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CATALOG OF EARTHQUAKES IN SOUTHERN ALASKA

APRIL-JUNE 1978



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This report (map) is preliminary and has not been reviewed for conformity with U.S. Geological Survey editorial standards (and stratigraphic nomenclature). Any use of trade names is for descriptive purposes only and does not imply endorsement by the U.S.G.S.

Menlo Park, California

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CATALOG OF EARTHQUAKES IN SOUTHERN ALASKA
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INTRODUCTION

The U.S. Geological Survey (USGS) began a regional program of telemetered seismic recording in south-central Alaska in 1971. The principal objectives of this program have been to use data recorded by this network to precisely locate earthquakes in the active seismic zones of southern Alaska, delineate seismically active faults, assess seismic risk, document potential premonitory earthquake phenomena, investigate current tectonic deformation, and study the structure and physical properties of the crust and upper mantle. A task fundamental to all of these goals is the routine cataloging of earthquake parameters for earthquakes located within and adjacent to the seismograph network.

The initial network of 10 stations, seven around Cook Inlet and three near Valdez, was installed in 1971. In subsequent summers additions or modifications to the network were made. By the fall of 1973, 26 stations extended from western Cook Inlet to eastern Prince William Sound, and four stations were located to the east between Cordova and Yakutat. A year later 20 additional stations were installed. Thirteen of these were placed along the eastern Gulf of Alaska with support from the National Oceanic and Atmospheric Administration (NOAA) under the Outer Continental Shelf Environmental Program to investigate the seismicity of the outer continental shelf, a region of interest for oil exploration. During the subsequent years the region covered by the network has remained relatively fixed while effort has been made to improve the instrumentation and installation of the stations in order to make them more reliable.

The locations of the stations of the USGS seismograph network are plotted in Figure 1 and listed in Table 1 along with the additional stations from which readings were obtained. Each USGS station has a single, vertical-component seismometer. The stations GLB, PNL, RDT, SKN, and VLZ also have north-south- and east-west-oriented horizontal seismometers.

This earthquake catalog presents origin times, focal coordinates, and magnitudes for 356 shocks occurring in the second quarter of 1978. Readings from a total of 71 stations were used to locate the shocks, including 12 stations operated by the NOAA Alaska Tsunami Warning Center (formerly Palmer Observatory), 14 stations operated by the Geophysical Institute of the University of Alaska (U. of A.), one station operated by the National Earthquake Information Service of the U.S. Geological Survey, and two stations operated in southwest Yukon Territory by the Department of Energy, Mines and Resources, Canada.

Earthquakes in south-central Alaska as small as magnitude 3.0 have been routinely located by the National Earthquake Information Service of the USGS and its predecessor since the great Alaska earthquake of 1964 and are published in the reports "Preliminary Determination of Epicenters" (PDE). In contrast, the shocks included in this catalog are as small as magnitude 0.5 and most are smaller than magnitude 3.0. Data for the larger historic earthquakes that occurred in south-central Alaska through 1975 have been tabulated by Meyers (1976).

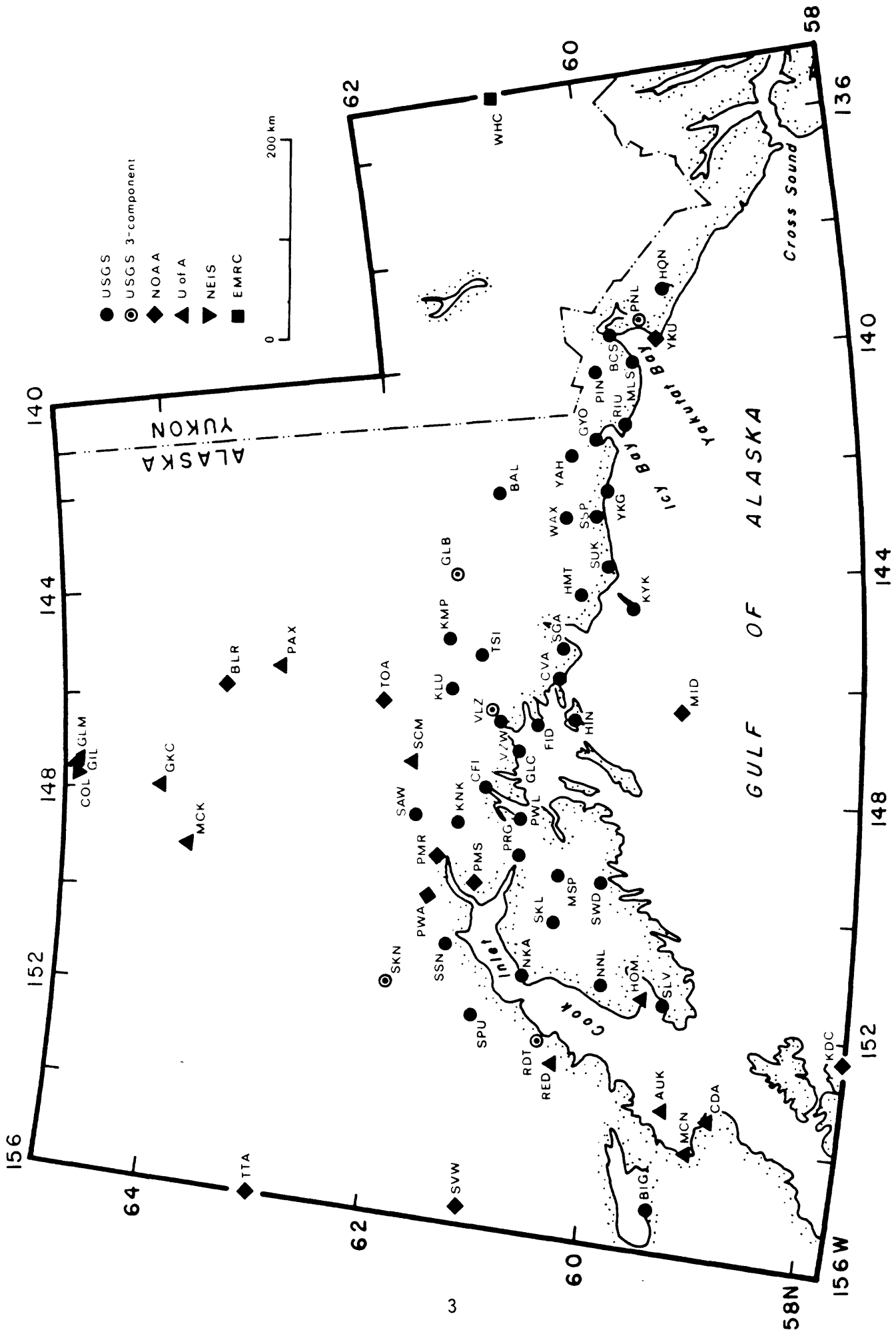


Figure 1. Map showing locations of USGS and other seismograph stations used in the preparation of this catalog.

Table 1. Station Data

STA CODE	STATION NAME	LATITUDE N	LONGITUDE W	ELEV M	P MOD	D KM	DLY1 SEC	DLY2 SEC	DLY3 SEC	TDLY SEC	MAG AT 1 HZ	INST
AUK	AUGUSTINE ISLAND	59 20.10	153 25.66	293	1	0.01	0.0	0.0	0.0	0.0		LCFA
AUM	AUGUSTINE MCLND	59 22.26	153 21.17	106	1	0.01	0.0	0.0	0.0	0.0		LCFA
BAL	BALDY	61 2.17	142 20.67	1300	3	0.01	0.0	0.0	-0.16	0.0	240000	USGS
BGS	BANCAS PCINT	59 56.50	135 37.00	10	3	0.01	0.0	0.0	-0.85	-0.27	30000	USGS
BIG	BIG MOUNTAIN	59 23.34	155 13.02	567	1	0.01	0.0	0.0	0.0	0.0	120000	USGS
BLR	BLACK RAFTS	63 30.10	145 50.70	805	2	0.01	0.0	0.0	0.0	0.0		NCAA
CDA	CAPE DUGLAS	58 57.32	153 31.77	386	1	0.01	0.0	0.0	0.0	0.0		LCFA
CFI	COLLEGE FICRD	61 10.96	147 45.59	3	2	0.01	0.0	0.0	0.0	0.0	120000	USGS
CUL	COLLEGE CUTPCST	64 54.00	147 47.60	320	2	0.01	0.0	0.0	0.0	0.0		NEIS
CVA	CORDOVA	60 32.79	145 44.96	90	2	0.01	0.0	0.0	0.0	-0.27		USGS
FID	FIDALGO	60 43.73	146 35.79	482	2	0.01	0.0	0.0	0.0	-0.27	240000	USGS
FYU	FCRT YUKEN	66 33.63	145 12.60	137	1	0.0	0.0	0.0	0.0	0.0		LCFA
GIL	GILMORE CREEK	64 58.50	147 29.70	350	1	0.01	0.0	0.0	0.0	0.0		NCAA
GKC	GOLD KING CREEK	64 10.72	147 56.08	490	1	0.0	0.0	0.0	0.0	0.0		LCFA
GLB	GILAHINA BLTTE	61 26.51	143 48.63	845	3	0.01	0.0	0.0	1.60	0.0	378000	USGS
GLC	GLACIER ISLAND	60 53.44	147 4.38	3	2	0.01	0.0	0.0	0.0	-0.27	171000	USGS
GLM	GILMORE DOME	64 59.23	147 23.33	220	2	0.01	0.0	0.0	0.0	0.0		LCFA
GYO	GLYCT HILLS	60 8.78	141 28.29	162	3	0.01	0.0	0.0	-0.06	-0.27	120000	USGS
HIN	HINCHINBROCK ISLAND	60 23.81	146 30.10	611	2	0.01	0.0	0.0	2.09	-0.27	240000	USGS
HMT	HAMILTON	60 20.19	144 15.64	620	3	0.01	0.0	0.0	-0.55	-0.27	120000	USGS
HDM	HOMER	59 39.50	151 38.60	192	1	0.01	0.0	0.0	0.0	0.0		LCFA
HON	HARLEQUIN	59 27.10	135 52.62	372	3	0.01	0.0	0.0	0.0	-0.27	120000	USGS
IMA	INDIAN MCLTAIN	66 4.11	153 40.72	1360	1	0.01	0.0	0.0	0.0	0.0		NCAA
KDC	KGDIAK	57 44.87	152 29.50	13	1	0.01	0.0	0.0	0.0	0.0		NCAA
KLU	KLUTINA	61 29.57	145 55.21	1021	2	0.01	0.0	0.0	0.0	0.0	216000	USGS
KMP	KIMBALL PASS	61 30.78	145 1.09	1143	2	0.01	0.0	0.0	0.0	-0.27	171000	USGS
KNK	KNIK GLACIER	61 24.75	148 27.34	595	2	0.01	0.0	0.0	0.0	0.0	60000	USGS
KYK	KAYAK ISLAND	59 52.10	144 31.35	375	2	0.01	0.0	0.0	1.57	-0.27	60000	USGS
MCK	MCKINLEY PARK	63 43.54	148 56.10	610	1	0.01	0.0	0.0	0.0	0.0		LCFA
MCH	MCNEIL RIVER	59 6.06	154 11.59	273	1	0.01	0.0	0.0	0.0	0.0		LCFA
MID	MIDDLETON ISLAND	59 25.67	146 20.34	37	1	0.01	0.0	0.0	0.0	-0.27		NCAA
MLS	MALASPINA GLACIER	59 46.00	140 9.00	30	3	0.01	0.0	0.0	0.0	-0.27	15000	USGS
MSP	MCDON PASS	60 25.35	149 21.64	150	1	0.01	0.0	0.0	0.0	0.0	120000	USGS
NKA	NIKISHKA	60 44.58	151 14.26	100	1	4.00	1.36	0.0	0.0	0.0	9000	USGS
NNL	NINILCHIK	60 2.53	151 17.78	362	1	4.00	0.67	0.0	0.0	0.0	126000	USGS
PAX	PAXSON	62 58.25	145 28.11	1130	2	0.01	0.0	0.0	0.0	0.0		LCFA
PIN	PINNACLE	60 5.80	140 15.40	975	3	0.01	0.0	0.0	-0.01	-0.27	60000	USGS
PMR	PALMER RESERVATORY	61 35.53	149 7.85	100	1	0.01	0.0	0.0	0.0	0.0		NCAA
PMS	ARCTIC VALLEY	61 14.68	149 33.63	716	1	0.01	0.0	0.0	0.0	0.0		NCAA
PNL	PENINSULA	59 40.06	135 23.82	585	3	0.01	0.0	0.0	-1.10	-0.27	60000	USGS
PRG	PORTAGE	60 51.87	149 1.21	35	1	0.01	0.0	0.0	0.0	0.0	198000	USGS
PWA	HOUSTON	61 39.65	145 52.72	137	1	0.01	0.70	0.0	0.0	0.0		NCAA
PWL	PORT BELLS	60 51.56	148 20.09	545	2	0.01	0.0	0.0	0.0	0.0	120000	USGS
RDY	REDDUBT	60 34.43	152 24.37	930	1	0.01	0.36	0.0	0.0	0.0	120000	USGS
RED	REDDUBT VOLCANO	60 25.14	152 46.32	1067	1	0.01	0.0	0.0	0.0	0.0		LCFA
RIU	RIOU	59 52.65	141 13.80	15	3	0.01	0.0	0.0	1.09	-0.27	7800	USGS
SAB	SABMILL	61 48.49	148 19.98	740	2	0.01	0.0	0.0	0.0	0.0	240000	USGS
SCM	SHEEP MOUNTAIN	61 50.00	147 19.66	1020	2	0.01	0.0	0.0	0.0	0.0		LCFA
SGA	SHERMAN GLACIER	60 32.44	145 12.42	424	2	0.01	0.0	0.0	2.17	-0.27	60000	USGS
SKD	SITKALIDAK ISLAND	57 9.85	153 4.82	135	1	0.01	0.0	0.0	0.0	0.0		LCFA
SKL	SKILAK	60 30.86	150 12.56	690	1	0.01	0.10	0.0	0.0	0.0	120000	USGS
SKN	SKWENTNA	61 58.82	151 31.76	564	1	0.01	0.0	0.0	0.0	0.0	240000	USGS
SLV	SELDOVIA	59 28.28	151 34.83	91	1	0.01	0.0	0.0	0.0	0.0	30000	USGS
SPU	SPURR	61 10.90	152 3.26	800	1	0.01	0.39	0.0	0.0	0.0	240000	USGS
SSN	SUSITNA	61 27.63	150 44.60	1297	1	0.01	0.67	0.0	0.0	0.0	30000	USGS
SSP	SUNSHINE PCINT	60 12.30	142 49.80	305	3	0.01	0.0	0.0	0.75	-0.27	120000	USGS
SUK	SUCKLING HILLS	60 3.32	143 47.31	295	3	0.01	0.0	0.0	2.14	-0.27	120000	USGS
SVW	SPARREVECHN	61 6.49	155 37.30	762	1	0.01	0.0	0.0	0.0	0.0		NCAA
SWD	SEWARD	60 6.22	149 26.96	91	1	0.01	0.0	0.0	0.0	0.0	30000	USGS
TNN	TANANA	65 15.40	151 54.70	504	1	0.01	0.0	0.0	0.0	0.0		LCFA
TGA	TCLSONA	62 6.29	146 10.34	505	2	0.01	0.0	0.0	0.0	0.0		NCAA
TSI	TSINA	61 13.57	145 20.24	1113	2	0.01	0.0	0.0	0.0	-0.27	120000	USGS
TTA	TATALINA	62 55.80	156 1.32	514	1	0.01	0.0	0.0	0.0	0.0		NCAA
VLZ	VALDEZ	61 7.89	146 19.52	10	2	0.01	0.0	0.10	0.0	-0.27	60000	USGS
VZW	VALDEZ WEST	61 3.54	146 33.24	796	2	0.01	0.0	0.0	0.0	-0.27	120000	USGS
WAX	WAXELL RIDGE	60 26.50	142 51.10	975	3	0.01	0.0	0.0	0.61	-0.27	30000	USGS
WHC	WHITEHORSE	60 44.20	135 5.50	732	3	0.01	0.0	0.0	2.55	0.0		EMRC
YAH	YAHTESE	60 21.51	141 44.70	213	3	0.01	0.0	0.0	0.17	-0.27	60000	USGS
YKC	YELLOWKNIFE	62 28.70	114 28.70	192	3	0.01	0.0	0.0	0.0	0.0		EMRC
YKG	YAKATGA	60 4.20	142 25.33	46	3	0.01	0.0	0.0	0.0	-0.27	7800	USGS
YKU	YAKUTAT	59 32.72	135 43.73	15	3	0.01	0.0	0.0	0.35	-0.27		NCAA

This table lists geographic coordinates and other pertinent information for stations used in the preparation of this catalog. P-MOD is the number of the P-wave velocity model assigned to the station (see text), where the numbers 1, 2, and 3 correspond to the western, central and eastern models. D is the thickness of the low-velocity surficial sedimentary layer in kilometers assigned in the calculation of traveltime delays to a given station. DLY1-3 are the station P-phase traveltime delays in seconds. TDLY is the telephone line delay in seconds. The magnification (MAG) of the vertical seismograph component is given at 1 Hz. The institutions (INST) operating the stations other than the USGS Office of Earthquake Studies are the NOAA Alaska Tsunami Warning Center, the Geophysical Institute of the University of Alaska (UOFA), the National Earthquake Information Service (NEIS), and the Department of Energy, Mines and Resources, Canada (EMRC).

