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Conductive Cooling of Dikes with Temperature-dependent  
Thermal Properties and Heat of Crystallization

by

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## Abstract

Temperature histories obtained from transient heat-conduction theory are applicable to most dikes despite potential complicating effects related to magma flow during emplacement, groundwater circulation, and metamorphic reaction during cooling. Here, machine-independent FORTRAN77 programs are presented to calculate temperatures in and around dikes as they cool conductively. Analytical solutions can treat thermal-property contrasts between the dike and host rocks, but cannot address the release of magmatic heat of crystallization after the early stages of cooling or the appreciable temperature dependence of thermal conductivity and diffusivity displayed by most rock types. Numerical solutions can incorporate these additional factors. The heat of crystallization can raise the initial temperature at the dike contact,  $\theta_{c1}$ , about 100°C above that which would be estimated if it were neglected, and can decrease the rate at which the front of solidified magma moves to the dike center by a factor of as much as three. Thermal conductivity and diffusivity of rocks increase with decreasing temperature and, at low temperatures, these properties increase still more if the rocks are saturated with water. Models that treat these temperature dependencies yield estimates of  $\theta_{c1}$  that are as much as 75°C beneath those which would be predicted if they were neglected.

Key words: Numerical analysis, finite-difference method, dikes, heat conduction, igneous intrusion, contact metamorphism.

## Introduction

Recent advances, particularly in the field of paleomagnetism, have provided measurement techniques that allow maximum temperatures attained in wallrocks adjacent to cooling dikes to be estimated with an accuracy of about  $\pm 25^{\circ}\text{C}$  (e.g., Buchan *et al.* 1980; McClelland-Brown, 1981). By combining these results with estimates of the initial magma temperature and the thermal properties of the magma and host rocks, it is possible to calculate the ambient temperature of the host rocks at the time of dike emplacement. This ambient temperature, in turn, can be combined with an estimate of the geothermal gradient to determine the approximate depth of emplacement, as well as the subsequent rate of uplift and denudation (see Buchan and Schwarz, 1986, for a review of the method). The method uses heat-conduction theory to determine cooling history; this is an excellent approximation for most dikes because they cool too quickly for buoyant hydrothermal circulation to become established. However, analytical solutions for conductive cooling are based upon assumptions that are too restrictive to permit temperatures to be calculated with an accuracy comparable to that of the measurements cited above (see Delaney, 1986). It is the purpose of this paper to provide FORTRAN77 programs that allow magmatic heat of crystallization and temperature-dependent thermal properties to be included in conductive cooling models of dikes.

## Thermal properties

The accuracy of theoretical calculations for temperatures depends not only upon validity of the assumptions used to derive solutions, but also upon the accuracy of the thermal property data, particularly conductivity,  $k$ , diffusivity,  $\kappa$ , and magmatic heat of crystallization,  $h$  (all mathematical symbols are summarized in Table 1). Although  $k$  and  $\kappa$  vary with lithology, these properties vary even more with temperature (Fig. 1). For most rocks at temperatures below  $200^{\circ}\text{C}$ ,  $k$  lies between 1.5 and  $3.0 \text{ W/m}^{\circ}\text{C}$  (quartzite is a notable exception), and  $\kappa$  typically ranges from  $0.5$  to  $1 \times 10^{-6} \text{ m}^2/\text{s}$ . Data collected at temperatures above  $500^{\circ}\text{C}$  are sparse for most rock types. Fortunately, thermal properties of dense basalt have been measured at temperatures well in excess of  $500^{\circ}\text{C}$ , and extrapolation to supersolidus conditions should not introduce large errors in thermal calculations. For

example,  $\underline{k}$  values from 1 to 1.5 W/m°C and  $\kappa$  values from 0.25- to 0.75- $\times 10^{-6}$  m<sup>2</sup>/s appear to be typical for basalt above 500°C. High-temperature values of  $\underline{k}$  and  $\kappa$  tend to be about 1/2 to 2/3 that which would be measured at low temperature.

Data for  $\underline{k}$  and  $\kappa$  can be described by a variety of empirical equations (e.g., Ramey *et al.*, 1974); we chose

$$\underline{k} = \underline{a}_1 + \underline{b}_1/(273.15+\theta) \quad (1a)$$

$$\kappa = \underline{a}_2 + \underline{b}_2/(273.15+\theta) \quad (1b)$$

where temperature  $\theta$  is in degrees Centigrade and the coefficients are obtained by least-squares fitting. Although equations of this form are used in the examples cited below, any equation can be used by altering the functions CONDM, CONDH, DIFFM, and DIFFH (Appendix 1), which return conductivity and diffusivity of the magma and host-rocks regions, respectively, given an input temperature. The conductivity modulus,  $\gamma$ , defined by

$$\gamma = (\underline{dk}/\underline{d\theta})/\underline{k} \quad (2)$$

is returned by the functions CONDMM and CONDMH (Appendix 1), given an input temperature.

The thermal properties summarized in Figure 1 apply to "dry" rocks. The presence of pore water, however, can have a profound effect upon thermal conductivity. For instance, rocks with porosities of only 1% typically have water-saturated  $\underline{k}$  about 10% greater than that for the dry sample (Touloukian *et al.*, 1981, p. 428). Thermal conductivity of water-saturated rock can be estimated from data for the dry rock using

$$\underline{k}_{\text{wet}} = \underline{k}_{\text{dry}} (\underline{k}_w/\underline{k}_{\text{air}})^\phi \quad (3)$$

where  $\phi$  is porosity and the subscript  $\underline{w}$  refers to water (Sass *et al.*, 1971). At modest pressures and 50°C,  $\underline{k}_w/\underline{k}_{\text{air}} \approx 20$ , so that a rock with 10% porosity may exhibit an increase in conductivity of ~40% if saturated with water. At 20 MPa and 550°C, a characteristic pressure and temperature near a dike contact at 2 km depth, the conductivity of water is small and  $\underline{k}_w/\underline{k}_{\text{air}} \approx 2$ , so

that the increase in conductivity due to water saturation is only about 7%. The influence of water upon  $\underline{k}$  is therefore greatly temperature dependent.

Although measurements of conductivity and diffusivity can, in principle, be used to estimate heat capacity per unit volume  $\rho C$  ( $= \underline{k}/\kappa$ ) such estimates rarely provide good fits to heat-capacity data. In this report, data for  $\underline{k}$  and  $\kappa$  are used rather than data for  $\rho C$ . It is nevertheless instructive to note that heat capacity of a water-saturated rock closely follows the relation  $(\rho C)_{\text{wet}} = (1-\phi)(\rho C)_r + \phi(\rho C)_w$ , where the subscript  $r$  denotes the rock matrix. For temperatures typical of the upper crust,  $(\rho C)_r \approx 2-3 \text{ MJ/m}^3 \cdot ^\circ\text{C}$  and  $(\rho C)_w \approx 3-4 \text{ MJ/m}^3 \cdot ^\circ\text{C}$ . Because, in general,  $\phi \ll 1$ , most heat resides in the solid matrix and not in pore water, so that porosity and pore fluid do not substantially influence the heat capacity of most rocks.

The heat released by a magma as it cools from its initial temperature  $\theta_{mi}$  to its solidus temperature  $\theta_s$  varies with chemistry and cooling rate. For a quickly quenched, glassy magma, the heat released is  $(\rho C)_m (\theta_{mi} - \theta_s)$ ; if cooled slowly to form a holocrystalline rock, then a heat of crystallization  $(\rho h)_m$  is released also. For unvesiculated magmas, the heat of crystallization per unit volume is typically  $700-1000 \text{ MJ/m}^3$ . It is assumed to be released evenly through the temperature interval from the intrusion temperature  $\theta_{mi}$  to the solidus temperature. The heat of crystallization can then be treated by defining a modified heat capacity and diffusivity:

$$(\rho C)_m' = (\rho C)_m + (\rho h)_m / (\theta_{mi} - \theta_s) \quad (4a)$$

$$\kappa_m' = \underline{k}_m / (\rho C)_m' \quad (4b)$$

where the subscript  $m$  denotes the magma and the subscript  $i$  denotes its initial (uncooled) value. These modified values apply only above the solidus temperature.

#### Problem formulation

Dikes are commonly idealized as tabular bodies of thickness  $T$ . At all positions not near the dike tip, heat conducts only in directions normal to the contact. We position an  $X$  coordinate so that it originates at one of the contacts and points away from the dike; the center of the dike is at  $X = -T/2$ .

We wish to obtain solutions to the heat-conduction equation for temperature-dependent thermal properties:

$$(\rho C) \partial \theta / \partial t = \partial k \partial \theta / \partial X^2 \quad (5)$$

(Carslaw and Jaeger, 1959, Ch. 1). Heat flux is given by Fourier's law,  $Q = -k \partial \theta / \partial X$ , and the gradient in this flux (right-hand side, eqs. 5) is exactly balanced with the accumulation of heat (left-hand side, eqs. 5). All heats of reaction--other than the crystallization of the magma, which will be incorporated through use of eqs. 4--and all heat transfer arising from fluid motion are assumed to be negligible.

From symmetry considerations, it is only necessary to consider the half-space  $X > -T/2$ . Thermal diffusion equations are distinguished for the host-rock region ( $X > 0$ ), the solidified-magma region ( $\chi_s < X < 0$ ), and the liquid-magma region ( $-T/2 < X < \chi_s$ ), where  $\chi_s$  is the position of the solidus isotherm  $\theta_s$ . Thermal properties are denoted by the subscripts  $h$  and  $m$  in the host-rock and magma (dike) regions, respectively. Properties of that portion of the dike occupied by magma are denoted with a prime (eqs. 4); this region need not be distinguished from the rest of the dike if no magmatic heat of crystallization is released. The magma region diminishes in size during cooling and disappears after the center of the dike cools beneath the solidus temperature. After expanding the right-hand side of eq. 5, the three energy equations are:

$$\partial \theta / \partial t = \kappa_h \left[ \partial^2 \theta / \partial X^2 + k_h^{-1} (\partial k_h / \partial X) (\partial \theta / \partial X) \right] \quad (0 < X < \infty) \quad (6a)$$

$$\partial \theta / \partial t = \kappa_m \left[ \partial^2 \theta / \partial X^2 + k_m^{-1} (\partial k_m / \partial X) (\partial \theta / \partial X) \right] \quad (\chi_s < X < 0) \quad (6b)$$

$$\partial \theta / \partial t = \kappa_m' \left[ \partial^2 \theta / \partial X^2 + k_m'^{-1} (\partial k_m' / \partial X) (\partial \theta / \partial X) \right] \quad (-T/2 < X < \chi_s; \theta > \theta_s) \quad (6c)$$

These equations have not been solved by analytical methods for cases where  $k$  and  $\kappa$  have temperature dependencies similar to those exhibited by rocks; they have been treated by numerical methods (e.g., Giberti et al., 1984). To obtain solutions, three initial and six boundary conditions must be specified:

$$\theta(\underline{x} > 0, \underline{t} = 0) = \theta_{hi}, \quad \theta(\chi_s < \underline{x} < 0, \underline{t} = 0) = \theta_{mi}, \quad \theta(-T/2 < \underline{x} < \chi_s, \underline{t} = 0) = \theta_{mi} \quad (7a)$$

$$\begin{aligned} \theta(\infty, \underline{t}) &= \theta_{hi}, & \theta(0^-, \underline{t}) &= \theta(0^+, \underline{t}) \equiv \theta_c, & \theta(\chi_s^-, \underline{t}) &= \theta(\chi_s^+, \underline{t}) \equiv \theta_s \\ \underline{Q}(0^-, \underline{t}) &= \underline{Q}(0^+, \underline{t}), & \underline{Q}(\chi_s^-, \underline{t}) &= \underline{Q}(\chi_s^+, \underline{t}), & \underline{Q}(\underline{x} = -T/2, \underline{t}) &= 0 \end{aligned} \quad (7b)$$

Equations 7a give the initial temperatures of the host rocks and magma. The first condition of eq. 7b assures that temperatures at great distance from the dike contact remain unchanged throughout the duration of cooling; the next two conditions assure that temperatures are continuous at the dike contact ( $\underline{x} = 0$ ) and at the position of the solidus isotherm ( $\underline{x} = \chi_s$ ). The latter three conditions assure that heat fluxes are continuous at the dike contact and at the position of the solidus isotherm, and that no heat crosses the mid-plane of the dike.

