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Finite-Difference Migration
by Optimized One-Way Equations

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FINITE-DIFFERENCE MIGRATION BY THE OPTIMIZATION OF ONE-WAY EQUATIONS

By Myung W. Lee and Sang Y. Suh

ABSTRACT

The principle component of the finite-difference migration scheme is the approximation of a one-way wave extrapolation operator or a downward continuation operator. Usually, this approximation can be carried out either by a Taylor series expansion or a continued fraction method of an exact one-way extrapolation operator (or a "square root" operator). Due to the truncation of the expansion, the dispersion relation of the conventional one-way equation is very inaccurate, particularly for high propagation angles. This dispersion error controls the limit of the dip angle to be properly migrated by the finite-difference method.

In order to improve the dispersion relation, an optimization method was investigated. The basic concept of the optimization is to modify the coefficients of the conventional equation in such a way that the modified coefficients provide a better dispersion relation. This optimization can be implemented by minimizing the weighted dispersion error using a least-squares method.

This study shows that the optimization improves the dispersion relation of the one-way wave equation substantially. For example, within the relative dispersion error of 1 percent, the optimized second-order equation is reliable up to the propagation angle of 65 degrees; while the conventional second-order equation, the so-called 45 degree equation, is reliable up to 45 degrees. Since the only differences between the optimum and conventional one-way equations are the coefficients in the rational approximation of the square-root equation, the conventional finite-difference migration computer program can be modified easily in order to improve the performance of steep-dip migration.

INTRODUCTION

One of the main purposes of reflection seismology is to image the subsurface structure by measuring the reflected waves on the surface. To accomplish this objective, the data is subjected to computer processing. Seismic migration is a process of reconstructing the subsurface structure from the measured data and has received a great deal of attention within the last decade. There are three different approaches in modern seismic migration, i.e., the finite-difference method (Claerbout and Doherty, 1972; Claerbout, 1976), the Kirchhoff integral method (French, 1975; Schneider, 1978), and the F-K method (Stolt, 1978; Gazdag, 1978). All of the methods are based on the wave equation and are conveniently called wave-equation migrations.

Wave-equation migration is accomplished by two steps--downward extrapolation and imaging. The three methods of migration differ in their approach on the extrapolation of the wave field. The difference between depth migration and time migration is the imaging of the extrapolated wave field. Since imaging is simply a method of representing the wave field, the method of extrapolation is of great importance in most migration schemes.

The theory of wave extrapolation is based on the square root equation. The conventional wave equation represents waves which propagate in positive and in negative z-directions simultaneously. On the contrary, the square root equation represents waves propagating in one z-direction only. In laterally homogeneous media, exact wave extrapolation can be achieved by the square-root equation in the frequency-wavenumber domain.

In laterally heterogeneous media, wave extrapolations can be accomplished by use of the finite-difference method. In this method, a wavefield can be extrapolated by a one-way equation which is a rational approximation of the square-root equation. The one-way equation is further approximated by a difference equation in the actual computation. There are two methods of rationalizing the square-root equation. One is by a Taylor series and the other is by continued fractions (Hildebrand, 1956, p. 406). The Taylor series method may be called an explicit scheme while the continued-fractional method may be called an implicit scheme. The conventional 15-degree equation is the first-order approximation of the square root equation by either method. The 45-degree is the second-order approximation by the implicit scheme.

One of the disadvantages in the finite-difference method is that it cannot handle steep-dip structures. This is due to the inaccurate dispersion relation of the one-way equation used in the method. The inaccuracy comes from the truncation of the exact series expression of the square-root equation. Therefore, more terms must be used, i.e., migration by higher order equations. Berkhout (1980) and Gazdag (1980) used explicit high-order equations in their migration. An advantage of this method is the accuracy of the derivatives, which are evaluated by either a convolution in the space domain or by a multiplication in the wavenumber domain. This method alone cannot handle the steep-dip limitation satisfactorily, as is demonstrated in a later section. Besides, this method is numerically unstable (Gazdag and Sguazzero, 1984). Ma (1981) developed a more practical approach to finite-difference migration using the high-order implicit equations. In his method, the high-order equation is split into a series of low-order equations that are solved separately.

Berkhout (1979) studied the dispersion relations of the first-, second-, and third-order approximate equations and found that the dispersion error could be reduced by modifying the coefficients of the equations. His results suggest that the dip limitation can be avoided by using a higher order equation with modified coefficients. Ma (1981) attempted a similar procedure for the fifth-order implicit equation.

In the first section of this paper, the theory of wave extrapolation is briefly reviewed and the dispersion relations of one-way equations both explicit and implicit are analyzed. In the next section, optimization of the implicit one-way equations (using a least-squares method) to minimize the dispersion error is discussed. Finally, the optimized equations are tested on three examples: (1) extrapolation of a monochromatic wave, (2) migration of a synthetic model, and (3) migration of field data. Two appendices--the finite-difference formulation of the one-way equation and a version using only CPU (Central Processing Unit) of the migration program--are included.

ONE-WAY EQUATIONS

Wave-equation migration consists of two steps: extrapolation and imaging. The finite-difference extrapolation uses the one-way equation which is a rational approximation of the square-root equation. In this section, the basic concept of wave extrapolation is reviewed and the various one-way equations in terms of their dispersion relations are investigated.

The theory of wave extrapolation starts from an assumption that the wave field $p(x, z, t)$ satisfies the two-dimensional scalar wave equation:

$$\frac{\partial^2 p}{\partial x^2} + \frac{\partial^2 p}{\partial z^2} = \frac{1}{v^2} \frac{\partial^2 p}{\partial t^2} \quad (1)$$

where x is the horizontal distance, z is the depth, t is time, and v is the velocity. By introducing k_x and ω , which are the apparent horizontal

wavenumber and the angular frequency, respectively, the wave field can be expressed by the following double Fourier transform:

$$p(x, z, t) = \sum_{k_x} \sum_{\omega} \hat{p}(k_x, z, \omega) \exp[i(k_x x + \omega t)] \quad (2)$$

For the moment, we assume v is independent of x . Substituting equation (2) into equation (1) gives an ordinary differential equation:

$$\frac{d^2 \tilde{p}}{dz^2} = \left(-\frac{\omega^2}{v^2} + k_x^2\right) \tilde{p} \quad (3)$$

Equation (3) has two solutions,

$$\tilde{p}(k_x, z + \Delta z, \omega) = \tilde{p}(k_x, z, \omega) \exp(\pm i k_z \Delta z) \quad (4)$$

where k_z is given by

$$k_z = \frac{\omega}{v} \left[1 - \left(\frac{v k_x}{\omega} \right)^2 \right]^{1/2} \quad (5)$$

One of the two solutions represents the wave propagating in the negative z -direction, while the other is in the positive z -direction. In order to extrapolate the wave field, we must choose only one of the two solutions for the following reason.

The wave equation is second order in z and has two independent solutions. Therefore, we need two boundary conditions to extrapolate waves in the z -direction. But we are given only one boundary condition in seismic migration, the wave observed on the surface. If the wave propagates in one direction only, we may discard the unnecessary solution in equation (4). This reduces the wave equation to the first order in z which can be solved with one boundary condition.

We choose the positive sign in equation (4) which implies that the wave propagating in the negative z-direction is considered. With the positive sign in equation (4), the extrapolation of the wave at $z = z_0$ to $z = z_0 +$

Δz can be accomplished by the correcting the phase angle, given by $k_z \Delta z$.

This is the basic concept of the phase shift method of migration (Gazdag, 1978). The above approach indicates that the wave extrapolation in the (k_x, z, ω) domain might be represented by the following square-root

equation,

$$\tilde{P}_z(k_x, z, \omega) = i \frac{\omega}{v} \left[1 - \left(\frac{v k_x}{\omega} \right)^2 \right]^{1/2} \tilde{P}(k_x, z, \omega) \quad (6)$$

where the subscript z represents the derivative with respect to that variable. Equation (6) is appropriate for the zero-offset migration. For the non-zero offset migration, a double square-root equation (Yilmaz and Claerbout, 1980) should be used.

The phase shift method is valid only for laterally homogeneous media. If the velocity changes horizontally, the extrapolation can be done in (x, z, ω) or in (x, z, t) domain with the one-way equation which is a rational approximation of equation (6), assuming that the logarithmic variation of velocity is less than that of the wave. There are two approaches in the approximation--explicit and implicit. The explicit method uses the Taylor series expansion while the implicit method uses continued fractions. Both of the methods require truncation of the exact expression. This is known as the paraxial approximation. Because of the truncation, the derived one-way equation is always different from the square-root equation. The difference may be represented by the dispersion relations. We investigate the dispersion relations of the one-way equations derived by both methods.

The simplest method of approximating the square-root expression of k_z given in equation (5) into k_x is the Taylor series method,

$$k_z = \frac{\omega}{v} \left(1 - \frac{1}{2} \frac{v^2 k_x^2}{\omega^2} - \frac{1}{8} \frac{v^4 k_x^4}{\omega^4} - \dots \right) \quad (7)$$

Let us define $k_z^{(n)}$, the n-th order approximation of k_z , by taking the first n+1 terms in the series expression. The first-order approximation of k_z produces the following one-way equation,

$$\tilde{P}_z = i \frac{\omega}{v} \left(1 - \frac{1}{2} \frac{k_x^2 v^2}{\omega^2} \right) \tilde{P} \quad (8)$$

in the (k_x, z, ω) domain. By inverse-transforming equation (8), the one-way equation can be written in the (x, z, ω) domain as

$$P_z = i \frac{\omega}{v} \left(1 - \frac{1}{2} \frac{v^2}{\omega^2} \partial_{xx} \right) P. \quad (9)$$

This equation is known as a 15-degree equation. In the wave extrapolation, the wave P and its x -derivative are known, but the z -derivative is unknown. Equation (9) represents the unknown P_z in terms of the known. Therefore,

the equation is an explicit one-way equation. The second-order approximation of k_z produces the one-way equation in (x, z, ω) domain as

$$P_z = i \frac{\omega}{v} \left(1 + \frac{1}{2} \frac{v^2}{\omega^2} \partial_{xx} - \frac{1}{8} \frac{v^4}{\omega^4} \partial_{xxxx} \right) P \quad (10)$$

which also is an explicit one-way equation. Generally, a one-way equation derived from the Taylor series method is the explicit equation.

The accuracy of the approximate one-way equation is determined in terms of its dispersion relation. Let us consider a plane wave in the direction of θ with respect to the z -axis. The apparent wave numbers in x - and z -directions are

$$k_x = k \sin \theta \quad (11)$$

$$k_z = k \cos \theta \quad (12)$$

respectively, where k is the true wave number ω/v . The dispersion relation of the first-order approximate one-way equation is found by substituting equation (11) into equation (7) resulting in

$$k_z^{(1)} = k \left(1 - \frac{1}{2} \sin^2 \theta \right) \quad (13)$$

Therefore, the dispersion error, $\Delta k_z^{(1)}$ is given by

$$\Delta k_z^{(1)} = k_z^{(1)} - k_z = k \left(1 - \frac{1}{2} \sin^2 \theta - \cos \theta \right) \quad (14)$$

and is a function of the propagation angle θ and of the wavenumber k . The relative dispersion error is defined by the dispersion error normalized by the wavenumber, which is a function of only the propagation angle. For a reflector having dip angle θ , the propagation angle of the normal ray is also θ with respect to the z -axis. For successful migration, a one-way equation which is accurate up to the propagation angle θ should be used.

Let us define the relative dispersion error limit as 1 percent. Figure 1 shows the relative dispersion error of explicit one-way equations obtained by the Taylor series method. The numbers on the figure are the order of the approximation. The higher order approximation gives the more accurate dispersion relation. Gazdag (1980) and Berkhout (1980) used the explicit higher order equations for migration. The x -derivatives were computed by convolution in (x, z, ω) domain or by multiplication in (k_x, z, ω) domain.

This method is effective in reducing the numerical error resulting from the approximation of derivatives by differences. However, the methods were not effective for steep-dip migration. Figure 1 indicates that a sixteenth order equation or more should be used to migrate a 75-degree dipping structure.