INSTRUMENTATION

The instrumentation in the USGS seismograph network is illustrated in the block diagram in Figure 2. Data from each seismometer are telemetered to the NOAA Alaska Tsunami Warning Center in Palmer. The standard equipment at each field station includes a vertical seismometer with a natural frequency of 1.0 Hz (Mark Products, Model L-4), a package consisting of an amplifier and a voltage-controlled oscillator (VCO model NCER 202, or ALVCO, see Rogers and others, 1980), and "air-cell" storage batteries (McGraw-Edison, Model ST-2-1000). The ALVCO crystal-referenced units have an automatic gain-ranging capability and provide daily information on the gain setting, geophone response, battery voltage, station identification, and temperature. Data are telemetered via a combination of leased telephone circuits (some of which are relayed by satellite and have a -0.27 sec delay) and VHF (162-174 MHz) radio links. The radio equipment consists of low-power transmitters (100 mW) and receivers adapted from HT-200 Motorola handie-talkie transceivers. Yagi antennae with 9 db directional gain (Scala, Model CAS-150) are used. At some sites where AC power is available, base-station radio receivers (G.E. Model R46AP66B) with greater sensitivity and reliability are used. The central recording facility incorporates a bank of discriminators (NCER J101 or Develco Model 6203), four 16 mm-film multi-channel oscillographs (Teledyne Geotech Develocorder, Model 4000D), a 14-channel analog tape recorder (Bell and Howell Model VR3700B), and a time-code generator (Datum, Model 9100).

The principle of operation is as follows: The seismometer translates movement of the ground into an electrical voltage that is fed into the amplifier/VCO unit where the amplified voltage causes the frequency of an audio-band oscillator to fluctuate about its center frequency. The frequency-modulated (FM) tone from the amplifier/VCO unit is carried directly by voice-grade telephone circuit to the recording site or alternately is fed through a VHF radio link onto a telephone circuit. At the recording site the FM seismic signal is demodulated by a discriminator. The demodulated signal, which is simply an amplified form of the initial signal from the seismometer, is recorded photographically on a multichannel oscillograph, together with time marks from a crystal-controlled chronometer. Twenty-four hours of data for 18 stations can be recorded on a single 43-m-long roll of 16-mm film.

Signals from more than one seismograph can be transmitted on a single telephone circuit by employing VCO units with different center frequencies. In the standard configuration there is a 340 Hz separation between center frequencies and a fixed bandwidth of 250 Hz. Up to eight seismic channels with center frequencies ranging from 680 to 3060 Hz may be placed on a single voice-grade telephone circuit.

Figure 3 illustrates the response characteristics of the entire seismic system from seismometer to film viewer. The response level at each station is adjusted in steps of 6 decibels so that the ambient seismic noise produces a small deflection of the trace on the film. As a result, the actual response for an individual station may differ from that of the typical station by a factor of 2, 4, 8, etc. The magnification of the typical station is about 6×10^4 at 1 Hz and 10^6 at 10 Hz. The gain of a station that has an ALVCO

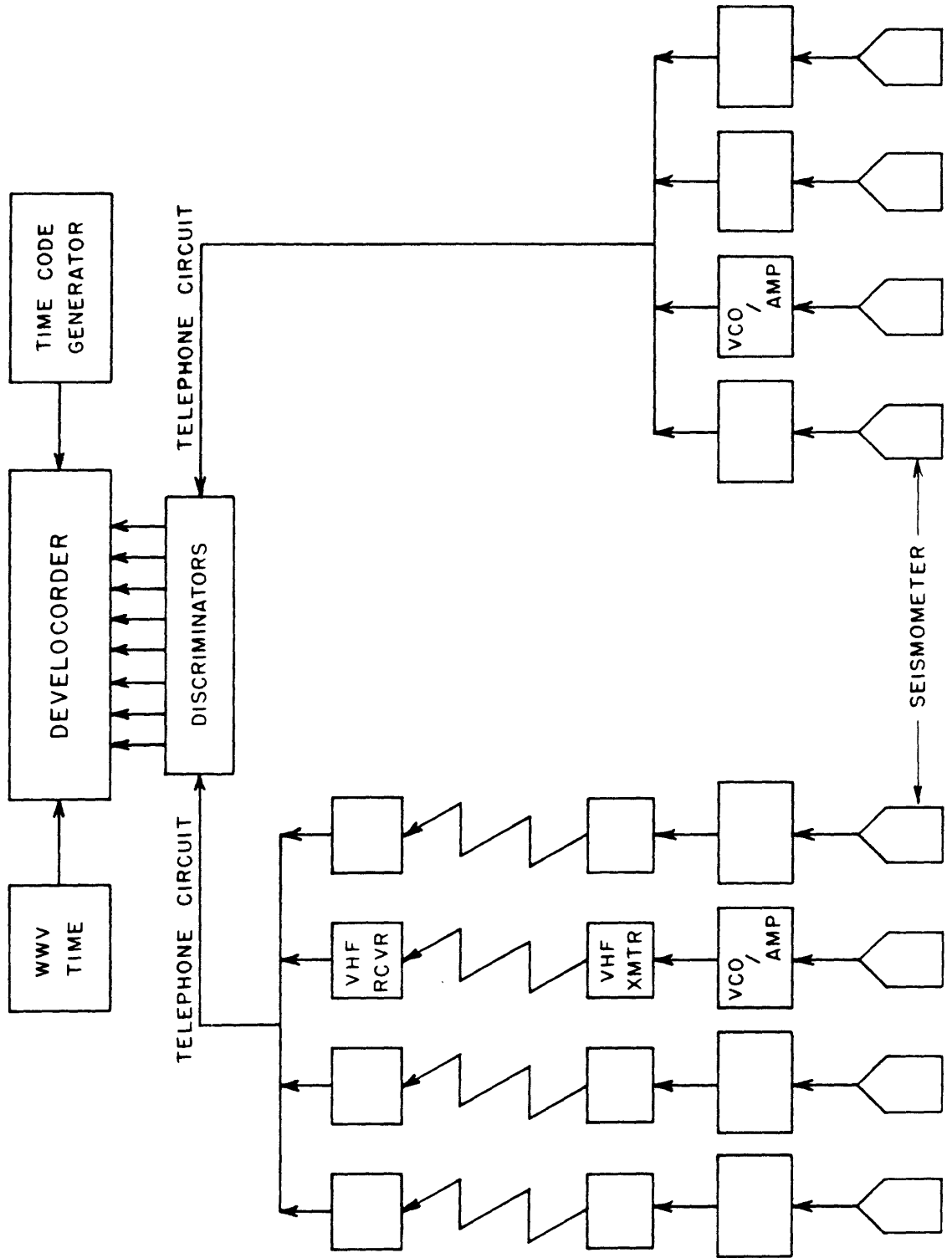


Figure 2. Block diagram of teletempered seismograph system in the USGS Alaska seismic network.

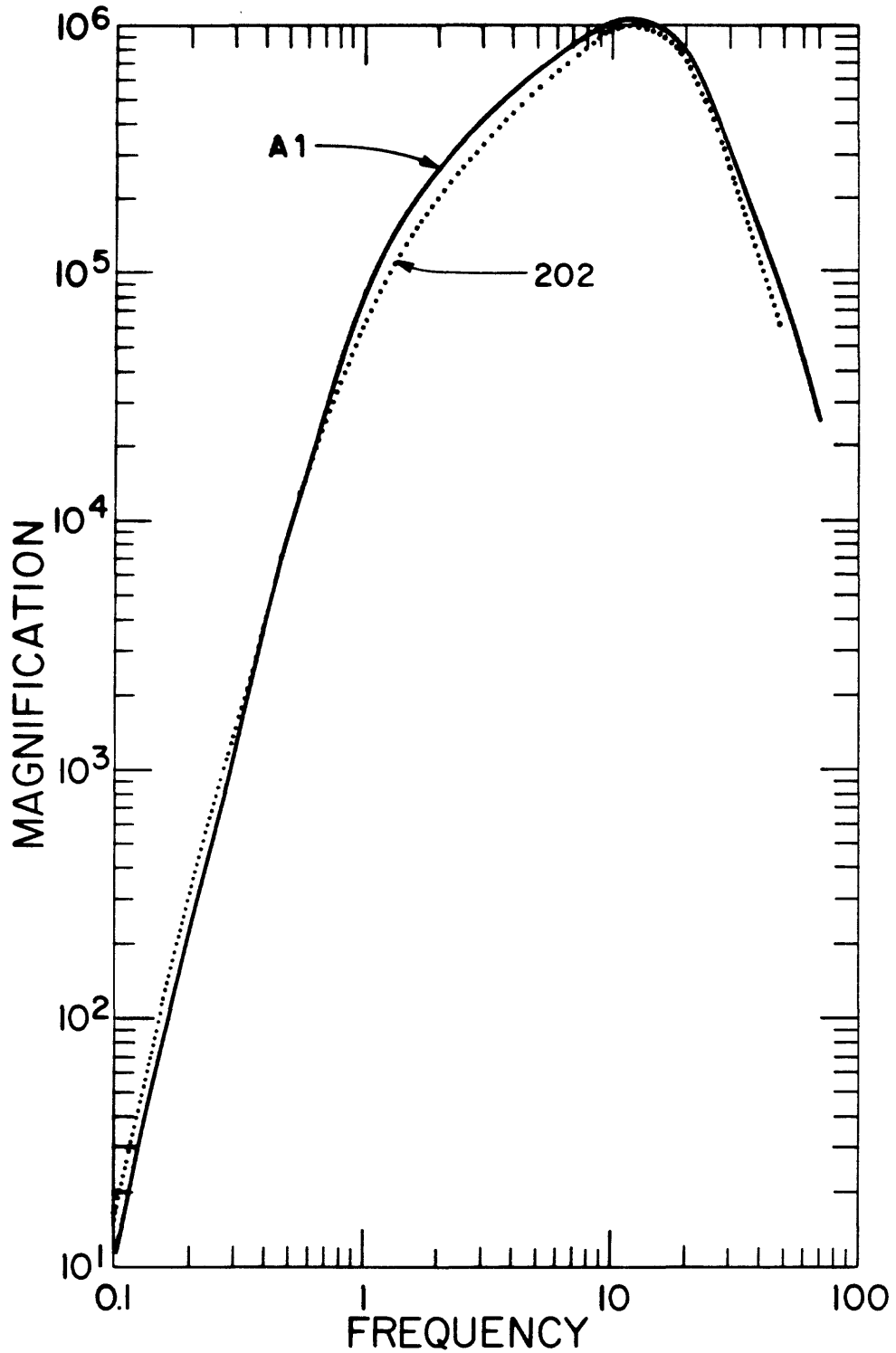


Figure 3. System response curves for typical USGS Alaska seismographs that incorporate the A1VCO unit (solid curve) and the older VCO model NCER 202 unit (dotted curve).

unit is automatically reduced by a factor of 10 when the fluctuations of the FM signal exceed a preset threshold.

The installation of a typical radio-linked station is shown in Figure 4. Degradation or interruption of data transmission due to inclement weather conditions is a major problem during the winter months. Some indication of the operational reliability of the USGS stations can be inferred from the plot of station use in Figure 5.

DATA PROCESSING

The 16-mm films (four per day) are mailed weekly from Palmer to Menlo Park where the seismic data are processed by the following multi-step routine:

1. Scanning. The scan film, which has 18 stations distributed throughout the network, is scanned to identify and note times of all seismic events whether of local, regional, or teleseismic origin.

2. Timing. For the "well-recorded" local earthquakes identified in the scanning process, the following data are read from each station: P- and S-wave arrival times, direction of first motion, duration of signal in excess of a given threshold amplitude, and period and amplitude of maximum recorded signal. The criterion for choosing earthquakes to be timed is the duration of the signal, which is related to the magnitude. The network is divided into three regions--western, central, and eastern--bounded approximately by longitudes 156° and 150° W, 150° and 145° W, and 145° and 138° W, respectively. In the western and central regions, only events with signal durations longer than 80 s and 20 s, respectively, are timed. In the eastern region, all earthquakes which are recorded by at least three stations and for which at least four clear arrivals can be read are timed. This criterion was established to select from the large number of earthquakes recorded by the network those shocks that are of greatest interest to current research objectives.

For this catalog, timing the seismic phases and measuring the waveform amplitude was accomplished by utilizing a newly-developed system consisting of a computer-based sonic digitizing table with interactive data processing capabilities (Pelton and others, 1982). The system has four main components including (1) an optical film transport unit that can display portions of up to four 16-mm Develocorder films concurrently, (2) a sonic digitizing unit activated by a hand-controlled cursor, (3) a microcomputer that controls the data organization and processing tasks, reduces the digitized data, computes a preliminary hypocenter location and magnitude, and provides an interface with a larger computer for final processing, and (4) a video display for easy monitoring of the current processing sequence, and a printer for permanent recording of each data analysis session. The system is designed to process one earthquake at a time and allow selective remeasurement of any digitized datum. This method is a significant improvement over the standard multi-step processing routine (for example, Lahr and others, 1974) where only one film at a time is viewed and digitized on a non-interactive basis and nearly all subsequent processing is done in a batch mode.



Figure 4. Installation of a typical seismograph station (ILM). VCO/amplifier unit, radio transmitter, and batteries are housed in a 30-inch diameter culvert partially set in the ground at the base of the antenna. Seismometer is buried in the ground about 30 meters from the culvert.

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Final computer processing is done utilizing the computing facilities at the Stanford Linear Accelerator Center and the computer program HYPOELLIPSE (Lahr, 1980). For shocks with a poor distribution of reporting stations, readings from additional stations outside the USGS network are sought and added.

