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Description of seafloor sediment and preliminary
geo-environmental report, Shelikof Strait, Alaska

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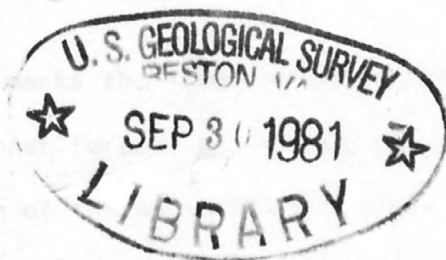
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INTRODUCTION

Shelikof Strait, situated between the Kodiak island group and the Alaska Peninsula (Fig. 1), is included in OCS oil and gas lease area 60. Environmental geologic studies are being conducted by the U.S. Geological Survey prior to the scheduled September 1981 sale date. Seismic-reflection records, collected with 40- to 95-cm³ airgun, 800-joule minisparker, 800-joule boomer, and 3.5- and 12-kilohertz systems and covering over 6,400 km of trackline have been examined to identify geologic conditions at or below the seafloor that might affect petroleum operations. Of the total trackline distance, 865 km were collected in June 1980 aboard the Geological Survey's ship R/V S.P. LEE. The remainder were collected by Nekton Inc. in 1979, under contract to the USGS (Fig. 2). Sediment samples were collected at 42 stations on the June 1980 cruise for geological and geotechnical analysis (Fig. 2).

The purpose of this report is to present physical and chemical measurements that have been made on sediment samples and to give a preliminary geo-environmental assessment of Shelikof Strait, based on presently completed analyses of the geophysical records and sediment samples.

SETTING

Shelikof Strait marks the location of a northeast-trending structural trough, forming an inner forearc basin (von Huene, 1979) that is located near the convergent margin of the North America plate where it is being underthrust by the Pacific plate. The major tectonic feature is a clearly defined Benioff zone, located at a depth of just less than 100 km beneath the strait (Pulpan and Kienle, 1979).

The Gulf of Alaska - Aleutian region, which includes sale area 60, is one of the most seismically active on earth and accounts for about 7 percent of the annual worldwide release of seismic energy; mostly in the form of large earthquakes (greater than magnitude 6). Since recording of large earthquakes began in 1902, at least 95 potentially destructive events ($M > 6$) have occurred in the vicinity of Shelikof Strait. Recurrence intervals of major earthquakes ($M > 7.5$) within a given area along the Gulf of Alaska - Aleutian system have been estimated to be between a maximum of 800 years (Plafker and Rubin, 1967) and a minimum of 33 years (Sykes, 1971).

At least 12 volcanoes classified as active (within historic time) or recently active ($< 10,000$ yr) are located along the Alaska Peninsula adjacent to the strait (Powers, 1958). The volcanoes are andesitic in composition and are subject to violent eruptions, as exemplified by the Katmai event of 1912, which expelled more than 25 km^3 of ash (Wilcox, 1959). The most recent eruption was that of Mt. Augustine in 1976 in nearby lower Cook Inlet.

Onshore geology and sparse deep seismic-reflection data indicate that many of the major geologic features of lower Cook Inlet extend into Shelikof Strait. These features include less than 2 km of Cenozoic and an undertermined thickness of Mesozoic strata, the Alaska - Aleutian Range batholith, and the Border Ranges fault (Magoon et al., 1979). Bedrock within the strait is covered by a blanket of relatively undeformed Quaternary glacial and marine sedimentary deposits.

BATHYMETRY

The bathymetry of Shelikof Strait is shown in Figure 3. The map was prepared by hand-picking depths from 3.5- and 12-kilohertz profiles along all

tracklines shown in Figure 2, correcting depths to mean lower low water, computer posting and contouring, and manually smoothing the final product.

The seafloor of Shelikof Strait consists of a gently southwest-sloping central platform bordered by narrow marginal channels adjacent to the Kodiak islands and the Alaska Peninsula. Water depths in the northeast part are generally less than 200 m whereas those in the southwest generally exceed 200 m and can be as much as 300 m. Superimposed on the platform are some local highs and lows with as much as 100 m relief. Along the axes of the marginal channels are several closed depressions of up to 100 m relief.

SHALLOW STRUCTURES

Figure 4 shows trends of shallow structures. Faults were identified in airgun, minisparker and uniboom records by the presence of offset strata and hyperbolic reflections. Only faults that disrupt sediment above bedrock were mapped, and distinction is made between those that intersect the seafloor and those that terminate below it. Fold axes were taken from the map prepared by Hoose and Whitney (1980).

Most major structures trend parallel to the axis of the strait, perpendicular to the direction of plate convergence. Faults that offset the seafloor or extend above bedrock into unconsolidated sediment occur along both margins of the strait. Faults in the central part of the strait cause as much as 100 m offset of the seafloor and produce horst and graben structures seen in some seismic reflection records (Fig. 5).

Shallow bedrock folds are asymmetric, with vergence toward the northwest on the Kodiak Island side of the strait and toward the southeast on the Alaska Peninsula side (Hoose and Whitney, 1980). Most folds are truncated at the unconformable contact with overlying unconsolidated sediment.

SEDIMENT

Stratigraphy: Sedimentary deposits of presumed Pleistocene and Holocene age overlie an irregular unconformity above Tertiary and older sedimentary bedrock. Thickness of unconsolidated sediment, measured from airgun, minisparker, and uniboom records, is generally about 100 ms of two-way acoustic penetration in the northeastern half of the study area and increases abruptly in the southwestern half to values exceeding 1000 ms (Fig. 6; see also Whitney et al., 1980 a,b). The thickening reflects a deepening of the unconformity. Interpretations of the seismic stratigraphy by Whitney et al. (1980 a,b), Hoose et al. (1980), and Holden (1980) reveal that the section above the unconformity comprises three sedimentary units: a lowermost (Pleistocene?) unit that fills the bedrock depression in the southwest half of the area and reaches thicknesses of more than 500 m, a lower Holocene unit generally about 100 m thick that overlies the unconformity in the northeast and the Pleistocene unit in the southwest, and an upper Holocene unit generally less than 20 m thick that covers most of the seafloor.

High-resolution seismic reflection records show that the platform area on the seafloor of Shelikof Strait represents the surface of a southwesterly prograding sediment body. This sediment body pinches out laterally across the strait to form the gently sloping seaward walls of the marginal channels (Fig. 7). The steep, landward channel walls appear to be fault scarps in some places, but more typically are the depositional surface of sediment derived from Pleistocene glaciers or the adjacent landmasses (Alaska Peninsula and Kodiak islands). Therefore, the channels are not erosional in origin but instead represent areas of little modern sediment accumulation. In fact, the overall sedimentary environment of Shelikof Strait apparently is depositional,

with no evidence of the erosion and large-scale reworking common nearby in Cook Inlet (Bouma et al., 1978) and on Kodiak Shelf (Hampton et al., 1979). Sedimentation reflects the dominantly barotropic flow of ocean water that enters the northeast end of the strait from Cook Inlet and the Gulf of Alaska (Schumacher et al., 1978; Muench and Schumacher, 1980).

Textures: Sedimentary textures were measured by sieving and pipetting into four size classes: coarse (>2 mm), sand ($2-0.062$ mm), silt ($0.062-0.004$ mm), and clay (<0.004 mm). Textures of surficial sediment grade uniformly down the strait from muddy sand at the northeast end to slightly sandy mud at the southwest end (Figs. 8,9), indicating progressive sorting by present-day transporting currents. A general fining across the strait, toward the southeast, exists in the southwestern half of the study area.

Index physical properties: Geotechnical index properties have been determined for many of the sediment cores. These include vane shear strength, sensitivity, water content, grain specific gravity, and plasticity (Atterberg limits) (Table 1).

Vane shear tests were performed with a motorized device at a rotation rate of $90^{\circ}/\text{min}$. The vane was $1/2$ inch diameter and $1/2$ inch high, inserted into the sediment to a depth twice the height of the vane.

Peak undisturbed strengths and remolded strengths were measured. On board ship, vane shear tests were performed at the ends of 1-m core sections immediately after recovery. The axis of vane rotation was parallel to the core axis in these tests. In the laboratory, within two weeks after termination of the cruise, core sections were split longitudinally and vane shear tests were performed at 20-cm intervals with the axis of vane rotation perpendicular to core axes. Replicate measurements were made on matching

halves of some cores. Some tests were performed using a torque cell to measure resistance to vane rotation; others were run using a spring. Peak vane shear strengths (S_u) generally increase toward the northeast (Fig. 10, Table 1), reflecting the increase in grain size. Most of the sediment can be classified as very soft ($S_u < 12$ kilopascals), but some is soft ($12\text{kPa} < S_u < 24\text{kPa}$) to medium ($24\text{kPa} < S_u < 48\text{kPa}$). These values are within typical ranges for shallow marine sediment (e.g., Keller, 1968, 1974).

S_u values ideally increase down core, reflecting an increase in effective stress and a decrease in water content. This is true for most cores in Shelikof Strait, except for cores at stations 530 and 550, where strengths decrease. This strength reduction down core may be due to cementation of the near-surface sediment or an internal fabric effect (e.g., Bennett et al., 1977).

Replicate vane tests made on matching core halves fall into two groups. In the first, the replicate tests were both made with the torque-cell apparatus, whereas in the second, one test was made with the torque cell and the other was made using a spring to measure resistance to vane rotation. Peak undisturbed strengths and remolded strengths were measured. The results are summarized in Table 2. Differences between replicate measurements are expressed as V , the coefficient of variation (difference between the two measurements, divided by the mean, expressed as a percent). As shown in the table, the range of V is large (0-113%), but the averages and standard deviations are moderate. The mean of all replicate torque-cell measurements is 24% for both peak undisturbed strengths and remolded strengths. Standard deviations are 20% and 22%, respectively. V -values for the torque-cell/spring replicate measurements have a grand mean of 22% for peak strengths and 26% for remolded strengths, with standard deviations of 16% and 26%, respectively.

Vane shear strength tests made at the ends of core sections measure strength along a vertical cylindrical surface within the sediment, whereas tests made on split core sections measure strength on a cylindrical surface whose axis is perpendicular to the core axis and contains planes in all directions from vertical to horizontal. Thus, end-core tests measure strength on planes that are of different orientation than those on which strength is measured in a split-core test. Some difference in end-core and split-core values might be expected, because strength can be anisotropic in sediments. Moreover, Bjerrum (1973) demonstrated an inverse relation between the magnitude of anisotropy (in a horizontal plane versus a vertical plane) and plasticity index using several different natural clays. In order to make a similar analysis of Shelikof Strait sediment, some adjustments of the data were made to account for the fact that end-core and split-core measurements were not taken at the same levels in cores. Namely, linear regression equations were derived for both the undisturbed and remolded split-core strengths as a function of water content for several cores with abundant vane strength data (Table 3). No anisotropy should exist for remolded samples, so the difference between the remolded end-core measurements and the corresponding split-core regression line was considered to represent the real deviation from linearity, reflecting variations within the sediment column that affect strength.

This difference, which also includes some experimental error, should be inherent in the undisturbed strength values, too, so the deviation computed for the remolded strength was subtracted from the corresponding undisturbed strength. Then, this corrected value was divided into the corresponding (equal water content) value on the undisturbed, split-core regression line to give a measure of anisotropy. As shown in Fig. 11, nearly all split-core

values exceed those from ends of cores, giving an anisotropy greater than one. No correlation with Bjerrum's (1973) experimental curve is evident, however.

Values of sensitivity, S , the ratio of undisturbed strength to remolded strength, fall in the low ($1 < S < 2$) to quick ($S > 16$) range (Terzaghi and Peck, 1948), with most being classified as medium sensitive ($2 < S < 4$) (Table 1). The coarser sediment in the northeastern area tends to have higher sensitivity values (Fig. 12, Table 1).

Water content (as a percentage of dry sediment weight) generally decreases to the northeast, inversely correlating with grain size (Fig. 13, Table 1). Moreover, water contents increase across the strait, from the Alaska Peninsula to Kodiak Island. Values in the northeast are perhaps low for marine sediment, but most are in the range of measurements taken elsewhere (Keller, 1968, 1974).

Atterberg limits describe the plasticity of sediment, in terms of the liquid limit (water content separating plastic and liquid behavior) and plastic limit (water content separating solid and plastic behavior). Useful derivatives are the plasticity index (difference between the liquid and plastic limits), and the liquidity index (position of the natural water content relative to the liquid and plastic limits). Certain trends in plasticity are evident in Shelikof Strait. Liquid limit, plastic limit, and plasticity index increase down the strait toward the southwest, and also generally across the strait, toward the southeast (Table 1, Figs. 14, 15, 16). These properties also generally increase with decreasing mean grain size (Figs. 17, 18, 19), although the data for plastic limit are quite scattered. Plastic limits are less variable than liquid limits, which is typically the case (Mitchell, 1976; Richards, 1962).

Correlations have been made between liquid limit (W_L) and compressibility (Herrmann et al., 1972; Skempton, 1944). The majority of Shelikof Strait samples fall within the medium ($30 < W_L < 50$) and high ($W_L > 50$) compressibility ranges.

All measured liquidity indices in Shelikof Strait are greater than 1 (Table 1) which is usual for near-seafloor marine sediment. Most cores show a decrease in liquidity index with depth, reflecting the decrease in water content. Sediment with a liquidity index greater than one behave as a liquid when remolded.

A plot of liquid limit versus plasticity index - termed a plasticity chart (Casagrande, 1948) - shows a trend parallel to the A-line that divides basic soil types (Fig. 20). Most sediments from Shelikof Strait plot below the A-line, which is typical of inorganic silts and silty clays. The linear trend of data points is expected for samples taken throughout the same sedimentary deposit (Terzaghi, 1955; Richards, 1962).

Other index properties obtained include grain specific gravity, bulk sediment density (assuming 100% saturation), void ratio, and porosity (Table 1). Sediment density decreases toward the southwest, whereas void ratio and porosity increase. Across the strait, toward the southeast, sediment density decreases, and void ratio and porosity increase. Grain specific gravity varies over a small range, with most values between 2.65 and 2.84. No trends are apparent. Typical variations with depth in cores are as follows: void ratio and porosity decrease, bulk sediment density increases, and grain density shows no trend.

Carbon: Dry-weight percentages of carbonate and organic carbon were measured for subsamples taken from the upper 2 to 3 cm of cores at 31

locations in Shelikof Strait (Figs. 21, 22). Carbon-carbonate analysis was performed on a LECO model WR-12 carbon determinator with induction furnace and acid digester. Subsamples were first freeze-dried, ground to a fine powder, and stored in a desiccator. Total carbon was measured using the induction furnace, and carbonate carbon was determined with the acid digester. Organic carbon content is calculated as the difference between total carbon and carbonate carbon contents. The reported values of organic carbon and carbonate carbon represent the average of 3 analyses from each core.

Surficial sediment of Shelikof Strait is characterized by low to intermediate contents of organic carbon, compared to other marine areas (Bordovskiy, 1965, 1969; Gardner, 1980; Lisitzin, 1972; Rashid and Brown, 1975). Values range from 0.10% to 3.16%, averaging 0.82%. Most values are between 0.40% and 1.50%.

Organic carbon content generally increases down the strait toward the southwest, as well as across the strait toward the southeast. These values vary inversely with grain size (Fig. 23). Correlations with other physical properties are shown in Figs. 24 through 28. Organic carbon content correlates positively with water content and plasticity index, whereas general inverse correlations are found with vane shear strength and sensitivity. Data are too scattered to define a correlation between organic carbon content and liquidity index. Correlations similar to those described above have been reported by others for low organic-carbon content sediments (Bordovskiy, 1965, 1969; Bush and Keller, 1981; Keller et al., 1979, Lisitzin, 1972; Mitchell, 1976; Odell et al., 1960).

Percent carbonate carbon is typically low in Shelikof Strait sediment, varying between 0.84% and 38.76% (average = 2.96%)(Fig. 22). Most values are

less than 3.50%. Two locations (535 and 553) with anomalously high values (21.67% and 38.76%, respectively) are near the boundary of the strait.

Clay mineralogy: Forty-four samples of surficial sediment were analyzed for clay mineralogy. Sample preparation and clay-mineral identification methods generally follow those presented by Hein et al. (1976). Samples were analyzed on a Picker high-angle x-ray diffractometer with a scintillation counter using nickel-filtered copper K α radiation. Carbonate and organic carbon were removed from sediment samples with Morgan's solution (sodium acetate and glacial acetic acid diluted with distilled water) and 30% hydrogen peroxide, respectively.

The <2 μ m size fraction was separated by centrifugation. This clay-size fraction was Mg-saturated and mounted on glass slides (Gibbs, 1965). The mounts were glycolated and then heat-treated at 500°C for one hour. An x-ray diffractogram ($2\theta = 3^\circ$ - 14°) was taken following each of the above treatments.

The semiquantitative technique of measuring peak areas was used to calculate the relative clay-mineral percentages. Biscaye's (1965) peak area weighting factors of two for chlorite-kaolinite, four for illite, and one for smectite were used in calculating relative percentages. Percentages of chlorite relative to kaolinite were obtained from a slow scan of the 24° - 26° 2θ diffractogram (Biscaye, 1964). Kaolinite was a minor component in these samples, making accurate determinations difficult. Biscaye's method showed no discernible kaolinite peak at 24.88° 2θ . The chlorite values presented here include any kaolinite that may have been present but was not measurable. Duplicate samples and duplicate sample runs showed reproducibility within 5%.

Illite and chlorite are the dominant clay minerals in Shelikof Strait, averaging 52% and 42%, respectively (Figs. 29,30; Table 4). Mixed layer clay (mostly smectite) occurrence is minor and averages 6% (Fig. 31). The major gradients in clay mineral abundances occur across the strait, perpendicular to the axis. At the northeast boundary of the strait, however, gradients tend to become oblique to the axis. The highest values of illite and the lowest values of chlorite generally occur along the axis. Mixed layer clays occur more abundantly on the southeastern side of the strait compared to the northwestern side, and most abundantly at the northeast end of the strait.

The flow that transports clay minerals into Shelikof Strait derives mainly from Cook Inlet and from the northeastern Gulf of Alaska (Muench and Schumacher, 1980). Clay mineral suites from these areas, as well as from nearby Kodiak Shelf, have been described by Hein et al. (1979). Average compositions of these suites, as well the average from Shelikof Strait, are presented in Table 5. The clay mineral suite in Shelikof Strait most closely resembles that from Cook Inlet, but some contribution from the northeastern Gulf (i.e., Copper River) surely is present.

The relative enrichment of chlorite and depletion of illite along the margins of the strait may represent contributions of clay minerals from the adjacent landmasses. Alternatively, the segregation might reflect hydraulic sorting processes (Gibbs, 1977; Knebel et al., 1977). Stratigraphic evidence (i.e., the non-depositional channels) suggests that the margins of the strait are hydrodynamically high-energy areas, implying that clay minerals with relatively low settling velocities would be depleted, which apparently is the case. Knebel et al. (1977) demonstrated that chlorite and kaolinite in San Francisco Bay sediment is coarser than illite, and that hydraulic sorting

on the basis of size exists. The distribution of mixed layer clays in Shelikof Strait, present in relatively small amounts and presumably finer grained than the other clays, shows a sorting trend, but it is not clearly compatible with that shown by the other clays. Mixed-layer clay distribution suggests a source from Kodiak Shelf.

Gas: Sediment samples at 15 stations were analysed for light hydrocarbon gases (methane through butane), by K. Kvenvolden and T. Vogel. In general, gas concentrations were low (Table 6). Methane was approximately 30 microliters/liter ($\mu\text{l/l}$) of wet sediment, ethane was about 100 nanoliters/liter (nl/l), propane was 100 nl/l , and ethane was 80 nl/l . Isobutane and n-butane were negligible.

One station showed anomalous gas concentrations. Sediment from station 539 exhibited large methane (1600 μ) and ethane (946 nl/l) concentrations. The sample was unusual, because the methane/ethane + propane ratio was high ($C_1/C_2 + C_3 = 1556$) indicating biogenic gas, and yet the ethane/ethene ratio was also high ($C_2/C_{2:1} \approx 16$), suggesting a thermogenic source. Ethene is normally the same concentration or greater than that of ethane in biogenic gases, but due to the low concentrations of the other saturated hydrocarbons (propane, iso-butane, and n-butane), the gas at station 539 can be assumed biogenic.

ACOUSTIC ANOMALIES

Anomalous acoustic signatures exist in many boomer and minisparker records. Typically, they appear as unusually strong reflections, with abrupt terminations, within the unconsolidated sediment section. Reflectors below the anomaly are commonly obscured. A few instances where all reflectors

beneath the seafloor are totally obscured, with no evidence of strong reflectors, were also found.

Anomalies occur most commonly in the northeastern half of the strait, but some also exist in the southwest (Fig. 32). Many anomalies occur over steeply dipping bedrock strata and anticlinal crests that have been truncated by erosion (Fig. 33).

Acoustic anomalies are not all easy to distinguish, because a continuous gradation exists from normal acoustic returns, through subtle deviations from normal, to distinct anomalies. Instrument settings, such as filter frequencies and gain modes (TVG versus AGC), have an influence on the appearance of anomalies. It is commonly a matter of judgment what to identify as a true acoustic anomaly. Only distinct anomalies are mapped on Fig. 32.

Acoustic anomalies have been shown in other areas to be caused by gas charging (Nelson et al., 1978; Whelan et al., 1976; Schubel, 1974). A similar causative relationship has not been confirmed in Shelikof Strait, but it cannot be discounted. The occurrence of some anomalies over truncated anticlines and steeply inclined bedrock strata is consistent with an origin due to migrated gas, but the absence of significant concentrations of gas in cores and of water-column gas seeps in the seismic records argues against it, unless, of course, the gas is completely trapped and cannot leak to the surface. Alternatively, the anomalies may be due to change in lithology along stratigraphic horizons.

CRATERS

Seafloor craters occur over an area of approximately 1500 km² on the progradational platform in Shelikof Strait (Fig. 34). The craters appear on

seismic reflection profiles as small indentations, typically 50 m in diameter and less than 5 m deep (Fig. 35). Broad, low relief rims about 1 m high can be detected on some. In side-scanning sonar records, the craters are subtle features and circular in plan (P.J. Hoose, personal communication). The craters are similar in appearance to those found on the Scotian Shelf by King and MacLean (1970). Disruption of seismic reflectors cannot be detected beneath most craters. Moreover, nearly all craters occur on the present-day seafloor. Only a few examples of buried craters were found (Figs. 34 and 35), and most of these occur within a subbottom depth of 25 m.

Origin of the craters is unknown, but one possibility is venting of either gas or buried, liquefied sediment. The lack of disruption of seismic reflectors suggests a shallow source; less than a few meters. Gas venting is believed to cause craters in other places, such as in Norton Sound where a buried Pleistocene peaty mud is the source of gas (Nelson et al., 1979). No evidence of an organic-rich layer was detected in Shelikof Strait cores, and as mentioned above, measured contents of hydrocarbon gases are low. Furthermore, the location of acoustic anomalies, which are also believed typically to be related to gas (Nelson et al., 1978; Whelan et al., 1976; Schubel, 1974), are almost mutually exclusive of the locations of craters in Shelikof Strait.

There is an interesting correlation of the occurrence of craters with the subsurface extent of the thick Pleistocene(?) unit of Whitney et al. (1980a,b). The two are nearly coincident. But if the two features were related, some disturbance of the intervening 100 m or so of unconsolidated sediment would be expected, which is not the case.

Alternatively, craters might be formed by collapse or venting of buried liquefied sediment. In particular, a layer of Katmai ash blankets most of the strait and was encountered in many cores. At nearly all locations within the crater field, penetration of the gravity core was stopped at subbottom depths of less than 35 cm. Dart coring at one locality revealed a dense layer of ash about 15 cm thick at this depth. Perhaps this material and other ash layers were originally deposited in a loose state and have liquefied after burial, although this process does not account for the relief of the craters, which is much greater than the thickness of ash recovered in cores.

Liquefaction, if it has occurred, could have been caused by a severe earthquake such as the one in 1964. On the other hand, the area is too deep for storm-wave loading to cause liquefaction (e.g., Hampton et al., 1978).

SEDIMENT SLIDES

Examination of seismic reflection records shows that the seafloor of Shelikof Strait is nearly devoid of sediment slides. Only one instance of a slide mass was found (Figs. 4, 36), and it was derived from an adjacent fault scarp. The slide mass extends for about 100 m along one trackline and is less than 10 m thick.

Although most of the seafloor is flat, several steep slopes exist in Shelikof Strait. Namely, the landward walls of the marginal channels and the large-offset fault scarps in the central part of the strait have declivities that commonly exceed the resolving capability of the seismic reflection system (about 15°) and may locally approach vertical. Evidently, the sediment underlying these slopes is generally strong enough to resist the downslope driving forces of gravity and earthquake accelerations.

ENVIRONMENTAL ASSESSMENT

The tectonic setting of Shelikof Strait, near the convergent margin of two major lithospheric plates, makes it subject to large earthquakes. The minimum recurrence interval of 33 years for a major earthquake that could affect the entire region might be exceeded by the lifetime of an oil-producing province, because the last major event was in 1964. So, although earthquakes cannot be predicted with confidence, seismic hazards are a valid concern for offshore development. Strong ground shaking, fault rupture, sediment displacement, and tectonic deformation have all been documented in nearby areas. Examination of the distribution of historic epicenters shows no areal concentrations (H. Pulpan, Univ. Alaska, personal communication), such as exist nearby on Kodiak Shelf (Hampton et al., 1979), that would imply some areas are more susceptible to local seismic affects than others.

Violent volcanic explosions are also associated with the tectonic setting, and eruptions from the volcanoes on the Alaska Peninsula could cause problems such as substantial ash accumulations and acid rains. More destructive but local effects such as hot ash flows are not likely in most parts of the strait.

