

Prepared in cooperation with

NEW YORK STATE DEPARTMENT OF TRANSPORTATION



HYDRAULIC ANALYSIS OF CHENANGO RIVER, BROOME COUNTY, NEW YORK IN RELATION TO STATE HIGHWAY PLAN

by Bernard Dunn

U.S. GEOLOGICAL SURVEY

Open-File Report 81-1020

Prepared in cooperation with

NEW YORK STATE DEPARTMENT OF TRANSPORTATION



Albany, New York

1981

UNITED STATES DEPARTMENT OF THE INTERIOR

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CONVERSION FACTORS AND ABBREVIATIONS

The following factors may be used to convert inch-pound units of measurement in this report to International System (SI) metric units.

Multiply	by	To obtain SI units
mile (mi)	1.609	kilometer (km)
square mile (mi2)	2.590	square kilometer (km ²)
cubic feet per second (ft ³ /s)	.02832	cubic meters per second (m ³ /s)
foot (ft)	.3048	meter (m)

Hydraulic Analysis of Chenango River, Broome County, New York in Relation to State Highway Plan

By

Bernard Dunn

ABSTRACT

Hydraulic analyses of the 50- and 100-year floods in a 3.2 mile-reach of the Chenango River in the towns of Fenton and Chenango were made to determine the effects of two alternative bridge designs on flood levels. Neither design would cause more than a 0.1-foot increase in water level of the 50-year flood nor more than a 0.2-foot increase in water level of the 100-year flood above levels that would occur during these floods under present channel conditions.

The discharges used in the analyses were 55,200 cubic feet per second for the 50-year flood and 63,000 cubic feet per second for the 100-year flood. Mean flow velocities and water-surface elevations at 17 cross sections are given for both bridge designs and are compared with those that would occur under present conditions.

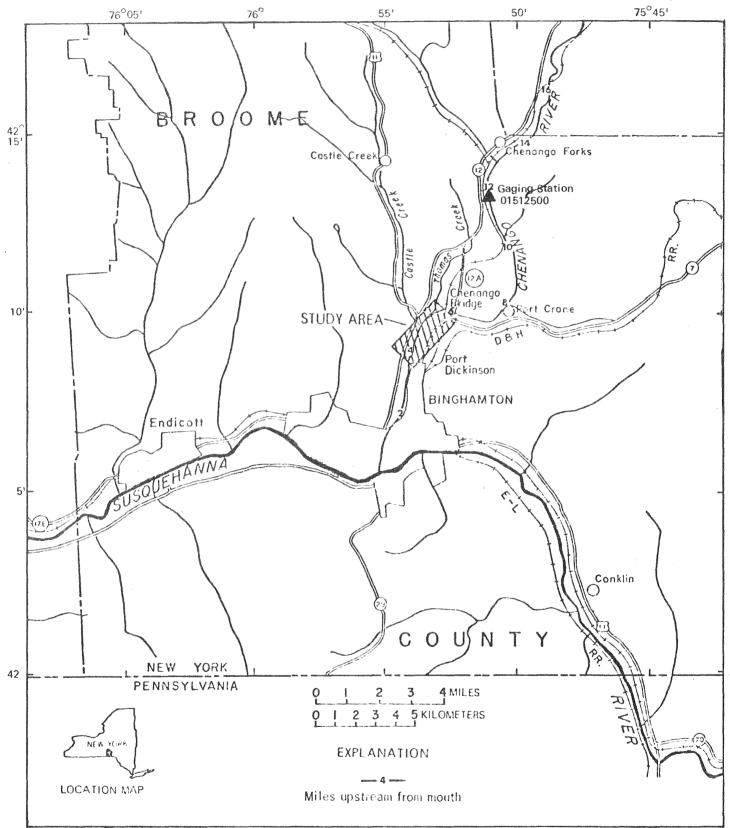
INTRODUCTION

The New York State Department of Transportation (NYSDOT) plans to construct a new highway that would include a new bridge over the Chenango River in the towns of Fenton and Chenango, about 1,400 ft north of the Port Dickinson village boundary (fig. 1). The plan also includes replacement of the present State Highway 12A bridge, 2.2 mi farther upstream, with a new one of the same size.

As part of a cooperative agreement with NYSDOT, a study was made to determine the effect the additional bridge would have on the water levels and flow velocity of a 50- and 100-year flood in the 3.2-mile reach upstream from the Port Dickinson village boundary. Two bridge designs were analyzed: one with a 1,000-foot opening and one with a 1,800-foot opening.