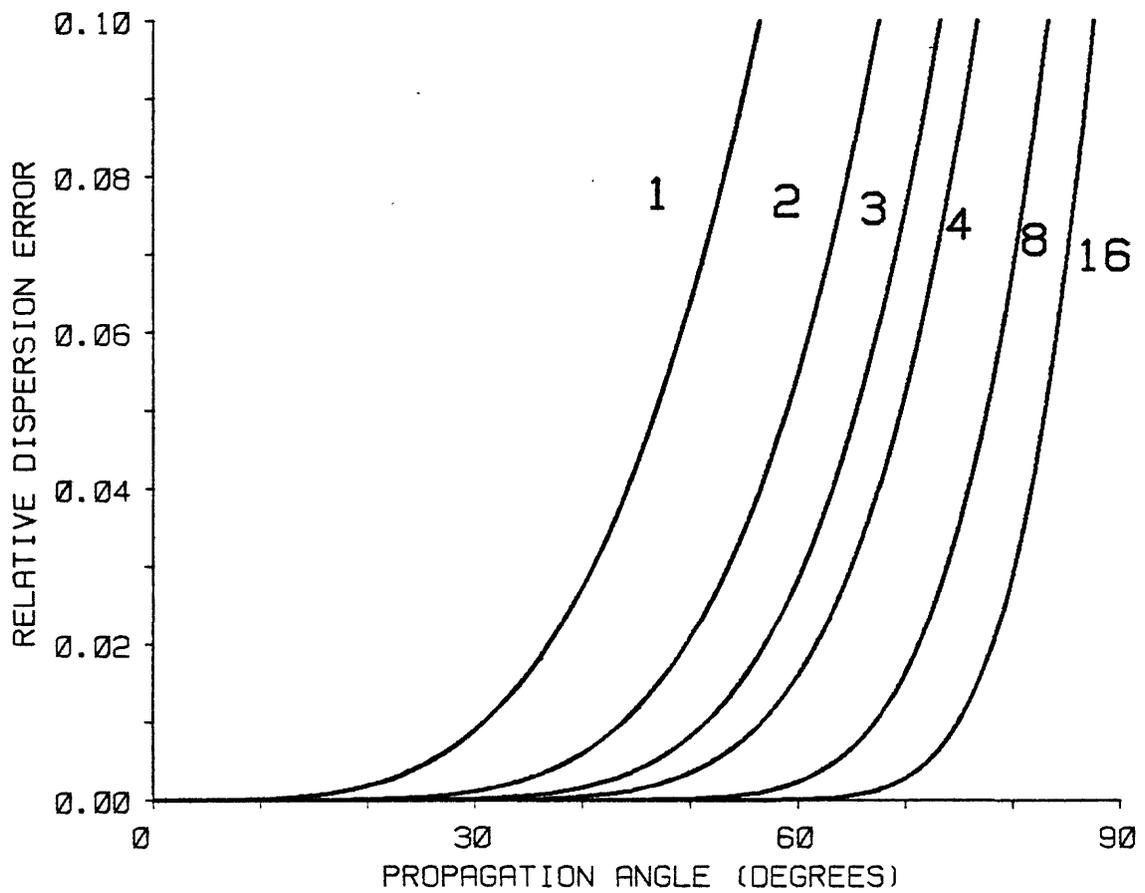


Figure 1.--Dispersion error in explicit one-way equations obtained by Taylor series approximation of the wave equation. Numbers annotated next to the curves indicate the order of approximation.

The second method of approximating k_z into k_x is the use of continued fractions. Let us define two new variables s and Y as

$$S = - \frac{v^2 k_x^2}{\omega^2} = - \frac{k_x^2}{k^2} \quad (15)$$

$$(1+S)^{1/2} = 1+Y \quad (16)$$

respectively. This method is the approximation of Y by a rational function of s , resulting in a quadratic equation by squaring equation (16)

$$Y^2 + 2Y - S = 0 \quad (17)$$

The smallest root of equation (17) is found by successive approximations (Claerbout, 1976, p. 207). By using n -th approximation of Y , Y_n , and

$(n+1)$ -th approximation of Y , Y_{n+1} , equation (17) can be written by

$$Y_n Y_{n+1} + 2Y_{n+1} - S = 0 \quad (18)$$

This gives a recurrence relation,

$$Y_{n+1} = \frac{S}{2+Y_n} \quad (19)$$

Starting from $Y_0 = 0$, we get the first and second approximations of Y as

$$Y_1 = \frac{S}{2} \quad (20)$$

$$Y_2 = \frac{2S}{4+S} \quad (21)$$

respectively. The third and fourth approximations are

$$Y_3 = \frac{4S+S^2}{8+4S} \quad (22)$$

$$Y_4 = \frac{8S+4S^2}{16+12S+S^2} \quad (23)$$

The first-order approximation of the one-way equation is obtained using equations (6), (15), (16), and (20), and is the same as the first-order equation obtained by the Taylor series method. The second-order equation by continued fractions is obtained using equation (21). In the (x, z, ω) domain, the equation is

$$P_z = i \frac{\omega}{v} \left(1 + \frac{2\partial_{xx}}{4k^2 + \partial_{xx}} \right) P. \quad (24)$$

Equation (24) is known as a 45-degree equation. The third and fourth order equations by continued fractions are obtained by the same method. These are

$$P_z = i \frac{\omega}{v} \left(1 + \frac{4k^2 \partial_{xx} + \partial_{xxxx}}{8k^4 + 4k^2 \partial_{xx}} \right) P \quad (25)$$

$$P_z = i \frac{\omega}{v} \left(1 + \frac{8k^2 \partial_{xx} + 4 \partial_{xxxx}}{16k^4 + 12k^2 \partial_{xx} + \partial_{xxxx}} \right) P. \quad (26)$$

Equation (24) contains an x-derivative term in its denominator. If the x-derivative is considered as the spatial convolution, the derivative in the denominator corresponds to the spatial deconvolution. Equation (24) may be converted to the convolutional form by multiplying both sides of the

equation by $4k^2 + \partial_{xx}$. The result represents the unknown P_z in terms of

P_{xxz} which is still unknown. Therefore, equation (24) is an implicit

equation. For the same reason, equations (25) and (26) are implicit equations. Generally, a one-way equation (with an order greater than two) derived by the continued fraction method is an implicit equation. Stolt (1978) derived similar equations by transforming the wave equation into the floating-time coordinate and by successively approximating the z-derivatives.

Ma (1981) introduced a convenient method of solving the higher order implicit equations in which the higher order equation is split into a series of lower order equations. The general form of Y_{2n} is given by

$$Y_{2n} = \sum_{i=1}^n a_i s^i / \left(1 + \sum_{i=1}^n b_i s^i \right). \quad (27)$$

Equation (27) may be split into partial fractions as

$$Y_{2n} = \sum_{i=1}^n \frac{\alpha_i s}{1 + \beta_i s}. \quad (28)$$

Therefore, the 2n-th order implicit equation is given by

$$P_z = i \frac{\omega}{v} \left(1 + \sum_{i=1}^n \frac{\alpha_i \partial_{xx}}{k^2 + \beta_i \partial_{xx}} \right) P \quad (29)$$

in the (x, z, ω) domain. Application of Marzuk's splitting method (Mitchell, 1969) to equation (29) gives the following series of second-order equations and a phase correction equation,

$$P_z = i \frac{\omega}{v} \frac{\alpha_m \partial_{xx}}{k^2 + \beta_m \partial_{xx}} P, \quad m=1, 2, \dots, n$$

$$P_z = i \frac{\omega}{v} P. \quad (30)$$

Thus, wave extrapolation by the $2n$ -th order implicit equation is accomplished by solving the second-order equations n times and by applying the $k\Delta z$ phase correction. In this method, the computing time of the extrapolation is approximately proportional to the order of the equation. It is possible to apply the splitting method to the $(2n-1)$ th order equation, but it has no advantage over $2n$ -th order equation. The computing time is almost the same but the dispersion relation is less accurate.

Figure 2 shows the relative dispersion error of one-way equations obtained by the continued fractions method. The numbers shown are the order of the approximation. The dispersion relation shown in this figure is more accurate than in figure 1. With the same order of approximation, the implicit equation is superior to the explicit. Still the implicit equation is not satisfactory. Even the eighth-order implicit equation shows more than 1 percent relative dispersion error for the propagation angle of 75 degrees. In order to get an implicit equation reliable up to 90 degrees propagation angle with 1 percent relative dispersion error, n must be 100 or more. Therefore, the problem of steep dip in finite-difference migration cannot be solved by using the higher order equations alone.

OPTIMIZATION OF ONE-WAY EQUATIONS

That the implicit equation better approximates the square-root equation than does the explicit equation has been shown. Furthermore, Berkhout (1979) modified the coefficients in second and third order implicit equations. In his method, the second and third order approximations of Y in equations (20) and (21) are modified as

$$Y_2 = \frac{1}{2} \frac{S}{1+a_2 S} \quad (31)$$

$$Y_3 = \frac{S}{2} \frac{1+a_3 S}{1+0.5 S} \quad (32)$$

respectively. Instead of the original coefficients $a_2 = a_3 = 0.25$, he used $a_2 = 0.279$ and $a_3 = 0.242$ respectively. The modified equations showed better dispersion relations than the originals. Ma (1981) introduced a modified version of his sixth-order equation, which corresponds to Y_5 in this paper. In this section, the optimization of one-way equations by modifying the coefficients is discussed.

The approximation of Y into Y_{2n} produces the error $E_{2n}(s)$ as

$$E_{2n}(s) = 1 + Y_{2n} - (1 + S)^{1/2} \quad (33)$$

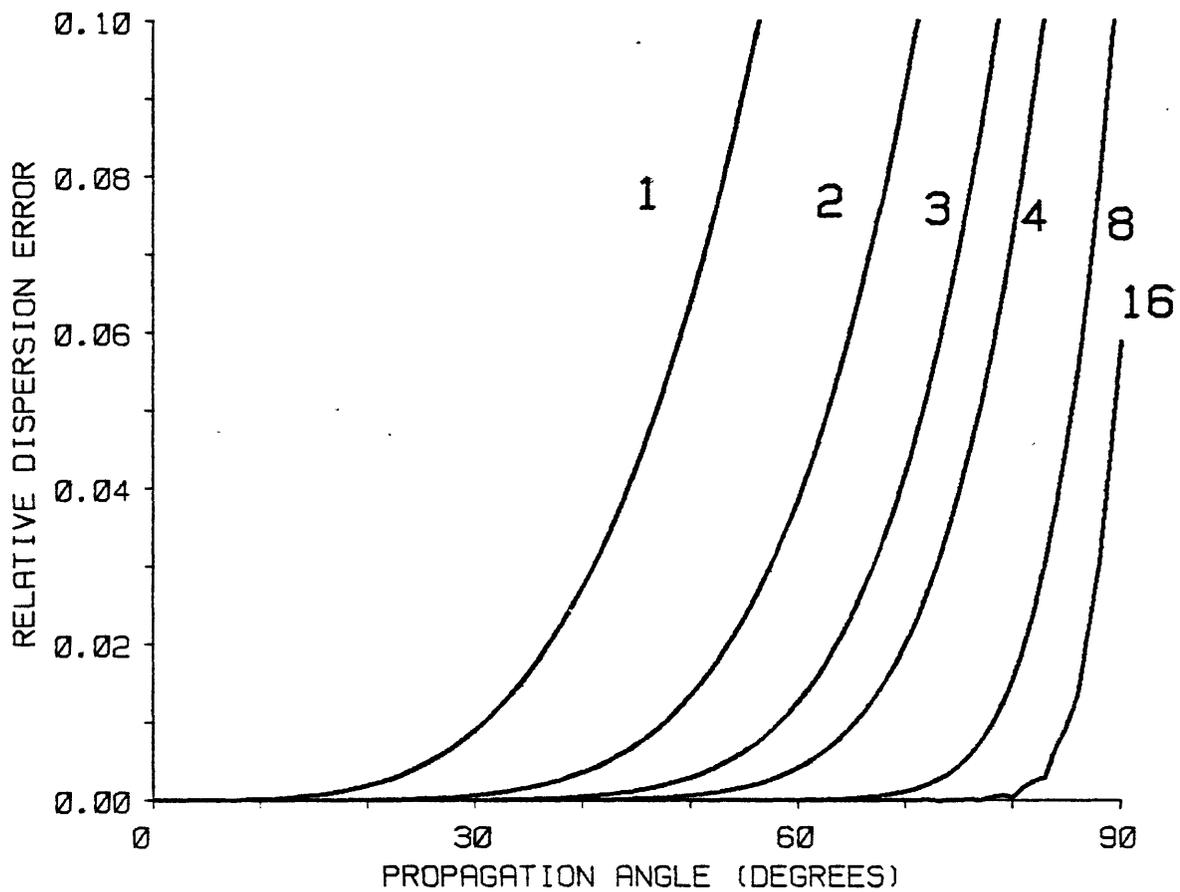


Figure 2.--Dispersion error in one-way equations obtained by the continued fractional approximation of the wave equation. Numbers annotated next to the curves indicate the order of approximation.

Substituting equation (27) into equation (33), and converting into the propagation angle θ gives

$$E_{2n}(\theta) = \sum_{i=1}^n a_i (-\sin^2 \theta)^i / \left[1 + \sum_{i=1}^n b_i (-\sin^2 \theta)^i \right] + 1 - \cos \theta. \quad (34)$$

The optimization procedure may be defined by finding coefficients a_i, b_i ($i = 1, 2, \dots, n$) which minimizes the following integral,

$$J = \int_0^{\phi} E_{2n}^2(\theta) d\theta \quad (35)$$

where ϕ is the maximum optimization angle. The direct approach using equation (35) is very difficult and requires laborious numerical integration. Moreover, it turns out to be a nonlinear least-squares method. The authors tried to solve the problem by the Newton-Gauss method employing the iterative Taylor series expansion but the result was not satisfactory. The difficulty occurs when n is greater than 2, greater than the fourth-order equation, mainly because the solution is very sensitive to the initial guess required in the Newton-Gauss method.

To circumvent this difficulty, we used the weighted dispersion error. The weighted error E'_{2n} is defined as the result of E_{2n} times its

denominator in equation (34),

$$E'_{2n}(\theta) = \sum_{i=1}^n a_i (-\sin^2 \theta)^i + (1 - \cos \theta) \left[1 + \sum_{i=1}^n b_i (-\sin^2 \theta)^i \right] \quad (36)$$

The optimized coefficients a_i, b_i , ($i = 1, 2, \dots, n$) can be found by minimizing the following integral

$$J' = \int_0^{\phi} [E'_{2n}(\theta)]^2 d\theta. \quad (37)$$

This is a linear least-squares method. The validity for using the weighted error can be justified by analyzing its result.

