

PREPROCESSOR AND POSTPROCESSOR COMPUTER PROGRAMS FOR A RADIAL-FLOW,
FINITE-ELEMENT MODEL

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U.S. GEOLOGICAL SURVEY

Open-File Report 87-680



West Trenton, New Jersey

1987

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CONVERSION FACTORS AND ABBREVIATIONS

For use of readers who prefer to use metric (International System) units, conversion factors for the inch-pound terms used in this report are listed below:

Multiply Inch-Pound Unit	By	To Obtain Metric Unit
<u>Length</u>		
inch (in.)	25.4	millimeter (mm)
foot (ft)	0.3048	meter (m)
<u>Area</u>		
square mile (mi ²)	2.590	square kilometer (km ²)
<u>Volume</u>		
gallon (gal)	.003785	cubic meter (m ³)
<u>Flow</u>		
foot per day (ft/d)	0.3048	meter per day (m/d)
foot squared per day (ft ² /d)	0.09294	meter squared per day (m ² /d)
gallon per minute (gal/min)	0.000063	cubic meter per second (m ³ /s)
gallon per minute per foot [(gal/min)/ft]	0.2070	liter per second per meter [(L/s)/m]

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ABSTRACT

Preprocessing and postprocessing computer programs that enhance the utility of the U.S. Geological Survey radial-flow model have been developed. The preprocessor program (1) generates a triangular finite-element mesh from minimal data input, (2) produces graphical displays and tabulations of data for the mesh, and (3) prepares an input data file to use with the radial-flow model.

The postprocessor program is a version of the radial-flow model, which was modified to (1) produce graphical output for simulation and field results, (2) generate a statistic for comparing the simulation results with observed data, and (3) allow hydrologic properties to vary in the simulated region.

Examples of the use of the processor programs for a hypothetical aquifer test are presented. Instructions for the data files, format instructions, and a listing of the preprocessor and postprocessor source codes are given in the appendixes.

INTRODUCTION

Background

Reilly (1984) developed a Galerkin Finite-Element Model (RADFLOW) to simulate ground-water flow in a radially-symmetric aquifer. The model can be used to simulate the response of an aquifer to pumping (Lindner and Reilly, 1983). Finite-element and node data are input manually, and output data are created as arrays by the RADFLOW model. This approach can be tedious and can introduce errors into the spatial discretization (finite-element mesh). In this report, new procedures are introduced to minimize data-entry errors and output manipulation.

Purpose and Scope

The purpose of this report is to present the preprocessor and postprocessor algorithms and computer programs that have been written for the radial, ground-water flow model, and to demonstrate the use of these computer programs. The preprocessor, called MESH, is a Fortran computer code, that contains algorithms for generating a triangular mesh, and creates and formats input data files for the ground-water flow model. The postprocessor program, named RADFLOW-S, is a modification of the Reilly (1984) code. Post-processing operations produce graphical displays and statistical evaluations of water-level changes in observation wells in the simulated region. This report includes (1) a general explanation of the

preprocessor and postprocessor concepts and algorithms; (2) a general summary of the MESH, and RADFLOW-S codes, as well as a listing of these codes; and (3) descriptions of how to use the preprocessors and postprocessors with input and output examples.

RADIAL FLOW MODEL

The user needs to have some familiarity with the geometry of the radial-flow regions, and the assumptions and requirements imposed on the preprocessing by the original radial-flow model to understand the preprocessor program. The flow region is radially symmetric, with a discharging well at the center of the region. Pumping is assumed to have little effect on water levels at large distances from the pumping well. This condition is approximated in the numerical simulation as a constant-head boundary at the lateral boundary of the flow region. The lower boundary of the flow region must be a no-flow boundary. The upper boundary may be either an impermeable boundary (no-flow boundary), or a free surface (water-table condition) (Reilly, 1984). Because of the radial symmetry, the hydrogeologic units in the radial-flow system are modeled as layers with uniform hydrologic properties. A conceptual model of such a region is shown in figure 1. Reilly (1984) describes the model assumptions and the geometric configuration of the region in more detail in the original program documentation.

The original radial-flow model code of Reilly (1984), requires the user to manually discretize the radial-aquifer region into three-node triangular elements, each with uniform hydraulic properties. The computer code simulates the radial flow in the discretized region by generating a system of algebraic equations derived from the Galerkin finite-element approximation of the differential equations of two-dimensional, radially-symmetric ground-water flow (Reilly, 1984; p. 5, eq. 13). Input data required to solve the system of equations include a number for each triangular finite-element, the finite-element node numbers, the location of each node in the region, and the hydraulic properties associated with each element.

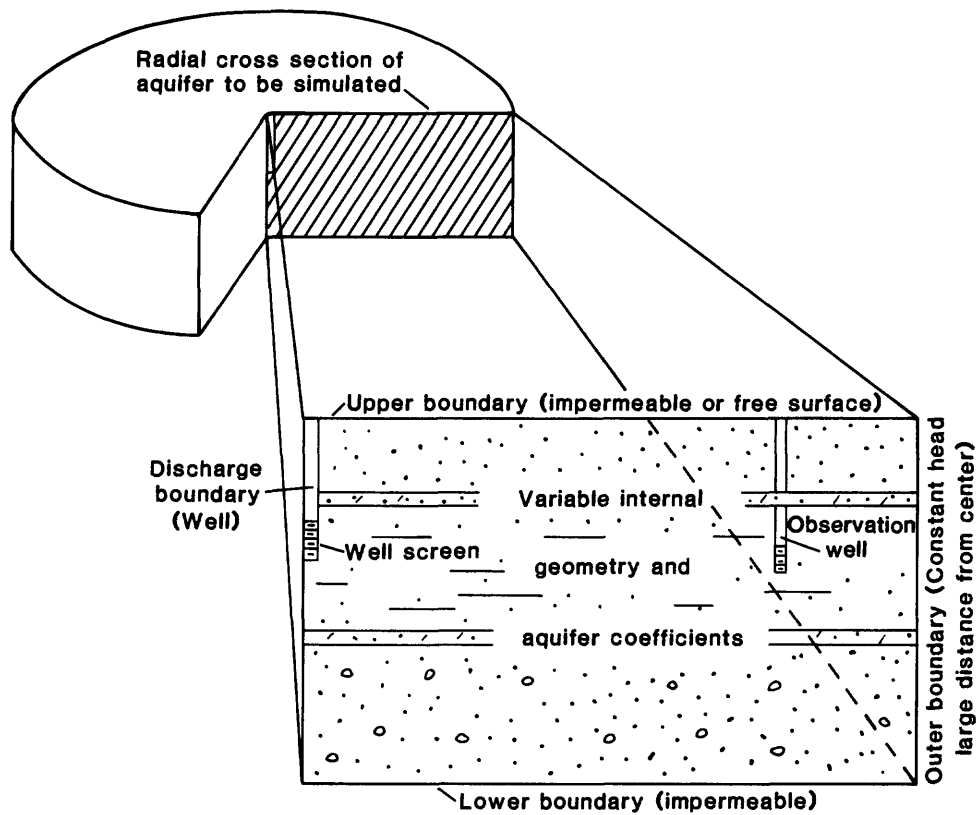


Figure 1.--Conceptual model for a radially symmetric ground-water flow system. (Modified from Linder and Reilly, 1983, fig. 6, p. 21)

PREPROCESSOR PROGRAM

The preprocessor program, MESH, automatically generates the finite-elements for the radial-flow finite-element program, RADFLOW-S. It generates a finite-element mesh from a minimum amount of information supplied by the user. Figure 2 is a representative example of a ground-water flow region that has been divided into triangular elements using MESH. The user inputs data that (1) defines zones of different hydraulic properties; (2) identifies sources or sinks, and the flow boundaries of the radial ground-water region; (3) creates a finite-element mesh of the dimensions needed to meet the required simulation accuracy; (4) generates triangular shapes of reasonable form that do not cause numerical difficulties; and (5) automatically numbers nodes for the region. Reilly (1984) gives a description of constraints in designing a mesh for a radial flow system, which is beyond the scope of this report. Pinder and Gray (1977), Steinmueller (1974) and many other authors discuss numerical stability and design of meshes used for finite-element analysis. A listing of the preprocessor code is given in appendix 1.

Preprocessor Concepts

The automatic, mesh-generating algorithm uses eight-node, quadratic, rectangular, finite elements. These rectangular finite elements are a family of two-dimensional finite elements that are different from the triangular finite elements that are generated for the numerical computations of the radial-flow model. Each rectangular finite element is defined by the program user as a subregion, which represents a radial section in the ground-water flow region. The horizontal and vertical extent of the subregions are determined from the hydrogeologic units in the radial-flow region. Generally, one or more rows of subregions are assigned to each hydrogeologic unit.

Examples of how rectangular elements are used to represent subregions is schematically shown for the simple region in figure 3(a). This region is divided into six rectangular, finite-elements. The node positions for the quadratic, rectangular elements in figure 3(a) are in the global reference frame, r, z , where " r " represents the radial distance from the well, and " z " the vertical elevation in relation to datum. In this example, the rectangular element that represents subregion 5 in the global reference frame has a range in " r " from 0 feet to 200 feet, and for " z " the range is 0 feet to 100 feet.

