5 3.9 .2	9+7 19 12 21 11
2.5 17 7.8 5.0 5.6	•1 •6 •3 •4 •3	1.2 1.9 .7 2.3 1.5	430 210 120 57 100	0 0 0 0	350 172 98 47 82	8.2 29 11 3.0 5.7	•1 •5 •1 •1	361 233 135 77 112	.03 .09 .06 .18	.02 .00 .02 .02	50 50 30 50 60	1.2 1.6 .7 .5 1.5	16 27 22 25 25
3.4 12 3.1 1.2 2.4	.3 .4 .1 .1	1.4 2.0 2.8 .5 1.3	28 190 170 23 260	0 0 0 0	23 156 139 19 210	5.8 28 11 5.6 2.4	•1 •3 •1 •1	68 206 156 36 230	1.6 .21 .01 .02	.01 .02 .02 .02	50 10 110 50 20	1.6 .9 .4 .2 1.3	25 15 9•7 10 15
3.4 4.4 7.6 5.6 2.8	.3 .5 .3	.8 1.3 1.9 1.4 1.5	37 57 80 93 66	0 0 0 0	30 47 66 76 54	1.7 6.1 6.1 17	•2 •3 •2 •1	76 76 102 124 99	.51 .04 .02 .01	.06 .01 .08 .06	50 20 50 5300 220	1.0 .9 .4 .7	39 19 27 25 19
1.8 5.5 2.5 3.0 1.5	.2 .3 .3	1.4 1.8 .9 1.1	31 170 24 32 39	0 0 0 0	25 140 20 26 32	.7 16 2.1 2.3 3.1	.1 .3 .0 .1	45 178 47 54 47	.04 .01 .41 .08	.03 .02 .07 .03	340 170 60 70 50	.4 .2 .7 .6	16 19 22 25 13
COUNTY													
2.5 14 33 39 13	.1 .3 .6 1.3	2.5 4.1 3.2 2.6 1.6	290 420 530 180 170	0 0 0 0	240 340 430 150 140	21 47 52 100 18	.2 .6 .1 .4	273 416 773 312 175	.05 .04 25 .02	.02 .15 .02 .02	1100 2000 40 160 40	.7 1.2 60 3.8	15 20 35 15 13
11 58 1.9 34 4.7	.3 1.5 .2 .9	3.0 4.0 1.0 3.3	200 490 19 380 44	0 0 0 0	160 400 16 310 36	37 29 2.7 18 1.0	•1 •5 •1 •?	245 456 35 342 65	.03 .01 .40 .01	.01 .02 .01 .09	2700 730 20 2000 70	10 3.5 .7 1.6	13 15 12 12 26