The earthquake locations are based on P and S arrivals. S arrivals are important for determining epicenters of shocks outside the network and depths of events in the Benioff zone beneath the network in Cook Inlet. Unfortunately for some large events, S cannot be read at any station because the traces on the film overlap each other or are too faint to follow.

The HYPOELLIPSE computer program determines hypocenters by minimizing differences between observed and computed traveltimes through an iterative least-squares scheme. In many respects the program is similar to HYP071 (Lee and Lahr, 1972), which has been used in the preparation of catalogs of central California earthquakes since January 1969. An important feature available in HYPOELLIPSE is the calculation of confidence ellipsoids for each hypocenter. The ellipsoids provide valuable insight into the effect of network geometry on possible hypocentral errors.

VELOCITY MODELS

Our experience with locating earthquakes in southern Alaska suggests that significant lateral variations are present in the velocity structure across the network. Such variations might be expected from the complicated geology and tectonics of the region (e.g., Plafker, 1967). Very little information in the form of direct measurement is available for the velocity structure in southern Alaska. In previous catalogs, only two P-wave velocity models consisting of horizontal layers of constant velocity were used to locate the earthquakes (e.g., Stephens, and others, 1979). These velocity models were derived by minimizing the traveltime residuals for selected sets of earthquakes in the Cook Inlet region (Model A of Matumoto and Page, 1969) and near Valdez. The models proved adequate for locating earthquakes as far east as Kayak Island, but earthquakes located farther to the east often had large traveltime residuals at nearby stations. An improved velocity model for the region east of Kayak Island was developed by minimizing the traveltime residuals for a selected set of aftershocks from the 1979 St. Elias earthquake that occurred north of Icy Bay (Stephens, and others, 1980b). A significant difference between this model and the earlier ones is that the new model consists of a single layer of linearly increasing velocity over a half-space of constant velocity, whereas the earlier models consist of several horizontal layers of constant velocity.

In the preparation of this catalog, the method of assigning velocity models to calculate theoretical traveltimes to various stations is different from that used in some earlier catalogs. Previously, the velocity model used was determined by the region in which the earthquake occurred and would then be the same for all stations for that event. In the revised procedure, each station always uses the same velocity model, and the model used is determined by the region in which the station is located. Thus, a station in the eastern

region will use the eastern velocity model to calculate traveltimes from events that occur in the western, central and eastern parts of the network.

West of longitude 148° 45' W the velocity model used is as follows:

<u>Layer</u>	<u>Depth (km)</u>	<u>P velocity (km/s)</u>
1	0 - D	2.75
2	D - 4	5.3
3	4 - 10	5.6
4	10 - 15	6.2
5	15 - 20	6.9
6	20 - 25	7.4
7	25 - 33	7.7
8	33 - 47	7.9
9	47 - 65	8.1
10	below 65	8.3

The thickness, D, of the first layer is allowed to vary between stations to account for the presence of thick sections of low-velocity sediments beneath the stations NKA and NNL, which are located in the Cook Inlet basin. For these stations D is 4 km. For all other stations D is 0.01 km. It is recognized that a model comprised of uniform horizontal layers may be a poor representation of the actual velocity structure, particularly in the vicinity of a subduction zone (Mitronovas and Isacks, 1971; Jacob, 1972), although such a model does have the advantage of simplifying the computation of traveltimes. In order to determine any bias that might result from this approximation, a set of events in the Benioff zone below Cook Inlet was relocated using a ray-tracing program of E. R. Engdahl that incorporates a more realistic, three-dimensional velocity model (Lahr, 1975). Hypocenter shifts, apparently due to the oversimplified flat-layer model, ranged from near zero at a depth of 60 km to as great as 25 km at the 160 km depth. The offsets were oriented in such a way that the dip of the Benioff zone would appear to be too great for locations based on a flat-layered model.

For earthquakes that occur between longitudes 148° 45' W and 144° 30' W, the velocity model used to locate the events is:

<u>Layer</u>	<u>Depth (km)</u>	<u>P velocity (km/s)</u>
1	0.0	2.75
2	0.01	6.4
3	below 39	8.0

East of longitude 144° 30' W the P-wave velocity of the first layer increases linearly from 5.0 km/s at the surface to 7.8 km/s at 32 km depth, while the half-space has a velocity of 8.2 km/s.

P-phase traveltime delays are applied to stations in the network that have consistent and large residuals for the locations of large groups of earthquakes. Each station has three delays (DLY1, DLY2, and DLY3 of Table 1)

assigned to it that correspond to the western, central, and eastern regions covered by the network. The particular delay that is used to locate an earthquake is determined by the region in which the earthquake occurs. For example, a station near Icy Bay that is used to locate an earthquake beneath Cook Inlet (western region) will be assigned a delay DLY1, but the same station will use DLY3 to locate an earthquake that occurs beneath Icy Bay (eastern region). Additional delays are applied at several stations to correct for a satellite link in the relay of the signal. S-phase delays are determined by multiplying the P-delay by 1.78, the P to S velocity ratio.

The initial trial depths for earthquakes which occur in the western, central, and eastern parts of the network are 75, 30, and 15 km, respectively, and reflect a progressive decrease in the range of depths of earthquakes from west to east.

MAGNITUDE

Magnitudes are determined from either the signal duration or the maximum trace amplitude. Eaton and others (1970) approximate the Richter local magnitude, which depends on maximum trace amplitudes recorded on standard horizontal Wood-Anderson torsion seismographs, by an amplitude magnitude based on maximum trace amplitudes recorded on high-gain, high-frequency vertical seismographs such as those operated in the Alaskan network. The amplitude magnitude XMAG used in this catalog is based on the work of Eaton and his co-workers and is given by the expression (Lee and Lahr, 1972)

$$\text{XMAG} = \log_{10} A - B_1 + B_2 \log_{10} D^2 \quad (1)$$

where A is the equivalent maximum trace amplitude in millimeters on a standard Wood-Anderson seismograph, D is the hypocentral distance in kilometers, and B₁ and B₂ are constants. Differences in the frequency response of the two seismograph systems are accounted for in A. It is assumed, however, that there is no systematic difference between the maximum horizontal ground motion and the maximum vertical motion. The terms $-B_1 + B_2 \log_{10} D^2$ approximate Richter's $-\log_{10} A_0$ function (Richter, 1958, p. 342), which expresses the trace amplitude for an earthquake of magnitude zero as a function of epicentral distance.

For small, shallow earthquakes in central California, Lee and others (1972) express the duration magnitude FMAG at a given station by the relation

$$\text{FMAG} = -0.87 + 2.00 \log_{10} T + 0.0035 \text{ DEL} \quad (2)$$

where T is the signal duration in seconds from the P-wave onset to the point where the peak-to-peak trace amplitude on the Geotech Model 6585 film viewer falls below 1 cm and DEL is the epicentral distance in kilometers.

Comparison of XMAG and FMAG estimates from equations (1) and (2) for 77 Alaskan shocks in the depth range 0 to 150 km and in the magnitude range 1.5 to 3.5 reveals a systematic linear decrease of FMAG relative to XMAG with

increasing focal depth. To remove this discrepancy, a linear dependence on depth is added to the expression for FMAG as follows:

$$\text{FMAG} = -1.15 + 2.00 \log_{10} T + 0.007 Z + 0.0035 \text{ DEL} \quad (3)$$

where Z is the focal depth in kilometers.

The magnitude preferentially assigned to each earthquake in this catalog is the FMAG estimate. The XMAG value is used only where no FMAG can be determined.

ANALYSIS OF QUALITY

Two types of errors enter into the determination of hypocenters: systematic errors limiting the accuracy of hypocenters and random errors limiting the precision. Systematic errors arise from an incorrect velocity model, misidentification of phases, or systematic timing errors and can be evaluated through controlled experiments such as locating the coordinates of a known explosion. Random errors result from random timing errors and are estimated for each earthquake through the use of standard statistical techniques.

For each earthquake, HYPOELLIPSE calculates the lengths and orientations of the principal axes of the joint confidence ellipsoid. The one-standard-deviation confidence ellipsoid describes the region of space within which one is 68 percent confident that the hypocenter lies, assuming that the only source of error is random reading error. The ellipsoid is a function of the station geometry for each individual event, the velocity model assumed and the standard deviation of the random reading error. The standard deviation determined from repeated readings of the same phases by four seismologists is as small as 0.01 to 0.02 s for the most impulsive arrivals and as large as 0.10 to 0.20 s for emergent arrivals. The confidence ellipsoids are computed for a standard deviation of 0.16 s and therefore likely overestimate the 68 percent confidence regions. The standard deviation of the residuals for an individual solution is not used to calculate the confidence ellipsoid because it contains information not only about random reading errors but also about the incompatibility of the velocity model to the data. Thus, the confidence ellipsoid is a measure of the precision of the hypocentral solution. In a few extreme cases the value calculated for one of the ellipsoid axes becomes very large corresponding to a spatial direction with very great uncertainty. In these cases an upperbound length of 25 km is tabulated.

To fully evaluate the quality of a hypocenter one must consider both the confidence ellipsoid and the root mean square (RMS) residual for the solution. The RMS residual reflects both systematic and random errors, but the random errors are typically much smaller. Hence the RMS residual is primarily a measure of the incompatibility of the velocity model, misinterpretation of phases, and systematic timing errors. Interpretation of the RMS residual may depend upon the location of the earthquake. In areas where the velocity model is incompatible with the real earth, RMS residuals could be large and reflect the incompatibility; alternatively, the RMS residuals could be small and not reflect the error in a bad hypocenter. Where

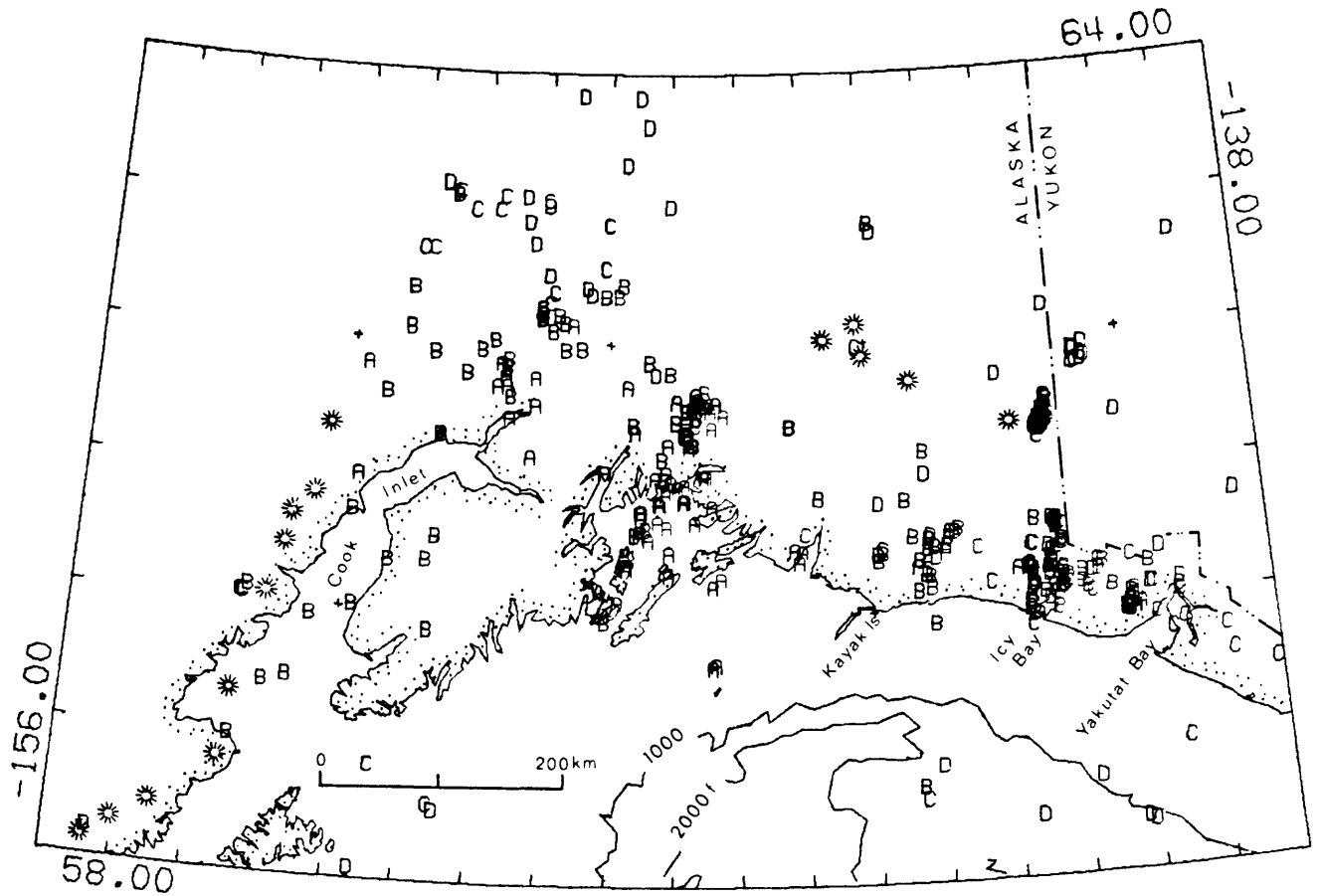


Figure 5. Map of earthquake epicenters for the period April - June, 1978. Earthquakes are plotted with a symbol that represents the quality of the location (see Appendix), with A and B representing better quality. Quaternary volcanoes (after King, 1969) are indicated by stars.

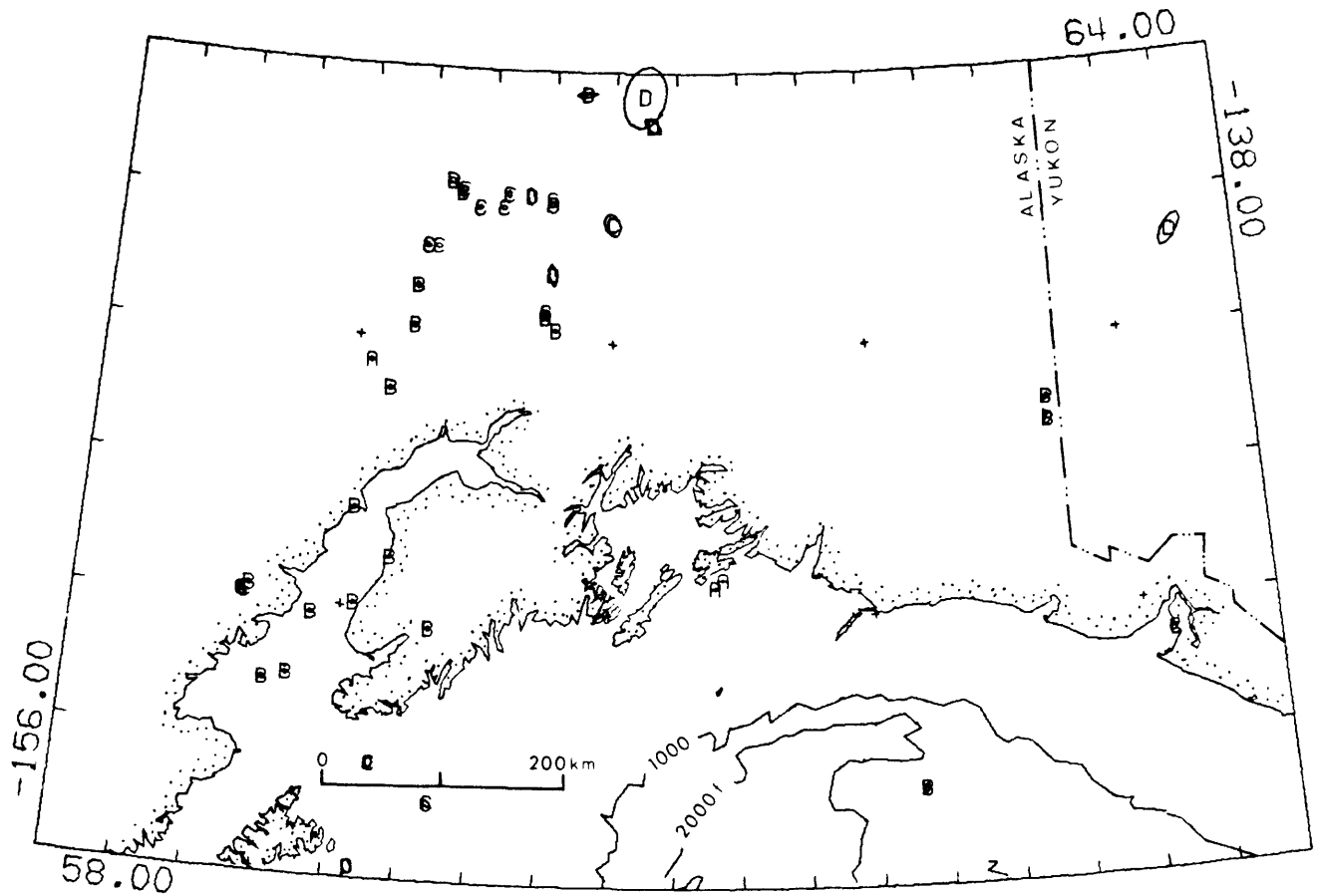


Figure 7. Map showing the epicenters of earthquakes from Figure 5 that have magnitudes of 3.5 and larger. The corresponding projections of the one-standard-deviation ellipsoids onto the surface are also plotted.

the velocity model is compatible, however, a large RMS residual would indicate probable misreadings of phases.

