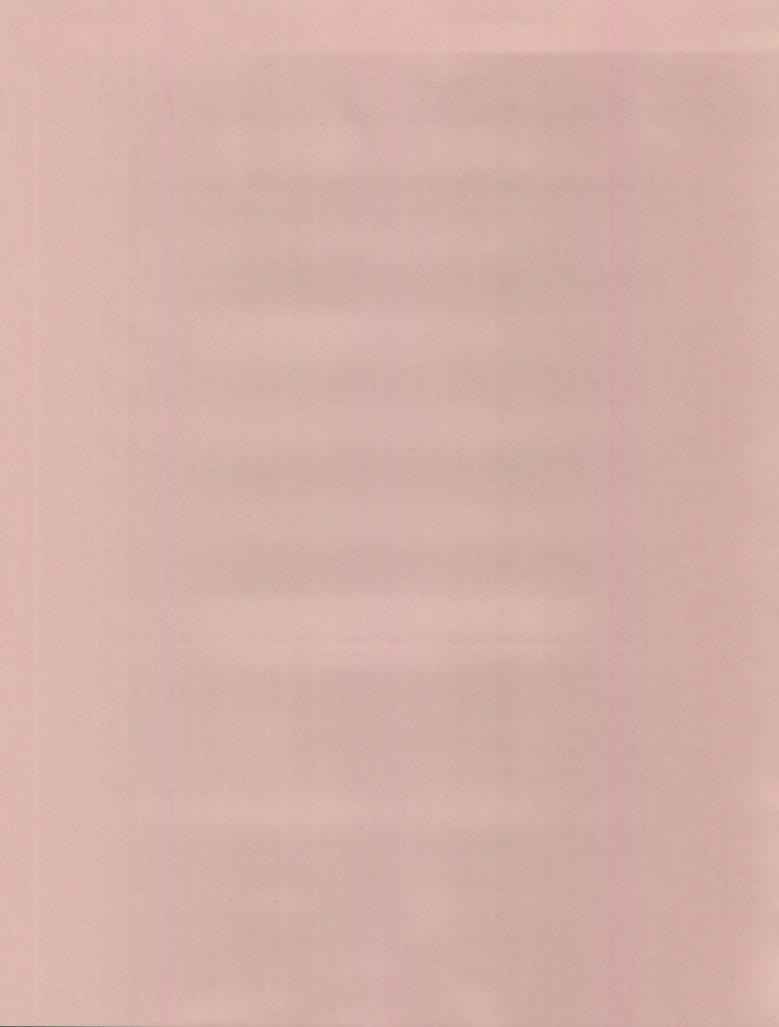
MAGNITUDE AND FREQUENCY OF HIGH FLOWS OF UNREGULATED STREAMS IN KANSAS

U.S. GEOLOGICAL SURVEY

Open-File Report 84-453

Prepared in cooperation with the KANSAS WATER OFFICE





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OF UNREGULATED STREAMS IN KANSAS

By P. R. Jordan

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UNITED STATES DEPARTMENT OF THE INTERIOR

WILLIAM P. CLARK, Secretary

GEOLOGICAL SURVEY

Dallas L. Peck, Director

For additional information write to:

District Chief U.S. Geological Survey, WRD 1950 Constant Avenue - Campus West University of Kansas Lawrence, Kansas 66046 [Telephone (913) 864-4321] Copies of this report can be purchased from:

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CONVERSION FACTORS

Inch-pound units of measurement used in this report may be converted to the International System of Units (SI) using the following factors:

Multiply inch-pound unit	By	To obtain SI unit
inch	1/25.4	millimeter
foot	0.3048	meter
mile	1.609	kilometer
square mile	2.590	square kilometer
foot per mile	0.1894	meter per kilometer
inch per hour	1/25.4	millimeter per hour
cubic foot per second (ft^3/s)	0.02832	cubic meter per second

 $^{^{1}}$ Exact conversion factor.

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ABSTRACT

Information on high-flow magnitude and frequency is needed for hydrologic evaluation of such factors as flood-control storage and dam safety. High-flow information given in this report is for streamflows unaffected by major regulation, such as by large reservoirs. High-flow magnitude and frequency data are given for 91 streamflow-gaging stations throughout Kansas. Results of frequency calculations are given for durations of high flow of 1, 3, 7, 15, 30, 60, 90, 120, and 183 consecutive days. Accuracy of the magnitude-frequency values is influenced by the variability of flow, the number of years of flow record, and the recurrence interval calculated.

High-flow magnitude and frequency for ungaged sites can be estimated from regression equations using significant drainage-basin characteristics of contributing-drainage area; 50-year, 24-hour rainfall; and free-water-surface evaporation. Standard errors of estimate for ungaged sites on ungaged streams range from 31 to 49 percent, generally increasing with recurrence interval. If an ungaged site is near a gaging station having 10 or more years of record on the same stream, the data for the gaging station may be used to improve the regression estimates.

INTRODUCTION

High-flow magnitude and frequency information is needed for design of future reservoirs and for safety evaluation of existing reservoirs. In design of new reservoirs, the information in this report will be particularly useful for small reservoirs whose small size cannot justify elaborate hydrologic modeling. Even for large reservoirs, this report's information may be superior to synthetic hydrographs based on estimated runoff relations and average storm patterns because it is based on adequate records of observed flows.

Inspection of existing reservoirs must include consideration of the volumes of flood water they can safely store or pass through. In addition, State regulations require certain classes of new reservoirs to provide flood-control storage equal to the inflow volume of specified frequency. This report can be used directly for that purpose.

This report applies only to high flows of 1-day and longer duration, unaffected by major regulation. For regulated flows, downstream from

major reservoirs, the responsible agency in most cases has determined expected high-flow magnitudes by detailed site-specific studies that include consideration of inflow, storage, evaporation, and reservoir-operation plans. Flood-peak magnitude and frequency are covered in other reports, most recently in Technical Report 11 of the Kansas Water Resources Board (Jordan and Irza, 1975).

This study was conducted by the U.S. Geological Survey in cooperation with the Kansas Water Office. Streamflow data analyzed were from gaging stations operated by the U.S. Geological Survey in cooperation with several State and Federal agencies.

Previous Studies

Results of the first comprehensive study of high flows (other than peak flows) in Kansas were reported by Furness and others (1964). The study was based on streamflow records through 1960 for which the smallest drainage area was 92 square miles. The report not only included high-flow probabilities and storage requirements at gaging stations but also a procedure for estimating storage requirements for ungaged sites with drainage areas of 150 to 7,500 square miles.

A series of working papers were prepared for the "Missouri River Basin Comprehensive Framework Study." High-flow magnitude and frequency for the Missouri River basin part of Kansas, based on streamflow records through 1963, were included in these papers, as described by the Missouri River Basin Inter-Agency Committee (1969).

Regression equations for estimating high-flow magnitude and frequency at ungaged sites were reported by Jordan and Hedman (1970) for selected recurrence intervals and durations of high flow. High-flow statistics, without frequency analysis, were given in two reports of streamflow statistics based on records through 1976 (Jordan, 1978, 1979).

SELECTION OF DATA FOR ANALYSIS

This study is limited to streamflow that is not significantly affected by regulation. Data from gaging stations downstream from major flood-control reservoirs, therefore, were excluded from the study. Not excluded, however, were gaging stations having flows affected by diversions for water supplies, by return flows from municipal or industrial use or from irrigated fields, and by structures such as low dams. These influences were assumed to have small effects on the high flows analyzed in this report, although in some cases the effects on long-duration (for example, 183-day) flows could be significant. A few of the gaging-station records used in the analysis were affected by small reservoirs in watershed districts during the later part of their records. These reservoirs affected small parts of the drainage to the stations used and were judged not to have significant effects on the high-flow magnitude-frequency values determined for this report.

Many stations at sites that are now affected by significant regulation of high flows were in operation before the reservoirs were built. Records of the earlier, unregulated flows were analyzed to aid in determining relations to basin characteristics, but high-flow magnitudes at these stations are not tabulated in this report because they are not applicable to current (1983) conditions.

Stations having at least 10 years of record of unregulated streamflow through 1980 were used in this study where available and applicable. For a few stations, records through 1981 were used. Stream gaging in Kansas began in the 1890's, so a few stations have long records. However, many of the first stations were on streams, such as the Kansas River, that now have regulated flow. Other early stations had their records interrupted for a substantial number of years. The longest record available for this study was 58 years, and four stations had more than 50 years. For most small basins having less than 150 square miles of drainage area, 1964 was the earliest record available; 25 basins were this small, and the smallest was 2.06 square miles.

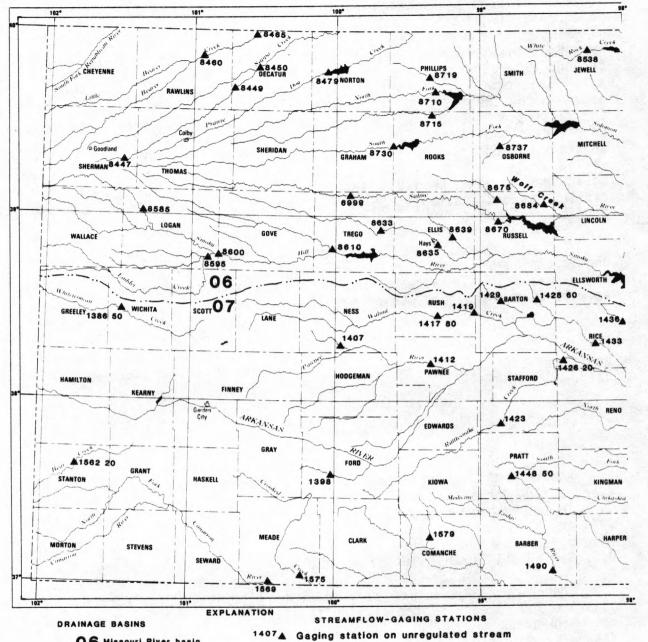
In the western part of Kansas (west of 99° longitude) streamflow conditions have changed markedly since about 1965 (Jordan, 1982). For these streams, data were analyzed for a limited recent period, 1966-80, as well as for the complete period of record.

The location of the gaging stations used in this study is shown in figure 1 for both those stations without significant regulation of flow and those now having regulation for which preregulation records were used.

HIGH-FLOW FREQUENCY AT GAGING STATIONS

Analysis of high-flow data began with the determination of the highest average flow for periods of 1, 3, 7, 15, 30, 60, 90, 120, and 183 consecutive days in each water year, October 1 through September 30. These data through 1976 are reported by Jordan (1978, 1979). Highest average flows for more recent years were determined by the same method, a computer program in the U.S. Geological Survey's WATSTORE water-data storage and retrieval system.

Frequency analysis was performed by fitting a log-Pearson Type-III distribution to each series of high flows. The log-Pearson Type-III method has been adopted by the U.S. Water Resources Council (1967, 1981) for frequency analysis of peak flows. No problems were encountered in applying the method to high flows of 1-day to 183-days duration. A few stations had high flows of zero (less than 0.05) cubic feet per second for some years, and a standard conditional-probability adjustment was used for these stations. In contrast to peak-flow data for many stations where information is available on historic peak flows outside the period of systematic record and can be used to improve the frequency calculations, high-flow data for 1 day and longer are available only for the period of systematic record. As recommended by the U.S. Water Resources Council (1981), the skewness coefficient used in each frequency computation was the weighted average of the coefficient calculated from the station's data



06 Missouri River basin

Basin boundary

07 Arkansas River basin

1795△ Gaging station on currently regulated stream, for which preregulation streamflow records were used

NOTE: Numbers shown are abbreviated versions of the complete 8-digit numbers

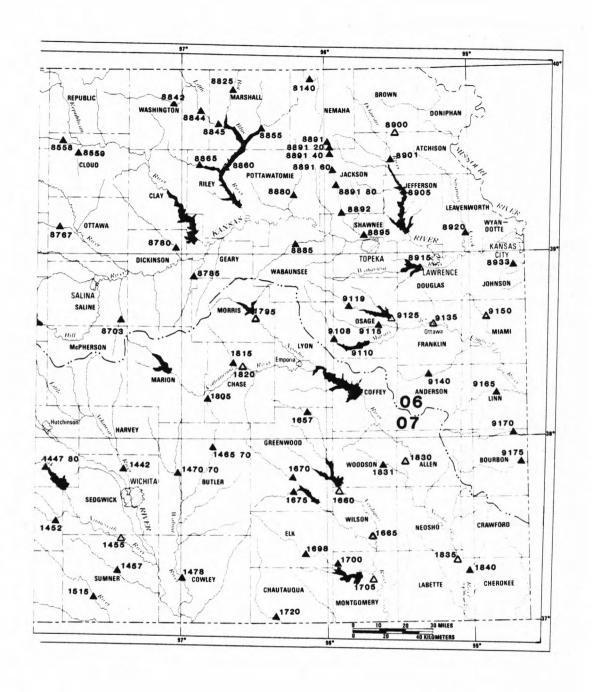


Figure 1.--Location of streamflow-gaging stations used in analysis of high-flow magnitude and frequency.

and the coefficient determined from a method of generalization. The methods of generalization and weighting used for this report are explained in the "Supplemental Information" section. An example of data used and the fitting of a log-Pearson Type-III distribution are shown in figure 2.

Results of Analysis

Results of the frequency analyses for stations now having unregulated flow are given in table 6 at the end of this report. For streams in the western part of the State (west of 99° longitude), results from records for 1966-80 are shown in addition to those from the entire period of record. The 1966-80 results may be better estimates of high flows for current (1983) conditions than calculations using data prior to 1966. However, the short period of record since 1965 causes the results to be erratic; for example, some 1966-80 frequency values are higher than those for the full period of record. The drainage areas shown in table 6 are the areas that directly contribute to surface runoff. These direct contributing areas are more pertinent to analysis of high flows than the total drainage areas.

Accuracy

The concept of the accuracy of frequency values is clearly stated by the Hydrology Committee of the U.S. Water Resources Council (1981, p. 9-1). The statement was written for peak flows but applies equally to high flows of 1-day or longer duration:

The record of annual peak flows at a site is a random sample of the underlying population of annual peaks and can be used to estimate the frequency curve of that population. If the same size random sample could be selected from a different period of time, a different estimate of the underlying population frequency curve probably would result. Thus, an estimated flood frequency curve can be only an approximation to the true frequency curve of the underlying population of annual flood peaks. To gauge the accuracy of the approximation, one may construct an interval or range of hypothetical frequency curves that, with a high degree of confidence, contains the population frequency curve. Such intervals are called confidence intervals and their end points are called confidence limits.

As indicated by this statement, accuracy of the discharge-frequency values presented herein is best at the 2-year and poorest at the 100-year recurrence interval. Good accuracy is associated with long records and low variability of discharge. Upper and lower confidence limits for each discharge frequency can be calculated by a complex procedure presented by the Water Resources Council (1981, Appendix 9). However, for the purpose of this report a simpler approach is taken.

STATION NUMBER 06886500

DISCHA	RGE-(CFS)	EST MEAN VALUE	AND RANKING FOR	THE FOLLOWING	NUMBER OF	CONSECUTIVE	DAYS IN	YEAR ENDING	SEPTEMBER 30	
MEAN										
	C AT WINKLER,	KS								
YEAR	1	3	7	15	30	60		90	120	183
1955	190.00 16	128.00 15	67.00 15	35.00 15	19.00 17	11.00	17	7.50 17	6.40 16	5.80 16
1956	199.00 15	87.00 16	43.00 16	22.00 17	21.00 16	12.00	16	7.90 16	6.00 17	3.90 17
1957	420.00 14	217.00 14	96.00 14	53.00 14	27.00 14	26.00	14	22.00 14	18.00 15	12.00 15
1958	5680.00 5	2030.00 7	1030.00 5	510.00 7	336.00 7	182.00	7	155.00 7	124.00 7	89.00 7
1959	806.00 13	501.00 13	341.00 12	182.00 12	112.00 13	63.00	13	57.00 12	52.0C 12	49.00 12
1960	3190.00 8	2420.00 4	1330.00 4	714.00 4	398.00	317.00	4	254.00 1	208.00 2	164.00 2
1961	2600.00 10	1320.00 10	672.00 10	381.00 11	274.00 10	176.00	8 .	131.00 9	109.00 9	87.00 8
1962	5920.00 3	2800.00 3	1620.00 2	985.00 1	594.00 1	346.00	1	246.00 2	210.00 1	175.00 1
1963	1970.00 11	705.00 12	319.00 13	162.00 13	113.00 12	67.00	.12	51.00 13	42.00 13	33.00 13
1964	5800.00 4	2220.00 6	935.00 8	654.00 6	340.00 6	176.00	9	128.00 10	109.00 10	79.00 9
1965	3610.00 6	2230.00 5	994.00 7	486.00 8	256.00 11	134.00	11	132.00 8	110.00 8	77.00 10
1966	151.00 17	65.00 17	37.00 17	28.00 16	23.00 15	21.00	15	19.00 15	18.00 14	15.00 14
1967	1650.00 12	942.00 11	643.00 11	419.00 10	275.CO 9	151.00	10	103.00 11	83.00 11	55.00 11
1968	3490.00 7	1370.00 9	1020.00 6	688.00 5	478.00 3	250.00	5	184.00 5	144.00 6	98.00 6
1969	2870.00 9	1970.00 8	955.00 9	471.00 9	289.00 8	184.00	6	166.00 6	145.00 5	142.00 3
1970	6390.00 1	3120.00 2	1430.00 3	793.00 3	441.00 4			220.00 4	169.00 4	115.00 5
1971	6060.00 2	3420.00 1	1660.00 1	963.00 2	566.00 2	321.00	2	228.00 3	177.00 3	131.00 4

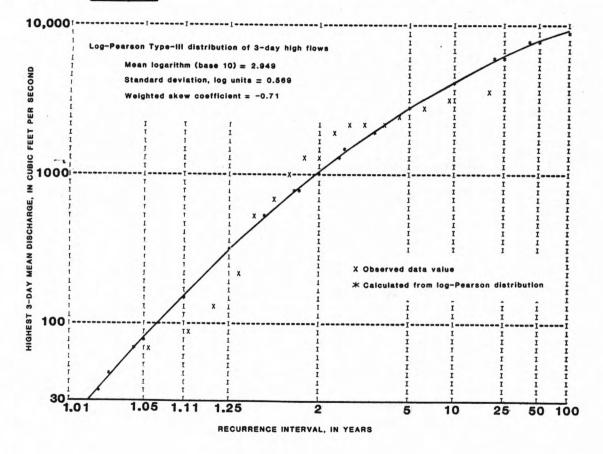


Figure 2.--Example of high-flow data and fitting of frequency distribution.