The mesh-generating program uses a local reference frame in the algorithm that divides each rectangular element representing a subregion into triangular finite elements. Zienkiewicz (1977) and Segerlind (1976) cover the concept of local reference frame in detail. The rectangular element, which represents the subregion in the r, z (global) reference frame, is transformed to a square element in the u, v (local) reference frame, where both u and v range from -1 to 1. This reference frame is centered within the boundaries of each subregion, as shown in figure 3(b). Once a subregion is divided, the coordinates are transformed back to the global coordinates that are required to solve the numerical equation for radial flow (Reilly, 1984; p.5, eq. 13). The local reference frame is used for the dividing operations because of the convenience of the identical geometry for each subregion. The transformation is done automatically using quadratic rectangular basis functions. The equations to transform a point " k " from the local reference frame coordinates, u, v , to the global reference frame, r, z , are:

$$R_i = \sum_{j=1}^8 N_j \times R_j,$$

and

$$Z_i = \sum_{j=1}^8 N_j \times Z_j,$$

where R_j, Z_j are the global coordinates for the eight nodes, $j=1, \dots, 8$, for the j quadratic, rectangular, finite element,
 R_i, Z_i are global coordinates for point k transformed to the global reference frame,

N_j are the quadratic, rectangular basis functions for the eight nodes, and $j=1, \dots, 8$ for the quadratic, rectangular, finite element in the local reference frame in counter-clockwise order, beginning with the lower left corner node.

Figure 4 shows a radial-flow region of 4 hydrogeologic units, 50 subregions, and 181 global nodes. These subregions were divided into the 480 finite-element, 273 finite-element node mesh in figure 2. (For sake of clarity, the eight nodes in each rectangular element that represents a subregion are referred to as global nodes. The nodes the program generates in the triangular mesh are called the finite-element nodes.) In this example, alternating layers of sand and clay are delineated into rows of subregions using rectangular elements. The subregion discretization is much coarser than the generated finite-element mesh. The algorithm requires the identification of a primary hydrogeologic unit, and in this example it is the lower sand unit. Note that the discretization intervals between nodes along the horizontal sides of each rectangular finite element is centered in the logarithmic scale, and is not centered in a linear scale. This consideration adds to the numerical stability of the radial-flow model solver (Reilly, 1984).

Preprocessor Algorithms

Division of Subregions

The preprocessor algorithm proceeds by dividing a subregion into simple rectangles, then into triangular finite elements as in fig. 3(b) through 3(d). These operations are completed for each subregion before numbering finite-element nodes and then proceeding to the next subregion. The algorithm requires: (1) the global locations of the eight nodes of the rectangular, finite element that represent each subregion, and (2) the number of row and column increments to be made for each subregion. The transformed subregion in figure 3(c) is divided into eight simple rectangles, by specifying five column increments along the u-axis and three row increments along the v-axis. The intersection of each row and column in the divided subregion is the location of a finite-element node, which is given a node number and assigned to a triangular finite element in subsequent operations in the code. Zienkiewicz and Phillips (1971) originated this algorithm, which Segerlind (1976) also used.

Node Numbering

The node numbering algorithm begins when the user discretizes the flow region into subregions. The radial-flow solver requires the lowest triangular finite-element node numbers to be along the constant-head boundary (Reilly, 1984). Because the automatic finite-element node-numbering algorithm is based on the sequence of subregions, constraints are made on the numbering of subregions by the user. The numbering algorithm requires the lowest subregion numbers to be in sequence, top to bottom, along the constant-head boundary. As an example, subregion 1 and 2 are the two subregions on the constant-head boundary in figure 3(a). A number for each subregion, and a global node number for each of the eight nodes in the

100 Global node number

15 Subregion number

K_h Horizontal hydraulic conductivity, in feet per day

K_v Vertical hydraulic conductivity, in feet per day

K_s Specific storage, in reciprocal feet

[illegible]

Figure 4.--Sample problem region with subregions, lithology, and final calibrated hydrogeologic properties.

rectangular element representing that subregion, are assigned by the user. Table 1 illustrates the assignment of global node numbers for the subregions in figure 3(a). Global node numbers can be in any order and are not the same as the triangular finite-element numbers to be generated by the algorithm.

The algorithm determines the number of finite-element nodes created in a subregion from the number of row and column increments specified by the user in each subregion. Each subregion must be divided into the same number of rows, if the subregions share a boundary along a vertical side, or divided into the same number of columns, if the shared boundary is along a horizontal side. Columns 2 and 3 in table 1 list these values for the example given in figures 3(a)-3(e). For example, subregion 1 has three rows of increments, and subregion 2 has five rows of increments.

The user must assign finite-element node numbers to finite-element nodes on the constant-head boundary. The number of finite-element nodes on this boundary is equal to the total number of row increments for each subregion along the constant-head boundary minus the number of shared rows. For the region shown in figure 3(a), three-row increments are assigned for subregion 1, and five-row increments are assigned for subregion 2; these subregions share one boundary. Therefore, seven finite-element nodes are located along this boundary ($5 + 3$ row increments $- 1$ row shared between subregion 1 and 2). For the example in figure 3, nodes 1 through 7 are assigned on the constant-head boundary.

Automatic numbering is done by the code after a subregion is divided into columns and rows, before creating the triangular finite elements in the subregion, and before proceeding to the next subregion to repeat the series of operations. Information on the spatial arrangement of the subregions is needed for the algorithm to avoid renumbering the finite-element nodes along shared subregion boundaries. This information is stored in the "connectivity matrix".

The numerical function of the connectivity matrix is demonstrated by example. Assembly of the connectivity matrix for the region in figure 3(a) is shown in table 2. This region consists of six subregions, numbered 1 through 6. Each subregion can have one neighboring subregion on each of its four sides. The orientation of each of the four sides is numbered 1 through 4. Side 1 is below, and sides 2, 3, and 4 are numbered counter-clockwise. The connectivity matrix identifies the subregion number on each shared side for each subregion, as shown in table 2 for figure 3(a). A zero is used where the subregion side is not shared. As indicated by table 2, subregion 5 in figure 3(a) is bounded by subregion 3 to the right (side 2), and by subregion 6 below (side 1); sides 3 and 4 are not shared.

The algorithm assigns node numbers to the corners of the simple rectangles formed from the intersection of the columns and rows in each divided subregion, row by row, from left to right, and top to bottom. The algorithm searches the connectivity matrix for each subregion to determine if nodes along its boundaries have been numbered previously. For subregion 5 in figure 3(a) and in table 2, the numbering algorithm proceeds through the subregions in numerical order and the search of the connectivity matrix determines that subregion 3 is divided and numbered, and that the

Table 1.--Global node numbers, and number of column and row increments for each subregion in figure 3(a).

Subregion number	Number of row increments	Number of column increment	Global node numbers associated with each subregion									
1	3	3	1	2	3	4	5	6	7	8		
2	5	3	10	11	12	13	3	2	1	9		
3	3	3	17	18	1	8	7	14	15	16		
4	5	3	20	21	10	9	1	18	17	19		
5	3	5	25	26	17	16	15	22	23	24		
6	5	5	28	29	20	19	17	26	25	27		

Table 2.--Connectivity matrix for the subregions shown in figure 3(a).

Subregion number	Shared boundary subregion number			
	Side 1	Side 2	Side 3	Side 4
1	2	0	0	3
2	0	0	1	4
3	4	1	0	5
4	0	2	3	6
5	6	3	0	0
6	0	4	5	0

nodes shared by subregion 5 and subregion 3 are numbered. Therefore, these finite-element nodes are not renumbered. However, because subregion 6 has not been divided and numbered, the nodes it shares along the boundary with subregion 5 are assigned. Node numbers on each boundary of the subregion are stored in an array. Segerlind (1976) and Collins (1973) discuss node numbering and illustrate the use of the connectivity matrix in more detail.

Division into Triangles

After numbering finite-element nodes and before the next subregion is divided, the algorithm divides each simple rectangle formed from the intersection of columns and rows in each subregion into two triangles as illustrated in figure 3(d). The creation of triangles, proceeds left-to-right, top-to-bottom, through all the simple rectangles in each subregion. The algorithm determines the proper numbering for diagonals from the simple rectangle, assigns the node sequence for each triangular element to produce the consistent counter-clockwise order needed to assemble the matrices in the numerical radial-flow equation (Reilly, 1984; p. 5, eq. 13), and gives each triangle a finite-element number. Reilly (1984) discusses the node-numbering conventions. Global coordinates for each node are calculated for each triangular finite-element node using the transformation operation described in the section on preprocessor concepts. The bandwidth is determined for each triangular-element. If it is the largest bandwidth in the region, it is recorded and printed in the final tabulation of results.

In summary, the preprocessor algorithms generate the finite-element mesh, one subregion at a time. The algorithm to divide each subregion into simple rectangles uses the geometry of a local reference frame. The user determines the resolution of the mesh by specifying the number of row and column increments. The number of simple rectangles produced for each subregion is determined from the number of assigned rows and columns for each subregion. The corners of these simple rectangles become the finite-element nodes, and each node is numbered. Each simple rectangle is divided into two triangular finite elements, and then each triangular element is numbered. The global locations of the finite-element nodes are determined by transforming the coordinates from local to global coordinates. These finite-element-mesh data are assembled with hydrogeologic data as described in the following section for input to the radial-flow model.