LUCAL IDENT- I- FIER	AQUIFER(S)	DATE OF SAMPLE	WELL YIELD (GAL/MIN)	SPE- CIFIC CON- DUCT- ANCE (MICFO- MHOS)	PH (UNITS)	WATER TEMPER- ATURE (DEG C)	COLI- FORM. TOTAL. IMMED. (COLS. PER 100 ML)	COLI- FORM. FECAL. 0.7 UM-MF (COLS./	HARD- NESS+ DIS- SOLVED- (MG/L AS CACO3)	HARD- NESS: NONCAR- BONATE: DIS: (MG/L CACO3)	CALCIUM DIS- SOLVED (MG/L AS CA)	MAGNE- SIUM, DIS- SOLVED (MG/L AS MG)
		-									ко	OTENAI
48N 01w 18RHB1 49N 01w 15NAC1 49N 01w 22DDC1 50N 04w 05DDA1 50N 05w 01AAD1	epe Qal Qgl	78-03-02 78-03-01 78-03-02 77-08-03 77-07-20	E10 E10 E20 >5 700	208 151 102 109 123	6.7 6.5 6.5 6.6 8.2	5.5 5.5 8.0 14.5 15.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	89 43 42 51 59	8 11 7	20 7.9 11 14 17	9.4 5.6 3.5 4.0 4.0
50N 05W 01CBF1 50N 05W 06DCC1 50N 05W 07ADD1 51N 03W 19AAD1 51N 04W 06ADA1	Qgl Qgl Qgl Qgl	77-07-20 77-07-21 77-08-01 77-07-28 77-07-12	1400 >3000 £10 £10 >1000	83 82 83 63 181	7.2 6.8 6.6 6.5 8.1	15.5 10.0 12.0 9.0 8.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	35 37 35 26 90	3 7 0 0	9.9 10 10 7.3 24	2.5 2.8 2.5 1.8 7.3
51N 04W 12ABA1 51N 04W 15AAA1 51N 04W 15DA61 51N 04W 17CRC1 51N 04W 19DCC2	Tor Qgl Qgl Qgl Qgl	77-07-27 77-07-13 77-07-26 77-07-27 77-07-21	£25 >100 £20 £20 >1000	180 248 144 320 335	6.7 8.0 8.0 7.6 7.8	14.0 7.0 9.5 8.0 9.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	81 120 71 180 190	0 0 0 24 30	20 30 20 36 38	7.5 11 5.1 22 22
51N 04W 22RCA1 51N 04W 23DAA1 51N 04W 24ABB1 51N 04W 27DDE1 51N 04W 29DBB1	Qgl Qgl Qgl Qgl	77-08-04 77-07-12 77-07-26 77-07-28 77-07-12	>200 >100 E20 >500 >1000	301 121 97 257 262	8.2 8.1 7.1 7.9 8.1	9.5 11.0 10.0 8.0 10.0	<1 <1 <1 <1	<1 <1 <1 <1	170 57 48 130 150	0 0 2 9 15	42 18 13 28 29	17 3.0 3.7 15 18
51N 04W 35ADH1 51N 05W 11DDH1 51N 05W 12ABA1 51N 05W 19CAO1 51N 05W 25DAB1	Qgl Qgl Qgl Qgl	77-07-26 77-07-13 77-07-13 77-07-21 77-07-20	+ 15 >100 >1000 >500 >1000	327 128 285 337 269	8.1 8.3 7.7 7.6 8.0	10.0 7.0 12.0 10.0 8.5	<1 <1 <1 <1	<1 <1 <1 <1	180 65 150 170 140	15 0 0 0 1	37 19 34 53 31	21 4.3 16 8.9 15
51N 05W 26BCA1 51N 05W 27BB61 51N 05W 31ACA1	Qgl Qgl Qgl	77-07-20 77-07-21 77-07-21	>1000 £10 >1500	272 264 276	7.9 7.9 8.0	8.5 9.0 8.5	<1 <1 <1	<1 <1 <1	140 150 160	1 2 12	32 32 36	15 16 18
51N 05W 35BDC1 52N 03W 07DAC1 52N 03W 07DCA1 52N 03W 19AAB1 52N 04W 10DAB1	Qgl Qgl Qgl TKi	77-07-20 77-08-04 77-08-02 77-08-02 77-08-02	>1000 >5 >200 E5 E2	248 186 164 89 304	8.0 7.8 7.0 6.5 7.6	15.0 8.5 9.0 9.5 14.0	<1 <1 83 <1 <1	<1 <1 81 <1 <1	130 100 83 38 160	17 6 1 0	28 34 26 11 42	15 4.8 4.3 2.5
52N 04W 14DCD1 52N 04W 17DDD1 52N 04W 20CCB1 52N 04W 27DCD1 52N 04W 31DAB1	Qg1	77-08-03 77-08-09 77-07-14 77-07-14 77-07-13	E10 150 <15 >20 E30	199 162 65 297 187	7.2 8.1 6.9 7.9 7.7	10.0 10.5 13.5 9.5 8.5	<1 <1 <1 <1 <1	<1 <1 <1 <1	96 85 21 170 94	0 3 0 9	17 23 6.6 33 26	13 6.8 1.2 20 7.1
52N 04W 32ABC1 52N 04W 35DCB1 53N 02W 07CAA1 53N 02W 19ADD1 53N 03W 03RAB1	Qgl(?) Qgl TKi	77-07-13 77-07-12 77-07-19 77-07-19 77-07-19	>1000 >1000 £10 >B >5	232 495 273 274 278	7.8 7.9 7.8 7.8 8.0	8.5 11.5 10.0 10.0	<1 <1 <1 <1	<1 <1 <1 <1 <1	120 270 140 130 150	0 0 1 0 2	28 50 33 39 35	12 36 14 8.7 16
53N 03W 09CDD1 53N 03W 21CDC1 53N 03W 22DAB1 53N 04W 06DD62 53N 04W 22CDU1	TKi & Qgl TKi Qgl	77-08-02 77-07-27 77-07-14 77-07-19 77-08-02	70 E20 >20 >500 E10	297 374 402 53 315	7.8 7.3 7.9 6.7 7.6	8.0 8.5 12.0 13.0 9.5	84 <1 <1 81 <1	<1 <1 <1 <1	160 210 200 21 170	20 4 26 0 6	36 54 50 6•4 35	17 18 17 1.3 20
53N 04W 24RBA1 53N 04W 33CHB1 53N 04W 36R8A1 54N 07W 34CCH1	Qg1(?) Qg1	77-08-02 77-07-28 77-07-27 77-08-22	>500 E20 E20 >5	262 302 199 229	7.8 7.7 7.6 7.3	8.0 8.0 7.0 11.5	<1 <1 <1 <1	<1 <1 <1 <1	140 170 92 130	7 22 2 0	34 36 27 36	13 19 6.0 10