With the standard least-squares method, the optimization coefficients are the solution of the following normal equations,

$$\begin{aligned} \sum_{j=1}^n a_j \int (-\sin^2 \theta)^{i+j} d\theta + \sum_{j=1}^n b_j \int (-\sin^2 \theta)^{i+j} (1 - \cos \theta) d\theta \\ = \int (-\sin^2 \theta)^i (1 - \cos \theta) d\theta, \end{aligned} \quad (38-a)$$

$$\sum_{j=1}^n a_j \int (-\sin^2 \theta)^{i+j} (1 - \cos \theta) d\theta + \sum_{j=1}^n b_j \int (-\sin^2 \theta)^{i+j} (1 - \cos \theta)^2 d\theta \quad (38-b)$$

$$\text{for } i = 1, 2, \dots, n. \quad = \int (-\sin^2 \theta)^i (1 - \cos \theta)^2 d\theta,$$

The integrals in the above equation can be calculated by the following integration table (Selby, 1971),

$$\int \sin^n x \, dx = -\frac{\sin^{n-1} x \cos x}{n} + \frac{n-1}{n} \int \sin^{n-2} x \, dx, \quad (39-a)$$

$$\int \sin^n x \cos x \, dx = \frac{1}{n+1} \sin^{n+1} x. \quad (39-b)$$

The solution of equation (38) gives the optimized one-way equation for each optimization angle θ . It is further split into a series of second-order equations, which may be solved by the conventional 45-degree migration algorithm.

The difficulty in the optimization is that equation (38) is ill-conditioned for the higher order equations. The double-precision computation employing 64 bits gives considerable error for optimization of the sixth-order and the eighth-order equations. Inversion of the ill-conditioned matrix is greatly affected by the number of significant digits. For this purpose, special Fortran subroutines are written, which compute addition, subtraction, multiplication, and division with arbitrary bits of precision. All of the computations for solving equation (38) is done by these subroutines.

Table 1 shows the optimized coefficients which are further split into a series of second-order equations given in equation (29). The sixth-order-or-less equations are computed with 100-bit precision; the eighth-order and tenth-order equations are computed with 200-bit and 300-bit precision, respectively. The first and second columns of the table represent the order of the equation and the maximum optimization angle. The third and fourth columns represent the numerator and denominator coefficients of the split equations.

The dispersion error of the optimized 2n-th order equation is given by

$$\Delta \frac{k_z}{k} = k \left(1 - \cos \theta - \sum_{i=1}^n \frac{d_i \sin^2 \theta}{1 - \beta_i \sin^2 \theta} \right). \quad (40)$$

The relative dispersion error is defined as Δk_z divided by the wave number k . Figure 3 shows the relative dispersion errors of the various one-way equations. M_2 through M_{10} are the errors in the optimized equations, the

subscripts of which represent the order. Y_2 is the error in the unmodified second-order equation, the conventional 45-degree equation. B_2 is the error in Berkhout's modified second-order equation. Berkhout's modified equation clearly is an improved version of the unmodified second-order equation. The optimized second-order equation (M_2) is better than B_2 . Note that two coefficients are modified in M_2 but only one coefficient is changed in B_2 .

Table 1.--Coefficients of optimized, fractioned one-way wave equations

Order	\emptyset	α_i	β_i
2	65	.478 242 060	.376 369 527
4	80	.040 315 157 .457 289 566	.873 981 642 .222 691 983
6	87	.004 210 420 .081 312 882 .414 236 605	.972 926 132 .744 418 059 .150 843 924
8	90	.000 523 275 .014 853 510 .117 592 008 .367 013 245	.994 065 088 .919 432 661 .614 520 676 .105 756 624
10	90	.000 153 427 .004 172 967 .033 860 918 .143 798 076 .318 013 812	.997 370 236 .964 827 992 .824 918 565 .483 340 757 .073 588 213

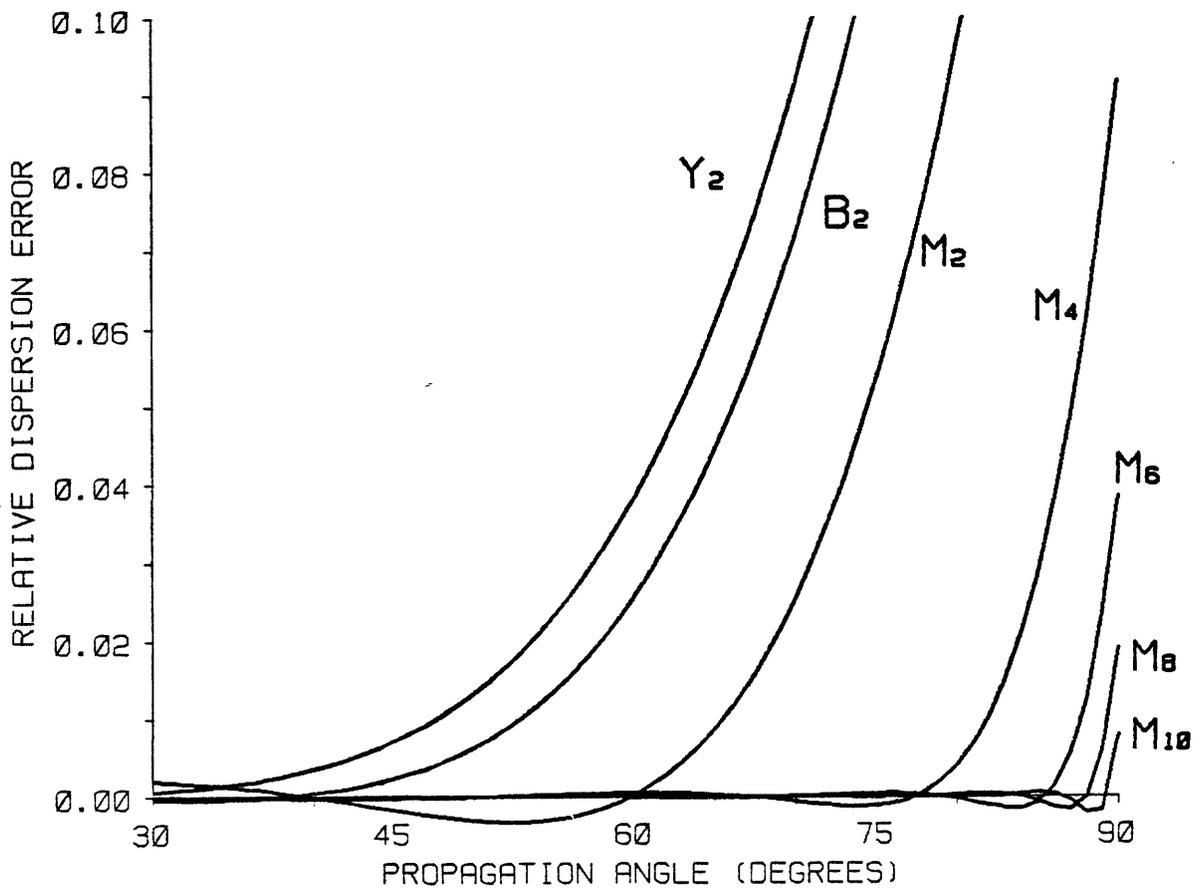


Figure 3.--Dispersion error in the optimized equations (M_2 through M_{10}), the conventional 45-degree equation (Y_2), and Berkhout's modified second-order equation (B_2).

The improvement of the optimization can be observed by comparing figures 2 and 3. Accepting the relative dispersion error limit of 1 percent, the second-order equation, which is accurate up to approximately 45 degrees in figure 2, is improved up to 65 degrees in figure 3. The fourth-order equation which is accurate up to 65 degrees in figure 2 is improved up to 82 degrees in figure 3. This behaviour can be observed in the eighth-order equation. The optimized tenth-order equation is accurate up to 90 degrees, which cannot be achieved by the 100th-order equation without the optimization. The validity for using the weighted error in the optimization procedure is established.

EXAMPLES

In this section, the optimized one-way wave equations are tested in three different examples. The first example is the extrapolation of a monochromatic cylindrical wave. The second example is the migration of a synthetic reflector model. The last example is the migration of field data.

Figure 4 is the result of monochromatic wave extrapolation by the finite-difference method. Figure 4A is computed by using the unmodified second-order equation. Figures 4B and 4C are computed by the optimized second- and fourth-order equation, respectively. The computational procedure is as follows. A two-dimensional (x, z) domain of 2,800 m by 1,200 m is divided by a regular grid having the intervals $\Delta x = \Delta z = 10$ m. With the origin on the upper left-hand corner of the domain, the grid index in x-direction (j) ranges from 0 to 280; while the grid index in z-direction (n) ranges from 0 to 120. A monochromatic wave source is located at $j = 80$ and $n = 0$. The wavelength is 100 m, which corresponds to the 30-Hz wave propagating through the 3-km/sec velocity medium. The theoretical solution of the wave is approximated by

$$(41)$$

where r is the distance from the source. The wave at the source is replaced by that of the adjacent grid point. Because of the spatial aliasing, the finite-difference method is not applicable near the source point. Therefore, the waves at $n = 1, 2$ and 3 are computed by equation (41). Waves at $n = 4$ through $n = 120$ are computed by the finite-difference method, the details of which are described in Appendix A. Figure 4 shows the real part of the wave field at even indices of j , $j = 0, 2, 4, \dots, 280$.

The accurate wave extrapolation should be represented by a semicircular wavefront. The amplitude should be inversely proportional to the square root of the distance from the source. The wavefront in figure 4A is not a perfect semicircle. The amplitude in figure 4A does not decay properly particularly in a 60-degree deviation from the vertical. These effects are caused by the error in the dispersion relation. Figure 4B shows better results than figure 4A, and figure 4C is better than figure 4B. The optimized second-order equation is better than the original second-order equation. The higher order equation is superior to the lower order equation. Figure 4C, which is computed by the optimized fourth-order equation, shows almost perfect results except for a minor amplitude anomaly in the upper-right corner. The results are anticipated from the previous discussion on one-way equations.

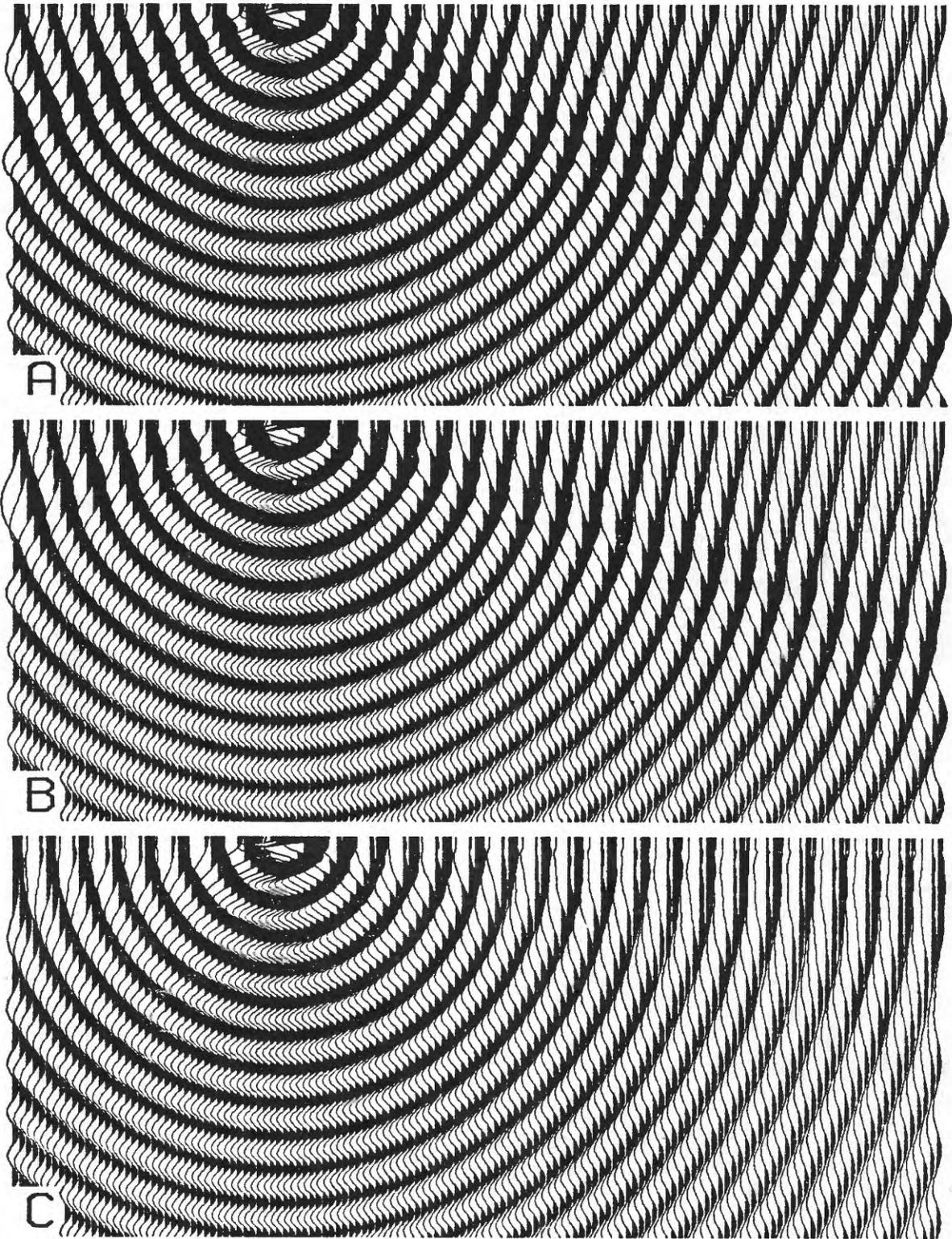


Figure 4.--Extrapolation of cylindrical wave by the conventional 45-degree equation (A), by the optimized second-order equation (B), and by the optimized fourth-order equation (C).