Preprocessor Input and Output

The MESH program can be used in two different modes, the "P" and "R" modes. The "P" mode is used to produce a plot of the finite-element mesh at a graphics terminal or to create a plotfile, which can be plotted. It also produces a descriptive output file called OUTPUT, which can be used instead of, or in conjunction with, a plotter to evaluate the generated finite-element mesh. It is not necessary to use either a graphics terminal or plotter to run the MESH program. Once the mesh geometry has been evaluated by the user, the "R" mode can be used to automatically create the properly formatted input data file to run RADFLOW-S.

General Input Requirements

The MESH program requires input from the BASIC DATA FILE in either the "P" or "R" mode. Following the order that data are input, the BASIC DATA FILE includes data on (1) the number of subregions and total number of global nodes in the modeled region, (2) the radial distance from the well head to the global nodes, (3) the vertical distance of the global nodes relative to a datum elevation, (4) subregion numbers and the connectivity matrix data, (5) the number of subregions and finite-element node numbers along the constant-head boundary, (6) the number of row increments for each subregion along the constant-head boundary, and (7) the global node numbers in each subregion and the number of row and column increments for each subregion.

A description of the input-data variables and formats for the BASIC DATA FILE is given in appendix 2. Sample input data, which produced the finite-element mesh shown in figure 3(e) from the subregions shown in figure 3(a), is presented in appendix 3. The BASIC DATA FILE for the region in figure 4 is presented in appendix 4, section A. This data set was used to produce the 480 finite-element mesh shown in figure 2.

"P" Operation Mode and Output

In "P" operation, the program prompts the user to choose the output device. The program uses the graphics device utility (GDIU) to facilitate graphical output. A graphics terminal compatible to the TAB 132/15-G¹ or TEKTRONICS 4010 terminals or plotting devices at the users installation may be chosen, or a plotfile can be created for input to another graphics plotter. Visual examination of the graphical output of the finite-element mesh can quickly show problems in the global-mesh data. Errors in the input data set can be corrected by referring to the OUTPUT file descriptions and by examining the graphical output.

The descriptive file OUTPUT is created in the "P" operation mode. The OUTPUT file includes (1) a tabulation of the connectivity matrix for all the subregions, (2) a list of the number of row and column increments in which each subregion is divided, (3) the finite-element node numbers for each subregion, and (4) the finite-element numbers and the associated finite-element node numbers, and the global coordinates of these finite-element nodes. The program prompts the user at the terminal to enter the maximum length of the "r" and "z" axes, and a choice of either an arithmetic or logarithmic plotting scale along the "r" axis. An example of the OUTPUT file containing mesh data for the simple region shown in figures 3(e) is given in appendix 5.

"R" Operation Mode and Output

The PROPERTIES data file and the BASIC DATA FILE are required input to run MESH in the "R" mode. The BASIC DATA FILE was previously described.

¹ "Use of brand names in this report is for identification purposes only and does not constitute endorsement by the U.S. Geological Survey."

PROPERTIES data are formatted in four sections. The first data section contains control data for setting up the simulation input data file. It contains (1) a simulation identifier, (2) identification of the hydraulic properties of the primary hydrogeologic unit in the region, (3) the number of hydrogeologic units that are distinct from the primary hydrogeologic unit, (4) the number of finite-element nodes along the screen in the discharging well (must be more than 1), and (5) the number of pumping periods. The second data section specifies the finite-element node numbers along the screen of the discharging well, and, therefore, is determined after evaluating the output on the mesh from "P" mode operation. The third data section assigns the hydraulic properties for those hydrogeologic units that the user has identified as distinct from the primary hydrogeologic unit. For the example shown in figure 4, one primary hydrogeologic unit and three distinct units were identified. The fourth data section gives information on the test-well discharge rate and duration.

A description of the PROPERTIES data-file input variables and their formats is given in appendix 2, section B. Further discussion of the function of these hydraulic properties to simulate a radial-flow system is described in the original RADFLOW report (Reilly, 1984).

MESH produces the RADFLOW.INPUT data file as output, which is used by the RADFLOW-S radial-flow model. The RADFLOW.INPUT data file is identical to the input file documented by Reilly (1984). The RADFLOW.INPUT file must be manually modified as described in the original report to simulate an aquifer test of an unconfined system (Reilly, 1984).

POSTPROCESSOR and MODIFIED PROGRAM

This section summarizes the concepts and modifications that are in the RADFLOW-S version but are not included in the original code radial-flow model. The original RADFLOW model determined water levels at each finite-element node at each time step in a summary output file. RADFLOW-S retains the summary output file as part of the output from the radial-flow simulations. The modified code is presented in appendix 6.

Postprocessor Concepts

The summary output file from the original model consists of a printout of large matrices from simulations, which can be can be unwieldy. To improve this, the innovation used in the RADFLOW-S program was to focus on only that portion of the computed results that are typically used in the analysis--that is, the computed drawdown in observation wells within the radial-flow region.

The postprocessor performs two functions: (1) it creates standard logarithmic plots from the observation-well water-level changes from the finite-element simulation and from the field data, and (2) it evaluates a Gaussian-norm statistic that compares the simulation results and field data at each observation well. An example of the logarithmic plot produced by the program is given in figure 5. Modifications to the hydrogeologic data and mesh can be made as iterative feedback to improve the match of simulation and field data.

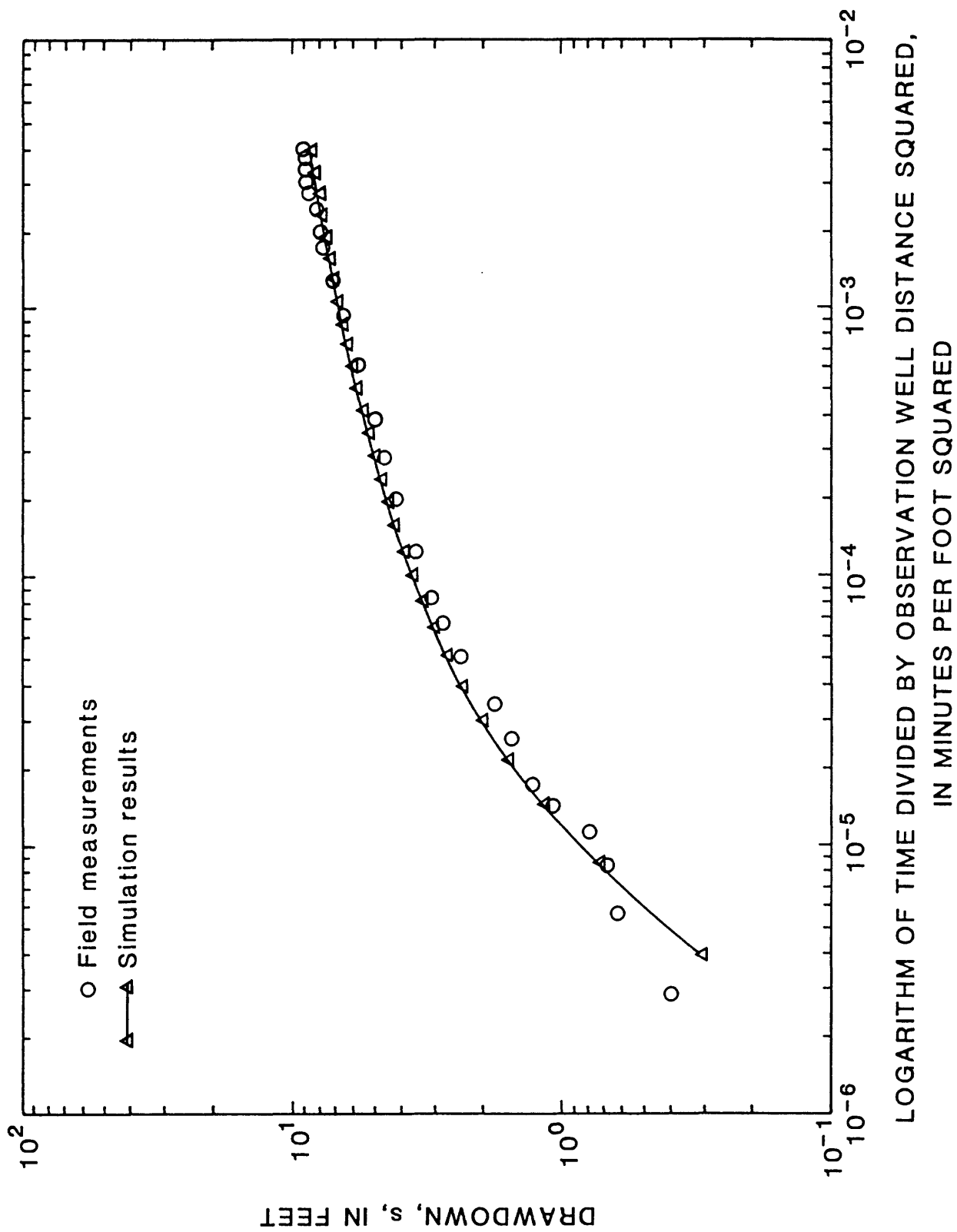


Figure 5.--Plot of simulated and observed drawdowns for example simulation shown in figure 2.