Before cooling commences at the dike center, the problem posed by eqs. 6 and 7 can be written in terms of the similarity variable:

$$\eta = \underline{x} / \sqrt{4\kappa_{hi} \underline{t}} \quad (8)$$

where the subscript hi denotes the host rock at its initial temperature. Distance and time are combined into a single independent variable, and the position of the solidus isotherm is transformed to a constant

$$\lambda_s = \chi_s / \sqrt{4\kappa_{hi} \underline{t}} \quad (9)$$

so that  $\chi_s(\underline{t}) \propto 1/\sqrt{\underline{t}}$ . Incorporating the definition of  $\gamma$ , eq. 2, the transformed thermal diffusion equations can be written as:

$$-2\eta \frac{d\theta}{d\eta} = (\kappa_h / \kappa_{hi}) \left[ \frac{d^2\theta}{d\eta^2} + \gamma_h \left( \frac{d\theta}{d\eta} \right)^2 \right] \quad (0 < \eta < \infty) \quad (10a)$$

$$-2\eta \frac{d\theta}{d\eta} = (\kappa_m / \kappa_{hi}) \left[ \frac{d^2\theta}{d\eta^2} + \gamma_m \left( \frac{d\theta}{d\eta} \right)^2 \right] \quad (\lambda_s < \eta < 0) \quad (10b)$$

$$-2\eta \frac{d\theta}{d\eta} = (\kappa_m^- / \kappa_{hi}) \left[ \frac{d^2\theta}{d\eta^2} + \gamma_m \left( \frac{d\theta}{d\eta} \right)^2 \right] \quad (-\infty < \eta < \lambda_s) \quad (10c)$$

Thus, the partial differential equations 6 are transformed into nonlinear ordinary differential equations. Equations 10 are to be solved in conjunction with six boundary conditions:



$$\begin{aligned}
\theta(\infty) &= \theta_{hi}, & \theta(0^-) &= \theta(0^+) \equiv \theta_{ci}, & \theta(\lambda_s^-) &= \theta(\lambda_s^+) \equiv \theta_s \\
\underline{Q}(0^-) &= \underline{Q}(0^+), & \underline{Q}(\lambda^-) &= \underline{Q}(\lambda^+), & \theta(-\infty) &= \theta_{mi}
\end{aligned} \tag{11}$$

The problem posed by eqs. 10 and 11 is known as a Stephan problem (Carslaw and Jaeger, 1959, Ch. 11). The properties of the transformation, eq. 8, show that, within the assumptions of the continuum theory, the temperature at the dike contact instantaneously rises to a value  $\theta_{ci}$  and remains unchanged until some time after the transformation becomes invalid. This occurs when the boundary condition  $\theta(-\infty) = \theta(-T/2, t) = \theta_{mi}$ , becomes invalid and must be replaced by  $\underline{Q}(-T/2, t) = 0$ ; this is when cooling commences at the dike center.

### Analytical solutions

For brevity and to emphasize scaling relations, analytical solutions are often written in terms of nondimensional variables. Nondimensional distance, time, and temperature are given by:

$$\underline{x} = \underline{X}/(\underline{T}/2) \tag{12a}$$

$$\tau = \underline{t} \cdot \kappa_{hi} / (\underline{T}/2)^2 \tag{12b}$$

$$\theta = (\theta - \theta_{hi}) / (\theta_{mi} - \theta_{hi}) \tag{12c}$$

Distance is normalized by dike half-thickness, time by the diffusivity of the host rocks at ambient temperature and the square of dike half-thickness, and temperature by the initial temperature difference between the magma and host rocks. All analytical solutions require that  $\underline{k}_m$ ,  $\underline{k}_h$ ,  $\kappa_m$ , and  $\kappa_h$  ( $\equiv \kappa_{hi}$ ) be constants.

Early-time solutions. The solution to the problem posed by eqs. 10 and 11, is:

$$\theta = 1 - (1 - \theta_s) [2 - \operatorname{erfc}(\eta \sqrt{\kappa_h / \kappa_m})] / [2 - \operatorname{erfc}(\lambda_s \sqrt{\kappa_h / \kappa_m})] \quad (\eta < \lambda_s) \tag{13a}$$

$$\theta = \theta_{ci} + (\theta_s - \theta_{ci}) \cdot \operatorname{erf}(\eta \sqrt{\kappa_h / \kappa_m}) / \operatorname{erf}(\lambda_s \sqrt{\kappa_h / \kappa_m}) \quad (\lambda_s < \eta < 0) \tag{13b}$$

$$\theta = \theta_{ci} \operatorname{erfc}(\eta) \quad (\eta > 0) \tag{13c}$$

(see Carslaw and Jaeger, 1959, Ch. 11) where erf is the error function and erfc its compliment. Differentiating eqs. 13 to obtain heat fluxes, and requiring that heat flux into and out of the interfaces between adjoining regions be the same, we obtain two equations to determine the unknowns  $\lambda_s$  and  $\theta_{ci}$ :

$$\frac{\sqrt{\kappa_h/\kappa_m}(1-\theta_s) \cdot e^{-\lambda_s^2 \kappa_h/\kappa_m}}{2 - \text{erfc}(\lambda_s \sqrt{\kappa_h/\kappa_m})} + \frac{\sqrt{\kappa_h/\kappa_m}(\theta_s - \theta_{ci}) \cdot e^{-\lambda_s^2 \kappa_h/\kappa_m}}{\text{erf}(\lambda_s \sqrt{\kappa_h/\kappa_m})} = 0 \quad (14a)$$

$$\frac{(k_m/k_h) \sqrt{\kappa_h/\kappa_m}(\theta_s - \theta_{ci})}{\text{erf}(-\lambda_s \sqrt{\kappa_h/\kappa_m})} - \theta_{ci} = 0 \quad (14b)$$

If the magma is quenched quickly such that  $(\rho h)_m = 0$ , then  $\theta_s = \theta_{mi}$ ,  $\lambda_s \rightarrow \infty$ , and temperatures are given by eqs. 13b, 13c, and 14b only. Equations 13 and 14 are used in the program EARLYA (Appendix 1) to provide temperatures as  $\theta(\eta)$  and  $\theta(X, t)$ .

Whole-time solution. The most general analytical solution to the problem posed by eqs. 6 and 7 is:

$$\theta = \frac{1+c}{2} \left\{ \sum_{n=1}^{\infty} (-c)^{n-1} \left[ \text{erf}\left(\frac{2n-x}{\sqrt{4d\tau}}\right) - c \cdot \text{erf}\left(\frac{2n+x}{\sqrt{4d\tau}}\right) \right] - \text{erf}\left(\frac{x}{\sqrt{4d\tau}}\right) \right\} \quad (-2 < x < 0) \quad (15a)$$

$$\theta = \frac{1-c}{2} \left\{ (1+c) \sum_{n=1}^{\infty} (-c)^{n-1} \cdot \text{erf}\left(\frac{x+2n/d}{\sqrt{4\tau}}\right) - \text{erf}\left(\frac{x}{\sqrt{4\tau}}\right) \right\} \quad (x > 0) \quad (15b)$$

where

$$c = \frac{d - k_m/k_h}{d + k_m/k_h} \quad (16a)$$

$$d = \sqrt{\kappa_m/\kappa_h} \quad (16b)$$

(Lovering, 1936). The initial temperature at the dike contact is given by:

$$\theta_{ci} = \frac{k_m/k_h}{k_m/k_h + \sqrt{\kappa_m/\kappa_h}} \quad (17)$$

Equations 15-17 show that temperatures are affected by thermal property contrasts, rather than the absolute values of those properties. If  $k_m/k_h = \kappa_m/\kappa_h = 1$ , then

$$\theta = \frac{1}{2} \{ \text{erf}[(2-x)/\sqrt{4\tau}] - \text{erf}[x/\sqrt{4\tau}] \} \quad (18)$$

so that the initial contact temperature is  $\theta_{c1} = 0.5$ . Equations 15 and 16, or 18, can be used to estimate the influence of the magmatic heat of crystallization on temperatures in the wallrocks by defining an equivalent intrusion temperature

$$\theta'_{mi} = \theta_{mi} + \frac{h}{C} \quad (19)$$

This approximation is inaccurate at distances less than about  $T/4$  from the dike contact, but is acceptable at greater distances if accuracies not better than about  $40^\circ\text{C}$  are acceptable (Jaeger, 1964).

The program WHOLEA (Appendix 1) provides temperatures as  $\theta(X,t)$ , as well as the maximum temperature  $\theta_{\max}(X)$ .

#### Numerical solutions

At times less than that required for cooling to commence at the dike center, numerical solutions to the problem posed by eqs. 6 and 7 are not accurate unless a great number of finite-difference nodes are used. Rather, at early times, eqs. 10 and 11 are solved, and temperatures are then converted from  $\theta(\eta)$  to  $\theta(X,t)$ . This temperature distribution is used as an initial condition for subsequent solution of eqs. 6 and 7.

Early-time solutions. Integration of eqs. 10 are executed by a Runge-Kutta method (Thompson, 1970) for first-order differential equations. Each eq. 10 is converted to two first-order equations by the substitution

$$\psi = \frac{d\theta}{d\eta} \quad (20)$$

which must be solved in conjunction with

$$-2\eta\psi = (\kappa_h/\kappa_{h1})[\underline{d}\psi/\underline{d}\eta + \gamma_h\psi^2] \quad (0 < \eta < \infty) \quad (21a)$$

$$-2\eta\psi = (\kappa_m/\kappa_{h1})[\underline{d}\psi/\underline{d}\eta + \gamma_m\psi^2] \quad (\lambda_s < \eta < 0) \quad (21b)$$

$$-2\eta\psi = (\kappa_m'/\kappa_{h1})[\underline{d}\psi/\underline{d}\eta + \gamma_m\psi^2] \quad (-\infty < \eta < \lambda_s) \quad (21c)$$

Because  $\chi_s$  occurs at a known temperature  $\Theta_s$ , eqs. 21b and 21c can be treated as the same equation with a temperature-dependent diffusivity function that employs eq. 4b above the solidus temperature.

Equations 20 and 21 are solved for the boundary conditions by use of the shooting method (Hornbeck, 1975, p. 205), whereby the coupled two-point boundary-value problems are treated as coupled initial-value problems. Successive guesses of  $\Theta_{c1}$  and  $\underline{d}\Theta/\underline{d}\eta$  evaluated at  $\eta = 0$  are integrated to  $\eta = +\infty$  and  $-\infty$ . If the guesses are correct, the temperature at  $\eta = +\infty$  is  $\Theta_{h1}$ , and that at  $\eta = -\infty$  is  $\Theta_{m1}$ . Newton-Raphson iteration is used to find the unknown temperature and temperature gradient at the dike wall.

The program EARLYN (Appendix 1) returns temperatures as  $\Theta(\eta)$  and  $\Theta(\underline{X}, \underline{t})$ .

Late-time solution. Using results from either the analytical or numerical early-time solution as an initial condition, temperatures are subsequently integrated using the Crank-Nicolson method (Hornbeck, 1975, p. 275), which is unconditionally stable for time steps of any size and retains second-order accuracy in the finite-difference approximation of the both the space and time derivatives. Denoting  $\underline{X}$ -nodes and  $\underline{t}$ -nodes with  $\underline{i}$  subscripts and  $\underline{j}$  superscripts, respectively, the finite-difference forms of each term in eqs. 6 are:

$$\kappa^{-1} \partial\Theta/\partial\underline{t} \approx [2/(\kappa_i^{j+1} + \kappa_i^j)] \cdot (\Theta_i^{j+1} - \Theta_i^j) / (\Delta\underline{t}) \quad (22a)$$

$$\partial^2\Theta/\partial\underline{X}^2 \approx \frac{1}{2}(\Theta_{i+1}^j - 2\Theta_i^j + \Theta_{i-1}^j) / (\Delta\underline{X})^2 + \frac{1}{2}(\Theta_{i+1}^{j+1} - 2\Theta_i^{j+1} + \Theta_{i-1}^{j+1}) / (\Delta\underline{X})^2 \quad (22b)$$

$$\begin{aligned} \underline{k}^{-1} (\partial\underline{k}/\partial\underline{X}) (\partial\Theta/\partial\underline{X}) \approx & [2/(\underline{k}_i^{j+1} + \underline{k}_i^j)] \cdot \frac{1}{2}(\underline{k}_{i+1}^j + \underline{k}_{i-1}^j) (\Theta_{i+1}^j - \Theta_{i-1}^j) / (2\Delta\underline{X})^2 \\ & + [2/(\underline{k}_i^{j+1} + \underline{k}_i^j)] \cdot \frac{1}{2}(\underline{k}_{i+1}^{j+1} - \underline{k}_{i-1}^{j+1}) (\Theta_{i+1}^{j+1} - \Theta_{i-1}^{j+1}) / (2\Delta\underline{X})^2 \end{aligned} \quad (22c)$$

where all  $\Theta_i^{j+1}$  are unknown temperatures at the  $\underline{t}^{j+1}$  time. Equations 22 assure conservation of energy between each node, so that all boundary conditions, except those at  $\underline{X} = -\underline{T}/2$  and  $\infty$ , are automatically satisfied. If there are  $\underline{n}$

$\underline{X}$ -nodes, then there is a system of  $\underline{n}-2$  equations of the form of eqs. 22, the remaining two nodes being subject to the remaining boundary conditions. Equation 22c is nonlinear because  $\underline{k}^{j+1}$  is a function of  $\tau^{j+1}$ . To linearize this term,  $\underline{k}^{j+1}$  is initially set equal to  $\underline{k}^j$ ; iteration is then used to recompute  $\underline{k}^{j+1}$  until it has an arbitrarily small effect upon the calculated temperature  $\theta^{j+1}$ . When written in matrix form to solve for the  $\underline{n}$  unknown temperatures, the coefficients form a tridiagonal matrix; this system is easily solved using the Thomas algorithm (von Rosenberg, 1975). A similar solution method was devised by Sanford (1982) for binary diffusion.

The program WHOLEN (Appendix 1) provides temperatures as  $\theta(\underline{X}, t)$ , as well as the maximum temperature  $\theta_{\max}(\underline{X})$ .