The result of extrapolation by the optimized sixth or higher order equation is almost the same as that by the optimized fourth-order equation. The minor amplitude error in the upper-right corner of figure 4C is not improved. This implies that factors other than the dispersion relation affect the high-angle extrapolation. It is apparent that one of the factors is the numerical error occurring from the derivative to the difference approximation. The split one-way equations resemble the second-order equation in the floating-time coordinate. In the floating-time coordinate, the apparent wave number in z-direction is less than the fixed-time coordinate for the propagation angle smaller than 60 degrees (Berkhout, 1980). If the propagation angle approaches 90 degrees, the zero apparent wavenumber in z-direction in the fixed-time coordinate increases to ω/v in the floating-time coordinate. The finite-difference approximation of P_z

described in Appendix A requires 18 or more grid points per one wavelength to give less than 1 percent approximation error. To handle a higher propagation angle, a more elaborate difference scheme is required. Otherwise, the grid interval Δz should be reduced. Another factor affecting high-angle extrapolation is the initial condition. Equation (41) is an asymptotic solution which is valid only if distance from the source is far greater than the wavelength. The minimum distance in figure 4 is 30 m, i.e., 0.3 times the wavelength. There must be considerable error in the initial condition.

Figure 5 is the newly computed result of wave extrapolation with a finer grid interval and improved initial condition. Figure 5A is computed by the optimized fourth-order equation. Figures 5B and 5C are computed by the optimized sixth- and eighth-order equations, respectively. In the computation, Δz is reduced to 5 m. The grid index in z-direction ranges from 0 to 240. To avoid the inaccurate initial condition, the finite-difference extrapolation starts from $n = 20$. The waves at $n = 0$ through $n = 19$ are computed by equation (41). The minimum distance from the source is now extended to 100 m which is the same as the wavelength. It is found that figure 5B is better than 5A, and 5C is better than 5B. The result shows that it is possible, at least theoretically, that high-angle extrapolation can be accomplished by the optimized high-order equations. The result by the optimized tenth-order equation is almost the same as the result by the optimized eighth-order equation. Figure 5 represents the propagation angle of up to 87 degrees.

Figure 6 is a synthetic reflector model for the migration test. The reflector is asymmetrically W-shaped, the leftmost segment representing a 70-degree dip, and the rightmost segment representing a 60-degree dip, respectively. Two segments in the central part simulate a 45-degree dip. There are four different velocities in the model, i.e., 2 km/sec, 3 km/sec, 3.5 km/sec, and 4 km/sec. The horizontal dimension of the model is 12.75 km and the vertical dimension is 6 km. This is not a realistic model, but it was chosen to test the migration algorithm for the steeply dipping events in the heterogeneous medium.

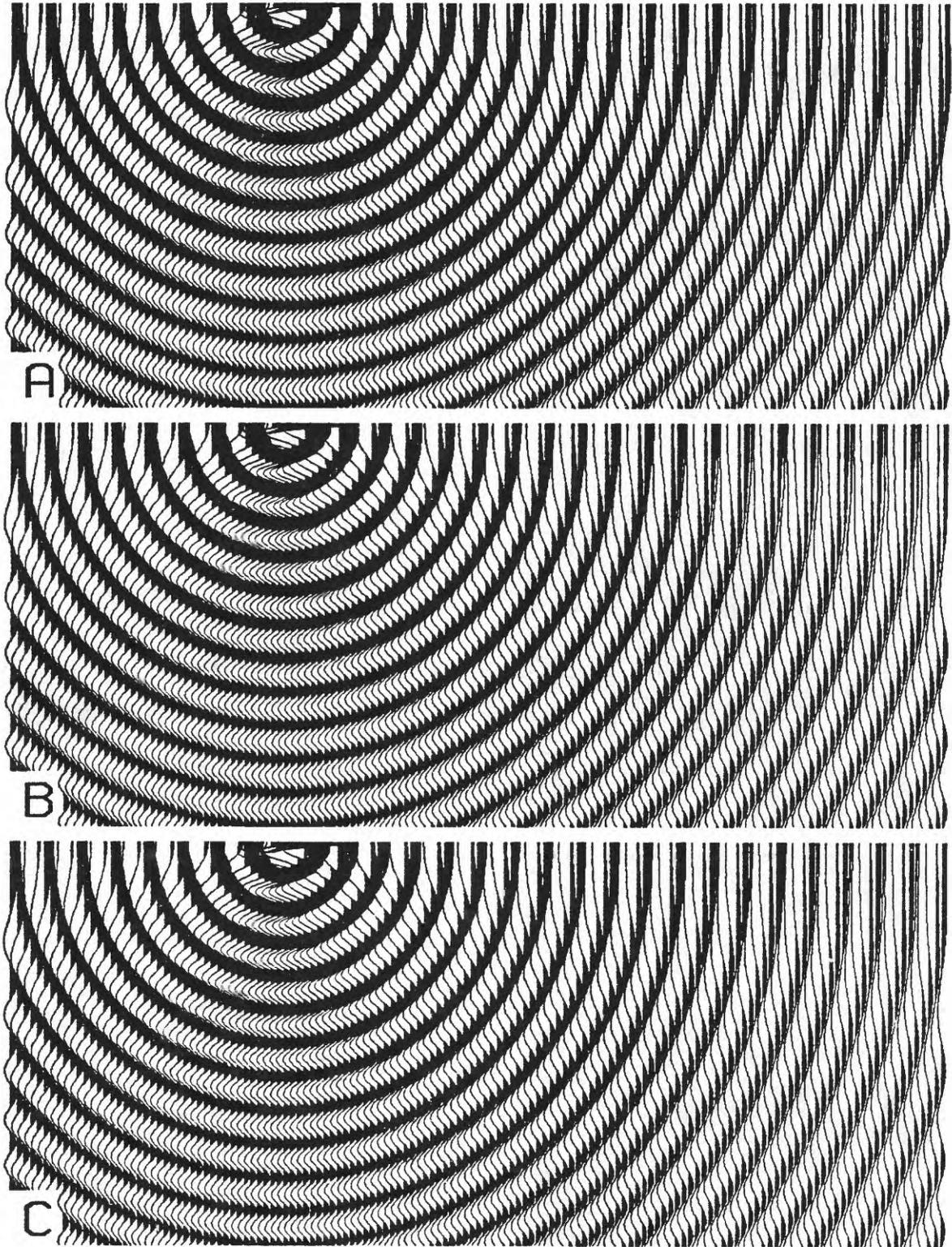


Figure 5.--Extrapolation of cylindrical wave with finer grid spacing by the fourth-order equation (A), sixth-order equation (B), and the eighth-order equation (C).

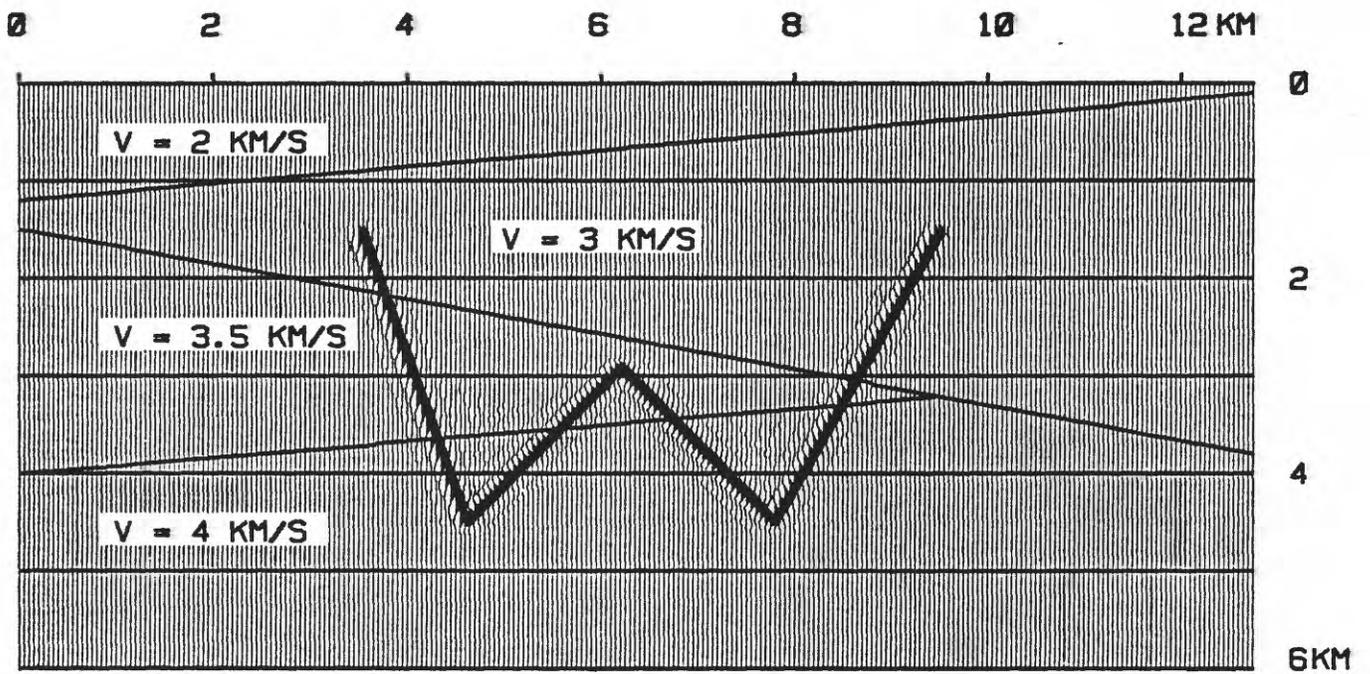


Figure 6.--A W-shaped reflector model simulating 45° , 60° , and 70° dips, simultaneously.

Figure 7 is a synthetic zero-offset section of figure 6. It was computed by the phase shift plus interpolation (PSPI) method (Gazdag and Sguazzero, 1984). In the computation, the grid interval is chosen as $\Delta x = \Delta z = 50$ m to give the number of grid points N_x and N_z by 256 and 121, respectively. The time increment Δt is 50 msec and the number of time samples N_t is 256. By taking N_x and N_t to the powers of two, the Fourier transforms required in the PSPI method is accomplished by the fast Fourier transform (FFT) routine. The PSPI method computes the diffraction which is difficult in the ray-tracing method. The dispersion relation of PSPI method approaches that of the exact square root equation as the number of reference velocities increases. The number of reference velocities used are four which is the same as that of the synthetic model. The computation should be accurate except in the region of the velocity boundary. The section shows a small amount of wrap-around effect, especially at the left-side boundary.

Figure 8 is the result of finite-difference migration of figure 7. Figure 8A is computed by the conventional 45-degree equation. Figures 8B and 8C are computed by the optimized second- and fourth-order equations, respectively. Figure 8A shows inaccurate migration except for the 45-degree dip reflector represented by the central part of W. Figure 8B shows better results than 8A. The 60-degree dipping segment on the right-hand side of W is almost accurately migrated in 8B. The 70-degree dipping segment is still distorted. Figure 8C, which is computed by the optimized fourth-order equation does not meet our anticipation satisfactorily. Although the 70-degree dipping segment is more accurately migrated in figure 8C than in 8B, it still shows a considerable amount of phase error and minor amplitude error. From the previous dispersion analysis, the equation should handle up to 80 degrees. The inaccuracy in the migration may be summarized as follows.

The amplitude error is primarily due to abrupt changes in velocity both in the synthesis of the zero-offset section and in the migration. The lateral velocity variation should be smooth to get an accurate synthetic section by the PSPI method. To make the velocity variation smooth, a high cut filter should be applied on the velocity boundary. This will give us many velocities in the filtered model, which require a number of reference velocities in the PSPI method. The computation time by the PSPI method increases almost linearly to the number of reference velocities. It took about 3,000 CPU seconds by the VAX 11/780 computer to produce figure 7 using four reference velocities.

The phase error, which is more significant than the amplitude error, in the migrated result in figure 8 is due to the numerical error occurring from derivative to difference approximation. In the migration, the spatial grid intervals Δx and Δz are 50 m. The time interval Δt is 50 msec. A 10 Hz signal propagating through the model having the average half velocity of 1,500 m/sec has a wavelength of 150 m. Therefore, the spatial grid interval of 50 m is too gross for the wavelength.