Previous Studies

Studies made by Dunn (1972, 1974) and Dunn and Lumia (1977) addressed the hydraulic effects that several different bridge alinements in this reach would have on flood flows. This reach has been analyzed in three other studies: two flood-insurance studies made for the towns of Fenton and Chenango, (Federal Emergency Management Agency, 1980a, 1980b) provided water surface profiles of the 10-, 50-, 100-, and 500-year floods, and a flood-plain information report (U.S. Army Corps of Engineers, 1971) provided profiles of the standard project flood and intermediate regional flood.



Base from U.S. Army Corps of Engineers, Baltimore District, 1971

Figure 1.--Major geographic features of Broome County and location of area depicted in figure 2.

Available Data

The data used in this study include:

- Cross sections of the Chenango River flood plain, determined by photogrammetric methods from aerial photographs taken in December 1978 (Federal Emergency Management Agency, 1980a, 1980b).
- Below-water cross sections of the river channel, obtained from the U.S. Army Corps of Engineers (1971) and the New York State Department of Transportation, Binghamton (written commun., June 13, 1973).
- 3. Plan drawings furnished by the New York State Department of Transportation.
- 4. Streamflow data collected by the U.S. Geological Survey during floods and field investigations.
- 5. Elevations at the downstream end of the reach, obtained from the stagedischarge relationship developed for the Town of Dickinson Flood Insurance Study (Federal Emergency Management Agency, 1977).

All elevations are referenced to the National Geodetic Vertical Datum of 1929 (NGVD), formerly referred to as Mean Sea Level Datum of 1929.

Description of Study Area

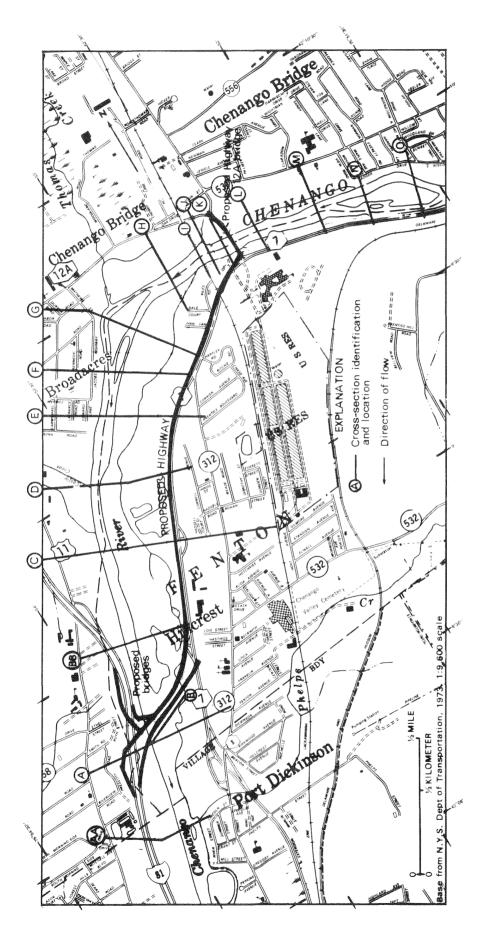
The 3.2-mile reach studied lies between Chenango Bridge and Port Dickinson (fig. 1). The drainage area at the downstream (south) end of the study reach is 1,593 square miles. The area is suburban with transportation facilities along the left (east) bank. Much of the area is on high ground and not subject to flooding, but the low-lying areas in the broad flood plain are flood prone.

The channel is fairly straight upstream from the two bridges at the north end of the study reach--the Erie-Lackawanna Railroad bridge and the State Highway 12A bridge (fig. 2). Downstream from the railroad bridge, the channel is straight for about 0.4 mile, then bends 50° to the left at the mouth of Thomas Creek, and then continues nearly straight through the remainder of the reach. About 0.4 mile downstream from Thomas Creek, Castle Creek enters the Chenango River from the right bank.

The low left bank, the principal flood plain, is lined with trees. During the growing season, the ground beyond the trees is covered with tall grass and light brush at the upper end of the reach and heavier brush at the lower end. The right bank is flat near the river but within a few feet rises steeply, except in the Broadacres area. Both banks are steep near the Highway 12A bridge.