Other parameters provided by HYPOELLIPSE that are useful in evaluating the quality of a hypocentral solution are: GAP, the largest azimuthal separation between stations measured from the epicenter; D3, the epicentral distance of the third closest station; NP, the number of P arrivals used in the solution; and NS, the number of S arrivals used in the solution. If GAP exceeds 180°, the earthquake lies outside the network of available stations and the solution is generally less reliable than for events occurring inside the network.

DISCUSSION OF CATALOG

Origin times, focal coordinates, magnitudes and related parameters for 356 earthquakes from April-June 1978 are listed in the Appendix. Epicenters for these shocks are plotted in Figure 6. In Figure 7, only the earthquakes with magnitudes greater than 3.5 are plotted. Vertical sections showing the depth distribution of all of the shocks are presented in Figures 8 and 9.

We estimate that this catalog is reasonably complete for shocks larger than magnitude 3.5 in the western, 2.5 in the central, and 2.0 in the eastern regions of the area covered by the network. The minimum magnitude of the listed earthquakes ranges from 0.5 for shocks at depths of 30 km or shallower to 2.3 for shocks deeper than 100 km.

The precision of the hypocenters or the relative accuracy of the locations of neighboring events is represented by the confidence ellipsoids. The precision of epicenters, expressed in terms of the maximum axes of the projected one-standard-deviation confidence ellipsoids (ERH), averages 7.3, 3.0, and 3.7 km, respectively, in the eastern, central, and western parts of the network. Similarly, the precision of focal depth (ERZ) averages about 7.0, 4.7, and 6.7 km, respectively. The variation in the precision of hypocenter determination across the network is strongly influenced by differences in the station coverage in the different regions.

The absolute accuracy of the earthquake locations is difficult to evaluate in the absence of known explosions. Hypocenter biases equal to and larger than the dimensions of the confidence ellipsoids are not unlikely from the oversimplified velocity model assumed in the preparation of this catalog.

The distribution of seismicity throughout the network does not vary markedly from that described for previous and later quarters (for example, Stephens and others, 1980a; Stephens and others, 1979; Fogleman, and others, 1978; Lahr, and others, 1974). A well-defined Benioff zone dips to the northwest beneath the Cook Inlet region (Figure 9, sections G-J). The depth to the top of this zone varies from about 50 km beneath the western Kenai Peninsula to about 115 km beneath the active volcanoes west of Cook Inlet. The dip of the Benioff zone appears to increase from northeast to southwest, but the depth to the seismic zone beneath the active volcanoes--Augustine, Iliamna, Redoubt, and Spurr--is nearly constant at about 115 km.

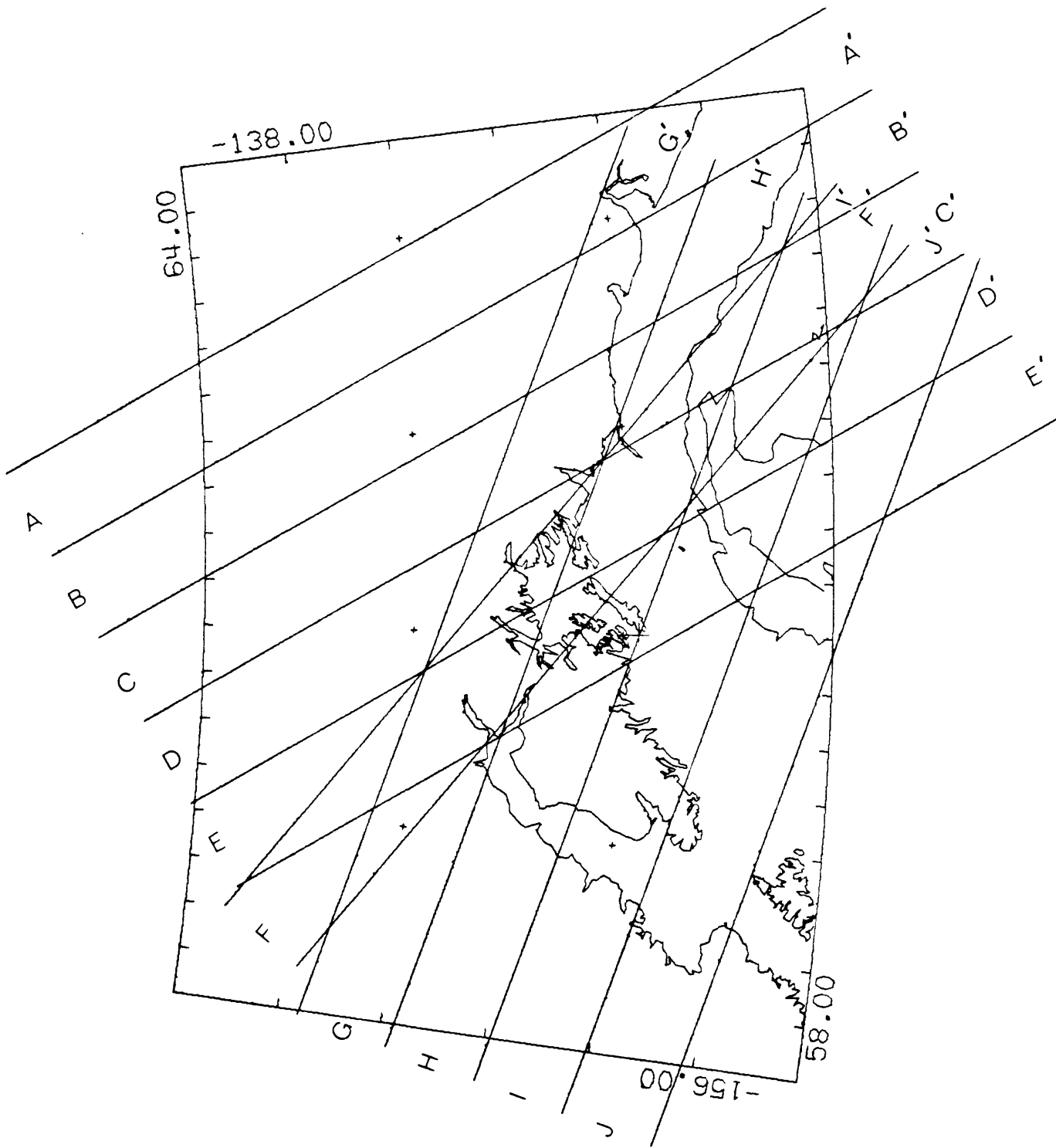


Figure 8. Reference map showing the locations of the vertical sections in Figure 9. Direction of view for sections A - E is N 60° E, for section F is N 40° E, and for sections G - J is N 20° E.

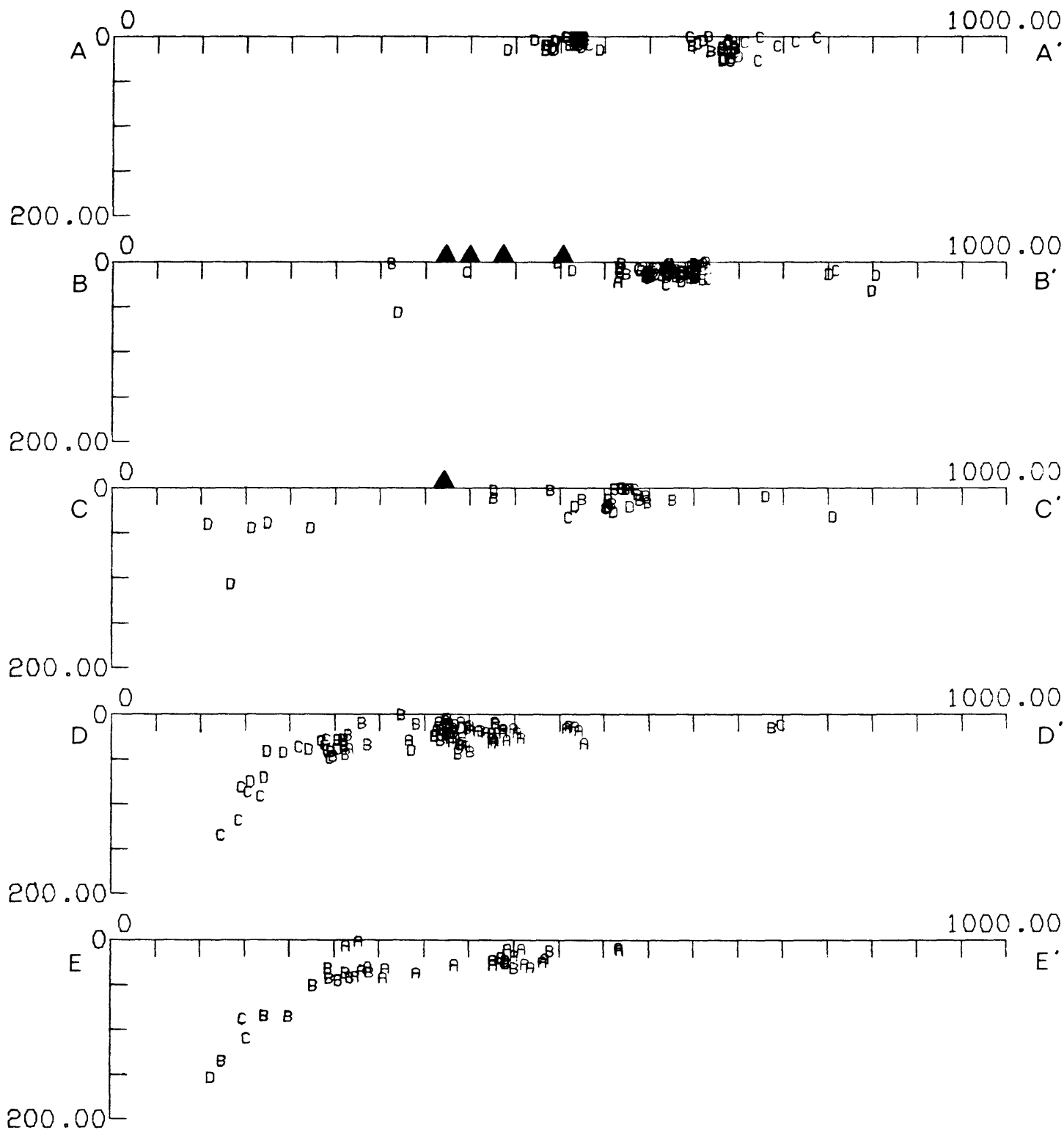


Figure 9 Vertical sections of hypocenters for the areas indicated in Figure 8. Quaternary volcanoes are plotted as triangles at zero depth. All distances are in kilometers. No vertical exaggeration.

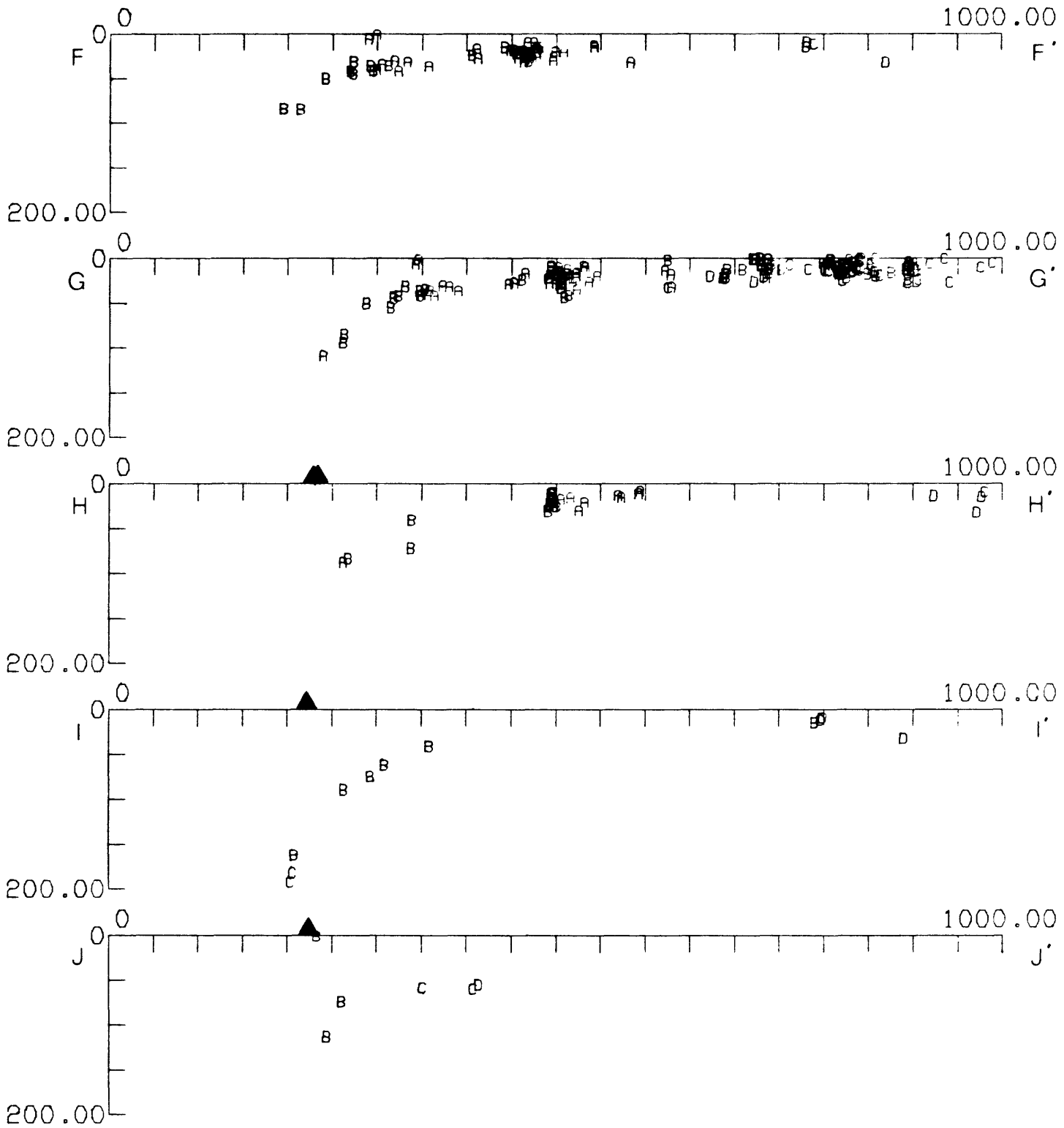


Figure 9 (continued).