### Use of Programs

The four programs make use of 26 subroutines and functions (Table 2; linking procedures are shown in Table 3). Before running the programs the user must construct a file containing up to 13 times when temperatures are to be saved and written to an output file. The number of times when temperatures are to be saved to file must be on the first line, with the times on the remaining lines; the first time must be zero. The user has a choice of using nondimensional times  $\tau$  (eq. 12a) stored in a file named TAU.DAT or of dimensional times in units of seconds stored in a file named DTAU.DAT (see Table 4 for examples). The remaining input parameters are read interactively from the default input device (keyboard, which is assumed to open automatically upon invocation as unit 5); examples are shown in Table 4. Some data are written to the standard output device (screen, which is assumed to open automatically upon invocation as unit 6) during execution; a complete listing of input parameters and results is written to one of the files EARLYA.DAT, WHOLEA.DAT, EARLYN.DAT or WHOLEN.DAT upon completion of all calculations. Error conditions are written to the standard error output (screen, assumed to open automatically as unit 0). Data files are opened and closed with calls to subroutines FOPEN and FCLOSE; it is user's responsibility to assure that opening and closing of files conform to the conventions documented in those subroutines (see Appendix ).

## Example

To illustrate the application of the programs and isolate the influence of the temperature dependence of thermal properties, consider the intrusion of a basaltic magma at an initial temperature of 1150°C to form a 2-m-thick dike in a sequence of basaltic lava flows at an ambient temperature of 50°C. If restricted to results of analytical solutions, one would be tempted to use eq. 18 ( $\underline{k}_m/\underline{k}_h = \kappa_m/\kappa_h = 1$ ). Temperature as a function of distance and time for  $\underline{k}_m/\underline{k}_h = \kappa_m/\kappa_h = 1$  is shown in Figure 2, where results are presented both in nondimensional form and in dimensional form for this particular case (see second column, Table 5, for input). Numerical solutions use the best fit for the temperature dependence of  $\underline{k}$  and  $\kappa$  (Fig. 1a):  $\underline{k}_m = \underline{k}_h = 0.689 + 522/(273.15+\theta)$  and  $\kappa_m = \kappa_h = 3.05 \times 10^{-7} + 1.25 \times 10^{-4}/(273.15+\theta)$ . If the host rock had 10% porosity and were saturated with water, then the best fit is:  $\underline{k}_h = 0.250 + 944/(273.15+\theta)$  and  $\kappa_h = 1.80 \times 10^{-6} + 2.50 \times 10^{-4}/(273.15+\theta)$ . A magmatic heat of crystallization  $(\rho h)_m = 900 \text{ MJ/m}^3$  is used and contrasted with the case in which  $(\rho h)_m = 0 \text{ MJ/m}^3$ . Temperatures are presented as a function of position and time for the temperature-dependent properties of "wet" basalt in Figure 3 (see third and fourth columns, Table 5, for input).

The analytical solution (eq. 18) indicates that  $\theta_{ci} = 600^\circ\text{C}$ ; the numerical solution for "dry" basalt reveals that  $\theta_{ci} = 545^\circ\text{C}$ , 55°C less than the analytical solution. The numerical solution for host rocks with the properties of "wet" basalt reveals that  $\theta_{ci} = 525^\circ\text{C}$ , 75°C less than would be indicated by the analytical solution. If the heat of crystallization is released evenly in the temperature interval between 1150°C and 950°C, then the analytical solution (eqs. 13 and 14) indicates that  $\theta_{ci} = 690^\circ\text{C}$ ; the numerical solution reveals that  $\theta_{ci} = 640^\circ\text{C}$ , 50°C less than the analytical solution. If the heat of crystallization is released and the host rocks have the properties of "wet" basalt, then  $\theta_{ci} = 618^\circ\text{C}$ , 72°C less than would be indicated by the analytical solution. The combined effect of treating water-saturation and the temperature dependence of thermal properties reduces estimates of maximum temperatures by almost as much as the latent heat of crystallization raises them. The difference among maximum temperatures in the host rocks is greatest

at the dike contact (Fig. 4). Maximum temperatures attained in the wallrocks are everywhere less than would be estimated by any existing analytical method.

### Conclusions

The theory of transient heat conduction remains the principal guide for analysis of cooling of most, but by no means all, dikes. Analytical solutions are useful for estimating temperatures and cooling rates where accuracies not greater than about 75°C are required (Delaney, 1986), but numerical solutions are important if temperature estimates in the vicinity of the dike contact are required to be more accurate. The reason for this is two-fold. First, analytically obtained estimates of maximum temperatures attained in the host rocks can only approximately account for the heat of crystallization associated with cooling, which can raise estimates of temperatures at the dike contact by 100°C or more. Second, analytical solutions do not address the temperature-dependence of thermal conductivity and diffusivity, which can lower estimates of temperatures at the dike contact by 50-70°C or more. These limitations are overcome by numerical methods of solution. However, the accurate prediction of rock properties in situ and of the relation between cooling rate and release of magmatic heat of crystallization limit the accuracy that even numerical solutions can achieve.

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c-345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

program earlya

c

c conductive cooling of an instantaneously emplaced dike; early-time,  
c analytic solution for the cooling history. magma and host rocks can  
c have different but constant thermal conductivity and diffusivity; the  
c magma can release a heat of crystallization in the interval between  
c its intrusion temperature and some specified lower temperature.  
c solution applies until cooling commences at dyke center; before this  
c time temperatures can be expressed in terms of a single variable that  
c combines distance and time. temperature data is calculated at *ii*  
c times, the first of which is 0. these times must exist in the file  
c TAU.DAT or DTAU.DAT before running this program. the former are  
c nondimensional times; the latter are dimensional in seconds.

c

c all variables are in units of m-k-s & degrees centigrade.

c coordinates are *x* and *tau*, and  $\eta = x/\sqrt{4*xkaph*tau}$ .

c *x* = 0 at the contact; *x* = -dike  $\frac{1}{2}$  thickness at the dike center.

c

implicit real\*4 (a-h,o-z), integer\*4 (i-n)

parameter (ii=13, jj=601)

dimension tau(ii), x(jj), t(jj,ii), eta(jj), tt(jj)

external start, solve2, tmpae1, tmpae2, tmpae3, finish

character ans\*1

common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,

+ xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,

+ jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,

+ bkapd, bkaph, iflag, itnum, err, jn

common /propa/ rkd, rkm, sqkapd, sqkapm, p

c

c (1) get dike half-thickness (dthck2), initial temperatures of dike  
c rock and host rock (tdi, thi), and conductivity and diffusivity of  
c dike rock (xkd, xkapd) and host rocks (xkh, xkaph). if a separate  
c magma region is specified (ians = 3), get latent heat of  
c crystallization per unit volume (xl), solidus temperature (ts),  
c as well as conductivity and diffusivity of magma (xkm, xkapm).  
c provide initial quesses of initial temperature at dike contact  
c (tci) and transformed position of solidification surface (xlam).  
c latent heat is released evenly in the interval from tdi to ts.

c

write(6,9)

9 format(/' Include heat of crystallization ? [y/n] ?? '\$)

read(5,'(1a)') ans

write(6,10)

10 format(/' dike half-thickness [m]: = '\$)

read(5,\*) dthck2

write(6,11)

11 format(/' initial temp. [deg.c]: dike rock & host rock = '\$)

read(5,\*) tdi, thi

write(6,12)

12 format(/' conductivity [w/m deg.c]: dike rock & host rock = '\$)

read(5,\*) xkd, xkh

write(6,13)

```

13  format(/'      diffusivity [m*m/s]: dike rock & host rock = '$)
    read(5,*) xkapd, xkaph
    xkm = xkd
    xkapm = xkapd
    if (ans .eq. 'n') then
        xl = 0.0e0
        xlam = -4.0e0
        ts = tdi
    else
        write(6,16)
16  format(/'      latent heat [j/m**3]: magma = '$)
        read(5,*) xl
        write(6,17)
17  format(/'      solidus temp. [deg. c]: magma = '$)
        read(5,*) ts
        write(6,18)
18  format(/'      quess: contact temp. [deg.c]: thi < tci < ts = '$)
        read(5,*) tci
        write(6,19)
19  format(/'      solidification surface: -2 < lambda < 0 = '$)
        read(5,*) xlam
    endif
c
c (2) prepare distance, time & eta vectors, and associated indeces.
c
    call start(x,tau,t,eta,tt,ii,jj)
c
c (3) calculate tci if there is no heat of crystallization,
c and tci and xlam by newton-raphson iteration if there is.
c
    if (xl .eq. 0.0e0) then
        rkd = xkd/xkh
        sqkapd = sqrt(xkapd/xkaph)
        tci = thi + (tdi-thi)*rkd/(rkd+sqkapd)
    else
        rkd = xkd/xkh
        rkm = xkm/xkh
        sqkapd = sqrt(xkapd/xkaph)
        if ((abs((tdi-ts)/(tdi-thi)) .gt. 1.0e-4) .and.
+         (abs((xl/(tdi-ts))/(xkm/xkapm)) .gt. 1.0e-4)) then
            xkapmp = xkm/((xkm/xkapm)+xl/(tdi-ts))
            sqkapm = sqrt(xkapmp/xkaph)
        else
            sqkapm = sqrt(xkapm/xkaph)
        endif
        itmax = 25
        err = 1.0e-4*(tdi-thi)
        call solve2(tmpae3,xlam,tci,err,itmax)
        if (itmax .ge. 25) stop
    endif
c
    write(6,90) tci
90  format(/'      contact temperature = ',1pg11.4,' deg. c')
    if (xl .ne. 0.0e0) write(6,91) xlam

```

```

91  format(' solidification surface, xlam = 'lpgl1.4/)
c
c (4) find latest possible valid early-time solution.
c
      do 30 i = ie-1, imax
        etax = -dthck2/sqrt(4.0e0*xkaph*tau(i))
        if (xl .eq. 0.0e0) then
          call tmpael(etax,t(1,i))
        else
          call tmpae2(etax,t(1,i))
        endif
        if ((t(1,i)-thi)/(tdi-thi) .lt. 0.9995e0) goto 31
30    continue
31    ie = i - 1
c
c (5) calculate temperatures as a function of eta.
c
      do 41 j = 1, jmax
        if (xl .eq. 0.0e0) then
          call tmpael(eta(j),tt(j))
        else
          call tmpae2(eta(j),tt(j))
        endif
41    continue
c
c (6) calculate temperatures in terms of x and tau
c
      do 42 j = 1, jc-1
42      t(j,1) = tdi
        t(jc,1) = tci
      do 43 j = jc+1, jmax
43      t(j,1) = thi
      do 44 i = 2, ie
        sqrtt = sqrt(4.0e0*xkaph*tau(i))
        do 45 j = 1, jmax
          etax = x(j)/sqrtt
          if (xl .eq. 0.0e0) then
            call tmpael(etax,t(j,i))
          else
            call tmpae2(etax,t(j,i))
          endif
45      continue
44      continue
c
        write(6,92)
92      format(' analytical early-time solution is finished')
c
c (7) finish up: write data to file "earlya.dat"; "tm" is a dummy.
c
        call finish(x,tau,t,eta,tt,tm,ii,jj,'ea')
c
        stop
      end

```

4-345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

program earlyn

c

c conductive cooling of an instantaneously emplaced dike. early-time  
 c numerical solution for the situation where magma and host rocks have  
 c different, temperature-dependent thermal conductivities and  
 c diffusivities, as defined by the functions condd, condmd, diffd,  
 c condh, condmh, & diffh. cond\_ is the conductivity function for dike  
 c or host rocks; condm\_ is the function for conductivity modulus,  
 c  $(1/k)(dk/dt)$ ; diff\_ is the function for diffusivity. the magma can  
 c release a heat of crystallization in the interval between its  
 c intrusion temperature and some specified lower temperature. solution  
 c applies before cooling commences at the dyke center; before this time  
 c temperatures can be expressed in terms of a single variable that  
 c combines distance and time. thus, the partial differential  
 c equations are converted to ordinary differential equations, and  
 c the transformed boundary conditions constitute a boundary-value  
 c problem. the method of solution, "the shooting method," treats the  
 c problem as an initial-value problem. the equations are then  
 c integrated to the "far" boundary. successive guesses (found by  
 c newton-raphson integration) are used to find the initial values that,  
 c when integrated, match the desired far boundary values. although the  
 c odes are second-order equations, they are converted to pairs of  
 c first-order equations for the numerical integration by a modified  
 c runge-kutta method. temperature data is calculated at ii times, the  
 c first of which is 0. these times must exist in the file TAU.DAT or  
 c DTAU.DAT before running this program. the former are nondimensional  
 c times; the latter are dimensional in seconds.

c

c all variables are in units of m-k-s & degrees centigrade  
 c coordinates are x (distance), tau (time), eta =  $x/\sqrt{4*kap\_h*tau}$ .  
 c x = 0 at dike contact; x = -dike\_1/2\_thickness at the dike center.

c

```

implicit real*4 (a-h,o-z), integer*4 (i-n)
real*8 xx, dxx, yy
character*1 ans
parameter (ii=13, jj=601)
dimension tau(ii), x(jj), t(jj,ii), eta(jj), tt(jj), yy(2)
external condd, condh, diffd, diffh, start, tmpnel, tmpne2,
+      tmpne3, oderk2, solve2, finish
common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+      xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+      jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+      bkapd, bkaph, iflag, itnum, err, jn