The proposed highway (fig. 2) will be on the east side of the river and will replace or be adjacent to State Highway 7. Dual bridges will cross the river at an angle of about 35° to the Chenango River about 1,400 ft north of the Port Dickinson village boundary. A new Highway 12A bridge the same length as the present one is proposed just upstream from the present one.

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Peak water-surface elevations and discharges at cross sections are given in tables 1 and 2. Figure 2.--Location of proposed highway.

HYDROLOGIC ANALYSES

Records of flood stages and discharges at gaging station 01512500 on Chenango River, 1.2 miles downstream from the village of Chenango Forks (fig. 1) and 6 miles upstream from the reach studied, have been collected by the Geological Survey since November 1912; the records for each year are published annually. The largest known flood since November 1912 occurred on July 8, 1935, when a peak discharge of 96,000 ft³/s was recorded.

Flood Frequency

The discharge-frequency relationship at a streamflow site is generally expressed in terms of recurrence interval or exceedance probability. (Recurrence interval is the average time interval between actual occurrences of a flood of equal or greater magnitude; exceedance probability, the reciprocal of recurrence interval, is the probability that a flood of specified magnitude will be equaled or exceeded in any one year.) The floods selected for this analysis are the 50- and 100-year floods.

The discharge-frequency relationship for the gaging station near Chenango Forks was determined by the weighted averaging of estimates derived from a log-Pearson Type III analysis and regional regression equations. These estimates were applied to the reach studied. A 63-year period of record (1913-1975) of annual peaks recorded at the gage were used in the log-Pearson analysis. The regional regression equations and weighted-averaging technique were those given by Zembrzuski and Dunn (1979).

Peak discharges of the 50- and 100-year floods in the study reach were computed to be 55,200 ft³/s and 63,000 ft³/s, respectively. These discharges are in agreement with those reported in the flood-insurance studies completed for the towns of Chenango and Fenton (Federal Emergency Management Agency, 1980a and 1980b). The value for 100-year flood stage and discharge in the study area differs from that given in previous reports (Dunn, 1972 and 1974, and Dunn and Lumia, 1977) because newer methods were used for estimation of flood frequencies.

HYDRAULIC ANALYSES

Hydraulic characteristics of the entire reach were analyzed to provide water-surface profiles of the 50- and 100-year floods for the present channel and its proposed modification.

Near the proposed bridge system north of the Port Dickinson village boundary, the highway will encroach on the flood plain between section AA and A (fig. 2) on the west side of the river and near section BB on the east side.

Water-surface profiles were developed by U.S. Geological Survey E431 and J635 step-backwater computer programs (Shearman, 1976 and Shearman, written commun., 1977). Starting water-surface elevations were obtained from the flood-insurance studies for the towns of Chenango and Fenton (Federal Emergency Management Agency, 1980a and 1980c). Results are presented in tables 1 and 2.

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		n a gana ang ang ang ang ang ang ang ang	er	Proposed 1,000)-ft bridge and Highway 12A	Proposed 1,800)-ft bridge and Highway 12A
		Present co	onditions		placement ² /		placement ² /
		Water-surface	Mean velocity	Water-surface	Mean velocity	Water-surface	Mean velocity
Sectio	<u>n1/</u>	elevation (ft)	(ft/s)	elevation (ft)	(ft/s)	elevation (ft)	(ft/s)
AA		850.7	3.3	850.7	3.3	850.7	3.3
А		851.2	3.9	851.2	4.5	851.2	4.5
В		10000 eF60	1000 GIGG	851.5	4.2	851.5	2.9
BB		851.7	3.0	851.8	3.4	851.7	3.2
С		852.3	4.6	852.4	4.6	852.3	4.6
D		853.2	3.6	853.2	3.7	853.2	3.8
Е		853.9	3.2	853.9	3.4	853.9	3.4
F		854.3	2.9	854.4	3.0	854.3	3.0
G		854.8	4.0	854.9	4.0	854.9	4.0
Н		855.9	4.7	856.0	4.7	855.9	4.7
I	Railroad bridge	856.5	8.0	856.5	8.0	856.5	8.0
J	0	857.0	6.5	857.0	6.4	857.0	6.5
K	Highway bridge	857.1	10.3	857.2	10.2	857.2	10.3
L	0-	859.2	5.1	859.1	5.1	859.1	5.2
М		859.9	4.9	859.8	4.9	859.8	5.0
N		860.6	5.3	860.5	5.3	860.5	5.3
0		860.9	4.9	860.9	4.9	860.9	4.9

Table 1.--Water-surface elevations and mean velocity of 50-year flood of Chenango River, near Fenton and Chenango, Broome County, N.Y.