SODIUM. DIS- SOLVED (MG/L AS NA)	SODIUM AD- SORP- TION RATIO	POTAS- SIUM, DIS- SOLVED (MG/L AS K)	BICAR- BONATE (MG/L AS HCO3)	CAR- HONATE (MG/L AS CO3)	ALKA- LINITY, TOTAL (MG/L AS CACO3)	SULFATE DIS- SOLVED (MG/L AS SO4)	FLUO- RIDE+ DIS- SOLVED (MG/L AS F)	SOLIDS. SUM OF CONSTITUENTS. DIS- SOLVED (MG/L)	NITRO- GEN+ NO2+NO3 DIS- SOLVED (MG/L AS N)	PHOS- PHORUS+ TOTAL (MG/L AS P)	IRON. DIS- SOLVED (UG/L AS FE)	CHLO- MIDF + JIS- SOLVED (MG/L AS CL)	SILICA. 015- 50LVEN (MG/L AS 5102)
COUNTY	t .												
7.7	0.4	1.9	98	0	80	24	0.4	141	0.02	0.01 .16	780 13000	0 • 5 • 5	28 23
4.5 4.6	.3 .3	1.0 .7	47 41	0	39 34	13 18	• 1 • I	92 81	.50 10•	.04	13000	1.3	20
2.5	.2	1.2	49	ŏ	40	6.2	• 0	69	•57	.01	10	1.6	13
2.7	• 1	1.3	63	0	52	5.2	.0	79	•86	.01	10	.9	14
1.8	• 1	.9	39	0	32	4.9	.0	54	•20	.01	10	.3	1 3
2.1	۶.	•8	41	0	34	4.6	•0	54 54	.54 .34	.01 .04	10 60	.6	11 10
2.0 1.8	•1 •2	.8 .8	34 34	0	28 28	9.2 2.2	•1	42	.17	.00	10	.6	10
2.4	.1	1.3	110	0	90	6.8	.0	110		.00	10	.6	1.3
7.0	•3	2.5	110	0	90	9.4	• 2	155	.35	.09	10	• A	52
2.3	.1	1.5	160	0	131	4.0	.0	140		.01	10	2•1	11
2.3	• 1	1.4	88	0	72	11	• 1	98	.61	•00	10	1.5	11
3.1 2.7	•1 •1	2•1 2•2	190 190	0	156 160	17 19	•1 •1	193 197	2.0 1.6	.00 .01	10 10	1.1	11
				•									12
3.5	• į	2.1	210	0	172	11	• 1	203	2.1	.01	0 10	۶.5 5.	11
1.9 1.8	•1 •1	1.1	88 56	0	72 46	2.9 2.9	.0 .1	63	.34	.00	20	. 7	ii
3.1	.1	2.0	150	0	120	9.3	.1	153	1.6	.02	0	2.1	15
2.7	.1	1.8	160	ō	130	9.5	.0	153		•00	10	1.5	15
3.6	.1	2.1	200	0	160	13	.0	202	2.9	.00	10	2.8	11
2.1	• 1	1.0	83	0	68	3.4	.0	83		.01	10	.8 .5	12 15
3.4	• 1	1.7	200	0	164	7.3	.0	177	.85	.01 .01	10 10	1.5	18
4.4 2.7	• 1	2.0 1.8	210 170	0	170 139	2.9 8.8	•1	198 159	1.0	.01	10	.,	11
2.2							,	163	.21	.01	10	.5	11
3.3 3.2	• 1 • 1	1.7	170 180	0	139 148	14 15	•1	170	.37	•01	10	.6	11
2.9	:1	1.9	180	0	148	15	• 1	179	.92	.01	30	1.0	11
2.1	.1	2.0	140	0	110	8.2	.1	149	2.2	.01	10	1.5	13
5.5	.1	2.0	120	0	98	3.9	• 1	125	•38	• 05	40	1.0 .8	16 16
2.5	• 1	2.0	100	0	82	3.7	• 1	110	1.2	.02	10 250	.9	16
2.6 6.8	•2	1.5 1.1	51 200	0	42 160	2.1 11	•1 •5	66 185	.37	.01	10	.3	11
4.7	2							136	.01	.04	2600	• 5	ک ک
4.7 2.6	.2 .1	1.4 1.2	140 100	0	115 82	2.7 4.4	.4	103	.26		10	• 5	14
3.5	.3	.8	39	ŏ	32	2.9	.i	45		•00	20	.3	10
2.1	. 1	2.5	190	0	160	10	. 1	172			20	• 3	10
2.4	.1	1.3	150	0	123	5.2	• 0	131		•00	10	•6	14
2.9	.1	1.5	160	0	131	12	•1	148			20 40	•5 •5	12 13
3.4	• 1	4.0	350	0	287	41	•1	320	.34		20	.9	8.0
3.4 7.8	•1 •3	1.6	170 170	0	139 139	13 12	•1	159 168	.15		10	.5	15
3.7	.1	.9 2.1	180	0	148	7.7	• 1	172	.37		10	. 4	16
2.8			170	0	140		,	175	.85	.00	10	2.5	7.9
2.8	•1 •1	2.3 2.4	250	0	210	19 9.6	•1	224	•28		10	.9	17
9.3	.3	.7	210	0	172	23	. 1	223		• 00	20	H•8	11
2.4	• 2	1.0	29	0	24	1.4	. 0	43	.33	-02	50	•5 •7	14 10
2.5	- 1	2.3	200	0	164	16	• 1	188	•64	.01	10		
3.0	.1	1.6	160	0	130	15	•1	157	.34	.01	30	•8 •8	9.5 10
3.4	• 1	2.0	180	0	148	19	• 1	180	.21 .40		20 10	•6	16
1.9 2.8	•1	1.2	110 160	0	90 131	3.4 13	• 1	112 156	.36		20	1.2	ii
2.0	• 1	1.5	100	U	1 31	1 2	• 1	150	• 32				