Postprocessor Algorithms

Calculation of Observation-well Drawdowns

As in the original model, the RADFLOW-S model calculates the ground-water potential, or head, for each triangular finite-element node in the mesh for each time step of the simulation period (Reilly, 1984). The postprocessor program uses triangular basis functions of the same type as in the numerical solution to the radial-flow equation (Reilly, 1984; p.4, eq. 7) to interpolate heads in observation wells from the node heads. The method of numerical interpolation using linear-triangular basis functions is basic and is described in detail in Segerlind (1976) and Zienkiewicz (1977).

Calculation of the Gaussian Norm

The Gaussian-norm statistic, "e", is a general comparison of the adequacy of the simulated drawdown and the observed drawdown for each observation for the entire period of simulation. It is expressed by the formula:

$$e = \sum_{i=1}^n \frac{h_i - h'_i}{h_i}$$

where h_i = is the observed head at the observation well point, i, at time t.

h'_i = is the calculated head at the observation well point, i, at time t.

n = number of observed head values at the observation well point.

For example, where the observed and calculated heads are approximately the same value, the Gaussian-norm statistic will approach zero, indicating that the field and simulation results are in good agreement. This comparison is done once for each observation well. Because the simulated values usually are calculated for times that are different from the times of the observed field data, the algorithm does a linear interpolation to determine a simulated value at the same time as the field data.

General Postprocessor Input and Output Description

The program, RADFLOW-S, is a modified version of the radial-flow finite-element program code, RADFLOW, with the addition of postprocessing subroutines, which are called PTPLOT, PMPLT, and EPSILON. PTPLOT and PMPLT subroutines generate logarithmic graphs of water-level changes versus time, and EPSILON calculates the Gaussian-norm statistic. PTPLOT prompts the user for input to control the plotting routines for water-level plots of each observation well, and calls the PMPLT and EPSILON subroutines. PMPLT prompts the user to name the input file that contains the drawdown data for each observation well, then reads these data files and generates plots of

corresponding field and simulated drawdown data. More detailed descriptions of these subroutines and data files follows.

Postprocessor Input

The RADFLOW-S program reads data both through user responses to prompts at the terminal and by reading data files. Subroutine PTPLOT prompts the user at the terminal for (1) the name of the file containing the field water-level data, (2) the headings for the logarithmic water-level graphs, and (3) axes limits for the graph. The graph axes limits must be given as log values that span the range of the data as shown in figure 5. The x-axis is in units of time per length squared, (time per square of the radial distance of the observation well from the pumped well), and the y-axis is in feet. Subroutine PTPLOT calls the GDIU and prompts the user to specify an output device to either output directly to a graphics terminal, or to create a plotfile for a plotter. The program plots the simulated water-level data in the order that the observation wells are included in the OB.WELL data file; therefore, the user follows the same order when responding to prompts for field data and plotting control.

The three datafiles required to run the program are: (1) the RADFLOW.INPUT data file, previously described in the section on the 'R' option for the preprocessor, MESH; (2) the OB.WELL data file, which contains data on the number of observation wells and their screen locations; and (3) user generated data files containing measured field data for each of the observation wells.

The OB.WELL data file lists the number of observation wells in the region, the location of the midpoint of the screen of each observation well, and the finite-element number in the mesh that contains the observation-well screen. The location of the observation well(s) in the finite-element mesh is determined by the user after running and reviewing the graphics output and the output tabulation file OUTPUT generated by MESH in "P" mode. The observation well location is assumed to be the midpoint of the total screen length. Drawdowns in up to five observation wells can be calculated. The requirement for observation-well data to run RADFLOW-S can be overridden by creating an empty data file. Further descriptions of the data file variables and the data formats are presented in appendix 1, section C. The OB.WELL data file used to create the plot shown in figure 5 is presented in appendix 4, section C.

Data files of field data on each observation well must be separate and must be given a label by the user. Each data file lists the number of water-level measurements for the observation well, the distance of the observation well from the pumped well, a prepumping reference water level (optional), and the water-level measurement and recorded time at each observation well. A dummy reference water-level value is used in place of a prepumping water-level if water-level measurements are entered as the drawdown (or recovery) value. Appendix 2, section D describes the input formats for these data. The data file for the observation well example shown in figure 5 is given in appendix 4, section D.

Postprocessor Output

Postprocessor output of logarithmic graphs of water-level changes may be plotted to a terminal screen or to another device by creating a plot file. The value of the Gaussian-norm statistic is shown on the user's terminal at the completion of the logarithm plot for each observation well. The code creates a summary output file in the format originally documented by Reilly (1984).

Summary

Preprocessing and postprocessing computer programs have been developed that simplify and enhance the utility of the U.S. Geological Survey radial-flow model. Principals of automatic mesh generation and data manipulation have been used in the programming. Features of the preprocessor include: (1) reduced user input for generating the finite-element mesh for the radial-flow model, (2) use of global and local reference-frame geometry to discretize the flow region, (3) a capability for the user to simply describe the spatial variation of hydrologic properties (horizontal and vertical hydraulic conductivity, and specific storage or specific yield) of subregions in the flow region, (4) automatic division of the flow region into triangular finite-elements, (5) automatic numbering of the finite-element nodes in the discretized region, and (6) generation of an input file to run the radial-flow model, RADFLOW-S.

The postprocessing program is part of the simulation code for the radial-flow system. The postprocessor features (1) interpolation of the water-level changes at observation wells for the simulated region; (2) plotting simulated water-level changes and field data from observation wells together for as many as five observation wells; and (3) calculation of a Gaussian-norm statistic, which compares the simulation to field results.

In addition to the program descriptions, discussion of the concepts in these processors and examples of their use for a hypothetical aquifer test are presented. Appendixes provide format instructions for the data files, example data files, and a listing of the preprocessor and postprocessor source codes.

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APPENDIXES

```

C*****
C
C
C
C
C
C*****
C* MESH.F77
C* WRITTEN BY AMLETO A. PUCCI AND DARYLL A. POPE, USGS TRENTON, NJ. 6/19/87
C*
C* Program MESH.F77 is a finite-element mesh generator and a pre-
C* processor program for running RADFLOW-S.F77, a Galerkin Finite-Element
C* model for simulating transient responses to aquifer tests. MESH.F77
C* automatically partitions second-order, quadrilateral, finite elements, or
C* "subregions", into linear triangular elements which may define a
C* multilayer, radially-symmetric, ground-water aquifer. It also can be used
C* in a pre-processor mode to create an input data-file for running
C* RADFLOW-S, which is a modified version of a program by Thomas Reilly
C* (1984).
C*****
c*
C* The program employs DISSPLA graphics , and is compatible with TAB graphics
C* terminals, and ZETA type plotters on the Prime system.
C*
C*
C* Mesh Generating Mode:
C* The program reads a data file which is needed to define the simulation
C* domain. The input data includes the number of quadrilateral subregions,
C* the number of regional nodes, the coordinates of the regional nodes,
C* connectivity data (or data which describes how the sub-regions are posi-
C* tioned next to each other), the number of subregions which appear at the
C* constant-head boundary of the domain, the number of nodes on the constant-
C* head boundary, the number of rows in each subregion, and information on
C* how each subregion is to be divided into triangular elements. An
C* annotated input file for mesh generating appears in Appendix 1.
C*
C* The program outputs a descriptor file, OUTPUT, which describes the
C* division of each subregion into triangular elements, and the numbering
C* and positions of each triangular element node. Graphics output can also be
C* used to examine the mesh.
C*
C* RADFLOW-S Input generation:
C* The program reads the same data file which is used to generate the mesh,
C* and a second data file which must be titled "PROPERTIES" . The second data
C* file of parameters needed to simulate an aquifer test as described in
C* Appendix 1.B of the supplemental data for running MESH.F77 and in WSP 2198.
C*
C*

```



```

C*****
C*
C*****
C*
C*          DEFINITION OF SELECTED PROGRAM VARIABLES
C*
C*  NB      -counter used for assigning finite element nodes
C*  NBW     -counter for calculating maximum bandwidth
C*  NELBW   -number of the triangular element causing the maximum bandwidth
C*  NEL     -counter for the total number of elements generated
C*  O2      -logical for output control
C*  INRG    -number of quadrilateral subregions used to define the problem
C*          domain
C*  INBP    -total number of global nodes used to discretized the domain
C*          into quadrilateral subregions
C*  XP,YP   -the global coordinates of the regional nodes
C*  JT      -connectivity data for each subregion
C*  NRC     -number of subregions which appear on the constant-head boundary
C*          of the domain
C*  TNR     -total number of element nodes which are located on the
C*          constant-head boundary
C*  NRB     -the number of constant-head nodes which appear in each
C*          subregion
C*  NNRB    -the node numbers on each side of a subregion, defined
C*          NNRB(subregion,side,node number)
C*  NELR    -counter for the number of elements in a subregion
C*  NROWS   -number of rows of nodes to divide a subregion into
C*  NCOL    -number of columns of nodes to divide a subregion into
C*  NDN     -global node numbers used to define the quadrilateral subregions
C*  N       -second order quadrilateral shape functions associated with
C*          each regional node
C*  XC,YC   -the x and y coordinates of all the generated regional nodes
C*  ICOMP   -array of digital data which determines the orientation of
C*          contiguous subregions
C*  NN      -temporary array used for numbering element nodes in a subregion
C*  XE,YE,  -the X and Y coordinates, and the node numbers of the four
C*  NE      node elementary quadrilateral which is divided into two
C*          triangles
C*  NTF     -logical file used to determine if the node has been assigned
C*  NODXY   -file of the X and Y positions for each node used for RADFLOW
C*  ELM     -node numbers for each triangular element
C*****
C*
PROGRAM MESH
  INTEGER NDN(8),NN(21,21),NNRB(50,4,21),JT(50,4),LB(3),NE(25)
  1 ,NR(4),NRB(10),NRC,TNR,NELR,REGION(50,32),ELM(800,3)
  1 ,JA(3),NELRC(50)
  REAL XP(200),YP(200),N(8),YC(21,21),XC(21,21),XE(25)
  1,YE(25),XRG(9),YRG(9),NODXY(1000,2)
  CHARACTER FILES*1,DATAFILE*32,ANS*1
  LOGICAL NTF(50)
  LOGICAL O2
  COMMON NODXY,ELM
  COMMON REGION,NELRC