The faults in Shelikof Strait that offset the seafloor imply recent activity and the probability of more to come. The seafloor offset (100 m) of some faults in the central part of the strait implies major movement in recent times. The short extent, irregular shape, and horst-like appearance of these faults suggest that perhaps they are caused by forces associated with localized uplift rather than being a direct result of regional compression.

The sedimentary environment of Shelikof Strait is depositional, with sandy material presently being deposited to the northeast and progressively

finer material accumulating to the southwest. Problems associated with scour or movement of large bedforms, a significant concern on Kodiak Shelf and in lower Cook Inlet, should not exist in Shelikof Strait. Accumulation of fine sediment does raise the possibility of pollutant storage on the seafloor, though. Pollutants introduced within the strait itself or in more diluted form from lower Cook Inlet and the northeastern Gulf of Alaska could be stored as contaminants on fine particles.

Seafloor sediment in Shelikof Strait exhibits physical properties (vane shear strength, water content, plasticity) similar to those of marine sediment elsewhere. Measurements of physical properties are useful for categorizing the shallow sediment types in the strait, but deeper samples and more sophisticated testing would be necessary for engineering design purposes. A few high values of sensitivity and compressibility were obtained, but most measurements of physical properties are in normal ranges for shallow marine sediment, and no unusual geotechnical problems are indicated. Deeper unconsolidated sediment apparently is stable, coarse-grained glacial debris. Geotechnical triaxial and consolidation testing now underway will give more detailed strength and consolidation information than is now available for the uppermost sedimentary units.

Sediment slides are uncommon in the strait; only one occurrence is known. Nevertheless, the steep slopes along fault scarps and also along the landward side of the marginal channels must be regarded as possible sites of local instability.

Indirect evidence for gas-charged sediment, in the form of acoustic anomalies, is especially common in the northeast part of the strait and warns that weak and unstable sediment, as well as high gas pressures, might be

present in the shallow subsurface. Low gas contents in cores (except one) and the absence of seeps from the seafloor, however, are inconsistent with the hypothesis of widespread gas-charged sediment.

The seafloor craters in the southwest area might also indicate the presence of gas-charged sediment, although the locations of craters is nearly exclusive of the locations of acoustic anomalies, which argues against this. A more likely explanation for the craters is sediment venting due to liquefaction. A source at depths of less than about 10 meters below the seafloor is likely for the liquefied layer, and therefore the venting may represent only a minor environmental concern.

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Table 1. Physical properties of sediment cores.

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk			Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay	density (gm/cm ³)		Void ratio	Porosity (%)	undisturbed		sensitized remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-ity index	
508	57°21.01'N	155°36.41'W	270	0	0	1	34	65	8.6												
				13	0	3	47	50	7.9	104.2	1.46	2.65	72.8	2.80	3.1	0.8	3.8	69	27	42	1.84
				21						106.2	1.48	2.92	74.5	2.81	5.0*	2.6*	1.9				
				35						105.1	1.48	2.89	74.3	2.81	4.9	0.9	5.4				
				55	0	2	44	54	8.0	88.9	1.55	2.47	71.2	2.84	8.2	2.1	4.0	70	40	30	1.63
				68											5.4	1.6	3.3				
				75						85.2	1.57	2.39	70.5	2.87	9.0	2.6	3.4				
				90											16.5	4.3	3.8				
				95						81.0	1.59	2.26	69.3	2.85	13.1	4.8	2.7				
				110	0	4	40	55	8.0	85.9	1.57	2.44	70.9	2.90	9.0	2.6	3.5	69	38	31	1.55
				121						66.4	1.64	1.76	63.8	2.71	4.2*	2.0*	2.0				
				130						82.9	1.58	2.33	70.0	2.88	11.6	4.0	2.9				
				153						87.6	1.56	2.49	71.4	2.91	10.8	3.9	2.8				
				170	tr	7	38	55	7.9	77.2	1.60	2.14	68.2	2.84	15.7	4.2	3.7	67	43	24	1.43
				190						81.6	1.58	2.24	69.1	2.81	11.4	3.2	3.6				
				210						66.7	1.66	1.86	65.0	2.85	11.1	4.0	2.8				
				213	0	21	35	44	6.8									51	30	21	
				221						55.7	1.74	1.56	60.9	2.86	9.0*	5.2*	1.8				

Table 1 continued

			Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
Latitude	Longitude	Water depth (m)		coarse	sand	silt	clay							undisturbed	sensitized	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid- plasticity index	
509	57°21.19'N	225	0	0	tr	34	66	8.6												
	155°08.66'W		5	0	1	42	57	8.2								83	45	38		
			12	0	1	45	54	8.1	123.8	1.42	3.34	77.0	2.76	3.5	0.9	3.9				
			30						111.8	1.46	3.06	75.4	2.80	4.9	1.8	2.7				
			48						121.3	1.44	3.33	76.9	2.81	4.1	2.5	1.7				
			70						120.6	1.44	3.35	77.0	2.84	4.0	1.6	2.4				
			90	0	2	43	55	8.1	113.5	1.45	3.05	75.3	2.75	4.9	1.6	3.0	46	26	20	4.73
			111						115.3	1.46	3.18	76.1	2.83	4.9	1.6	3.0				
			132	0	1	40	59	8.3	104.7	1.49	2.92	74.5	2.85	7.2	1.7	4.2	85	45	40	1.49
			152						100.6	1.51	2.82	73.8	2.87	10.8	3.4	3.2				
			172	0	1	42	57	8.2	96.6	1.52	2.68	72.9	2.84	11.5	3.5	3.3	78	45	33	1.56
			192						94.8	1.52	2.62	72.4	2.83	10.0	3.3	3.0				
			212	0	tr	38	62	8.5	98.2	1.49	2.74	73.3	2.77	8.5	2.6	3.3	82	41	41	1.40
510	57°39.22'N	305	0	0	2	41	57	8.2												
	155°17.18'W		15	0	3	48	49	7.8	119.2	1.44	3.23	76.4	2.77	4.0*	2.2*	1.8				
			30	0	2	48	50	7.9	107.7	1.47	2.89	74.3	2.74	3.1	1.2	2.7	70	34	36	2.05
			37	0	4	54	42	7.3									69	41	28	
			50						89.7	1.51	2.30	69.7	2.62	5.8	1.4	4.2				
			70						101.0	1.50	2.83	73.9	2.86	5.7	1.9	3.0				
			90	0	2	45	53	8.0	96.4	1.51	2.62	72.4	2.78	4.9	1.8	2.7	69	42	27	2.01
			107	0	2	45	53	8.0	98.8	1.51	2.75	73.3	2.84	7.9	2.2	3.6				
			115						87.9	1.55	2.45	71.0	2.85	5.0*	2.0*	2.5				
			125						88.8	1.55	2.46	71.1	2.83	9.3	3.3	2.8				
			145	0	2	46	52	8.0	96.5	1.44	3.48	77.7	2.89	7.2	2.2	3.2	74	41	33	1.68
			165						87.3	1.56	2.46	71.1	2.88	8.8	4.8	1.8				
			185	0	3	48	49	7.8	87.3	1.55	2.41	70.6	2.82	9.4	3.5	2.7				
			200	0	3	46	51	7.9									69	36	33	
			205						68.5	1.63	1.81	64.8	2.75	15.5	4.4	3.5				
			215						81.9	1.57	2.22	68.9	2.77	7.8*	3.6*	2.1				

Table 1 continued

Station	Latitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm^3)	Void ratio	Porosity (%)	Grain Vane shear strength (kPa)				Atterberg limits				
				coarse	sand	silt	clay						specific gravity	undisturbed	sensitivity	remolded	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-ity index	
511	57°39.08'N 154°50.14'W	214	0	0	1	33	66	8.6													
			15	0	1	44	55	8.2	109.5	1.45	2.89	74.3	2.88	2.6	1.4	1.9	74	38	36	1.99	
			35						113.8	1.48	3.11	75.7	2.89	3.3	1.7	1.9					
			65						105.7	1.47	2.82	73.8	2.73	4.5	1.6	2.8					
			85	0	1	46	53	8.1	103.1	1.48	2.73	73.2	2.71	6.2	2.1	3.0					
			93	0	1	46	53	8.1										76	42	34	
			105						101.2	1.51	2.87	74.2	2.90	6.8	2.8	2.4					
			125						99.5	1.52	2.83	73.9	2.91	9.7	3.1	3.1					
			145	0	1	45	54	8.1	91.9	1.55	2.62	72.4	2.92	9.4	3.4	2.8	69	21	48	1.48	
			165						95.1	1.52	2.64	72.5	2.84	9.9	3.3	3.0					
			190						86.2	1.54	2.28	69.5	2.70	10.6	3.4	3.1					
			210	0	1	44	55	8.2	84.7	1.57	2.38	70.5	2.88	13.5	4.9	2.7	70	44	26	1.57	
			230						86.9	1.56	2.41	70.7	2.84	11.0	4.8	2.5					
512	57°52.5'N 154°14.9'W	195	0	0	tr	80	20	6.8													
			13	0	tr	52	48	7.9	103.9	1.46	2.65	72.6	2.81	6.2	1.4	4.4	71	41	30	2.04	
513	57°54.8'N 154°19.8'W	205	0	0	2	46	52	8.0													
			12	0	3	43	54	8.0	96.2	1.51	2.61	72.3	2.77	3.2	1.2	2.8	67	37	30	1.97	
514	57°55.3'N 154°25.0'W	222	0	0	3	51	46	7.7													
			22	0	5	52	43	7.5									63	36	27		
			28	0	4	52	44	7.6	89.7	1.55	2.50	71.4	2.85	4.0	1.6	2.4					
515	57°59.0'N 154°27.3'W	238	0	1	4	62	33	7.1													
			74						61.5	1.65	1.59	61.4	2	65	5.2*	2.4*	2.1				
516	58°09.3'N 154°10.6'W	295	0	0	3	56	41	7.5													
			30						87.1	1.52	2.26	69.3	2.65	3.6	2.6	1.4					

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay							undisturbed	sensitized remolded	liquidity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquidity index
517	57°55.3'N	154°00.9'W	180	0	0	1	38	61	8.4												
				15	0	1	52	47	7.8	111.5	1.46	3.04	75.2	2.78	4.9	1.2	4.2	72	39	33	2.20
518	58°00.3'N	153°51.6'W	180	0	0	1	37	62	8.4												
				15	0	2	49	48	7.8	103.8	1.47	2.71	73.1	2.67	5.4	1.8	3.0				
				28						87.3	1.51	2.18	68.6	2.56	4.0	1.3	3.0				
519	58°05.5'N	154°01.3'W	200	0	0	3	46	51	7.9												
				15	0	6	52	42	7.4	114.2	1.44	3.01	75.0	2.69	4.1	0.7	5.6	65	39	26	2.89
520	58°13.2'N	153°56.2'W	213	0	0	6	46	48	7.6												
				9											3.4	0.7	4.6				
				12						115.4											
				15	0	9	52	39	7.2	95.1	1.50	2.51	71.5	2.70	3.2	0.2	19.5	58	34	24	2.55
				22											2.9	0.6	5.0				
				27											4.9	1.2	4.2				
				35						89.2	1.54	2.40	70.6	2.76				57	34	23	2.40
521	58°07.93'N	151°45.93'W	179	0	0	1	40	59	8.3												
				12	0	4	49	47	7.7												
522	58°05.5'N	151°41.4'W	185	0	0	1	37	62	8.4												
				6	0	2	49	49	7.9	126.4	1.40	1.21	76.1	2.60	3.1	1.6	1.9	86	45	41	1.99
523	58°01.2'N	151°34.2'W	189	0						44.3	1.82	1.20	54.8	2.78	9.8*	1.6*	6.0				
				109						40.7	1.87	1.12	52.8	2.81	10.2*	1.4*	7.8				
				219						44.1	1.83	1.21	54.7	2.80	10.8*	1.2*	3.3				
				276						43.6	1.85	1.22	55.0	2.87	9.8*	2.6*	3.7				

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (Weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk			Grain Vane shear strength (kPa)			Atterberg limits				
					coarse	sand	silt	clay			density (gm/cm ³)	Void ratio	Porosity (%)	specific gravity	undisturbed	sensitive remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-plasticity index
524	58°15.94'N	153°41.87'W	175	0	0	14	51	35	6.8												
525	58°23.7'N	153°37.2'W	158	0	0	43	31	27	5.2												
			15					45.7	1.80	1.24	55.3	2.77	9.5	1.6	5.8						
			35					45.0	1.82	1.23	55.2	2.80	23.5	5.4	4.4						
			55	0	33	42	25	5.5	43.8	1.82	1.19	54.2	2.77	31.3	5.6	5.6	40	28	12	1.32	
			85					40.5	1.86	1.10	52.3	2.77	27.8	6.6	4.2						
			100					53.9	1.77	1.38	58.0	2.79	17.1	3.3	5.2						
			125	0	22	44	34	6.4	56.3	1.73	1.56	60.9	2.83	11.5	3.2	3.6	43	27	16	1.83	
			145					43.0	1.85	1.18	54.2	2.82	20.2	3.9	5.2						
			165	0	60	21	19	4.0	35.1	1.92	0.95	48.8	2.78	35.7	8.3	4.3	35	25	10	1.01	
526	58°29.0'N	153°27.1'W	138	0	0	48	31	21	4.7												
			20					49.6	1.78	1.36	57.6	2.80	7.1	2.0	3.6						
			40					46.4	1.80	1.27	55.9	2.79	11.5	3.3	3.5						
			65	0	30	45	25	5.6	45.3	1.81	1.23	55.1	2.77	7.6	2.3	3.3					
			77											8.0*	2.6*	3.0					
			85					38.6	1.85	1.08	51.9	2.75	10.7	2.6	4.1						
			100					47.4	1.83	1.23	55.1	2.81	14.8	3.3	4.4						
			125	0	33	41	26	5.6	51.1	1.80	1.29	56.3	2.80	5.9	1.7	3.4					
			129	0	25	43	32	6.1									43	27	16		
			145					49.1	1.72	1.55	60.7	2.80	18.5	4.9	3.8						
			165					41.7	1.81	1.28	56.1	2.82	11.0	3.0	3.7						
177	0	11	69	20	5.6		1.70	1.27	55.9	2.73	9.2*			35	23	12					

Table 1 continued

Station	Latitude	Water	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk			Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
				coarse	sand	silt	clay			density (gm/cm ³)	Void ratio	Porosity (%)		undist- urbed	sensi- remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid- ity index
527	58°34.2'N 153°17.6'W	153	0	0	56	23	21	4.3												
			15**	11	42	30	17	3.9	36.8	1.90	1.00	50.0	2.78	16.4	4.9	3.4	34	22	12	1.23
			23						37.7	1.88	1.01	50.2	2.74	13.0*	1.8*	7.2				
			35						33.1	1.95	0.90	47.3	2.77	19.4	4.9	3.9				
			55						32.4	1.94	0.87	46.4	2.74	8.6	2.1	4.2				
			58						34.4	1.92	0.92	48.0	2.74							
			70**	11	69	11	9	2.4	31.5	1.95	0.84	45.6	2.73	15.2	3.3	4.6	20			
			95						38.0	1.89	1.03	50.8	2.79	26.7	6.6	4.1				
			115**	13	50	20	17	3.3	36.3	1.86	0.94	48.4	2.65	16.1	3.7	4.3	29	23	6	2.22
			123						23.3	2.07	0.62	38.3	2.72	19.8*	3.2*	6.0				
528	58°39.4'N 153°0.7'W	159	0	8	33	30	29	5.0												
			15	1	37	38	24	5.2	40.6	1.84	1.08	52.0	2.73	21.7	4.2	5.2	35	23	12	1.47
			35						53.5	1.73	1.44	59.0	2.75	15.6						
			52						47.8	1.79	1.30	56.5	2.78	11.6*	2.8*	4.2				
			62						43.8	1.84	1.20	54.8	2.81	16.6	5.0	3.3				
			82	tr	43	30	27	5.2	49.0	1.75	1.28	56.2	2.68	11.4	1.6	7.0	38	26	12	1.92
			94						38.2	1.87	1.01	50.4	2.72	15.6	3.1	5.0				
			119						44.2	1.80	1.17	54.0	2.71	22.2	6.6	3.4				
			146	tr	30	35	35	6.0	54.0	1.72	1.43	58.9	2.71	15.7	5.7	2.8	39	24	15	2.00
			152						46.6	1.78	1.23	55.1	2.70	17.0*	5.0*	2.9				
			175						47.1	1.78	1.25	55.6	2.72	17.2	4.5	3.8				
			190						51.5	1.73	1.43	58.9	2.74	16.3	3.9	4.2				
			219	3	46	30	31	5.4	52.0	1.73	1.38	57.9	2.71	16.6	4.5	3.7	36	31	5	4.20
			234						47.8	1.79	1.31	56.7	2.80	15.6	4.0	3.9				
			252						48.4	1.80	1.34	57.2	2.83	16.2*	1.6*	9.8				

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay							undisturbed	sensit- remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-ity index
529	58°44.4'N 152°57.4'W	136	0	0	39	29	32	5.5													
			15	0	27	41	32	6.1			1.85	1.01	50.3	2.68							
			55	4	71	16	9	2.8			1.85	1.01	50.3	2.68							
			60							38.4					11.6*	3.4*	3.4				
			110							27.9	1.99	0.74	42.5	2.71	14.2*	4.0*	3.6				
			200												19.6*	3.2*	6.3				
530**	58°49.7'N 152°47.6'W	165	0	1	76	10	13	3.0													
			15	tr	68	16	16	3.6	41.1		1.83	1.08	52.0	2.70	12.4	3.1	3.9				
			35	tr	77	11	12	3.0	42.3		1.79	1.09	52.1	2.63	10.2	1.3	7.8				
			40												4.2*						
			47								1.75	1.26	55.7	2.67	4.2*						
531	58°54.9'N 152°37.3'W	161	0	4	87	3	6	2.0													
									41.9						16.2	3.1	5.2				
532	58°45.85'N 152°27.98'W	195	0	54	44	tr	2	-0.2													
533	58°50.4'N 152°23.9'W	120	0	100	0	0	0	-2.0													
			15												6.0	2.1	2.9				
534	58°39.6'N 152°47.1'W	185	0	0	37	41	22	5.2													
			15	0	47	24	29	5.0	49.7		1.76	1.33	57.2	2.75	19.6	3.5	5.5	44	29	15	1.38
			35						41.0		1.83	1.08	51.9	2.69	19.1	4.2	4.5				
			49	0	68	15	17	3.6										38	32	6	
			60	tr	60	18	22	4.2	45.6						30.1	7.2	4.2	41	30	11	
			83						58.1		1.65	1.44	59.0	2.54	23.8*	2.4*	10.4				

Table 1 continued

Station	Latitude	Water	Depth in core (cm)	Grain size (weight percent)				Mean grain size φ	Water content (%)	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
				coarse	sand	silt	clay							undist- urbed	sensi- remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid- ity index
535	58°37.0'N	98	0	5	89	2	4	1.8												
	152°42.0'W		15	0	0	56	44	7.8	39.4	1.51	2.61	72.3	2.76	14.2	1.8	7.9				
536	58°31.4'N	190	0	0	17	35	48	7.2												
	152°52.6'W		15	0	13	44	43	7.1	77.5	1.57	2.02	66.8	2.66	11.3	2.3	4.9	68	43	25	1.38
			30						82.9	1.58	2.33	70.0	2.88							
			35											9.7	2.8	3.5				
			40						76.5	1.59	2.06	67.3	2.75	7.4*	2.4*	3.0				
			55						77.1	1.60	2.13	68.0	2.82	9.9	2.1	4.8				
			75						66.2					10.4	2.6	3.9				
			91	1	35	27	37	5.8	69.7	1.63	1.88	65.3	2.76	7.1	2.2	3.2	48	31	17	2.28
			111						49.2	1.76	1.31	56.8	2.73	13.9	3.2	4.3				
			129						43.9	1.83	1.21	54.7	2.81	10.6	2.1	5.2				
			140						39.0	1.87	1.07	51.6	2.78	6.0*	2.6*	2.3				
			150						41.5	1.86	1.15	53.4	2.81	16.4	4.9	3.3				
			170	0	11	45	44	7.3	44.2					11.9	3.0	3.9	37	23	14	1.51
			190						48.6					4.5	1.6	2.8				
			210						48.2					9.0	2.9	3.1				
			240						51.3					11.6*	3.2*	3.6				

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (Weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk			Grain Vane shear strength (kPa)				Atterberg limits				
					coarse	sand	silt	clay			density (gm/cm ³)	Void ratio	Porosity (%)	specific gravity	undisturbed		sensitized remolded	tivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-plasticity index
537	58°29.0'N	153°07.6'W	160	0	0	23	36	41	6.6													
				20	0	14	44	43	7.2	67.6	1.66	1.88	65.2	2.84	9.0	2.6	3.4	57	34	23	1.46	
				40						64.5	1.67	1.77	63.9	2.81	15.8	4.7	3.4					
				60						63.5	1.67	1.74	63.5	2.80	17.6	4.8	3.7					
				75	0	18	38	45	7.0						17.1	4.7	3.6	56	30	26		
				85						64.7	1.67	1.77	63.9	2.80	14.6*	3.2*	4.5					
				100						59.4	1.69	1.61	61.6	2.77	27.0	6.8	4.0					
				120						71.2	1.63	1.97	66.3	2.83	27.8	7.5	3.7					
				139	0	37	32	31	5.6	55.1	1.72	1.48	59.7	2.75	22.2	5.5	4.0					
				157						53.8	1.73	1.45	59.1	2.75	22.1	6.1	3.6					
				176						53.5	1.74	1.44	59.1	2.76	25.4	6.3	4.0					
				185						54.7	1.72	1.46	59.3	2.73	18.2*	4.2*	4.4					
538	58°25.2'N	153°00.2'W	190	0	0	18	35	47	7.1													
				15	0	46	24	30	5.1	87.9	1.54	2.44	70.9	2.79	7.3	2.1	3.6	70	32	38	1.47	
				24						88.9	1.54	2.41	70.7	2.77	13.2*	3.2*	4.0					
				35						86.9	1.55	2.36	70.3	2.78	9.9	3.3	3.0					
				55						79.2	1.58	2.15	68.2	2.77	13.9	3.4	4.1					
				75	0	7	42	51	7.7	86.4	1.55	2.36	70.2	2.79	9.1	2.4	3.8	70	41	29	1.57	
				95						79.8	1.59	2.20	68.8	2.82	14.9	4.0	3.7					
				115						63.2	1.69	1.77	64.0	2.87	25.9	6.7	3.9					
				124						63.1	1.67	1.71	63.1	2.77	23.0*	5.8*	4.0					
				135	0	18	38	44	7.0	70.2	1.62	1.89	65.4	2.75	15.8	4.2	3.8	60	31	29	1.35	
				155						55.0	1.73	1.49	59.9	2.78	29.2	8.9	3.3					
				175						68.4	1.56	2.33	69.9	2.82	22.2	5.9	3.7					
				195	0	26	38	35	6.2	55.9	1.72	1.51	60.2	2.77	24.6	5.0	4.9	48	29	19	1.42	
				205						65.1	1.66	1.77	63.9	2.78	17.0	6.4	2.6					
				224						61.1	1.69	1.65	62.2	2.79	16.4*	5.8*	2.9					

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay							undisturbed	sensitive remolded	tensitivity	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-plasticity index
539	58°21.3'N	153°12.4'W	175	0	0	9	36	55	7.8												
				15	0	4	47	49	7.8												
				60						89.7	1.54	2.47	71.2	2.82	9.8*	3.2*	3.1				
				65	0	3	42	55	8.1												
				110						150.8	1.37	4.18	80.7	2.83	7.2*	4.0*	3.3				
				135						89.5	1.54	2.46	71.1	2.81	10.2*	3.2*	3.1				
540	58°21.5'N	153°07.6'W	210	0	0	20	45	35	6.5												
				15	0	20	35	45	6.9												
				60						76.9	1.58	2.01	66.8	2.68	13.6*	2.8*	4.8				
				110						79.2	1.58	2.15	68.3	2.78	14.6*	4.0*	3.7				
				204						51.6	1.75	1.40	58.3	2.77	27.0*	6.2*	4.3				
				248						48.2	1.79	1.32	56.9	2.80	23.8*	5.0*	4.8				
541	58°15.8'N	153°22.0'W	167	0	0	4	41	55	8.0												
				15	0	5	57	37	7.2	96.1					5.0	1.6	3.2	63	39	24	2.38
542	58°18.6'N	153°26.9'W	155	0	0	9	47	44	7.4												
				15	0	15	55	30	6.5	76.7					5.9	2.0	3.0	56	35	21	1.99
543	58°10.77'N	153°31.97'W	180	0	0	2	48	50	7.9												