All of the seismic activity in the southern part of the network east of longitude 146° W occurs at depths less than about 35 km. The number of larger magnitude earthquakes which occur in the east is considerably smaller than that in the western part of the network (Figure 7). Most of the seismic activity in the eastern part of the network appears to be concentrated beneath Icy Bay and near Waxell Ridge northeast of Kayak Island.

One notable feature in the seismicity during this quarter is a prominent cluster of events centered near 61° 20' N, 141° 15' W, immediately south of the junction between the Totshunda and Duke River faults. A second, less prominent cluster is located about 60 km northeast of the first near the Denali fault. Poor station distribution and uncertainty in the velocity structure contribute to poor locations for these events and preclude making a clear association of the seismicity with particular faults; the apparent SSW-NNE trend of the main cluster also may be a result of mislocation errors. Although earthquakes continually occur in these areas, the interesting aspect of the clusters is that they occurred during relatively short periods of time in April (Figure 10). Only one of the located earthquakes in each group did not occur during April. Both of these later events, which were among the largest magnitude events in each cluster, did not occur until June. Within the swarm-like character of the main cluster are what appear to be several minor mainshock-aftershock sequences.

Nineteen earthquakes listed in the catalog are located outside of the map area of Figure 6. Of these events, the largest one had a coda-duration magnitude of 6.7 (6.0 m_b , 6.6 M_s) and occurred at 03:42 on April 12 southeast of Kodiak Island. Although this earthquake had a prominent aftershock sequence with many events recorded by the USGS network, only the location of the mainshock is presented in the catalog (see Gedney, 1978, for a more complete listing of the aftershocks). Nine earthquakes with coda-duration magnitudes ranging from 2.3 to 3.9 were located southeast of the network in the vicinity of Cross Sound and Glacier Bay.

The contents of the Appendix may be obtained in forms amenable to computer input (punched cards or magnetic tape) by contacting the authors.

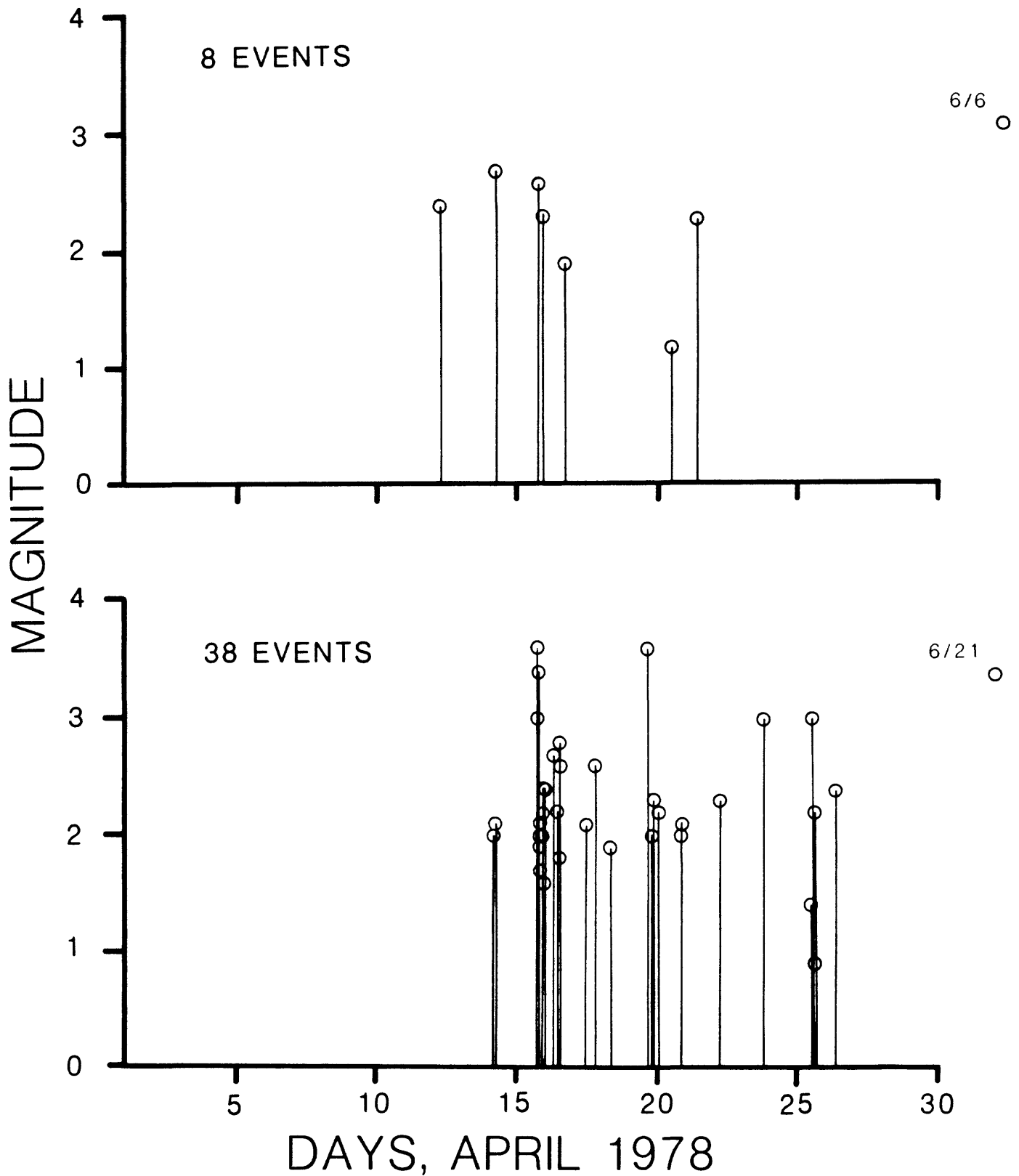


Figure 10. Magnitude versus time distribution of earthquakes for two clusters north of eastern portion of network (see text). The main cluster is plotted in the lower part of the figure. Dates and magnitudes for two events that occurred in June are indicated at right.

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We are indebted to all of those who have spent time fabricating, installing, and maintaining the seismograph network in Alaska, particularly John Rogers. W. H. K. Lee was responsible for much of the work in developing the interactive digitizing-data processing system used in analyzing the data for this catalog.

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APPENDIX

Catalog of Earthquakes

Earthquakes from southern Alaska are listed in chronological order. The following data are given for each event:

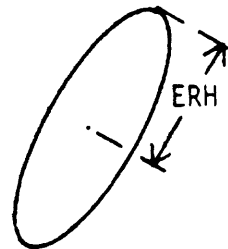
- (1) Origin time in Universal Time (UT): date, hour (HR), minute (MN), and second (SEC). To convert to Alaska Standard Time (AST) subtract ten hours.
- (2) Epicenter in degrees and minutes of north latitude (LAT N) and west longitude (LONG W).
- (3) DEPTH, depth of focus in kilometers.
- (4) MAG, duration magnitude (FMAG) of the earthquake, if available, otherwise amplitude magnitude (XMAG, indicated by "a").
- (5) NP, number of P arrivals used in locating earthquake.
- (6) NS, number of S arrivals used in locating earthquake.
- (7) GAP, largest azimuthal separation in degrees between stations.
- (8) D3, epicentral distance in kilometers to the third closest station to the epicenter.
- (9) RMS, root-mean-square error in seconds of the traveltimes residuals:

$$\text{RMS} = \sqrt{\sum_i (R_{P_i}^2 + R_{S_i}^2) / (NP + NS)}$$

where R_{P_i} and R_{S_i} are the observed minus the computed arrival times of P- and S-waves respectively at the i-th station.

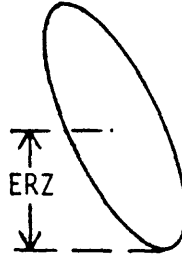
- (10) ERH, largest horizontal deviation in kilometers from the hypocenter within the one-standard-deviation confidence ellipsoid. This quantity is a measure of the epicentral precision for an event. Values of ERH that exceed 25 km are tabulated as 25 km.

Projection of ellipsoid
onto horizontal plane:



- (11) ERZ, largest vertical deviation in kilometers from the hypocenter within the one-standard-deviation confidence ellipsoid. This quantity is a measure of the depth precision for an event. Values of ERZ that exceed 25 km are tabulated as 25 km.

Projection of ellipsoid onto vertical plane:



- (12) Q, quality of the hypocenter. This index is a measure of the precision of the hypocenter (see section Analysis of Quality) and is calculated from ERH and ERZ as follows:

Q	$\frac{ERH}{ERZ}$	$\frac{ERZ}{ERH}$
A	≤ 2.5	≤ 2.5
B	≤ 5.0	≤ 5.0
C	≤ 10.0	≤ 10.0
D	> 10.0	> 10.0

- (13) AZ1, DIP1, and SE1 are the azimuth in degrees (clockwise from north), dip in degrees, and standard error in kilometers of the most nearly horizontal of the three principal axes of the one-standard-deviation error ellipsoid. Values of SE1 that exceed 25 km are tabulated as 25 km.
- (14) AZ2, DIP2, and SE2 are defined as above, but correspond to the principal axis of intermediate dip.
- (15) AZ3, DIP3, and SE3 are defined as above, but correspond to the most nearly vertical principal axis.

SOUTHERN ALASKA EARTHQUAKES, APRIL - JUNE 1978

1978	HR	MIN	SEC	LAT N	LONG W	DEPTH	MAG	NP	NS	GAP	D3	RHS	ERH	ERZ	Q	AZ1	DIPI	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3		
APR	12	1	56	30.1	63 5.3	149 44.9	81.1	3.6	20	11	119	154	0.56	2.7	8.5	C	328	2	2.4	81	4	1.2	217	67	7.9	
12	3	42	6.1	56 23.3	152 16.1	38.2	6.7	11	0	286	335	0.33	24.9	16.1	D	355	9	25.0	91	31	25.0	251	57	14.3		
6.0 MB 4.2 MS																										
FELT (V) AT SITKINAK, (IV) AT OLD HARBOR, (III) AT KODIAK,																										
AND (II) AT OUGA BAY AND ZECHAR BAY																										
6.5 MS (BRK), 6.3 MS, 6.6 MB (PAS)																										
12	4	55	4.4	61 51.6	140 42.4	9.2	2.4	4	3	322	100	0.08	18.2	17.6	D	155	6	6.3	59	44	25.0	251	45	3.9		
12	22	7	5.4	61 35.7	146 37.7	15.7	3.0	33	3	98	62	0.64	1.1	1.6	A	11	1	1.1	281	12	0.7	106	78	1.6		
3.5 ML PHR																										
12	22	9	29.9	61 37.7	146 39.5	8.7	2.1	21	14	175	84	0.67	1.2	1.7	A	289	15	0.8	23	15	1.2	156	69	1.8		
13	5	27	35.0	60 49.4	143 28.6	12.4	1.5	6	6	121	78	1.58	1.8	4.0	B	150	5	0.9	81	10	1.5	269	66	3.8		
13	5	34	32.6	60 16.9	141 37.1	1.8	1.9	13	3	131	68	0.40	1.9	2.6	B	292	15	0.7	30	29	1.2	178	57	3.0		
13	12	30	39.0	61 14.5	146 46.1	17.4	2.0	19	2	149	78	0.21	2.2	1.6	A	7	8	1.1	275	13	0.7	128	75	1.6		
13	16	14	13.4	60 13.5	140 42.1	15.3	1.1	6	4	165	60	0.13	11.4	12.5	D	287	14	1.6	27	36	8.8	179	51	14.8		
14	1	55	10.1	61 47.1	140 41.6	15.0	2.7	15	7	242	167	2.22	7.3	9.2	C	292	12	1.6	194	34	3.9	39	53	11.2		
14	1	56	27.6	61 30.5	141 11.2	9.2	2.0	10	6	252	152	2.01	2.6	2.4	B	127	1	1.3	36	35	2.9	218	55	2.0		
14	2	14	29.5	61 26.6	141 16.6	9.2	2.1	7	4	248	145	1.42	2.9	4.1	B	30	0	2.9	120	2	1.7	300	88	4.1		
14	6	45	56.1	60 15.8	141 7.5	5.9	2.4	7	2	149	78	0.21	2.2	4.0	B	18	13	2.0	284	15	0.8	147	70	4.2		
14	14	42	49.1	63 36.7	147 24.2	44.7	3.5	12	4	292	248	1.06	7.8	24.7	D	39	2	3.5	309	9	6.8	141	81	25.0		
14	18	47	3.7	56 57.8	140 36.8	15.0	3.6	12	3	305	313	0.96	19.2	21.5	D	82	5	7.2	348	38	14.5	178	52	25.0		
15	8	8	45.9	60 22.1	151 18.9	62.2	3.7	33	1	78	64	0.68	1.4	3.2	B	81	1	0.9	151	6	1.2	342	69	3.0		
3.5 MB																										
15	11	39	12.3	58 12.6	136 39.1	15.0	3.0	5	3	349	258	0.58	25.0	25.0	D	47	0	25.0	317	40	25.0	137	50	25.0		
15	12	44	28.5	60 22.7	143 54.1	17.4	2.1	14	5	69	67	0.81	1.9	2.9	B	127	7	0.8	33	30	1.1	229	59	3.3		
15	17	9	45.7	59 55.9	141 36.3	5.5	1.9	7	6	185	77	0.20	3.0	3.6	B	283	2	1.0	191	38	1.7	16	52	4.4		
15	17	33	11.9	61 31.6	141 12.8	0.8	3.6	30	3	152	154	1.67	2.9	2.5	B	123	12	1.3	26	29	3.1	233	55	2.4		
3.3 MB																										
3.8 ML PHR 4.1 ML EPRC																										
15	17	37	58.6	61 25.4	141 16.4	0.8	2.0	5	4	249	143	0.97	5.0	4.1	B	208	6	5.0	299	12	2.3	92	77	4.2		
15	17	39	59.3	61 54.6	140 33.4	15.0	2.6	8	7	275	203	2.33	11.2	14.3	D	292	12	2.7	193	35	3.2	38	52	17.9		
15	17	49	0.4	61 26.1	141 12.9	0.4	3.4	30	2	149	144	1.41	3.3	1.7	B	297	1	1.2	27	6	3.3	198	84	1.6		
3.4 ML EPRC																										
15	18	0	34.4	61 22.1	141 12.0	0.2	1.9	5	3	247	140	1.15	6.1	4.3	C	215	4	6.1	306	11	2.2	105	78	4.3		
15	18	9	46.9	61 28.2	141 14.8	0.3	3.0	23	3	148	155	1.45	3.2	1.8	B	29	3	3.3	298	12	1.3	133	78	1.8		
3.5 MB																										
3.5 ML PHR 3.1 ML EPRC																										
15	18	15	6.0	61 17.9	141 19.2	3.8	2.0	5	3	240	146	0.99	6.4	5.5	C	296	19	2.5	191	38	7.4	47	46	4.2		
15	18	24	9.3	61 19.1	141 24.8	2.0	2.0	5	4	239	146	0.81	6.6	4.3	C	302	15	2.4	204	28	7.4	57	58	3.0		
15	18	35	57.0	61 20.4	141 14.8	0.3	2.1	7	5	243	149	0.85	4.9	4.1	B	232	11	4.0	134	37	5.6	336	51	2.8		
15	18	46	56.8	61 23.8	141 10.2	5.0	1.7	6	3	249	153	1.03	3.5	4.7	B	280	13	1.4	17	29	2.3	169	58	5.4		
15	21	30	34.2	61 17.9	141 23.1	0.4	2.1	5	2	229	147	0.94	5.8	3.8	C	304	11	2.3	212	11	5.9	78	74	3.7		
15	21	40	14.9	59 54.7	140 10.3	14.4	1.8	8	1	107	31	0.68	2.6	2.7	B	137	13	1.2	261	29	2.0	31	45	2.9		
15	21	58	49.8	61 19.4	141 18.5	0.1	2.4	10	2	231	148	0.90	3.9	1.7	B	209	3	3.9	117	36	2.0	303	54	1.6		
15	22	2	44.0	61 49.8	140 36.1	12.0	2.3	11	4	258	193	2.43	13.5	13.1	D	305	7	3.1	42	44	18.4	208	45	4.0		
15	22	21	53.2	61 19.5	141 23.4	0.2	2.4	7	2	230	150	0.79	5.1	2.4	C	303	13	1.4	209	15	5.3	72	70	2.1		
15	22	27	59.8	61 18.7	141 18.8	0.4	2.2	7	4	240	147	1.12	5.2	2.0	C	123	6	1.4	214	9	5.3	0	79	1.9		
15	23	40	45.0	61 26.5	141 16.7	0.2	1.6	5	2	250	160	0.99	8.1	8.0	C	275	5	3.6	181	44	9.3	10	46	6.6		
16	5	24	0.5	61 20.9	141 22.1	0.4	2.7	8	3	241	150	1.57	5.3	3.5	C	305	22	2.4	205	23	5.6	74	57	3.1		
16	8	49	19.5	59 28.2	152 43.2	74.1	3.6	29	7	66	74	0.66	1.7	3.5	B	310	1	1.7	40	10	1.1	214	80	3.5		
3.9 MB																										
16	11	53	23.6	61 21.8	141 20.6	1.6	2.2	5	3	243	152	1.08	5.4	3.9	C	189	32	6.2	74	34	3.3	310	40	1.8		
3.0 ML PHR																										
16	11	53	23.6	61 21.8	141 20.6	2.0	2.6	8	3	235	154	1.44	5.4	3.0	C	113	4	1.8	204	11	5.5	3	78	2.9		
16	11	59	35.9	61 23.1	141 15.8	5.0	2.8	12	4	235	154	1.33	4.1	3.3	B	220	20	4.3	121	23	1.6	347	59	3.4		
16	12	6	41.0	61 14.7	141 22.5	9.2	1.8	5	3	235	132	0.88	9.7	5.8	C	300	13	2.5	203	28	10.8	52	59	3.3		
16	15	30	53.2	61 52.4	140 43.9	9.2	1.9	5	2	279	197	1.26	17.8	18.2	D	285	25	3.4	177	34	5.4	43	46	25.0		
16	20	36	17.1	62 52.9	143 52.4	1.9	3.4	27	3	189	160	0.86	4.2	1.4	B	261	15	4.1	347	38	1.8	152	49	1.0		
3.0 ML PHR																										
17	3	42	32.7	58 44.8	137 11.0	15.0	2.9	9	3	333	230	0.88	25.0	19.6	D	36	3	25.0	304	40	6.1	130	50	25.0		