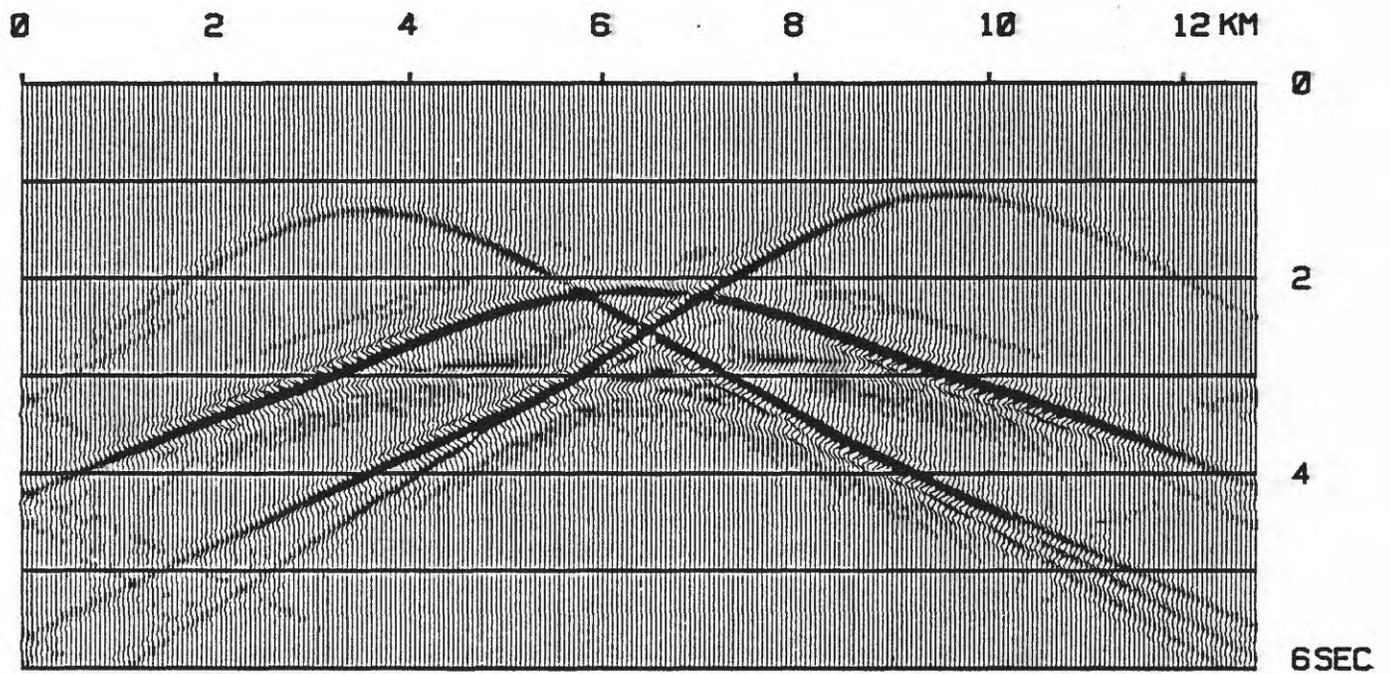


Figure 7.--Synthetic zero-offset time section of figure 6.

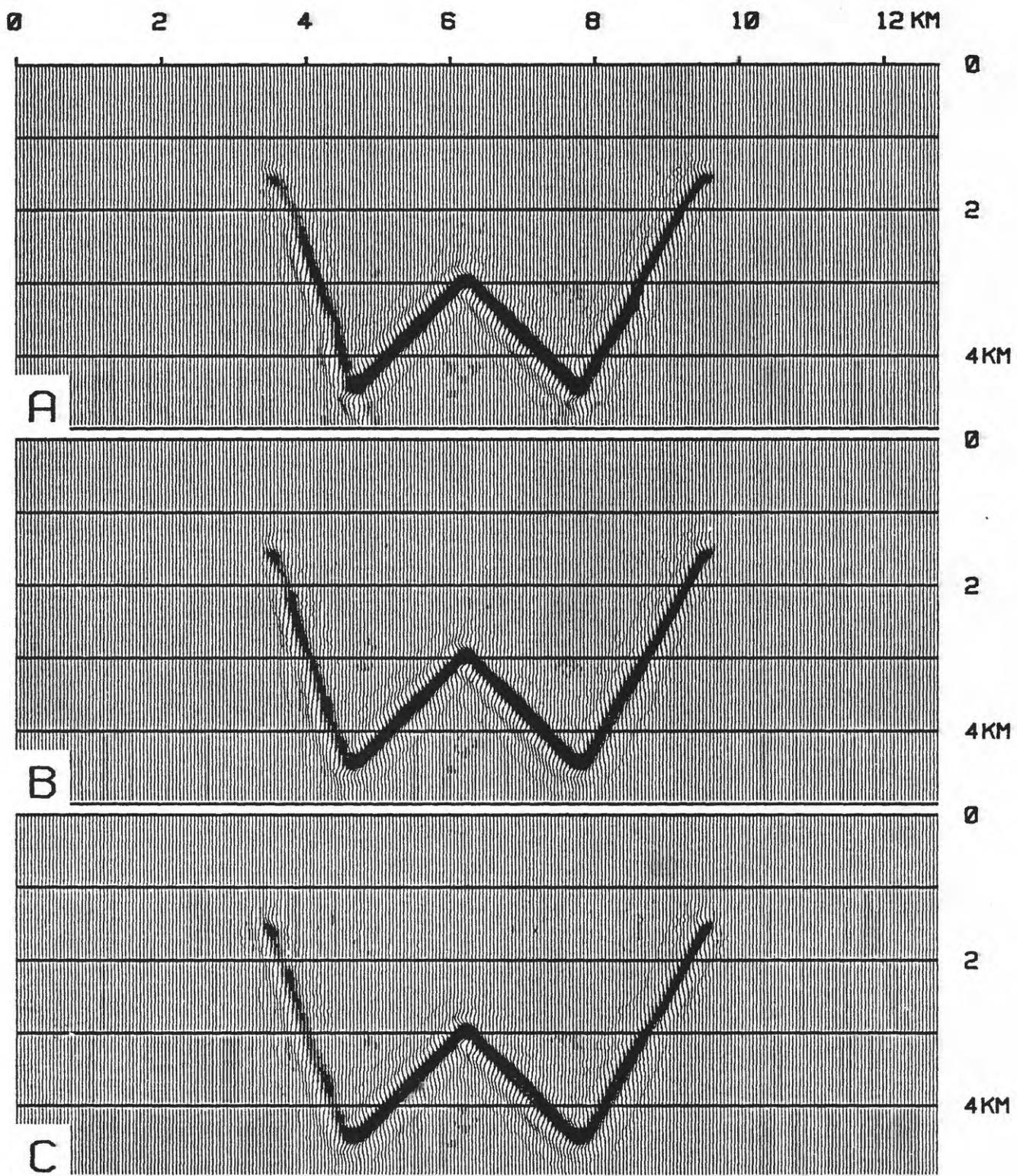


Figure 8.--Finite-difference migration of figure 7 by the conventional 45-degree equation (A), the optimized second-order equation (B), and the optimized fourth-order equation (C).

To accurately approximate the derivatives to differences within a 1 percent limit, the finite-difference method described in Appendix A requires about five grid points in x-direction and about eighteen grid points in z-direction, respectively. Therefore, the spatial grid intervals Δx and Δz should be reduced to less than 30 m and 10 m, respectively. The reduction gives us an increase in the number of grid points about ten times that of the previous grid points. It took approximately 2,640 CPU seconds by the VAX 11/780 computer to migrate figure 7 by the fourth-order equation with 50 m grid spacing. Migration with finer grid spacing will take hours of CPU time and days of clocktime by a time-sharing computer. The problem of computing time may be reconciled by using an array processor. The next example is actually computed by the array processor.

Figure 9 is a stacked section. The data were collected at Block 7 of the Korean continental shelf in 1980 and were processed using the seismic data processing facilities of the U.S. Geological Survey. The main hardware of the facility consists of a VAX 11/780 computer and FPS-120B array processors. The operating seismic software is DISCO (Digicon's Interactive Seismic Computer). The common depth point (CDP) interval of figure 9 is 25 m, the number of traces are 501, and the horizontal dimension is 12.5 km.

Figure 10 shows the migrated section of figure 9 by employing the optimized second-order equation. The stacking velocity produced by NMO analysis is directly used for the migration. As the stacking velocity is given in the time domain, the time migration algorithm is applied. The variable z in the depth migration is replaced by the two-way travel time of the image ray. The extrapolation step of the migration Δt is 48 msec. The maximum frequency is 40 Hz. To speed up the computation, almost all of the migration algorithm is written in the assembler language of the array processor. The computing time of figure 10 is 59 CPU seconds and 271 AP seconds.

Figure 9 contains considerable noise in the lower half of the section. The noise is primarily considered as the P-S converted wave. Therefore, it is hardly expected that a good migrated result in that portion will be achieved. On the contrary, the upper half of the section shows relatively good signal-to-noise ratio. The effect of migration is well observed in figure 10. Several diffractions are nicely focused. The bowtie at 5 km and on 1.3 sec in figure 9 is successfully migrated to give the syncline structure in figure 10.

CONCLUSION

One of the disadvantages in the finite-difference migration is that it cannot handle a steep-dip structure. This is due to the inaccurate dispersion relation of the one-way wave equation utilized in the scheme. In this paper, an optimization method is studied in order to improve the dispersion relation of the implicit one-way wave equations. The basic concept of the optimization is modifying the coefficients, which has been attempted by Berkhout (1979) and Ma (1981). In our optimization, all of the adjustable coefficients are subject to the modification, i.e., the number of optimized coefficients is the same as the order of the one-way equation.

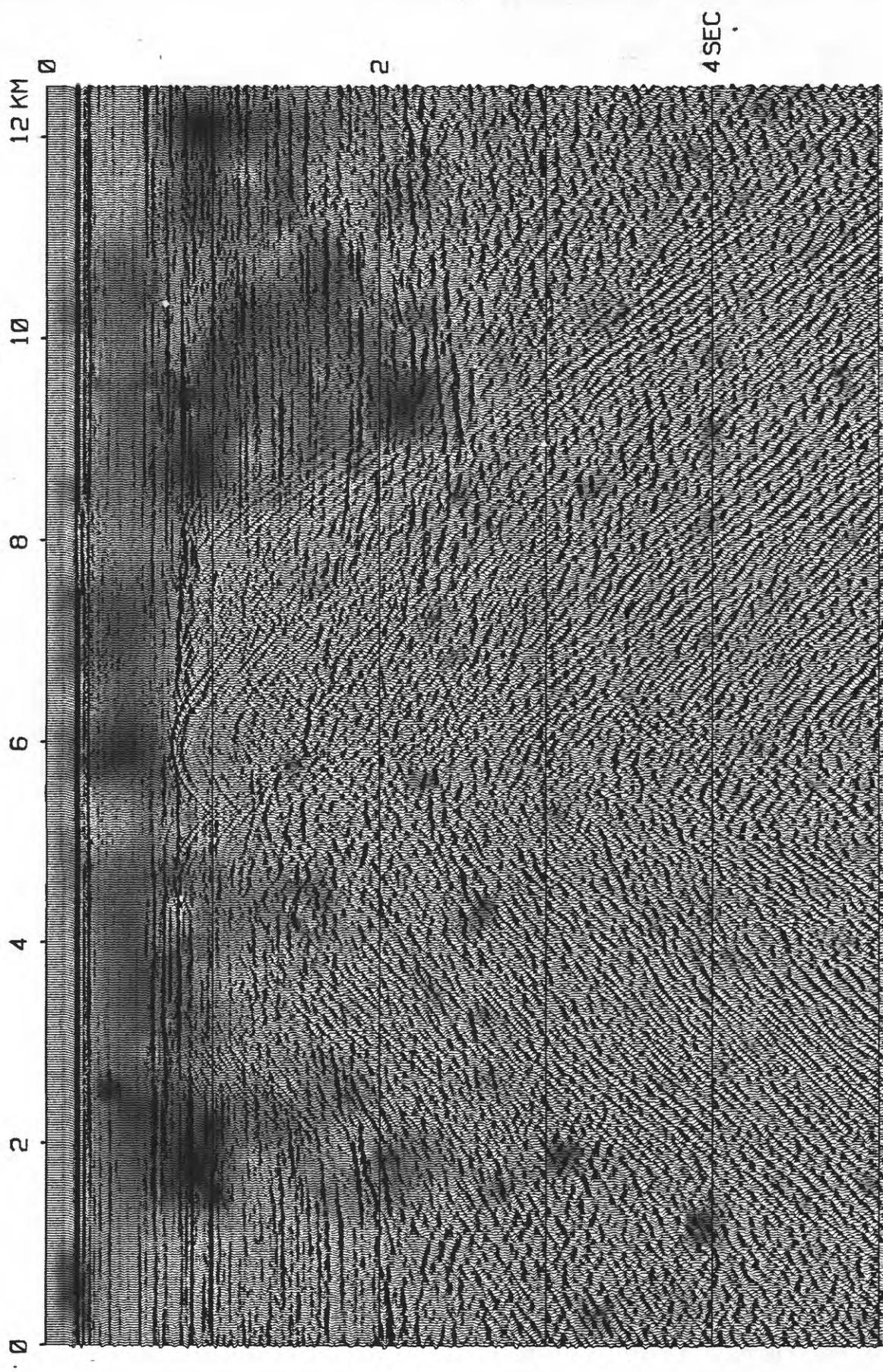


Figure 9.--CMP stack of a Korean offshore line.