 $\frac{1}{2}$

Locations are given in figure 2. Proposed replacement is identical to present bridge.

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Table 2.---Water-surface elevations and mean velocity of 100-year flood of Chenango River, near Fenton and Chenango, Broome County, N.Y.

	and for a first of the state of the	na na manana mangana na manana manana manana manana	Proposed 1,000-ft bridge	-ft bridge	Proposed 1,800-ft bridge	ft bridge
			at section B an	nd Highway, 12A	at section B and Highway	d Highway 12A
	Present conditi	nditions	bridge replacement2/	$lacement^2/$	bridge replacement 2^{7}	acement ²⁷
	Water-surface	Mean velocity	Water-surface	Mean velocity	Water-surface	Mean velocity
Section1/	elevation (ft)	(ft/s)	elevation (ft)	(ft/s)	elevation (ft)	(ft/s)
AA	852.3	က က	852.3		852.3	ຕ° ຕ
A	852.7	ۍ . س	852.7	4 . 4	852.7	4.4
В	Access		853.1	4.4	853.1	3.0
BB	853.2	3.0	853.4	3.5	853.3	о. с С
U	853.7	4.5	853.9	4 . 4	853.8	L4 a L4
Ω	854.5	າ ເ	854.7	3.6	854.6	3.6
۲J	855.1	3.1	855.2	3.2	855.2	3.2
Ы	855.5	2.8	855.6	2.9	855.6	2.9
9	856.0	4.0	856.1	4.0	856.0	4.0
Ш	856.9	4°1	857.0	4.7	856.9	4.7
I Railroad bridge	d 857.3	8.7	857.4	9°Q	857.4	8.7
5	857.9	6.7	858.0	6.7	857.9	6.7
K Highway bridge	858.1	10.9	858°2	10.8	858 • 1	10.8
L	860.5	5.1	860.4	5,1	860.4	5.1
M	861.1	5.0	861.0	5.0	861.0	5.0
N	861.7	5.6	861.6	5.6	861.6	5.6
0	862.1	5.1	862.0	5.1	862.0	5.1
			Annonem and the state of the st			

Locations are given in figure 2. $\frac{1}{2}$

Proposed replacement is identical to present bridge.

The maximum changes in water-surface elevation (in feet) that would result from the two bridge designs, in relation to the present condition, are as follows:

	50-year flood Bridge opening		100-year flood Bridge opening	
Reach	1000 ft	1800 ft	1000 ft	1800 ft
Below Highway 12A bridge Above Highway 12A bridge	+0.1	+0.1	+0.2 -0.1	+0.1 -0.1

SUMMARY

This report presents 50- and 100-year flood profiles that would result from a proposed highway along a reach of the Chenango River in the towns of Fenton and Chenango. The NYSDOT plan calls for replacement of the present State Highway 12A bridge, near the upstream end of the reach and construction of a dual bridge at the downstream end of the reach, 1,400 ft upstream from the Port Dickinson village boundary. Two alternate designs for the dual bridge near Port Dickinson are considered--one with a 1,000-foot opening and one with a 1,800-foot opening. Flood conditions that would result from each alternative are compared with those of the present river channel.

Results of the study are summarized as follows:

50-year flood.--The plan with either the 1,000-foot or the 1,800-foot bridge opening will increase the water-surface elevation of the 50-year flood by a maximum of 0.1 foot above present 50-year flood levels in the reach below the Highway 12A bridge. Upstream from the Highway 12A bridge, water-surface elevation of the 50-year flood will decrease by a maximum of 0.1 foot.

<u>100-year flood</u>.--The plan with the 1,000-foot bridge opening will increase the water-surface elevation of the 100-year flood by a maximum of 0.2 foot above present flood levels in the reach below the Highway 12A bridge. The plan with the 1,800-foot bridge opening will cause a maximum increase of 0.1 foot above present flood levels. Upstream from the Highway 12A bridge, water-surface elevation of the 100-year flood will decrease by a maximum of 0.1 foot regardless of which bridge design is used downstream.

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