```

```

C*****
*
C      DATA INITIALIZATION
C*****
*****
      DATA NE/25*0/
      DATA ((NN(I,J), I=1,21),J=1,21)/441*0/
      DATA ((NODXY(I,J),I=1,1000),J=1,2)/2000*0/
      DATA NTF/50 * .FALSE./
      NB=0
      NBW=0
      NELBW=0
      NEL=0
      O2 = .FALSE.
      CALL TNOUA('ENTER DATA FILE: ',INTS(17))
      READ(1,10) DATAFILE
10    FORMAT(A32)
      OPEN(UNIT=40,FILE=DATAFILE,STATUS='OLD')
      OPEN(UNIT=90,FILE='OUTPUT',STATUS='NEW')

C
C*****
C INPUT FROM SCREEN FOR CONTROL OF FILES TO BE OUTPUT
C*****
20    WRITE(1,30) 'DO YOU WISH TO PLOT THE MESH OR TO GENERATE'
      WRITE(1,30) 'THE INPUT FILES FOR USE IN RADFLOW.F77?'
      CALL TNOUA('ENTER P FOR PLOTTING OR R FOR RADFLOW:',INTS(38))
30    FORMAT(A48)
      READ(1,40) FILES
40    FORMAT(A1)
      IF (FILES .EQ. 'P') THEN
          O2 = .NOT. O2
      ELSE IF (FILES .EQ. 'R') THEN
          GO TO 50
      ELSE
          GO TO 20
50    ENDIF

C*****
C INPUT AND OUTPUT OF TITLE,CONTROL CARD,GLOBAL COORDINATES,AND
C CONNECTIVITY DATA
C*****
      READ(40,60) INRG,INBP
60    FORMAT (2I4)
      READ(40,70)(XP(I),I=1,INBP)
      READ(40,70)(YP(I),I=1,INBP)
70    FORMAT(8F10.5)
      DO 80 I=1,INRG
80    READ(40,90)NRG,(JT(NRG,J),J=1,4)
90    FORMAT (5I3)
      WRITE(90,100)
100   FORMAT(/1X,17HCONNECTIVITY DATA/
1,39H                                SHARED BOUNDARY/1X,
142HSUBREGION                      1      2      3      4 /)

```

```

C100  FORMAT(/1X,39HCONNECTIVITY DATA          SHARED BOUNDARY/1X,
C      143HSUB REGION          1      2      3      4  )
      DO 110 I=1,INRG
110   WRITE(90,120)I,(JT(I,J),J=1,4)
120   FORMAT(2X,I3,16X,4(I2,5X))
C*****
C  INPUT OF NODE NUMBERS ALONG CONSTANT-HEAD BOUNDARY
C*****
      READ(40,130) NRC,TNR
130   FORMAT(2I3)
      DO 140 I=1,NRC
140   READ(40,150) NRB(I)
150   FORMAT (I3)
      NB=TNR
      K=2
      DO 160 I=1,NRC
          IM=I-1
          NNRB(I,2,1)=NNRB(IM,2,NRB(IM))
          DO 160 J=2,NRB(I)
              NNRB(I,2,J)=K
              K=K+1
160   CONTINUE
      NNRB(1,2,1)=1
C*****
C  LOOP ON THE SUBREGIONS TO GENERATE THE ELEMENTS
C*****
      DO 420 KK=1,INRG
          NELR=0
          READ (40,170)NRG,NROWS,NCOL,(NDN(I),I=1,8)
170   FORMAT(11I4)
          IF (NRG .NE. 1) THEN
              WRITE(90,175)
175   FORMAT(/30X,41H*NOTE: COORDINATES ARE MULTIPLIED BY .001)
              ENDIF
          WRITE(90,180) NRG,NROWS,NCOL,(NDN(I),I=1,8)
180   FORMAT(1H1//1X,
164H***** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBERS
1,13H IN SUBREGION
1,I2,6H ****//22HNUMBER OF INCREMENTS =//10X,I2,11H ROWS   AND,4X
1,I2,8H COLUMNS//10X,19HGLOBAL NODE NUMBERS,10X,8I5)
C*****
C  GENERATION OF THE ELEMENT NODAL COORDINATES
C*****
      DO 190 I=1,8
          II=NDN(I)
          XRG(I)=XP(II)
190   YRG(I)=YP(II)
          XRG(9)=XP(1)
          YRG(9)=YP(1)
          TR=NROWS-1
          DETA=2./TR
          TR=NCOL-1
          DSI=2./TR
          DO 200 I=1,NROWS

```

```

TR=I-1
ETA=1.-TR*DETA
DO 200 J=1,NCOL
  TR=J-1
  SI=-1.+TR*DSI
  N(1)=-0.25*(1.-SI)*(1.-ETA)*(SI+ETA+1.)
  N(2)=0.5*(1.-SI**2)*(1.-ETA)
  N(3)=0.25*(1.+SI)*(1.-ETA)*(SI-ETA-1.)
  N(4)=0.50*(1.+SI)*(1.-ETA**2)
  N(5)=0.25*(1.+SI)*(1.+ETA)*(SI+ETA-1.)
  N(6)=0.50*(1.-SI**2)*(1.+ETA)
  N(7)=0.25*(1.-SI)*(1.+ETA)*(ETA-SI-1.)
  N(8)=0.50*(1.-SI)*(1.-ETA**2)
  XC(I,J)=0.0
  YC(I,J)=0.0
  DO 200 K=1,8
    XC(I,J)=XC(I,J)+XRG(K)*N(K)
200    YC(I,J)=YC(I,J)+YRG(K)*N(K)
C*****
C  GENERATION OF THE SUBREGION NODE NUMBERS
C*****
  KN1=1
  KS1=1
  KN2=NROWS
  KS2=NCOL
  DO 270 I=1,4
    NRT=JT(NRG,I)
    IF(NRT.EQ.0.OR.NRT.GT.NRG)GO TO 270
    DO 210 J=1,4
210    IF(JT(NRT,J).EQ.NRG)NRTS=J
    K=NCOL
    IF(I.EQ.2.OR.I.EQ.4)K=NROWS
    JL=1
    DO 260 J=1,K
      GO TO(220,230,240,250),I
220    NN(NROWS,J)=NNRB(NRT,NRTS,JL)
    KN2=NROWS-1
    GO TO 260
230    NN(J,NCOL)=NNRB(NRT,NRTS,JL)
    KS2=NCOL-1
    GO TO 260
240    NN(1,J)=NNRB(NRT,NRTS,JL)
    KN1=2
    GO TO 260
250    NN(J,1)=NNRB(NRT,NRTS,JL)
    KS1=2
260    JL=JL+1
270    CONTINUE
    IF(NRG.GT.NRC)GO TO 290
    KS2=NCOL-1
    DO 280 I=1,NROWS
280    NN(I,NCOL)=NNRB(NRG,2,I)

```

```

290      DO 300 I=KN1,KN2
          DO 300 J=KS1,KS2
              NB=NB+1
300      NN(I,J)=NB
C*****
C  STORAGE OF THE BOUNDARY NUMBERS
C*****
          DO 310 I=1,NCOL
              NNRB(NRG,1,I)=NN(NROWS,I)
310      NNRB(NRG,3,I)=NN(1,I)
          DO 320 I=1,NROWS
              NNRB(NRG,2,I)=NN(1,I)
320      NNRB(NRG,4,I)=NN(I,1)
C *****
C  OUTPUT OF THE SUBREGION NODE NUMBERS
C*****
          WRITE(90,330)
330      FORMAT(/1X,27HFINITE-ELEMENT NODE NUMBERS/)
          DO 340 I=1,NROWS
340      WRITE(90,350) (NN(I,J),J=1,NCOL)
350      FORMAT(1X,20I5)
C*****
C  DIVISION INTO TRIANGULAR ELEMENTS
C*****
          WRITE (90,355)
355      FORMAT (/5X,49HELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND
117H NODE COORDINATES)
          WRITE(90,360)
360      FORMAT(/3X,17HNEL  NODE NUMBERS,9X,4HX(1),8X,4HY(1),8X,4HX(2),8X,
14HY(2),8X,4HX(3),8X,4HY(3)      )
          K=1
          DO 370 I=1,NROWS
              DO 370 J=1,NCOL
                  XE(K)=XC(I,J)
                  YE(K)=YC(I,J)
                  NE(K)=NN(I,J)
370      K=K+1
          L=NROWS-1
          DO 410 I=1,L
              DO 410 J=2,NCOL
                  NR(1)=NCOL *I+J-1
                  NR(2)=NCOL *I+J
                  NR(3)=NCOL *(I-1)+J
                  NR(4)=NCOL *(I-1)+J-1
                  DO 410 IJ=1,2
                      NEL=NEL+1
                      NELR=NELR+1
                      REGION(KK,NELR)=NEL
                      J1=NR(1)
                      J2=NR(IJ+1)
                      J3=NR(IJ+2)
                      JA(1)=J1
                      JA(2)=J2
                      JA(3)=J3