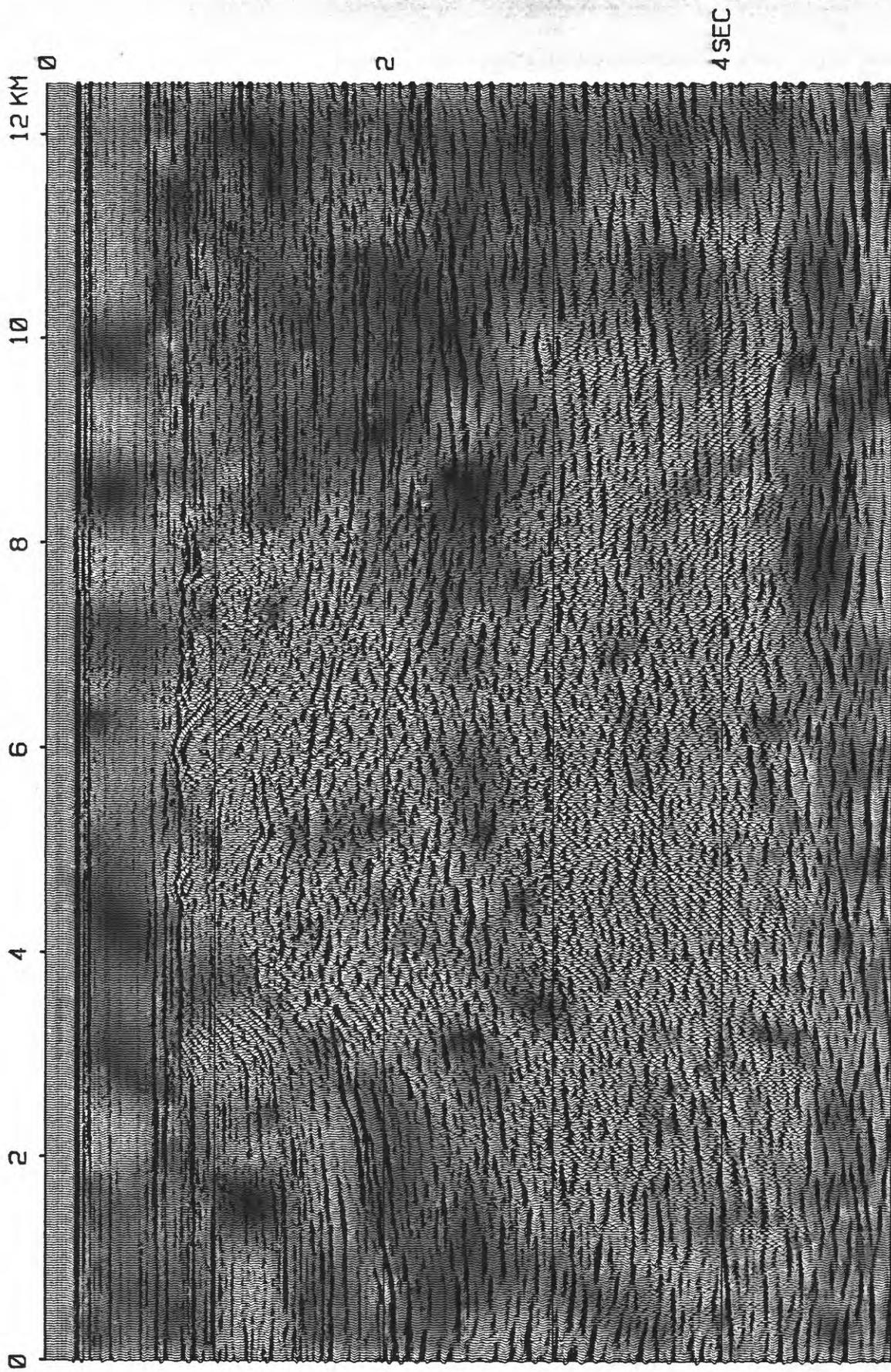


Figure 10.--Finite-difference time migration of figure 9 by the optimized second-order equation.

A least squares method, which minimizes the weighted dispersion error, is investigated. By introducing the weighted error, the least-squares method is reduced to the linear problem. Optimized coefficients are computed for up to the tenth-order equation. Each of the optimized equations shows significantly improved dispersion relation over the corresponding unoptimized equation. Using the optimized equations, the steep-dip migration can be achieved accurately without going to the higher order equation.

The optimized equations are tested on three examples. The first example is on the extrapolation of the monochromatic cylindrical wave. In the example, the optimized second-order equation shows better results than the unoptimized second-order equation which is known as the 45-degree equation. The computing times by the two equations are exactly the same. The optimized higher order equations show substantially better results than the lower order equations. The second example which is on the migration of a synthetic model, shows similar results. A stack section is migrated by the optimized second-order equation. The result is considered as acceptable.

The extrapolation of high-angle waves requires suppression of numerical error occurring from the derivative to the difference approximation as well as the one-way equations having accurate dispersion relation up to that angle. One of the methods of suppressing the numerical error is by working with finer grid intervals. Use of a finer grid interval will result in many hours of computing time. A method should be developed to control the numerical error effectively.

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APPENDIX A. Finite-Difference Formulation of the One-Way Equation.

A $2n$ -th order implicit equation is split into n second-order implicit equation. Therefore, it is sufficient to describe the solution method of the second order equation which is given by

$$P_j = i \frac{\omega}{v} \frac{\alpha \partial_{xx}}{k^2 + \beta \partial_{xx}} P. \quad (A-1)$$

A two-dimensional wave field is defined on (x, z) domain. The domain is divided into a regular grid, the intervals of which are Δx and Δz . The wave field at an intersection, $P(j\Delta x, N\Delta z)$ is denoted by P_j^n . The problem of extrapolation is to find wave P_j^{n+1} ($j = 0, 1, \dots, J$) from the given P_j^n ($j = 0, 1, \dots, J$). The finite-difference method employs the difference approximation of equation (A-1).

The z -derivative in equation (A-1) is approximated by

$$\partial_z \approx \frac{z}{\Delta z} \frac{\delta_z}{r_z} \quad (A-2)$$

where

$$\delta_z f(z) = f(z+\Delta z) - f(z)$$

$$r_z f(z) = f(z+\Delta z) + f(z)$$

This is an expression of Crank-Nicolson's scheme of the finite-difference method. The x -derivative in equation (A-1) is approximated by

$$\partial_{xx} \approx \frac{1}{(\Delta x)^2} \frac{\delta_{xx}}{1 + 1/2 \delta_{xx}} \quad (A-3)$$

where

$$\delta_{xx} f(x) = f(x+\Delta x) - 2f(x) + f(x-\Delta x).$$

Equation (A-2) is accurate within 1 percent if 18 or more grid points exist per one wavelength. Equation (A-3) is accurate within 1 percent if 5 or more grid points exist per one wavelength (Claerbout, 1976). Substituting equations (A-2) and (A-3) to equation (A-1) gives

$$2 \delta_z \left[k^2 \Delta x^2 + (\beta + k^2 \Delta x^2 / 12) \delta_{xx} \right] P_j^n = i k \alpha \Delta z r_z \delta_{xx} P_j^n \quad (A-4)$$

Expanding equation (A-4) in z index gives

$$2 \left[k^2 \Delta x^2 + (\beta + k^2 \Delta x^2 / 12) \delta_{xx} \right] (P_j^{n+1} - P_j^n) = i k \alpha \Delta z \delta_{xx} (P_j^{n+1} + P_j^n). \quad (A-5)$$

Expanding equation (A-5) in x index gives

$$A_j P_{j-1}^{n+1} + B_j P_j^{n+1} + C_j P_{j+1}^{n+1} = D_j \quad (A-6)$$

where

$$A_j = 2 \left(\beta + k^2 \Delta x^2 / 12 \right) - i k d \Delta z$$

$$B_j = 2 \left[k^2 \Delta x^2 - 2 \left(\beta + k^2 \Delta x^2 / 12 \right) \right] + 2 i k d \Delta z$$

$$C_j = A_j$$

$$D_j = A_j^* P_{j-1}^n + B_j^* P_j^n + C_j^* P_{j+1}^n,$$

for $j = 1, 2, \dots, J-1$,

where A_j^* , B_j^* , and C_j^* indicate the complex conjugate of A_j , B_j , and C_j , respectively.

Equation (A-6) gives $J-1$ equations for $J+1$ unknowns. The remaining two equations are given from the boundary conditions. A conventional boundary condition such as Dirichlet or Neumann is subject to artificial reflections at the boundary. To suppress the artificial reflections, Clayton and Engquist (1980) suggest

$$P_z = i \frac{\omega}{v} \frac{a + b \partial_x / k}{1 + c \partial_x / k} P \quad (\text{A-7})$$

in the fixed-time coordinate. The coefficients a , b , and c are determined so that the dispersion relation of equation (A-7) approximates the quarter circle. The boundary condition for equation (A-1) may be in the form of

$$P_z = i \frac{\omega}{v} \frac{d \partial_x}{k + c \partial_x} P \quad (\text{A-8})$$

where the coefficients c and d are determined as the dispersion relation approximates to one-half that of the interior. If it approximates $+k_x$ axis,

it is used at the $+x$ boundary; if it approximates $-k_x$ axis, it is used at

the $-x$ boundary. The coefficients are found by the least squares method which is very similar to the optimization of one-way equations.

The finite-difference formulation of equation (A-9) uses equation (A-2). The formulation at $x = 0$ boundary is

$$(k \Delta x + 2c \delta_x) \delta_z P_0^n = i k d \Delta z \delta_x \gamma_z P_0^n \quad (\text{A-9})$$

Expanding equation (A-9) in the z index gives

$$(k \Delta x + 2c \delta_x) (P_0^{n+1} - P_0^n) = i k d \Delta z \delta_x (P_0^{n+1} + P_0^n) \quad (\text{A-10})$$

Expanding equation (A-10) in x index gives

$$B_0 P_0^{n+1} + C_0 P_1^{n+1} = D_0 \quad (\text{A-11})$$

where

$$B_0 = k\Delta x - 2C + ikd\Delta z$$

$$C_0 = k\Delta x + 2C - ikd\Delta z$$

$$D_0 = B_0^* P_0^n + C_0^* P_0^n$$

The finite-difference equation at $x = J\Delta x$ boundary can be derived by changing the subscripts as 0 to J and 1 to J-1, and the coefficients C to A as

$$A_J P_{J-1}^{n+1} + B_J P_J^{n+1} = D_J \quad (\text{A-12})$$

where

$$A_J = k\Delta x + 2C - ikd\Delta z$$

$$B_J = k\Delta x - 2C + ikd\Delta z$$

$$D_J = A_J^* P_{J-1}^n + B_J^* P_J^n$$

Equation (A-11) is added to the top of equation (A-6) and equation (A-12) is appended to the bottom of equation (A-6). Introducing vectors \underline{P}^{n+1} and \underline{D} which represent P_j^{n+1} and D_j ($j = 0, 1, \dots, J$), the result will be

$$\underline{M} \underline{P}^{n+1} = \underline{D} \quad (\text{A-13})$$

where matrix \underline{M} is given by a tridiagonal matrix as

$$\underline{M} = \begin{pmatrix} B_0 & C_0 & & & & & & & \text{Zero} \\ A_1 & B_1 & C_1 & & & & & & \\ & A_2 & B_2 & C_2 & & & & & \\ & & & \ddots & \ddots & & & & \\ & & & & A_{J-1} & B_{J-1} & C_{J-1} & & \\ \text{Zero} & & & & & B_J & C_J & & \end{pmatrix}$$

The solution to equation (A-13) may be found by introducing an auxiliary equation

$$P_{J-1}^{n+1} = E_J P_J^{n+1} + F_J P_{J+1}^{n+1} \quad (\text{A-14})$$

Coefficients E_j and F_j are found by comparing the coefficients to equation

(A-13). The unknowns are then computed by backward substitution (Claerbout, 1976).

APPENDIX B. CPU Version of the Migration Program

This program computes a depth-migrated section from a zero-offset seismic section. The name of the program is FXZMIG. It is written in Fortran 77 language. Five files are referenced by the program. The first file is named by FXZMIG.DAT and is intended for reading the input parameters only. A more thorough description on the parameters may be found later. The second file is the trace file containing the zero-offset seismic section. The format of the file is UNFORMATTED, i.e., the information is represented by the internal format. Each trace consists of one record. There is no header in the trace, i.e., the file should contain amplitude information only. The third file is the velocity file containing the migration velocities in (x, z) domain. Like the trace file, it is UNFORMATTED and has no header. The velocity should be defined at every trace and at every depth step. The fourth file is named by FXZMIG.OUT and will contain the migrated result in (x, z) domain after the successful run of the program. The last file is a scratch file intended for the program internally.

Four lines of input parameters are required for the program to run. The first line defines six parameters: NX, NZ, NT, DX, DZ, and DT. NX is the number of traces; NZ, the number of depth steps; NT, the number of time samples; DX and DZ, the spatial intervals in meters; and DT, the temporal interval in msec. The second line defines two parameters, NESTDR and WPCNT. NESTDR represents the order of the one-way equation which will be used for the migration. The number indicates half of the order, i.e., 1 is the optimized second order, 2 is the optimized fourth order, and so on. It should not exceed 5. If NESTDR is less than 1, the conventional 45-degree equation will be used for the migration. WPCNT is a parameter for the numerical dip-filter. If it is 0, no dip-filter will be applied. The dip-filter algorithm may be found in Claerbout (1976).