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ORIGIN TIME		LAT N		LONG W		DEPTH	HAG	HP	NS	GAP	D3	RHS	EPH	EPZ Q	AZ1	DIP1	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3	
1978	HR	MM	SEC	DEG	MIN	KM				DEG	KM	SEC	KM	DEG	DEG	KM	DEG	KM	DEG	KM	DEG	KM	DEG	KM
APR	17	8	22	8.0	60 26.0	143 50.3	21.4	2.1	10	4	71	74	0.96	1.7	3.0 B	88	17	1.1	352	20	0.9	216	63	3.3
	17	8	34	43.2	60 25.6	143 54.6	21.9	1.3A	5	2	147	109	0.45	6.0	12.5 D	64	10	1.8	350	23	1.2	196	65	13.8
	17	10	11	12.1	61 25.2	141 16.4	0.4	2.1	4	3	248	157	0.98	2.7	3.0 B	19	3	2.6	109	4	1.6	252	85	3.0
	17	18	58	19.3	61 19.5	141 16.0	5.9	2.6	16	4	219	132	1.53	3.4	1.9 B	122	7	1.0	213	9	3.4	355	79	1.8
	17	19	50	3.3	60 10.3	143 6.9	16.3	0.9	6	2	158	105	0.94	4.6	2.5 B	157	22	5.0	261	28	1.0	35	53	2.0
	18	2	52	16.9	60 35.7	141 9.6	15.9	1.0A	4	4	191	81	0.15	2.0	5.1 C	225	1	2.0	315	3	1.1	117	87	5.1
	18	2	52	38.2	60 34.1	141 12.1	10.6	1.8	7	6	184	81	0.66	1.8	4.2 B	34	3	1.6	303	9	1.1	142	80	4.2
	18	2	53	57.8	60 35.9	141 11.4	12.7	1.9	5	6	191	80	0.79	2.9	6.9 C	334	8	1.1	81	14	1.8	219	67	7.0
	18	2	57	8.1	60 36.1	141 11.4	15.9	2.2	6	3	187	79	0.25	1.4	3.0 B	215	3	1.4	305	7	1.0	102	82	3.0
	18	7	58	5.9	61 20.3	141 22.0	0.9	1.9	6	5	241	133	1.03	4.9	3.0 B	217	18	5.1	120	19	1.9	347	63	2.8
	18	21	4	40.1	60 23.6	143 2.0	20.9	0.5A	4	4	124	81	0.31	14.6	22.1 D	261	6	2.9	332	33	1.5	162	52	25.0
	19	0	7	5.6	62 9.3	148 43.7	36.0	2.6	12	2	214	83	0.29	2.8	1.9 B	178	22	2.9	81	38	1.3	294	46	2.1
	19	1	49	2.3	60 3.5	153 29.2	191.9	5.2	29	0	82	112	0.53	2.3	6.7 C	134	2	2.3	44	10	1.6	235	80	6.8
	19	14	52	18.6	61 1.3	146 30.3	10.5	3.2	28	2	49	33	0.55	0.9	1.0 A	261	9	0.7	157	11	0.9	24	70	1.0
	19	17	4	39.7	61 21.8	141 12.9	11.3	3.6	11	2	237	151	1.49	4.9	4.4 B	306	21	1.9	198	39	5.4	57	44	3.9
	19	19	31	19.9	61 19.5	141 24.2	0.1	2.0	8	5	239	129	1.46	3.8	2.4 B	214	8	3.8	120	25	1.6	320	64	2.5
	19	21	44	10.9	61 19.4	141 16.6	1.8	2.3	11	2	219	136	0.88	2.6	2.3 B	136	32	2.1	23	32	2.8	259	41	2.1
	19	22	43	1.3	61 1.2	146 32.4	8.8	2.1	19	2	58	33	0.58	1.1	1.4 A	149	6	0.9	261	19	0.7	45	61	1.4
	20	0	15	35.1	61 18.7	141 20.3	7.9	2.2	7	1	230	148	0.45	6.9	3.7 C	218	11	7.0	122	30	2.6	326	58	3.8
	20	6	57	41.0	59 58.7	141 39.6	7.6	1.5	7	5	176	70	0.20	2.7	3.6 B	303	14	1.0	205	28	2.0	57	58	4.1
	20	12	1	42.2	61 46.5	140 45.0	15.0	1.2A	5	3	275	186	1.00	17.4	19.0 D	284	26	4.8	178	31	7.0	47	48	25.0
	20	21	27	29.4	61 22.5	141 15.2	0.5	2.0	5	2	246	137	0.86	5.9	3.3 C	148	6	2.2	81	9	5.4	278	65	3.0
	20	21	23	52.6	61 25.2	141 11.5	1.9	2.1	6	2	250	140	1.01	6.2	4.7 C	140	6	2.2	81	30	5.9	240	48	3.3
	20	23	27	8.8	58 7.3	136 28.9	15.0	3.7	8	5	344	272	0.62	25.0	20.5 D	43	1	25.0	312	40	11.5	134	50	25.0
	20	23	37	1.6	59 8.5	137 6.9	15.0	2.3	4	3	347	100	0.22	25.1	25.0 D	207	3	25.0	300	40	25.0	113	50	25.0
	21	5	25	29.5	61 10.9	143 9.8	0.3	1.5	9	3	160	106	0.24	2.4	2.6 B	117	10	0.8	215	38	2.1	15	50	2.8
	21	7	31	35.4	60 35.7	141 10.2	15.0	2.0	9	6	187	81	0.82	3.7	6.1 C	309	5	1.5	39	8	3.6	187	81	6.1
	21	10	1	18.7	60 1.2	151 49.2	74.6	3.8	31	0	65	104	0.62	1.8	4.4 B	320	1	1.4	81	4	0.9	219	59	3.8
	21	10	19	15.4	61 47.1	140 36.2	4.5	2.3	9	5	271	189	2.45	15.8	11.7 D	163	34	4.2	282	36	3.4	44	36	19.3
	21	20	40	39.1	64 34.2	147 57.0	27.4	4.2	19	0	145	315	0.16	11.0	13.5 D	280	12	7.4	181	36	1.7	25	51	17.1
	21	21	24	24.9	58 51.6	143 4.2	9.2	2.6	8	7	249	150	1.58	11.5	7.6 D	114	30	1.7	224	32	13.3	351	44	4.1
	21	21	48	43.5	59 38.0	146 21.4	8.5	3.0	25	4	109	107	0.63	1.6	1.5 A	30	8	1.6	127	41	1.1	291	48	1.7
	21	21	51	48.9	59 36.7	146 24.3	11.2	3.1	26	2	118	110	0.72	1.5	1.5 A	341	23	1.3	93	40	1.3	229	41	1.8
	21	23	20	45.2	60 16.3	143 11.2	6.9	1.8	10	4	116	48	0.98	1.3	2.7 B	88	4	0.9	357	8	1.3	204	81	2.7
	22	4	3	50.0	61 19.8	141 22.4	0.4	2.3	12	5	231	132	1.28	4.5	2.6 B	210	8	4.5	118	13	1.7	331	75	2.6
	22	13	13	6.0	60 8.9	141 34.3	10.4	1.2	6	4	158	73	0.12	11.5	4.4 D	190	11	11.7	92	35	5.6	295	53	2.4
	22	14	50	46.3	60 15.6	143 7.6	13.2	1.7	6	6	120	97	0.95	3.2	4.2 B	275	23	1.0	17	27	1.2	150	53	5.2
	22	15	39	40.0	60 18.3	141 37.3	1.5	1.7	6	2	133	79	0.16	3.7	8.2 C	46	9	1.8	312	21	1.0	158	67	8.9
	22	16	14	36.6	60 38.0	141 16.1	15.9	2.7	14	2	183	82	0.45	1.7	3.6 B	305	1	1.0	35	5	1.7	204	85	3.6
	23	0	32	48.0	60 27.3	142 23.6	7.4	1.0	5	2	112	100	0.24	5.7	9.8 C	118	4	5.7	28	6	1.2	242	83	9.9
	23	0	47	25.9	60 8.9	140 52.1	7.1	2.3	8	3	139	58	0.35	2.6	2.2 B	289	0	0.9	199	28	2.8	19	62	1.9
	23	1	2	29.2	60 6.5	140 47.1	19.8	1.5	5	3	176	52	0.17	4.4	3.0 B	104	8	0.9	9	30	5.0	207	59	1.9
	23	7	6	17.8	60 16.8	141 38.3	4.5	2.3	17	3	147	50	0.72	2.7	3.3 B	294	7	1.4	29	37	1.4	195	52	4.0
	23	8	24	51.7	62 23.3	151 8.5	84.2	3.6	27	10	107	105	0.70	2.2	4.2 B	86	2	1.5	356	6	2.2	194	84	4.2
	23	19	0	55.9	58 57.1	137 9.7	15.0	2.7	6	4	350	178	0.48	29.7	23.8 D	281	6	25.0	315	39	8.9	165	39	25.0