```

c

c (1) get dike half-thickness (dthck2), initial temperatures of dike  
 c rock and host rock (tdi, thi), and conductivity and diffusivity  
 c functions of dike rock (akd, bkd, akapd, bkapd) and host rocks  
 c (akh, bkh, akaph, bkaph). get the latent heat of crystallization  
 c per unit volume (xl), and solidus temperature (ts). get initial  
 c guesses of initial temperature at dike contact (tci) and trans-  
 c formed position of solidification surface (xlam). latent heat is  
 c released evenly in the temperature interval from tdi to ts.

```

c
  write(6,9)
9  format(/' Include heat of crystallization ? [y/n] ?? '$)
  read(5,'(1a)') ans
  write(6,10)
10 format(/'   dike half-thickness [m]:                      = '$)
  read(5,*) dthck2
  write(6,11)
11 format(/'       initial temp. [deg.c]: dike rock & host rock = '$)
  read(5,*) tdi, thi
  write(6,12)
12 format(/'   conductivity: [w/m deg.c] = a + b/(273.15+t[deg.c])'
+   //' dike rock -- a, b = '$)
  read(5,*) akd, bkd
  write(6,13)
13 format(' host rock -- a, b = '$)
  read(5,*) akh, bkh
  write(6,14)
14 format(/'   diffusivity: [m**2/s] = a + b/(273.15+t[deg.c])'
+   //' dike rock -- a, b = '$)
  read(5,*) akapd, bkapd
  write(6,13)
  read(5,*) akaph, bkaph
  if (ans .le. 'n') then
    ts = tdi
    xlam = -4.0e0
  else
    write(6,16)
16  format(/'       latent heat [j/m**3]:  magma                = '$)
    read(5,*) xl
    write(6,17)
17  format(/'       solidus temp. [deg. c]:  magma                = '$)
    read(5,*) ts
  endif
  write(6,18)
18  format(/' quess: temp. at contact [deg.c]:  thi < tci < ts = '$)
  read(5,*) tci
  write(6,19)
19  format(/'                               error tolerance [generally <1.0e-3] = '$)
  read(5,*) err

```

c

c (2) compute special values for the conductivity and diffusivity.

c

```

  xkd = condd(tdi)
  xkapd = diffd(tdi)
  xkh = condh(thi)
  xkaph = diffh(thi)

```

c

c (3) prepare distance, time & eta vectors, and associated indeces.

c

```

  call start(x,tau,t,eta,tt,ii,jj)

```

c

c (4) initial quess of tci is provided before calling this subroutine;  
c qch is a quess of the heat flux into the host-rock half-space. these

```

c two parameters are sufficient to integrate the heat to x = +infinity.
c to perform the integration to x = -infinity, we set qcd = qch*(xkd/xkh)
c where xkd and xkh are evaluated at the contact temperature. the
c integrater, looks to see when temperatures have exceeded ts, and
c positions xlam in that fashion.

```

```

c
      itmax = 25
      err = err*(tdi-thi)
      qch = -2.0e0*(tci-thi)/sqrt(3.142e0)
      call solve2(tmpnel,tci,qch,err,itmax)
      err = err/(tdi-thi)
      if (itmax .ge. 25) stop

```

```

c
c (5) integrate equations stopping to tabulate tempertures.
c iflag = 0: integrate equations for magma.
c iflag = 1: integrate equations for host rock

```

```

c
      dxx = deta/(1.0e0*nk)
      rkci = condd(tci)/condh(tci)
      tt(kc) = tci

```

```

c
      iflag = 0
      iflag = 0
      xx = 0.0e0
      yy(1) = tci
      yy(2) = -qch/rkci
      istart = 1
      do 31 j = kc-1, 1, -1
        do 32 k = 1, nk
          call oderk2(dxx,xx,yy,tmpne2,istart)
          if ((sngl(yy(1)) .gt. ts) .and. (iflag .eq. 0)) then
            xlam = -(xx+(xx-dxx))/2.0e0
            iflag = 1
          endif
32      continue
31      tt(j) = yy(1)

```

```

c
      iflag = 1
      xx = 0.0d0
      yy(1) = tci
      yy(2) = qch
      istart = 1
      do 30 j = kc+1, jmax
        do 33 k = 1, nk
          call oderk2(dxx,xx,yy,tmpne2,istart)
33      continue
30      tt(j) = yy(1)

```

```

c
      write(6,90) tci
90      format(/' analytical early-time solution is finished'
+          //' contact temperature = ',lpg11.4,' deg. c')
      if (x1 .ne. 0.0e0) write(6,91) xlam
91      format(/' solidification surface, eta = ',lpg11.4,/)

```

```

c

```

```
c (5) convert from tt(eta) to t(x,tau)
c
c      call tmpne3(x,tau,t,eta,tt,ii,jj)
c
c (6) write data to file "earlyn.dat"; "tm" is a dummy.
c
c      call finish(x,tau,t,eta,tt,tm,ii,jj,'en')
c
c      stop
c      end
```



```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
c      program wholea
c
c conductive cooling of an instantaneously emplaced dike; whole-time,
c analytic solution for the cooling history. magma and host rocks may
c have different but constant thermal conductivity and diffusivity.
c no latent heat of crystallization can be included in this solution,
c unless by the method of an equivalent intrusion temperature.
c temperature data is calculated at ii times, the first of which is 0.
c these times must exist in the file TAU.DAT or DTAU.DAT before running
c this program. the former are nondimensional times; the latter are
c dimensional in seconds.
c
c all variables are in units of m-k-s & degrees centigrade.
c coordinates are x and tau.
c x = 0 at the contact; x = -dike_1/2_thickness at the dike center.
c
c      implicit real*4 (a-h,o-z), integer*4 (i-n)
c      parameter (ii=13, jj=601)
c      dimension tau(ii), x(jj), t(jj,ii), eta(jj), tt(jj), tm(jj)
c      external start, tmpael, tmpall, tmpal2, tmpal3, finish
c      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+          xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+          jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+          bkapd, bkaph, iflag, itnum, err, jn
c      common /propa/ rkd, rkm, sqkapd, sqkapm, p
c
c (1) get dike half-thickness (dthck2), initial temperatures of dike
c rock and host rock (tdi, thi), and conductivity and diffusivity
c of dike rock (xkd, xkapd) and host rocks (xkh, xkaph).
c
c      write(6,10)
10      format(/' dike half-thickness [m]:                = '$)
c      read(5,*) dthck2
c      write(6,11)
11      format(/' initial temp. [deg.c]: dike rock & host rock = '$)
c      read(5,*) tdi, thi
c      write(6,12)
12      format(/' conductivity [w/m deg.c]: dike rock & host rock = '$)
c      read(5,*) xkd, xkh
c      write(6,13)
13      format(/' diffusivity [m*m/s]: dike rock & host rock = '$)
c      read(5,*) xkapd, xkaph
c
c (2) prepare distance & time vectors, and associated indeces.
c
c      call start(x,tau,t,eta,tt,ii,jj)
c
c (3) calculate initial temperatures.
c
c      sqkapd = sqrt(xkapd/xkaph)
c      rkd = xkd/xkh
c      p = (sqkapd-rkd)/(sqkapd+rkd)

```

```

        tci = thi + (tdi-thi)*rkd/(rkd+sqkapd)
c
        do 21 j = 1, jc-1
21      t(j,1) = tdi
        t(jc,1) = tci
        do 22 j = jc+1, jmax
22      t(j,1) = thi
c
c (4) calculate temperatures.
c
        if ((abs(p).lt.1.0e-5) .and. (abs(sqkapd-1.0e0).lt.1.0e-5)) then
            do 40 i = 2, imax
                call tmpall(tau(i),x(1),t(1,i))
                do 45 j = 2, jmax
                    if ((t(j-1,i)-thi)/(tdi-thi) .gt. 1.0e-4) then
                        call tmpall(tau(i),x(j),t(j,i))
                    else
                        t(j,i) = thi
                    endif
45      continue
                write(6,90) tau(i), t(1,i), t(jc,i)
40      continue
            else
                do 41 i = 2, ie
                    sqrtt = sqrt(4.0e0*xkaph*tau(i))
                    do 46 j = 1, jmax
                        etal = x(j)/sqrtt
46      call tmpael(etal,t(j,i))
                        write(6,90) tau(i), t(1,i), t(jc,i)
41      continue
                    do 42 i = ie+1, imax
                        call tmpal2(tau(i),x(1),t(1,i))
                        do 47 j = 2, jmax
                            if ((t(j-1,i)-thi)/(tdi-thi) .gt. 1.0e-4) then
                                call tmpal2(tau(i),x(j),t(j,i))
                            else
                                t(j,i) = thi
                            endif
47      continue
                        write(6,90) tau(i), t(1,i), t(jc,i)
42      continue
                    endif
c
90      format(/' time = ',1pg11.4,' sec.: ',
+           ' temperature: dike center = ',1pg11.4,' deg. c',
+           /'
+           ' contact = ',1pg11.4,' deg. c')
c
c (5) find maximum temperature attained at each position.
c
        do 60 j = 1, jc-1
60      tm(j) = tdi
        tm(jc) = tci
c

```

```
if ((abs(p).lt.1.0e-5) .and. (abs(sqkapd-1.0e0).lt.1.0e-5)) then
  do 61 j = jc+1, jmax
    xlog = alog(x(j)/(2.0e0*dthck2+x(j)))
    taum = -(2.0e0*dthck2+x(j))*dthck2/(2.0e0*xkaph*xlog)
61   call tmpall(taum,x(j),tm(j))
  else
    taum = tau(ie+1)
    do 62 j = jc+1, jmax
62   call tmpal3(x(j),tm(j),taum)
  endif
c
  write(6,91)
91  format(/' analytical late-time solution is finished')
c
c (4) finish up: write data to file "wholea.dat".
c
  call finish(x,tau,t,eta,tt,tm,ii,jj,'wa')
c
990  stop
end
```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

program wholen

c

c conductive cooling of an instantaneously emplaced dike. whole-time  
 c numerical solution for the situation where magma and host rocks have  
 c different, temperature-dependent thermal conductivities and  
 c diffusivities, as defined by the functions condh, condm, diffd,  
 c condh, condm, & diffh. cond is the conductivity function for dike  
 c or host rocks; condm is the function for conductivity modulus,  
 c  $(1/k)(dk/dt)$ ; diff is the function for diffusivity. the magma can  
 c release a heat of crystallization in the interval between its  
 c intrusion temperature and some specified lower temperature. the  
 c initial temperature distribution is given by an early-time solution  
 c computed from either of the programs EARLYA or EARLYN, which must,  
 c therefore be run first. the method of solution is crank-nicolson  
 c with iterative improvement. temperature data is calculated at ii  
 c times, the first of which is 0. these times must exist in the file  
 c TAUD.DAT before running this program; these are dimensional in seconds.

c

c all variables are in units of m-k-s & degrees centigrade.

c coordinates are x and tau.

c  $x = 0$  at the contact;  $x = -\text{dike\_}1/2$  thickness at the dike center.

c

```
implicit real*4 (a-h,o-z), integer*4 (i-n)
parameter (ii=13, jj=601)
dimension tau(ii), x(jj), t(jj,ii), tm(jj)
character meth*2, str*50
external tmpnl, finish
common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+          xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+          jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+          bkapd, bkaph, iflag, itnum, err, jn
```

c

c (1) get times when temperatures will be stored from file TAUD.DAT

c

```
call fopen(2,'TAUD.DAT','old','exclusive',ios)
if (ios .ne. 0) then
  write(0,995)
995  format('error trying to open file TAUD.DAT')
  stop
endif
read(2,'(1x,i4)') imax
read(2,'(1x,lpg14.5)') (tau(i), i=1,imax)
call fclose(2,'keep',ios)
```

c

c (2) get data on temperatures, thermal properties, etc., from  
 c file EARLYN.DAT or EARLYA.DAT. (this means program earlyn or  
 c earlya must be run before wholen.)

c

```
write(6,1)
1  format('/ Is input file EARLYA.DAT or EARLYN.DAT ?? [a/n] ?? `')
read(5,'(1a)') meth(2:2)
write(6,3)
```

```

3   format(/' number of iterations between output-time steps'
+     /'                                     (generally >5) = '$)
    read(5,*) itnum
    write(6,'(/)')
c
    if ((meth(2:2) .eq. 'a') .or. (meth(2:2) .eq. 'A')) then
        call fopen(1,'EARLYA.DAT', 'old', 'exclusive', ios)
    else
        call fopen(1,'EARLYN.DAT', 'old', 'exclusive', ios)
    endif
    if (ios .ne. 0) then
        write(0,996)
996   format('error trying to open EARLY_.DAT')
        stop
    endif
c
    read(1,10) ie, jmax, tdi, thi, tci, dthck2, dx, jc, meth(2:2)
    write(6,10) ie, jmax, tdi, thi, tci, dthck2, dx, jc, meth(2:2)
10   format(1x,i4/1x,i4//1x,1pe10.3/1x,1pe10.3/1x,1pe10.3//
+         1x,1pe10.3/1x,1pe10.3/1x,i4//1x,a1/)
    read(1,20) xl, ts, xlam
    write(6,20) xl, ts, xlam
20   format(1x,1pe10.3/1x,1pe10.3/1x,1pe10.3/)
    read(1,30) xkd, xkapd, xkh, xkaph
    write(6,30) xkd, xkapd, xkh, xkaph
30   format(1x,1pe10.3/1x,1pe10.3/1x,1pe10.3/1x,1pe10.3/)
    if (meth(2:2) .eq. 'a') then
        akd = xkd
        bkd = 0.0e0
        akapd = xkapd
        bkapd = 0.0e0
        akh = xkh
        bkh = 0.0e0
        akaph = xkaph
        bkaph = 0.0e0
    else
        read(1,34) akd, bkd, akapd, bkapd, akh, bkh, akaph, bkaph
        write(6,34) akd, bkd, akapd, bkapd, akh, bkh, akaph, bkaph
        read(1,36) err
        write(6,36) err
34   format(1x,4(1pe10.3,1x)//1x,4(1pe10.3,1x)/)
36   format(1x,1pe10.3/)
    endif
c
    read(1,'(1x,/1x,/1x,/1x,/1x/)')
c
    str(1:20) = '(1x,18x, (f8.2,1x))'
    write(str(9:10),'(i2)') ie+1
    do 70 j = 1, jmax
70   read(1,str(1:20)) x(j), (t(j,i),i=1,ie)
c
    call fclose(1,'keep',ios)
c
c (3) temperatures: late-time solution, t[x,tau].