Table 1 continued

Station	Latitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk		Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
				coarse	sand	silt	clay			density (gm/cm^3)	Void ratio			undisturbed		sensitized remolded	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-ity index
545	58°22.5'N 153°53.5'W	175	0	0	17	49	34	6.6												
			22											4.5	1.9	2.4				
			30	0	0	59	41	7.6	68.8	1.65	1.90	65.6	2.83	5.6	1.9	3.0	45	25	20	2.19
			50						65.8	1.64	1.74	63.6	2.71	9.3	2.2	4.2				
			70						93.5	1.52	2.55	71.8	2.79	6.6	2.2	3.0				
			85	1	5	54	40	7.3									54	28	26	
			90						75.0	1.58	2.20	68.8	2.80	5.6	1.7	3.2				
			97						65.3	1.65	1.75	63.7	2.75	8.8*	2.0*	4.4				
			110	0	7	58	35	7.1	65.1	1.66	1.78	64.0	2.79	11.4	2.6	4.3				
			130	0	4	54	42	7.5	59.5	1.69	1.61	61.6	2.76	13.3	3.3	4.1	48	29	19	1.61
			150						65.2	1.66	1.79	64.2	2.81	11.4	3.1	3.6				
			170						60.9	1.70	1.69	62.8	2.83	11.4	4.0	2.9				
			184						55.6	1.72	1.51	60.2	2.76	14.4*	5.0*	2.9				
			185	0	4	57	39	7.4	66.8	1.66	1.84	64.8	2.84	11.1	3.8	2.9	46	29	17	2.22
			210						65.8	1.65	1.78	64.0	2.76	11.0	3.1	3.5				
			225						64.8	1.65	1.74	63.5	2.75	12.3	3.1	3.9				
			241						66.4	1.65	1.81	64.4	2.79							
			245						68.7	1.65	1.91	65.6	2.84	11.6	2.3	5.0				
			261											16.2*	2.4*	6.5				
			265	0	3	52	45	7.7	71.3	1.62	1.94	66.0	2.78	14.2	4.0	3.6	54	34	20	1.87
546	58°28.8'N 153°47.0'W	97	0	0	10	59	31	6.8												
			9	0	11	63	26	6.6	54.2	1.71	1.42	58.7	2.68	6.6	1.7	3.8	43	28	15	1.75
547	58°13.0'N 153°14.4'W	89	0	1	6	55	38	7.2												
			15	0	8	60	32	6.9	70.9	1.62	1.92	65.8	2.77	2.5	0.7	3.8	42	29	13	3.22
			27						62.8	1.67	1.69	62.8	2.75	5.0*	1.8*	2.7				
			35						57.9					6.4	1.6	4.1				
			53	0	5	62	33	7.1	56.4	1.70	1.48	59.7	2.69	6.8	1.6	4.1	41	27	14	2.10
			67						57.4	1.69	1.52	60.2	2.70	6.6*	2.0*	3.3				

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Water content (%)	Mean grain size ϕ	Wet bulk density (gm/cm ³)	Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay							undisturbed	sensitized	remolded	liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-plasticity index
548	58°37.9'N	153°25.1'W	64	0	tr	7	57	36	7.1												
				20	0	0	67	34	7.4	54.2	1.72	1.44	59.0	2.72	4.9	1.6	3.0	40	19	21	1.68
				40						53.7	1.72	1.42	58.6	2.70	6.3	1.6	3.8				
				60	0	7	62	31	6.9	60.7	1.68	1.63	62.0	2.75	4.9	0.9	5.5	30	29	1	26.0
				80						50.7	1.75	1.35	57	5	2.73	6.4	2.3	2.8			
549	58°43.3'N	153°15.0'W	87	0	2	30	28	40	6.1												
				15	0	26	53	21	5.7	43.6	1.82	1.14	53.2	2.73	9.4	1.7	5.4	29	25	4	4.65
				30						45.4	1.78	1.18	54.2	2.67	12.3	2.1	6.0				
				42						51.1	1.74	1.14	57.3	2.80	5.2*	2.0*	2.7				
550	58°50.8'N	153°10.3'W	165	0**	9	63	14	14	3.0												
				15**	0	41	37	22	5.0	42.4	1.79	1.09	52.0	2.62	37.5	5.4	7.0	30			
				35						41.2	1.84	1.10	52.5	2.74	11.9	3.3	3.6				
				55						37.8	1.89	1.03	50.7	2.78	22.2	2.6	8.4				
				84	2	52	28	19	4.3	39.3	1.85	1.04	51.1	2.72	27.9	2.7	10.3	28	21	7	2.61
				100						41.7	1.83	1.11	52.6	2.72	15.6*	2.0*	7.9				
				124						39.1	1.86	1.04	51.0	2.72	20.2	3.3	6.1				
				144**	0	51	29	20	4.5	34.2	1.92	0.91	47.7	2.73	16.1	1.5	10.8	26			
				158						30.8	1.98	0.83	45.5	2.77	18.9	2.6	7.2				
				175						31.4	1.94	0.86	46.3	2.72	11.4*	1.4*	8.6				
551	58°51.6'N	152°54.4'W	155	0	0	32	36	32	5.8												
				15	0	28	41	29	5.9	56.1	1.72	1.53	60.5	2.79	10.6	2.1	5.2	43	26	17	1.77
				35						44.8	1.81	1.21	54.7	2.76	18.0	2.7	6.6				
				55	0	55	27	18	4.2	37.8	1.89	1.02	50.5	2.77	22.6	4.0	5.6	29	25	4	3.20
				75						30.2	1.97	0.80	44.5	2.72	20.2*	4.0*	5.1				

Table 1 continued

Station	Latitude	Longitude	Water depth (m)	Depth in core (cm)	Grain size (weight percent)				Mean grain size ϕ	Water content (%)	Wet bulk density (gm/cm^3)		Void ratio	Porosity (%)	Grain specific gravity	Vane shear strength (kPa)			Atterberg limits			
					coarse	sand	silt	clay	undisturbed		sensitized	remolded				liquid limit (%)	plastic limit (%)	plasticity index (%)	liquid-plasticity index			
552	58°47.2'N	135°02.5'W	135	0	0	38	35	27	5.4													
				15	0	21	47	32	6.3	59.0	1.70	1.60	61.6	2.78	11.5	1.6	7.0	41	26	15	2.20	
				35						51.0	1.76	1.38	58.1	2.78	10.7	2.1	5.2					
				60						47.5	1.78	1.28	56.1	2.75	12.2*	2.6*	4.6					
				69	0	32	42	26	5.6	51.7	1.75	1.39	58.1	2.75	10.9	2.6	4.1	40	26	14	1.84	
				74						46.1	1.80	1.25	55.5	2.77	29.4*	6.6*	4.5					
				89						47.7	1.80	1.28	56.1	2.78	8.9	1.6	5.4					
				110	0	30	39	31	5.9	50.5	1.75	1.44	58.9	2.78	13.2	4.0	3.3	41	27	14	1.68	
				125						46.1	1.80	1.25	55.6	2.78	11.9	2.8	4.3					
				145	0	48	30	21	4.6	38.9	1.88	1.05	51.3	2.77	23.1	5.1	4.5	31	23	8	1.99	
				161						45.8	1.81	1.25	55.5	2.79	25.9	6.7	3.9					
				174						41.5	1.84	1.11	52.7	2.75	19.2*	4.2*	4.5					

* Vane inserted parallel to axis of core; inserted perpendicular to axis for all others. ** High sand content; probable nonplastic behavior during testing.

Table 2. Replicate vane shear measurements on split-core halves. S_u indicates undisturbed strength, S_r indicates remolded strength, subscript 1 refers to first core half, subscript 2 refers to second. V_u and V_r are the coefficients of variation for replicate undisturbed and remolded strength measurements, respectively. The notation tc-sp indicates that a torque cell was used to measure strength on the first core half and a spring was used on the second, whereas tc-tc indicates that torque-cell measurements were made on both halves.

<u>Core</u>	<u>Depth in core (cm)</u>	<u>S_{u1} (kPa)</u>	<u>S_{u2} (kPa)</u>	<u>S_{r1} (kPa)</u>	<u>S_{r2} (kPa)</u>	<u>V_u (%)</u>	<u>V_r (%)</u>
508 G1 (tc-tc)	13	3.1	3.5	0.8	1.3	12	48
	35	4.9	3.2	0.9	1.2	42	29
	55	8.2	9.5	2.1	2.5	15	17
	75	9.0	7.3	2.6	1.8	21	36
	110	9.0	10.0	2.6	2.6	11	0
	130	11.6	14.8	4.0	4.7	24	16
	153	10.8	12.4	3.5	3.5	14	0
	170	15.7	14.3	4.2	3.9	9	7
	190	11.4	15.6	3.2	4.1	31	25
	210	11.1	21.6	4.0	2.6	64	42
511 G1 (tc-sp)	15	2.6	3.22	1.4	1.6	21	13
	65	4.5	6.0	1.6	2.4	29	40
	85	6.2	5.2	2.1	2.5	18	17
	105	6.8	7.5	2.8	3.3	10	16
	125	9.7	7.8	3.1	3.0	22	3
	145	9.4	7.8	3.4	3.6	19	6
	165	9.9	7.8	3.3	3.3	24	0
	190	10.6	11.3	3.4	4.6	6	30
	210	13.5	13.2	4.9	5.9	2	19
	230	11.9	10.2	4.8	4.8	15	0

<u>Core</u>	<u>Depth in core (cm)</u>	<u>S_{u1} (kPa)</u>	<u>S_{u2} (kPa)</u>	<u>S_{r1} (kP2)</u>	<u>S_{r2} (kP2)</u>	<u>V_u (%)</u>	<u>V_r (%)</u>
525 G1	15	9.5	9.5	1.6	2.6	0	48
(tc-tc)	35	23.5	10.5	5.4	3.7	76	37
	55	31.3	19.4	5.6	5.1	47	9
	85	27.8	24.0	6.6	6.5	15	2
	105	17.1	17.4	3.3	4.9	2	19
	125	11.5	11.4	3.2	4.0	1	22
	145	20.2	17.4	3.9	4.0	15	3
	165	35.7	28.1	8.3	7.5	24	10
526 G2	20	7.1	7.5	2.0	2.3	5	14
(tc-sp)	40	11.5	7.9	3.3	2.3	37	36
	65	7.6	9.3	2.3	2.5	20	8
	85	10.7	6.6	2.6	2.2	47	17
	105	14.3	13.8	3.3	4.5	4	31
	125	5.9	8.3	1.7	2.2	34	26
	145	18.5	14.4	4.9	4.9	25	0
	165	11.0	4.9	3.0	2.2	77	31

<u>Core</u>	<u>Depth in core (cm)</u>	<u>S_{u1} (kPa)</u>	<u>S_{u2} (kPa)</u>	<u>S_{r1} (kPa)</u>	<u>S_{r2} (kPa)</u>	<u>V_u (%)</u>	<u>V_r (%)</u>
528 G3	15	21.7	27.1	4.2	15.0	22	113
(tc-sp)	62	16.6	16.0	5.0	4.4	4	13
	82	11.4	19.1	1.6	4.1	50	88
	94	15.6	15.7	3.1	6.4	1	69
	119	22.2	19.3	6.6	6.6	14	0
	146	15.7	19.5	5.7	7.6	22	29
	175	17.2	20.8	4.5	6.8	19	41
	190	16.3	20.2	3.9	5.4	21	32
	210	16.6	13.4	4.5	3.9	21	14
	234	15.6	18.2	4.0	5.4	15	30
545 G1	50	9.3	6.2	2.2	1.6	40	32
(tc-tc)	70	6.6	5.4	2.2	2.1	20	5
	90	5.6	4.5	1.7	1.5	22	12
	106	11.4	5.3	2.6	1.0	73	89
	130	13.3	15.2	3.3	4.1	13	22
	150	11.4	9.6	5.1	3.3	17	6
	170	11.4	17.6	4.0	5.4	43	30
	185	11.1	9.4	3.8	3.4	17	11
	205	11.0	13.8	3.1	3.3	23	6
	225	12.3	10.0	3.1	3.8	21	21
	245	11.6	13.2	2.3	5.4	13	81
	265	14.2	14.0	4.0	5.6	1	33

Table 3. Strength anisotropy in sediment cores. S_{ue} is the undisturbed vane shear strength measurement taken on ends of core sections, and S_{us} is the corresponding predicted split-core value. S_{re} and S_{rs} are the measured and predicted remolded vane shear measurements, respectively. Corrected $S_{ue} = S_{ue} - (S_{re} - S_{rs})$. (Negative strength values are an artifact of the analytical procedure. These values are not used in Fig. 11.)

Core	Depth in core (cm)	Water content (%)	Estimated plasticity index (%)	S_{ue} (kPa)	Corrected S_{ue} (kPa)	S_{us} (kPa)	S_{re} (kPa)	S_{rs} (kPa)	Anisotropy
508	21	106.2	42	5.0	3.4	4.4	2.6	1.0	1.3
	121	66.4	31	4.2	7.2	15.1	2.0	5.0	2.1
	221	55.7	21	9.0	9.9	17.9	5.2	6.1	1.8
510	15	119.2	36	4.0	2.0	-0.1	2.2	0.2	-0.1
	115	87.9	27	5.0	6.0	9.0	2.0	3.0	1.5
527	23	37.7	12	13.0	16.8	22.0	1.8	5.6	1.3
	123	23.3	6	19.8	15.2	-4.4	3.2	-1.4	-0.3
528	52	47.8	12	11.6	13.0	16.8	2.8	4.2	1.3
	152	46.6	15	17.0	15.4	17.0	5.8	4.2	1.1
534	83	58.1	11	23.8	25.5	24.3	2.4	4.1	1.0
536	40	76.5	25	7.4	7.1	9.3	2.4	2.1	1.3
	140	39.0	14	6.0	6.6	11.6	2.6	3.2	1.8
	240	51.3	14	11.6	11.2	10.9	3.2	2.8	1.0
537	85	64.7	23	14.6	16.8	19.8	3.2	5.4	1.2
	185	54.7	23	18.2	19.9	22.8	4.2	5.9	1.2
538	24	88.9	38	13.2	12.3	8.0	3.2	2.3	0.6
	124	63.1	29	23.0	23.4	22.6	5.8	6.2	1.0
	224	61.1	19	16.4	17.1	23.7	5.8	6.5	1.4
545	97	65.3	26	8.8	9.8	11.0	2.0	3.0	1.1
	184	55.6	17	14.4	12.8	12.8	5.0	3.4	1.0

Table 3 cont.

Core	Depth in core (cm)	Water content (%)	Estimated plasticity index (%)	S _{ue} (kPa)	Corrected S _{ue} (kPa)	S _{us} (kPa)	S _{re} (kPa)	S _{rs} (kPa)	Anisotropy
547	27	62.8	13	5.0	4.4	4.9	1.8	1.2	1.1
	67	57.4	14	6.6	6.2	6.5	2.0	1.6	1.0
550	100	41.7	7	15.6	16.7	19.7	2.0	3.1	1.2
	175	31.4	7	11.4	12.5	20.9	1.4	2.5	1.7
551	75	30.2	4	20.2	20.7	27.6	4.0	4.5	1.3
552	69	47.5	14	12.2	13.0	15.5	2.6	3.4	1.2
	89	46.1	14	29.4	26.5	16.4	6.6	3.7	0.6
	174	41.5	18	19.2	19.6	19.5	4.2	4.6	1.0

Table 4. Clay mineralogy of tops of cores.

Station	% chlorite	% illite	% mixed layer	% smectite in mixed layer	Corrected % smectite	Corrected % illite
507	42	53	5	75	4	54
508	43	49	8	75	6	51
509	44	47	9	75	7	49
510	44	56	0	0	0	56
511	41	51	8	75	6	53
512	44	47	9	81	7	49
513	40	52	8	75	6	54
514	42	53	5	70	4	54
515	40	53	7	80	6	54
516	37	58	5	75	4	59
517	46	46	8	80	6	48
518	40	52	8	70	6	54
519	47	47	6	75	5	48
520	46	50	4	79	3	51
521	39	52	9	75	7	54
522	43	50	7	70	5	52
523	40	52	8	74	6	54
525	38	56	6	75	5	57
526	45	48	7	79	6	49
527	37	56	7	79	6	57
528	37	56	7	75	5	58
529	34	54	12	75	9	57
530	40	47	13	79	10	50
531	51	42	7	75	5	44
532	40	41	19	70	13	47
534	46	48	6	75	5	49
535	42	29	29	77	22	36
536	47	46	7	76	5	48
537	42	49	9	77	7	51
538	44	50	6	80	5	51
539	43	48	9	81	7	50
540	49	44	7	80	6	45
541	47	47	6	77	5	48
542	47	47	6	84	5	48
543	45	44	11	70	8	47
545	44	48	8	77	6	50
546	45	48	7	75	5	50
547	48	46	6	75	5	47
548	32	60	8	79	6	62
549	40	54	6	75	5	55
550	38	56	6	79	5	57
551	45	50	5	75	4	51
552	35	58	7	82	6	59
553	37	53	10	91	9	54

Table 5. Clay mineralogy (percents) of Shelikof Strait and possible source areas.

	<u>Shelikof Strait</u>		<u>Cook Inlet</u>		<u>Kodiak Shelf</u>		<u>Copper River and Delta</u>	
	average	range	average	range	average	range	average	range
chlorite	42	32-51	42	29-64	51	30-69	56	53-64
illite	52	36-66	46	32-61	34	19-43	31	27-39
smectite	6	0-22	3	0-19	5	0-30	tr	0-1

Table 6. Light hydrocarbon gas contents of sediment cores.

Station	Depth in core (cm)	C ₁	C ₂	C _{2:1}	C ₃	i-C ₄	n-C ₄	C ₁	C ₂
		Methane (μl/l)	Ethane (nl/l)	Ethene (nl/l)	Propane (nl/l)	Isobutane (nl/l)	n-butane (nl/l)	$\frac{C_1}{C_2+C_3}$	$\frac{C_2}{C_{2.1}}$
509	100-110	177	228	248	224	24	42	390	0.9
511	96-106	36	46	12	52	0	0	365	3.9
514	30-40	23	48	28	46	14	0	247	1.7
523	100-110	10	24	22	44	0	0	156	1.1
525	100-110	1	0	0	0	0	0		
526	50-60	18	116	100	116	26	14	80	1.2
	100-110	16	36	28	80	18	0	137	1.3
	200-210	38			66				
527	100-110	25	202	300	192	26	24	62	0.7
528	100-110	1	0	0	76	0	0	13	
529	100-110	12	80	84	116	0	24	60	1.0
	200-210	48	184	60	96	12	28	172	3.0
534	50-60	6	88	66	90	22	20	34	1.3
536	100-110	26	162	102	138	22	0	85	1.6
537	100-110	62	106	95	82	0	0	330	1.1
538	100-110	17	130	72	92	0	0	79	1.8
	200-210	27	186	88	158	28	26	79	2.1
539	100-110	1628	946	58	100	0	0	1556	16.1
540	100-110	16	224	100	228	24	48	35	2.3
	204-214	16	130	72	118	22	26	63	1.8
545	100-110	51	56	48	50	0	0	480	1.2
	200-210	83	42	38	34	0	0	1070	1.2
548	96-106	28	64	50	0	0	0	244	1.3
549	42-51	1	0	0	0	0	0		

Table 6 cont.

		C ₁	C ₂	C _{2:1}	C ₃	i-C ₄	n-C ₄	C ₁	C ₂
	Depth in core	Methane	Ethane	Ethene	Propane	Isobutane	n-butane	<u>C₁</u>	<u>C₂</u>
Station	(cm)	(μl/l)	(nl/l)	(nl/l)	(nl/l)	(nl/l)	(nl/l)	C ₂ +C ₃	C _{2.1}
550	100-110	28	64	50	54	0	0	244	1.3
	200-210	17	42	26	54	18	24	180	1.6
551	91-101	30	154	82	126	20	16	107	1.9
552	50-60	18	44	36	36	0	0	231	1.2
	100-110	14	24	18	62	0	0	165	0.4

FIGURE CAPTIONS

1. Location map of the study area in Shelikof Strait
2. Tracklines of continuous seismic reflection profiles and locations of sampling stations (numbered). Solid lines represent the 1979 Nekton survey contracted by the USGS Conservation Division, and dashed lines represent the 1980 R/V S.P. LEE cruise.
3. Bathymetry of Shelikof Strait, 5-m contour interval. Depths corrected to mean lower low water.
4. Shallow structures. Bold lines represent fault offset of the seafloor (hachures on downthrown side), dashed lines indicate buried faults that offset unconsolidated sediment, and dotted lines indicate uncertain extent of buried faults. Fold axes (from Hoose and Whitney, 1980) denoted by narrow lines.
5. Boomer seismic reflection profile showing high-offset faults.
6. Thickness of near-surface sedimentary units of probable Pleistocene and younger age. Contour interval: 25 milliseconds of two-way travel time, except 100 ms for dotted contours where data are relatively sparse and contours are generalized.
7. Seismic reflection record across marginal channel.
8. Pie-diagrams showing relative abundances of textural classes in sediment samples.
9. Mean grain size of seafloor sediment, in phi-units.
10. Vane shear strength (in kilopascals) at shallowest level measured in core (typically at 15 cm; none deeper than 74 cm).
11. Anisotropy of vane shear strength versus plasticity index, including experimentally derived curve of Bjerrum (1973). S_{us} is the predicted (from the regression line) value of undisturbed strength measured on a split core, and corrected S_{ue} is the (corrected) value of undisturbed strength measured on an end of core. Both values are hypothetically from the same depth in the core.
12. Sensitivity at shallowest level measured in core (typically at 15 cm; none deeper than 74 cm).
13. Water content at shallowest level measured in core (typically at 15 cm; none deeper than 74 cm).
14. Liquid limit at shallowest level measured in core (typically at 15 cm; none deeper than 129 cm).

15. Plastic limit at shallowest level measured in core (typically at 15 cm; none deeper than 129 cm).
16. Plasticity index at shallowest level measured in core (typically at 15 cm; none deeper than 129 cm)
17. Liquid limit versus mean grain size.
18. Plastic limit versus mean grain size.
19. Plasticity versus mean grain size.
20. Plasticity chart.
21. Organic carbon (percent dry weight) in seafloor sediment.
22. Carbonate carbon (percent dry weight) in seafloor sediment.
23. Organic carbon versus grain size.
24. Water content versus organic carbon.
25. Plasticity index versus organic carbon.
26. Shear strength versus organic carbon.
27. Sensitivity versus organic carbon.
28. Liquidity index versus organic carbon.
29. Illite content of seafloor sediment.
30. Chlorite content of seafloor sediment.
31. Mixed-layer clay (mostly smectite) content of seafloor sediment.
32. Locations of acoustic anomalies along tracklines.
33. Uniboom seismic reflection record showing acoustic anomaly over truncated fold in bedrock. Vertical scale is in two-way travel time.
34. Locations of craters along tracklines. Dots represent seafloor craters; circles represent buried craters.
35. Uniboom seismic reflection record showing seafloor and buried craters. Vertical scale is in two-way travel time.
36. Uniboom seismic reflection record showing slump mass at base of seafloor escarpment. Vertical scale is in two-way travel time.