```

```

        LB(1)=IABS(NE(J1)-NE(J2))+1
        LB(2)=IABS(NE(J2)-NE(J3))+1
        LB(3)=IABS(NE(J1)-NE(J3))+1
        DO 380 IK =1,3
            IF(LB(IK).LE.NBW) GO TO 380
            NBW=LB(IK)
            NELBW=NEL
380      CONTINUE
C*****
*
C      CREATION OF THE ARRAY NODXY(1000,2)
C      FOR USE IN OUTPUT TO RADFLOW
C*****
*
        IF (NTF(KK) .EQV. .TRUE.) GO TO 390
        DO 390 II=1,3
            NODXY(NE(JA(II)),1)=XE(JA(II)) * 1000.
            NODXY(NE(JA(II)),2)=YE(JA(II)) * 1000.
390      CONTINUE
C*****      WRITING DATA TO FILE OUTPUT
        WRITE(90,400)NEL,NE(J1),NE(J2),NE(J3),XE(J1),YE(J1),XE(J2),YE(J2)
        1,XE(J3),YE(J3)
400      FORMAT(1X,4I5,3X,6F12.4)
C*****      CREATION OF ARRAY ELM(800,3) NEEDED TO PRODUCE 'RADFLOW.INPUT'
        ELM(NEL,1)=NE(J1)
        ELM(NEL,2)=NE(J2)
        ELM(NEL,3)=NE(J3)
410      CONTINUE
        NTF(KK) = .NOT. NTF(KK)
        NELRC(KK)=NELR
C*****
*
C      OUTPUT OF SELECTED FILES
C*****
*
420      CONTINUE
C
C      FINISH WRITING TO FILE 'OUTPUT'
C
        WRITE(90,430) NBW,NELBW
430      FORMAT(///1X,21HBANDWIDTH QUANTITY IS,I4,22H CALCULATED IN ELEMENT
        *,I4)
        CLOSE(90)
        CLOSE(40)
C*****
*
        IF (O2 .EQV. .TRUE.) THEN
            CALL PLOT(NEL,NB)
        ELSE
            CALL RADIN(NEL,NB,TNR)
        ENDIF
        STOP
        END
        SUBROUTINE RADIN(NEL,NB,TNR)

```

```

      INTEGER NND(50),DIFFK,REGION(50,32),ELM(800,3),NELRC(50),RN,RD
*,NCH,NQ,NDIF,NSCON,NTS,TNR
      REAL NODXY(1000,2),PPR,PPZ,S,SY,PR,PZ,Q,QRCH,DELT,TMAXF,TSM
      COMMON NODXY,ELM
      COMMON REGION,NELRC
C
      OPEN(UNIT=80,FILE='PROPERTIES',STATUS='OLD')
      OPEN(UNIT=100,FILE='RADFLOW.INPUT',STATUS='NEW')
C***** READ BASIC VARIABLES FROM 'PROPERTIES' AND WRITE TO 'RADFLOW.INPUT'
      READ(80,10) TITLE
      WRITE(100,10) TITLE
10     FORMAT (T1,A25)
      READ(80,20) PPR,PPZ,IPP
      WRITE(100,20) PPR,PPZ,IPP
20     FORMAT(F10.0,F10.2,I10)
      READ(80,30) S,SY
      WRITE(100,30) S,SY
30     FORMAT(F10.9,3X,F10.9)
      READ(80,40) NQ,NDIF
40     FORMAT(T16,2I5)
      WRITE(100,50) NEL,NB,TNR,NQ,NDIF
50     FORMAT(5I5)
      DO 70 I=1,NQ
          READ(80,60) NND(I)
          WRITE(100,60) NND(I)
60     FORMAT(I5)
70     CONTINUE
C***** READ VALUES FOR SUBREGIONS OF DIFFERING HYDRAULIC CONDUCTIVITIES
C***** FROM 'PROPERTIES' AND WRITE TO 'RADFLOW.INPUT'
      READ(80,80)DIFFK
80     FORMAT (I3)
      DO 120 I=1,DIFFK
          READ(80,90)PR,PZ,B,DIFFS
90     FORMAT (F10.5,F10.5,I4,F10.9)
          DO 120 J=1,B
              READ(80,100) RN
100    FORMAT(I4)
              C=NELRC(RN)
              DO 120 K=1,C
                  WRITE(100,110) REGION(RN,K),PR,PZ,DIFFS
110    FORMAT (I10,F10.5,F10.5,5X,F10.9)
120    CONTINUE
C***** WRITE ELEMENT DATA TO 'RADFLOW.INPUT'
      DO 130 I=1,NEL
130    WRITE(100,140) I,ELM(I,1),ELM(I,2),ELM(I,3)
140    FORMAT (4I5)
      NSCON=1
C***** WRITE NODAL COORDINATES TO FILE 'RADFLOW.INPUT'
      DO 170 I=1,NB
          IF (I .LE. TNR) THEN
              WRITE(100,150) I,NODXY(I,1),NODXY(I,2),NSCON
150    FORMAT (I10,F10.0,F10.0,10X,I3)
          ELSE
              WRITE(100,160) I,NODXY(I,1),NODXY(I,2)

```

```

160     FORMAT (I10,F10.0,F10.0)
      ENDIF
170     CONTINUE
C*****     READ PUMPING DATA FROM 'PROPERTIES' AND WRITE TO 'RADFLOW.INPUT'
      READ(80,180) Q,QRCH,DELT,TMAXF,TSM,NTS
      WRITE(100,180) Q,QRCH,DELT,TMAXF,TSM,NTS
180     FORMAT (5F10.3,I10)
      CLOSE(80)
      CLOSE(100)
      RETURN
      END
      SUBROUTINE PLOT(NEL,NB)
C      A. PUCCI AND D. POPE                                VERSION 3/2/87
C
C*****
C      DISPLA PROGRAM TO PLOT TRIANGULAR MESH
C*****
C
C      NEL=NUMBER OF ELEMENTS, NB=NUMBER OF NODES
C      XD,YD ARE ARRAYS USED REPEATEDLY IN PLOTTING EACH ELEMENT BORDER
C
C      NODXY CONTAINS THE X AND Y COORDINATES OF EACH NODE
C      ELM  CONTAINS THE NUMBERS OF THE NODES WHICH ARE AT THE CORNERS OF
C           EACH ELEMENT
C
      INTEGER ELM(800,3)
      REAL NODXY(1000,2),XD(4),YD(4),XMAX,YMAX
      CHARACTER DEV*1,ANS*1,SCALE*1,RESP1*1,RESP2*2,PEN2*4,PEN3*4
      CHARACTER*1  OPT          /*  DEVICE OPTION CODE
      CHARACTER*50  DES          /*  DEVICE DESCRIPTION
      CHARACTER*32  PALET        /*  DEVICE PALET
      LOGICAL       FLAGS(3)     /*  DEVICE OPTION FLAGS
C GDIU              /*      1-PLOT FILE REQUIRED
C GDIU              /*      2-DEVICE IS NOT A GRAPHIC TERMINAL
C GDIU              /*      3-DEVICE HAS GRAPHIC INPUT
      REAL          SIZE(2)      /*  OPTIONAL MAX WIDTH AND HEIGHT OF PLOT
      CHARACTER*128 PLTFIL       /*  NAME OF PLOT FILE, IF NEEDED
      INTEGER       LUPLOT       /*  LOGICAL UNIT TO OPEN PLOT FILE ON
      INTEGER       NDEV         /*  DEVICE NUMBERS
      CHARACTER*8   COLOR        /*  PLOT COLOR
      COMMON NODXY,ELM
C      NEL = TOTAL NUMBER OF ELEMENTS
C
      WRITE(1,*) 'LENGTH OF X-AXIS?'
      WRITE(1,*) 'MAXIMUM RADIAL DISTANCE FOR DOMAIN.'
      READ(1,10) XMAX
10     FORMAT(F6.0)
      WRITE(1,*) 'LENGTH OF Y-AXIS?'
      WRITE(1,*) 'MAXIMUM DEPTH BELOW SURFACE'
      READ(1,10) YMAX
      WRITE(1,*) 'DO YOU WANT THE RADIAL DISTANCE ON A LOG OR AN'
      WRITE(1,*) 'ARITHMETIC SCALE? (ENTER L OR A)'
      READ(1,40) SCALE