The standard error of an estimate, as explained in most textbooks on basic statistics, is a statistical measure of the accuracy of the estimate. In error distributions commonly encountered in a large group of similar calculations, about 68 percent of the calculated values are within one standard error of the true value. For this report, approximate standard errors were calculated by the method presented by Nash and Amorocho (1966). In table 6 (at the end of this report), a footnote on each of the four extremes for each station indicates the approximate percentage standard error. Since the calculations are from logarithmic data, the actual percentage standard errors are not equal in the positive and negative directions, but the average of the positive and negative values without regard to sign is shown. For the average of 20 percent, the directional standard errors are +22 and -18 percent; for the average of 50 percent, the directional standard errors are +62 and -38 percent.

HIGH-FLOW FREQUENCY ESTIMATES AT UNGAGED SITES

High-flow magnitude-frequency information may be needed at innumerable sites other than the 91 gaging stations that are shown in table 6 (at the end of this report). In this section of the report, "ungaged sites" comprises all stream sites that are not in table 6 and that are not affected by major regulation of high flow. Such sites include gaging stations having short-term records of streamflow (less than 10 years) as well as sites never gaged. An "ungaged" site may be on the same stream as one of the stations in table 6. If close enough, data for that station will be useful in making an estimate. If far from a station in table 6 or for an ungaged stream, the estimate can be made by using relations to physical and climatic basin characteristics. The relations to physical and climatic characteristics will be described first, then the use of these relations together with data in table 6, where applicable, will be described.

Relations of High-flow Frequency to Basin Characteristics

High-flow data used in this study were for the stations in table 6 plus stations on currently regulated streams for which preregulation records were used (fig. 1). For the basins west of 99° longitude, the frequency values for 1966-80 were used in order to represent current (1983) conditions. However, the 1966-80 period of only 15 years, together with the generally inconsistent nature of streamflows in western Kansas, reduces the reliability of the results for that region.

The high-flow frequency values can be identified by abbreviations in the form $\underline{d},\underline{Q}_{\mathsf{T}}$, where \underline{Q} is the average high flow for d consecutive days and T is the recurrence interval in years. For example, 15, \underline{Q}_{50} identifies the 15-day high flow for a 50-year recurrence interval.

Selection of physical and climatic characteristics for study was made after examining similar analyses, such as those by James (1968), Jordan and Hedman (1970), and Jordan and Irza (1975). The basin characteristics that were examined are defined as follows:

Contributing-drainage area (CDA), in square miles, is the drainage area that contributes surface runoff to the site. For most sites in Kansas, the contributing-drainage area is equal to the total drainage area. The method of determining the contributing-drainage area for sites where part of the total drainage does not contribute to surface runoff is explained in Technical Report 11 of the Kansas Water Office (formerly Kansas Water Resources Board) (Jordan and Irza, 1975, p. 25-27).

Main-channel length (L), in miles, is the length of the main low-water channel between the site and the drainage divide. The main channel is the one that drains the largest part of a basin.

<u>Main-channel slope</u> (\underline{S}), in feet per mile, is the slope between points on the main channel that are 10 percent and 85 percent of the main-channel length from the site to the drainage divide.

50-year, 24-hour rainfall ($\overline{150}$), in inches, was determined for the centroid of each basin from a map shown in the report by Hershfield (1961). The $\overline{150}$ was used as the rainfall characteristic because it was found to be slightly more significant statistically than several other indices to the general rainfall magnitude and intensity. The distribution of 50-year, 24-hour rainfall ($\overline{150}$) is shown for Kansas in figure 3.

<u>Free-water-surface evaporation (EV)</u>, in inches, is the average annual evaporation at the centroid of the drainage basin from map 3 of Farnsworth and others (1982). The Kansas part of the map is shown in figure 4.

Soil permeability (PS), in inches per hour, is determined from a generalized soil map (Jordan and Irza, 1975, fig. 9).

Pertinent statistical properties of the physical and climatic characteristics are shown in tables 1 and 2. A wide range of values for each characteristic used is desirable for detecting the relationship to the high flow. Low correlations between characteristics are desirable to prevent some relations from being obscured by random variation.

The standard least-squares multiple-regression technique was used in the statistical analysis. The technique, which is described in numerous textbooks, has been applied widely in hydrology, including studies of both peak flow and high flow (Benson, 1962, 1964; Jordan and Hedman, 1970; Thomas and Benson, 1970; Jordan and Irza, 1975). In order to achieve a nearly linear relationship between high flows and basin characteristics, all values were converted to their logarithmic equivalents. The resulting multiple linear regression model is of the general form:

$$\log \underline{Y} = \log \underline{a} + \underline{b_1} \log \underline{X_1} + \underline{b_2} \log \underline{X_2} + \dots + \underline{b_k} \log \underline{X_k}, \tag{1}$$

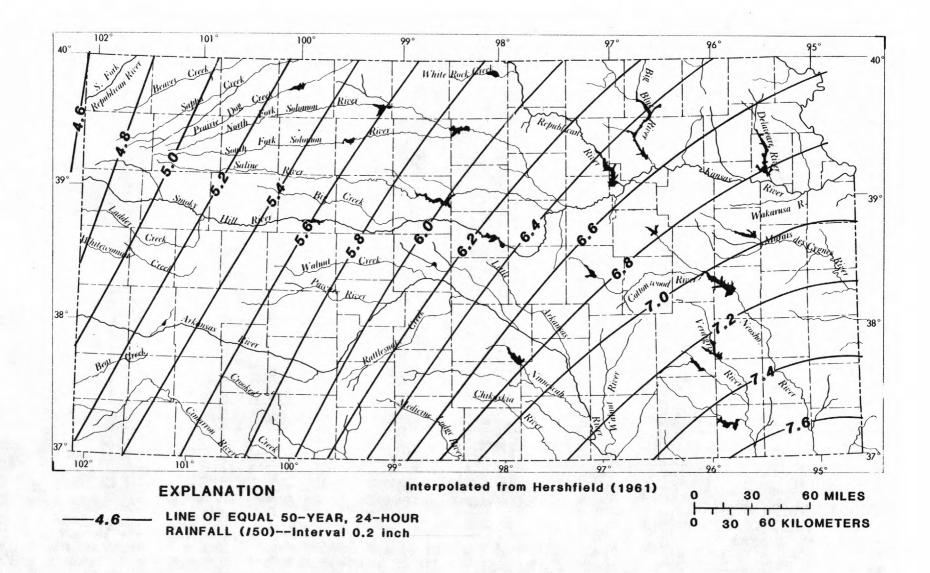


Figure 3.--Geographic distribution of 24-hour rainfall for 50-year recurrence interval.

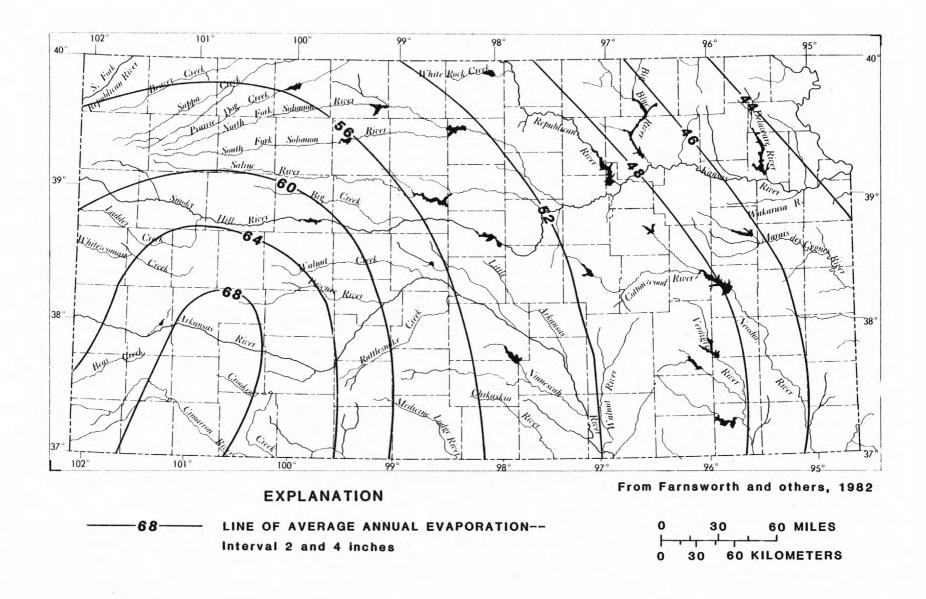


Figure 4.--Average annual free-water-surface evaporation.

which is equivalent to

$$\underline{Y} = \underline{a} \ \underline{X_1} \ \underline{X_2} \ \cdot \ \cdot \underline{X_k} \ , \tag{2}$$

in which

 \underline{Y} is the regression estimate of high-flow discharge (dependent variable); \underline{a} is a constant determined by the statistical analysis; \underline{X}_1 , \underline{X}_2 , \dots \underline{X}_k are drainage-basin characteristics (independent variables);

and

 $\underline{b_1}$, $\underline{b_2}$, . . . $\underline{b_k}$ are exponents determined by the statistical analysis.

Table 1.--Pertinent statistical properties of physical and climatic basin characteristics used in regression calculations

[CDA, contributing-drainage area, in square miles; <u>L</u>, main-channel length, in miles; <u>S</u>, main-channel slope, in feet per mile; <u>I50</u>, 50-year, 24-hour rainfall, in inches; <u>EV</u>, free-water-surface evaporation, in inches; <u>PS</u>, soil permeability, in inches per hour

Character- istic	Mean	Standard deviation	Minimum	Maximum
CDA	895	1,480	2.06	9,100
L	84.3	76.3	2.94	381
S	7.95	4.32	1.85	25.1
Ī50	6.34	0.733	4.8	7.5
EV	52.6	6.65	44	68
150 EV PS	0.794	0.598	0.1	4.6

Table 2.--Matrix of correlation coefficients of physical and climatic basin characteristics used in regression calculations

[CDA, contributing-drainage area, in square miles; <u>L</u>, main-channel length, in miles; <u>S</u>, main-channel slope, in feet per mile; <u>I50</u>, 50-year, 24-hour rainfall, in inches; <u>EV</u>, free-water-surface evaporation, in inches; <u>PS</u>, soil permeability, in inches per hour]

	log <u>CDA</u>	log <u>L</u>	log <u>S</u>	log(<u>150</u> -4.0)	log (<u>EV</u> -20.0)	log <u>PS</u>
log CDA	1.000	0.947	-0.539	-0.234	0.251	0.238
log L	.947	1.000	527	326	.338	.333
log S	539	527	1.000	382	.205	.085
log (I50-4.0)	234	326	382	1.000	673	443
log (EV-20)	.251	.338	.205	673	1.000	.550
log <u>PS</u>	.238	.333	.085	443	.550	1.000

In order to use the linear model described above, after examination of the residuals as explained in the "Supplemental Information" section, the characteristic $\underline{150}$ was used in the form ($\underline{150}$ -4.0), and \underline{EV} was used in the form (\underline{EV} -20.0). These two characteristics and \underline{CDA} were the only ones found to be significant enough statistically (5-percent level) to include in the regression equations. The resulting form of equation 2 is:

$$\underline{Y} = \underline{a} \ \underline{CDA}^{\underline{b}_1} \ (\underline{I50} - 4.0)^{\underline{b}_2} \ (\underline{EV} - 20.0)^{\underline{b}_3} \ .$$
 (3)

The constants (\underline{a}) , exponents (\underline{b}) , and standard errors of estimate determined for all high-flow magnitude-frequency values are given in table 3. The regression equations should be used only within the ranges of minimum and maximum values shown in table 1. Because of the unique character of the Cimarron River, its data were not used in developing the regression equations, and the equations are not applicable to it.

For an example of the application of a regression equation to estimate a high-flow magnitude-frequency value at an ungaged site, assume that an estimate of the 15-day, 10-year high flow is needed for a site on Wolf Creek near its mouth in Lincoln County, Kansas. A gaging station was in operation at the site during 1946-53 but has less than 10 years of record; so the site is considered "ungaged" for this purpose. From table 3, for the 15-day, 10-year high flow (15, Q_{10}), the regression constant is 211, and the exponents are 0.871 for contributing-drainage area (CDA), 2.747 for 50-year, 24-hour rainfall minus 4.0 (I50-4.0), and -1.606 for evaporation minus 20.0 (EV-20.0). Thus, the regression equation is

$$15_{,010} = 211 \ \underline{CDA}^{0.871} \ (\underline{I50} - 4.0)^{2.747} \ (\underline{EV} - 20.0)^{-1.606} \ . \tag{4}$$

Measured from topographic maps, the contributing-drainage area is 261 square miles. From figures 3 and 4, at the centroid of the drainage basin, $\underline{150}$ is 5.9 inches, and \underline{EV} is 55 inches. The estimate of 15, $\underline{Q_{10}}$ now can be calculated as:

$$15,\underline{Q}_{10} = 211 (261)^{0.871} (5.9-4.0)^{2.747} (55-20.0)^{-1.606}$$

$$= 519 \text{ ft}^3/\text{s.}$$
(5)

Accuracy of this estimate is indicated in table 3 by a standard error of estimate of 33 percent. This is the estimate that would be used if table 6 (at the end of this report) did not include data for a gaging station on the same stream.

Ungaged Sites On Gaged Streams

If the ungaged site is near a gaging station listed in table 6 on the same stream, the data for the gaging station can be used to improve the estimates resulting from application of the regression equations. The

Table 3.--Constants and exponents for regression equation 3 for estimating high-flow magnitude and frequency at ungaged sites

Period	Recurrence	Constant		Exponents		Standard
of consecu- tive days	interval (years)	<u>a</u>	b1 (for CDA)	b2 (for 150- 4.0)	b3 (for EV- 20.0)	error of estimate (percent)
1 day	2 5	3,300	0.731	2.936	-2.071	36
		3,040	.691	2.472	-1.632	33
	10	2,700	.676	2.215	-1.401	35
	25	2,220	.664	1.936	-1.149	39
	50	1,890	.659	1.752	984	44
	100	1,630	.656	1.580	838	49
3 day	2 5	1,010	.829	3.111	-2.087	36
		889	.797	2.707	-1.666	31
	10	794	.785	2.467	-1.447	32
	25	685	.776	2.195	-1.216	36
	50	609	.771	2.008	-1.065	40
	100	546	.768	1.833	930	44
7 day	2	498	.874	3.223	-2.154	36
	5	406	.852	2.864	-1.741	31
	10	330	.843	2.634	-1.503	32
	25	237	.835	2.365	-1.226	35
	50	182	.831	2.179	-1.033	38
	100	140	.828	2.000	854	42
15 day	2 5	361	0.901	3.293	-2.276	36
		287	.880	2.962	-1.870	32
	10	211	.871	2.747	-1.606	33
	25	123	.865	2.509	-1.278	36
	50	81.3	.861	2.335	-1.047	39
	100	53.2	.857	2.169	824	43
30 day	2	280	.919	3.336	-2.379	37
	2 5	280	.904	3.027	-2.056	32
	10	225	.898	2.819	-1.827	33
	25	138	.892	2.578	-1.512	36
	50	89.2	.888	2.405	-1.273	39
	100	56.6	.885	2.233	-1.039	42
60 day	2	234	.941	3.339	-2.503	37
	5	215	.926	3.061	-2.166	33
	10	162	.919	2.869	-1.919	34
	25	90.8	.913	2.651	-1.585	38
	50	56.4	.908	2.482	-1.335	41
	100	35.6	.903	2.309	-1.095	45

Table 3.--Constants and exponents for regression equation 3 for estimating high-flow magnitude and frequency at ungaged sites--Continued

Period of consecu- tive days	Recurrence interval - (years)	Constant <u>a</u>	b ₁ (for CDA)	b ₂ (for 150- 4.0)	b3 (for EV- 20.0)	Standard error of estimate (percent)
90 day	2 5 10 25 50 100	185 208 160 89.9 55.9 32.0	0.953 .938 .934 .930 .927	3.372 3.106 2.927 2.722 2.564 2.417	-2.535 -2.264 -2.037 -1.712 -1.469 -1.214	37 33 34 37 41 44
120 day	2 5 10 25 50 100	152 199 145 79.7 47.5 27.8	.954 .941 .938 .936 .935	3.367 3.136 3.001 2.833 2.705 2.578	-2.528 -2.316 -2.087 -1.772 -1.528 -1.289	39 33 34 37 40 44
183 day	2 5 10 25 50 100	124 153 108 55.5 33.0 17.5	.968 .958 .952 .949 .947	3.385 3.194 3.074 2.919 2.794 2.674	-2.571 -2.363 -2.127 -1.796 -1.553 -1.283	40 33 34 38 41 45

recommended procedure is to use a weighted estimate, Qwu:

$$Q_{WU} = W_E Q_{EU} + W_Q R_Q Q_{EU} , \qquad (6)$$

in which

is the weighting factor (explained below) for Q_{Eu} ; WE

is the high-flow value from application of the regression QEu equation at the ungaged site;

 $\begin{array}{l} \text{Wg = 1.0 - WE and is the weighting factor for R}_{g}; \text{ and} \\ \text{Rg = Q}_{gg}/\text{Q}_{Eg} \text{ , a regression adjustment factor, where Q}_{gg} \text{ is the high-flow value determined from gaged data (table 6), and Q}_{Eg} \end{array}$ is the high-flow value from application of the regression equation at the gaging station.