```

```
c      call tmpnl(tau,x,t,tm,ii,jj)
c
c (4) finish up: write data to file "wholen.dat";  "eta" & "tt" are dummies.
c
c      call finish(x,tau,t,eta,tt,tm,ii,jj,'wn')
c
990  stop
     end
```

c2345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

```
c
      subroutine tmpael(eta,t)
c
c temperature as a function of  $x/\sqrt{4\tau}$ . analytic and early-time
c history for cooling of a hot half-space brought instantaneously
c into contact with a cool half-space. thermal properties of the
c two bodies can differ, but are constants. the problem is
c a modification of the newmann problem discussed in chapter 11 of
c carslaw and jaeger, 1959, p. 288. sqkapd and tci must be set before
c calling this subroutine.
```

```
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      external erfunc
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
      common /propa/ rkd, rkm, sqkapd, sqkapm, p
```

```
c
      if (eta .lt. 0.0e0) then
        erfcx = 1.0e0 - erfunc(eta/sqkapd)
        t = tdi - (tdi-tci)*(2.0e0-erfcx)
      elseif (eta .eq. 0.0e0) then
        t = tci
      else
        erfcx = 1.0e0 - erfunc(eta)
        t = thi + (tci-thi)*erfcx
      endif
```

```
c
      return
      end
```

c-345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

subroutine tmpae2(eta,t)

c

c temperature as a function of  $x/\sqrt{4\tau}$ . analytic and early-time  
 c history for cooling of a hot half-space brought instantaneously  
 c into contact with a cool half-space. the hot body consists of a cool  
 c part and a hot part that is releasing additional heat due to  
 c crystallization. thermal properties in these three regions can  
 c differ, but are constant within each. the problem is a modification  
 c of the newmann problem discussed in chapter 11 of carslaw and jaeger,  
 c 1959, p. 288. tci, ts, xlam, sqkapm, and sqkapd must be set prior  
 c to calling this subroutine.

c

implicit real\*4 (a-h,o-z), integer\*4 (i-n)

external erfunc

common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,

+ xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,

+ jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,

+ bkapd, bkaph, iflag, itnum, err, jn

common /propa/ rkd, rkm, sqkapd, sqkapm, p

c

if (eta .lt. xlam) then

erfcx = 1.0e0 - erfunc(eta/sqkapm)

erfcl = 1.0e0 - erfunc(xlam/sqkapm)

t = tdi - (tdi-ts)\*(2.0e0-erfcx)/(2.0e0-erfcl)

elseif (eta .eq. xlam) then

t = ts

elseif (eta .lt. 0.0e0) then

erfx = erfunc(eta/sqkapd)

erfl = erfunc(xlam/sqkapd)

t = tci + (ts-tci)\*erfx/erfl

elseif (eta .eq. 0.0e0) then

t = tci

else

erfcx = 1.0e0 - erfunc(eta)

t = thi + (tci-thi)\*erfcx

endif

c

return

end



```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine tmpae3(x1,x2,y1,y2)
c
c interface equations for the generalized newmann problem of cooling
c with latent heat x1 released over the temperature interval between
c tdi to ts. these equations are derived by requiring that the heat
c lost from the zone of crystallizing magma be equal to that entering
c the zone of solidified magma (for y1), and that lost from the zone
c of solidified magma be equal to that entering the host rock (for y2).
c the first equation has a known temperature (ts) and an unknown
c position (x1); the second has a known position (0) and an unknown
c temperature (x2). called by solve2.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      external erfunc
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, x1, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
      common /propa/ rkd, rkm, sqkapd, sqkapm, p
c
      xld = x1/sqkapd
      erfld = erfunc(xld)
      tci = thi + rkd*(ts-thi)/(rkd-sqkapd*erfld)
      xlm = x1/sqkapm
      erfclm = 1.0e0 - erfunc(xlm)
      y1 = rkm*(tdi-ts)*exp(-xlm*xlm)*(sqkapd*erfld) +
+      rkd*(ts-x2)*exp(-xld*xld)*(sqkapm*(2.0e0-erfclm))
      y2 = tci - x2
c
      return
      end

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

subroutine tmpall(tau,x,t)

c

c temperature as a function of time and position. analytic, whole  
c time history for cooling of a heated slab embedded in an infinite  
c body. slab and body have identical, constant thermal properties.  
c carslaw and jaeger, 1959, p. 54, has an equivalent solution for a  
c coordinate system with an origin at the slab center.

c

implicit real\*4 (a-h,o-z), integer\*4 (i-n)

external erfunc

common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,  
+ xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,  
+ jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,  
+ bkapd, bkaph, iflag, itnum, err, jn

c

sqrttp = sqrt(4.0e0\*xkaph\*tau)

xl = (2.0e0\*dthck2+x)/sqrttp

x2 = x/sqrttp

erfxl = erfunc(xl)

erfx2 = erfunc(x2)

t = thi + (tdi-thi)\*0.5e0\*(erfxl-erfx2)

c

return

end

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

subroutine tmpal2(tau,x,t)

c

c temperature as a function of time and position. analytic, whole-time  
c history for cooling of a heated slab embedded in an infinite body.  
c although slab and body can have different thermal properties, they  
c are constants and not functions of temperature. solution given by  
c Lovering, 1936, geol. soc. am. bull. 47:87-100. sqkapd and p must be  
c set prior to calling this subroutine.

c

implicit real\*4 (a-h,o-z), integer\*4 (i-n)

external erfunc

common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,  
+ xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,  
+ jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,  
+ bkapt, bkaph, iflag, itnum, err, jn  
common /propa/ rkd, rkm, sqkapd, sqkapm, p

c

if (x/dthck2 .lt. 0.0e0) then

sqrm = sqrt(4.0e0\*xkapd\*tau)

xl = (2.0e0\*dthck2+x)/sqrm

x2 = (2.0e0\*dthck2-x)/sqrm

t = erfunc(xl) - p\*erfunc(x2)

do 20 l = 2, 50

xl = (2.0e0\*l\*dthck2+x)/sqrm

x2 = (2.0e0\*l\*dthck2-x)/sqrm

tt = (-p)\*\*(l-1)\*(erfunc(xl)-p\*erfunc(x2))

t = t + tt

if (abs(tt) .lt. 1.0e-6) goto 30

20 continue

30 xl = x/sqrm

t = thi + (tdi-thi)\*0.5e0\*(1.0e0+p)\*(t-erfunc(xl))

elseif (x/dthck2 .eq. 0.0e0) then

sqrh = sqrt(4.0e0\*xkaph\*tau)

xl = (2.0e0\*dthck2/sqkapd)/sqrh

t = erfunc(xl)

do 22 l = 2, 50

xl = (2.0e0\*l\*dthck2/sqkapd)/sqrh

tt = (-p)\*\*(l-1)\*erfunc(xl)

t = t + tt

if (abs(tt) .lt. 1.0e-6) goto 32

22 continue

32 t = thi + (tdi-thi)\*0.5e0\*(1.0e0-p\*p)\*t

else

sqrh = sqrt(4.0e0\*xkaph\*tau)

xl = ((2.0e0\*dthck2/sqkapd)+x)/sqrh

t = erfunc(xl)

do 21 l = 2, 50

xl = ((2.0e0\*l\*dthck2/sqkapd)+x)/sqrh

tt = (-p)\*\*(l-1)\*erfunc(xl)

t = t + tt

if (abs(tt) .lt. 1.0e-6) goto 31

21 continue

```
31      x1 = x/sqrh
      t = thi + (tdi-thi)*0.5e0*(1.0e0-p)*((1.0e0+p)*t-erfunc(x1))
endif
c
      return
end
```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

c

subroutine tmpal3(x,tm,taum)

c

c maximum temperature as a function of position. analytic, whole  
 c history for cooling of a heated slab embedded in an infinite body.  
 c although slab and body can have different thermal properties, they  
 c are constants and not functions of temperature. solution given by  
 c Lovering, 1936, geol. soc. am. bull. 47:87-100. sqkapd and p must be  
 c set prior to calling this subroutine.

c

implicit real\*4 (a-h,o-z), integer\*4 (i-n)

external tmpal2

common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,  
 + xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,  
 + jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,  
 + bkapt, bkaph, iflag, itnum, err, jn

c

c (1) search to find time when dtemp/dtime = 0, for  
 c a given x, then calculate temperature at that time.

c

chart = dthck2\*dthck2/xkaph  
 do 10 j = 1, 25  
 taum0 = 0.99e0\*taum  
 tauml = 1.01e0\*taum  
 dtaum = tauml - taum0  
 dtaum0 = taum - taum0  
 dtauml = tauml - taum  
 call tmpal2(taum,x,tm)  
 call tmpal2(taum0,x,tm0)  
 call tmpal2(tauml,x,tml)  
 f = (tml-tm0)/dtaum  
 f0 = (tm-tm0)/dtaum0  
 f1 = (tml-tm)/dtauml  
 fp = (f1-f0)/((dtaum0+dtauml)/2.0e0)  
 er = -f/fp  
 taum = taum + er  
 if (abs(er/chart) .lt. 1.0e-3) then  
 call tmpal2(taum,x,tm)  
 return  
 endif  
 10 continue

c

if (j .ge. 25) then  
 write(0,25)  
 25 format('/ tmpal4: loop not converging!'/)  
 stop  
 endif

c

end

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine tmpnl(tau,x,t,tm,ii,jj)
c
c  temperature as a function of time and position.  numerical & late-
c  time history for cooling of a heated slab embedded in an infinite
c  body.  slab and body can have different temperature-dependent
c  thermal properties.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      parameter (jjj=600)
      dimension tau(ii), x(jj), t(jj,ii), ttl(jjj), tt2(jjj),
+      xkl(jjj), xk2(jjj), xkap1(jjj), xkap2(jjj), tm(jj)
      external tmpn11, tmpn12
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+      xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+      jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+      bkaph, bkaph, iflag, itnum, err, jn
c
c (1) initialize tt2(j) to t(j,ie), xk2(j) and rhc2(j).  tt2(j) is the
c best guess of the temperature of the current time; t(j,i) is the
c temperature at the last time, tau(i); xk2(j) is the thermal
c conductivity at the best guess of the temperature of the current
c time, as is heat capacity rhc2(j).  ttl, xkl & rhcl are temperature,
c conductivity & heat capacity at last successful time step.
c
      jn = jmax - 1
      do 1 j = 1, jc-1
        tt2(j) = t(j,ie)
1      tm(j) = tdi
        tt2(jc) = t(jc,ie)
        tm(jc) = tci
      do 2 j = jc+1, jn
        tt2(j) = t(j,ie)
2      tm(j) = thi
        tm(jmax) = thi
c
      call tmpn11(tt2,xk2,xkap2,jjj)
c
c (2) step through successive temperatures.  this gets a bit confusing.
c outside loop increments to the next time when temperatures will be
c saved in the matrix t(j,i), tau(i).  the next loop increments itnum
c times from tau(i-1) to tau(i).  the inside loop is only used if
c thermal properties are nonconstant, and is the iterative improvement.
c
c primary loop point; loops are for i = ie, ie+1, ie+2, ... imax.
c define time step for 2nd loop, and normalize it by dyke_thick**2.
c
      do 10 i = ie + 1, imax
        dxtau = dx*dx/((tau(i)-tau(i-1))/itnum)
c
c secondary loop point; itnum steps between successive values of i.
c at top of loop, a successful time step has just been completed, so
c that tt2, rhc2 & xk2 are assigned to ttl, rhcl & xkl; temperatures

```

c at the next time are then computed.

c

```
do 20 ii = 1, itnum
  do 29 j = 1, jn
    tt1(j) = tt2(j)
    xkap1(j) = xkap2(j)
29    xk1(j) = xk2(j)
```

c

```
call tmpnl2(dxtau,tt1,tt2,xk1,xk2,xkap1,xkap2,jjj)
```

c

c tertiary loop point; iterative improvement, if necessary.  
 c tt2 is used to calculate temperature-dependent thermal props.  
 c t(j,i) is used only to save storage, and compare previous guess  
 c with the newest guess. if they are very nearly the same, then  
 c solution has converged and is ready to leave this loop and go  
 c to the next time step.