	LOCAL IDENT- I- FIER	AQUIFER(S)	DATE OF Sample	WELL YIELD (GAL/MIN)	SPE- CIFIC CON- DUCT- ANCE (MICRO- MHOS)	PH (UNITS)	WATER TEMPER- ATURE (DEG C)	COLI- FORM, TOTAL, IMMED. (COLS. PER 100 ML)	COLI- FORM+ FECAL+ U.7 UM-MF (COLS./ 100 ML)	HARD- NFSS, DIS- SOLVED (MG/L AS CACO3)	HARD- NESS+ NONCAR- BONATE, DIS. (MG/L CACO3)	CALCIUM DIS- SOLVED (MG/L AS CA)	MAGNE- SIUM, DIS- SOLVED (MG/L AS MG)
													LATAH
	03W 03RCH1		78-05-17	E10	129	7.1	8.5	<1	<1	54	Û	14	4.6
	03W 098HD1		78-05-17	£10	968	7.1	10.5	<1	<1	230	50	78	8.7
	04w 068AC1	Tcr	78-05-18	£20	324	8.0	15.5	<1	<1	65	0	18	4.8
	04# 09RAD1 05w 03DBC1	Tcr Tcr	78-05-18	£10	338 396	8.1 7.2	10.5	<1	<1	72	0	20	5.3
4114	05W 0308C1	ICI	78-05-18	€10	370	1.42	12.0	14	<1	180	45	44	16
												S	SHOSHONE
	02E 03AbC1		78-02-28	E10	171	6.3	9.0	<1	<1	69	36	14	8.3
48N	026 028DA1		78-02-28	£20	46	6.1	9.0	<1	<1	16	7	4.5	1.2
48N	03E 06ADA1		78-02-28	£10	274	6.1	10.5			100	59	27	7.8
	03E 110001		78-02-28	E10	199	6.2	8.5	<1	<1	88	44	25	6.3
48N	05E 36R881	Qg1(?)	78-03-02	E5	104	6.4	5.5			49	3	15	2.9
	01E 349DC1		78-03-01	E200	166	6.0	9.0	<1	<1	68	51	18	5.6
49N	OSE ORCAVI	€p€	78-03-01	£10	106	6.3	4.0	<1	<1	42	17	6.2	6.4

Metallic

	LOCAL IDENT- I- FIER	DATE OF Sample	IRON, DIS- SOLVED (UG/L AS FE)	LEAD. OIS- SOLVED (UG/L AS PR)	MERCURY DIS- SOLVED (UG/L AS HG)	MOLYB- OENUM+ DIS- SOLVED (UG/L AS MO)
				_	0.0	
	OPE 03ABC1	78-02-28	30	5	0.0	į.
	02E 05BDA1	78-02-28	0	9	• 0	0
48N	03F 06ADA1	78-02-28	130	7	.0	0
4AN	03F 11DDD1	78-02-28	30	10	.0	0
48N	05F 368BH1	78-03-02	90	15	• 0	0
49N	01E 348DC1	78-03-01	380	7	.0	1
49N	UPE 08CAA1	78-03-01	30	7	.0	1

SODIUM. DIS- SOLVED (MG/L AS NA)	SODIUM, AD- SORP- TION RATIO	POTAS- SIUM, DIS- SOLVED (MG/L AS K)	BICAR- BONATE (MG/L AS HCO3)	CAR- RONATE (MG/L AS CO3)	ALKA- LINITY. TOTAL (MG/L AS CACO3)	SULFATE DIS- SOLVED (MG/L AS SO4)	FLUO- RIDE+ DIS- SOLVED (MG/L AS F)	SULIDS. SUM OF CONSTI- TUENTS. DIS- SOLVED (MG/L)	NITRO- GEN+ NO2+NO3 DIS- SOLVED (MG/L AS N)	PHOS- PHORUS, TOTAL (MG/L AS P)	IRON. DIS- SOLVED (UG/L AS FE)	CHLO- RIDE • DIS- SOLVED (MG/L AS CL)	511.1CA • 015 - 57LVED (M6/L 45 5102)
COUNTY													
5.6 110 50 49 13	0.3 3.2 2.7 2.5	2.2 4.1 2.9 2.8 1.7	79 220 200 200 160	0 0 0 0	65 180 160 160 130	2.1 140 9.7 11 5.8	0.1 1.4 .3 .2	106 565 206 208 278	0.01	0.03 .00 .02 .01	20 1400 60 50	1.4 100 2.9 3.4 17	37 13 14 18 44
COUNTY													
5.6 1.1 9.6 2.6 1.3	•3 •1 •4 •1	1.3 .5 1.4 1.1 2.9	41 11 49 54 56	0 0 0 0	34 9 40 44 46	44 9•7 73 44 5•6	• 1 • 0 • 1 • 0 • 0	117 35 165 128 66	.12 .20 .52 1.3 .43	.00 .01 .00 .01	30 0 130 30 90	.7 .3 .2 2.0	// 11 13 11 0.1
3.6 5.2	•2	1.2	21 30	0 0	17 25	52 23	• 0 • 1	112 91	.46 1.0	.03 .17	380 30	1.5	17

trace elements

SELE- NIUM, DIS- SOLVED (UG/L AS SE)	VANA- DIUM. DIS- SOLVED (UG/L AS V)	7INC+ DIS- SOLVED (UG/L AS ZN)	ARSENIC DIS- SOLVED (UG/L AS AS)	CADMIUM DIS+ SOLVED (UG/L AS CD)	CHRO- MIUM+ DIS- SOLVFD (UG/L AS CR)	COPPEH. DIS- SOLVED (UG/L AS CU)
0 0 0 0	0.0 .0 .0	210 110 1200 3600 210	0 0 8 0	2 3 4 23	0 0 0 0	77 27 8 3 22
0	•0	110 230	0	3	0	9 67