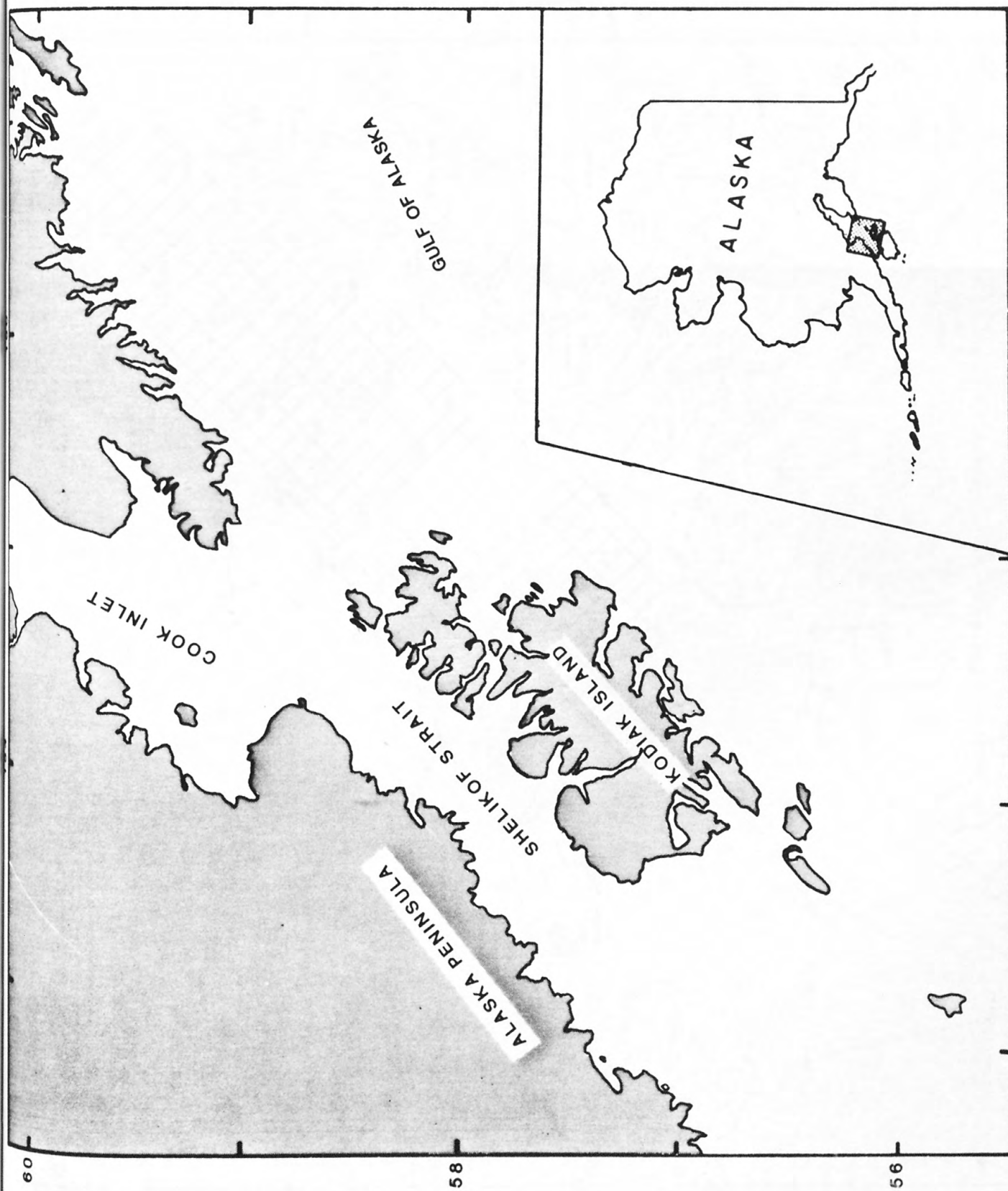


Fig. 1

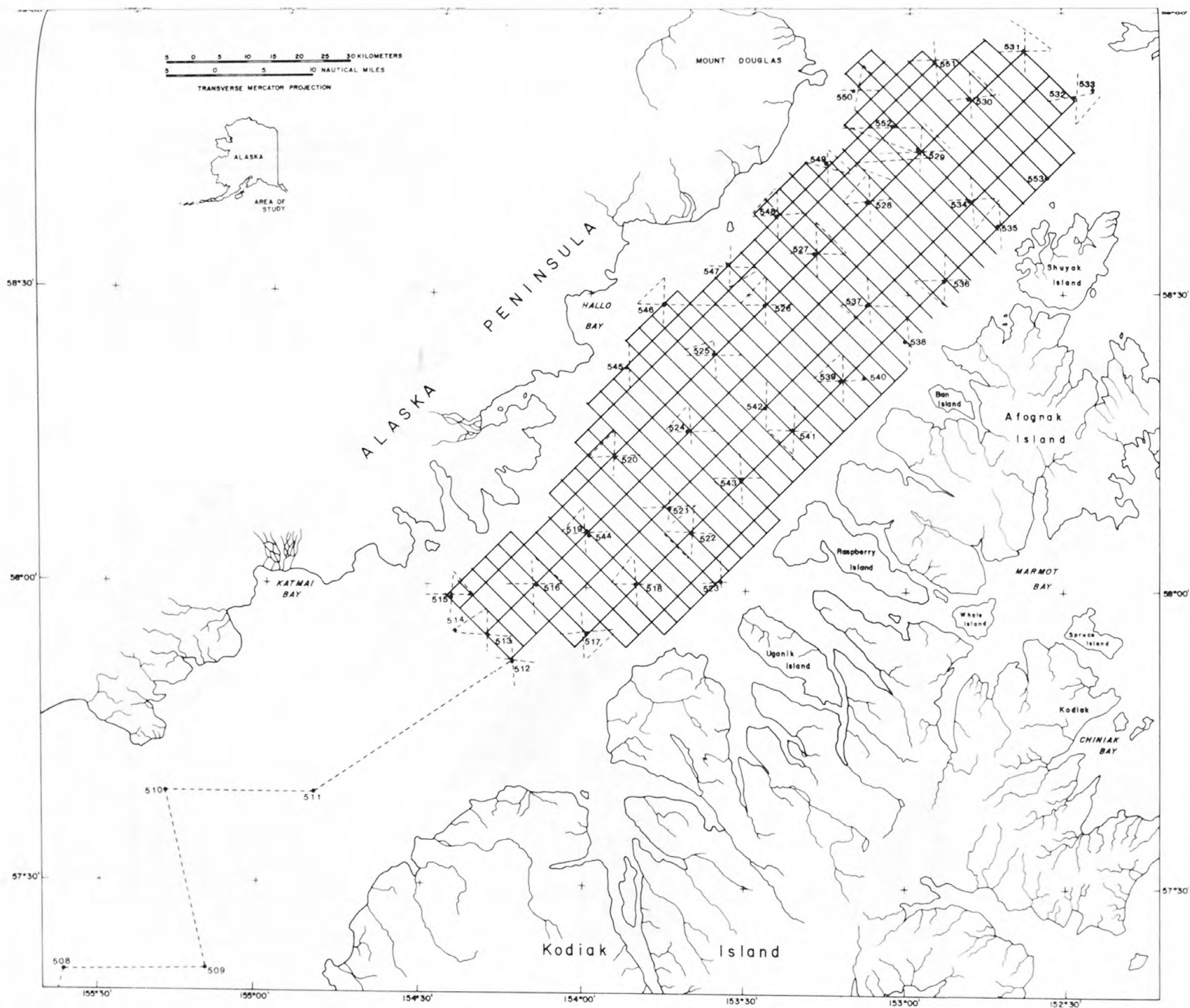
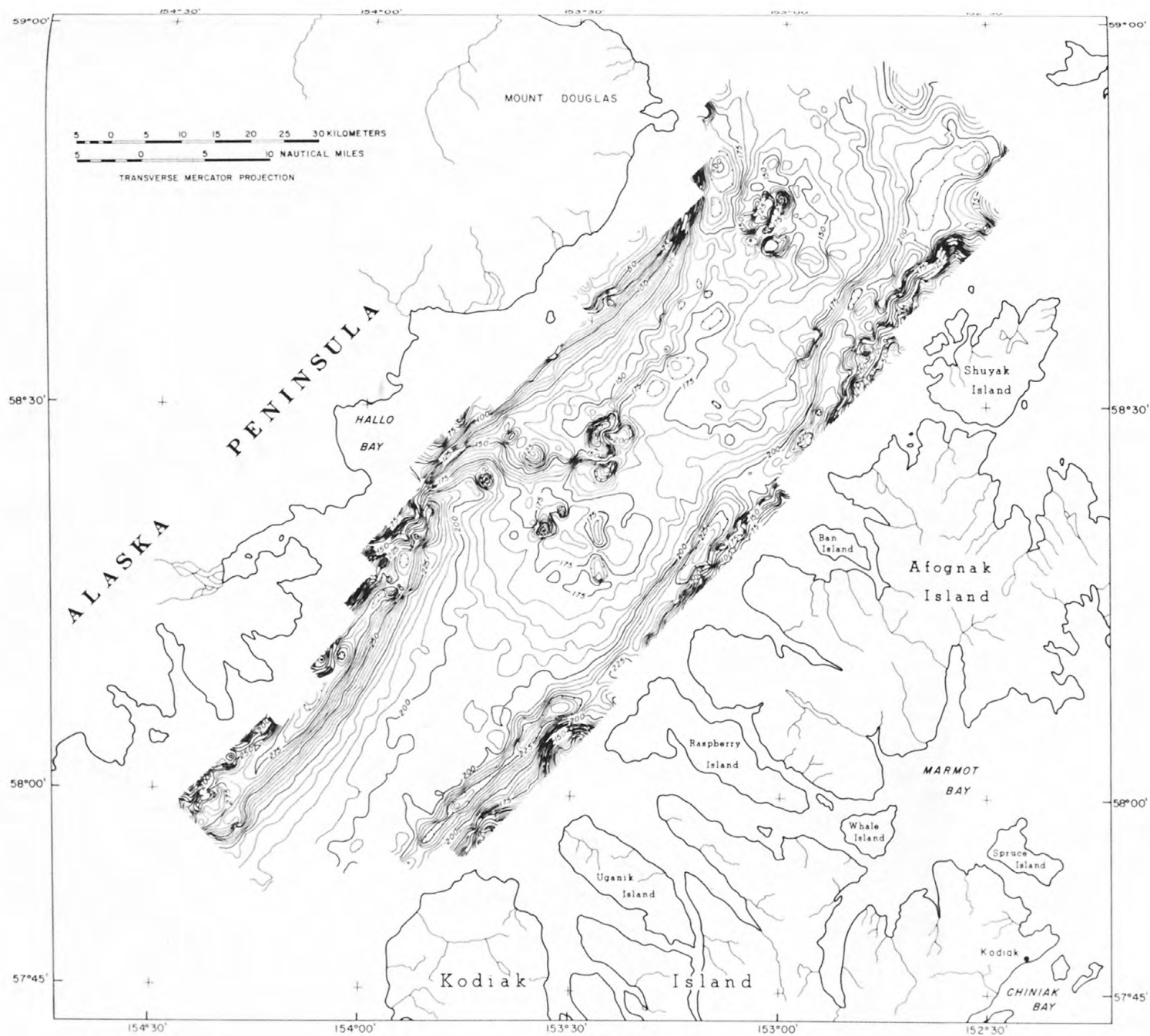


Fig. 2



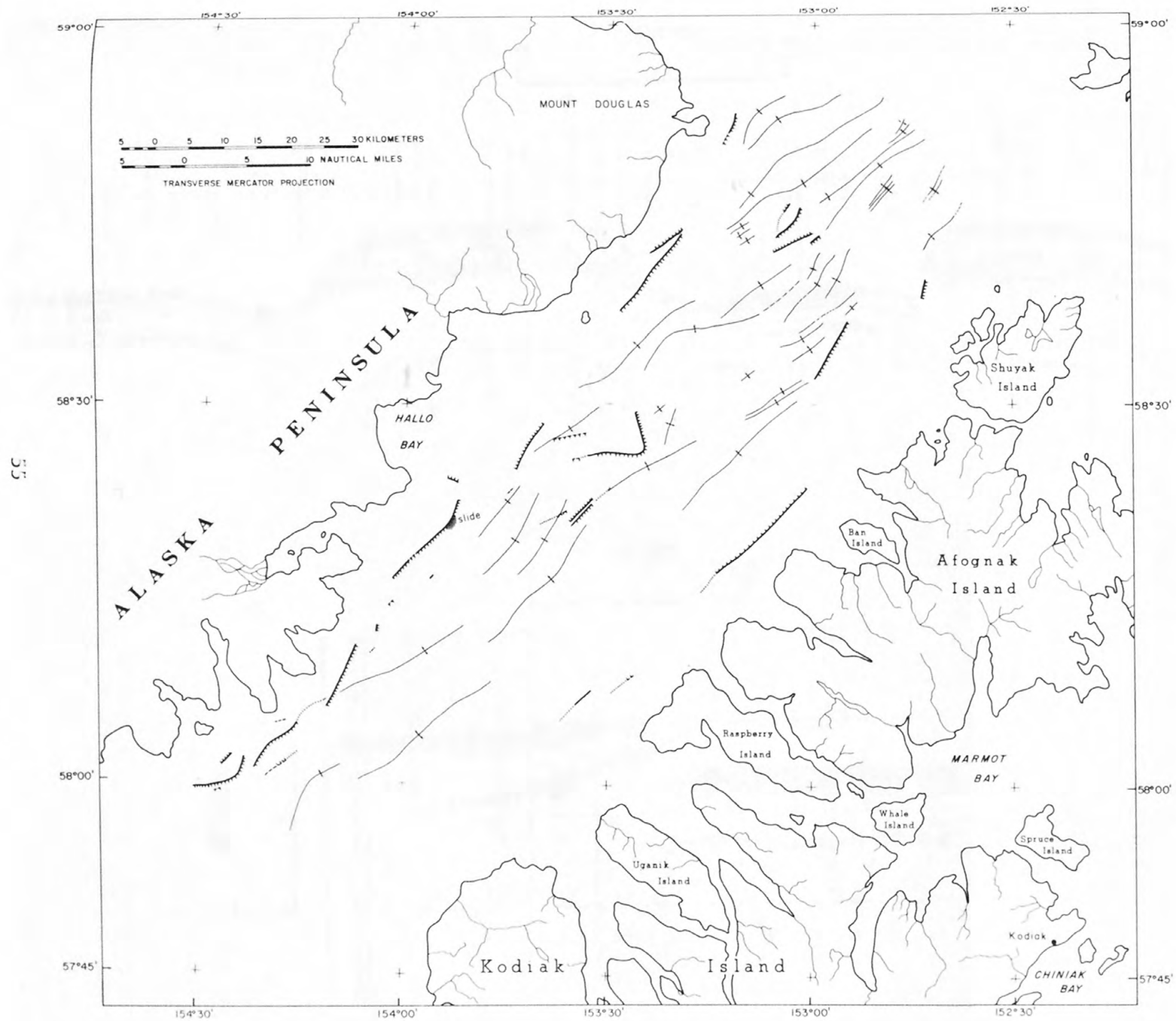
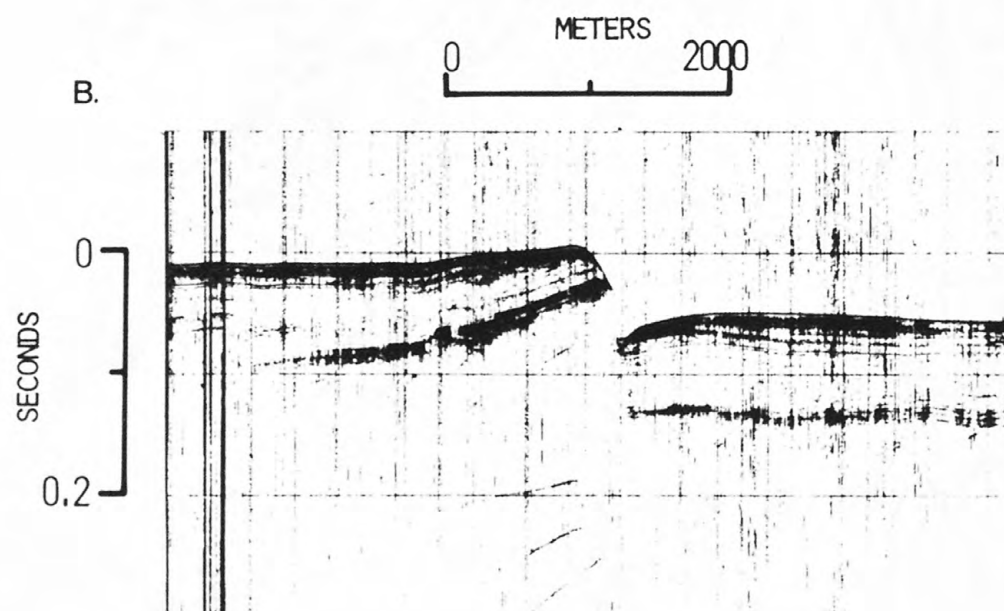
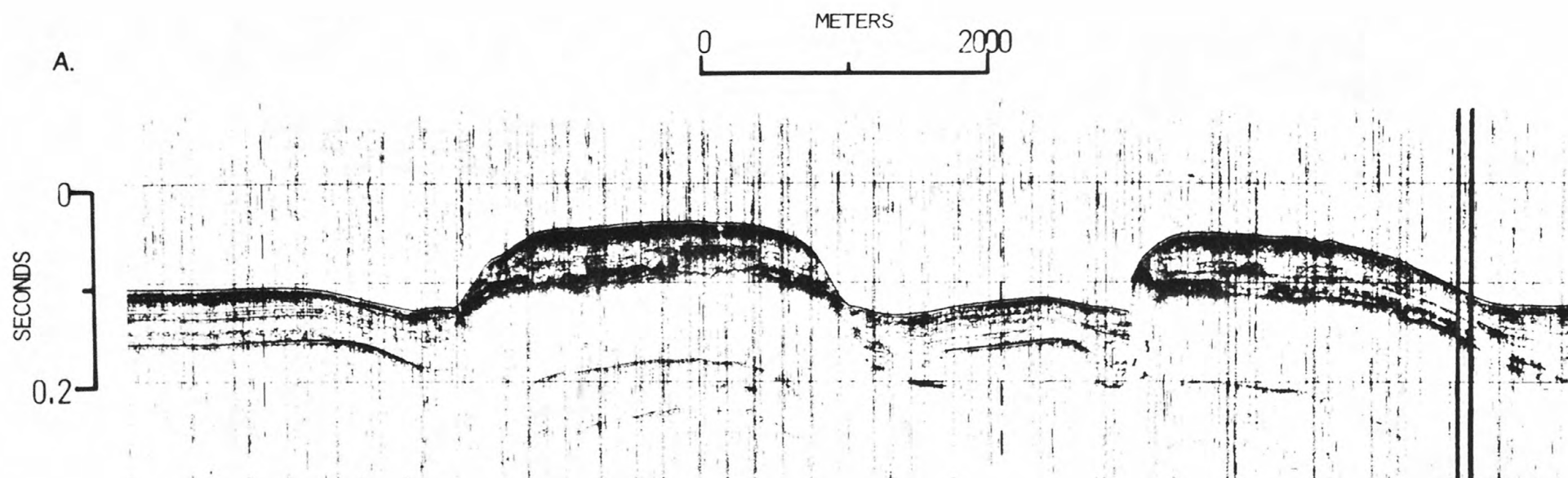