c

```
if (bkd+bkh+bkapd+bkaph .ne. 0.0e0) then
  do 30 iii = 1, 10
    do 31 j = 1, jn
31      t(j,i) = tt2(j)
        call tmpnl1(tt2,xk2,xkap2,jjj)
        call tmpnl2(dxtau,tt1,tt2,xk1,xk2,xkap1,xkap2,jjj)
        terr = abs(t(1,i)-tt2(1))
        do 32 j = 2, jn
32          terr = amax1(terr,abs(t(j,i)-tt2(j)))
            if (terr/(tdi-thi) .lt. err) goto 22
30      continue
22      if (iii .ge. 10) then
        write(0,21)
21      format(/' problem in tempnl: not converging')
        stop
      endif
    endif
```

c

c end of 3rd loop.

c

c at each time step, see if temperatures at each x-node have peaked  
 c out. if so, this is the maximum temperature attained at that  
 c position in the host rock

c

```
do 28 j = jc, jmax-1
28    tm(j) = amax1(tm(j),tt2(j))
20    continue
```

c

c end of 2nd loop.

c

```
do 11 j = 1, jn
11    t(j,i) = tt2(j)
        t(jmax,i) = thi
        write(6,12) tau(1), t(1,i), t(jc,i)
12    format(/' time = ',1pg11.4,' sec.: ',
+          ' temperature: dike center = ',1pg11.4,' deg. c',
+          /)
```

```

+                                     contact = ',lpgll.4,' deg. c')
10  continue
c
c end of 1st loop.
c
c now find x-nodes where temperatures have not yet peaked out.
c
      do 9 j = jn, jc, -1
        if (tm(j) .gt. tt2(j)) goto 8
9      tm(j) = thi
c
8      write(6,90)
90     format(/' numerical late-time solution is finished')
      terr = abs((t(jn,imax)-thi))
      if (terr/(tdi-thi) .gt. err/10.0e0) write(0,91)
91     format(/' beware! temperatures near the node furthest from the'/
+           ' dike are no longer equal to thi. perhaps the input'/
+           ' parameter ndt, in program earlya or earlyn,'
+           ' should be increased.'/)
c
      return
      end

```



```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine tmpn11(tt2,xk2,xkap2,jjj)
c
c initialize tt2, xk2 and rhc2. these are vectors of temperature,
c conductivity and heat capacity to be used as the "current guess" at
c each time step.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      dimension tt2(jjj), xk2(jjj), xkap2(jjj)
      external condd, condh, diffd, diffh
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+               xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+               jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+               bkapd, bkaph, iflag, itnum, err, jn
c
c heat capacity is conductivity/diffusivity, and is calculated at each
c x-node. at contact it is averaged between dike and host-rock.
c
      do 1 j = 1, jc-1
        xk2(j) = condd(tt2(j))
1       xkap2(j) = diffd(tt2(j))
c
      xk2(jc) = (condd(tt2(jc))+condh(tt2(jc)))/2.0e0
      xkap2(jc) = (diffd(tt2(jc))+diffh(tt2(jc)))/2.0e0
c
      do 2 j = jc+1, jn
        xk2(j) = condh(tt2(j))
2       xkap2(j) = diffh(tt2(j))
c
      return
      end

```

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine tmpnl2(dxtau,ttl,tt2,xk1,xk2,xkap1,xkap2,jjj)
c
c finite difference equations for the cooling of a dyke (-dthck2 <= x
c <= 0) adjacent to host rocks (x >= 0), where both magma and host
c rocks have temperature-dependent thermal conductivity and heat
c capacity. the difference equations use the crank-nicolson approach
c which is unconditionally stable and has second-order accuracy.
c this routine is called iteratively: a succession of guesses of the
c new temperature, t(j,1), is used to estimate the values of
c conductivity, xk2, and heat capacity, rhc, so that the sytem of
c equations can be solved.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      parameter (j4=600)
      dimension a(j4), b(j4), c(j4), yy(j4), ttl(jjj),
+      tt2(jjj), xk1(jjj), xk2(jjj), xkap1(jjj), xkap2(jjj)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+      xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+      jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+      bkapd, bkaph, iflag, itnum, err, jn
c
c (2) prepare coefficients for first eqn., x = -dthck2, the center
c of the dike. at that node, x(1), the temp gradient is zero. from
c symmetry, the temp. at the "imaginary" node on the far side of the
c dike center is the same as at the first node in from the center.
c thus, t(x(0)) = t(x(2)), where t(x(1)) is the temperature at the
c dike center.
c
      xkap = (xkap1(1)+xkap2(1))/2.0e0
      xtxkap = dxtau/xkap
      a(1) = 0.0e0
      b(1) = -2.0e0*(1.0e0+xtxkap)
      c(1) = 2.0e0
      yy(1) = 2.0e0*(1.0e0-xtxkap)*ttl(1) - 2.0e0*ttl(2)
c
c (3) prepare values for -dthck2 < x < infinity -- actually, just
c short of infinity, the third to last node.
c
      do 20 j = 2, jn-1
        xkap = (xkap1(j)+xkap2(j))/2.0e0
        xtxkap = dxtau/xkap
        xk = (xk1(j)+xk2(j))/2.0e0
        dxk1 = (xk1(j+1)-xk1(j-1))/(xk*4.0e0)
        dxk2 = (xk2(j+1)-xk2(j-1))/(xk*4.0e0)
        a(j) = 1.0e0 - dxk2
        b(j) = -2.0e0*(1.0e0+xtxkap)
        c(j) = 1.0e0 + dxk2
        yy(j) = 2.0e0*(1.0e0-xtxkap)*ttl(j)
+      - (1.0e0-dxk1)*ttl(j-1) - (1.0e0+dxk1)*ttl(j+1)
      20 continue
c
c (4) prepare values for x = infinity. here, the next value of

```

c temperature is known as a boundary condition, and can therefore  
c be put on the "right-hand-side" of the system of eqns.  
c thus,  $t(x(jn+1)) = th1$ , which is known for all time steps.

```
c
      xkap = (xkap1(jn)+xkap2(jn))/2.0e0
      xtxkap = dxtau/xkap
      xk = (xk1(jn)+xk2(jn))/2.0e0
      dxk1 = (xkh-xk1(jn-1))/(xk*4.0e0)
      dxk2 = (xkh-xk2(jn-1))/(xk*4.0e0)
      a(jn) = 1.0e0 - dxk2
      b(jn) = -2.0e0*(1.0e0+xtxkap)
      c(jn) = 0.0e0
      yy(jn) = 2.0e0*(1.0e0-xtxkap)*ttl(jn)
+      - (1.0e0-dxk1)*ttl(jn-1) - 2.0e0*(1.0e0+dxk1)*th1
c
c (5) solve for tt2
c
      call thomas(jn,a,b,c,tt2,yy,jjj)
c
      return
      end
```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function condd(t)
c
c thermal conductivity of dike rock from temperature:  $k = a + b/t[k]$ 
c           for basalt:  $a = 0.6893$ ,  $b = 522.3$ 
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      condd = akd + bkd/(273.15e0+t)
c
      return
      end
```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function condmd(t)
c
c thermal conductivity modulus of magma from temperature, (dk/dT)/k.
c thermal conductivity:  $k = a + b/t$  [k]
c           for basalt:  $a = 0.6893$ ,  $b = 522.3$ 
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      tt = 273.15e0 + t
      xk = akd + bkd/tt
      condmd = -(1.0e0/xk)*bkd/(tt*tt)
c
      return
      end
```

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function diffd(t)
c
c diffusivity of dike rock, kap[m*2/s] = a + b/t[k]
c       for basalt: a = 0.3052e-6,  b = 0.1247e-3
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      external condd
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      diffd = akapd + bkapd/(t+273.15e0)
c
c take heat of crystallization into account, if necessary.
c
      if ((t.gt.ts) .and. (abs((tdi-ts)/(tdi-thi)).gt.1.0e-4)) then
        xk = condd(t)
        diffd = xk/((xk/diffd)+xl/(tdi-ts))
      endif
c
      return
      end

```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function condh(t)
c
c thermal conductivity of host rock from temperature:  $k = a + b/t[k]$ 
c       for basalt: a = 0.6893, b = 522.3
c       sandstone:  = 0.4049,   = 732.9
c       limestone:  = 0.2101,   = 630.3
c       granite:    = 0.5543,   = 567.4
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      condh = akh + bkh/(273.15e0+t)
c
      return
      end
```

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function condmh(t)
c
c thermal conductivity modulus of host rock from temperature, (dk/dT)/k.
c thermal conductivity:  $k = a + b/t$  [k]
c       for basalt: a = 0.6893, b = 522.3
c       sandstone:  = 0.4049,  = 732.9
c       limestone:  = 0.2101,  = 630.3
c       granite:    = 0.5543,  = 567.4
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      tt = 273.15e0 + t
      xk = akh + bkh/tt
      condmh = -(1.0e0/xk)*bkh/(tt*tt)
c
      return
      end

```



```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function diffh(t)
c
c diffusivity of host rock: kap[m*2/s] = a + b/t[k]
c       for basalt: a = 0.3052e-6,  b = 0.1247e-3
c       sandstone:  = 0.5773e-7    = 0.3032e-3
c       limestone:  = 0.1464e-6    = 0.1805e-3
c       granite:    = 0.3147e-6    = 0.3172e-3
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+             xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+             jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+             bkapd, bkaph, iflag, itnum, err, jn
c
      diffh = akaph + bkaph/(273.15e0+t)
c
      return
      end
```

c-345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

```

c
      subroutine start(x,tau,t,eta,tt,ii,jj)
c
c initialize various vectors and quantities used in calculations. this
c subroutine is called by earlya, earlyn, wholea, where storage is set
c for the variables initialized here.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      dimension tau(ii), x(jj), t(jj,ii), eta(jj), tt(jj)
      character ans*1
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+                xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+                jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+                bkapd, bkaph, iflag, itnum, err, jn
c
c (1) make vector x.
c
c ndt : number of dike thickness solution will be taken from contact.
c nndt: number of nodes per dike thickness.
c jmax: total number of nodes. (jmax-1)/2 must be an even number,
c       and jmax must be less than jj.
c jc  : index where x(jc) = 0 = dike contact.
c dx  : distance between x-points.
c
      write(6,1)
1      format(/'  ndt: # of dike half-thicknesses away from contact'
+            /'      that are to be included in solution'
+            // '    & EARLYA   if output will be used by &'
+            /'    & EARLYN   WHOLEN, then ndt > 15   &'
+            // ' nndt: # of nodes per dike half-thickness.'
+            // ' (ndt+1)*nndt <= 600,                ndt, nndt = '$)
      read(5,*) ndt, nndt
c
      do 7 j = 0, 10
        nndt = nndt + j
        jmax = nndt*(ndt+1) + 1
        jmax2 = (jmax-1)/2
        if (jmax-1 .eq. jmax2*2) goto 8
7      continue
8      if (jmax .gt. jj) then
        write(6,2)
2      format(/' Too many nodes!!!')
        stop
      endif
      jc = nndt + 1
      dx = dthck2/nndt
      do 3 j = 1, jmax
3      x(j) = -dthck2 + (j-1)*dx
c
c (2) make vector eta = x/sqrt(4*kappa_h*tau) and associated indeces
c
c kc: index where eta(kc) = 0 = dike contact.
c nk: number of nodes between successive values of eta such that

```

```

c      at least 100 nodes are used in each numerical integration
c      of the early-time equations.
c
c      deta = 5.0e0/(jmax-1)
c      do 6 k = 1, jmax
6      eta(k) = (-2.5e0) + (k-1)*deta
c      kc = 2.5e0/deta + 1
c      do 4 nk = 1, 200
c        if (nk*kc .ge. 100) goto 5
4      continue
5      continue
c
c (3) get times when temperatures are to be calculated. there are
c ii times, but the first one must be 0. the times are stored in the
c files TAUN.DAT or TAUD.DAT, one time per line. TAUD.DAT must have
c time values in units of seconds; TAUN.DAT has nondimensional times,
c which are converted to dimensional values using dyke half-thickness
c and the diffusivity of the host rocks at ambient temperature.
c
c imax : number of times when solutions are calculated (<=ii).
c ie   : number of times when solutions are calculated
c        using early-time approximations.
c penet: penetration time for temperatures to first begin
c        dropping at dike center. approximate and
c        conservatively estimated.
c chart: characteristic cooling time, used to convert from
c        nondimensional to dimensional times. most cooling
c        is finished when tau = chart.
c
c      chart = dthck2*dthck2/xkaph
c      penet = 0.5e0*(dthck2*dthck2/(16.0e0*xkapd))
c      ie = 0
c
c      write(6,11)
11     format(/' input times are in files TAUD.DAT [Dimensional]'
+           /'                               or TAUN.DAT [Nondimensional]'
+           /' which one?? [d/n] ? '$)
c      read(5,'(1a)') ans
c      if ((ans .eq. 'n') .or. (ans .eq. 'N')) then
c        call fopen(1,'TAUN.DAT','old','exclusive',ios0)
c        if (ios0 .ne. 0) stop
c        read(1,*) imax
c        read(1,*) (tau(i), i=1,imax)
c        do 10 i = 2, imax
c          tau(i) = tau(i)*chart
c          if ((tau(i) .ge. penet) .and. (ie .eq. 0)) ie = i - 1
10     if ((i .eq. imax) .and. (ie .eq. 0)) ie = imax
c      rewind(1)
c      write(1,'(1x,i4)') imax
c      write(1,'(1x,1pg14.5)') (tau(i)/chart, i=1,imax)
c      call fopen(2,'TAUD.DAT','unknown','exclusive',ios1)
c      if (ios1 .ne. 0) stop
c      write(2,'(1x,i4)') imax
c      write(2,'(1x,1pg14.5)') (tau(i), i=1,imax)