The recommendation for W_E is to (arbitrarily) assume that the station data in table 6 provide the best estimate at the station and that the regression equation provides the best estimate where the area draining to the ungaged site (A_{U}) is less than one-half or more than double the area draining to the gaging station (A_q). Thus, where $A_{II}/A_{II} = 1.0$, W_F = 0.0;

where $A_u/A_g \le 0.5$, $W_E = 1.0$; and where $A_u/A_g \ge 2.0$, $W_E = 1.0$. Between these points, a convenient interpolation formula can be used:

$$W_{E} = 0.5 - 0.5 \cos(4.53 \ln \frac{A_{u}}{A_{u}})$$
 (7)

In using this formula, interpret the expression in parentheses as an angle in radians. The weighting factor W_E also can be determined from figure 5, the graph of equation 7.

Basin characteristics used in the regression equations are shown in table 4 to facilitate calculation of R_α for the gaging stations in table 6.

The "ungaged" site on Wolf Creek near its mouth will be used for an example of the method of improving a regression estimate. Figure 1 and table 6 show station 06868400 on Wolf Creek in Russell County. From table 6, station 06868400 has a contributing-drainage area of 163 square miles and a 15,010 (0qq) of 487 ft $^3/s$. The ratio Au/Ag is 261/163 = 1.60, which is within the range where the method is applicable. The regression result at station 06868400 can be calculated using the basin-characteristics data in table 4, with the same regression constant and exponents that were previously used for the ungaged site:

$$Q_{Eq} = 211 (163)^{0.871} (5.9-4.0)^{2.747} (55-20)^{-1.606} = 344 \text{ ft}^3/\text{s}$$
. (8)

Thus, $R_g = Q_{gg}/Q_{Eg} = 487/344 = 1.42$.

From equation 7 or figure 5, $W_F = 0.765$.

$$W_q = 1.0 - W_E = 1.0 - 0.765 = 0.235.$$

 Q_{Eu} is the regression result for 15, Q_{10} at the ungaged site, calculated previously as 519 ft³/s. The weighted estimate Q_{wu} is calculated as

$$Q_{Wu} = W_E \ Q_{Eu} + W_g \ R_g \ Q_{Eu}$$
;
= 0.765 (519) + 0.235 (1.42) 519 ;
= 570 ft³/s, the improved estimate for 15, Q_{10} at the ungaged site.

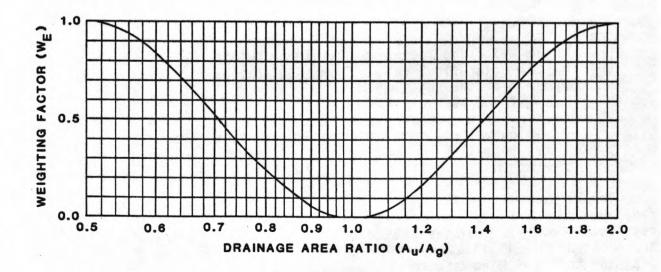


Figure 5.--Interpolation of weighting factor for ungaged site on gaged stream.

Table 4.--Gaging-station values of basin characteristics used in regression equations

[CDA, contributing-drainage area, in square miles; $\underline{150}$, 50-year 24-hour rainfall, in inches; \underline{EV} , free-water-surface evaporation, in inches]

Station number	CDA	150	<u>EV</u>
06814000	276	6.5	45
06844700	74	4.8	58
06844900	378	4.9	58
06845000	900	4.9	57
06846000	1,117	4.8	57
06846500	1,324	4.9	56
06847900	590	5.1	57
68538000	227	5.8	51
06855800	330	5.9	51
06855900	56	6.1	51
06858500	650	4.7	59
06859500	1,460	5.0	63
06860000	3,390	4.9	61
06861000	5,220	5.0	62
06863300	297	5.5	61
06863500	594	5.6	61
06863900	54	5.8	58
06866900	696	5.2	59
06867000	1,502	5.5	59
06867500	212	5.8	56
06868400	163	5.9	55
06870300	120	6.5	52
06871000	849	5.3	57
06871500	341	5.4	58
06871900	65	5.4	55
06873000	1,040	5.4	59
06873700	52	5.8	55
06876700	384	6.1	53
06878000	300	6.3	50
06878500	230	6.6	50
06882500	4,540	6.2	45
06884200	344	6.1	47
06884500	3,440	5.8	47
06885500	410	6.4	45
06886500	174	6.3	48

Table 4.--Gaging-station values of basin characteristics used in regression equations--Continued

Station number	CDA	<u>150</u>	<u>EV</u>
06888000	243	6.5	46
06888500	316	6.7	48
06889100	2.1	6.5	45
06889120	10.5	6.5	45
06889140	16.9	6.6	45
06889160	49.3	6.6	45
06889180			
	80	6.6	45
06889200	157	6.7	45
06889500	290	6.7	46
06890100	431	6.7	44
06890500	922	6.6	45
06892000	406	6.8	44
06893300	26	6.9	44
06910800	177	7.0	48
06911500	111	6.9	47
06911900	114	6.8	45
06914000	334	7.2	47
06916500	198	7.2	46
06917000	295	7.3	45
06917500	408	7.4	45
07138650	750	4.0	62
		4.9	
07139800	73.8	5.8	68
07140700	58.2	5.7	65
07141200	2,010	5.7	66
07141780	1,152	5.6	64
7141900	1,306	5.7	68
07142300	356	6.1	62
07142620	598	6.2	61
07142860	43	6.1	56
07142900	61	6.0	58
07143300	499	6.2	61
07143600	71	6.4	55
07144200	1,250	6.6	53
07144780	550		56
07144850 07144850	21	6.5 6.4	59
07145200			57
07145200	543	6.6	
07145700	154	7.1	54
07146570	30	7.0	51
07147070	426	6.9	52
07147800	1,872	7.1	51

Table 4.--Gaging-station values of basin characteristics used in regression equations--Continued

Station number	CDA	<u>150</u>	EV
07149000	903	6.5	59
07151500	794	6.9	56
07156220	835	⁵ 1 ² /	66 1/
07156900	4,220	1/	
07157500	813	5.8	68
07157900	39	6.2	63
07165700	181	7.1	49
07167000	307	7.1	50
07167500	129	7.2	50
07169800	220	7.3	. 50
07170000	575	7.3	53
07172000	445	7.4	50
07180500	110	6.9	51
07181500	92	6.8	51
07183100	177	7.3	48
07184000	197	7.5	45

Regression equations not applicable to Cimarron River.

SUMMARY

High-flow magnitude and frequency data are given in this report for 91 streamflow-gaging stations where flow is unaffected by major regulation, such as by large reservoirs. Equations are given for estimating high-flow magnitude and frequency at ungaged sites. Data or estimates of high flow are needed for evaluation of such factors as flood-control storage and dam safety.

Results of frequency calculations are given for durations of high flow of 1, 3, 7, 15, 30, 60, 90, 120, and 183 consecutive days. The calculations were made by using the log-Pearson Type-III distribution with a weighted-average skew coefficient calculated from a regionalized value and a value from the station data for each gaging station. Because of changes in flow characteristics in western Kansas since about 1965, high-flow magnitude and frequency values for stations west of 99° longitude are given for 1966-80 as well as for the entire period of record. Accuracy of the magnitude-frequency values is indicated by standard errors that are less than 20 percent for stations where variability is low and records are long, and standard errors of more than 50 percent where variability is high and records are short.

Regression equations are given for estimating high-flow magnitude and

frequency for ungaged sites or gaging stations that have less than 10 years of record. The drainage-basin characteristics used in the equations are contributing-drainage area, 50-year, 24-hour rainfall, and free-water-surface evaporation. Standard errors of estimate range from 31 to 49 percent, generally increasing with recurrence interval. If an ungaged site is near a gaging station having 10 or more years of record on the same stream, the gaging-station data may be used to improve the estimates.

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SUPPLEMENTAL INFORMATION

Explanation of Selected Statistical Terms

For purposes of hydrologic analysis and design of flood-control reservoirs, the degree of extremity of a high flow is expressed by its probability of exceedence. A very low probability indicates an extreme flow. A high flow that has a probability of 2 percent has a 2-percent chance of being exceeded in any 1 year. Another interpretation of the probability concept is that during a period of 1,000 years, if all conditions remain the same, about 20 of the years will have high flows exceeding the 2-percent probability flow.

Although the concept of probability is the most meaningful way of classifying and comparing extreme hydrologic events, the terminology in more common use is the recurrence interval, in years, which is 100 times the reciprocal of the probability when the probability is in percent. Thus, a 2-percent probability high flow has a recurrence interval of 50 years. A high-flow magnitude having a recurrence interval of $\underline{\mathbf{T}}$ years is expected to be exceeded an average of once in each period of $\underline{\mathbf{T}}$ years. That magnitude may be exceeded more than once in any particular period of $\underline{\mathbf{T}}$ years, or no flow exceeding that magnitude may occur during an equivalent period. The fact that a flow of given magnitude occurs in 1 year does not reduce the probability of a flow of equal or greater magnitude occurring during the next year.

Recurrence intervals in this report are based on the <u>annual series</u> of high flows. For this series, only the highest flow of each selected number of days for each year is used even though the second highest in 1 year may have exceeded the highest of some other year. Use of the annual series permits simple, straightforward computations and interpretation of recurrence intervals.

In the statistical calculation of a regression equation, the <u>dependent variable</u> is the variable whose magnitude is to be calculated from the values of the other variables. In this report, the dependent variable is always a high-flow magnitude, known for gaged sites and unknown for ungaged sites. The <u>independent variables</u> are the variables to be used in calculating an estimated value of the dependent variable. The values of the independent variables are known for gaged sites and are known or can be measured for ungaged sites. Independent variables are not required to be unrelated to each other, although some difficulties of interpretation and applicability can occur if they are closely related.

When a regression equation is developed, a <u>residual</u> is the amount by which an observed magnitude of the dependent variable differs from the magnitude calculated from the independent variables. Study of residuals is an important part of the use of the statistical regression technique. When residuals for each step of a stepwise regression are plotted against each independent variable, the plots can reveal any significant nonlinearities that may occur within the range of the data studied. Different transformations of the data then may be used to produce linear relationships and reduce the errors of the estimate. When residuals are plotted on a map, they may show the effect of some variable or variables that differ geographically but which are not included in the regression. The map, together with the hydrologist's knowledge of the region, may provide a clue to the missing variables.

In this report, standard error of estimate is the measure of the errors associated with the calculation of high-flow magnitude by a regression equation. Standard error of estimate, originally calculated in logarithmic units, can be interpreted to represent percentage errors. The percentages are unequal in the positive and negative directions. For example, a standard error of estimate of 0.17 logarithmic units represents errors of +48 percent and -32 percent; the average of the two percentages without regard to sign is 40 percent. In a large number of similar calculations, about two-thirds of the calculated high-flow magnitudes would be within the stated percentages of the true magnitudes.

Mean, standard deviation, and skewness coefficient are defined in standard textbooks on statistics, and their specific definitions are not repeated in this report. Their general meanings are that the mean is a measure of the central tendency of a group of data, standard deviation measures the variability, and skewness coefficient measures the degree and direction of departure from a symmetrical distribution.

Regionalization of Skew Coefficients

Log-Pearson Type-III frequency tables for high flows are calculated from three parameters for each set of data—the mean, the standard deviation, and the skew coefficient. Because the mean is calculated from each data value to the first power, the standard deviation from data value to the second power, and the skew coefficient from each data value to the third power, the mean is the most stable (has the least variation between time samples) and the skew coefficient the least stable. In a typical time

sample of 15 to 25 years the calculated skew coefficient can be drastically affected by a single extremely high or low discharge value in 1 year. Therefore, it is desirable to use information from a group of stations having long periods of record instead of a single station having a short-term record in determining the best value of skew coefficient to use for a particular frequency calculation.

Selection of Records for Study

The Hydrology Committee of the U.S. Water Resources Council used records of 25 years and longer through 1973 in producing a map of the United States showing the regional variations of skew coefficients of peak flows. In Kansas there are now numerous stations that have records of 29 years or longer (through 1980) of unregulated high flow, including records of flow prior to reservoir construction. Therefore, the decision was made to use 29 years as the minimum record length for the final determination of regionalized values for skew coefficients. However, some 21-28 year records were used in the preliminary step of identifying regions.

Relation of Skew Coefficient to Duration of High Flow and to Location

Because high-flow frequency distributions are calculated for nine different durations of consecutive days, the variation of skew coefficients with number of days had to be considered as well as the regional variation. The regional variation was examined first for a short duration (3 days) and for a long duration (120 days) by plotting the skew coefficients on a map of the State. The 3-day coefficients showed the most variation and were used in identifying the geographic trends. The geographical variation of these coefficients was such that it could not reasonably be described by contour lines. Instead, the coefficients showed a grouping in three distinct regions (fig. 6), although the western region exhibited large, apparently random variation. Next the variation of skew coefficient with number of days was examined within each of these regions. Variations in the northeast region are shown in figure 7. In each region the median coefficient for each number of days and for the peak was calculated. Coefficients for peak discharges were included for aid in determining relations. The regionalized coefficients to be used were determined by drawing a smooth curve averaging the median coefficients, then rounding the curve values to the nearest 0.1 skew unit. Table 5 shows the resulting regionalized skew coefficients.

Weighting of Regional and Station Skew

The regionalized skew coefficient and the coefficient calculated from station data can be combined to give a better estimate of the skew coefficient for a given station (U.S. Water Resources Council, 1981, p. 12).

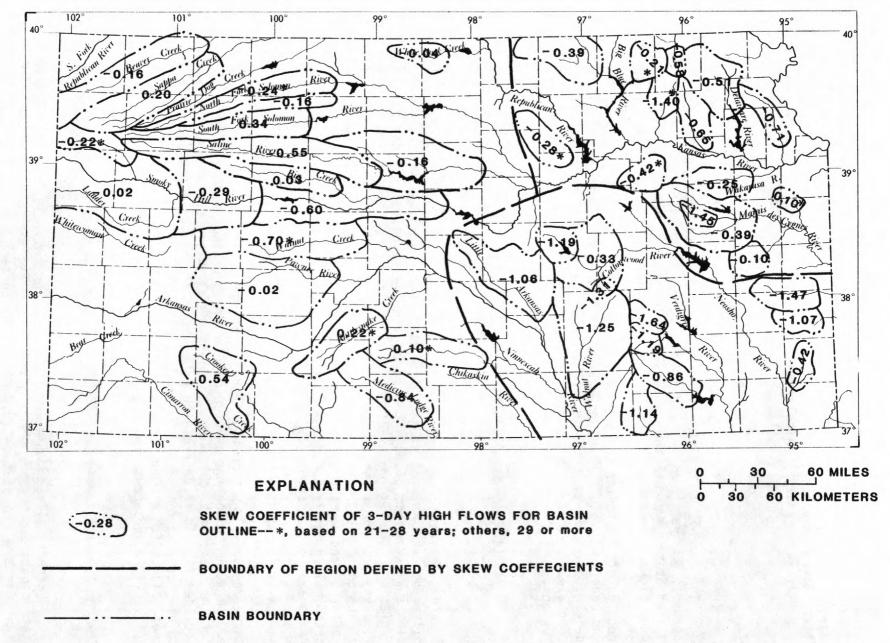


Figure 6.--Geographic variation of skew coefficients and regions defined for analysis.

The regionalized and station skews are weighted in inverse proportion to their individual mean-square errors. The mean-square error of station skew is a function of record length and station skew and was determined from table 1 of the U.S. Water Resources Council report (1981). The mean-square error of the regionalized skew was calculated from the variation of the coefficients within each region for record lengths of 29 years and longer.

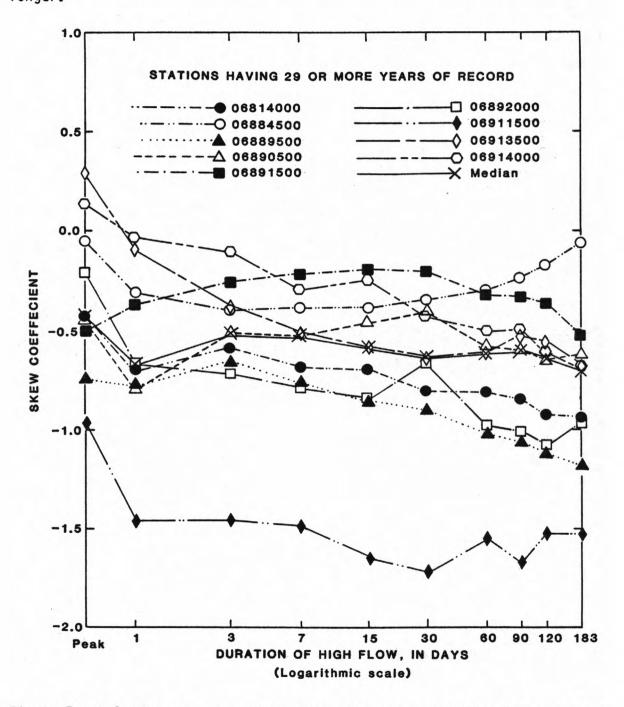


Figure 7.--Relation of skew coefficient to number of consecutive days of high flow in northeastern Kansas.