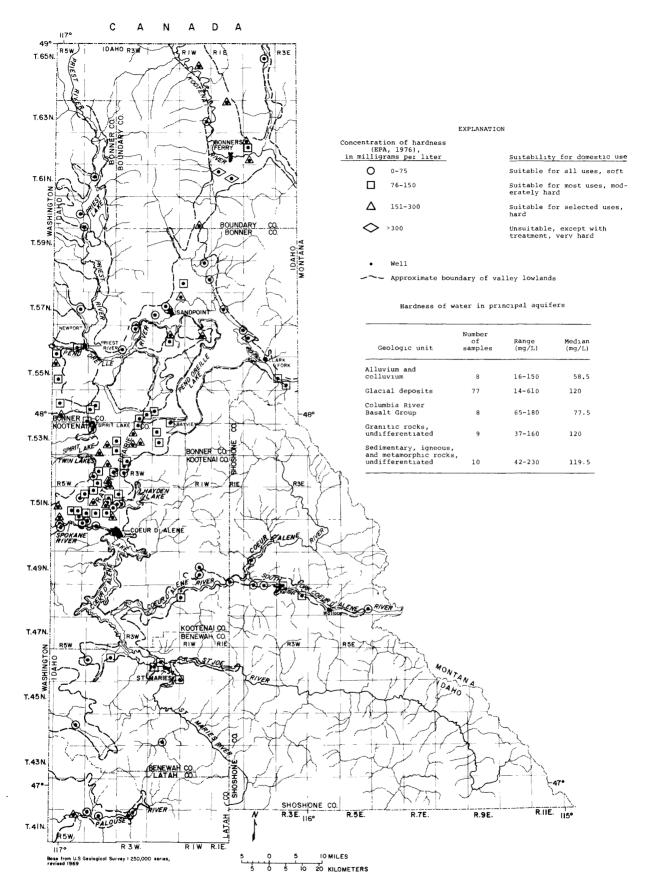


Figure 4.--Hardness in ground water.

Dissolved Solids

Dissolved-solids concentrations are an indication of total mineral content in water. As used in this report, "dissolved solids" represents the sum of the major chemical constituents in each water sample. Dissolved solids consist mainly of the cations (calcium, magnesium, potassium, and sodium) and anions (bicarbonate, carbonate, chloride, fluoride, nitrate, and sulfate), plus silica.

Dissolved-solids concentrations exceeding 500 mg/L occurred in water from only two wells--one in the Kootenai River valley and one in the Palouse River valley (see table 3). Concentrations ranging from 250 to 500 mg/L occurred most often in samples collected from wells tapping alluvial and glacial deposits in the Kootenai River valley. Dissolved-solids concentrations less than 250 mg/L were most common and reflect the general ground-water quality in north Idaho.

The EPA (1977b) recommends that dissolved-solids concentrations in water for public supplies not exceed 500 mg/L. However, their recommendation relates to the esthetic qualities of drinking water. If none of the individual constituents that contribute to the dissolved-solids concentration are present in a concentration that would be harmful, dissolved-solids concentrations greater than 500 mg/L may have no harmful physiological effects and even may be beneficial to health (EPA, 1977c).

Dissolved solids affect the suitability of water for livestock, irrigation, industry, and domestic uses; but, because the concentrations in the study area are relatively low, ranging from 28 to 773 mg/L, there is little cause for concern by ground-water users.

The distribution of dissolved solids in water from aquifers that locally provide the first occurrence (with depth) of a suitable water supply is shown in figure 5. The table in figure 5 shows the range and median concentration of dissolved solids in water from each of the various geologic units.

<u>Nitrate</u>

For convenience, the concentration of nitrite-plusnitrate ions is expressed in terms of the concentration of elemental nitrogen present, and nitrite-plus-nitrate is hereafter referred to collectively as nitrate. Nitrate

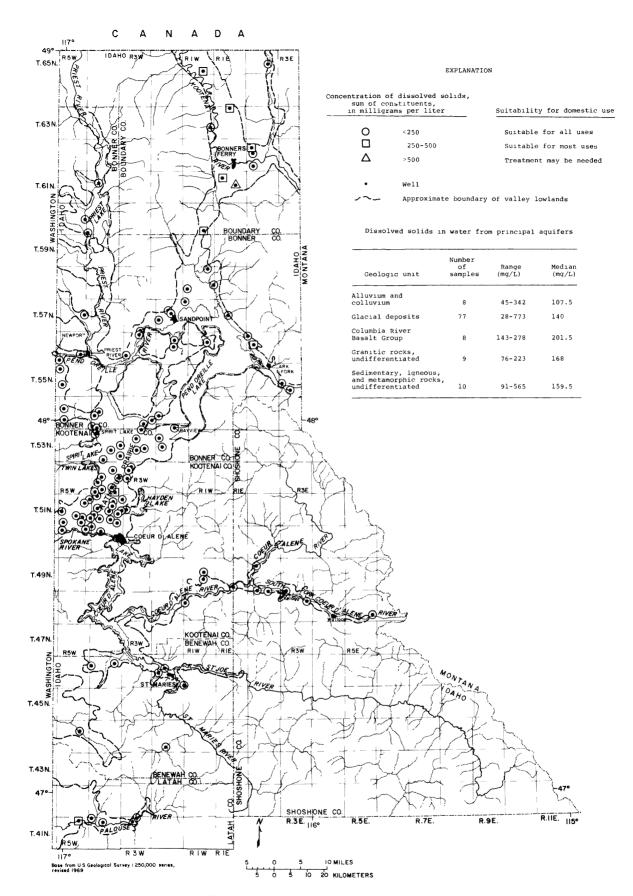


Figure 5.--Dissolved solids In ground water.

concentrations in water samples from wells in the study area ranged from 0.00 to 25 mg/L (see table 3). A mandatory limit of 10 mg/L nitrate has been established for public water supplies by EPA (1977a). In the 104 water samples analyzed for nitrate, concentrations exceeded 1 mg/L in 15 samples and exceeded 10 mg/L in 2 samples (fig. 6). Most nitrate concentrations were less than 0.5 mg/L.