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1978	ORIGIN TIME	LAT N	LONG W	DEPTH	MAG	NP	NS	GAP	D3	RMS	ERH	ERZ Q	AZ1 DIP1	SE1	AZ2 DIP2	SE2	AZ3 DIP3	SE3					
	HR MN SEC	DEG MIN	DEG MIN	KM				DEG	KM	SEC	KM	KM	DEG DEG	KM	DEG DEG	KM	DEG DEG	KM					
APR	23 19 17	44.5	60 13.8	140 51.2	17.7	2.3	8	3	157	65	0.31	4.3	4.5 B	309	5	1.3	44	43	2.5	214	47	5.7	
	23 20 25	3.5	63 1.2	147 2.8	44.9	3.1	13	6	284	180	0.80	6.9	18.7 D	175	5	6.6	266	13	3.5	64	76	19.2	
	23 21 9	21.1	61 32.5	141 13.1	0.4	3.0	13	4	242	169	1.57	5.5	3.9 C	300	10	2.2	34	18	5.7	182	69	3.7	
	24 1 8	48.6	61 9.4	149 13.9	36.9	2.5	17	6	52	49	0.39	1.1	1.3 A	83	21	0.8	181	21	0.9	312	60	1.4	
	24 3 2	32.4	60 33.6	143 6.3	26.5	1.4	4	3	145	106	0.64	11.1	22.5 D	2	15	1.0	267	21	1.8	125	64	25.0	
	24 7 36	37.4	60 33.1	143 22.3	13.0	1.4	4	3	204	102	0.64	2.8	3.7 B	261	1	2.6	329	8	1.1	164	67	3.4	
	24 10 5	2.9	60 22.8	150 45.3	71.9	3.3	29	3	86	79	0.62	1.3	2.8 B	368	0	1.3	81	5	0.8	258	84	2.8	
	25 0 21	29.7	58 12.3	155 22.2	4.6	3.4	10	1	251	169	0.58	9.2	25.0 D	315	0	3.2	45	2	9.2	225	88	25.0	
	25 7 36	6.6	60 3.0	153 26.6	182.0	4.7	28	1	81	122	0.35	2.2	6.2 C	125	4	2.2	34	6	1.6	248	83	6.3	
	25 9 21	12.9	60 5.5	141 25.4	10.1	1.9	8	5	123	65	0.37	2.8	1.4 B	27	9	2.8	120	19	1.0	273	69	1.4	
	25 11 14	10.1	61 26.1	141 17.3	0.4	3.0	19	5	177	159	1.51	4.0	2.8 B	115	5	1.5	207	17	4.1	9	72	2.6	
	25 11 40	52.9	61 21.1	141 17.2	0.2	1.9A	4	3	244	135	0.65	6.3	4.9 C	81	14	4.6	170	39	7.1	334	49	2.8	
	25 12 53	9.9	61 22.3	141 20.5	9.2	2.2	5	4	244	137	1.31	3.2	3.1 B	117	17	1.6	222	41	3.3	10	44	3.0	
	25 14 19	40.7	61 19.5	141 19.1	0.0	0.9A	4	2	241	134	0.76	8.1	5.6 C	302	24	2.5	198	28	8.9	66	52	4.6	
	26 5 3	1.4	61 20.8	141 20.0	1.8	2.4	5	3	243	133	0.67	4.6	3.7 B	310	15	2.3	210	32	5.1	61	54	3.1	
	28 0 54	10.5	61 21.2	147 36.4	17.5	3.0	25	4	79	64	0.42	1.0	1.7 A	179	13	1.0	272	14	0.6	48	71	1.8	
	28 3 2	28.3	60 48.1	143 52.9	20.4	1.3A	4	3	238	87	0.78	10.3	26.5 D	163	3	1.5	81	19	3.3	241	56	25.0	
	28 5 37	29.1	60 13.1	141 20.3	21.9	1.5	4	2	134	88	0.23	20.6	10.7 D	289	14	2.3	192	27	23.1	44	59	2.9	
	28 8 31	9.6	62 1.2	149 49.4	31.7	2.6	18	4	160	82	0.47	2.8	2.0 B	83	6	1.3	176	23	3.0	339	66	1.8	
	28 12 59	38.8	60 2.4	140 9.3	12.0	1.9	8	5	151	32	0.68	3.7	2.1 B	38	16	3.9	135	23	1.5	276	61	2.0	
	28 15 9	7.9	60 17.5	140 32.7	10.1	1.5	7	3	185	127	0.47	3.6	3.1 B	290	21	1.1	183	38	4.1	42	45	2.5	
	28 16 6	35.1	60 32.3	142 49.8	1.4	1.8	3	3	233	151	0.63	4.0	4.1 B	136	6	1.3	81	43	4.3	232	37	2.6	
	28 21 32	6.4	63 4.8	149 23.3	75.0	3.7	16	3	215	166	0.82	7.3	20.1 D	81	1	2.4	341	13	5.5	175	74	20.3	
	29 5 55	42.0	60 27.9	143 50.0	22.4	1.9	5	4	198	103	0.82	4.9	5.2 C	323	17	0.9	81	31	3.1	213	46	6.3	
	29 12 27	42.3	59 55.8	141 33.0	1.8	2.0	10	2	184	74	0.38	2.5	2.0 A	130	5	1.1	38	29	2.6	229	61	1.7	
	29 17 12	53.6	61 20.0	146 46.3	25.9	3.2	23	3	97	68	0.45	1.2	1.8 A	276	10	0.7	8	10	1.1	142	76	1.8	
	29 17 30	32.5	63 50.2	148 29.8	40.4	3.7	26	11	114	226	0.78	7.3	24.2 D	186	3	1.3	277	14	4.1	84	76	25.0	
	29 18 43	12.4	61 34.8	146 57.2	17.7	2.2	14	3	122	72	0.37	1.2	2.0 A	270	9	0.8	1	9	1.2	135	77	2.0	
	30 1 2	59.2	60 12.5	141 4.1	11.4	1.5	4	4	196	98	0.07	23.7	8.6 D	274	0	1.2	184	19	25.0	4	71	3.0	
	30 3 41	21.0	60 33.3	147 23.6	17.8	2.4	17	4	153	86	0.44	1.9	1.9 A	261	17	0.8	152	36	1.5	10	47	2.3	
	30 9 1	56.8	60 10.4	141 3.3	11.3	1.7	5	4	139	104	0.09	8.7	5.5 C	280	3	0.9	188	31	10.1	15	59	2.0	
	30 9 30	0.1	60 4.1	141 12.2	3.0	2.1	6	3	162	92	0.16	4.8	2.2 B	19	1	4.8	109	12	1.3	284	78	2.3	
	30 9 34	40.8	60 5.0	141 15.5	10.9	1.6	7	4	161	89	0.84	6.1	2.7 C	14	0	6.1	284	4	1.1	104	86	2.7	
	30 11 1	22.1	60 26.7	141 8.3	6.7	1.5	5	5	174	93	0.40	3.0	7.2 C	81	5	1.5	348	18	1.9	186	71	7.6	
	30 11 3	30.8	60 26.9	141 8.8	10.8	1.4	6	5	173	93	0.27	3.1	5.8 C	317	10	1.0	81	15	1.1	205	52	5.6	
	30 11 7	14.2	60 28.4	141 7.7	6.8	2.2	9	3	177	91	0.46	2.5	3.6 B	316	10	0.9	51	27	1.7	207	61	4.1	
	30 11 14	48.0	60 28.2	141 8.1	8.8	1.5	6	5	177	94	0.37	3.7	5.0 B	311	8	0.8	44	16	3.6	195	72	5.1	
	30 11 47	52.7	60 21.9	147 44.6	10.4	2.9	30	6	102	89	0.53	1.0	1.6 A	172	8	1.0	265	21	0.6	62	67	1.8	
	30 11 23	47	5.5	60 7.7	141 7.5	1.9	2.3	11	2	128	48	0.17	2.8	2.9 B	109	5	0.9	14	44	1.8	204	46	3.6
	30 11 2	44	56.9	61 57.8	148 27.5	34.2	2.6	14	4	193	61	0.56	4.3	1.5 B	0	2	4.3	267	43	1.8	92	47	1.1
	2 2	47	8.7	60 50.1	146 51.8	17.6	2.3	20	3	111	44	0.41	1.2	1.2 A	261	23	0.6	154	25	1.1	26	53	1.4
	2 6	57	46.1	61 36.6	151 28.5	94.5	4.2	24	3	87	57	0.63	1.8	3.2 B	83	6	1.2	174	9	1.7	320	79	3.2
	2 7	11	57.1	60 19.5	143 18.7	1.2	1.3	7	5	105	40	0.60	1.6	2.0 A	116	2	1.0	25	23	1.5	211	67	2.1
	2 14	21	56.4	60 35.1	147 32.8	10.2	2.6	21	3	127	86	0.32	1.9	2.5 A	261	20	0.8	157	24	1.4	25	56	2.8
	3 7	53	30.1	60 32.2	143 8.5	1.0	1.7	5	3	185	71	0.65	2.6	3.8 B	265	8	2.5	357	14	1.0	146	74	3.9

SOUTHERN ALASKA EARTHQUAKES, APRIL - JUNE 1978

ORIGIN TIME	LAT N	LONG N	DEPTH	MAG	NP	NS	GAP	D3	RMS	EPH	EPZ Q	AZI	DIP1	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3		
1978	DEG MIN	DEG MIN	KM	KM	MP	MP	DEG	KM	SEC	KM	KM	DEG	DEG	KM	DEG	DEG	KM	DEG	DEG	KM		
MAY 3 15 8 17.0	60 43.1	138 27.7	2.4	2.1	6	2	270	143	0.75	16.0	10.7	D	316	13	2.7	81	20	16.1	205	49	6.2	
3 22 9 59.1	60 28.4	145 9.8	14.2	2.0	10	9	138	83	0.49	1.9	1.7	A	356	29	1.2	108	34	0.8	236	42	2.3	
3 22 55 43.6	60 36.2	141 13.6	12.5	3.0	12	6	187	78	0.57	2.1	3.7	B	315	9	0.9	47	13	2.0	191	74	3.8	
3 23 1 55.9	60 37.9	141 11.4	18.0	2.2	8	5	190	94	0.84	3.3	5.3	C	304	10	1.1	210	21	2.6	58	67	5.7	
3 23 3 32.4	60 36.8	141 11.9	5.9	2.4	11	3	188	93	0.53	4.2	3.3	B	304	3	1.1	214	17	4.3	44	73	3.2	
4 5 5 9.4	60 22.8	145 5.8	32.6	2.2	10	6	145	81	0.64	1.5	1.9	A	291	10	0.9	26	27	1.3	182	61	2.0	
4 10 7 11.7	58 12.2	136 26.3	15.0	3.4	6	3	347	100	0.68	25.0	20.9	D	40	0	25.0	310	40	13.0	130	50	25.0	
5 5 32 47.3	63 10.1	150 41.3	153.4	5.5	26	0	108	193	0.52	3.0	10.2	D	281	0	3.0	11	1	2.2	191	89	10.2	
5.2 MB																						
5 9 23 52.2	60 38.0	147 6.9	16.2	2.3	21	10	121	69	0.55	1.2	1.5	A	261	17	0.6	155	25	0.9	19	56	1.7	
5 12 5 42.5	62 44.1	149 14.2	42.3	3.0	22	6	235	127	0.56	5.3	11.8	D	84	4	1.7	353	8	5.1	200	81	11.9	
6 5 45 54.0	60 36.0	142 40.6	7.4	2.5	11	3	173	61	0.37	3.0	6.3	B	136	18	0.8	81	30	1.3	260	42	5.6	
6 7 31 48.9	61 15.7	146 43.3	12.8	2.2	14	3	114	50	0.41	1.1	1.7	A	185	5	1.1	277	17	0.7	79	72	1.8	
6 22 16 40.9	60 17.7	140 37.1	0.4	1.7	7	4	207	64	0.40	6.7	6.1	C	299	18	1.1	193	40	0.1	48	44	4.4	
6 22 43 54.1	62 26.1	147 48.1	28.8	3.0	16	2	212	119	0.46	4.0	3.3	B	321	30	2.6	81	36	1.5	205	37	4.8	
7 7 45 17.0	62 22.5	148 54.2	30.0	3.0	13	2	258	96	0.37	5.6	4.5	C	298	10	3.0	200	37	6.8	41	51	2.2	
8 4 38 55.5	60 59.2	151 50.0	87.0	3.3	25	6	60	80	0.64	1.5	2.5	A	150	5	1.3	81	15	0.9	259	64	2.4	
8 14 5 25.7	62 59.2	149 49.4	86.3	4.1	27	5	116	149	0.50	2.2	8.8	C	207	1	1.5	297	1	2.2	72	89	6.8	
3.2 MB																						
8 15 35 2.0	59 54.2	143 4.0	13.3	2.4	6	3	165	81	0.47	3.1	3.4	B	93	2	2.1	105	38	2.6	0	52	3.0	
9 3 4 24.1	60 39.9	147 30.9	20.0	2.2	14	6	144	83	0.41	2.3	3.7	B	275	13	0.9	179	24	1.6	31	62	4.1	
9 12 57 53.7	60 34.6	141 11.3	5.0	2.9	9	4	202	93	0.60	3.3	6.2	C	282	8	1.3	190	14	3.0	41	74	6.4	
10 12 50 17.1	58 53.9	136 18.2	24.1	3.9	8	2	273	216	0.62	21.8	23.2	D	81	2	2.9	333	37	18.4	173	49	25.0	
4.2 ML EMRC																						
12 12 16 5.4	62 13.4	149 5.7	48.6	4.6	30	0	104	96	0.31	2.2	5.5	C	89	2	1.2	359	6	2.1	197	84	5.6	
5.1 MB																						
12 13 43 33.4	60 17.6	141 39.9	13.9	2.3	11	3	166	68	0.31	3.0	6.2	C	92	12	1.5	359	13	2.6	223	72	6.5	
12 14 59 49.4	62 13.0	149 5.2	41.4	2.9	27	3	80	96	0.48	1.7	5.2	B	325	1	1.3	81	7	1.1	228	63	4.8	
12 21 3 12.1	62 15.6	149 5.3	39.6	3.0	14	4	245	100	0.32	3.6	9.6	C	352	4	3.6	83	6	1.4	229	83	9.7	
13 3 9 52.2	61 55.1	150 45.0	50.8	3.3	19	3	168	93	0.77	2.4	3.2	B	81	4	1.4	346	4	2.4	214	82	3.2	
13 13 43 55.3	62 11.2	149 5.4	46.6	3.6	25	3	80	93	0.57	1.7	3.6	B	81	4	1.1	329	8	1.4	192	66	3.4	
14 3 5 42.0	62 21.7	148 18.5	39.0	2.9	14	4	251	114	0.69	3.2	17.2	D	176	2	3.2	85	4	1.6	292	85	17.3	
14 11 5 1.6	59 58.1	140 10.4	4.2	1.8	7	3	112	31	0.65	1.4	1.8	A	300	13	0.8	204	23	1.2	57	63	1.9	
14 11 6 53.9	59 58.0	140 10.7	8.0	1.4	7	4	115	32	0.37	3.3	5.6	C	261	2	2.8	145	16	1.3	357	60	5.4	
14 15 57 26.3	62 49.1	143 50.0	56.4	2.9	7	5	292	229	0.72	8.2	26.3	D	331	4	7.0	81	5	4.1	210	69	25.0	
14 23 26 46.1	60 0.6	141 37.4	18.1	2.0	7	2	149	71	0.39	2.8	3.5	B	287	20	0.6	188	24	2.3	53	58	3.9	
15 11 11 55.5	60 7.9	141 17.0	4.5	1.7	6	4	162	86	0.22	2.0	3.8	B	282	7	0.8	15	26	2.4	178	63	4.1	
15 12 7 26.8	60 16.4	141 35.5	8.2	2.2	11	4	165	51	0.39	2.4	2.4	A	290	8	0.8	28	44	1.8	192	45	2.9	
16 1 11 36.9	61 56.9	150 1.8	42.5	3.4	16	2	86	66	0.42	2.4	4.6	B	324	0	1.9	81	15	1.3	234	59	4.3	
2.8 ML PFR																						
16 16 11 28.9	61 0.4	147 9.1	18.6	2.1	13	4	108	83	0.26	1.5	3.1	B	163	2	1.4	261	19	0.8	67	69	3.3	
18 15 3 1.5	61 30.7	146 48.1	22.2	2.6	18	2	175	71	0.47	2.1	2.9	B	279	12	0.8	13	17	2.0	156	69	3.0	
19 13 31 1.9	60 26.6	142 53.0	1.2	1.4	5	4	132	150	0.11	2.2	2.5	A	292	12	2.2	197	24	1.1	47	63	2.7	
19 20 43 18.3	59 58.2	141 14.2	0.2	1.3	8	4	153	104	0.64	4.2	3.2	B	92	1	1.0	182	10	4.2	356	80	3.1	
21 0 42 42.6	63 3.4	149 2.5	91.2	3.8	20	3	96	163	0.54	2.6	7.5	C	91	3	2.5	182	8	1.4	341	81	7.6	
21 8 10 33.5	62 12.4	148 49.5	28.9	2.8	11	6	247	131	0.42	3.3	2.4	B	188	29	3.6	81	31	1.1	313	46	2.2	
21 10 28 36.6	59 32.9	138 42.2	5.4	1.6	6	2	271	68	0.58	7.3	4.8	C	261	0	7.3	349	35	1.3	171	55	5.8	
21 11 59 15.3	60 3.6	140 6.7	14.5	1.5	6	5	177	33	0.83	1.8	1.8	A	302	18	1.7	128	32	0.8	345	52	2.1	
21 14 25 32.6	58 56.5	139 28.7	9.2	2.9	9	4	259	100	0.80	7.4	6.9	C	261	22	1.8	146	41	8.7	10	39	5.7	
22 9 10 12.0	61 0.4	147 17.4	18.6	2.0	13	4	113	53	0.40	1.3	1.9	A	12	8	1.3	279	20	0.6	123	68	2.0	