Table 5.--Regionalized skew coefficients for 1-day through 183-day high flows

[See figure 6 for region boundaries]

	Skew coefficient for indicated duration of high flow								
Region	1 day	3 day	7 day	15 day	30 day	60 day	90 day	120 day	183 day
West	-0.1	-0.1	0	0.1	0.2	0.3	0.3	0.3	0.4
Northeast	5	5	5	6	6	6	6	6	7
Southeast	-1.1	-1.1	-1.1	-1.1	-1.0	-1.0	-1.0	-1.0	-1.0

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow

ation number, name, and location	Contri- buting- drain- age area (square	analy- zed	rence interval (years)	Maximum average discharge, in cubic feet per second, for indicated period of consecutive days										
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 days		
06 8140 00 Turkey Creek near Seneca	276	1950-80	2	3680.0ª	2040.0	1100.0	647.0	427.0	2=1.0	231.0	197.0	154.0ª		
(Nemaha County, 2.0 miles down-			5	8220.0	4660.0	2510.0	1440.0	964.0	633.0	514.0	435.0	336.0		
stream from Clear Creek, 5.0			10	11800.0	6810.0	3630.0	2050.0	1380.0	902.0	728.0	510.0	466.0		
miles upstream from Big Nemaha			25	16600.0	9820.0	5170.0	2860.0	1920.0	1250.0	1010.0	830.0	625.0		
River, and 8.0 miles northwest			50	20300.0	12200.0	6350.0	3470.0	2320.0	1510.0	1210.0	986.0	736.0		
of Seneca.)			100	23900.0b	14600.0	7540.0	4060.0	2700.0	1760.0	1400.0	1130.0	837.cb		
06 8447 00 South Fork Sappa Creek	74.0	1968-80	2	14.0 ^C	7.0	3.2	1.5	0.0	0.5	0.3	0.3	0.2 ^b		
near Brewster			5	109.0	38.0	17.0	8.2	4.0	2.5	1.7	1.4	0.9		
(Sherman County, 9.0 miles south-			10	284.0	35.0	37.0	19.0	8.9	5.5	3.5	2.2	1.5		
west of Brewster.)			25	717.0	185.0	31.0	41.0	20.0	11.6	6.9	3.3	2.5		
			50	1270.0	304.0	133.0	69.0	33.0	18.0	11.6	4.1	3.3		
			100	2100.0 ^C	477.0	210.0	111.0	54.0	29.0	16.0	5.0	4.4°		
6 8449 00 South Fork Sappa Creek	378	1960-80	2	116.0 ^b	31.0	42.0	22.0	13.0	7.9	5.7	4.6	3.2b		
near Achilles			5	580.0	375.0	188.0	103.0	55.0	27.0	20.0	16.0	11.0		
(Decatur County, 5.5 miles south-			10	1480.0	821.0	412.0	238.0	122.0	54.0	39.0	31.0	22.0		
east of Achilles, 14 miles south-			25	4250.0	1870.0	956.0	585.0	287.0	114.0	83.0	07.0	47.0		
west of Oberlin, and 18.5 miles			50	8710.0	3160.0	1650.0	1050.0	500.0	139.0	139.0	112.0	80.0		
upstream from confluence with			100	17000.0°	5040.0	2690.0	1790.0	826.0	304.0	225.0	181.0	131.0°		
		1966-80	2	112.0°	63.0	31.0	16.0	8.9	5.3	3.8	3.0	2.1b		
		1300-00	5	530.0	292.0	139.0	73.0	39.0	19.0	13.0	10.0	7.0		
			10	1100.0	596.0	286.C	150.0	81.0	37.0	26.0	20.0	14.0		
			25	2250.0	1200.0	588.0	310.0	170.0	80.0	55.0	42.0	29.0		
			50	3470.0	1820.0	916.0	481.0	271.0	133.0	91.0	69.0	47.0		
			100	5010.0°		1340.0	701.0	408.0	217.0	148.0	111.0	76.0°		
16 8450 00 Sappa Creek near Oberlin	900	1930-31.	2	498.0b	310.0	175.0	99.0	63.0	38.0	29.0	24.0	18.0 ^b		
(Decatur County, 0.3 mile down-		1945-72	5	1370.0	856.0	481.C	262.0	163.0	99.0	75.0	62.0	45.0		
stream from confluence of North			10		1470.0	824.0	440.0	271.0	168.0	127.0	105.0	73.0		
and South Forks and 3.5 miles sout	th-		25		2650-0		767.0	471.0	300.0	224.0	185.0	125.0		
west of Oberlin.)			50			2150.0		675.0	440.C	324.0	268.0	176.0		
			100			3030.0		936.0	625.0	454.0	377.0	239.0 ^b		
6 8460 00 Beaver Creek at Ludell	1,117	1930-31,	2	307.0 ^b	179.0	110.0	75.0	50.0	34.0	28.0	24.0	20.0b		
(Rawlins County, 0.5 mile south		1946 - 53	5	805.0	524.0	306.0	201.0	130.0	90.0	72.0	62.0	48.0		
of Ludell and 9.6 miles down-			10	1290.0	899.0	517.0	338.0	222.0	155.0	125.0	106.0	79.0		
stream from Little Beaver Creek.)			25		1580.0	898.0	593.0	400.0	288.0	235.0	194.0	141.0		
CONTROL OF SERVICE STREET, STR			50	2830.0		1280.0	856.0	592.0	438.0	363.0	294.0	210.0		
			100			1750.0	1200.0	849.0	647.0	544.0	433.0	303.f		

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	buting- drain- age area (square	rain- zed interval Maximum average discharge ge (years) for indicated peri rea							e, in cubic feet per second, iod of consecutive days					
	miles)		_	1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 day		
06 8465 00 Beaver Creek at Cedar	1,324	1947-80	2	347.0ª	221.0	128.0	78.0	50.0	32.0	24.0	19.0	13.0 ^b		
Bluffs			5	918.0	632.0	402.0	245.0	163.0	110.0	86.0	71.0	53.0		
(Decatur County, at U.S. High-			10	1520.0	1080.0	733.0	436.0	298.0	208.0	167.0	140.0	108.0		
way 83, 0.2 mile north of Cedar			25	2610.0	1880.0	1400.0	792.0	557.0	402.0	335.0	289.0	235.0		
Bluffs, and 1.0 mile south of			50	3690.0	2670.0	2130.0	1160.0	827.0	612.0	524.0	461.0	389.0		
Kansas-Nebraska State line.)			100	5040.0b	3640.0	3100.0	1620.0	1170.0	888.0	781.0	700.0	615.0°		
		1966-80	2	237.0ª	129.0	70.0	42.0	24.0	14.0	11.0	8.7	5.7b		
			5	389.0	255.0	154.0	99.0	61.0	36.0	28.0	22.0	16.0		
			10	489.0	354.0	231.0	153.0	98.0	59.0	45.0	36.0	27.0		
			25	612.0	495.0	351.0	240.0	160.0	99.0	74.0	59.0	46.0		
			50	699.0	609.0	458.0	317.0	219.0	137.0	101.0	80.0	65.0		
			100	782.0b	728.0	580.0	406.0	290.0	183.0	133.0	104.0	88.0°		
6 8479 00 Prairie Dog Creek above	590	1963-80	2	488.0b	288.0	142.0	76.0	46.0	27.0	22.0	18.0	14.0b		
Keith Sebelius Lake			5	1300.0	738.0	355.0	184.0	108.0	62.0	46.0	38.0	28.0		
(Norton County, 4.0 miles east			10	2020.0	1130.0	540.0	282.0	160.0	98.0	69.0	58.0	69.0		
of Clayton.)			25	3050.0	1680.0	837.0	435.0	259.0	167.0	106.0	91.0	63.0		
7			50	3870.0	2130.0	1080.0	568.0	343.0	238.0	139.0	122.0	83.0		
			100	4720.0C	2580.0	1350.0	717.0	440.0	330.0	178.0	161.0	106.0 ^b		
		1966-80	2	412.0b	244.0	122.0	67.0	41.0	26.0	20.0	17.0	13.0 ^b		
			5	1150.0	639.0	309.0	162.0	95.0	57.0	41.0	33.0	24.C		
			10	1830.0	991.0	479.0	252.0	145.0	84.0	60.0	47.0	34.0		
			25	2860.0	1510.0	741.0	394.0	226.0	127.0	88.0	68.0	68.0		
			50	3720.0	1930.0	965.0	520.0	298.0	165.0	113.0	86.0	60.0		
			100	4630.0 ^C		1210.0	663.0	381.0	209.0	141.0	106.0	74.0b		
6 8538 00 White Rock Creek near	227	1958-80	2	1010.0ª	570.0	316.0	177.0	108.0	64.0	50.0	42.0	31.0a		
Burr Oak			5	2070.0	1190.0	651.0	366.0	229.0	130.0	101.0	84.0	63.0		
(Jewell County, 3.5 miles north-			10		1730.0	930.0	523.0	336.0	189.0	145.0	121.0	92.0		
east of Burr Oak.)			25			1340.0	752.0	503.0	280.0	213.0	180.0	137.0		
A control of the cont			50		3350.0	1680.0	941.0	651.0	361.0	272.0	232.0	179.0		
			100		4210.0	2050.0		819.0	454.0	338.0	292.0	227.0 ^b		
6 8558 00 Buffalo Creek near	330	1960-80	2	1510.0b	1160.0	727.0	416.0	271.0	168.0	131.0	110.0	84.0ª		
Jamestown			5		2710.0	1610.0	876.0	560.0	343.0	258.0	227.0	174.0		
(Cloud County, 1.1 miles north			10		4360.0		1330.0	835.0	509.0	374.0	335.0	256.0		
of Jamestown.)			25	10800.0			2120.0	1300.0	764.0	561.0	514.0	392.0		
			50	16100.0				1740.0	1040.0	734.0	682.0	519.0		
			100					2270.0		937.0	882.0	671.0b		

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	analy- zed	rence interval (years)	val Maximum average discharge, in cubic feet per second								
	miles)		-	1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 day
36 8559 00 Wolf Creek near Concordia	56	1963-80	2	508.0ª	250.0	131.0	69.0	42.0	25.0	20.0	16.0	12.0 ^b
(Cloud County, at State Highway			5	1000.0	521.0	282.0	152.0	96.0	60.0	47.0	40.0	31.0
9, 3.8 miles southwest of			10	1400.0	745.0	412.0	224.0	145.0	94.0	72.0	63.0	49.0
Concordia.)			25	1980.0	1070.0	606.0	335.0	222.0	149.0	113.0	100.0	78.0
			50	2450.0	1340.0	772.0	431-0	290.0	199.0	150.0	133.0	106.0
			100	2960.0 ^b	1630.0	953.0	539.0	367.0	257.0	192.0	171.0	137.0°
06 8585 00 North Fork Smoky Hill	650	1948-53,	2	95.0 ^b	50.0	26.0	15.0	8.9	5.7	4.3	3.6	2.7b
River near McAllaster		1960-80	5	485.0	236.0	116-0	63.0	38.0	24.0	. 17.0	13.0	8.5
(Logan County, at U.S. Highway			10	1080.0	508.0	251.0	133.0	77.0	48.0	34.0	25.0	16.0
40, 3.0 miles east of			25	2440.0	1120.0	565.0	293.0	162.0	100.0	71.0	52.0	32.0
McAllaster.)			50	4050.0	1830.0	950.0	486.0	258.0	160.0	113.0	82.0	52.0
			100	6300.0 ^C	2830.0	1510.0	703.0	388.0	242.0	172.0	127.0	80.0 ^C
		1966-80	2	47.0b	25.0	13.0	7.0	4.0	2.6	1.9	1.7	1.4b
			5	192.0	93.0	43.0	23.0	14.0	9.3	6.4	5.1	3.4
			10	371.0	176.0	80.0	42.0	26.0	18.0	12.0	8.8	5.2
			25	712.0	334.0	150.0	76.0	47.0	34.0	23.0	15.0	8.0
			50	1050.0	495.0	224.0	111.0	69.0	51.0	34.0	22.0	11.0
			100	1470.0°	695.0	318.0	155.0	96.0	74.0	48.0	30.0	14.0°
06 8595 00 Ladder Creek below Chalk	1,460	1952-79	2	157.0b	93.0	52.0	29.0	19.0	13.0	10.0	8.9	7.4ª
Creek near Scott City			5	604.0	328.0	173.0	94.0	57.0	35.0	28.0	23.0	18.0
(Logan County, 5.0 miles down-			10	1250.0	645.0	332.0	189.0	105.0	63.0	49.0	40.0	29.0
stream from Chalk Creek and			25	2760.0	1350.0	684.0	418.0	210.0	123.0	95.0	77.0	54.0
23 miles northeast of Scott			50	4660.0	2180.0	1100.0	720.0	337.0	195.0	151.0	121.0	52.0
City.)			100	7490.0	3380.0	1710.0	1200.0	525.0	301.0	234.0	185.0	123.0b
		1966-80	2	102.0b	54.0	30.0	17.0	11.0	7.4	6.0	5.2	4.6b
			5	447.0	219.0	111.0	56.0	32.0	19.0	14.0	12.0	10.0
			10	1090.0	515.0	249.0	121.0	65.0	36.0	26.0	21.0	16.0
			25	3120.0	1410.0	655.0	306.0	157.0	80.0	56.0	44.0	31.0
			50	6470.0	2840.0	1290.0	597.0	298.0	146.0	99.0	74.0	50.0
			100	13000.0°	5530.0	2480.0	1130.0	555.0	260.0	174.0	125.0	80.0b
06 8600 00 Smoky Hill River at	3,390	1940-80	2	689.0b	407.0	225.0	128.0	77.0	48.0	35.0	27.0	23.0b
Elkader			5	2650.0	1560.0	847.6	483.0	283.0	172.0	125.0	94.0	73.0
(Logan County, at U.S. Highway			10	5270.0	3130.0	1700.0	987.0	578.0	352.0	267.0	210.0	139.0
83 at Elkader, 0.1 mile down-			25	10800.0	6530.0	3590.0	2150.0	1270.0	786.0	647.0	551.0	291.0
stream from Ladder Creek.)			50	17100.0	10500.0	5830.0	3580.0	2150.0	1350.0	1190.0	1100.0	479.0
			100	25600.0°	16000.0	9030.0	5700.0	3480.0	2220.0	2130.0	2130.0	762.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	analy- zed	Recur- rence interval (years)										
	miles)		,	1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 da	ys 183 days	
(06 8600 00)Continued		1966-80	2	353.0 ^b	177.0	91.5	50.5	29.6	17.9	14.1	11.7	8.8 ^b	
			5	1060.0	521.0	260.0	135.0	75.8	42.5	31.7	25.1	18.1	
			10	1900.0	928.0	461.C	234.0	130.0	70.4	50.8	39.4	27.8	
			25	3530.0	1740.0	872.0	435.0	239.0	126.0	87.4	66.5	46.0	
			50	5280.0	2620.0	1330.0	660.0	361.0	187.0	127.0	95.3	65.3	
			100	7600.0C	3810.0	1970.0	971.0	532.0	272.0	180.0	134.0	90.8b	
06 8610 00 Smoky Hill River near	5,220	1951-80	2	1510.0b	858.0	454.0	251.0	148.0	90.5	71.7	59.5	43.6b	
Arnold			5	4520.0	2630.0	1420.0	809.0	503.0	308.0	238.0	193.0	136.0	
(Trego County, 12 miles north			10	7650.0	4000.0	2540.0	1490.0	974.0	604.0	460.0	367.0	258.0	
of Arnold.)			25	13000.0	5190.0	4700.0	2861.0	2000.0	1270.0	952.0	746.0	532.0	
			50	17900.0	11800.0	6970.0	4360.0	3210.0	2090.0	1540.0	1200.0	865.0	
			100	23600.0C	16200.0	9900.0	6360.0	4940.0	3290.0	2410.0	1840.0	1360.0b	
		1966-80	2	1010.0b	539.0	273.0	148.0	83.0	51.0	40.0	33.0	24.0 ^b	
			5	2790.0	1390.0	694.0	383.0	220.0	127.0	97.0	77.0	54.0	
			10	4550.0	2210.0	1110.0	619.0	363.0	202.0	151.0	120.0	82.0	
			25	7470.0	3540.0	1810.0	1020.0	616.0	329.0	238.0	190.0	129.0	
			50	10100.0	4760.0	2460.0	1400.0	862.0	450.0	319.0	254.0	174.0	
			100	13200.0 ^C	6160.0	3230.0	1860.0	1170.0	594.0	412.0	328.0	227.0b	
06 8633 00 Big Creek near Ogallah	297	1956-68	2	720.0b	440.0	221.0	122.0	70.0	42.0	31.0	26.0	20.00	
(Trego County, at State Highway			5	2550.0	1530.0	737.0	404.0	227.0	128.0	95.0	77.0	57.0	
147, 5 miles south of Ogallah,			10	4590.0	2720.0	1310.0	727.0	410.0	233.0	173.0	138.0	102.0	
9.0 miles upstream from Ogallah			25	8140.0	4770.0	2310.0	1320.0	760.0	441.0	332.0	257.0	194.0	
Creek, and 10 miles west of			50	11500-0	6670.0	3260.0	1920.0	1120.0	669.0	508.0	388.0	298.0	
Ellis.)			100	15300.0°	8850.0	4370-0	2650.0	1580.0	976-0	748.0	563.0	442.0C	
06 8635 00 Big Creek near Hays	594	1947-80	2	1060.0ª	612.0	336.0	183.0	114.0	71.7	55.2	46.6	35.9ª	
(Ellis County, 0.6 mile east of			5	2540.0	1570.0	857.0	478.0	302.0	192.0	143.0	116.0	86.1	
Munjor, and 6.0 miles southeast			10	3940.0	2570.0	1420.0	824.0	524.0	336.0	245.0	194.0	142.0	
of Hays.)			25	6200.0	4350.0	2450.0	1520.0	979.0	630.0	450.0	349.0	249.0	
			50	825C.0	6100.0	3500.0	2300.0	1490.0	963.0	679.0	519.0	364.0	
			100	10600.0b	8270.0	4850.0	3370.0	2220.0	1430.0	996.0	751.0	519.0 ^b	
		1966-80	2	831.0 ^b	469.0	255.0	139.0	63.0	53.0	42.0	36.0	28.0ª	
			5	1690.0	970.0	497.0	256.0	151.0	99.0	77.0	61.0	47.0	
			10	2330.0	1360.0	662.0	345.0	207.0	139.0	106.0	83.0	63.0	
			25	3170.0	1890.0	897.0	469.0	288.0	200.0	151.0	115.0	37.0	
			50	3810.0	2310.0	1080.0	568.0	357.0	254.0	191.0	143.0	108.0	
			100	4430.0b	2720.0	1260.0	671.0	432.0	316.0	236.0	174.0	131.0b	