Excessive concentrations of nitrate in a water supply generally are an indication of man-caused contamination. Potential sources of nitrate in water supplies are municipal and industrial waste waters, septic-tank effluent, leachates from barnyards and feedlots, cropland and lawn fertilizers, animal wastes, leachates from garbage dumps and landfills, and certain kinds of mine drainage. Natural sources of nitrate in ground water include decaying plants and soluble nitrogen compounds or minerals in soils and rock materials. Natural sources are minor contributors of nitrogen to most ground water in north Idaho.

Ten water samples that had nitrate concentrations between 1 and 10 mg/L were from glacial deposits consisting of sand and gravel, in which water levels in wells ranged from 11 to 299 ft below land surface. Additional data are necessary to accurately determine the principal source(s) leading to the elevated concentration of nitrate in north Idaho ground water.

Concentrations exceeding 1 mg/L were common in the southern part of Rathdrum Prairie north of Coeur d'Alene and west of Hayden Lake. Wells sampled in this area are completed in glacial deposits consisting of sand and gravel, in which water levels generally are greater than 200 ft below land surface. Nitrate concentrations averaged 1.8 mg/L and were consistently higher than the probable ambient concentration of less than 0.5 mg/L. Potential sources of these nitrates are described above.

Iron

Concentrations of dissolved iron in water from 116 wells in the study area ranged from 0 to 13,000 $\mu g/L$ (see table 3). Concentrations in 15 of 116 samples (fig. 7) exceeded the recommended limit of 300 $\mu g/L$ for public water supplies (EPA, 1977a). The highest iron concentrations were from wells in alluvial aquifers, glacial deposits, and the basement complex. The highest individual concentration, 13,000 $\mu g/L$, was in a sample from well 49N-1W-15DACl completed in argillite of Precambrian age. A concentration of

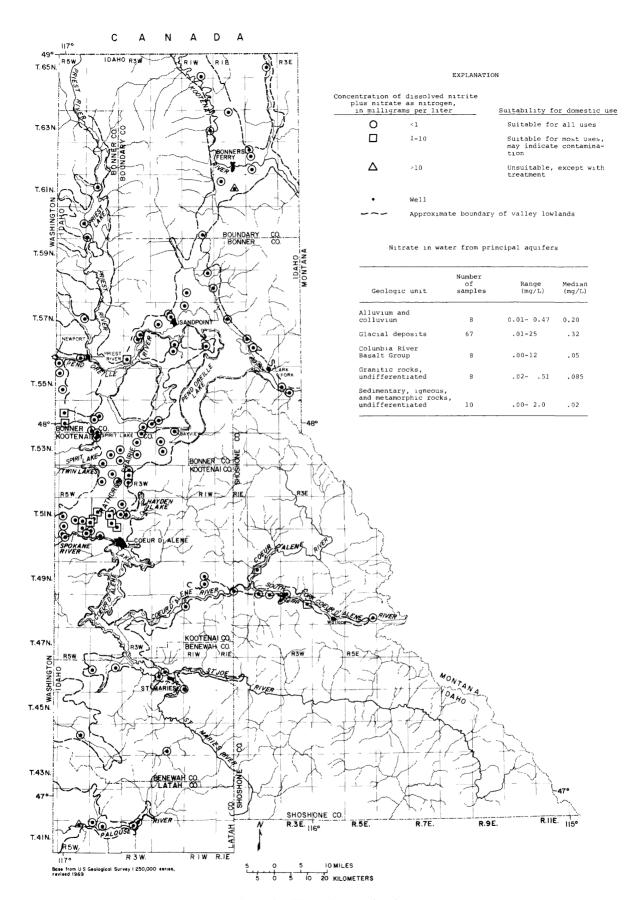


Figure 6.--Nitrate in ground water.

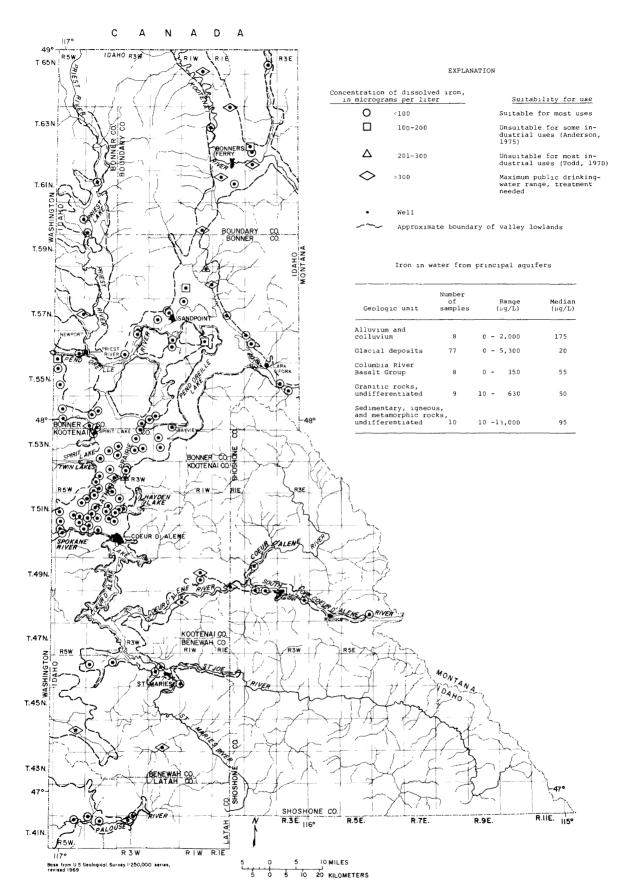


Figure 7.--Iron in ground water.