```



```

40    FORMAT(A1)
      IF (SCALE .EQ. 'L') THEN
        XMAX = LOG(XMAX)
        DO 20 I = 1,NB
          IF (NODXY(I,1) .NE. 0) THEN
            NODXY(I,1) = LOG(NODXY(I,1))
          ENDIF
20    CONTINUE
      ENDIF

C
C*****
C  SUBROUTINE G_QRDV PRESENTS MENU OF AVAILABLE DEVICES
C*****
C
      LUPLT = 51
C
      NDEV = 0
30    CALL G_QRDV(NDEV)
C
      CALL G_DVDF(OPT,DES,PALET,FLAGS,SIZE,-NDEV,IRTN)
      IF (IRTN .NE. NDEV) STOP 'BAD DEVICE SELECTED'
      IF (FLAGS(1)) GO TO 90
C
      CALL G_INIT(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0) STOP 'ERROR TRYING TO INITIALIZE GRAPHIC DEVICE'
C
      CALL G_GRMO(NDEV,1,1,LUPLT,IERR)
      IF(IERR .NE. 0)STOP 'ERROR TRYING TO GO TO GRAPHIC MODE'
C
      CALL PAGE(10.,10.)
      CALL AREA2D(9.,9.)
      CALL XNAME('DISTANCE FROM WELL',18)
      CALL YNAME('DEPTH BELOW SURFACE',19)
      CALL GRAF(0.,500.,XMAX,YMAX,-50.,0.)
      DO 70 I=1,NEL
        DO 60 JJ=1,3
          XD(JJ)=NODXY(ELM(I,JJ),1)
60      YD(JJ)=NODXY(ELM(I,JJ),2)
          XD(4)=NODXY(ELM(I,1),1)
          YD(4)=NODXY(ELM(I,1),2)
          CALL CURVE(XD,YD,4,0)
70    CONTINUE
C
      CALL ENDPL(0)
      CALL G_TXMO(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0)STOP 'ERROR AT END OF PLOT'
      CALL G_DNPL(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0)STOP 'ERROR AT END OF PLOT'
      CALL TNOUA('DO YOU WANT ANOTHER PLOT, Y OR N?  : ',INTS(34))
      READ(1,80) ANS
80    FORMAT(A1)
      IF (ANS .EQ. 'Y') THEN
        GO TO 30
      ENDIF

```

```

      GO TO 100
C
90    OPEN(LUPLT,FILE='FEM.PLOT',STATUS='NEW')
C
      CALL G_INIT(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0) STOP 'ERROR TRYING TO INITIALIZE GRAPHIC DEVICE'
C
      CALL G_GRMO(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0) STOP 'ERROR TRYING TO GO TO GRAPHIC MODE'
C
      CALL PAGE(30.,30.)
      CALL AREA2D(28.,28.)
      CALL XNAME('DISTANCE FROM WELL',18)
      CALL YNAME('DEPTH BELOW SURFACE',19)
      CALL GRAF(0,50,XMAX,YMAX,-50,0)
      DO 120 I=1,NEL
        DO 110 JJ=1,3
          XD(JJ)=NODXY(ELM(I,JJ),1)
110      YD(JJ)=NODXY(ELM(I,JJ),2)
          XD(4)=NODXY(ELM(I,1),1)
          YD(4)=NODXY(ELM(I,1),2)
          CALL CURVE(XD,YD,4,0)
120      CONTINUE
C
      IF (PALET.NE.' ') THEN
        PEN2 = PALET (9:12)
        PEN3 = PALET (13:16)
      ENDIF
C
C    LABEL TRIANGULAR ELEMENTS
      CALL TNOUA('DO YOU WANT TO LABEL THE ELEMENT NUMBERS? ',INTS(42))
      READ(1,125) RESP1
      IF (RESP1.EQ.'N') GO TO 135
125    FORMAT(A1)
      CALL HEIGHT(0.08)
      IF (PALET.NE.' ') CALL SETCLR(PEN2)
      DO 130 J=1,NEL
        X = (NODXY(ELM(J,1),1)+NODXY(ELM(J,2),1)+NODXY(ELM(J,3),1))/3.0
        Y = (NODXY(ELM(J,1),2)+NODXY(ELM(J,2),2)+NODXY(ELM(J,3),2))/3.0
130    CALL RLINT(J,X,Y)
C    LABEL NODE NUMBERS ON PLOT
135    CALL TNOUA('DO YOU WANT TO LABEL THE NODE NUMBERS? ',INTS(39))
      READ(1,125) RESP2
      IF (RESP2.EQ.'N') GO TO 150
      CALL HEIGHT('RESET')
      CALL HEIGHT(0.05)
      IF (PALET.NE.' ') CALL SETCLR(PEN3)
      CALL MSHIFT(0.0,-0.05)
      DO 140 K=1,NB
        IF (SCALE.EQ.'A') THEN
          XSP=NODXY(K,1)+5.
        ELSE
          XSP = NODXY(K,1) + .4
        ENDIF

```

```

      YSP=NODXY(K,2)+3.
140   CALL RLINT(K,XSP,YSP)
150   CALL ENDPL(0)
      CALL G_TXMO(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0)STOP 'ERROR AT END OF PLOT'
      CALL G_DNPL(NDEV,1,1,LUPLT,IERR)
      IF(IERR.NE.0)STOP 'ERROR AT END OF PLOT'
      CLOSE(51)
100   RETURN
      END

```

APPENDIX 2

Formats for input files

SECTION A

BASIC DATA FILE

Group 1

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	1-4	I4	INRG	= Number of subregions in mesh
	5-8	I4	INBP	= Number of global-mesh nodes

Group 2: Coordinates of boundary points

Number of cards depends on number of boundary points

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
--	1-80	8(F10.5)	XP	= X-coordinates of global-mesh nodes. Number of values = INBP. Origin is pumping well (feet/1000).
	1-80	8(F10.5)	YP	= Y-coordinates of global-mesh nodes. Number of values = INBP. Origin is land surface (feet/1000).

Group 3: Connectivity data

INRG number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1-INRG	1-3	I3	NRG	= subregion number.
	4-15	4(I3)	JT(NRG,K)	= Number of the subregion which shares side K with subregion NRG, K=1 to 4.

Group 4: Data on subregions along constant head boundary

TNR + 1 number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	1-3	I3	NRC	= Number of subregions along the constant-head boundary.

	4-6	I3	TNR	= Total number of rows along the constant-head boundary.
2-INRG	1-3	I3	NRB(I)	= Number of rows in each subregion in order from top to bottom. I=1 to NRC.

Group 5: subregion Data

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
INRG number of cards				
1-INRG	1-4	I4	NRG	= subregion number.
	5-8	I4	NROWS	= Number of rows in subregion.
	9-12	I4	NCOL	= Number of columns in subregion.
	13-44	8(I4)	NDN(I)	= Numbers of the boundary points which define the subregion, I=1 to 8.

SECTION B
PROPERTIES

GROUP 1: Title and problem setup

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	1-80	20A4	TITLE	= Any title the user wishes.
2	1-10	F10.0	PPR	= Primary radial hydraulic conductivity in feet per day (ft/d).
	11-20	F10.0	PPZ	= Primary vertical hydraulic conductivity (ft/d).
	21-30	I10	IPP	= Number of pumping periods.
3	1-10	F10.0	S	= Coefficient of compressive storage (Ss) in 1/ft.
	11-20	F10.0	SY	= Specific Yield (unitless).
4	16-20	I5	NQ	= Number of nodes associated with well screen.
	21-25	I5	NDIF	= Number of elements having different hydraulic conductivities than the primary ones on card 2.

Group 2: Nodes along the well screen

NQ number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
--	1-5	I5	NND(I)	= Node along well screen.

Group 3: Data to assign secondary hydrologic properties to user defined sets of subregions

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	1-3	I3	DIFFK	= Number of subsets of subregions to be assigned secondary properties.

Subgroups: This section will be repeated for each subset of subregions

1	1-10	F10.0	PR	= Radial hydraulic conductivity assigned to all elements contained in the subregions in this subset (ft/d).
	11-20	F10.0	PZ	= Vertical hydraulic conductivity (ft/d).
	21-24	I4	B	= Number of subregions in this subset of subregions.
	25-34	F10.9	DIFFS	= Coefficient of compressive storage (Ss) in feet ⁻¹ .
2-B	1-4	I4	RN	= subregion number to be included in this subset.

Group 4: Pumping period information used in RADFLOW-S.F77

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
	1-10	F10.0	Q	= Pumping rate in cubic feet per second (ft ³ /sec).
	11-20	F10.0	QRCH	= Recharge rate (ft/d).
	21-30	F10.0	DELT	= Initial time step (Days).
	31-40	F10.0	TMAXF	= Maximum length of pumping Period (Days).
	41-50	F10.0	TSM	= Time step multiplier (each time step after DELT is multiplied by TSM).
	51-60	I10	NTS	= Number of time steps in Pumping period.

For more information on RADFLOW options for pumping period simulations see Reilly (1984 pg. 27).

SECTION C

OB.WELL

Group 1: Number of observation wells you have data for

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	1-4	I4	NNO	= Number of observation wells you wish to use.

Group 2: Location of midpoint of screen for each observation well

NNO number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
--	2-7	F6.0	XBAR(I)	= X-coordinate (in feet) of the midpoint of the screen for each observation well, I=1 to NNO.
--	9-14	F6.0	YBAR(I)	= Y-coordinate (in feet) of the midpoint of the screen for each observation well, I=1 to NNO.

Group 3: Element numbers that contain the screen for each observation well

NNO number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
--	1-4	I4	NNE(I)	= Element number that contains the midpoint of the screen for each observation well, I=1 to NNO.