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	analy- zed	Recur- rence interval (years)		Maxim				ic feet per			
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 day	s 183 days
06 8639 00 North Fork Big Creek near	54	1963-80	2	129.0 ^b		33.0	17.0	9.0	4.7	3.5	2.8	1.9b
(Ellis County, 3.5 miles north-			10	652.0	310.0 675.0	144.0 312.0	166.0	91.0	51.0	36.0	28.0	20.0
west of Victoria.)			25	3730.0	1530.0	710.0	396.0	220.0	127.0	87.0	66.0	49.0
west of victorial)			50	6660.0	2570.0	1210.0	697.0	392.0	234.0	156.0	118.0	88.0
			100	11200.0°		1950.0	1170.0	604.0	407.0	267.0	200.0	152.0
		1966-80	2	104.0°	57.0	28.0	14.0	7.6	4.1	2.9	2.3	1.5 b
			5	537.0	271.0	125.0	63.0	34.0	19.0	13.0	10.0	7.2
			10	1270.0	607.0	275.0	141.0	77.0	44.0	30.0	23.0	17.0
			25	3210.0	1430.0	638.0	337.0	187.0	109.0	75.0	57.0	43.C
			50	5830.0	2480.0	1100.0	597.0	336.0	201.0	138.0	104.0	81.0
			100	9990.0°	4060.0	1810.0	1010.0	573.0	353.0	242.0	181.0	144.0°
6 8669 00 Saline River near Wakeene	y 696	1956-66	2	1700.0b	945.0	475.0	245.0	142.0	92.0	71.0	61.0	45.0b
(Trego County, at U.S. Highway			5	4980.0	2480.0	1250.0	682.0	385.0	243.0	187.0	153.0	106.0
283, 1 mile upstream from Trego			10	8370.0	3920.0	1980.0	1120.0	635.0	402.0	307.0	245.0	167.0
Creek and 5 miles north of			25	14100.0	6140.0	3130-0	1860.0	1060.0	684.0	522.0	404.0	272.0
Wa Keeney).			100	19500.0°		5260.0	2530.0 3320.0	1960.0	1300.0	734.0	738.0	374.0 499.0°
06 8670 00 Saline River near Russell	1.502	1946-53,	2	2090.08	1320.0	761.0	457.0	298.0	194.G	153.0	133.0	106.Cª
(Russell County, at U.S. Highway	2,502	1960-80	5	4650.0	3010.0	1780.0	1070.0	711.0	458.0	354.0	301.0	228.0
281, 2.0 miles downstream from			10	6730.0	4460.0	2750.0	1680.0	1140.0	744.0	572.0	480.0	354.0
Salt Creek and 5.0 miles north			25	9680.0	6600.0		2750.0	1920.0	1290.0	982.0	815.0	586.0
of Russell.)			50	12000.0	8380.0	5740.0	3780.0	2710.0	1560.0	1420.0	1170.0	825.0
			100	1440u.0b	16300.0	7390.0	5060.0	3710.0	2630.0	2000.0	1640.0	1140.0b
		1966-80	2	1510.0b	900.0	506.0	309.0	191.0	128.0	103.0	92.0	74.0ª
			5	3230.0	1880.0	1000.0	593.0	368.0	237.0	189.0	164.0	129.0
			10	4550.0	2620.0	1370.0	415.0	514.0	331.0	264.0	225.0	175.0
			25	6300.0	3610.0	1860.0	1120.0	729.0	478.0	383.0	321.0	246.0
			50	7510.0	4350.0	2230.0	1370.0	910.0	609.0	491.0	408.0	309.0
			100	8910.0°	5080.0	2600.0	1630.0	1110.0	760.0	618.0	507.0	382.0b
06 8675 00 Paradise Creek near	212	1947-53,	2	530.0b	291.0	145.0	82.0	52.0	31.0	23.0	20.0	14.0b
Paradise		1963-74	5	1900.0	979.0	481.0	286.0	190.0	119.0	89.0	75.0	54.0
(Russell County, at U.S. Highway			10	3500.0	1770.0	869.0	529.0	359.0	230.0	173.0	146.0	104.0
281, 4.5 miles southeast of Para-			25	6480.0	3240.0	1590.0	989.0	692.0	456.0	342.0	291.0	208.0
dise.)			50	9450.0	4700.0	2320.0	1460.0	1040.0	699.0	525.0	447.0	322.0
			100	13100.0°	6520.0	3220.0	2040.0	1490.0	1020.0	764.0	653.0	474.0°

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

	buting- drain- age area (square	zed	rence interval (years)		Maxir	-	-	e, in cubi				
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	s 183 days
06 8684 00 Wolf Creek near Lucas	163	1960-71	2	737.0 ^C	337.0	155.0	87.0	50.0	31.0	23.0	19.0	14.0 ^b
(Russell County, 1.2 miles west			5	2920.0	1230.0	550.0	277.0	151.0	98.0	70.0	57.0	40.0
of Lucas and 4.0 miles upstream			10	5200.0	2230.0	995.0	487.0	266.0	178.0	127.0	102.0	71.0
from East Fork.)			25	9350.0	3950.0	1790.0	861.0	481.0	334.0	240.0	192.0	132.0
			50	13200.0	5520.0	2540.0	1220.0	700.0	500.C	361.0	290.0	200.0
			100	17600.0°	7320.0	3430.0	1660.0	977.0	718.0	524.0	423.0	292.0°
6 8703 00 Gypsum Creek near Gypsum	120	1955-71	2	1130.0b	605.0	325.0	185.0	119.0	74.0	57.0	49.0	38.0b
(Saline County, 2.6 miles upstream	n		5	2500.0	1310.0	731.0	408.0	262.0	164.0	126.0	110.0	84.0
from Stag Creek and 3.5 miles sout	th		10	3340.0	1740.0	978.0	540.0	353.0	219.0	170.0	149.0	111.0
of Gypsum.)			25	4220.0	2160.0	1230.0	669.0	449.0	275.0	215.0	191.0	139.0
			50	4720.0	2390.0	1370.0	740.0	506.0	308.0	242.0	215.0	154.0
			100	5110.0C	2570.0	1480.0	793.0	552.0	333.0	263.0	235.0	166.0°
6 8710 00 North Fork Solomon River	849	1953-80	2	973.0b	507.0	272.0	157.0	104.0	70.C	55.0	49.0	39.0ª
at Glade			5	2810.0	1420.0	729.0	394.0	249.0	159.0	121.0	103.0	77.0
at Glade (Phillips County, at U.S. High-			10	4660.0	2390.0	1220.0	650.0	402.0	251.0	187.0	156.0	112.0
way 183, 0.5 mile south of			25	7710.0	4070.0	2130.0	1120.0	685.0	417.0	303.0	246.0	170.0
Glade.)			50	10500.0	5690.0	3050.0	1610.0	976.0	586.0	418.0	332.0	223.0
			100	13600.0°	7640.0	4220.0	2230-0	1350.0	802.0	563.0	437.0	287.0b
		1966-80	2	539.0b	306.0	174.0	107.0	71.0	51.0	41.0	36.0	30.0ª
			5	1780.0	926.0	497.0	272.0	168.0	110.0	85.0	72.0	57.0
			10	3280.0	1640.0	876.0	457.0	273.0	170.0	128.0	107.0	82.0
			25	6200.0	3020.0	1630.G	814.0	470.0	278.0	205.0	165.0	124.0
			50	9280.0	4460.0	2440.0	1200.0	679.0	388.0	282.0	221.0	163.0
			100	13300.0b	6340.0	3540.C	1710.0	956.0	529.0	380.0	290.0	209.0b
5 8715 00 Bow Creek near Stockton	341	1952-80	2	470.0b	257.0	136.0	74.0	47.0	31.0	24.0	21.0	18.0ª
(Rooks County, at U.S. Highway			5	1240.0	666.0	340.0	178.0	111.0	70.0	52.0	44.0	33.0
183, 8.5 miles north of Stock-			10	1960.0	1080.0	554.0	289.0	181.0	112.0	80.0	65.0	48.0
ton.)			25	3110.0	1790.0	938.0	495.0	312.0	189.0	132.0	103.0	72.0
			50	4110.0	2460.0	1320.0	708.0	450.0	268.0	184.0	140.0	94.0
			100	5230.0b	3260.0	1810.0	984.0	631.0	371.0	251.0	136.0	122.0b
		1966-80	2	418.0b	231.0	121.0	66.0	39.0	25.0	20.0	19.0	16.0ª
			5	1420.0	702.0	344.0	171.0	95.0	57.0	43.0	37.0	29.0
			10	2580.0	1230.0	596.0	290.0	157.0	90.0	65.0	54.0	41.C
			25	4710.0			518.0	279.0	150.0	105.0	84.0	61.0
			50			1580.0	763.0	411.0	213.0	145.0	113.0	81.0
			100			2230.0	1090.0	589.0	296.0	197.0	149.0	104.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	analy- zed	Recurrence interval (years)		Maxir	num average for ind			ic feet per			
	miles)			l day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 days
06 8719 00 Deer Creek near	65	1967-80	2	277.0 ^b	125.0	59.0	30.0	17.0	10.0	7.8	6.5	5.4 ^b
Phillipsburg			5	885.0	352.0	155.0	70.0	39.0	23.6	17.0	14.0	11.0
(Phillips County, 5 miles west			10	1580.0	580.0	248.0	121.0	61.0	36.0	25.0	20.0	17.0
of Phillipsburg.)			25	2850.0	956.0	400.0	199.0	97.0	57.0	39.0	30.0	26.0
			50	4140.0	1300.0	537.0	271.0	132.0	78.0	53.0	40.0	34.0
			100	5730.0°	1690.0	694.0	358.0	175.0	103.0	69.0	51.0	44.0 ^b
06 8730 00 South Fork Solomon River	1,040	1946-80	2	1740.0b	836.0	479.0	272.0	175.0	115.0	91.2	79.4	62.3ª
above Webster Reservoir			5	5450.0	2720.0	1440.0	778.0	503.0	318.0	241.0	200.0	148.0
(Rooks County, 4 miles north of			10	10000.0	5620.0	2640.C	1400.0	921.0	573.0	423.0	342.0	246.0
Damar, 7 miles downstream from			25	19400.0	9860.0	5170.0	2710.0	1830.0	1120.0	807.0	634.0	441.0
Wild Horse Creek, and 11 miles			50	29800.0	15400.0	8090.0	4220.0	2920.0	1780.0	1250.0	966.0	659.0
upstream from Webster Dam.)			100	44000.0b	23300.0	12200.0	6350.0	4520.0	2730.0	1900.0	1440.0	960.0b
		1966-80	2	857.0b	449.0	234.0	132.0	87.0	59.0	49.0	43.0	35.0ª
			5	2340.0	1160.0	598.0	315.0	190.0	117.0	90.0	77.0	60.0
			10	4080.0	1980.0	1020.0	524.0	300.0	176.0	131.0	110.0	82.0
			25	7540.0	3600.0	1890.0	938.0	510.0	283.0	200.0	164.0	120.0
			50	11400.0	5380.0	2860.0	1400.0	734.0	392.0	269.0	217.0	156.0
			100	16500.0°	7800.0	4210.0	2030.0	1030.0	535.0	357.0	284.0	199.0b
06 8737 00 Kill Creek near Blooming-	- 52	1964-80	2	59.0°	31.0	14.0	10.0	5.7	3.3	2.5	2.3	1.8b
ton			5	314.0	147.0	63.C	33.0	18.0	11.0	7.8	6.6	5.0
(Osborne County, 9.0 miles south-			10	697.0	305.0	143.0	60.0	33.0	20.0	14.0	12.0	8.9
west of Bloomington.)			25	1530.0	623.0	347.0	109.0	61.0	39.0	28.0	23.0	16.0
			50	2500.0	967.0	529.0	162.0	91.0	61.0	44.0	36.0	25.0
			100	3850.0°	1420.0	1100.0	232.0	134.0	94.0	67.0	55.0	38.0C
		1966-80	2	69.0°	35.0	19.0	11.0	6.3	3.6	2.7	2.3	1.7b
			5	342.0	163.0	72.0	35.0	20.0	12.0	8.6	7.0	5.4
			10	739.0	335.0	139.0	63.0	35.0	23.0	16.0	13.0	10.0
			25	1590.0	672.0	266.0	114.0	65.0	44.0	32.0	25.0	18.0
			50	2560.0	1030.0	402.C	168.0	98.0	69.0	50.0	40.0	28.0
			100	3910.¢	1500.0	578.0	243.0	144.0	106.0	76.0	62.0	43.0°
06 8767 00 Salt Creek near Ada	384	1960-80	2	1200.0b	844.0	544.0	294.0	178.0	109.0	86.0	71.0	55.0b
(Ottawa County, 3 miles south-			5	380.0	3040.0	1820.0	1000.0	589.0	345.0	260.0	210.0	158.0
east of Ada.)			10	6750.0	5900.0	3210.0	1820.0	1070.0	611.0	450.0	361.0	269.0
			25	11700.0	11900.0	5650.0	3330.0	1950.0	1100.0	791.0	634.0	470.0
			50	16300.0	13600.0	7950.0	4830.0	2840.0	1600.0	1130.0	902.0	570.0
			100	21600.00	27900.0	10600.0	6680.0	3950.0	2210.0	1530.0	1230.0	917.0C

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

	Contri- buting- drain- age area	Records analy- zed	rence interval (years)		Maxi			ge, in cubi				
	(square miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 day	s 183 days
06 8780 00 Chapman Creek near Chapman	n 300	1955-80	2	3010.0ª	2000.0	1070.0	616.0	387.0	232.0	182.0	155.0	122.0ª
(Dickinson County, at State			5	5620.0	3910.0	2080.0	1160.0	721.0	426.0	335.0	286.0	221.0
Highway 18, 5.0 miles northwest			10	7630.0	5400.0	2830.0	1540.0	954.0	559.0	438.0	375.0	285.0
of Chapman.)			25	10400.0	7490.0	3820.0	2030-0	1250.0	722.0	560.0	482.0	361.0
			50	12600.0	9140.0	4580.0		1460.0	837.0	645.0	557.0	411.0
			100	14900.0b	10900.0	5330.0	2710.0	1660.0	946-0	722.0	628.0	457.0b
06 8785 00 Lyon Creek near Woodbine	230	1955-74	2	4770.0b	2510.0	1340.0	607.0	473.0	296.0	235.0	199.0	150.0b
(Geary County, 2.0 miles down-			5	10600.0	5380.0	2740.0	1520.0	974.0	593.G	464.0	386.0	286.0
stream from Cary Creek and 7.0			10	14500.0	7170.0	3550.0	2460.0	1270.0	767.0	596.0	494.0	363.0
miles north of Woodbine.)			25	18800.0	9070.0	4350.0	4120.0	1570.0	942.0	728.0	602.0	439.0
			50	21500.0	10200.0	4800.0	5730.0	1740.0	1040.0	803.0	663.0	481.0
			100	23800.0°	11100.0	5140.0	7720.0	1870.0	1120.0	860.0	712.0	513.0 ^b
06 8825 00 Big Blue River at Hull	4,540	1920-24,	2	7060.0a	5290.0	3520.0	2200.0	1490.0	1060.0	881.0	777.0	655.0a
(Marshall County, a quarter of a	.,	1929-40	5	11700.0	8670.0	6060.0	3850.0	2480.0	1760.0	1420.0	1230.0	969.0
mile west of Hull and 2 miles up-		2323 10	10	14600.0	11200.0	7870.0	5040.0	3180.0	2220.0	1760.0	1510.0	1150.0
stream from Deer Creek.)			25	17800.0	14100.0	10200.0	6610.0	4100.0	2780.0	2150.0	1840.0	1350.0
Stream from beer dicer.			50	20000.0	16100.0	12000.0	7810.0	4790.0	3180.0	2420.0	2060.0	1470.0
			100	21900.0b	17900.0	13700.0	9020.0	5500.0	3550.0	2660.0	2260.0	1580.0b
06 8842 00 Mill Creek at Washington	344	1960-80	2	3650.0ª	2340.0	1270.0	726.0	452.0	257.0	205.0	183.0	144.0a
(Washington County, at U.S. High-	1.7	1300-00	5	6770.0	4560.0	2480.0	1370.0	829.0	515.0	381.0	336.0	263.0
way 36, 0.5 mile east of Washing-			10	8830.0	6100.0	3320.0	1790.0	1070.0	730.0	498.0	436.0	339.0
ton.)			25	11300.0	7990.0	4340.0	2270.0	1330.0	1040.0	637.0	553.0	426.0
con. /			50	12900.0	9310.0	5050.0	2590.0	1510.0	1310.0	732.0	631.0	483.0
			100	14500.0 ⁰	10500.0	5720.0	2880.0	1060.0	1590.0	819.0	701.0	534.0b
06 8845 00 Little Blue River at	3,440	1923-24,	2	10100.0ª	7790.0	5000.0	3280.0	2280.0	1530.0	1220.0	1050.0	844.0ª
Waterville	3,440	1929-57,									1890.0	
(Marshall County, 1 mile down-		1959-80	10								2500.0	
stream from Coon Creek and 0.3		1939-00	25	34700.0	27500.0	18700.0	11600.0	7780.0	4940.0	3920.0	3300.0	2460.0
mile north of Waterville.) In-			50	42200.0	33200.0	22700.0	13900.0	9240.0	5820.0	4650.0	3900.0	2890.0
cludes data from station			100	50000.0b	39200.0	26700.0	16200.0	10700.0	6670.0	5380.0	4510.0	3320.0ª
06884400 for 1959-80.												
06 8855 00 Black Vermillion River	410	1954-80	2	5330.0a	3060.0	1710.0	1040.0	658.0	399.0	313.0	258.0	198.0a
near Frankfort			5	11100.0	6030.0	3250.0	1910.0	1240.0	735.0	571.0	467.0	359.0
(Marshall County, 0.2 mile down-			10	16200.0	8400.0	4380.0	2510.0	1640.0	963.0	743.0	604.0	464.0
stream from Robidoux Creek, and			25	24100.0	11800.0	5880.0	3240.0	2120.0	1240.0	949.0	766.0	586.0
2.2 miles southwest of Frankfort.	.)		50	31000.0	14500.0	7020.0	3760.0	2460.0	1430.0	1090.0	876.0	668.0
			100	38900.0b	17400.0	8150.0	4250.0	2780.0	1620.0	1220.0	977.0	742.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