```

```

else
  call fopen(1,'TAUD.DAT','old','exclusive',ios0)
  if (ios0 .ne. 0) stop
  read(1,*) imax
  read(1,*) (tau(i), i=1,imax)
  do 12 i = 2, imax
    if ((tau(i) .ge. penet) .and. (ie .eq. 0)) ie = i - 1
12    if ((i .eq. imax) .and. (ie .eq. 0)) ie = imax
  rewind(1)
  write(1,'(lx,i4)') imax
  write(1,'(lx,lpg14.5)') (tau(i), i=1,imax)
  call fopen(2,'TAUN.DAT','unknown','exclusive',ios1)
  if (ios1 .ne. 0) stop
  write(2,'(lx,i4)') imax
  write(2,'(lx,lpg14.5)') (tau(i)/chart, i=1,imax)
endif
call fclose(1,'keep',ios0)
call fclose(2,'keep',ios1)
c
write(6,90) jmax, dx
90  format(/' total number of nodes, jmax = ',i4
+      /' spacing between nodes,   dx = ',lpg11.4,' meters'/)
c
return
end

```

c-345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2

```

c
      subroutine finish(x,tau,t,eta,tt,tm,ii,jj,meth)
c
c write data to file.  output units of time can be hours, days, years.
c starting with a summary of the input parameters, the remainder of the
c file is a matrix.  the first column is distance, starting at the dike
c center (x=-dthck2), and going past the contact (x=0) to some
c specified distance.  the remaining columns are temperatures at times
c that are labelled above each column.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      dimension tau(ii), x(jj), t(jj,ii), eta(jj), tt(jj), tm(jj)
      character meth*2, str*50, time*5
      common /prop/ tdi, thi, dthck2, xkaph, xkapd, xkapm, xkh, xkd,
+                xkm, xl, ts, xlam, tci, dx, deta, imax, ie, jmax,
+                jc, nk, kc, akd, akh, akapd, akaph, bkd, bkh,
+                bkaph, bkapd, iflag, itnum, err, jn
c
c (1) figure out best units for output times
c
      chart = dthck2*dthck2/xkaph
      if (chart .lt. 1.0e6) then
        time = 'hours'
        tunit = 3600.0e0
      elseif (chart .lt. 8.6e7) then
        time = 'days'
        tunit = 3600.0e0*24.0e0
      else
        time = 'years'
        tunit = 3600.0e0*24.0e0*365.25e0
      endif
c
c (2) open output file
c
      if (meth .eq. 'ea') then
        call fopen(1,'EARLYA.DAT','unknown','exclusive',ios)
      elseif (meth .eq. 'en') then
        call fopen(1,'EARLYN.DAT','unknown','exclusive',ios)
      elseif (meth .eq. 'wa') then
        call fopen(1,'WHOLEA.DAT','unknown','exclusive',ios)
      else
        call fopen(1,'WHOLEN.DAT','unknown','exclusive',ios)
      endif
      if (ios .ne. 0) stop
c
c (3) put out general conditions
c
      if (meth(1:1) .eq. 'e') then
        write(1,10) ie, jmax, tdi, thi, tci, dthck2, dx, jc, meth(2:2)
        write(1,20) xl, ts, xlam
        write(1,30) xkd, xkapd, xkh, xkaph
        if (meth(2:2) .eq. 'n') then
          write(1,34) akd, bkd, akapd, bkaph
        
```

```

    write(1,35) akh, bkh, akaph, bkaph
    write(1,36) err
endif
write(1,60) time
str(1:14) = `(1x, (f11.3))`
write(str(5:6),`(i2)` ) ie
write(1,str(1:14)) (tau(i)/tunit,i=1,ie)
write(1,`( / ) `)
str(1:27) = `(1x,3(f8.2,1x), (f8.2,1x))`
write(str(16:17),`(i2)` ) ie
do 70 j = 1, jmax
70   write(1,str(1:27)) eta(j), tt(j), x(j), (t(j,i),i=1,ie)
else
write(1,10) imax, jmax, tdi, thi, tci, dthck2, dx, jc, meth(2:2)
write(1,30) xkd, xkapd, xkh, xkaph
if (meth(2:2) .eq. `n`) then
    write(1,34) akd, bkd, akapd, bkapd
    write(1,35) akh, bkh, akaph, bkaph
    write(1,36) err
endif
write(1,61) time
str(1:14) = `(1x, (f10.2))`
write(str(5:6),`(i2)` ) imax
write(1,str(1:14)) (tau(i)/tunit,i=1,imax)
write(1,`( / ) `)
str(1:32) = `(1x,f9.3,1x,f6.1,2x, (f6.1,1x))`
write(str(21:22),`(i2)` ) imax
do 71 j = 1, jmax
71   write(1,str(1:32)) x(j), tm(j), (t(j,i),i=1,imax)
endif
c
    call fclose(1,`keep`,ios)
c
990   return
c
c (4) formats
c
10   format(1x,i4,` = number of temperature-distance profiles`/
+       1x,i4,` = number of distance data points`//
+       1x,lpel0.3,` deg c = initial temperature of dike rocks`/
+       1x,lpel0.3,` deg c = initial temperature of host rocks`/
+       1x,lpel0.3,` deg c = initial temperature at contact`//
+       1x,lpel0.3,` meters = dike half-thickness`/
+       1x,lpel0.3,` m = distance between distance data points`/
+       1x,i4,` = index number for x(jc) = 0 = dyke wall`//
+       1x,a1,` = solution method (a = analytic, n = numeric)`//)
20   format(1x,lpel0.3,` j/m*m*m = total heat of crystallization`/
+       1x,lpel0.3,` deg c = solidus temperature`/
+       1x,lpel0.3,` = x(solidus)/sqrt(4*kappa_h*tau)`//)
30   format(1x,lpel0.3,` w/m deg.c = k_m, conductivity, dike rocks`/
+       1x,lpel0.3,` m*m/s = kappa_m, diffusivity, dike rocks`/
+       1x,lpel0.3,` w/m deg.c = k_h, conductivity, host rocks`/
+       1x,lpel0.3,` m*m/s = kappa_h, diffusivity, host rocks`//)
34   format(1x,4(lpel0.3,1x),`a_k, b_k, a_kap, b_kap -- dike rocks`//)

```

```
35  format(1x,4(1pe10.3,1x),`a_k, b_k, a_kap, b_kap -- host rocks`/)  
36  format(1x,1pe10.3,` = fractional maximum relative error`/)  
60  format(1x,`      eta  t(eta)      x      t(x) with `,a5,  
+    1x,` = time units; values on next line.`/)  
61  format(1x,`      x      t_max  t(x) with `,a5,  
+    1x,` = time units; values on next line.`/)  
c  
  end
```

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      function erfunc(z)
c
c the error function; numerical recipes, p. 164
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
c
      x = abs(z)
      t = 1.0e0/(1.0e0+0.5e0*x)
      arg = x*x + 1.26551223e0 - t*(1.00002368e0+t*(0.37409196e0+
+          t*(0.09678418e0+t*(-0.18628806e0+t*(0.27886807e0+
+          t*(-1.13520398e0+t*(1.48851587e0+t*(-0.82215223e0+
+          t*0.17087277e0)))))))))
c
      if (z .ge. 0.0e0) then
        if (arg .gt. 10e0) then
          erfunc = 1.0e0
        else
          erfunc = 1.0e0 - t*exp(-arg)
        endif
      else
        if (arg .gt. 10.0e0) then
          erfunc = -1.0e0
        else
          erfunc = -1.0e0 + t*exp(-arg)
        endif
      endif
c
      return
      end

```



```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine oderk2(h,t,y,deriv,istart)
c
c solve the system of 2 first-order ordinary differential equations:
c
c  $dy(i)/dt = f(i,t,y(1),y(2))$ , for  $i = 1, 2$ 
c
c this routine advances the solution by a distance h employing a
c fourth-order runge_kutta method. preceeding the first call, istart
c must be set to 1. upon input, t is the current distance, y is the
c current solution of the system of ordinary differential equations
c as given in subroutine deriv, wk is a work space that must be saved
c between calls to oderk. upon output, t is updated, to t+h, solution
c y is updated by  $dy(i)/dt = f(i,t+h,y(1),y(2))$ , and istart = 2 to
c signal a successful integration.
c
      implicit real*8 (a-h,o-z), integer*4 (i-n)
      dimension a(4), b(4), c(4), y(2), wk(2,2)
      external deriv
      data a /0.5e0, 0.292893219e0, 1.707106781e0, 0.166666667e0/
      data b /2.0e0, 1.0e0, 1.0e0, 2.0e0/
      data c /0.5e0, 0.292893219e0, 1.707106781e0, 0.5e0/
c
      if (istart .ne. 2) then
        wk(1,2) = 0.0e0
        wk(2,2) = 0.0e0
        qt = 0.0e0
        istart = 2
        call deriv(t,y,wk)
      endif
c
      do 105 j = 1, 4
        do 104 i = 1, 2
          temp = a(j)*(wk(i,1)-b(j)*wk(i,2))
          w = y(i)
          y(i) = y(i) + h*temp
          temp = (y(i)-w)/h
104      wk(i,2) = wk(i,2) + 3.0e0*temp - c(j)*wk(i,1)
          temp = a(j)*(1.0e0-b(j)*qt)
          w = t
          t = t + h*temp
          temp = (t-w)/h
          qt = qt + 3.0e0*temp - c(j)
          call deriv(t,y,wk)
105      continue
c
      return
      end

```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine thomas(n,a,b,c,x,y)
c
c the thomas algorithm is an efficient method for solving a tri-
c diagonal system of equations. the 3 central diagonals of the
c matrix are given as the 3 vectors a, b, c, each of length n. b is
c the central vector. the first element of a and the last of c are
c never referenced. note that no element of b can equal 0, and that
c b and y are altered by this routine.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      dimension a(*), b(*), c(*), x(*), y(*)
c
c forward elimination
c
      do 2 i = 2, n
        w = a(i)/b(i-1)
        b(i) = b(i) - c(i-1)*w
2      y(i) = y(i) - y(i-1)*w
c
c back substitution.
c
      x(n) = y(n)/b(n)
      do 3 i = n-1, 1, -1
3      x(i) = (y(i)-c(i)*x(i+1))/b(i)
c
      return
      end
```

```

c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine solve2(func,a,b,error,itmax)
c
c determination of the roots to a system of 2 equations for 2 unknowns,
c  $f(x) = 0$ , where  $x(1)$  and  $x(2)$  are the unknowns and  $f(1)$  and  $f(2)$ 
c are the equations. upon input,  $x$ , a vector of length 2, is the
c initial guess of the roots; as output, it is the solution. upon
c input, itmax, is the maximum allowable number of iterations, or
c guesses; as output, it is the number of guesses required to find
c the solution. error is the allowable difference between an exact
c and acceptable solution.
c
      implicit real*4 (a-h,o-z), integer*4 (i-n)
      dimension y(2), x1(2), y1(2), x2(2), y2(2), ddx(2)
      external func
c
c begin by checking to see if present guess of  $x$  is a solution.
c
      do 1 j = 1, itmax
        call func(a,b,y(1),y(2))
        if ((abs(y(1)) .lt. error) .and. (abs(y(2)) .lt. error)) then
          itmax = j
          return
        else
91      write(6,91) a, b, y(1), y(2)
      format('for x(1,2) = ',2(1pg11.4,1x),
+        ', func(x(1,2)) = ',2(1pg11.4,1x))
      ddx(1) = 1.0e-4*a
      ddx(2) = 1.0e-4*b
      x1(1) = a + ddx(1)
      x1(2) = b
      x2(1) = a
      x2(2) = b + ddx(2)
      call func(x1(1),x1(2),y1(1),y1(2))
      call func(x2(1),x2(2),y2(1),y2(2))
      dy1dx1 = (y1(1)-y(1))/ddx(1)
      dy1dx2 = (y2(1)-y(1))/ddx(2)
      dy2dx1 = (y1(2)-y(2))/ddx(1)
      dy2dx2 = (y2(2)-y(2))/ddx(2)
      det = dy1dx1*dy2dx2 - dy2dx1*dy1dx2
      ddx(1) = (y(2)*dy1dx2-y(1)*dy2dx2)/det
      ddx(2) = (y(1)*dy2dx1-y(2)*dy1dx1)/det
      a = a + ddx(1)
      b = b + ddx(2)
        endif
1      continue
c
      itmax = j
      write(6,90) itmax
90      format(/'solve2 failed after ',i4,' iterations'/)
      return
      end

```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine fopen(unit,name,status,acces,iostat)
c
c   note that this subroutine is highly system dependent; beware.
c
      integer unit,iostat
      character*(*) name,status,access
c
      open(unit,status=status,iostat=iostat)
c
      return
      end
```