 $5,300~\mu g/L$ was in a sample from well 57N-5W-14DCCl completed in a glacial-sand aquifer. Most concentrations such as these are probably due to minerals in the local geologic formations and are not widespread areally. Corrosion of well casings and iron bacteria in water also may add to the concentration of iron in some well water.

Iron in water is objectionable because concentrations greater than 100 $\mu g/L$ may precipitate on exposure to air, resulting in turbidity and staining, changes in food and beverage taste, and possible deposition in plumbing. Most water for domestic use having excessive iron may be improved by the use of commercially available filters.

Most concentrations exceeding 300 $\mu g/L$ were from wells in the Kootenai River valley, where 50 percent of the wells sampled had an iron concentration of 1,700 $\mu g/L$ or more. The average iron concentration in all wells sampled in this valley was 949 $\mu g/L$. All samples in the Kootenai River valley containing more than 300 $\mu g/L$ of iron were obtained from glacial aquifers consisting of sand and gravel, in which water levels in wells ranged from 10 to 100 ft below land surface. No specific iron source or cause for the high concentrations in these aquifers was determined.

Trace Elements

Ground water from seven wells upstream from Cataldo, Idaho, along the Coeur d'Alene and South Fork Coeur d'Alene River valleys, was analyzed for metallic trace elements (see table 3). Except for one sample in which the arsenic concentration was 8 µg/L, arsenic, chromium, mercury, molybdenum, selenium, and vanadium concentrations were negligible. Dissolved cadmium concentrations ranged from 2 to 23 µg/L; copper from 3 to 77 µg/L; lead from 5 to 15 µg/L; and zinc from 110 to 3,600 µg/L (fig. 8). Mandatory and recommended maximum limits for the most significant trace elements in public water supplies (EPA, 1977a and 1977b) are 10 µg/L for cadmium (mandatory); 1,000 ug/L for copper (recommended); 50 μg/L for lead (mandatory); and 5,000 μg/L for zinc (recommended). The concentration of cadmium exceeded the mandatory level at site 48N-3E-11DDD1. The presence of most of these elements probably is natural -- a result of the geologic conditions of the sampling area; however, leachates from mining and smelting operations in the Coeur d'Alene mining district may also be contributing some of these elements.

Table 4 summarizes the more common possible sources of cadmium, copper, lead, and zinc in ground water. The significance of the elements to human health is also briefly discussed, as are the maximum limits permissible for public water supply.

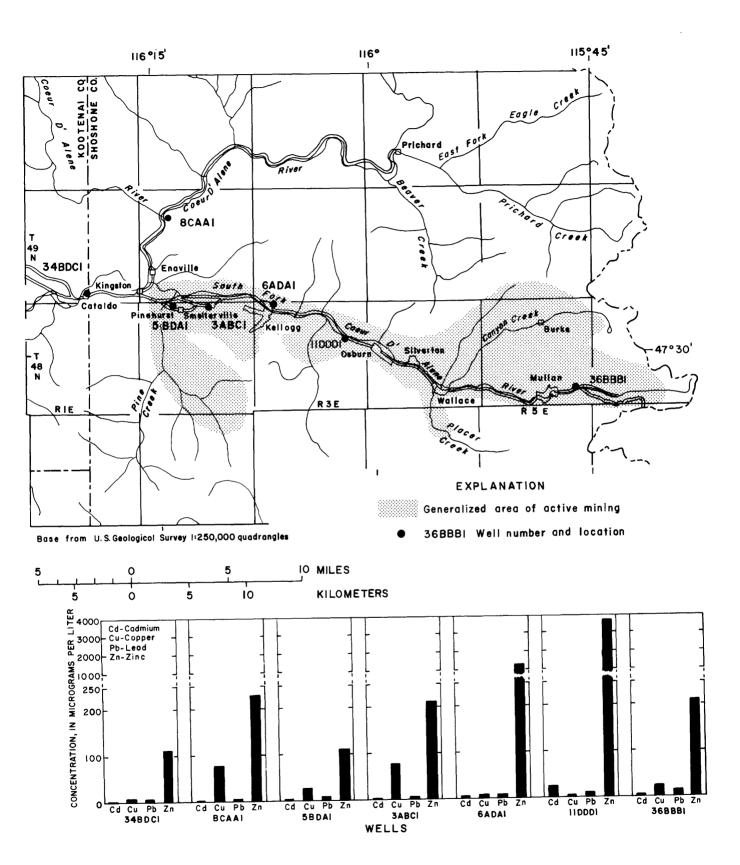


Figure 8.--Selected metallic trace elements in ground water in the Coeur d' Alene mining district.