Fig. 4



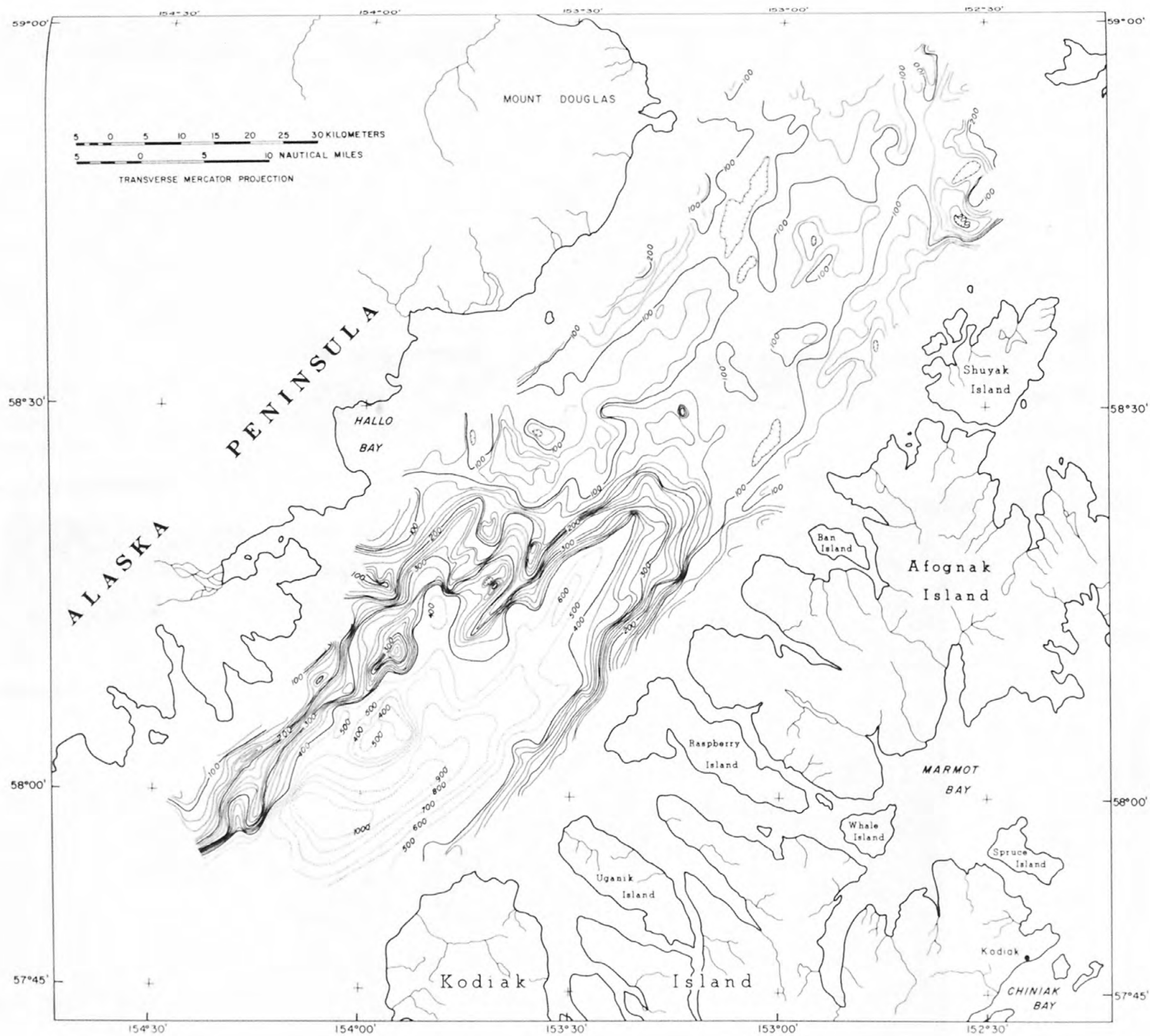


Fig. 3

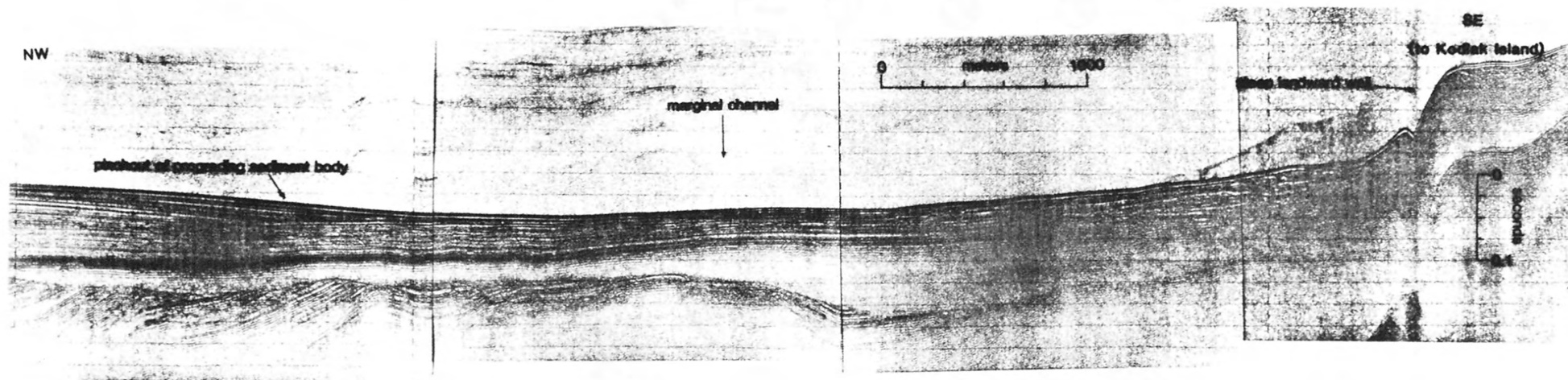


Fig. 7

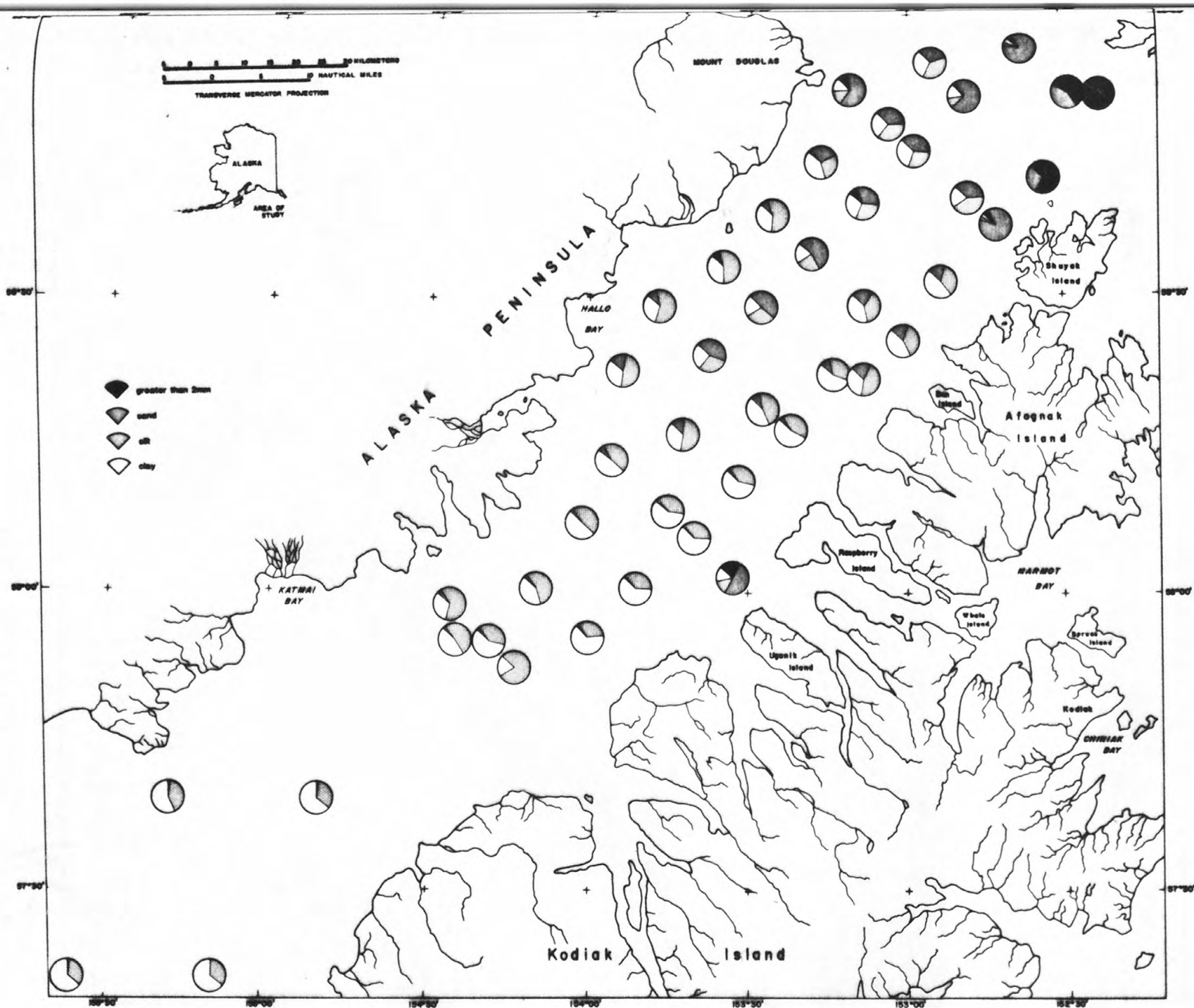


Fig. 8

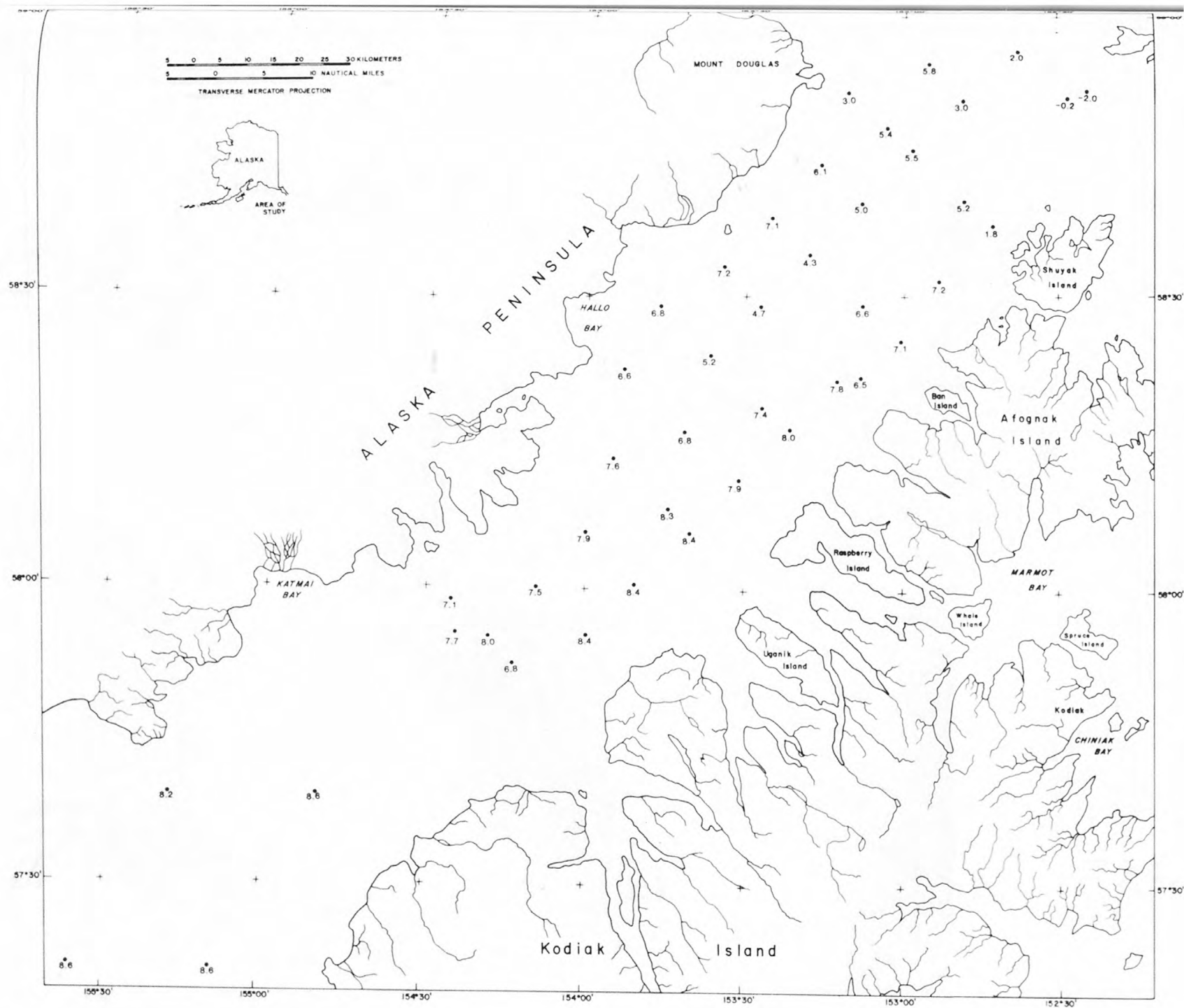


Fig. 9

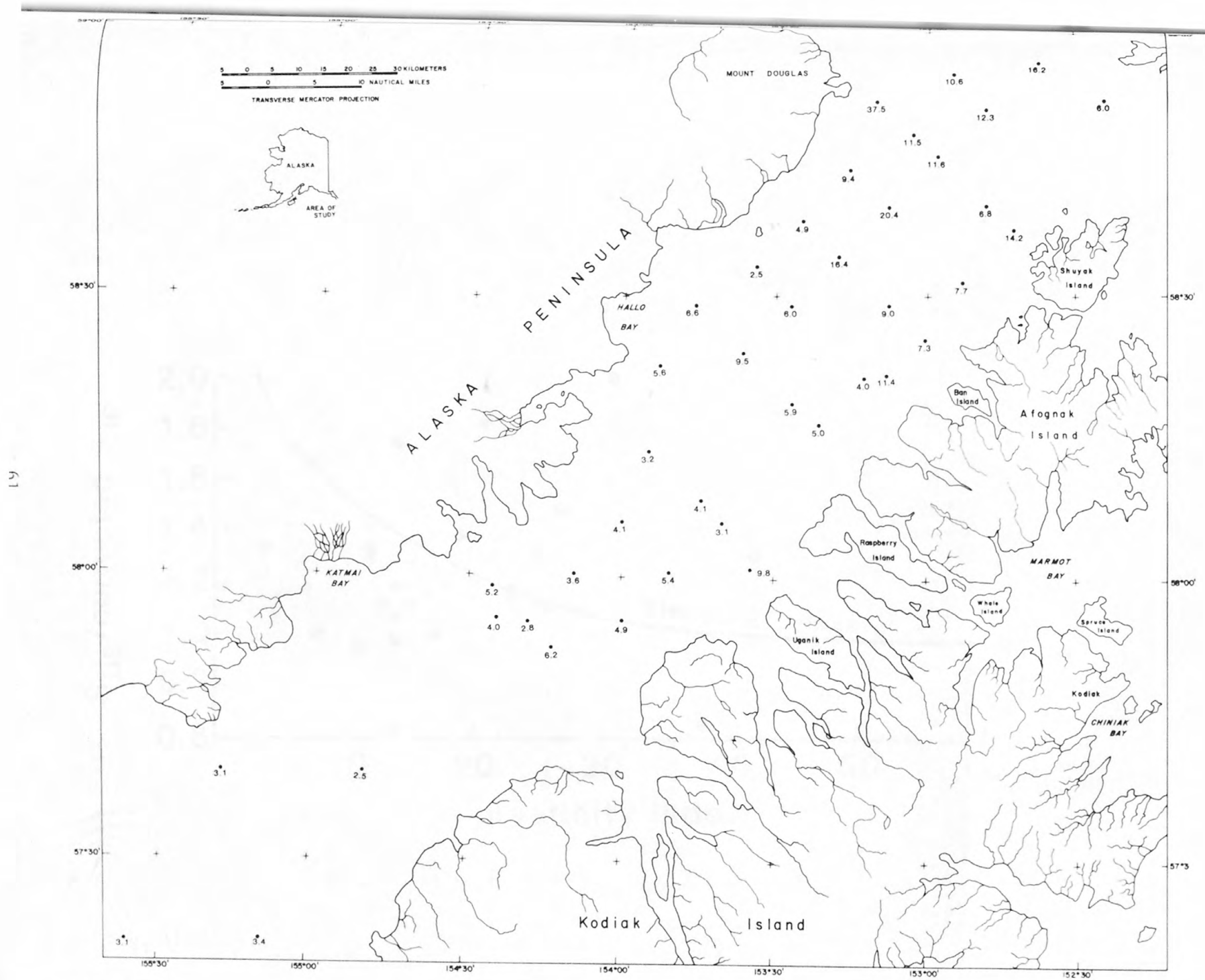


Fig. 10

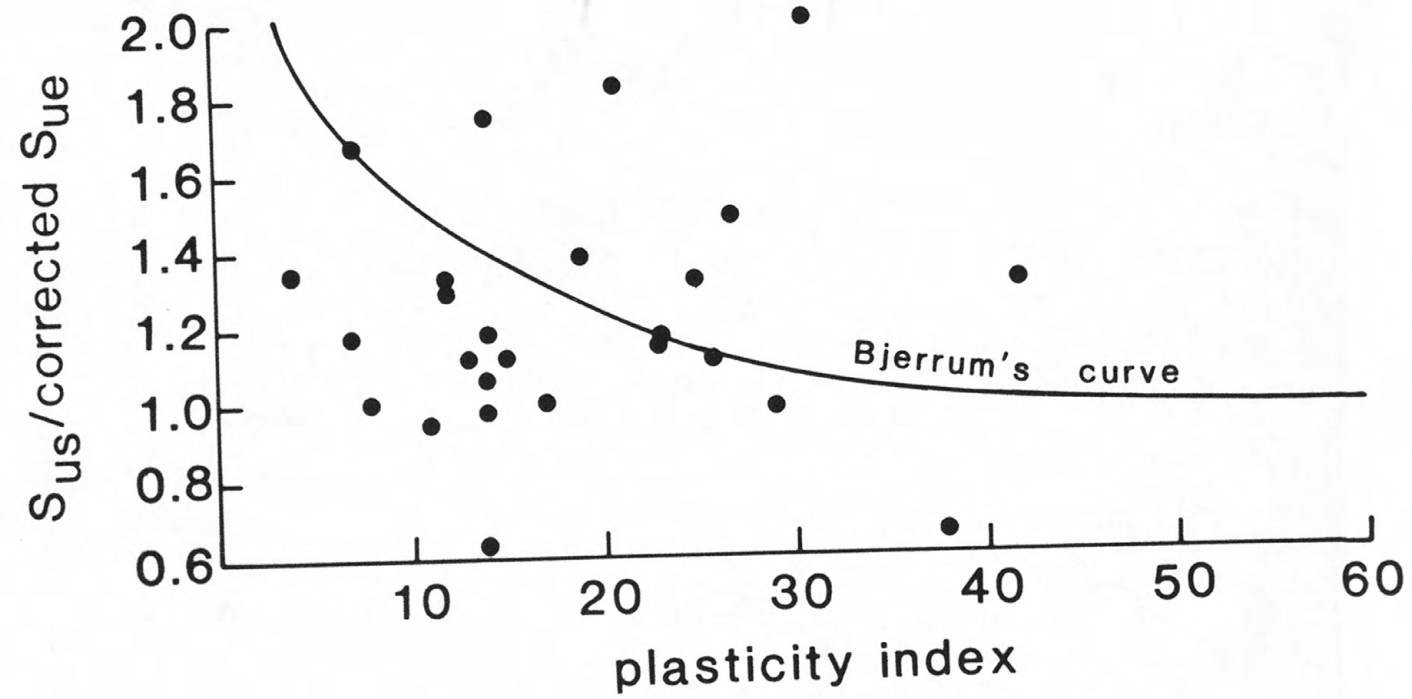


Fig. 11

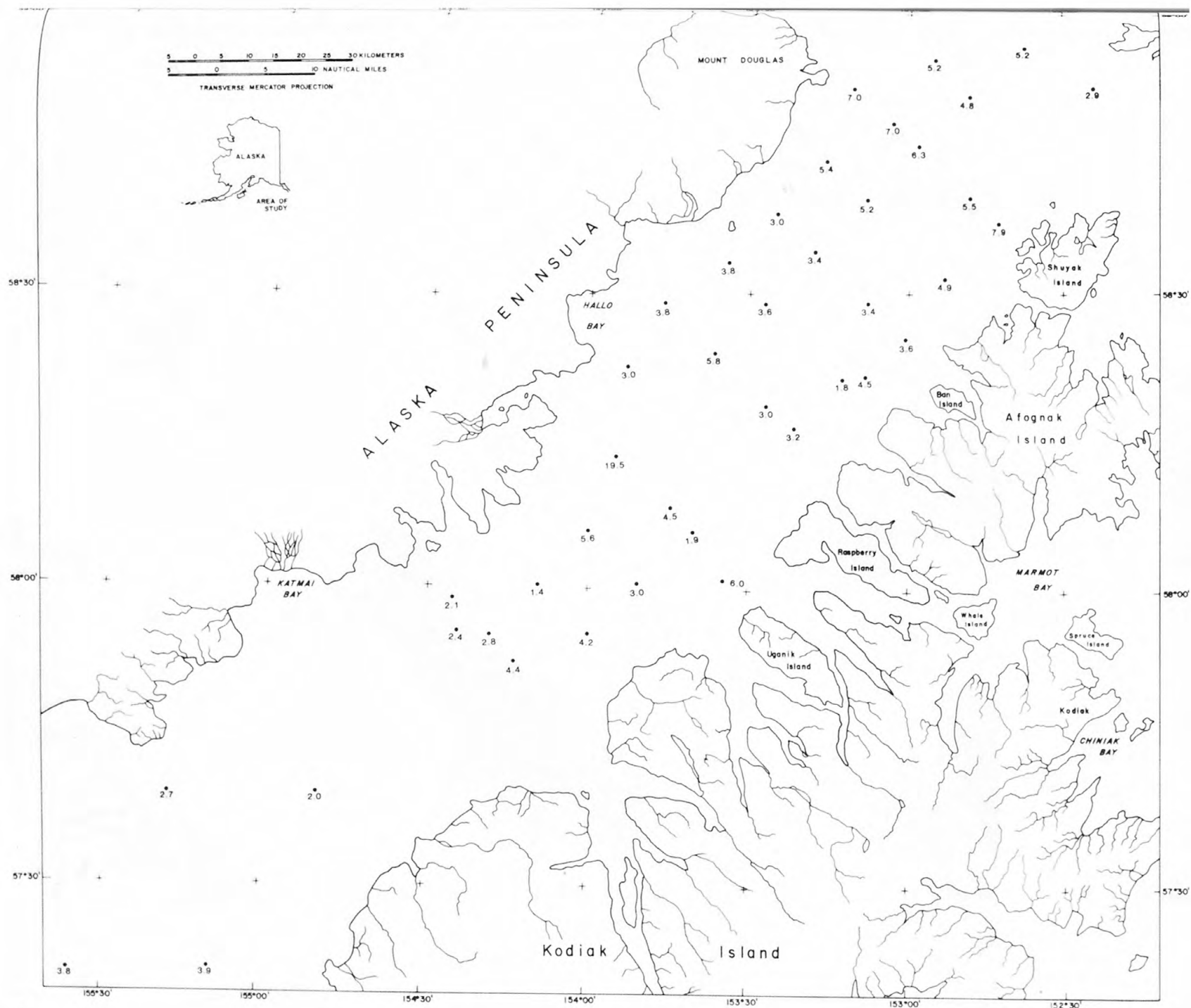


Fig. 12

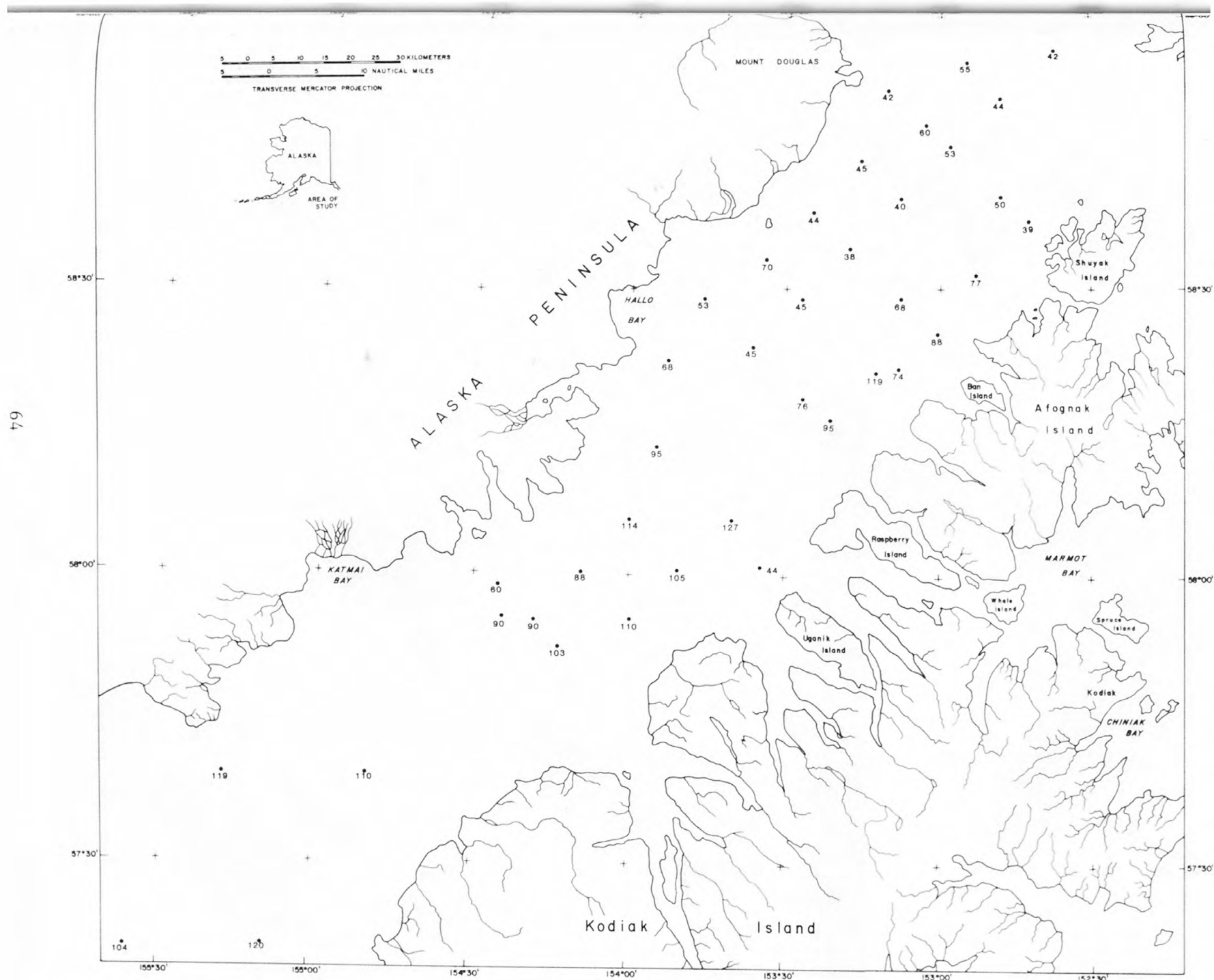


Fig. 13

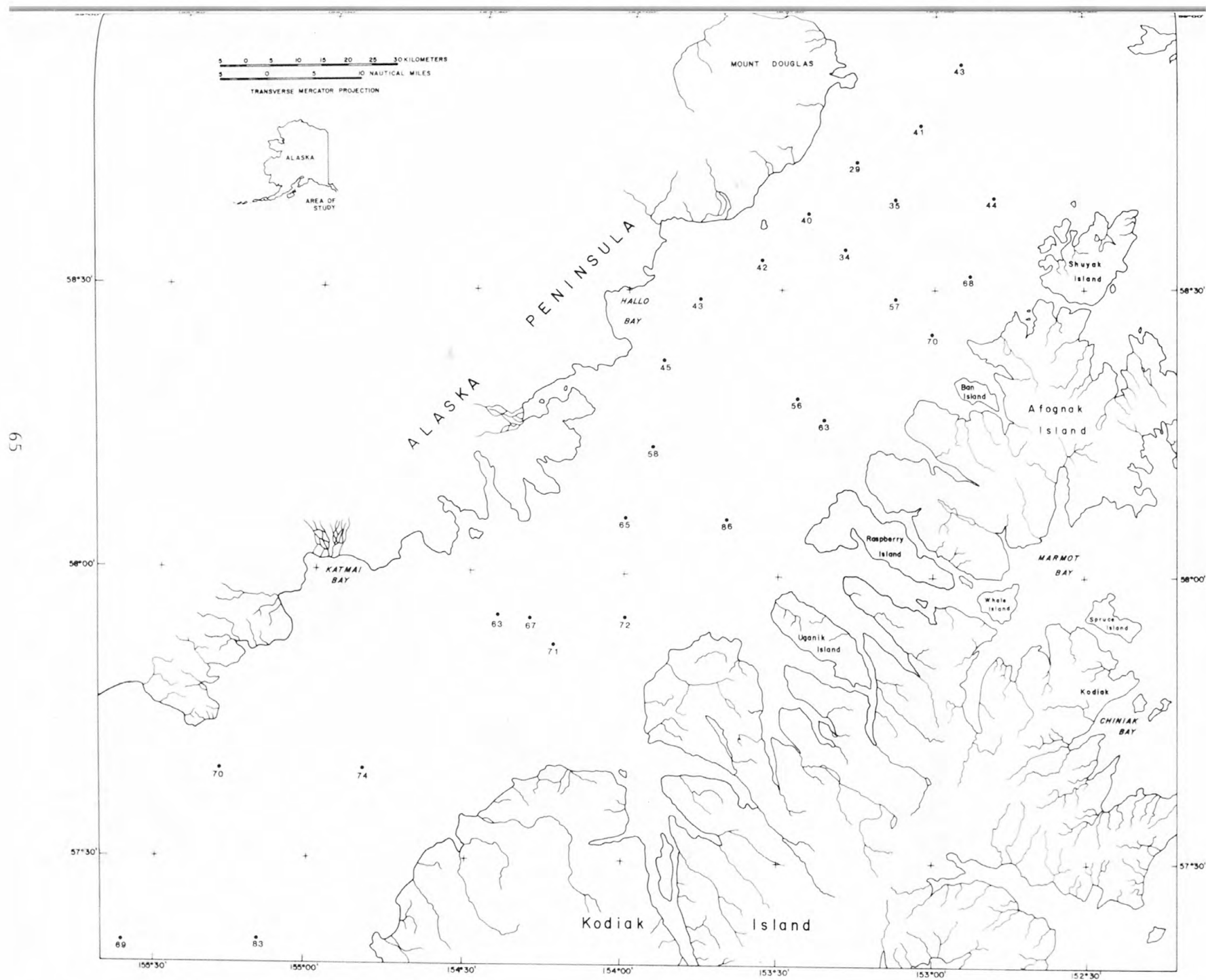


Fig. 14

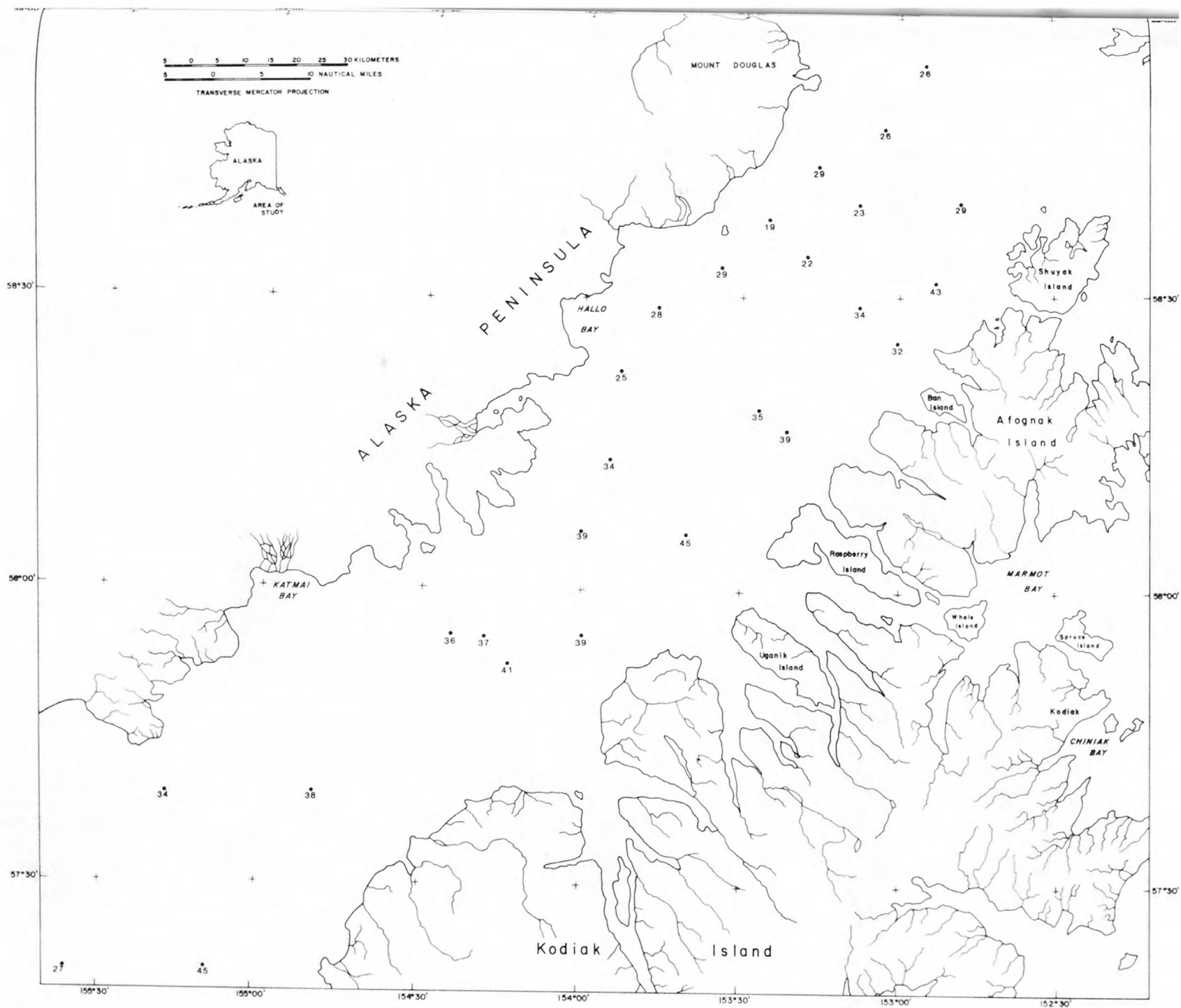
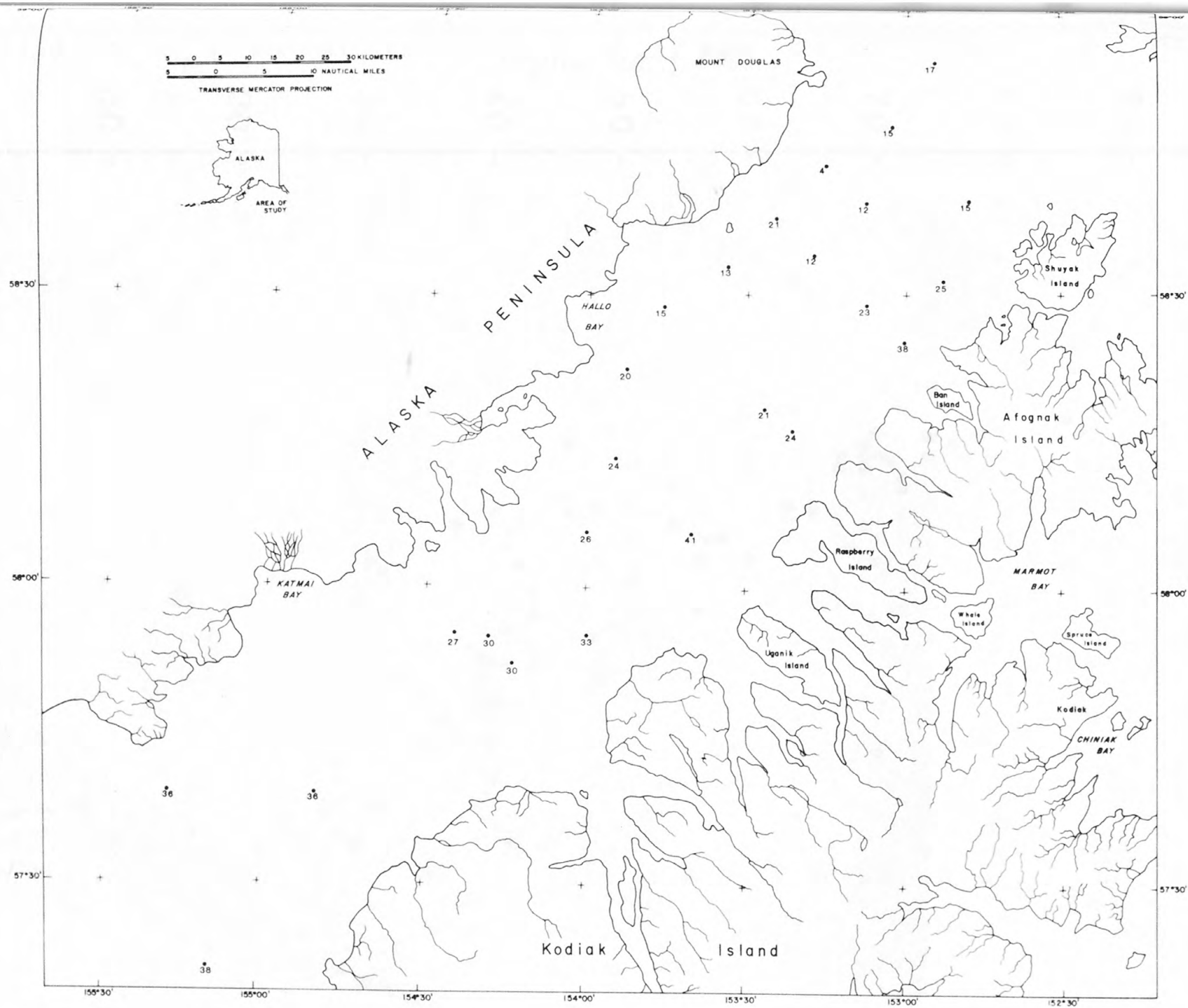