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ORIGIN TIME		LAT N	LONG W	DEPTH	MAG	NP	NS	GAP	D3	RHS	ERH	ERZ	Q	AZI	DIP1	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3						
1978	HR	MIN	SEC	DEG	MIN	DEG	MIN	DEG	KH	SEC	KH	SEC	KH	DEG	DEG	KH	DEG	DEG	KH	DEG	DEG	KH						
	MAY	22	11	40	23.2	60	27.1	141	33.9	6.0	1.9	5	2	182	83	3.4	8.2	9.1	C	276	0	1.1	186	41	4.4	6	49	11.4
		22	16	34	59.6	60	27.6	143	9.0	0.9	2.4	8	3	147	57	0.81	2.0	3.4	B	91	1	1.1	182	22	1.6	359	68	3.6
		23	2	25	7.2	57	46.1	156	16.3	127.2	5.5	8	4	275	24.0	0.17	18.9	26.1	D	330	4	5.5	261	17	16.7	73	63	25.0
		23	10	34	56.2	59	56.7	148	3.0	12.1	2.7	14	4	163	162	0.65	2.5	2.6	B	261	17	1.8	144	32	1.6	11	46	2.9
		23	21	46	27.8	61	23.6	145	12.1	11.1	1.0	4	4	165	40	0.19	1.4	5.3	B	330	4	1.3	261	7	1.0	94	68	4.9
		23	22	34	15.1	60	8.9	143	18.8	8.6	1.6	8	7	145	42	0.55	1.7	3.6	B	81	5	0.6	169	6	1.6	310	82	3.6
		24	0	3	47.8	62	53.7	149	20.4	41.4	3.1	12	6	272	172	0.47	5.3	21.6	D	320	3	3.2	81	4	3.3	205	59	18.7
		24	8	30	2.2	58	31.8	150	27.6	54.9	3.4	19	6	159	193	0.60	5.6	21.4	D	27	1	1.5	117	11	3.8	292	79	21.8
		24	13	35	16.3	60	50.6	146	49.6	18.4	3.0	23	4	112	87	0.43	1.5	1.7	A	261	22	0.7	155	25	1.3	25	54	1.9
		24	19	49	56.3	61	45.2	149	38.6	40.9	2.4	13	4	201	57	0.36	2.4	2.3	A	355	6	2.4	86	9	1.0	232	79	2.3
		25	0	52	32.4	61	23.3	145	13.4	2.4	1.0	4	3	161	39	0.16	2.7	24.1	D	220	1	0.9	310	5	1.7	119	85	24.2
		25	18	15	47.0	61	56.1	144	8.5	10.9	2.1	6	2	252	108	0.25	7.1	4.4	C	81	14	3.4	173	32	8.1	330	55	1.9
		26	2	45	18.3	60	35.6	147	36.4	23.1	2.5	18	2	125	97	0.40	2.3	3.3	B	261	14	0.8	157	24	1.6	17	59	3.7
		26	8	48	29.4	60	34.8	142	43.9	10.9	1.6	5	3	171	127	0.21	2.9	2.8	B	104	28	1.5	354	33	1.3	225	44	3.8
		26	22	17	18.3	60	13.9	140	37.0	15.8	1.9	4	4	206	126	0.29	25.0	2.7	D	29	2	25.0	297	41	1.6	121	49	3.0
		26	22	57	47.8	59	52.3	139	47.6	6.1	1.3	5	3	155	36	0.59	4.3	7.2	C	313	3	0.8	221	29	1.7	48	61	8.2
		27	1	45	30.0	60	49.7	147	14.3	29.9	2.1	15	5	146	93	0.42	2.1	2.0	A	261	16	0.7	151	41	2.1	7	43	2.1
		27	14	50	9.9	60	33.2	150	37.8	41.0	2.9	21	2	98	95	0.47	1.4	3.3	B	261	0	0.9	336	6	1.2	171	74	3.2
		27	17	52	0.9	60	10.1	141	8.7	11.3	2.1	5	3	171	94	0.17	6.2	4.5	C	283	5	0.9	16	31	7.0	185	59	3.3
		27	18	21	6.1	61	25.7	146	48.8	15.8	1.9	13	9	144	62	0.61	1.1	1.9	A	6	3	1.1	275	19	0.5	105	71	2.0
		28	21	29	18.1	60	48.0	147	12.5	21.0	2.1	13	4	147	95	0.24	1.9	2.4	A	264	18	0.8	166	23	1.7	28	60	2.6
		29	6	24	45.3	60	6.3	153	23.1	162.0	4.4	25	3	110	82	0.43	2.2	3.5	B	30	5	1.3	121	6	2.2	261	82	3.5
		29	7	20	47.8	60	3.5	139	26.1	17.6	1.5	4	2	240	46	0.34	8.9	4.9	C	229	25	9.7	123	31	1.5	351	48	3.4
		29	11	27	12.5	60	11.6	142	12.8	12.4	1.7	6	4	167	109	0.88	4.0	8.2	C	10	9	3.1	104	22	1.1	259	66	8.9
		29	21	12	11.7	59	56.9	140	0.5	13.6	1.3	6	2	130	84	0.58	2.2	2.1	A	132	15	1.0	234	39	2.4	25	47	1.9
		29	22	19	29.4	58	27.2	141	41.2	32.1	2.9	9	4	259	188	0.91	8.5	10.6	D	286	6	2.3	192	33	6.4	25	56	12.0
		30	1	54	17.4	60	27.3	145	3.1	18.5	2.3	14	3	116	87	0.35	1.9	1.9	A	137	11	0.9	261	39	2.0	37	39	1.7
		31	7	52	37.1	61	52.2	147	22.9	0.5	2.1	8	7	216	99	0.60	3.7	2.5	B	281	9	0.8	15	24	4.0	172	64	2.1
		31	12	15	22.4	60	22.6	143	16.8	1.3	2.3	9	3	108	89	0.30	2.1	3.4	B	199	13	1.9	105	16	0.9	326	69	3.6
		31	18	29	26.2	61	26.8	149	34.1	42.2	3.2	23	2	91	28	0.35	1.6	2.4	A	261	1	0.9	159	17	1.5	354	69	2.5
		31	18	29	26.2	61	26.8	149	34.1	42.2	3.2	23	2	91	28	0.35	1.6	2.4	A	261	1	0.9	159	17	1.5	354	69	2.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5
		31	21	17	12.2	60	27.3	147	4.5	30.5	2.4	15	3	169	86	0.47	2.1	1.5	A	154	6	2.1	261	20	0.9	50	63	1.5

SOUTHERN ALASKA EARTHQUAKES, APRIL - JUNE 1978

ORIGIN TIME		LAT N	LONG W	DEPTH	MAG	NP	NS	GAP	D3	RMS	ERH	ERZ	Q	AZI	DIP1	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3			
1978	HR	MIN	SEC	DEG	MIN	DEG	MIN	DEG	MIN	SEC	KH	KH	KH	DEG	DEG	KH	DEG	DEG	KH	DEG	DEG	KH			
	JUN	7	5	40	46.5	58	37.0	143	19.2	11.6	2.9	19	5	228	232	0.65	8.2	3.6	C	20	3	8.2	112	22	
		7	12	37	49.1	59	55.7	152	26.0	89.3	3.6	29	7	87	72	0.58	1.8	3.1	B	10	3	1.4	100	4	
		7	20	54	32.4	59	43.9	138	46.6	10.1	1.7	5	2	254	77	0.52	5.0	5.7	C	330	23	1.3	81	24	
		8	2	49	4.8	60	12.2	146	24.3	13.5	3.8	30	3	68	85	0.66	1.1	1.6	A	297	12	0.8	202	22	
		9	3	23	34.1	60	48.1	146	24.0	20.2	2.2	17	2	96	37	0.71	1.4	1.8	A	146	3	1.1	261	14	
		10	2	27	28.9	60	59.1	147	3.0	20.5	2.0	12	3	84	62	0.26	1.1	2.3	A	275	4	0.7	5	4	
		10	8	24	0.9	57	57.8	156	44.0	0.4	4.8	11	0	258	246	0.26	17.7	9.5	D	81	2	17.7	348	3	

SOUTHERN ALASKA EARTHQUAKES, APRIL - JUNE 1978

ORIGIN TIME		LAT N	LONG W	DEPTH	MAG	NP	NS	GAP	D3	RPS	ERH	ERZ Q	AZI	DIP1	SE1	AZ2	DIP2	SE2	AZ3	DIP3	SE3							
1978	HR	MIN	SEC	HR	MIN	SEC	MIN	SEC	KM	KM	KM	KM	DEG	DEG	KM	DEG	DEG	KM	DEG	DEG	KM							
JUN	20	11	26	36.3	61	28.6	146	14.0	34.4	1.8	7	3	198	55	0.38	2.3	2.1	A	134	32	2.6	261	34	1.4	19	34	1.6	
	20	12	43	5.1	62	24.7	148	23.0	41.6	2.8	9	5	259	165	0.29	3.9	18.7	D	0	2	3.9	90	3	2.0	236	86	18.7	
	21	0	33	29.2	62	12.4	141	6.4	15.0	3.4	16	5	266	248	0.78	17.9	18.8	D	0	2	4.5	195	42	7.1	32	47	25.0	
	21	2	6	50.8	60	19.1	140	7.8	8.0	2.3	13	3	207	83	0.43	4.6	5.7	C	301	11	1.9	36	24	4.2	188	63	6.1	
	21	21	9	3.6	62	17.9	148	58.2	28.2	2.8	13	6	224	122	0.58	3.3	5.2	C	348	3	3.1	81	29	1.4	253	61	5.9	
	21	22	58	44.0	59	25.1	153	3.7	112.9	4.1	26	3	80	84	0.33	2.4	4.3	B	116	4	2.3	25	15	1.4	221	74	4.5	
	22	2	22	8.0	61	32.4	149	10.4	32.0	3.2	23	3	71	39	0.62	1.8	1.4	A	81	12	0.8	261	44	1.1	351	0	1.5	
	22	5	14	4.9	63	6.9	150	29.5	134.7	4.6	25	3	78	166	0.52	2.7	7.8	C	185	3	1.5	275	4	2.7	58	85	7.8	
	22	5	35	19.1	61	49.5	149	37.4	41.9	2.6	14	3	172	65	0.21	2.4	3.4	B	90	7	1.0	359	7	2.4	225	80	3.4	
	23	6	9	28.6	61	53.0	149	35.9	36.6	2.8	13	3	218	67	0.19	4.4	1.8	B	327	21	3.6	261	38	2.2	86	42	1.3	
	23	6	19	46.8	60	18.4	143	10.3	0.9	2.1	6	3	108	49	0.52	2.7	5.5	C	214	5	2.7	123	16	1.2	321	73	5.7	
	23	21	56	31.3	61	46.5	150	14.9	45.1	2.9	12	4	159	63	0.18	3.4	4.4	B	168	16	3.3	81	19	1.3	299	65	4.7	
	24	6	1	3.7	60	00.8	146	41.0	26.8	2.5	19	2	127	54	0.46	1.8	1.8	A	261	18	1.0	137	40	1.6	6	37	1.9	
	24	6	13	16.1	58	55.6	136	42.9	10.3	3.0	6	2	347	186	0.68	25.0	20.0	D	27	1	25.0	296	44	12.6	118	46	25.0	
	24	7	43	18.0	61	24.5	146	40.2	43.8	2.3	11	3	140	62	0.44	2.3	4.4	B	261	8	1.4	363	14	2.1	140	72	4.4	
	24	10	26	52.3	60	51.3	144	47.2	2.2	2.4	18	6	118	65	0.95	2.2	2.9	B	42	5	2.2	134	17	0.9	296	72	3.0	
	24	11	33	44.4	58	23.1	140	10.9	32.1	2.9	8	4	280	150	0.44	6.7	25.0	D	297	0	4.6	27	0	6.7	0	90	25.0	
	24	13	24	53.5	61	24.6	147	38.1	24.5	2.5	20	3	124	76	0.33	1.8	4.7	B	186	5	1.6	277	18	0.8	81	71	5.0	
	24	23	18	0.7	58	34.3	150	32.7	59.6	4.1	26	0	177	169	0.30	3.9	7.7	C	35	5	1.7	125	8	3.8	273	81	7.8	
	25	1	11	31.3	62	5.5	151	9.5	64.8	3.5	30	1	101	83	0.50	2.0	3.3	B	349	2	2.0	81	5	1.3	238	84	3.3	
	25	5	24	53.6	60	4.7	136	57.8	15.0	2.4	3	3	326	183	0.37	17.4	21.0	D	331	9	8.0	261	39	4.5	72	46	25.0	
	25	5	40	59.3	61	46.9	147	16.9	39.9	2.2	7	4	201	88	0.38	5.8	25.0	D	81	2	3.4	172	3	5.6	318	86	25.0	
	25	5	58	1.2	58	21.4	140	6.2	15.0	2.6	5	4	296	157	0.48	16.2	19.7	D	281	0	6.4	12	39	4.8	191	51	25.0	
	25	9	52	53.9	61	19.9	146	50.6	15.3	1.4	7	5	126	95	0.15	4.9	9.0	C	355	10	2.2	261	26	1.0	104	62	10.1	
	25	10	55	27.1	61	47.3	147	3.1	10.5	2.9	21	3	194	83	0.45	2.3	3.1	B	193	5	2.3	285	25	0.9	92	64	3.4	
	25	17	0	4.2	61	31.9	146	42.5	10.7	2.0	13	4	162	74	0.54	1.5	2.2	A	187	10	1.4	281	25	0.8	77	63	2.5	
	25	20	4	44.3	61	25.8	146	57.7	10.4	1.8	8	3	143	60	0.29	1.7	3.2	B	184	4	1.6	276	24	0.9	85	66	3.5	
	26	17	40	8.2	60	45.9	147	29.9	27.8	2.5	18	4	114	75	0.38	1.9	2.3	A	261	10	0.7	347	27	1.8	152	61	2.5	
	26	17	57	30.7	62	52.9	148	2.6	36.4	3.5	17	4	266	190	0.63	9.4	8.9	C	202	24	7.7	93	36	2.1	318	44	11.7	
	26	18	26	23.6	60	38.2	147	25.9	25.9	2.4	15	5	135	81	0.48	3.2	3.1	B	261	11	0.9	145	43	2.4	1	40	3.6	
	26	21	10	23.3	60	15.4	139	51.6	0.1	1.8	7	3	216	57	0.42	2.9	3.8	B	310	5	1.1	43	30	2.3	211	59	4.2	
	28	16	40	59.0	61	33.5	146	34.1	4.6	1.8	12	4	196	76	0.66	2.8	2.9	B	13	28	1.7	265	30	0.9	137	47	3.8	
	28	22	37	5.5	60	6.0	139	49.1	24.6	1.3	4	3	235	54	0.45	9.5	2.1	C	208	4	9.5	116	26	1.3	306	64	2.1	
	29	6	44	26.1	61	18.7	150	36.9	55.4	3.1	22	6	68	79	0.66	1.2	3.3	B	90	3	0.9	180	9	1.1	342	81	3.4	
	29	8	52	32.9	62	41.1	150	51.7	109.1	4.2	26	4	76	136	1.19	2.7	6.9	C	11	2	1.4	101	3	2.7	247	86	6.9	
	29	10	45	20.8	61	43.5	141	57.8	4.0	2.7	9	3	250	188	0.57	16.2	18.2	D	102	29	2.4	211	31	7.8	338	45	25.0	
	30	11	38	14.8	62	21.2	147	52.4	23.1	2.7	18	9	224	131	0.54	3.0	2.8	B	93	18	1.5	199	40	3.5	344	44	2.2	
	30	12	34	22.4	63	49.4	147	32.4	106.2	4.3	16	3	282	306	0.67	21.0	24.4	D	298	9	16.4	31	18	20.5	183	70	25.0	
	30	18	13	25.5	61	48.8	151	48.1	109.0	3.6	24	13	98	72	0.67	1.7	2.3	A	86	2	1.2	177	16	1.6	349	74	2.4	
	30	20	48	24.2	60	1.3	139	25.1	22.3	0.9A	4	2	234	47	0.31	10.3	3.9	D	130	2	1.9	221	17	10.8	33	73	2.4	
	30	23	22	57.9	59	48.9	139	23.7	27.0	1.6	5	4	184	50	0.23	6.8	2.8	C	317	9	0.9	261	9	5.6	109	54	2.3	