The third line describes two parameters, SW1 and SW4, i.e., the lowcut and highcut frequencies, respectively, in Hz. The highcut frequency should not exceed Nyquist frequency. The fourth line defines the name of two input files, i.e., the velocity file and the trace file. All the lines should be physically separated by a carriage return for an interactive job. For a batch job, the lines must be on separate cards. The parameters within a line should be separated by a comma and/or spaces, i.e., in free format of the Fortran language. Each file name should be enclosed in a pair of apostrophies. The following example shows the input parameters used in the computation of figure 8C.

Example of the input parameters

256	120	130	50	50	50
2	0				
1	9				

'VEL008', 'MDLPHS.OUT'

The program statements are as follows.

```

C      * * * * *
C
C      PROGRAM ** F X Z M I G ** VERSION HG.3 SEP/28/84
C
C      FINITE-DIFFERENCE WAVE EQUATION MIGRATION IN (F,X,Z) DOMAIN
C
C      * * * * *
C
C      PROGRAM FXZMIG
C
C      INCLUDE 'FXZMIG.CMB/LIST'
C
C      CONETENTS OF FILE FXZMIG.CMB
C
COMMON / BLK1 /
1  NX,          ! NO. OF TRACES,
2  NZ,          ! NO. OF SAMPLES
3  NT,          ! NO. OF TIME SAMPLES,
4  DX,          ! TRACE INTERVAL,
5  DZ,          ! Z-STEP INTERVAL,
6  DT,          ! SAMPLING TIME,
7  NX2,NY,NX1, ! NX*2, NX-2, NX-1,
8  NTFRT,       ! FFT LENGTH IN TIME,
9  NW,DW,       ! NO. OF FREQUENCIES, AND INCREMENT,
A  SW0,SW1,SW4, ! START(SW0,SW1) AD END(SW4) FRQUENCIES
B  WIMAG,AMIMAG ! DIP-FILTER PARAMETERS

COMMON / BLK2 /
1  EXTBUFF(12,5), ! EXTRAPOLATION MATRIX,
2  BNDBUFF(2,5), ! BOUNDARY MATRIX
3  NESTDR         ! ORDER OF THE NEST

CHARACTER*56 FILVEL, FILTRC
COMMON / BLKF / FILVEL, FILTRC

PARAMETER
1  LDVVEL = 11, ! VELOCITY FILE
2  LDVTRC = 12, ! TRACE FILE
3  LDVMIG = 13 ! MIGRATED OUTPUT

END OF FILE FXZMIG.CMB

DIMENSION BUF (320 000)
DATA MAXBFS / 320 000 /

CALL GETCRD
CALL ALCMEM (MAXBFS, IV, IM, JM, IA, IB, IC, ID, IQ)
CALL EDTVEL (BUF)
CALL TM2FRQ (BUF, BUF(IQ))
CALL EXTCON
CALL MLTSTP (BUF(IV), BUF(IM), BUF(JM), BUF(IA), BUF(IB),
+          BUF(IC), BUF(ID), BUF(IQ))
CALL OUTPUT (BUF)
STOP 'NORMAL COMPLETION'
END

```

```

SUBROUTINE GETCRD                                57
C                                                    58
C READ INPUT DATA FROM CARD.                    59
C                                                    60
C INCLUDE 'FXZMIG.CMB/NOLIST'                    61
C                                                    62
C READ/WRITE SECTION.                            63
C                                                    64
OPEN (UNIT = 5, FILE = 'FXZMIG', TYPE = 'OLD', READONLY) 65
WRITE (6, 60)                                     66
READ (5, *) NX, NZ, NT, DX, DZ, DT              67
WRITE (6, 62) NX, NZ, NT, DX, DZ, DT           68
READ (5, *) NESTDR, WPCNT                       69
WRITE (6, 64) NESTDR, WPCNT                    70
READ (5, *) SW1, SW4                             71
WRITE (6, 66) SW1, SW4                         72
READ (5, *) FILVEL, FILTRC                      73
WRITE (6, 68) FILVEL, FILTRC                   74
CLOSE (5)                                        75
C                                                    76
C FORMAT SECTION                                  77
C                                                    78
60 FORMAT (1H1///35(' *')//)                    79
1 ' WELCOME TO *** F X Z M I G ***'5X'VERSION HG.3'/ 80
2 ' FINITE-DIFFERENCE WAVE EQ. MIGRATION IN (F,X,Z)', 81
3 ' DOMAIN'// 35(' *')//                        82
4 ' INPUT DATA SUMMARY'//                      83
62 FORMAT (T9'NX'T19'NZ'T29'NT'T38'DX'T49'DZ'T59'DT'/ 84
+ 3I10, 3F10.1)                                 85
64 FORMAT ('0'T5'NESTDR'T16'WPCNT'/ I10,F10.1) 86
66 FORMAT ('0'T8'SF1'T18'SF4' / 2F10.1)        87
68 FORMAT ('0 FILVEL =',2X,A/' FILTRC =',2X,A) 88
C                                                    89
C PARAMETER EXAMINATION SECTION                  90
C                                                    91
NX2 = NX + NX                                   92
NY = NX - 2                                     93
NX1 = NX - 1                                   94
DT = DT / 1000.                                95
NTFFT = KPOWR2 (NT)                            96
FNYQ = 0.5 / DT                                97
C                                                    98
IF (SW1.GE.SW4 .OR. SW4.GT.FNYQ) STOP 'ERROR IN SFRQ' 99
C                                                    100
C                                                    101
C                                                    102
PI = ACOS (-1.)                                102
DW = 2. * PI / (NTFFT * DT)                    103
SW1 = 2. * PI * SW1                             104
SW4 = 2. * PI * SW4                             105
C                                                    106
IW1 = SW1 / DW + 1.0                            107
IW4 = SW4 / DW - 0.5                            108
NW = IW4 - IW1 + 1                              109
SW0 = DW * IW1                                  110
SWMAJ = (SW1 + SW4) / 2.                        111
WIMAG = - WPCNT * SWMAJ / 100.                 112

```

	RETURN	113
	END	114
	 SUBROUTINE ALCMEM (MAXBFS, IV, IM, JM, IA, IB, IC, ID, IQ)	115
C		116
C	ALLOCATE MEMORY OF THE GLOBAL BUFFER AND	117
C	CHECK THE MAXIMUM BUFFER SIZE.	118
C		119
	INCLUDE 'FXZMIG.CMB/NOLIST'	120
C		121
	IV = 1 ! VBUF START ADDRESS	122
	IM = IV + NX ! AMBUF	123
	JM = IM + NX ! AM2BUF	124
	IA = JM + NX ! ABUF	125
	IB = IA + NX2 ! BBUF	126
	IC = IB + NX2 ! CBUF	127
	ID = IC + NX2 ! DBUF	128
	IQ = ID + NX2 ! QBUF	129
	IQ = MAX0 (IQ, IV + NTFFT*2 - 1)	130
	NBFEXT = IQ + NX2 * NW - 1	131
	NBFDMX = NX * NZ	132
	NBFREQ = MAX0 (NBFEXT, NBFDMX)	133
C		134
	IF (NBFREQ .GT. MAXBFS) STOP 'INSUFFICIENT BFS'	135
	RETURN	136
	END	137
	 SUBROUTINE MLTSTP (VBUF, AMBUF, AM2BUF, ABUF, BBUF, CBUF, DBUF, QBUF)	138
		139
+		140
C		141
C	MULTISTEP EXTRAPOLATION AND IMAGING.	142
C		143
	INCLUDE 'FXZMIG.CMB/NOLIST'	144
	COMPLEX QBUF(NX,NW)	145
	DIMENSION VBUF(NX)	146
C		147
C		148
	REWIND LDVVEL	148
	OPEN (UNIT = LDVMIG, FILE = 'FXZMIG.OUT', FORM = 'UNFORMATTED',	149
+	TYPE = 'UNKNOWN')	150
	CALL IMAGEZ (QBUF, ABUF)	151
	DO 20 IZ = 2, NZ	152
	READ (LDVVEL) VBUF	153
	DO 10 JW = 1, Nw	154
	SW = SW0 + DW * (JW - 1)	155
	CALL VSMULT (NX, VBUF, SW, AMBUF)	156
10	CALL EXTPOL (QBUF(1,JW), ABUF, BBUF, CBUF, DBUF, AMBUF, AM2BUF)	157
	CALL IMAGEZ (QBUF, ABUF)	158
	TYPE *, IZ, '-TH STEP COMPLETED'	159
20	CONTINUE	160
	RETURN	161
	END	162