Fig. 15



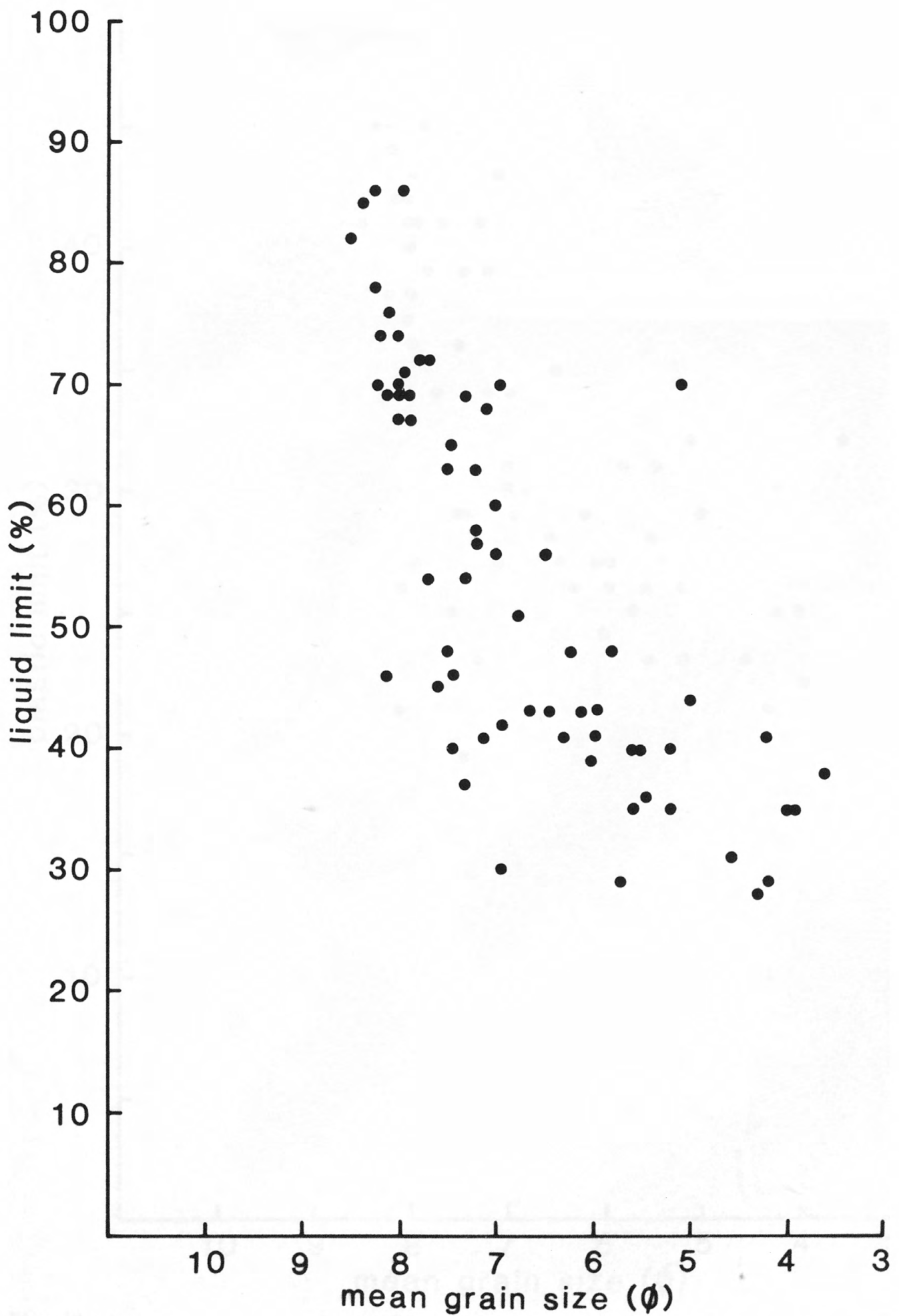


Fig. 17

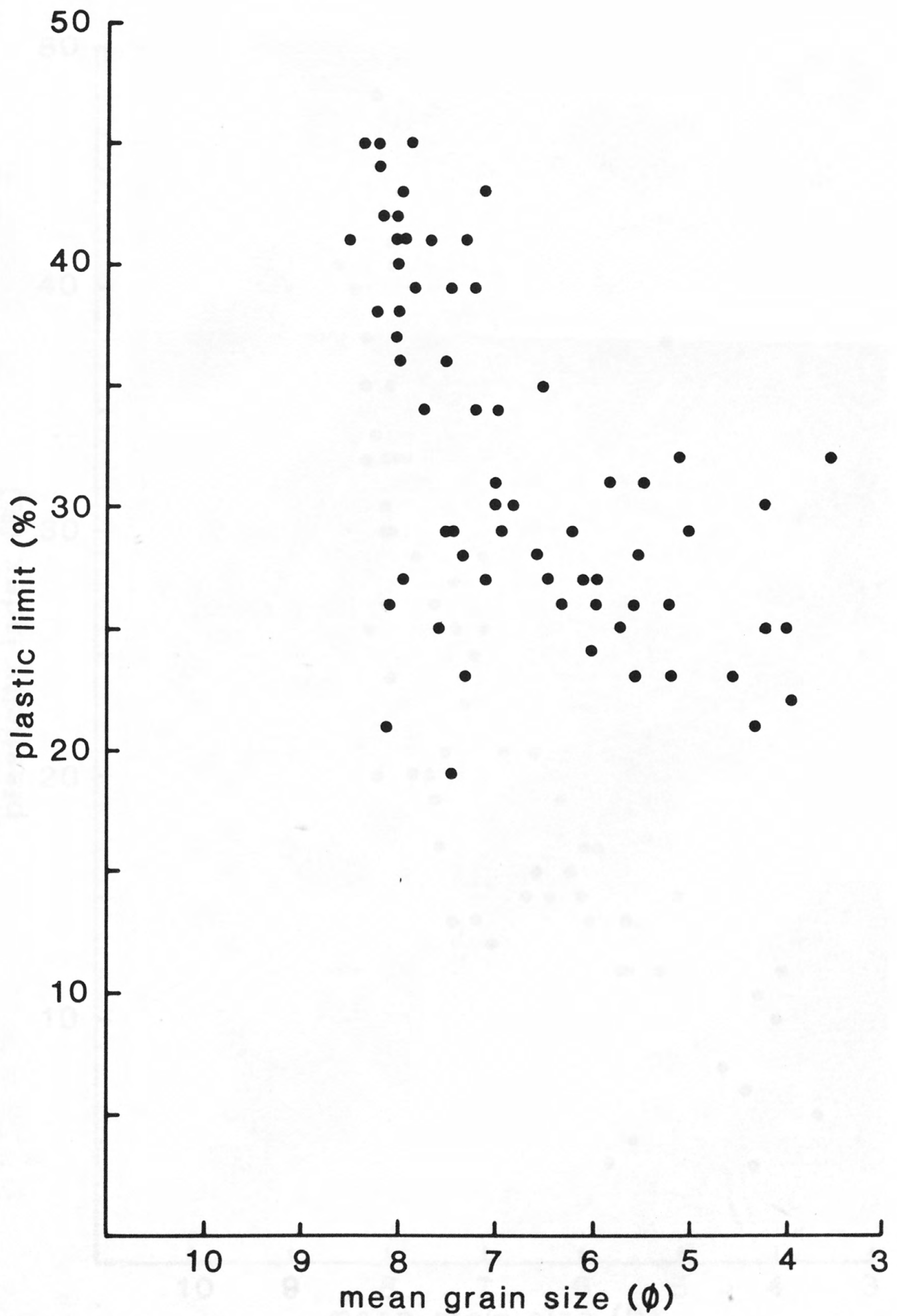


Fig. 18

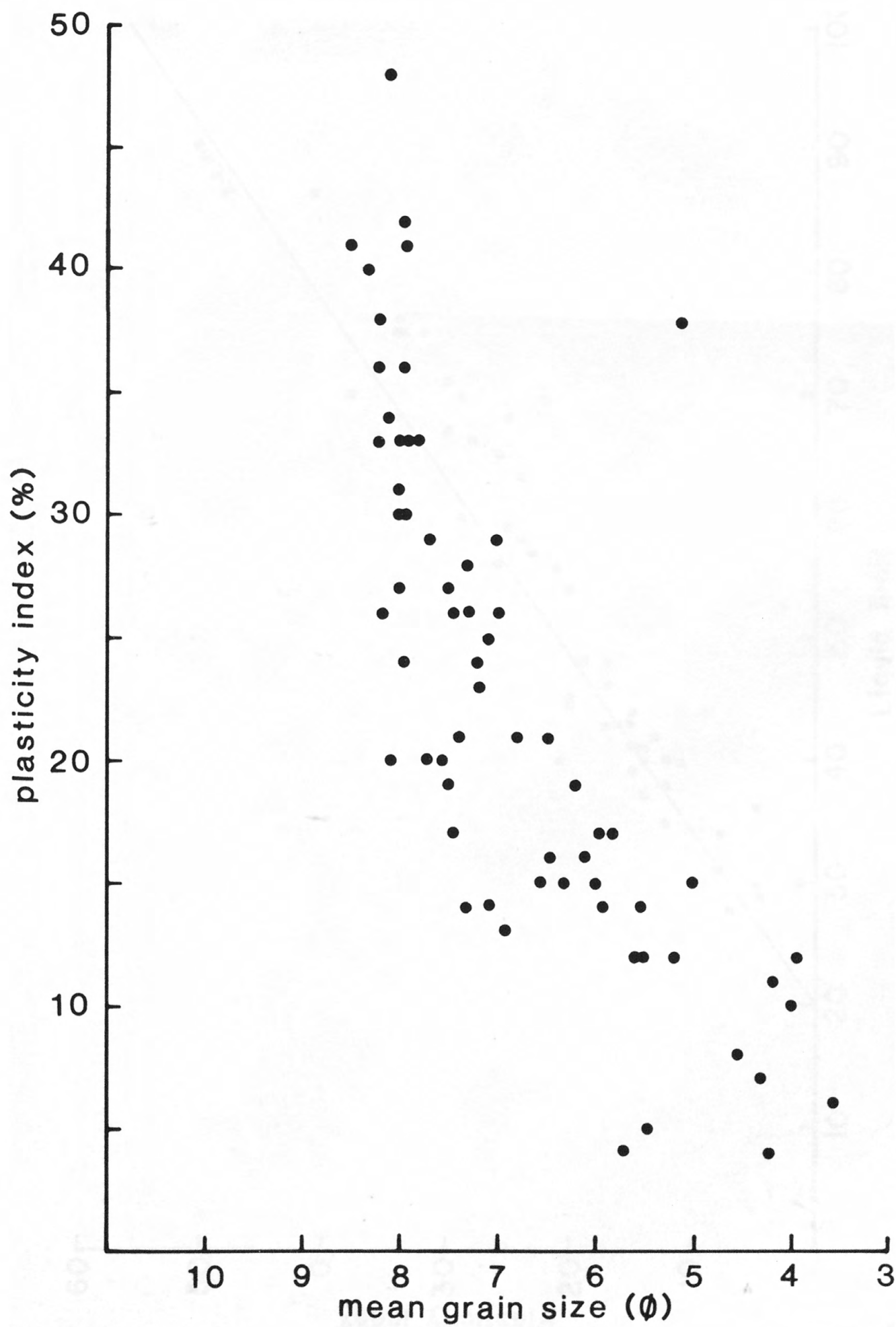


Fig. 19

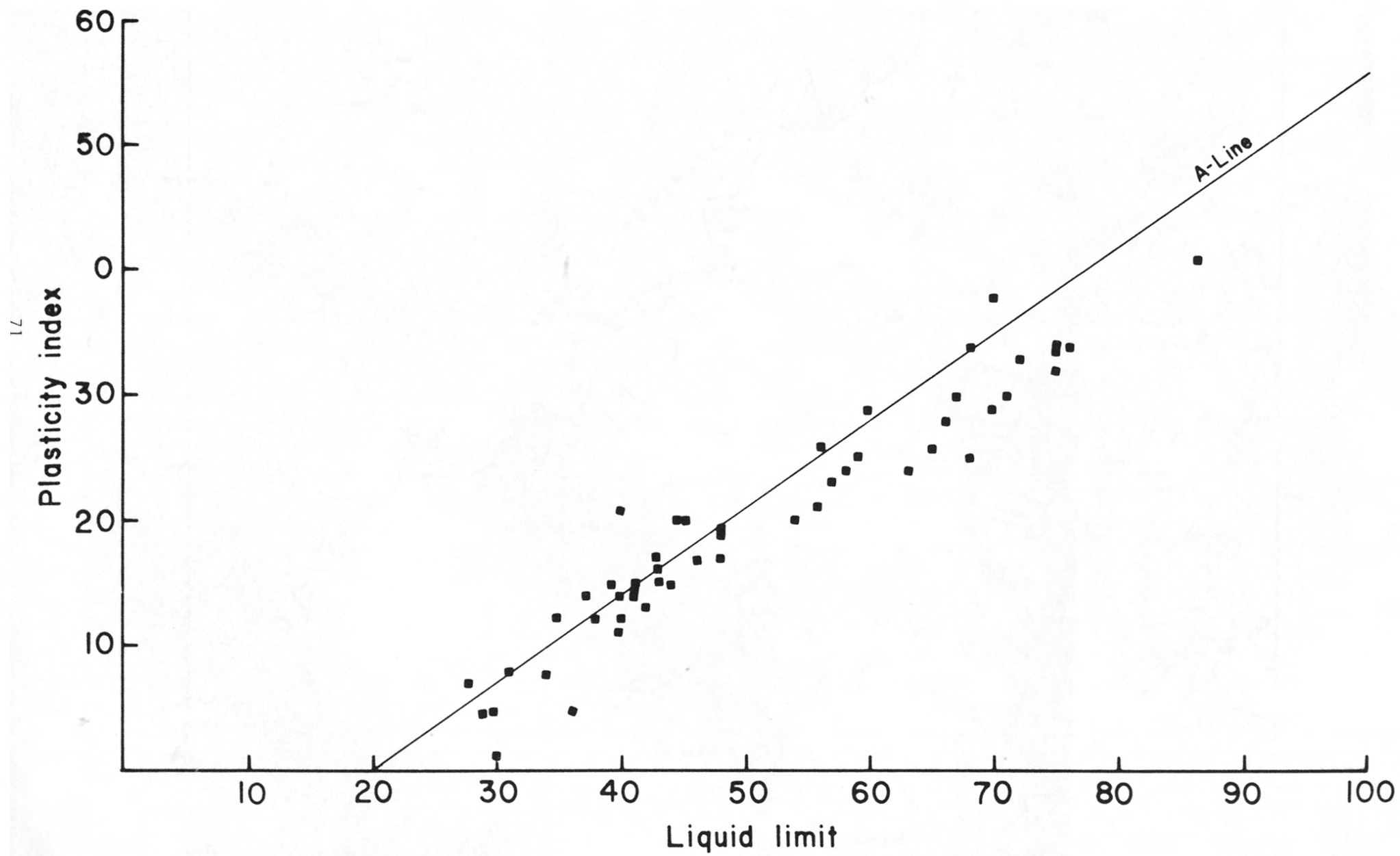


Fig. 20

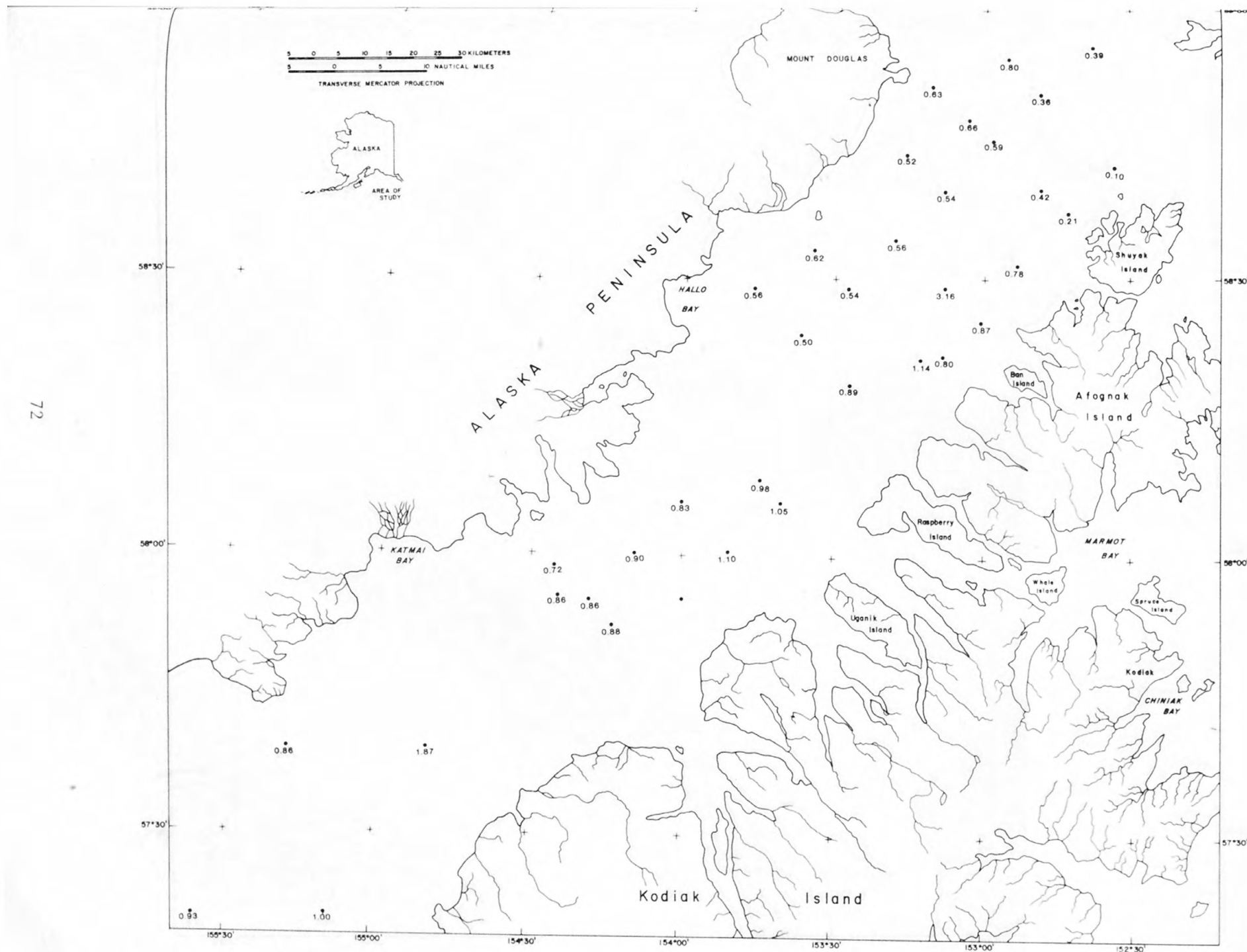
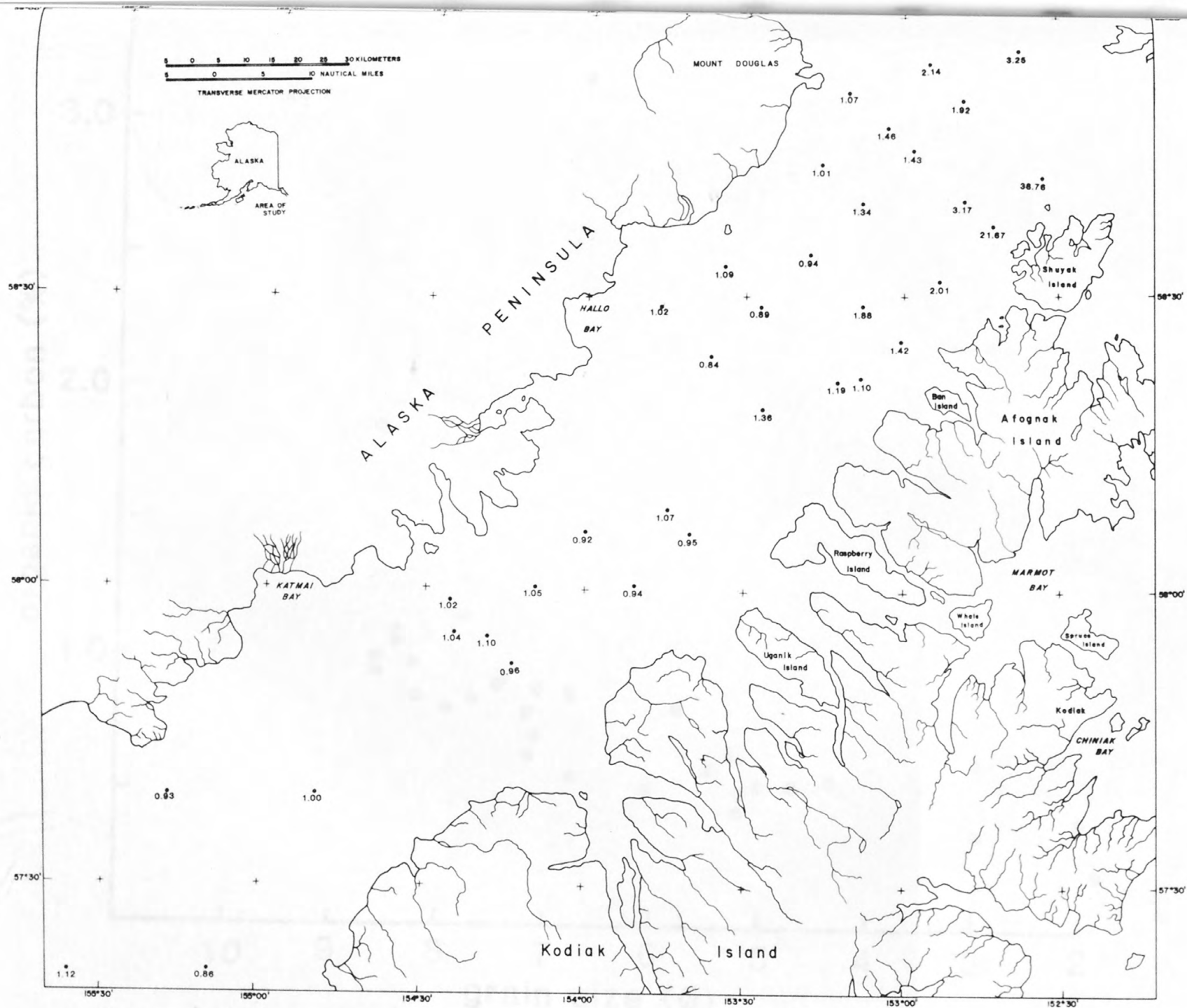