```
c 345678-1-2345678-2-2345678-3-2345678-4-2345678-5-2345678-6-2345678-7-2
c
      subroutine fclose(unit,status,iostat)
c
c   note that this subroutine is highly system dependent; beware.
c
      integer unit,iostat
      character*(*) status
      close(unit,status=status,iostat=iostat)
c
      return
      end
```

Table 1: Symbols Used

$\underline{C}$	heat capacity per kilogram mass (at constant volume)
$\underline{h}$	heat of crystallization
$\underline{k}$	thermal conductivity
$\underline{Q}$	heat flux, $-\underline{k} \cdot \partial \theta / \partial \underline{X}$
$\underline{T}$	dike thickness
$\underline{t}$	time
$\underline{\tau}$	time, $\underline{\tau} = \underline{\kappa}_{hi} / (\underline{T}/2)^2$
$\underline{X},$	coordinate $_{hi}$ pointed away from dike wall
$\underline{x}$	coordinate pointed away from dike wall, $\underline{x} / (\underline{T}/2)$
$\underline{\eta}$	similarity variable, $\underline{x} / \sqrt{4 \underline{\kappa}_{hi} \underline{t}}$
$\theta$	temperature
$\theta$	temperature, $(\theta - \theta_{hi}) / (\theta_{mi} - \theta_{hi})$
$\underline{\kappa}$	diffusivity, $\underline{k} / (\rho \underline{C})$
$\lambda$	similarity constant, $\chi_s / \sqrt{4 \underline{\kappa}_{hi} \underline{t}}$
$\rho$	density
$\underline{x}$	interface position

## Subscripts

c	dike contact
h	host rock
i	initial
m	magma
s	solidus

TABLE 2: Subroutines and Functions.

START	Initialize distance arrays for $X$ and $\eta$ ; read input times in non-dimensional $\tau$ or dimensionnal $\underline{t}$ form; perform initial estimate to find greatest time when early-time solutions apply.
FINISH	Write results to file, including all parameters; times are converted to units of hours, days, or years.
TMPAE1	Analytic early-time, calculate $\Theta(\eta)$ for $(\rho h)_m = 0$ (eqs. 13b,c).
TMPAE2	Anal. early-time, calculate $\Theta(\eta)$ for $(\rho h)_m \neq 0$ (eqs. 13a,b,c).
TMPAE3	Anal. early-time, calculate $\Theta_{ci}$ and $\lambda_s$ (eqs. 14a,b), called before TMPAE1 or TMPAE2.
TMPAL1	Anal. whole-time, calculate $\Theta(\underline{X}, \underline{t})$ for $\frac{k_m}{k_h} = \kappa_m / \kappa_h = 1$ (eq. 18).
TMPAL2	Anal. whole-time, calculate $\Theta(\underline{X}, \underline{t})$ for $\frac{k_m}{k_h} \neq 1, \kappa_m / \kappa_h \neq 1$ (eqs. 15a,b).
TMPAL3	Anal. whole-time, calculate $\Theta_{\max}(\underline{X})$ .
TMPNE1	Numeric early-time, driving routine for numerical integrator, called by SOLVE2, calls ODERK2.
TMPNE2	Num. early-time, called by integrator to evaluate eqs. 20, 21, called by ODERK2.
TMPNE3	Num. early-time, convert $\Theta(\eta)$ to $\Theta(\underline{X}, \underline{t})$ .
TMPNL	Num. late-time, driving routine, calls TMPNL1, TMPNL2
TMPNL1	Num. late-time, set arrays of temperatures and rock properties for current time step.
TMPNL2	Numeric late-time, set up eqs. 22a,b,c, calls THOMAS.
ERFUNC	(function) The error function.
SOLVE2	Newton-Raphson iteration to solve 2 equations with 2 unknowns.
ODERK2	Fourth-order Runge-Kutta solution for 2 1st-order ordinary differential equations.
THOMAS	Thomas algorithm for solving a tridiagonal system of equations.
CONDM	(function) Calculate $\frac{k_m}{k_h}(\theta)$ using eq. 1a.
CONDH	(function) Calculate $\frac{k_h}{k_m}(\theta)$ using eq. 1a.
CONDMM	(function) Calculate $\gamma_m(\theta)$ using eq. 2.
CONDMH	(function) Calculate $\gamma_h(\theta)$ using eq. 2.
DIFFM	(function) Calculate $\kappa_m(\theta)$ using eq. 1b, or $\kappa'_m$ using eqs. 1b, 3 if $\theta > \theta_s$ and $(\rho h)_m \neq 0$ .
DIFFH	(function) Calculate $\kappa_h(\theta)$ using eq. 1b.
FOPEN	open a file
FCLOSE	close a file

Table 3: Linking programs to  
subroutines and functions.

Analytical		Numerical	
EARLYA	WHOLEA	EARLYN	WHOLEN
START	START	START	TMPNL
TMPAE1	TMPAE1	SOLVE2	TMPNL1
TMPAE2	TMPA11	TMPNE3	TMPNL2
FINISH	TMPA12	FINISH	FINISH
SOLVE2	TMPA13	TMPNE1	THOMAS
TMPAE3	FINISH	ODERK2	CONDM
ERFUNC	ERFUNC	TMPNE2	CONDMM
FOPEN	FOPEN	CONDM	DIFFM
FCLOSE	FCLOSE	CONDMM	CONDH
		DIFFM	CONDMH
		CONDH	DIFFH
		CONDMH	FOPEN
		DIFFH	FCLOSE
		FOPEN	
		FCLOSE	



Table 4: Examples of files TAU.DAT, DTAU.DAT

TAU.DAT	DTAU.DAT (seconds)
$(\underline{t} \cdot (\underline{T}/2)^2 / \kappa_{hi})$	(equivalent to TAU.DAT if $\underline{T}/2 = 1$ meter and $\kappa_{hi} = 0.75 \times 10^{-6} \text{ m}^2/\text{s}$ )
13	13
0.0000	0.0000
2.0000e-3	2.6667e3
5.0000e-3	6.6667e3
1.0000e-3	1.3333e4
2.0000e-2	2.6667e4
5.0000e-2	6.6667e4
1.0000e-2	1.3333e5
2.0000e-1	2.6667e5
5.0000e-1	6.6667e5
1.0000e-1	1.3333e6
2.0000e0	2.6667e6
5.0000e0	6.6667e6
1.0000e1	1.3333e7

Table 5: Examples for keyboard input

	EARLYA	WHOLEA	EARLYN	WHOLEN
include heat of crystallization ? (y/n)	y		n	
dike thickness (m)	1	1	1	
initial temperature, magma & host rock (°C)	1150 50	1150 50	1150 50	
conductivity, magma & host rock (W/m·°C)	2.25 2.25	2.25 2.25		
conductivity coefficients a1 & b1: dike rock			0.689 522	
host rock			0.250 944	
diffusivity, magma host rock (m <sup>2</sup> /s)	7.5e-7 7.5e-7	7.5e-7 7.5e-7		
diffusivity coefficients a2 & b2: dike rock			3.06e-7 1.25e-4	
host rock			1.80e-7 2.50e-4	
latent heat (MJ/m <sup>3</sup> )	900e+6			
solidus temperature (°C)	950			
guess initial dike- contact temperature (°C)	700		600	
guess $\lambda_s$	-0.4			
relative error			1.0e-4	
number of dike thicknesses from contact, & number of points per dike thick- ness, where temperatures are to be calculated.	3 30	3 30	19 30	
times when temperatures are to be calculated are in file TAU.DAT (nondimen- sional) or DTAU.DAT dimensional) (n/d)	n	n	d	
read input from EARLYA.DAT (analytic early time) or EARLYN.DAT (numerical early time) (a/n)				n
number of time steps be- tween times TAU?				10

## FIGURE CAPTIONS

1. Thermal conductivity  $k$  and diffusivity  $\kappa$  as functions of temperature for basalt (A), granite (B), limestone (C) and sandstone (D). Also shown is heat capacity per unit volume  $\rho C$  for basalt,  $k$  for diabase and quartzite, and  $\kappa$  for diabase. Data from Touloukian *et al.* (1981).
2. Temperature as a function of distance from dike contact at various times, analytical solution. Thermal properties of the dike and host rocks are identical and constant; no latent heat. Bottom and left axes are nondimensional distance and time, respectively; top and right axes are dimensional equivalents for example (Table 5, column 1).
3. Temperature as a function of distance from dike contact at various times. Thermal properties of magma are that of "dry" basalt, and those of host rocks are that of "wet" basalt with a porosity of 10%; no heat of crystallization (Table 5, columns 3, 4).
4. Maximum temperature achieved in wallrocks versus distance from dike contact. Solid lines are for constant  $\kappa_m/\kappa_h = k_m/k_h = 1$  with no latent heat (lower line) and latent heat of  $900 \text{ MJ/m}^3$  (upper line). Dotted lines are for temperature dependent properties of "dry basalt" with latent heat and without. Dashed lines with dots are for temperature dependent properties of "wet basalt" host rocks with latent heat and without. Dashed line is analytical solution using eqs. 18 and 19 to approximate the influence of latent heat.

FIGURE 2

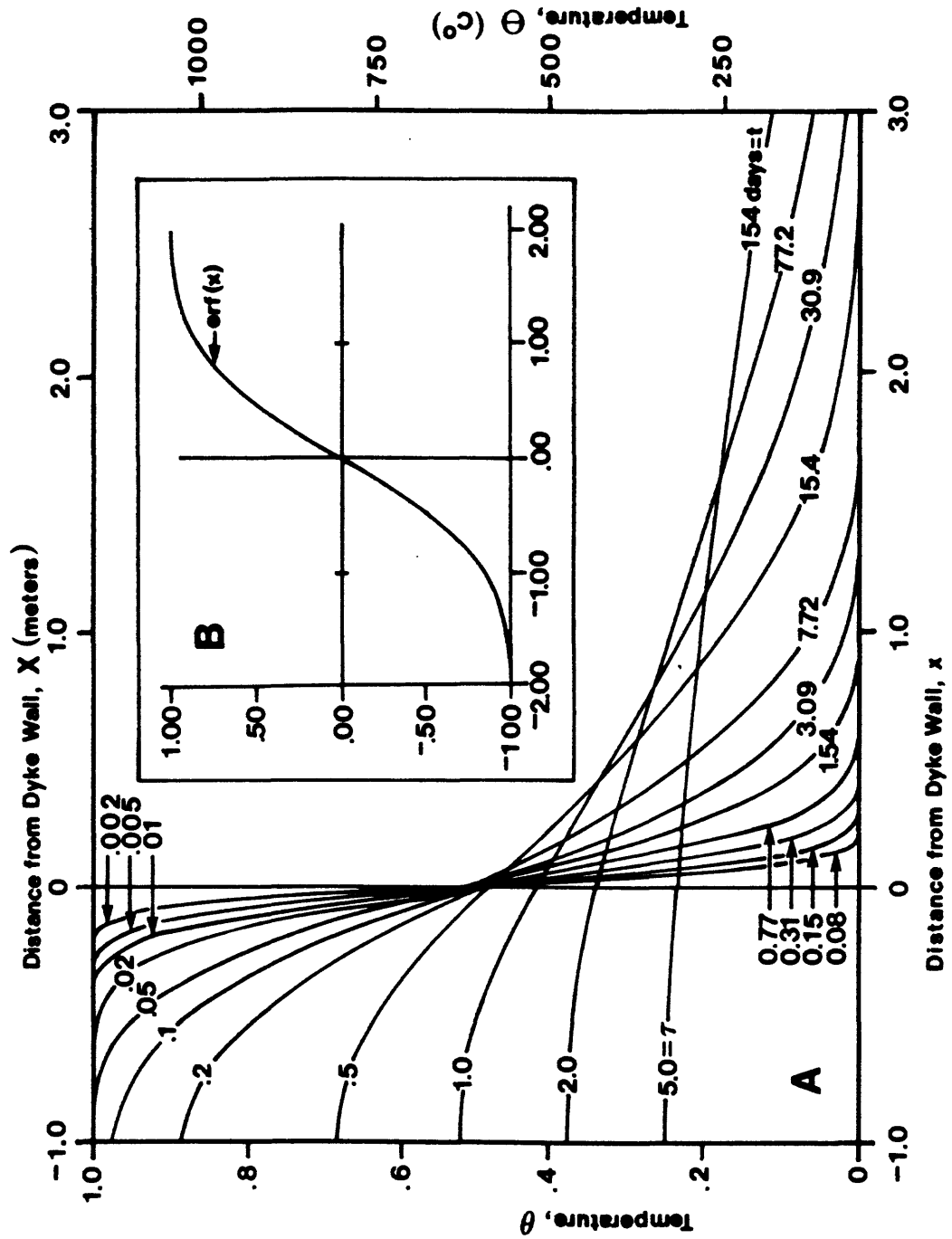


FIGURE 3

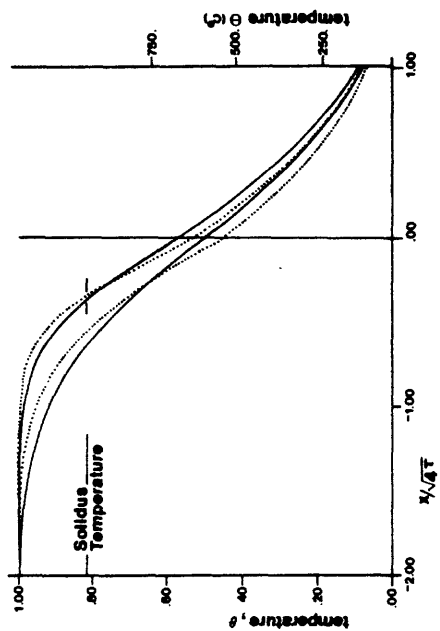


FIGURE 4