tation number, name, and location	Contri- buting- drain- age area (square	Records analy- zed	rence interval (years)		Maxim				ic feet per			
9411 Tarin - 1912 (1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 - 1912 -	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 days
06 8865 00 Fancy Creek at Winkler	174	1955-71	2	2040.0b	1040.0	548.0	311.0	194.0	119.0	94.0	78.0	60.0b
(Riley County, 0.2 mile down-			5	5410.0	2730.0	1430.0	806.0	479.0	283.0	219.0	181.0	138.0
stream from Otter Creek, 0.4			10	8320.0	4180.0	2170.0	1220.0	710.0	411.0	315.0	260.0	196.0
mile south of Winkler and 5.0			25	12500.0	6210.0	3190.0	1780.0	1020.0	582.0	438.0	360.0	267.0
miles northwest of Randolph.)			50	15700.0	7790.0	3970.0	2200.0	1250.0	709.0	527.0	432.0	316.0
			100	19000.0°	9370.0	4750.0	2620.0	1480.0	832.0	611.0	500.0	362.0°
06 8880 00 Vermillion Creek near	243	1937-45,	2	3230.0b	1830.0	981.0	628.0	409.C	257.0	201.0	168.0	127.0b
Wamego		1955-71	5	6840.0	3850.0	1960.0	1280.0	838.0	523.0	410.0	340.0	260.0
(Pottawatomie County, 1 mile up-			10	9390.0	5230.0	2590.0	1690.0	1120.0	691.0	544.0	448.0	343.C
stream from Indian Creek and 14			25	12500.0	6840.0	3290.0	2140.0	1440.0	876.0	692.0	566.0	431.0
miles northeast of Wamego.)			50	14600.0	7900.0	3740.0	2420.0	1640.0	990.0	784.0	640.0	483.0
			100	16600.0b	8840.0	4130.0	2650.0	1820.0	1090.0	862.0	701.0	527.Cb
06 8885 00 Mill Creek near Paxico	316	1955-80	2	5320.0a	2560.0	1400.0	948.0	628.0	426.0	340.0	291.0	225.0ª
(Wabaunsee County, at Inter-			5	11000.0	5220.0	2980.0	1820.0	1170.0	759.0	609.0	517.0	399.0
state Highway 70, 1.0 mile			10	15400.0	7300.0	4150.0	2420.0	1510.0	956.0	766.0	649.0	498.0
southwest of Paxico and 2.0 miles			25	21200.0	10200-0	5770.0	3150.0	1890.0	1170.0	932.0	789.0	599.0
downstream from Kuenzli Creek.)			50	25600.0	12400.0	7040.0	3670.0	2130.0	1300.0	1030.0	874.0	658.0
			100	30000.0b	14800.0	8330.0	4140.0	2340.0	1410.0	1110.0	945.0	706.0b
06 8991 00 Soldier Creek near Goff	2.06	1965	-80 2	76.0ª	37.0	21.0	12.0	7.2	4.4	3.1	2.6	1.9ª
(Nemaha County, 3.3 miles south-			5	131.0	62.0	33.0	19.0	12.0	7.2	5.1	4.3	3.0
west of Goff.)			10	172.0	77.0	41.0	24.0	15.0	8.9	6.2	5.2	3.7
27.			25	225.0	96.0	49.0	28.0	18.0	11.0	7.4	6.3	4.4
			50	265.0	109.0	54.0	31.0	20.0	12.0	8.1	7.0	4.8
			100	306.0b	122.0	58.0	33.0	21.0	13.0	8.7	7.5	5.1 b
6 8891 20 Soldier Creek near	10.5	1965	-80 2	308.0ª	156.0	88.0	54.0	34.0	20.0	15.0	12.0	9.1ª
Bancroft			5	478.0	251.0	142.0	90.0	57.0	33.0	25.0	22.0	15.0
(Nemaha County, 4.0 miles west			10	581.0	308.0	174.0	110.0	70.0	41.0	30.0	28.0	19.0
of Bancroft.)			25	696.0	372.0	207.0	131.0	84.0	49.0	36.0	34.0	22.0
			50	772.0	413.0	228.0	143.0	92.0	53.0	39.0	37.0	25.0
			100	839.0 b	450.0	245.0	153.0	98.0	57.0	41.0	40.0	26.0 ^b
06 8891 40 Soldier Creek near	16.9	1965-	-80 2	452.0 a	236.0	131.0	78.0	48.0	29.0	23.0	19.0	14.0ª
Soldier			5	751.0	402.0	226.0	133.0	85.0	49.0	39.0	32.0	23.0
(Jackson County, 2.0 miles north			10	925.0	499.0	281.0	163.0	109.0	63.0	47.0	39.0	27.0
of Soldier.)			25	1110.0	603.0	339.0	193.0	. 138.0	78.0	56.0	46.0	32.0
			50	1220.0	668.0	375.0	211.0	157.0	88.0	02.0	51.0	35.0
			100	1320.0b		405.0	225.0	175.0	98.0	66.0	54.0	37.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

	Contri- buting- drain- age area (square	analy- zed	rence interval (years)		Maxir		e discharg icated per					
	miles)			l day	3 days	7 days	15 days	30 days	60 days	90 days	120 day:	s 183 days
06 8891 60 Soldier Creek near	49.3	1965-80	2	1320.0ª	752.0	398.0	241.0	158.0	98.C	75.0	63.0	46.0ª
Circleville			5	2080.0	1220.0	636.0	368.0	246.0	150.0	117.0	100.0	72.0
(Jackson County, at State High-			10	2490.0	1480.0	769.0	436.0	294.0	178.0	139.0	119.0	86.0
way 16, 5.8 miles southwest of			25	2920.0	1760.0	906.0	503.0	341.0	206.0	161.0	140.0	101.0
Circleville.)			50	3180.0	1940.0	989.0	543.0	369.0	222.0	175.0	152.0	110.0
			100	3400.0b	2080.0	1060.0	575.0	391.0	235.0	185.0	162.0	118.0 ^b
06 8891 80 Soldier Creek near St.	80	1965-80	2	2000.0ª	1070.0	562.0	357.0	237.0	150.0	119.0	101.0	75.0ª
Clere			5	3270.0	1790.0	932.0	572.0	382.0	237.0	188.0	160.0	117.0
(Jackson County, 7.8 miles east			10	4030.0	2260.0	1160.0	699.0	466.0	287.0	229.0	195.0	142.0
of St. Clere.)			25	4670.0	2800.0	1430.0	838.0	558.0	341.0	272.0	232.0	171.0
			50	5400.0	3170.0	1600.0	927.0	615.0	376.0	300.0	256.0	190.0
			100	5880.0b	3510.0	1760.0	1000.0	665.3	406.0	323.0	276.0	207.0 ^b
06 8892 00 Soldier Creek near Delia	157	1959-80	2	3100.0ª	1770.0	956.0	597.0	404.0	256.0	204.0	174.0	131.0ª
(Shawnee County, 5.1 miles upstream	ım		5	4900.0	3080.0	1610.0	962.0	653.0	400.0	317.0	271.0	202.0
from Walnut Creek and 5.5 miles			10	5980.0	3980.0	2040.0	1220.0	801.0	485.0	381.0	329.0	245.0
southwest of Delia.)			25	7210.0	5100.0	2550.0	1500.0	964.0	578.0	449.0	392.0	294.0
			50	8010.0	5900.0	2900.0	1680.0	1070.0	637.0	492.0	432.0	328.0
			100	8740.0b	6680.0	3240.0	1850.0	1160.0	690.0	528.0	468.0	358.0b
06 8895 00 Soldier Creek near Topeka	290	1930-32,	2	4030.0ª	2340.0	1340.0	857.0	562.0	372.0	291.0	247.0	191.0ª
(Shawnee County, 1.5 miles up-		1936,	5	8030.0	5020.0	2810.0	1800.0	1170.0	732.0	573.0	481.0	367.0
stream from Halfday Creek and 4.0		1938-80	10	10900.0	7090.0	3910.0	2470.0	1590.0	972.0	760.0	632.0	478.0
miles northwest of Topeka.)			25	14400.0	9850.0	5320.0	3310.0	2110.0	1250.0	977.0	804.0	600.C
			50	17000.0	11900.0	6350.0	3910.0	2470.0	1440.0	1120.0	916.0	677.0
			100	19400.0b	14000.0	7350.0	4470.0	2800.0	1600.0	1250.0	1010.0	743.0b
06 8901 00 Delaware River near	431	1970-81	2	9310.0b	5070.0	2860.0	1810.0	1160.0	719.0	547.0	449.0	339.0ª
Muscotah			5				3010.0			906.0	750.0	573.0
(Atchison County, 2.0 miles			10				3840.0			1150.0	965.0	740.0
south of Muscotah.)			25				4890.0				1250.0	956.0
			50				5670.0					1120.0
			100				6430.0				1680.0	1280.0b
06 8905 00 Delaware River at Valley	922	1923-67	2	11500 - na	6710-0	3720-0	2360.0	1530-0	999.0	794.0	670.0	508.0ª
Falls			5				4760.0			1560.0		978.0
(Jefferson County, 200 feet down-			10				6540.0		2680.0			1310.0
stream from Walnut Creek, 300			25				8880.0		3600.0			1720.0
feet upstream from Atchison,			50				10600.0					2010.0
Topeka and Santa Fe Railway			100								3020.0	
Co. bridge, a quarter of a				THE REST		30						
o. rage, a quarter or a												

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Tonganoxie	age area (square	zed	interval					e, in cubi		days	120 4-	ys 183 days
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 da,	ys 103 days
6 8920 00 Stranger Creek near	406	1930-80	2	4930.0ª	3630.0	2150.0	1320.0	869.0	577.0	459.0	393.0	303.0ª
Tonganoxie			5	8740.0	6820.0	4160.0	2500.0	1660.0	1060.0	849.0	719.0	551.C
(Leavenworth County, at U.S.			10	11300.0	9030.0		3300.0	2220.0	1380.0	1100.0	924.0	708.0
Highway 40, 2.0 miles upstream			25	14500.0		7310.0	4250.0	2930.0	1740.0	1390.0	1150.0	0.688
from Tonganoxie Creek and 4.0			50	16700.0		8550.0	4910.0	3430.0		1570.0	1300.0	1000.0
miles east of Tonganoxie.)			100	18800.0b	15600.0	9710.0	5510.0	3920.0	2190.0	1740.0	1430.0	1100.0b
6 8933 00 Indian Creek at Overland	26.6	1964-80	2	1080.0ª	525.0	270.0	153.0	97.0	63.0	49.0	41.0	34.0ª
Park			5	1580.0	794.0	423.0	246.0	160.0	98.0	74.0	62.0	49.0
(Johnson County, at Marty			10	1900.0	966.0	538.0	311.0	205.0	121.0	92.0	76.0	58.0
Street in Overland Park.)			25	2280.0	1170.0	682.0	394.0	262.0	149.0	113.0	92.0	68.0
			50	2550.0	1320.0	791.0	457.0	306.0	170.0	128.0	104.0	75.0
			100	2810.0b	1460.0	901.0	519.0	350.0	191.0	144.0	115.0	81.0 ^b
6 9108 00 Marais des Cygnes River	177	1970-81	2	4180.0ª	2010.0	1130.0	702.0	443.0	288.0	224.0	184.0	144.0ª
near Reading			5	6710.0	3530.0	1950.0	1120.0	678.0	433.0	342.0	291.0	222.0
(Lyon County, 1.9 miles downstream	m		10	8610.0	4760.0	2610.0	1440.0	846.0	535.0	424.0	308.0	275.0
from confluence of One Hundred and	d		25	11300.0	6580.0	3580.0	1690.0	1070.0	669.0	532.0	470.0	341.0
Forty-two Mile Creek and Elm Creek	k,		50	13400.0	8140.0	4410.0	2250.0	1240.0	773.0	615.0	549.0	389.0
4.3 miles upstream from Duck Creek and 3.0 miles north of Reading.)	k		100	15700.0b	9860.0	5320.0	2630.0	1420.0	880.0	699.0	630.0	438.0 ^b
6 9115 00 Salt Creek near Lyndon	111	1940-80	2	2400.0ª	1250.0	782.0	394.0	247.0	142.0	120.0	98.0	76.0b
(Osage County, 2.5 miles east of	111	1940-00	5	5450.0	2870.0	1410.0	911.0	592.0	374.0	293.0	242.0	183.0
Lyndon.)			10	7600.0	4000.0	1640.0	1260.0	829.0	580.0	413.0	344.0	257.0
Lymoon. /			25	10100.0	5340.0	1780.0	1660.0	1100.0	880.0	551.0	464.0	341.0
			50	11800.0	6230.0	1830.0	1900-0	1260.0	1120.0	639.0	542.0	394.0
			100	13300.0 ^b		1860.0	2110.0	1410.0	1380.0	713.0	609.0	439.0 ^b
06 9119 00 Dragoon Creek near	114	1961-80	2	3060.0ª	1400.0	749.0	462.0	299.0	189.0	149.0	124.0	94.0ª
Burlingame			5	5400.0	2400.0	1280.0	751.0	476.0	303.0	243.0	205.0	155.0
(Osage County, 0.2 mile down-			10	7120.0	3110.0	1670.0	945.0	588.0	375.0	303.0	258.0	193.0
stream from U.S. Highway 56, 2.0			25	9400.0	4010.0	2190.0	1190.0	720.0	458.0	374.0	322.0	238.0
miles downstream from Plum Creek	,		50	11200.0	4680.0	2590.0	1360.0	810.0	515.0	422.0	368.0	269.0
and 3.0 miles south of Burlingame	e.)		100	13000.0 ^b	5340.0	2990.0	1530.0	894.0	567.0	468.0	410.0	298.0 ^b
06 9140 00 Pottawatomie Creek near	334	1940-80	2	7790.0	4680.0	2480.0	1440.0	908.0	577.0	442.0	375.0	295.0ª
Garnett			5	13900.0	8360.0	4430.0	2560.0	1630.0	1020.0	794.0	666.0	534.0
(Anderson County, at Highway 59,			10	18700.0	11200.0	5850.0	3380.0	2150.0	1320.0	1040.0	804.0	695.0
0.6 mile downstream from conflu-			25	25500.0	15100.0	7750.0	4470.0	2830.0	1710.0	1360.0	1110.0	858.0
ence of North Pottawatomie and			50	31000.0	18200.0	9210.0	5320.0	3330.0	1990.0	1590.0	1280.0	1020.0
Cedar Creeks, 0.2 mile upstream			100	36900.0 ^b	21500.0	10700.0	6180.0	3830.0	2260.0	1810.0	1440.0	1150.0b
from Atchison, Topeka and Santa Fe Railway Co., bridge, 4.0 mile	es											