Table 4. Source and significance of selected metallic trace elements in water

Constituent	Sources or causes	Range of concentrations in sampled wells	Significance
Cadmium (Cd)	Rare element. Occurs in nature chiefly as a sulfide salt in association with zinc and lead ores. Concentration of cadmium in most freshwater is l µg/L or less; greater concentrations are rare and often associated with mining or industrial processes.	2-23 μg/L	Nonessential, nonbeneficial element to animal and plant metabolism. Biologically recognized to be toxic, producing tumors, renal dysfunction, hypertension, arteriosclerosis, growth inhibition, chronic diseases of old age, and cancer. May be ingested or inhaled. Stored largely in the kidneys and liver and is excreted at an extremely slow rate. Mandatory maximum limit for public water supplies is 0.01 mg/L (10 µg/L). ²
Copper (Cu)	Occurs as a natural or native metal and in various mineral forms, such as cuprite and malachite. Present in sewage, agricultural, and industrial wastes. Common constituent in industrial products. May be used as algicide in public water-supply systems. May be present in leachates from mine dumps and mill tailings.	3-77 µg/L	Essential in very small quantities to plant and animal metabolism. Recommended daily requirement for normal growth in children is 0.1 mg/day (100 $^{\mu}$ g/day). Estimated daily requirement for adults is 2 mg/day (2,000 $^{\mu}$ g/day). Natural concentrations in water are not known to have adverse effects on humans. An excess of 1 mg/L (1,000 $^{\mu}$ g/L) may impart some taste to water. Ingestion of excessive quantities results in liver damage. Recommended maximum limit for public water supplies is mg/L (1,000 $^{\mu}$ g/L).
Lead (Pb)	Occurs in nature commonly as lead sulfide, lead sulfate, lead carbonate, and lead chlorophosphate. Relatively insoluble. Incorporated into groundwater system through precipitation; lead-dust fallout; erosion and leaching of soil; urban runoff, and municipal, industrial, and mining wastes.	5-15 μg/L	A toxic metal that tends to accumulate in animal and human tissues. No beneficial or desirable nutritional value. Lead intoxication and lead poisoning most seriously affect children, frequently resulting in irreversible damage to the brain, anemia, neurological dysfunction, and renal impairment. Most common symptoms of lead poisoning are anemia, severe intestinal cramps, paralysis of nerves, loss of appetite, and fatigue; the symptoms usually develop slowly. Mandatory maximum limit for public water supplies is 0.05 mg/L (50 µg/L). ²
Zinc (Zn)	Common sulfide mineral often associated with sulfides of other metals, especially lead, copper, cadmium, and iron. Widely used metal, found in many industrial wastes. Incorporated into many metallic industrial products. May be dissolved from galvanized pipe. Present in mine discharge and leachates from mine dumps and mill tailings.	110-3,600 μg/L	Daily intake requirement for preschool age children is 0.3 mg/kg (300 $\mu g/kg$) body weight³. Deficiency of zinc in children leads to growth retardation. Essential to human metabolism. More than 5,000 $\mu g/L$ produces a bitter or astringent taste. Recommended maximum limit for public water supplies is 5 mg/L (5,000 $\mu g/L$).

¹Hem (1970) ²U.S. Environmental Protection Agency (1977a) ³U.S. Environmental Protection Agency (1976) ⁶U.S. Environmental Protection Agency (1977b)

SUMMARY AND CONCLUSIONS

Ground water occurs in all the geologic units described in this report—in alluvial and glacial deposits of Quaternary age, basalt of Tertiary age, granitic rocks of Tertiary and Cretaceous age, and undifferentiated sedimentary, igneous, and metamorphic rocks of Cambrian and Precambrian age (basement complex).

Wells completed in the alluvial and glacial aquifers generally yield 1 to 3,000 gal/min. Wells completed in basalt, granite, or basement-complex aquifers commonly yield 2 to 25 gal/min and average about 13 gal/min.

Hardness of the ground water ranges from 14 to 610 mg/L in samples. Most of the samples have hardness less than 150 mg/L.

Dissolved-solids concentrations in samples from the various aquifers range from 28 to 773 mg/L. In general, water in glacial deposits and basement-complex aquifers contains the highest dissolved-solids concentrations.

Nitrate concentrations range from 0 to 25 mg/L in samples. In the 104 water samples analyzed for nitrate, concentrations exceed 1 mg/L in 15 samples and exceed 10 mg/L in 2 samples, which surpasses the mandatory maximum limit for public water supplies. The natural background concentration of nitrate in ground water in most of the study area probably is less than 0.5 mg/L. Locally, where water contains excessive nitrate concentrations, contamination probably reflects certain land uses.

Dissolved-iron concentrations in ground-water samples range from 0 to 13,000 $\mu g/L$. Concentrations in 15 of 116 samples exceed the recommended maximum of 300 $\mu g/L$ for public water supplies. Iron concentrations in water may be due, in part, to corrosion of the water system or iron bacteria.

Concentrations of dissolved arsenic, cadmium, chromium, copper, lead, mercury, molybdenum, selenium, vanadium, and zinc were analyzed for seven wells in the Coeur d'Alene River valley upstream from Cataldo, in the Coeur d'Alene mining district. All concentrations of mercury, molybdenum, selenium, and vanadium are negligible. One sample contains 8 $\mu g/L$ of arsenic; all the other samples contain negligible arsenic. Dissolved cadmium concentrations range from 2 to 23 $\mu g/L$; copper from 3 to 77 $\mu g/L$; lead from 5 to 15 $\mu g/L$; and zinc from 110 to 3,600 $\mu g/L$. Of these four elements, only cadmium exceeds the mandatory maximum limit established

for public water supplies. High zinc concentrations are an indication of ground-water contamination due to mining activities.

In the study area, ground-water quantity is sufficient and quality is adequate in most places to meet population and economic demands. Alluvial and glacial aquifers are used the most at present (1978) and will probably be subject to the greatest water-quality changes in the future. Future changes in population, urban development, industrial-center locations, mining activities, irrigation, crop treatment, and recreational land and water uses may affect water quality. Periodic reevaluation of ground-water quality may be required to monitor possible adverse changes.

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