Fig. 21



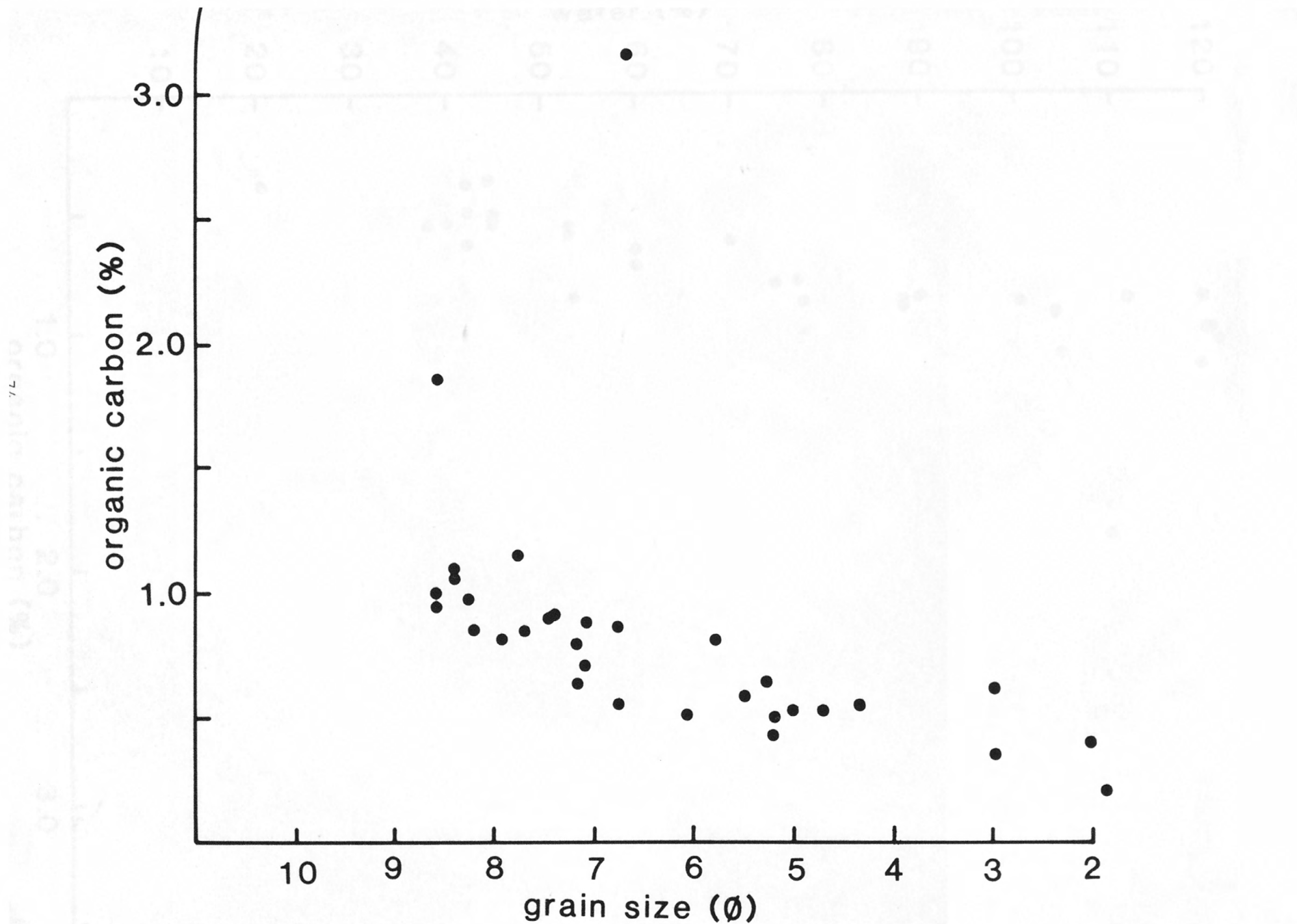


Fig. 23

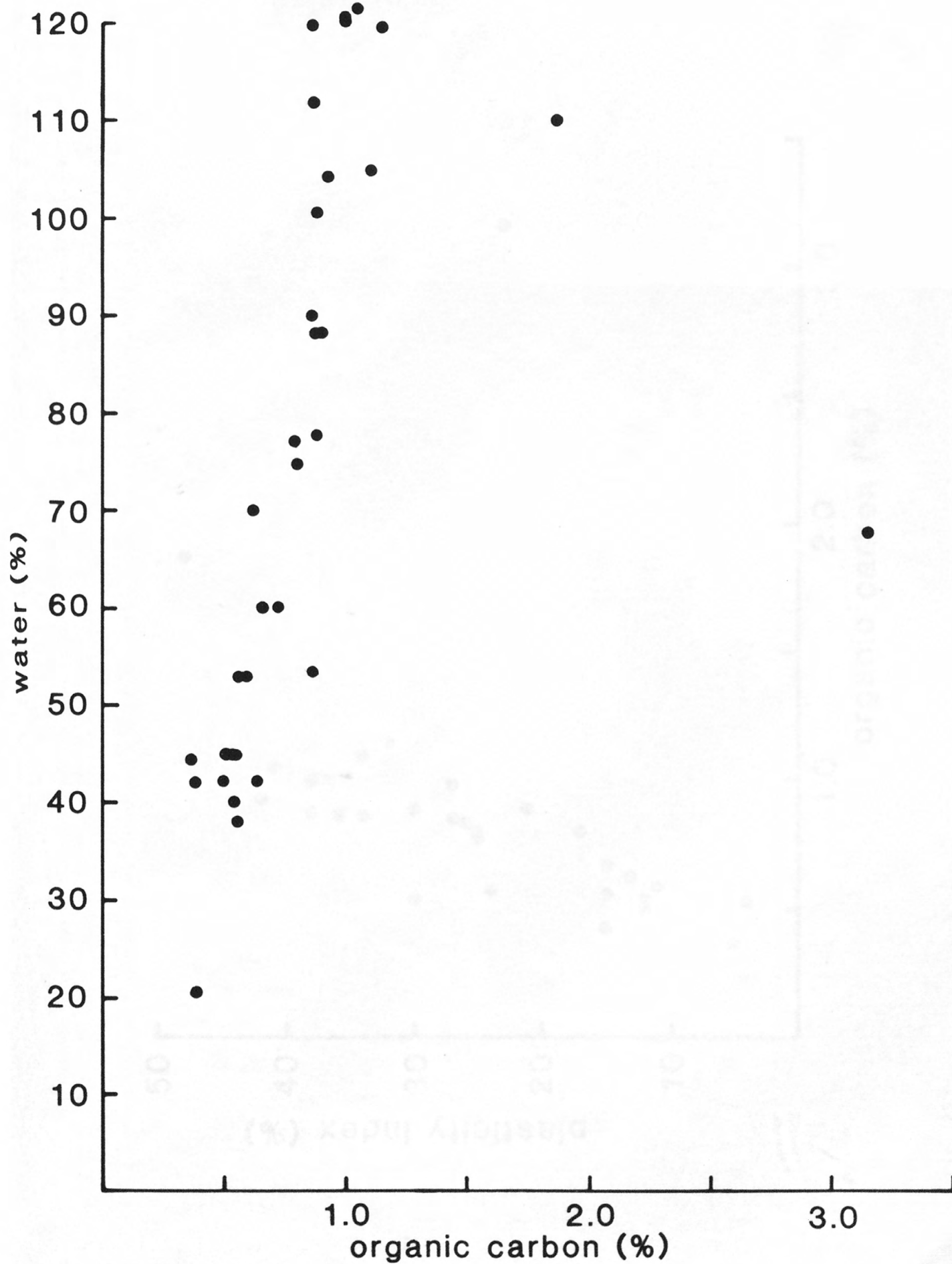


Fig. 24

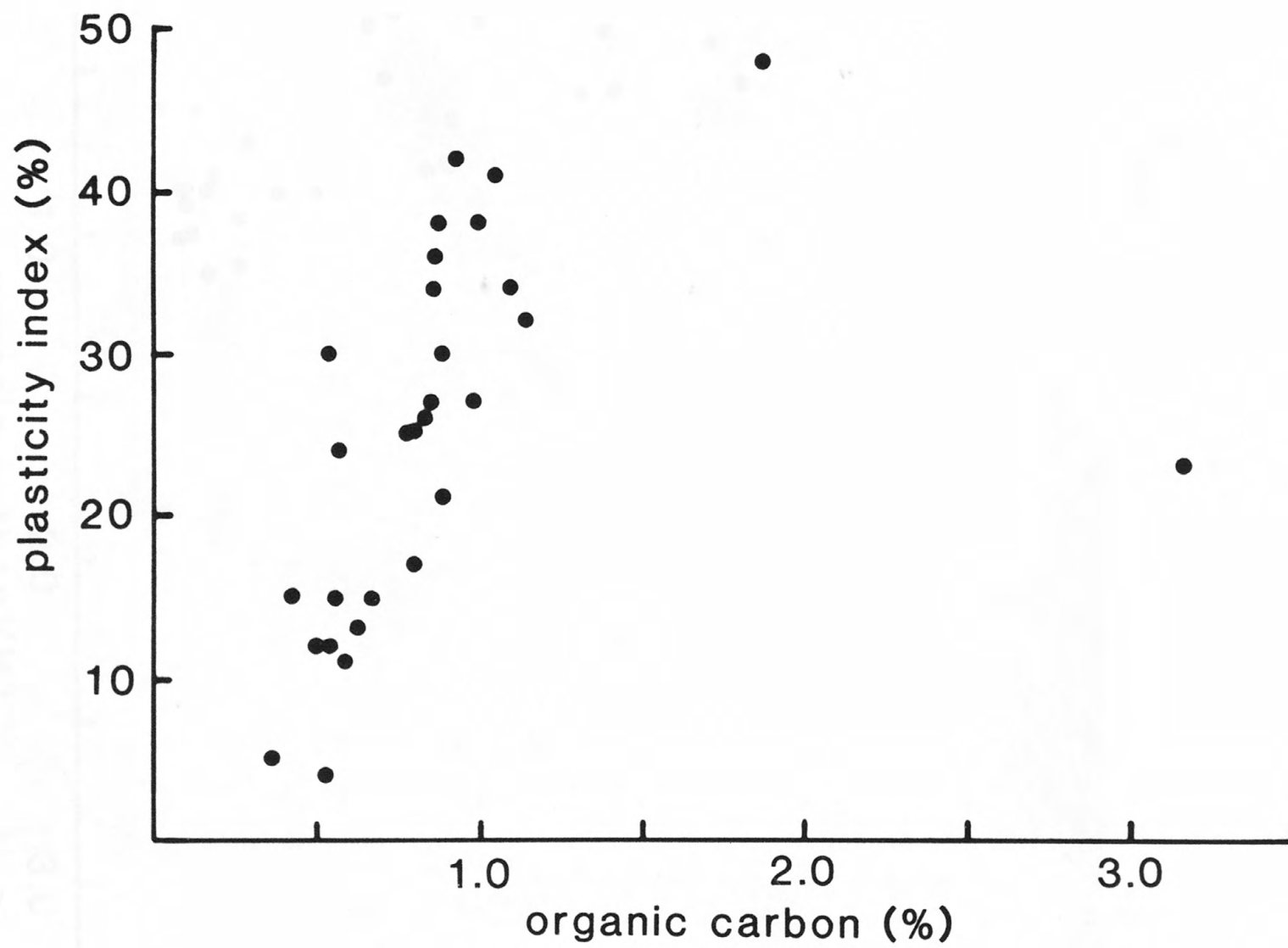
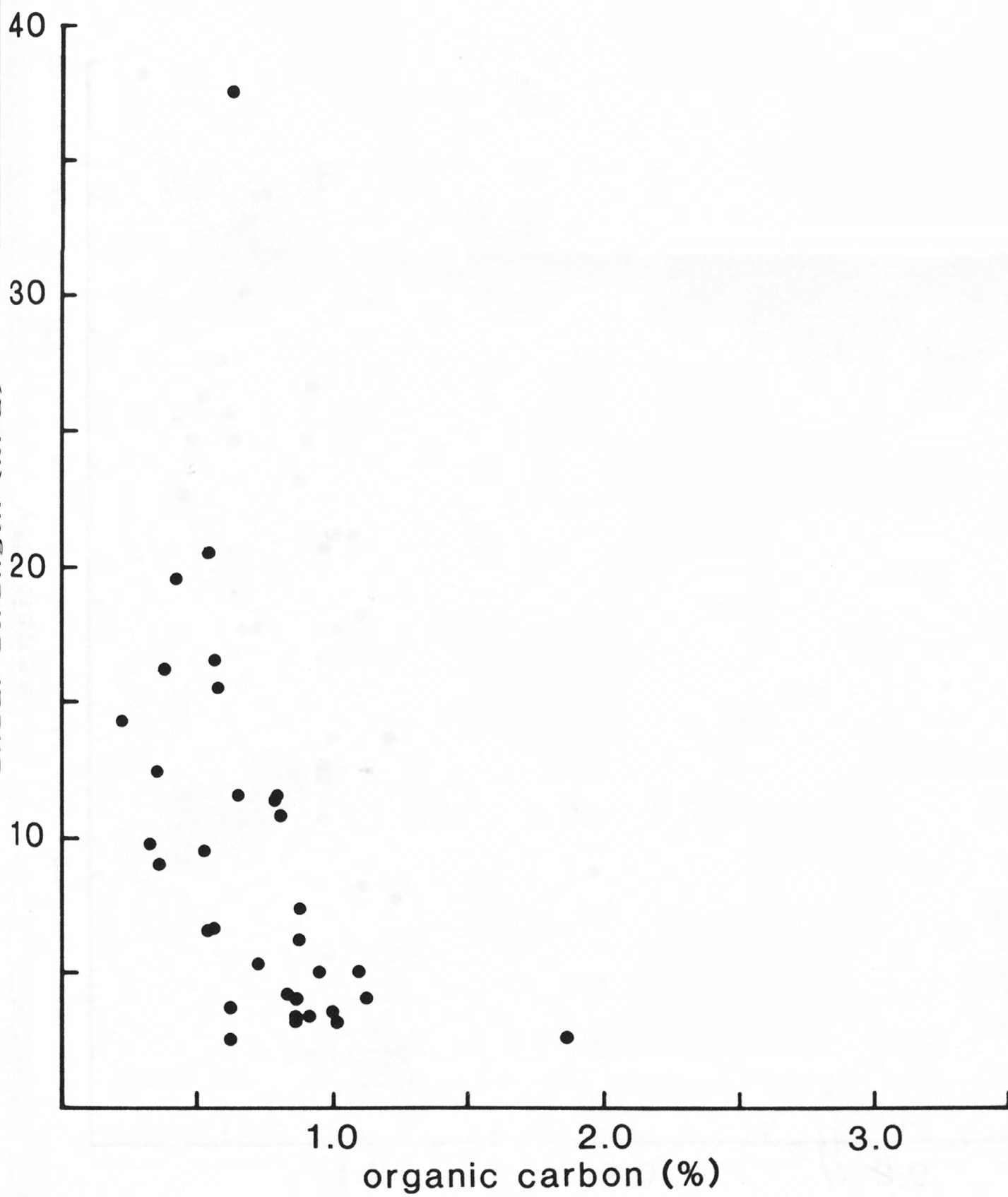