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area	Records analy- zed	Recur- rence interval (years)		Maxi	mum averag for ind		e, in cub				
	(square miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 day	s 183 days
06 9165 00 Big Sugar Creek at	198	1930-31,	2	4250.0a	2300.0	1240.0	743.0	471.0	296.0	231.0	205.0	161.0ª
Farlinville		1950-70	5	8060.0	4440.0	2330.0	1420.0	910.0	588.C	484.0	416.0	329.0
(Linn County, at State Highway			10	11300.0	6270.0	3200.0	1990.0	1290.0	854.0	719.0	590.0	465.0
7 at Farlinville, 5.2 miles up-			25	16300.0	9080.0	4670.0	2870.0	1870.0	1290.0	1100.0	846.0	659.0
stream from Richland Creek and 14	.0		50	20600.0	11500.0	5890.0	3630.0	2380.0	1690.0	1460.0	1060.0	816.0
miles upstream from Little Sugar Creek.)			100	25500.0b	14300.0	7280.0	4480.0	2960.0	2160.0	1880.0	1290.0	983.0 ^b
06 9170 00 Little Osage River at	295	1950-80	2	6530.Qa	4160.0	2370.0	1410.0	860.0	560.0	438.0	367.0	281.0ª
Fulton			5	11500.0	7600.0	4270.0	2540.0	1580.0	1030.0	840.0	713.0	554.0
(Bourbon County, at U.S. Highway			10	14000.0	9470.0	5300.0	3180.0	2020.0	1310.0	1100.0	935.0	730.0
69, 0.8 mile north of Fulton.)			25	16300.0	11300.0	6280.0	3820.0	2500.0	1610.0	1390.0	1180.0	929.0
			50	17500.0	12200.0	6830.0	4190.0	2800.0	1800.0	1580.0	1350.0	1060.0
			100	18300.0b	13000.0	7250.0	4490.0	3060.0	1950.0	1740.0	1490.0	1170.0b
06 9175 00 Marmaton River near Fort	408	1922-24,	2	9410.0°	5980.0	3380.0	1980.0	1250.0	799.0	628.0	517.0	404.0ª
Scott		1930-71	5	16900.0	11200.0	6420.0	3820.0	2470.0	1520.0	1170.0	963.0	751.0
(Bourbon County, 0.6 mile down-			10	21200.0	14300.0	8310.0	5040.0	3320.0	2000.0	1530.0	1260.0	976.0
stream from Wolverine Creek and 1			25	25500.0	17600.0	10400.0	6470.0	4390.0	2580.0	1960.0	1600.0	1230.0
mile north of Fort Scott.)			50	0.00185	19600.0	11700.0	7440.0	5140.0	2980.0	2250.0	1830.0	1400.0
			100	30100.0 ^b	21300.0	12800.0	8310.0	5850.0	3350.0	2520.0	2040.0	1550.0b
07 1386 50 Whitewoman Creek near	750	1967-81	2	79.0 ^C	32.0	15.0	8.3	4.9	2.8	2.2	1.6	1 . 2 ^b
Leoti			5	356.0	139.0	59.0	32.0	18.0	10.0	7.0	5.2	3.6
(Wichita County, at State Highway			10	743.0	285.0	120.0	62.0	34.0	18.0	13.0	9.1	6.0
96, 7 miles west of Leoti.)			25	1570.0	591.0	252.0	116.0	65.0	32.0	55.0	16.0	10.0
			50	2490.0	929.0	403.0	173.0	100.0	48.0	32.0	23.0	14.0
			100	3730.0 ^C	1380.0	611.0	251.0	151.0	69.0	45.0	32.0	19.0°
07 1398 00 Mulberry Creek near Dodge	73.8	1969-81	2	108.0 ^C	50.0	23.0	13.0	7.0	3.8	2.7	2.4	1.4 ^b
City			5	417.0	168.0	63.0	32.0	17.0	8.9	6.0	5.0	3.1
(Ford County, near U.S. Highway			10	769.0	293.0	108.0	51.0	26.0	14.0	9.2	7.6	4.9
283, 9 miles south of Dodge City.)		25	1380.0	501.0	192.0	83.0	42.0	23.0	15.0	12.0	8.0
			50	1940.0	690.0	280.0	115.0	59.0	32.0	20.0	17.0	11.0
			100	2580.0°	901.0	399.0	156.0	80.0	44.0	27.0	22.0	16.0°

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

tation number, name, and location	Contri- buting- drain- age area (square	Records analy- zed	rence interval (years)		Maxim				c feet per secutive o			
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	183 days
7 1407 00 Guzzlers Gulch near	58.2	1962-80	2	178.0b	81.0	40.0	20.0	12.0	6.5	4.6	3.6	2.3b
Ness City			5	608.0	290.0	148.0	72.0	32.0	17.0	12.0	9.1	5.8
(Ness County, 11 miles south-			10	1040.0	508.0	265.C	131.0	54.0	28.0	19.0	15.0	10.0
west of Ness City.)			25	1720.0	855.0	459.0	234.0	92.0	49.0	33.0	25.0	17.0
			50	2290.0	1150.0	631.0	331.0	130.0	69.0	47.0	35.0	24.0
			100	2880.0°	1470.0	820.0	444.0	179.0	96.C	64.0	48.0	33.0b
**												
		1966-80	2	140.0b	65.0	32.0	16.0	10.0	5.3	3.7	2.9	1.9b
			5	551.0	268.0	139.0	69.0	30.0	16.0	11.0	8.0	5.1
			10	1020.0	507.0	273.0	137.0	54.0	29.0	19.0	14.0	9.0
			25	1840.0	930.0	523.0	269.0	102.0	54.0	35.0	26.0	17.0
			50	2600.0	1320.0	769.0	404.0	156.0	83.0	54.0	39.0	26.0
			100	3460.0°	1770.0	1060.0	572.0	232.0	124.0	80.0	57.0	38.0°
7 1412 00 Pawnee River near Larned	2,010	1925-80	2	2150.0a	1630.0	908.0	502.0	306.0	180.0	132.0	106.0	75.Cª
(Pawnee County, 0.8 mile north of			5	4500.0	3680.0	2110.0	1200.0	740.0	452.0	326.0	257.0	179.0
U.S. Highway 156 and 14 miles			10	6750.0	5620.0	3290.0	1890.0	1210.0	750.0	534.0	418.0	289.0
west of Larned.)			25	10500.0	8820.0	5280.0	3080.0	2050.0	1310.0	921.0	715.0	490.0
			50	14100.0	11800.0	7180.0	4220.0	2910.0	1910.0	1320.0	1020.0	696.0
			100	18500.0b	15300.0	9470.0	5610.0	4010.0	2690.0	1850.0	1420.0	960.0b
		1966-80	2	1820.0ª	1420.0	769.0	401.0	240.0	134.0	95.0	75.0	52.0 ^b
			5	3510.0	2910.0	1610.0	689.0	519.0	291.0	204.0	157.0	110.0
			10	5040.0	4240.0	2370.0	1360.0	778.0	436.0	303.0	231.0	162.0
			25	7550.0	6310.0	3580.0	2150.0	1200.0	671.0	462.0	349.0	245.0
			50	9900.0	8170.0	4590.0	2900.0	1590.0	587.0	607.0	456.0	320.0
			100	12700.0b		5970.0	3800.0	2040.0	1140.0	776.0	590.0	406.0b
07 1417 80 Walnut Creek near	1,152	1970-81	2	1170.0b	798.0	406.0	221.0	120.0	67.0	52.0	41.0	30.0b
Rush Center			5		1680.0	858.0	475.0	253.0	143.0	106.0	84.0	64.0
(Rush County, at State High-			10		2380.0		692.0	371.0	211.0	154.0	121.0	96.0
way 96, 3.0 miles west of			25			1770.0		558.0	322.0	228.0	176.0	147.0
Rush Center.)			50			2210.0		725.0	422.0	293.0	225.0	193.0
Nusir Geneer.			100			2670.0		916.0	539.G	366.0	279.0	247.0°
07 1419 00 Walnut Creek at Albert	1,306	1959-80	2	1750.0a	1430.0	834.0	463.0	261.0	158.0	114.0	94.0	67.0b
(Barton County, 0.2 mile north			5			1830.0		582.0	363.0	262.0	211.0	151.0
of Albert and 14 miles northwest			10			2670.0		871.0	555.0	408.0	319.0	230.0
of Great Bend.)			25				2220.0		867.0	657.0	497.0	360.0
or dreat bend.)			50			4950.0		1730.0	1150.0	898.0	660.0	481.0

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

	Contri- buting- drain- age area		Recur- rence interval (years)		Maxin				ic feet per			
	(square miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	s 183 day
(07 1419 00)Continued		1966-80	2	1620.0ª	1340.0	752.0	419.0	226.0	129.0	95.0	76.0	54.0 b
			5	2750.0	2320.0	1380.0	825.0	476.0	287.0	207.0	163.0	119.0
			10	3500.0	2970.0	1830.0	1140.0	697.0	437.0	310.0	244.0	182.0
			25	4440.0	3760.0	2400.0	1570.0	1040.0	631.0	477.0	378.0	286.0
			50	5120.0	4320.0	2820.0	1910.0	1340.0	908.0	631.0	503.0	386.0
			100	5770.0b	4840.0	3240.0	2260.0	1690.0	1180.0	810.0	652.0	505.0b
07 1423 00 Rattlesnake Creek near	356	1960-80	2	362.0b	264.0	166.0	110.0	74.0	53.0	45.0	41.0	35.0
Macksville			5	1140.0	800.0	473.0	287.0	176.0	113.G	91.0	30.0	67.0
(Stafford County, 8 miles south-			10	2080.0	1440.0	842.0	490.0	288.0	174.0	136.0	117.0	97.0
east of Macksville.)			25	3990.0	2740.0	1590.0	891.0	498.0	285.0	213.0	179.0	147.0
			50	6080.0	4150.0	2430.0	1330.0	721.0	397.0	289.0	238.0	195.0
			100	8910.0 ^C	6060.0	3600.0	1930.0	1020.0	540.0	384.0	311.0	256.0 b
		1966-80	2	436.0 ⁱ⁾	309.0	191.0	123.0	81.0	55.0	45.0	39.0	34.0 h
			5	1390.0	953.0	573.0	342.0	209.0	128.0	100.0	84.0	71.0
			10	2570.0	1740.0	1040.0	603.0	354.0	207.0	157.0	129.0	108.0
			25	4950.0	3330.0	2020.0	1130.0	637.0	355.G	259.0	209.0	174.0
			50	7580.0	5090.0	3130.0	1720.0	945.0	509.0	364.0	289.0	242.0
			100	11100.0°	7480.0	4680.0	2520.0	1360.0	712.0	499.0	391.0	329.0°
07 1426 20 Rattlesnake Creek near	598	1961-80	2	349.0 ^b	326.0	274.0	202.0	152.0	114.0	94.0	65.0	71.0ª
Raymond			5	763.0	700.0	548.0	389.0	277.0	195.0	158.0	140.0	119.0
(Rice County, 3.5 miles south of			10	1150.0	1040.0	779.0	548.0	382.0	261.0	212.0	186.0	156.0
Raymond.)			25	1760.0	1560.0	1120.0	792.0	542.0	362.0	294.0	255.0	214.0
			50	2320.0	2030.0	1420.0	1010.0	662.0	449.0	366.0	315.0	264.0
			100	2970.0b	2560.0	1740.0	1250.0	841.0	549.0	448.0	383.0	321.0b
07 1428 60 Cow Creek near Claflin	43	1967-80	2	415.0b	213.0	104.0	56.0	33.0	18.0	13.0	11.0	7.5b
(Barton County, at State High-			5	974.0	497.0	238.0	131.0	78.0	43.0	31.0	24.0	18.0
way 4, 2.5 miles west of Claflin.)		10	1480.0	752.0	356.0	200.0	120.0	66.0	48.0	37.0	28.0
			25	2280.0	1150.0	537.0	308.0	188.0	106.0	77.0	59.0	46.0
			50	2980.0	1490.0	692.0	404.0	249.0	143.0	104.0	80.0	64.0
			100	3770.0C	1860.0	862.0	511.0	319.0	187.0	137.0	106.0	85.0 ^C
07 1429 00 Blood Creek near Boyd	61	1963-80	2	520.0b	237.0	115.0	64.0	35.0	20.0	15.0	12.0	8.1 ^b
(Barton County, at State High-			5	1090.0	474.0	239.0	137.0	75.0	45 . C	32.0	25.0	17.0
way 4, 1.3 miles northwest of			10	1580.0	682.0	354.0	203.0	115.0	70.0	49.0	38.0	26.0
Hoisington and 11.9 miles up-			25	2330.0	1010.0	542.0	310.0	182.0	114.0	77.0	60.0	42.0
stream from Cneyenne Bottoms.)			50	2980.0	1290.0	717.0	409.0	246.0	157.0	104.0	0.05	57.0
			100	3710.0b	1620.0	925.0	524.0	325.0	210.0	137.0	106.0	75.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square		rence interval (years)		Maxi	num averag			ic feet pe			
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 day	s 183 day
(07 1429 00) Continued		1966-80	2	540.0b	247.0	122.0	66.0	37.0	21.0	16.0	13.0	8.9b
			5	1160.0	499.0	255.0	145.0	80.0	49.0	35.0	28.0	19.0
			10	1700.0	720.0	378.0	223.0	124.0	77.0	54.0	42.0	29.0
			25	2530.0	1060.0	580.0	357.0	201.0	127.0	85.0	66.0	47.0
			50	3250.0	1370.0	768.0	489.0	277.0	177.0	117.0	90.0	04.0
			100	4050.0b	1710.0	991.0	653.0	373.0	239.0	155.0	119.0	85.0b
07 1433 00 Cow Creek near Lyons	499	1939-51,	2	2070.0ª	1570.0	936.0	518.0	348.0	209.0	148.0	134.0	99.0a
(Rice County, near Missouri		1962-80	5	4440.0	3430.0	1970.0	1160.0	701.0	417.0	318.0	263.0	196.0
Pacific Railroad bridge, 500			10	6230.0	4810.0	2700.0	1730.0	947.0	566.C	475.0	358.0	272.0
feet downstream from Little Cow			25	8590.0	6570.0	3600.0	2610.0	1250.0	757.0	733.0	483.0	378.0
Creek and 3.0 miles south of			50	10300.0	7840.0	4230.0	3360.0	1450.0	895.0	970.0	575.0	463.0
Lyons.)			100	12000.0b	9030.0	4800.0	4210.0	1650.0	1030.0	1250.0	466.0	551.00
7 1436 00 Little Arkansas River nea	r 71	1960-71	2	643.0a	309.0	158.0	81.0	46.0	28.0	21.0	17.0	13.0
Little River			5	940.0	445.0	232.0	127.0	78.0	50.C	38.0	33.0	24.0
(Rice County, 1 mile north-			10	1080.0	517.0	270.0	153.0	98.0	64.0	50.0	44.0	32.0
west of Little River.)			25	1210.0	591.0	307.0	180.0	122.0	81.0	64.0	57.0	42.0
			50	1270.0	635.0	328.0	196.0	137.0	93.0	75.0	67.0	49.0
			100	1320.0b	673.0	345.0	210.0	151.0	103.0	84.0	76.0	56.0
07 1442 00 Little Arkansas River at	1,250	1923-80	2	4800.0ª	4260.0	2850.0	1700.0	1050.0	651.0	502.0	423.0	326.0ª
Valley Center			5	11900.0	9120.0	6210.0	3810.0	2460.0	1530.0	1160.0	964.0	723.0
(Sedgwick County, 0.5 mile west			10	18700.0	12300.0	8430.0	5310.0	3560.0	2240.0	1700.0	1400.0	1040.0
of Valley Center.)			25	29800.0	15800.0	10900.0	7130.0	5000.0	3200.0	2430.0	1990.0	1480.0
			50	40000.0	18000.0	12500.0	8360.0	60.00.0	3940.0	2990.0	2440.0	1820.0
•			100	51900.0b	19900.0	13800.0	9470.0	7030.0	4670.0	3560.0	2900.0	2170.0
7 1447 80 North Fork Ninnescah	550	1966-80	2	2910.0b	1890.0	1110.0	693.0	455.0	297.0	243.0	215.0	180.0
River above Cheney			5	9090.0	5010.0	2650.G	1490.0	912.0	543.0	426.0	370.0	299.0
Reservoir			10	15700.0	7900.0	4010.0	2140.0	1270.0	728.0	557.0	481.0	382.0
(Reno County, at State High-			25	27300.0	12600.0	6030.0	3040.0	1770.0	978.6	731.0	626.0	489.0
way 17, 12 miles south of			50	38300.0	16600.0	7730.0	3760.0	2160.0	1170.0	863.0	735.0	570.0
Hutchinson and 12.5 miles up-			100	51300.0C	21100.0	9550.0	4500.0	2570.0	1370.0	997.0	545.0	651.0b
stream from Cheney Dam.)												
7 1448 50 South Fork South Fork	21	1962-80	2	175.0b	79.0	37.0	19.0	11.0	5.7	4.6	3.6	2.70
Ninnescah River near			5	532.0	256.0	125.0	72.0	43.0	22.0	14.0	11.0	6.7
Pratt			10	876.0	435.0	210.0	133.0	82.0	41.0	24.0	19.0	11.0
(Pratt County, 6.0 miles south-			25	1410.0	716.0	365.0	240.0	155.0	76.0	40.0	31.0	17.0
west of Pratt.)			50	1850.0	956.0	495.0	341.0	228.0	111.0	55.0	42.0	23.0
			100	2320.0°	1210.0	637.0	459.0	316.0	153.0	73.0	56.0	30.0