	SUBROUTINE TM2FRQ (BUF, QBUF)	163
C		164
C	GET TIME-DOMAIN DATA, TRANSFORM, AND SAVE ON QBUF IN	165
C	DEMULTIPLICED FORM.	166
C		167
	INCLUDE 'FXZMIG.CMB/NOLIST'	168
C		169
	COMPLEX QBUF(NX,NW)	170
C	DIMENSION BUF(NTFFT*2)	171
	DIMENSION BUF(2)	172
C		173
	OPEN (UNIT = LDVTRC, FILE = FILTRC, FORM = 'UNFORMATTED',	174
+	TYPE = 'OLD', READONLY)	175
	NT2 = NT + NT	176
	NTFFT2 = NTFFT + NTFFT	177
	IW1 = 2 * IFIX(SW0 / DW + 0.5) + 1	178
C		179
	DO 10 IX = 1, NX	180
	CALL STORE (NTFFT2, BUF, 0.)	181
	READ (LDVTRC) (BUF(J), J = 1, NT2, 2)	182
	CALL FFTC (NTFFT, BUF, 1.)	183
	CALL MOVEJC (NW, BUF(IW1), QBUF(IX,1), 1, NX)	184
10	CONTINUE	185
	CLOSE (LDVTRC)	186
	RETURN	187
	END	188
	SUBROUTINE OUTPUT (BUF)	189
	INCLUDE 'FXZMIG.CMB/NOLIST'	190
	DIMENSION BUF(NX,NZ)	191
	REWIND LDVMIG	192
	DO 10 JZ = 1, NZ	193
10	READ (LDVMIG) (BUF(IX,JZ), IX = 1, NX)	194
	REWIND LDVMIG	195
	DO 20 IX = 1, NX	196
20	WRITE (LDVMIG) (BUF(IX,JZ), JZ = 1, NZ)	197
	RETURN	198
	END	199
	SUBROUTINE IMAGEZ (QBUF, BUF)	200
C		201
C	IMAGE THE MIGRATED WAVE FILED	202
C		203
	INCLUDE 'FXZMIG.CMB/NOLIST'	204
C		205
	COMPLEX QBUF(NX, NW)	206
	DIMENSION BUF(NX)	207
C		208
	DO 10 IX = 1, NX	209
	CALL SUMVJ (NW, QBUF(IX,1), BUF(IX), NX2)	210
10	CONTINUE	211
	WRITE (LDVMIG) (BUF(IX), IX = 1, NX)	212
	RETURN	213
	END	214

```

SUBROUTINE EXTPOL (QBUF, ABUF, BBUF, CBUF, DBUF, AMBUF, AM2BUF) 215
C 216
C 217
C 218
INCLUDE 'FXZMIG.CMB/NOLIST' 219
COMPLEX QBUF(NX), ABUF(NX),BBUF(NX),CRUF(NX),DBUF(NX) 220
COMPLEX XTINER, XTOUTR 221
DIMENSION AMBUF(NX) 222
C 223
CALL VVMULT (NX, AMBUF, AMBUF, AM2BUF) 224
DO 10 K = 1, NESTDR 225
CALL CFBND2 (AMBUF, BBUF(1), XTINER, XTOUTR, BNDDBUF(1,K)) 226
ABUF(1) = XTINER * QBUF(2) + XTOUTR * QBUF(1) 227
CALL CFBND2 (AMBUF(NX), BBUF(NX), XTINER, XTOUTR, BNDDBUF(1,K)) 228
ABUF(NX)= XTINER * QBUF(NX1) + XTOUTR * QBUF(NX) 229
CALL CFINT2 (CBUF, ABUF, DBUF, BBUF, EXTBUF(1,K), AMBUF,AM2BUF) 230
CALL CVAMMA (NY, QBUF,QBUF(3), CBUF(2), QBUF(2), DBUF(2), 231
+ DBUF(2)) 232
CALL TRIDGX (NX, QBUF, ABUF, BBUF, DBUF) 233
10 CONTINUE 234
C 235
DO 20 IX = 1, NX 236
20 QBUF(IX) = QBUF(IX) * CEXP (CMPLX (0., DZ * AMBUF(IX))) 237
RETURN 238
END 239

SUBROUTINE CFINT2 (CLF, CNF, CLD, CND, CFM, AMB, AM2) 240
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CALL VSMULJ (NY, AMB(2), CFM(3,4), CND(4), 1, 2)          269
C                                                         270
RETURN                                                    271
END                                                       272

SUBROUTINE CFBND2 (AMREAL, XTRATE, XTINER, XTOUTR, BCOF)    273
C                                                         274
C COMPUTE TRANSPARENT BOUNDARY COEFFICIENTS(XTRATE,XTINER,XTOUTR) 275
C SEE PAGE 40-R EG. (11)                                   276
C                                                         277
INCLUDE 'FXZMIG.CMB/NOLIST'                               278
COMPLEX EYEB, XTRATE, XTINER, XTOUTR, CMDZ, CAMX, CSCALE, CAM 279
DIMENSION BCOF(2)                                         280
C                                                         281
C                                                         282
ADX      = BCOF(1) * DX                                   283
EYEB     = CMPLX (0., 2. * BCOF(2))                       284
CAM      = CMPLX (AMREAL, AMIMAG)                         285
CMDZ     = CAM * DZ                                       286
CAMX     = CAM * ADX                                       287
CSCALE  = 1. / (CMDZ + CAMX + EYEB)                       288
XTRATE  = CSCALE * (CMDZ - CAMX + EYEB)                   289
XTINER  = CSCALE * (CMDZ + CAMX - EYEB)                   290
XTOUTR  = CSCALE * (-CMDZ + CAMX + EYEB)                  291
RETURN                                       292
END                                           293

SUBROUTINE CFINTI (CFM, B, C, DFCNMR, ALPHA)              294
C                                                         295
C INITIALIZE CFM(3,4) EXTRAPOLATION MATRIX GIVEN IN P42-R 296
C EQ. (10A).                                              297
C                                                         298
C DEFINITION OF THE EXTRAPOLATION MATRIX : CFM(3,4)     299
C                                                         300
CFM(1,J) : CONSTANT TERM                                 301
CFM(2,J) : COEFF. OF AM * AM                             302
CFM(3,J) : COEFF. OF I * AM                             303
J = 1    : OLD/OFF-DIAGONAL                             304
J = 2    : NEW/OFF-DIAGONAL                             305
J = 3    : OLD/DIAGONAL                                  306
J = 4    : NEW/DIAGONAL                                  307
INCLUDE 'FXZMIG.CMB/NOLIST'                               308
DIMENSION CFM(3,4)                                       309
C                                                         310
C                                                         311
BETA     = ALPHA - 0.5                                    312
F1       = (B + B) * DX * DX / DFCNMR                    313
F2       = (F1 + F1) * AMIMAG                            314
G2       = C * DZ                                         315
G1       = -G2 * AMIMAG                                   316
C                                                         317
CALL CFINTJ (CFM(1,1), F1, F2, G1, G2, ALPHA, -1., -1.) 318
CALL CFINTJ (CFM(1,2), F1, F2, G1, G2, ALPHA, -1., 1.) 319
CALL CFINTJ (CFM(1,3), F1, F2, G1, G2, BETA, 2., 2.)   320

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CALL CFINTJ (CFM(1,4), F1, F2, G1, G2, BETA, 2., -2.)          321
C                                                                322
RETURN                                                         323
END                                                             324

SUBROUTINE CFINTJ (COF, F1, F2, G1, G2, ALPHA, R1, R2)        325
C                                                                326
C GENERATE A 3-ELEMENT EXTRAPOLATION COEFFICIENT VECTOR IN  327
C P 42-R EQ. (10).                                           328
C COF(1) : CONSTANT TERM                                       329
C COF(2) : COEFF. OF AM * AM                                   330
C COF(3) : COEFF. OF I * AM                                   331
C                                                                332
DIMENSION COF(3)                                              333
C                                                                334
COF(1) = R1 + R1 + R2 * G1                                     335
COF(2) = ALPHA * R1 * F1                                       336
COF(3) = R1 * ALPHA * F2 + R2 * G2                               337
RETURN                                                         338
END                                                             339

SUBROUTINE EXTCON                                             340
C                                                                341
C GENERATE EXTRAPOLATION COEFFICIENTS                          342
C                                                                343
INCLUDE 'FXZMIG.CMB/NOLIST'                                    344
DIMENSION DFCBUF(2)                                           345
DOUBLE PRECISION A(15), B(15)                                  346
DATA      MODE      / -1 /                                     347
C                                                                348
DATA      A(1) / 0. 376 369 527 234 052 / ! 65                349
DATA      B(1) / 0. 478 242 059 603 743 /                     350
C                                                                351
DATA      A(2) / 0. 873 981 642 171 890 / ! 80                352
DATA      B(2) / 0. 040 315 156 988 852 /                     353
DATA      A(3) / 0. 222 691 982 666 100 /                     354
DATA      B(3) / 0. 457 289 565 835 625 /                     355
C                                                                356
DATA      A(4) / 0. 972 926 131 694 782 / ! 87                357
DATA      B(4) / 0. 004 210 419 911 239 /                     358
DATA      A(5) / 0. 744 418 058 525 258 /                     359
DATA      B(5) / 0. 081 312 382 016 760 /                     360
DATA      A(6) / 0. 150 843 924 026 968 /                     361
DATA      B(6) / 0. 414 236 604 654 513 /                     362
C                                                                363
DATA      A(7) / 0. 991 834 774 675 097 / ! 89                364
DATA      B(7) / 0. 000 737 959 542 660 /                     365
DATA      A(8) / 0. 911 282 437 100 351 /                     366
DATA      B(8) / 0. 016 329 891 492 279 /                     367
DATA      A(9) / 0. 602 498 780 802 238 /                     368
DATA      B(9) / 0. 120 110 756 314 730 /                     369
DATA      A(10) / 0. 102 624 305 081 323 /                    370
DATA      B(10) / 0. 362 806 692 332 044 /                    371
C                                                                372

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DATA      A(11) / 0. 997 370 236 438 328 /      ! 90      373
DATA      B(11) / 0. 000 153 427 175 533 /      374
DATA      A(12) / 0. 964 827 991 878 123 /      375
DATA      B(12) / 0. 004 172 967 255 246 /      376
DATA      A(13) / 0. 824 918 564 779 961 /      377
DATA      B(13) / 0. 033 860 917 808 142 /      378
DATA      A(14) / 0. 483 340 757 434 262 /      379
DATA      B(14) / 0. 143 798 075 648 762 /      380
DATA      A(15) / 0. 073 588 212 879 826 /      381
DATA      B(15) / 0. 318 013 812 535 422 /      382
C
DATA      DFCBUF / 1. 000 000 000, 0. 124 600 000 /      383
C
C
IF (NESTDR .LT. 1)      THEN      387
    NESTDR = 1      388
    A(1) = 0.25      389
    B(1) = 0.5      390
ENDIF      391
IF (MODE .GE. 0)      THEN      ! MODELING MODE      392
    DX = ABS (DX)      393
    DZ = ABS (DZ)      394
ELSE      ! MIGRATION MODE      395
    DX = -ABS (DX)      396
    DZ = -ABS (DZ)      397
ENDIF      398
C
K0 = (NESTDR * (NESTDR - 1)) / 2      399
DO 10 K = 1, NESTDR      400
AA = 1. / A(K+K0)      401
BB = AA * B(K+K0)      402
CALL CFBNDG (BNDBUF(1,K), A(K+K0), B(K+K0))      403
CALL CFINTI (EXTRBUF(1,K), AA, BB, DFCBUF(1), DFCBUF(2))      404
RETURN      405
END      406
END      407

SUBROUTINE CFBNDG (BCOF, A, B)      408
C
C      GENERATE THE TRANSPARENT BOUNDARY COEFFICIENTS AS      409
C
C       $B*XX / (1 + A*XX) == BB*Y / (1 + AA*Y)$ , WHERE      410
C      XX = DERIV(X)**2 / M, AND      411
C      Y = I * DERIV(X) / M.      412
C      BCOF(1) = AA      413
C      BCOF(2) = BB      414
C
C      DIMENSION BCOF(2)      415
C      LOGICAL VIRGIN      416
C      DATA VIRGIN / .TRUE. /      417
C
C      COMPUTE INTEGRALS (S2 THRU S6)      418
C
C      IF (VIRGIN)      THEN      419
C          VIRGIN = .FALSE.      420
C          S2 = ATAN (1.)      421
C          422
C          423
C          424
C          425
C          426

```


C		479
C	THIS IS A STACK OF ELEMENTARY SUBPROGRAMS REFERENCED	480
C	BY THE MIGRATION PROGRAM.	481
C		482
C	C C	483
C		484
	FUNCTION KPOWR2 (NUMBER)	485
C		486
C	FIND A NUMBER WHICH IS .GE. THE ARGUMENT AND IS ALSO	487
C	A POWER OF 2.	488
C		489
	KPOWR2 = 1	490
	DO 10 K = 1, 15	491
	KPOWR2 = KPOWR2 + KPOWR2	492
	IF (KPOWR2 .GE. NUMBER) RETURN	493
10	CONTINUE	494
	STOP 'ERROR IN KPOWR2'	495
	END	496
	SUBROUTINE CVAMMA (N, A, B, C, D, E, F)	497
	COMPLEX A(N), B(N), C(N), D(N), E(N), F(N)	498
	DO 10 I = 1, N	499
10	F(I) = (A(I) + B(I)) * C(I) + D(I) * E(I)	500
	RETURN	501
	END	502
	SUBROUTINE FFTC (LX, CX, SIGNI)	503
C		504
C	FAST FOURIER TRANSFORM. SEE CLAERBOUT P 12.	505
C		506
	COMPLEX CX(LX), CARG, CEXP, CW, CTEMP	507
	J = 1	508
	DO 30 I = 1, LX	509
	IF (I .GT. J) GO TO 10	510
	CTEMP = CX(J)	511
	CX(J) = CX(I)	512
	CX(I) = CTEMP	513
10	M = LX / 2	514
20	IF (J .LE. M) GO TO 30	515
	J = J - M	516
	M = M / 2	517
	IF (M .GE. 1) GO TO 20	518
30	J = J + M	519
	L = 1	520
40	ISTEP = 2 * L	521
	DO 50 M = 1, L	522
	CARG = CMPLX(0., 3.14159265 * SIGNI * (M - 1) / L)	523
	CW = CEXP(CARG)	524
	DO 50 I = M, LX, ISTEP	525
	CTEMP = CW * CX(I + L)	526
	CX(I+L) = CX(I) - CTEMP	527
50	CX(I) = CX(I) + CTEMP	528
	L = ISTEP	529
	IF (L .LT. LX) GO TO 40	530

	RETURN	531
	END	532
	 SUBROUTINE MOVEJC (N, A, B, JA, JB)	533
	COMPLEX A(N), B(N)	534
	IA = 1 - JA	535
	IB = 1 - JB	536
	DO 10 I = 1, N	537
	IA = IA + JA	538
	IB = IB + JB	539
10	B(IB) = A(IA)	540
	RETURN	541
	END	542
	 SUBROUTINE STORE (N, X, CONST)	543
	DIMENSION X(N)	544
	IF (N .LT. 1) GO TO 12	545
	DO 10 I = 1, N	546
10	X(I) = CONST	547
12	RETURN	548
	END	549
	 SUBROUTINE SUMVJ (N, X, SIGMA, JMP)	550
	DIMENSION X(2)	551
	SIGMA = 0.	552
	IX = 1 - JMP	553
	DO 10 I = 1, N	554
	IX = IX + JMP	555
10	SIGMA = SIGMA + X(IX)	556
	RETURN	557
	END	558
	 SUBROUTINE TRIDGX (N, T, A, B, D)	559
C		560
C	TRIDIAGONAL EQUATION WITH TRANSPARENT BOUNDARY CONDITION.	561
C		562
	COMPLEX T(N), A(N), B(N), D(N), DEN	563
		564
	N1 = N - 1	565
	DO 10 I = 2, N1	566
	DEN = 1. / (B(I) + A(I) * B(I-1))	567
	B(I) = - A(I) * DEN	568
10	A(I) = (D(I) - A(I) * A(I-1)) * DEN	569
	T(N) = (A(N1) * B(N) + A(N)) / (1. - B(N) * B(N1))	570
	DO 20 J = 1, N1	571
	I = N - J	572
20	T(I) = B(I) * T(I + 1) + A(I)	573
	RETURN	574
	END	575
	 SUBROUTINE VSMSAJ (N, A, S1, S2, C, JMPA, JMPC)	576

	DIMENSION	A(N), C(N)	577
	JA	= 1 - JMPA	578
	JC	= 1 - JMPC	579
	DO 10 I	= 1, N	580
	JA	= JA + JMPA	581
	JC	= JC + JMPC	582
10	C(JC)	= S1 * A(JA) + S2	583
	RETURN		584
	END		585
	SUBROUTINE	VSMULJ (N, A, S, C, JMPA, JMPC)	586
	DIMENSION	A(N), C(N)	587
	IJA	= 1 - JMPA	588
	IJC	= 1 - JMPC	589
	DO 10 I	= 1, N	590
	IJA	= IJA + JMPA	591
	IJC	= IJC + JMPC	592
10	C(IJC)	= S * A(IJA)	593
	RETURN		594
	END		595
	SUBROUTINE	VSMULT (N, A, S, C)	596
	DIMENSION	A(2), C(2)	597
	DO 10 I	= 1, N	598
10	C(I)	= S * A(I)	599
	RETURN		600
	END		601
	SUBROUTINE	VVMULT (N, A, B, C)	602
	DIMENSION	A(N), B(N), C(N)	603
	DO 10 I	= 1, N	604
10	C(I)	= A(I) * B(I)	605
	RETURN		606
	END		607