Fig. 25



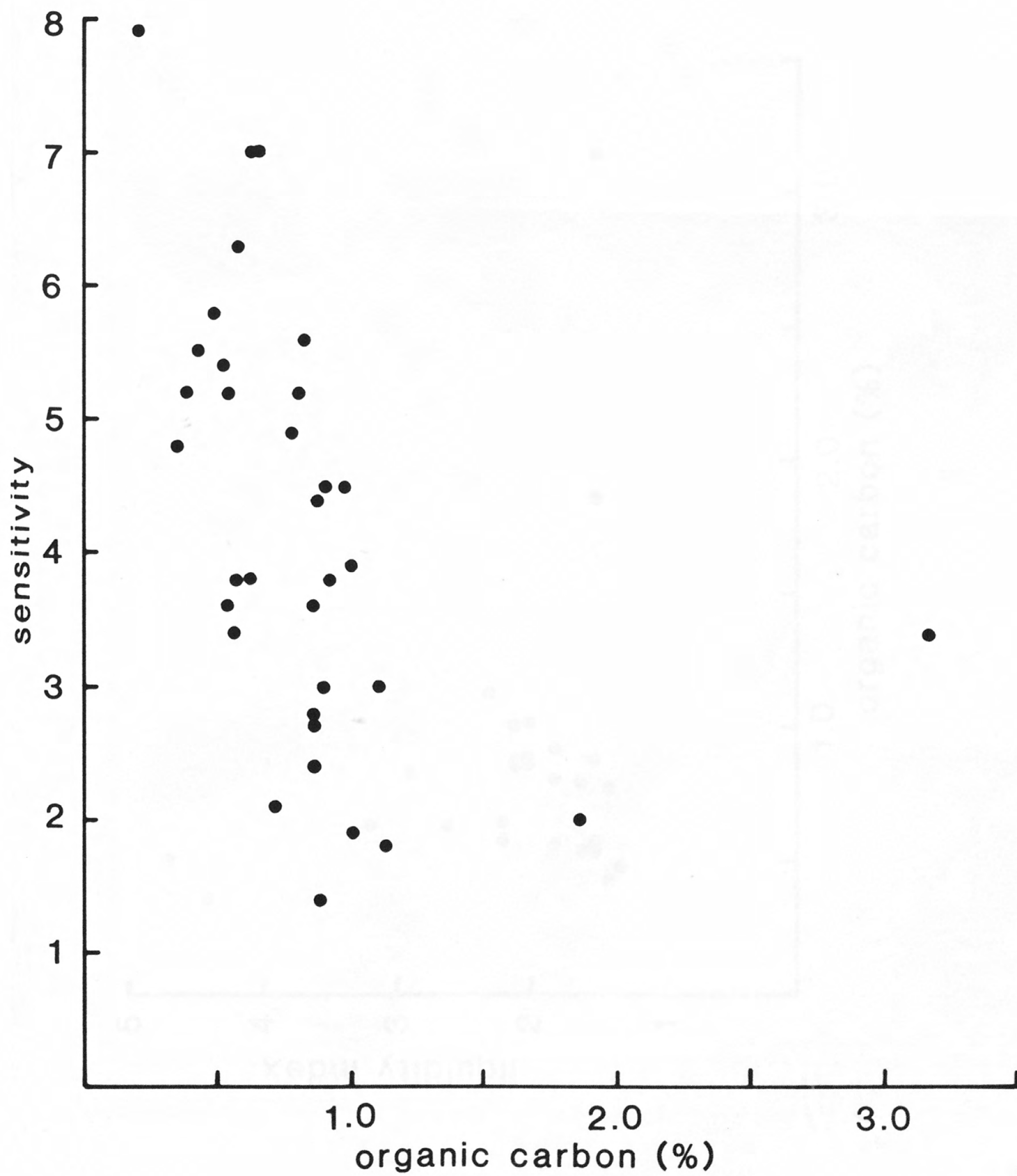


Fig. 27

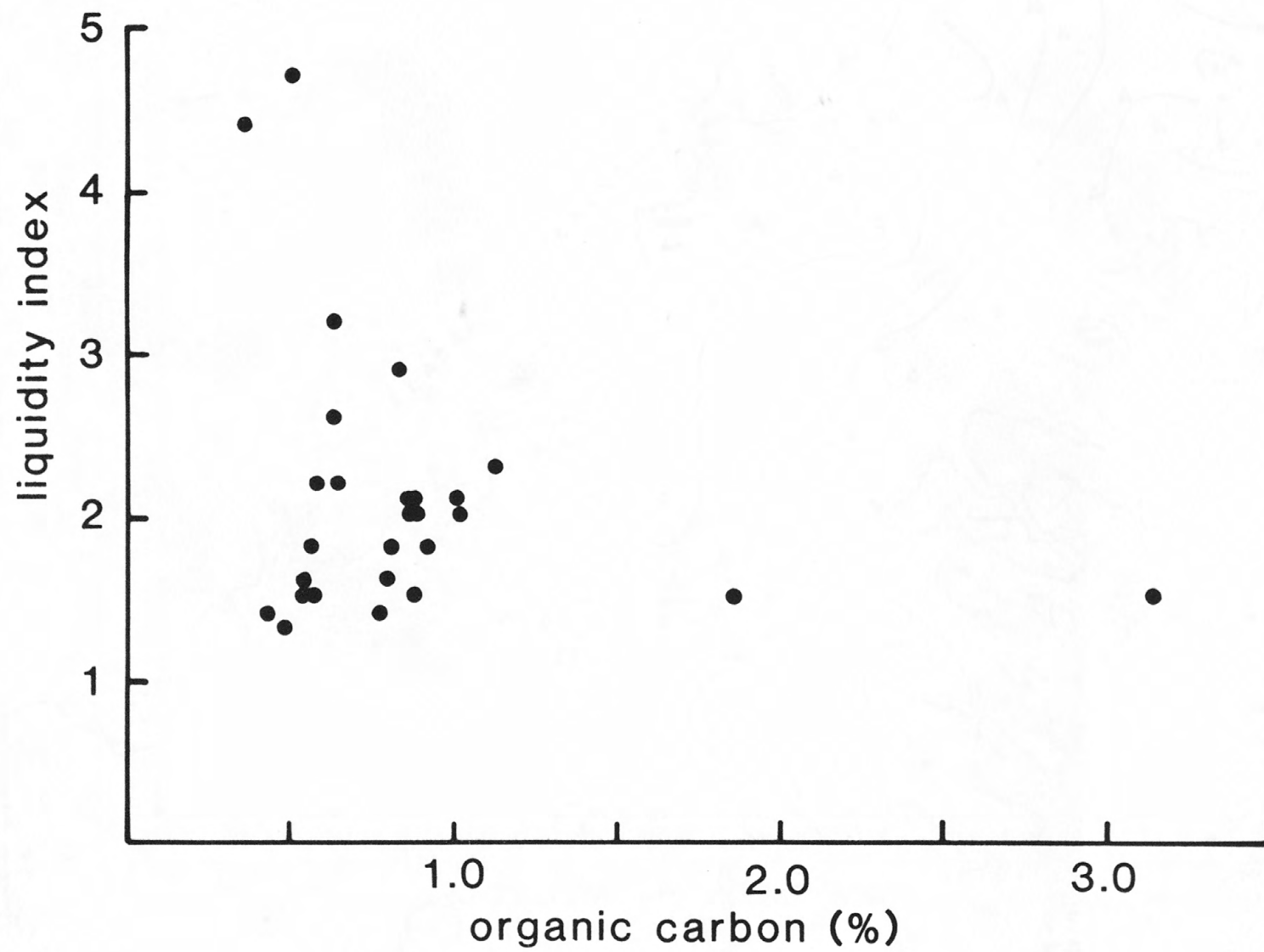


Fig. 28

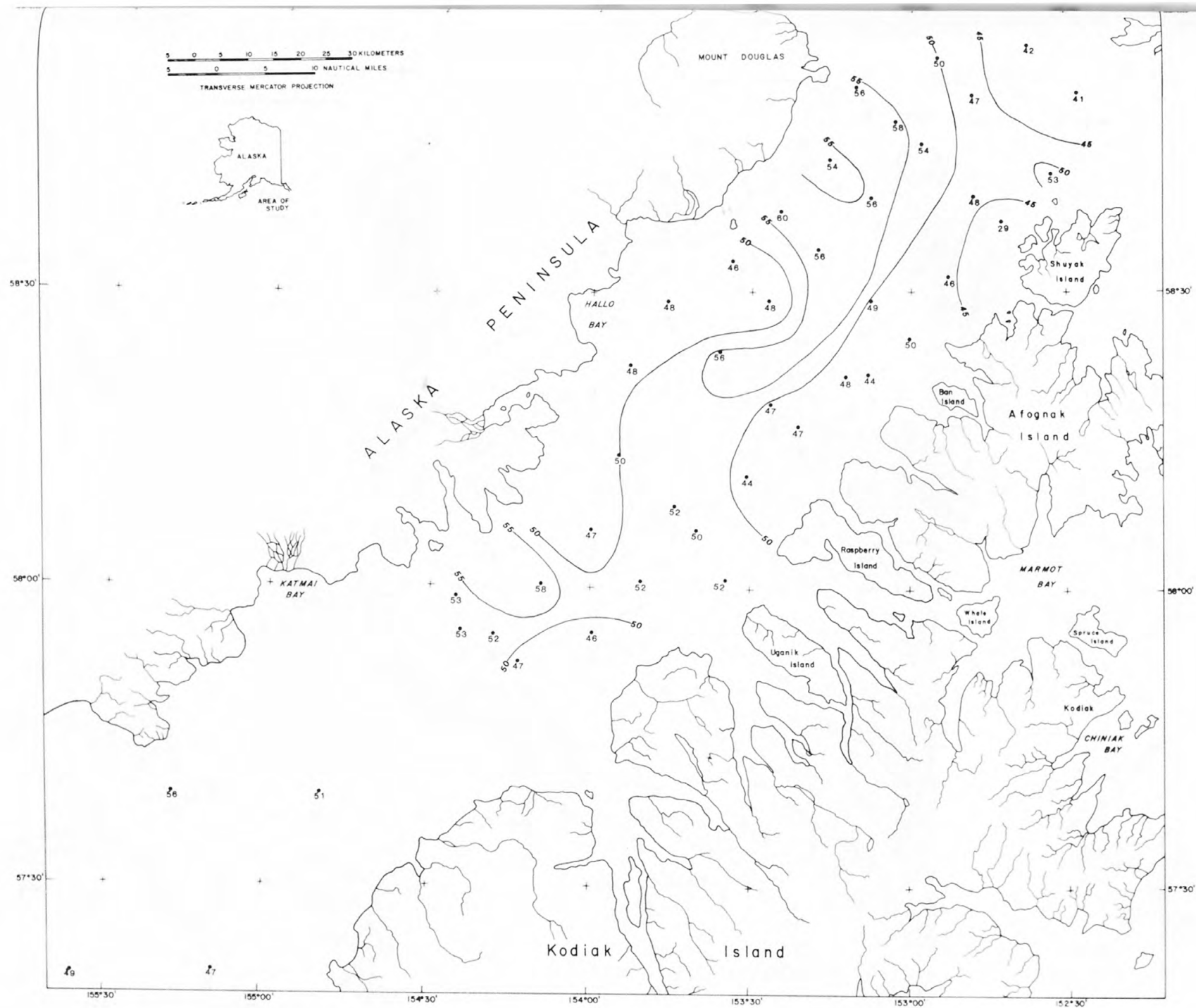


Fig. 29

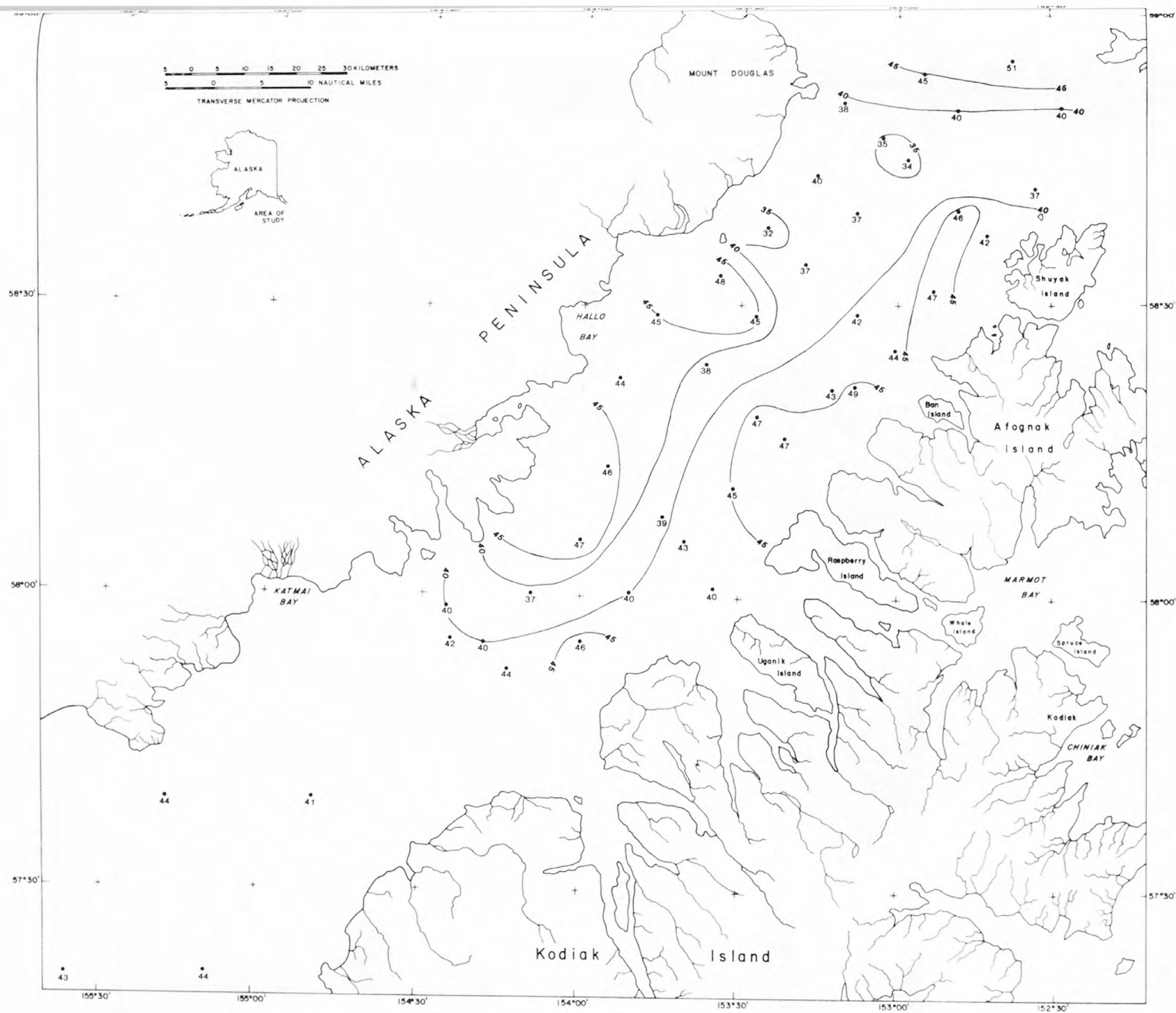


Fig. 30

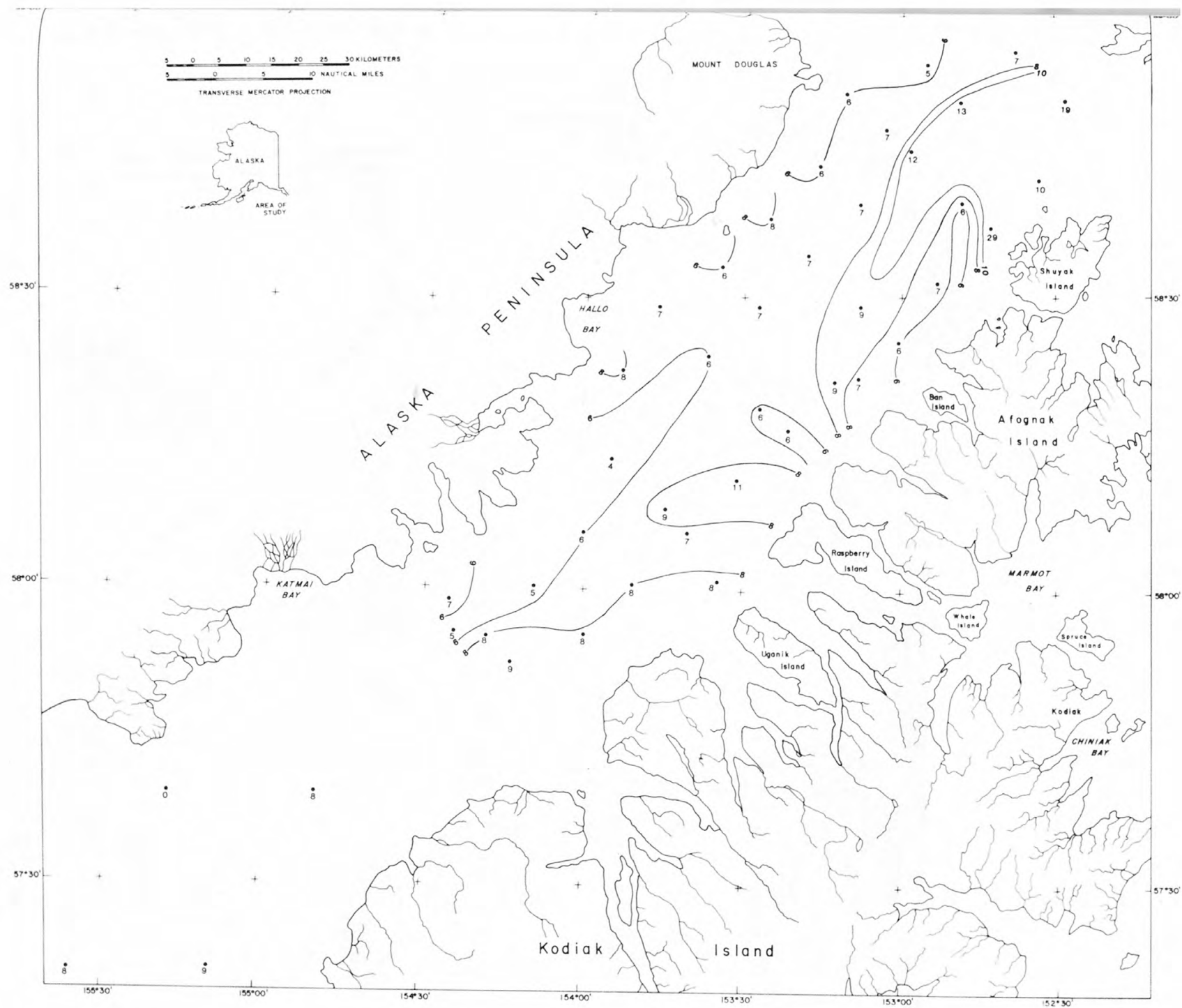
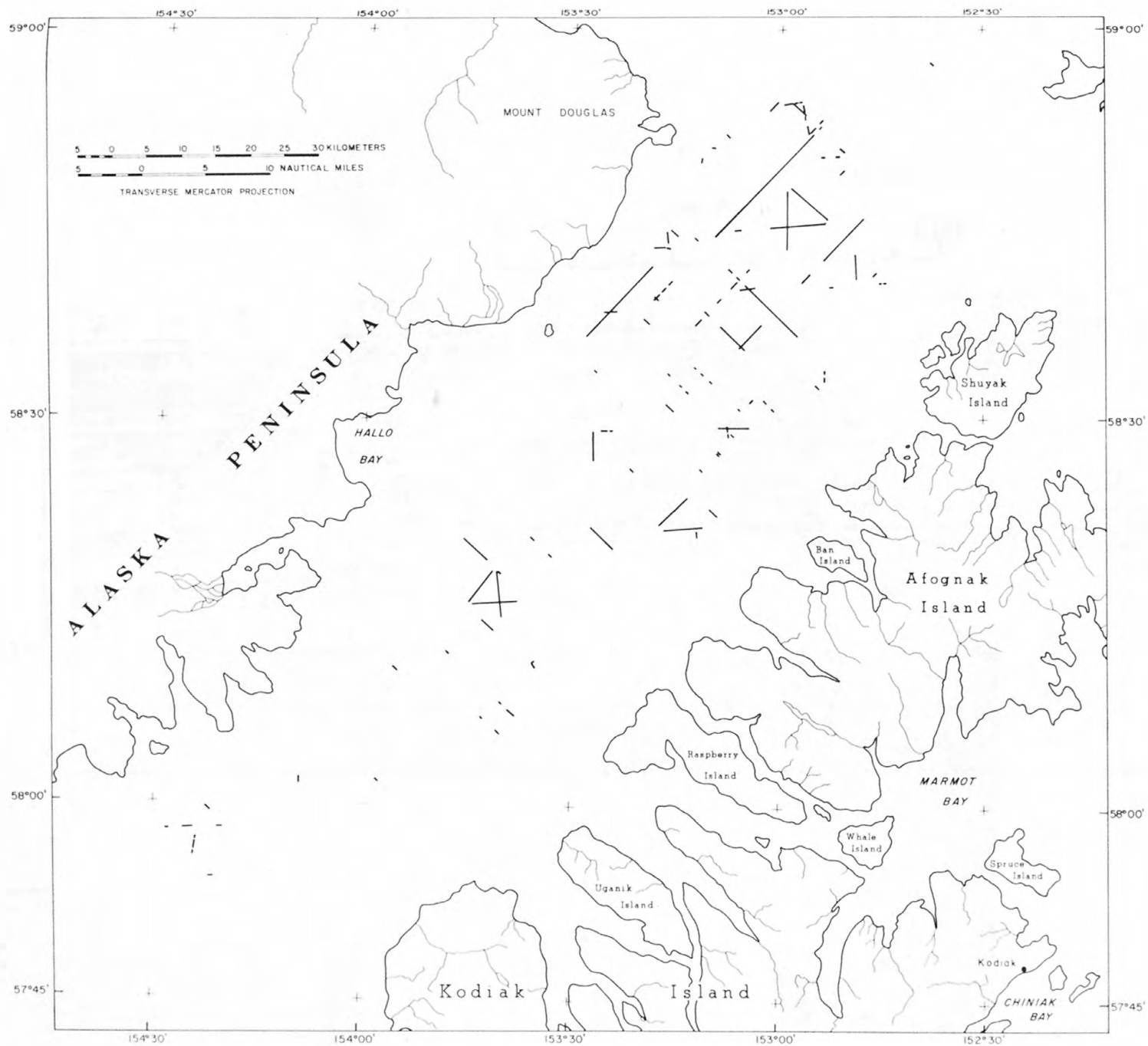


Fig. 31

CC



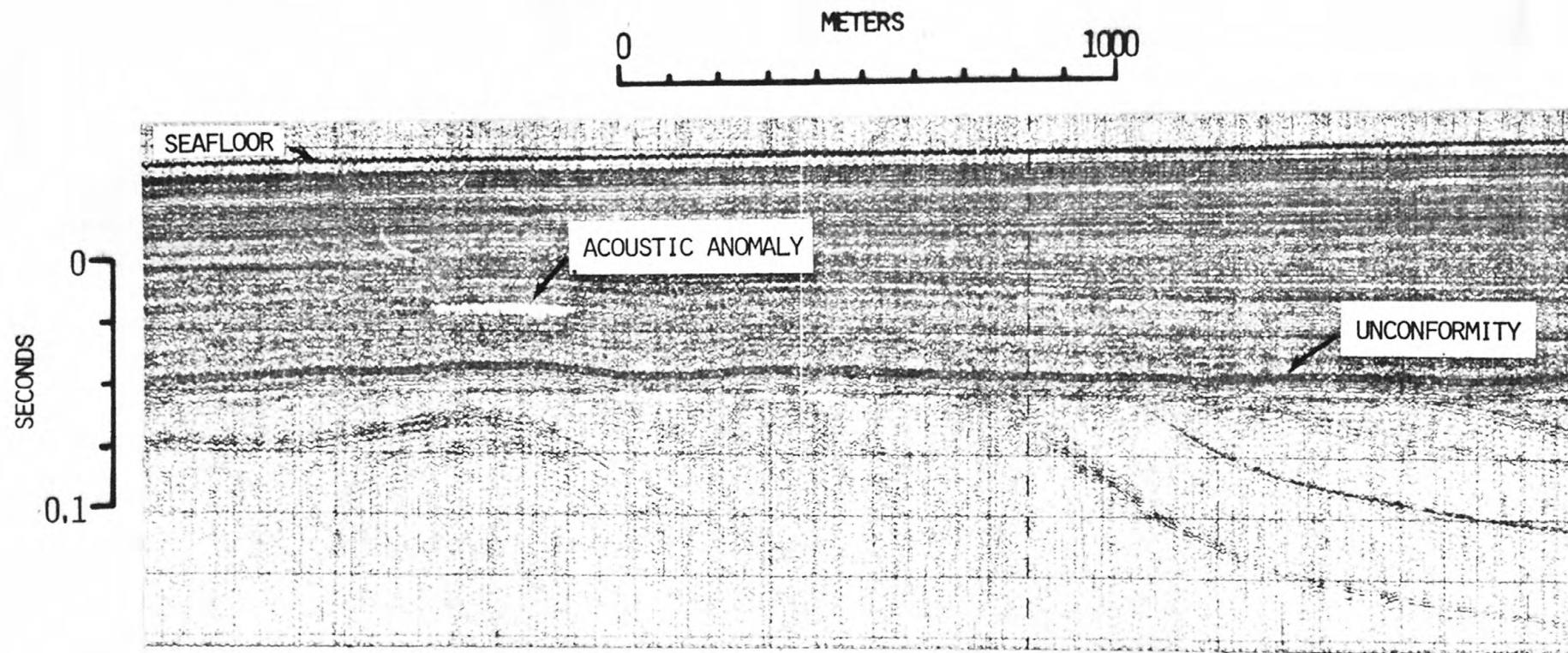


Fig. 33

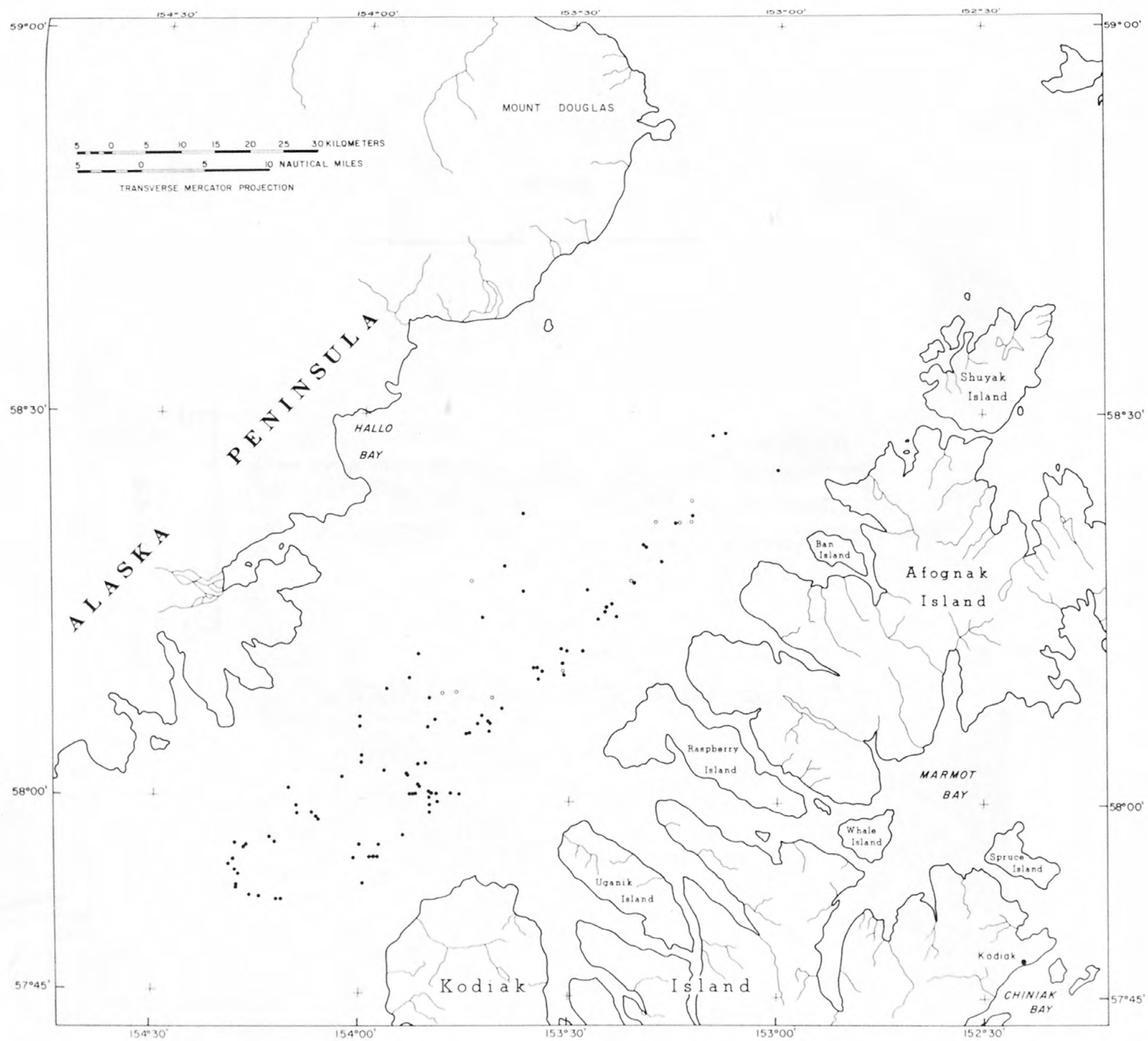


Fig. 24

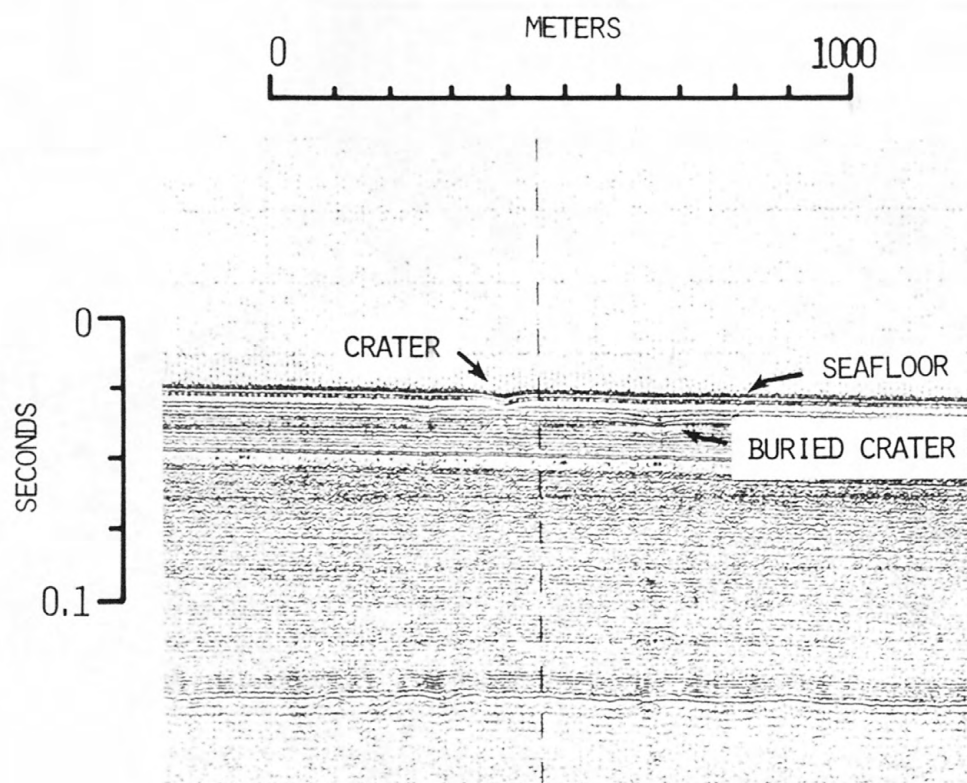


Fig. 35

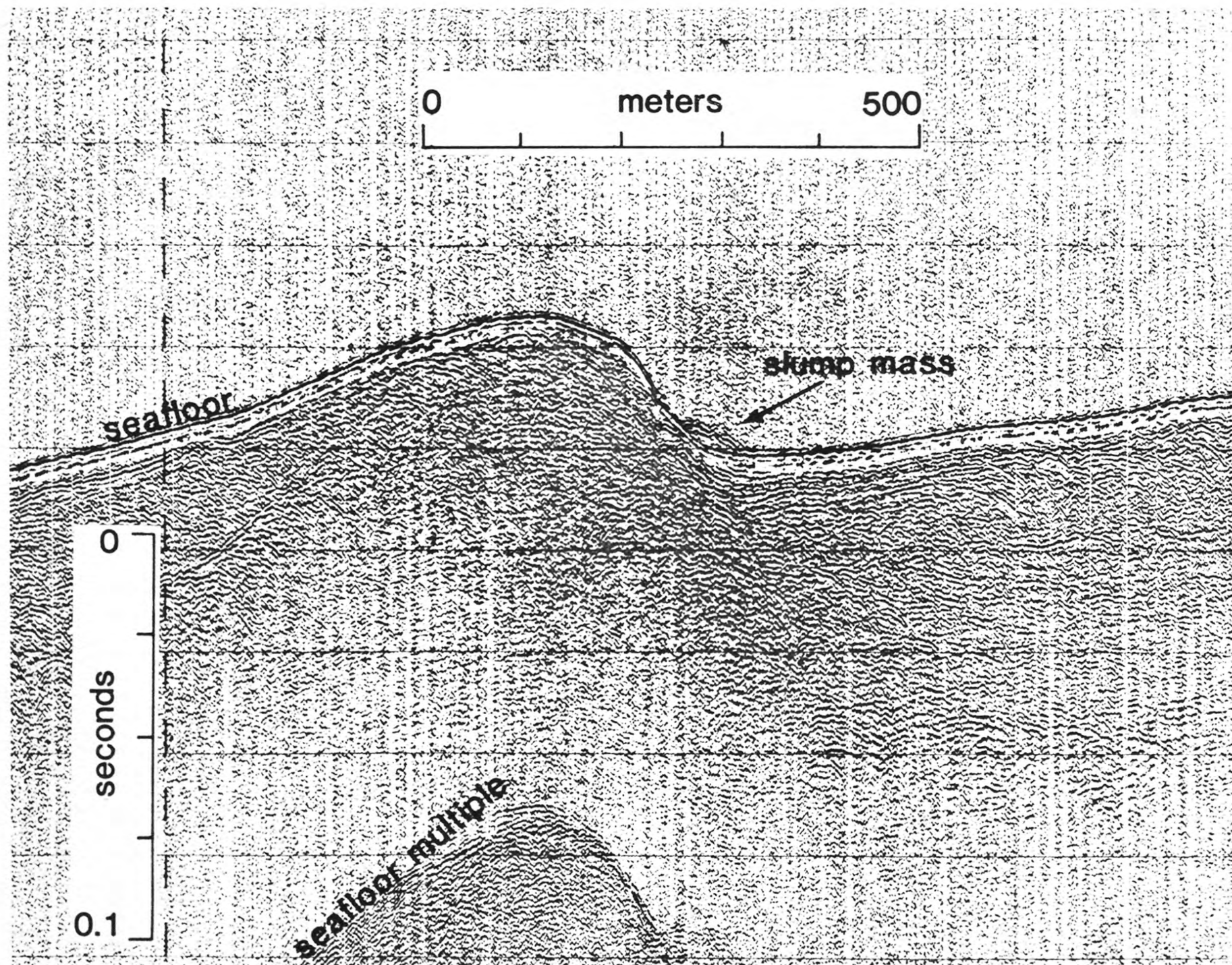


Fig. 36

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