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	Records analy- zed	Recur- rence interval (years)		Maxi			ge, in cub				
	miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 days	s 183 days
07 1452 00 South Fork Ninnescah	543	1951-59	2	3520.0ª	2120.0	1230.0	783.0	540.0	383.0	317.0	288.0	246.0ª
River near Murdock		1965-80	5	7860.0	4630.0	2590.0	1530.0	962.0	653.0	513.0	452.0	306.0
(Kingman County, 4.0 miles south-			10	11800.0	6990.0	3860.0	2190.0	1310.0	881.0	672.0	583.0	458.0
east of Murdock.)			25	18100.0	10900.0	5940.0	3240.0	1830.0	1230.0	909.0	773.0	589.0
			50	23800.0	14500.0	7890.0	4190.0	2280.0	1540.0	1110.0	936.0	698.0
			100	30300.0b	18800.0	10200.0	5300.0	2780.0	1390.0	1340.0	1120.0	817.0ª
07 1457 00 Slate Creek at Welling-	154	1970-80	2	2850.0b	1710.0	918.0	472.0	285.0	166.0	124.0	104.0	81.0ª
ton			5	5080.0	3110.0	1650.0	813.0	505.0	290.0	210.0	184.0	132.0
(Sumner County, at U.S. Highway			10	6500.0	4010.0	2140.0	1040.0	655.0	376.0	269.0	240.0	166.0
81, at southern edge of Welling-			25	8330.0	5040.0	2730.0	1310.0	842.0	484.0	343.0	310.0	208.0
ton.)			50	9560.0	5730.0	3140.0	1500.0	977.0	563.0	396.0	362.0	237.0
			100	10700.0b	6340.0	3520.0	1680.0	1110.0	640.0	447.0	413.0	266.0b
07 1465 70 Cole Creek near DeGraff	30	1962-80	2	996.0b	497.0	200.0	145.0	89.0	52.0	40.0	35.0	25.0a
(Butler County, 5.0 miles south-			5	2010-0	933.0	482.0	269.0	163.0	94.0	71.0	61.0	43.0
east of DeGraff.)			10	2710.0	1190.0	613.0	340.0	205.0	115.0	90.0	76.0	53.0
			25	3560.0	1470.0	749.0	413.0	247.0	142.0	109.0	91.0	64.0
			50	4150.0	1640.0	831.0	456.0	272.0	156.0	121.0	100.0	70.0
			100	4700.0b	1780.0	898.0	491.0	291.0	168.0	131.0	108.0	76.0b
07 1470 70 Whitewater River at Towan	da 426	1962-80	2	6790.0 ^b	4480.0	2390.0	1360.0	886.0	544.0	429.0	364.0	204.0a
(Butler County, at State Highway			5	13400.0	8460.0	4430.0	2520.0	1690.0	1050.0	783.0	579.0	478.0
254, 0.5 mile west of Towanda and			10	17700.0	10900.0	5640.0	3220.0	2200.0	1370.0	1000.0	884.0	619.0
2.4 miles downstream from West			25	22500.0	13400.0	6930.0	3970.0	2770.0	1750.0	1250.0	1120.0	788.0
Branch.)			50	25700.0	14900.0	7700.0	4430.0	3130.0	2010.0	1400.0	1280.0	904.0
			100	28400.0b	16200.0	8340.0	4620.0	3440.0	2230.0	1530.0	1430.0	1010.0b
07 1478 00 Walnut River at Winfield	1,872	1923-80	2	19700.0ª	14900.0	8790.0	5250.0	3320.0	2100.0	1620.0	1340.0	1030.0a
(Cowley County, at U.S. Highway			5	36700.0	29300.0	17800.0	10600.0	6760.0	4240.0	3250.0	2700.0	2080.0
77, 1.0 mile south of Winfield.)			10	46300.0	37800.0	23300.0	13900-0	8960.0	5630.0	4300.0	3580.0	2780.0
			25	55700.0	46500.0	29200.0	17300.0	11400.0	7200.C	5500.0	4530.0	3570.0
			50	61100.0	51500.0	32700.0	19300.0	12900.0	8200.0	6270.0	5230.0	4090.0
			100	65200.0t	55500.0	35600.0	20900.0	14200.0	9070.0	6940.0	5790.0	4550.0b
07 1490 00 Medicine Lodge River near	903	1939-50,	2	2760.0	1670.0	945.0	587.0	378.0	260.0	210.0	186.0	157.0ª
Kiowa		1955,	5	5130.0		1820.0		702.0	473.0	363.0	310.0	256.0
(Barber County, at State High-		1960-80	10	5800.0		2500.0		996.0	662.0	495.0	416.0	338.0
way 14, 200 feet downstream from			25		5790.0				965.G	703.0	579.0	465.0
the Atchison, Topeka and Santa			50	10500.0		4220.0		1920.0	1240.0	891.0	725.0	578.0
Fe Railway Co. bridge and 1.5			100			5020.0			1570.0	1110.0	893.0	709.0ª
miles northeast of Kiowa.)												

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area	analy- zed	Recur- rence interval (years)	Maximum average discharge, in cubic feet per second, for indicated period of consecutive days								
	(square miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 da	ys 183 days
07 1515 00 Chikaskia River near	7-94	1951-65,	2	5280.0b	3140.0	1800.0	1080.0	685.0	430.0	351.0	307.0	250.0ª
Corbin		1976-80	5	11800.0	6750.0	3690.0	2160.0	1370.0	920.0	710.0	599.0	470.0
(Sumner County, at State Highway			10	18200.0	10100.0	5350.0	3080.0	1960.0	1400.0	1050.0	860.0	662.0
49, 1 mile upstream from Prairie			25	28800.0	15400.0	7930.0	4480.0	2880.0	2220.0	1610.0	1230.0	963.0
Creek and 3 miles west of			50	38900.0			5680.0	3690.0	3030.0	2140.0	1660.0	1230.0
Corbin.)			100	51000.0b	25800.0	12800.0	7010.0	4620.0	4020.0	2790.0	2110.0	1550.0 ^D
7 1562 20 Bear Creek near Johnson	835	1967-80	2	232.0°	103.0	45.0	22.0	12.0	6.4	4.4	3.4	2.3 ^C
(Stanton County, at U.S. Highway			5	1140.0	603.0	258.0	125.0	71.0	40.0	27.0	21.0	14.0
270, 3.5 miles north of Johnson.)			10	2450.0	1410.0	610.0	293.0	172.0	100.0	67.0	52.0	34.0
			25	5190.0	3280.0	1450.0	692.0	424.0	255.0	171.0	132.0	86.0
			50	8280.0	5570.0	2530.0	1200.0	755.0	463.0	312.0	241.0	158.0
			100	12500.0°	8910.0	4150.0	1960.0	1270.0	812.0	540.0	417.0	276.0°
7 1569 00 Cimarron River near 4	,220	1966-80	2	1120.0b	659.0	397.0	250.0	179.0	134.0	118.0	110.0	97.0ª
Forgan, Oklahoma (Meade County, Kansas, at State			5	3020.0	1710.0	937.0	532.0	333.0	222.0	178.0	157.0	129.0
			10	5110.0	2900.0	1520.0	816.0	476.0	297.0	227.0	192.0	153.0
Highway 23, 0.8 mile north of			25	9010.0	5200-0	2600.0	1320.0	714.0	416.0	300.0	243.0	185.0
Oklahoma-Kansas State line and			50	13000.0	7670.0	3740.0	1840.0	941.0	523.0	363.0	295.0	211.0
7.8 miles north of Forgan.)			100	18200.0C	11000.0	5240.0	2490.0	1220.0	649.0	434.0	331.0	238.0ª
7 1575 00 Crooked Creek near Nye			2	586.0b	342.0	220.0	140.0	89.0	60.0	49.0	43.0	36.0ª
(n	813	1943-80	5	1850.0	1090.0	708.0	430.0	256.0	166.0	127.0	105.0	81.0
(Meade County, 11.5 miles west			10	3480.0	2090.0	1370.0	816.0	475.0	305.C	224.0	178.3	133.0
of Englewood.)			25	6980.0	4340.0	2860.0	1690.0	968.0	618.0	433.0	332.0	236.0
			50	11100.0		4700.0	2760.0	1580.0	1010.0	682.0	510.0	353.0
			100	16900.0b		7450.0	4370.0	2500.0	1600.0	1050.0	765.0	516.0b
		1966-80	2	340.0b	213.0	144.0	96.0	62.0	41.0	35.0	31.0	27.0a
		_500.00	5	846.0	549.0	370.0	235.0	143.0	89.0	71.0	61.0	49.0
			10	1390.0	933.0	633.0	396.0	234.0	141.0	109.0	90.0	71.0
			25	2410.0		1160.0	725.0	418.0	241.0	178.0	143.0	110.0
			50	3470.0	2510.0	1760.0	1100.0	625.0	349.0	250.0	198.0	149.0
			100		3630.0			915.0	495.0	346.0	268.0	199.0
7 1579 00 Cavalry Creek at	39	1967-81	2	144.0 ^b	61.0	30.0	17.0	10.0	6.6	4.8	4.2	3.₽
Coldwater		-30. 0.	5	469.0	208.0	102.0	55.0	31.0	17.0	13.0	10.0	7.8
(Comanche County, 1.0 mile			10	869.0	398.0	196.0	105.0	56.0	29.0	21.0	16.0	12.0
west of Coldwater.)			25	1680.0	802.0	399.0	212.0	109.0	53.0	38.0	28.0	20.0
The state of the s			50	2560.0		638.0	337.0	169.0	80.0	56.0	40.0	27.0
			20									200

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age	- analy- zed	Recurrence interval Maximum average discharge, in cubic feet per second, (years) for indicated period of consecutive days									
	area (square miles)			1 day	3 days	7 days	15 days	30 days	60 days	90 days	120 day	rs 183 days
07 1657 00 Verdigris River near	181	1956-76	2	4090.0b	2340.0	1370.0	777.0	466.0	285.0	240.0	208.0	166.0b
Madison			5	8260.0	4630.0	2660.0	1490.0	892.0	503.0	481.0	429.0	334.0
(Greenwood County, at State High-			10	10800.0	5980.0	3380.0	1880.0	1130.0	720.0	618.0	556.0	430.0
way 57, 1.5 miles east of Madison			25	13600.0	7340.0	4070.0	2250.0	1350.0	871.0	750.0	681.0	523.0
and 3.0 miles upstream from			50	15300.0	8130.0	4440.0	2460.0	1470.0	954.0	824.0	769.0	574.0
Haldenman Creek.)			100	16700.0b	8760.0	4730.0	2610.0	1570.0	1020.0	879.0	802.0	613.0b
07 1670 00 Fall River near Eureka	307	1947-76	2	5970.0b	3230.0	1840.0	1100.0	721.0	465.0	380.0	322.0	246.0b
(Greenwood County, at State High-			5	14300.0	7340.0	4100.0	2410.0	1620.0	1040.0	853.0	732.0	571.0
way 99, 3.0 miles southeast of			10	19500.0	9800.0	5480.0	3210.0	2200.0	1420.C	1150.0	994.0	781.0
Eureka and 5.0 miles downstream			25	24700.0	12200.0	6890.0	4030.0	2800.0	1820.0	1470.0	1270.0	1010.0
from Spring Creek.)			50	27600.0	13600.0	7680.0	4500.0	3160.0	2070.0	1660.0	1440.0	1140.0
			100	29800.0°	14600.0	8300.0	4860.0	3450.0	2260.0	1800.0	1570.0	1250.0b
7 1675 00 Otter Creek at Climax	129	1947-80	2	3100.0b	1520.0	838.0	513.0	321.0	203.0	159.0	133.0	102.0b
(Greenwood County, at State High-			5	7660.0	3630.0	1970.0	1210.0	774.0	492.0	390.0	337.0	261.0
way 99, 0.5 mile south of Climax			10	10900.0	5060.0	2710.0	1660.0	1070.0	678.0	541.0	470.0	368.0
and 5.5 miles downstream from			25	14500.0	6650.0	3520.0	2130.0	1390.0	873.0	702.0	610.0	482.0
South Branch.)			50	16900.0	7620.0	4010-0	2410.0	1590.0	986.0	796.0	690.0	548.0
			100	18300.0b	8430.0	4400.0	2630.0	1740.0	1070.0	870.0	752.0	601.0°
07 1698 00 Elk River at Elk Falls	220	1968-80	2	7880.0b	4400.0	2400.0	1280.0	783.0	490.0	385.0	320.0	236.0ª
(Elk County, at U.S. Highway 60			5	15300.0	7890.0	4160.0	2140.0	1280.0	790.0	621.0	528.0	393.0
in Elk Falls, 2 miles upstream			10	20900.0	10300.0	5300.0	2680.0	1590.0	951.0	761.0	654.0	492.0
from Wildcat Creek.)			25	28500.0	13200.0	6630.0	3300.0	1920.0	1140.0	915.0	794.0	608.0
			50	34400.0	15300.0	7540.0	3720.0	2140.0	1200.0	1010.0	886.0	687.0
			100	40500.0b	17300.0	8370.0	4090.0	2320.0	1360.0	1100.0	966.0	759.0b
7 1700 00 Elk.River near Elk City	575	1939-69	2	9820.0b	6060.0	3320.0	1970.0	1240.0	780.0	618.0	514.0	399.0b
(Montgomery County, 150 feet down-			5	22100.0	14100.0	7760.0	4620.0	2920.0	1350.0	1410.0	1160.0	917.0
stream from Salt Creek and 1.3 mil	les		10	30900.0	19800.0	11100.0	6600.0	4210-0	2670.0	1970.0	1600.0	1280.0
south of Elk City.)			25	41400.0	26800.0	15200.0	9080.0	5860.0	3710.0	2650.0	2120.0	1700.0
			50				10800.0					1980.0
			100	55000.0b	35700.0	20700.0	12400.0	8170.0	5140.0	3510.0	2750.0	2210.0 ^b
07 1720 00 Caney River near Elgin	445	1940-80	2	8800.08	4850.0	2800.0	1690.0	1080.0	689.0	528.0	444.0	343.0ª
(Chautauqua County, 2 miles west			5	17930.0	9700.0	5540.0	3350.0	2180.3		1080.0	907.0	712.0
of Elgin.)			10	23900.0	12700.0	7240.0	4370.0	2870.0		1420.0		944.0
			25	30500.0	15800.0	9060.0	5470.0	3620.0			1510.0	1200.0
			50				6130.0				1700.0	1350.0
			100	38400.0b	19300.0	11100.0	6670.0	4460.0	2940.0	2200.0	1860.0	1470.0b

Table 6.--Magnitude and frequency of high flows at streamflow-gaging stations having unregulated flow--Continued

Station number, name, and location	Contri- buting- drain- age area (square	uting- analy- rence rain- zed interval Maximum average discharge, in cubic feet per so ge (years) for indicated period of consecutive day										
	miles)			1 day	days	7 days	15 days	30 days	60 days	90 days	120 days	183 days
07 1805 00 Cedar Creek near	110	1939-80	2	2560.0ª	1160.0	617.0	357.0	223.0	145.0	116.0	100.0	76.0ª
Cedar Point			5	4930.0	2180.0	1210.0	719.0	457.0	289.0	230.0	199.0	148.0
(Chase County, 4.0 miles south of			10	6320.0	2770.0	1570.0	933.0	595.0	372.0	295.0	254.0	188.0
Cedar Point.)			25	7780.0	3340.0	1920.0	1150.0	737.0	455.C	361.0	308.0	226.0
			50	8630.0	3670.0	2130.0	1280.0	815.0	501.0	398.0	338.0	246.0
			100	9320.0b	3920.0	2300.0	1380.0	882.0	537.0	427.0	360.0	202.0b
07 1815 00 Middle Creek near Elmdale	92	1939-50	2	2490.0b	1170.0	630.0	381.0	233.0	143.0	100.0	90.0	69.00
(Chase County, 4 miles northwest o	f		5	5150.0	2310.0	1280.0	782.0	488.0	288.0	210.0	174.0	131.0
Elmdale.)			10	6830.0	3000.0	1690.0	1030.0	657.0	381.0	276.3	225.0	167.0
			25	8650.0	3750.0	2120.0	1300.0	649.C	486.0	349.0	279.0	206.0
			50	9760.0	4190.0	2390.0	1470.0	972.0	553.C	396.0	311.0	229.0
			100	10700.0°	4560.0	2610.0	1610.0	1080.0	610.0	435.0	338.0	248.00
07 1831 00 Owl Creek near Piqua	177	1960-70	2	4990.0b	2810.0	1470.0	857.0	481.0	275.0	227.0	194.0	148.0
(Woodson County, 5.4 miles			5	9410.0	5170.0	2670.0	1500.0	873.0	505.0	439.0	378.0	293.0
southwest of Piqua.)			10	12300.0	6660.0	3400.0	1870.0	1120.0	651.0	578.0	496.0	390.0
			25	15500.0	8340.0	4180.0	2270.0	1380.C	814.0	738.0	631.0	502.0
			50	17700.0	9430.0	4660.0	2510.0	1550.0	920.0	844.0	717.0	576.0
			100	19600.0°	10400.0	5070.0	2720.0	1700.0	1010.0	937.0	792.0	641.00
07 1840 00 Lightning Creek near	197	1939-46,	2	5040.0ª	3350.0	1790.0	1020.0	635.0	400.0	314.0	259.0	200.0ª
McCune		1960-80	5	9100.0	5810.0	3160.0	1780.0	1100.0	688.0	522.0	442.0	347.0
(Cherokee County, 5.0 miles south			10	12000.0	7430.0	4030.0	2290.0	1400.0	881.0	650.0	559.0	441.0
of McCune and 13.0 miles southwes	t		25	15800.0	9380.0	5200.0	2910.0	1760.0	1120.C	795.0	697.0	553.0
of Parsons.)			50	18600.0	10700.0	5990.0	3350.0	2000.0	1280.0	890.0	791.0	629.0
			100	21400.0b	12000.0	6740.0	3770.0	2230.0	1440.0	976.0	578.0	599.0b

^a Approximate standard error less than 20 percent.

 $^{^{\}rm b}$ Approximate standard error 20 to 50 percent.

C Approximate standard error larger than 50 percent.