SECTION D

Observation well data file

Group 1

One card

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
1	2-4	I3	N	= Number of observed data points in file.
	5-9	F5.0	R	= Distance of observed well from pumping well (in feet).
	11-15	F5.1	RE	= Reference elevation. Will be zero if the data is drawdown data. If the data is water level data this should be the elevation of the measuring point of the well.

Group 2: Time-drawdown or Time-water-level data

N number of cards

<u>Card</u>	<u>Columns</u>	<u>Format</u>	<u>Variable</u>	<u>Definition</u>
--	1-10	F10.0	T(I)	= Time of measurement in minutes. I=1,N.
	11-20	F10.3	S(I)	= Drawdown or water-level data in feet, I=1 to N.

APPENDIX 3

Example of BASIC DATA FILE for the six subregion example mesh shown in figure 3.

The description of the input data file format is given in appendix 2, section A.

6 29

.4	.5	.6	.6	.6	.5	.4	.4
.4	.4	.5	.6	.6	.3	.2	.2
.2	.3	.2	.2	.3	.1	0.0	0.0
0.0	.1	0.0	0.0	.1			
.1	.1	.1	.05	0.0	0.0	0.0	.05
.15	.2	.2	.2	.15	0.0	0.0	.05
.1	.1	.15	.2	.2	0.0	0.0	.05
.1	.1	.15	.2	.2			

1	2	0	0	3
2	0	0	1	4
3	4	1	0	5
4	0	2	3	6
5	6	3	0	0
6	0	4	5	0

2 7

3

5

1	3	3	1	2	3	4	5	6	7	8
2	5	3	10	11	12	13	3	2	1	9
3	3	3	17	18	1	8	7	14	15	16
4	5	3	20	21	10	9	1	18	17	19
5	3	5	25	26	17	16	15	22	23	24
6	5	5	28	29	20	19	17	26	25	27

APPENDIX 4

Data files used for example simulation shown in figure 4.

SECTION A

BASIC DATA FILE for generating figure 4.

The description of the input data file format is given in appendix 2, section A.

50	181						
10.69	17.9	30.	30.	30.	17.9	10.69	10.69
10.69	10.69	17.9	30.	30.	10.69	10.69	17.9
30.	30.	10.69	10.69	17.9	30.	30.	10.69
10.69	17.9	30.	30.	6.40	3.82	3.82	3.82
6.40	3.82	3.82	6.40	3.82	3.82	6.40	3.82
3.82	6.40	3.82	3.82	6.40	2.28	1.36	1.36
1.36	2.28	1.36	1.36	2.28	1.36	1.36	2.28
1.36	1.36	2.28	1.36	1.36	2.28	.813	.485
.485	.485	.813	.485	.485	.813	.485	.485
.813	.485	.485	.813	.485	.485	.813	.290
.173	.173	.173	.290	.173	.173	.290	.173
.173	.290	.173	.173	.290	.173	.173	.290
.104	.062	.062	.062	.104	.062	.062	.104
.062	.062	.104	.062	.062	.104	.062	.062
.104	.037	.022	.022	.022	.037	.022	.022
.037	.022	.022	.037	.022	.022	.037	.022
.022	.037	.013	.008	.008	.008	.013	.008
.008	.013	.008	.008	.013	.008	.008	.013
.008	.008	.013	.005	.003	.003	.003	.005
.003	.003	.005	.003	.003	.005	.003	.003
.005	.003	.003	.005	.002	0.0	0.0	0.0
.002	0.0	0.0	.002	0.0	0.0	.002	0.0
0.0	.002	0.0	0.0	.002			
0.302	0.302	0.302	0.209	0.117	0.117	0.117	0.209
0.378	0.454	0.454	0.454	0.378	0.525	0.597	0.597
0.597	0.525	0.632	0.650	0.650	0.650	0.632	0.687
0.709	0.709	0.709	0.687	0.117	0.117	0.209	0.302
0.302	0.378	0.454	0.454	0.525	0.597	0.597	0.632
0.650	0.650	0.687	0.709	0.709	0.117	0.117	0.209
0.302	0.302	0.378	0.454	0.454	0.525	0.597	0.597
0.632	0.650	0.650	0.687	0.709	0.709	0.117	0.117
0.209	0.302	0.302	0.378	0.454	0.454	0.525	0.597
0.597	0.632	0.650	0.650	0.687	0.709	0.709	0.117
0.117	0.209	0.302	0.302	0.378	0.454	0.454	0.525
0.597	0.597	0.632	0.650	0.650	0.687	0.709	0.709
0.117	0.117	0.209	0.302	0.302	0.378	0.454	0.454
0.525	0.597	0.597	0.632	0.650	0.650	0.687	0.709
0.709	0.117	0.117	0.209	0.302	0.302	0.378	0.454
0.454	0.525	0.597	0.597	0.632	0.650	0.650	0.687
0.709	0.709	0.117	0.117	0.209	0.302	0.302	0.378
0.454	0.454	0.525	0.597	0.597	0.632	0.650	0.650
0.687	0.709	0.709	0.117	0.117	0.209	0.302	0.302
.378	.454	.454	.525	.597	.597	.632	.650

			.650		.687		.709		.709		.117		.117		.209		.302
			.302		.378		.454		.454		.525		.597		.597		.632
			.650		.650		.687		.709		.709						
1	2	0	0	6													
2	3	0	1	7													
3	4	0	2	8													
4	5	0	3	9													
5	0	0	4	10													
6	7	1	0	11													
7	8	2	6	12													
8	9	3	7	13													
9	10	4	8	14													
10	0	5	9	15													
11	12	6	0	16													
12	13	7	11	17													
13	14	8	12	18													
14	15	9	13	19													
15	0	10	14	20													
16	17	11	0	21													
17	18	12	16	22													
18	19	13	17	23													
19	20	14	18	24													
20	0	15	19	25													
21	22	16	0	26													
22	23	17	21	27													
23	24	18	22	28													
24	25	19	23	29													
25	0	20	24	30													
26	27	21	0	31													
27	28	22	26	32													
28	29	23	27	33													
29	30	24	28	34													
30	0	25	29	35													
31	32	26	0	36													
32	33	27	31	37													
33	34	28	32	38													
34	35	29	33	39													
35	0	30	34	40													
36	37	31	0	41													
37	38	32	36	42													
38	39	33	37	43													
39	40	34	38	44													
40	0	35	39	45													
41	42	36	0	46													
42	43	37	41	47													
43	44	38	42	48													
44	45	39	43	49													
45	0	40	44	50													
46	47	41	0	0													
47	48	42	46	0													
48	49	43	47	0													
49	50	44	48	0													
50	0	45	49	0													

5 13

3

3

3

3

5

1	3	3	1	2	3	4	5	6	7	8
2	3	3	10	11	12	13	3	2	1	9
3	3	3	15	16	17	18	12	11	10	14
4	3	3	20	21	22	23	17	16	15	19
5	5	3	25	26	27	28	22	21	20	24
6	3	3	32	33	1	8	7	29	30	31
7	3	3	35	36	10	9	1	33	32	34
8	3	3	38	39	15	14	10	36	35	37
9	3	3	41	42	20	19	15	39	38	40
10	5	3	44	45	25	24	20	42	41	43
11	3	3	49	50	32	31	30	46	47	48
12	3	3	52	53	35	34	32	50	49	51
13	3	3	55	56	38	37	35	53	52	54
14	3	3	58	59	41	40	38	56	55	57
15	5	3	61	62	44	43	41	59	58	60
16	3	3	66	67	49	48	47	63	64	65
17	3	3	69	70	52	51	49	67	66	68
18	3	3	72	73	55	54	52	70	69	71
19	3	3	75	76	58	57	55	73	72	74
20	5	3	78	79	61	60	58	76	75	77
21	3	3	83	84	66	65	64	80	81	82
22	3	3	86	87	69	68	66	84	83	85
23	3	3	89	90	72	71	69	87	86	88
24	3	3	92	93	75	74	72	90	89	91
25	5	3	95	96	78	77	75	93	92	94
26	3	3	100	101	83	82	81	97	98	99
27	3	3	103	104	86	85	83	101	100	102
28	3	3	106	107	89	88	86	104	103	105
29	3	3	109	110	92	91	89	107	106	108
30	5	3	112	113	95	94	92	110	109	111
31	3	3	117	118	100	99	98	114	115	116
32	3	3	120	121	103	102	100	118	117	119
33	3	3	123	124	106	105	103	121	120	122
34	3	3	126	127	109	108	106	124	123	125
35	5	3	129	130	112	111	109	127	126	128
36	3	3	134	135	117	116	115	131	132	133
37	3	3	137	138	120	119	117	135	134	136
38	3	3	140	141	123	122	120	138	137	139
39	3	3	143	144	126	125	123	141	140	142
40	5	3	146	147	129	128	126	144	143	145
41	3	3	151	152	134	133	132	148	149	150
42	3	3	154	155	137	136	134	152	151	153
43	3	3	157	158	140	139	137	155	154	156
44	3	3	160	161	143	142	140	158	157	159
45	5	3	163	164	146	145	143	161	160	162
46	3	3	168	169	151	150	149	165	166	167
47	3	3	171	172	154	153	151	169	168	170
48	3	3	174	175	157	156	154	172	171	173
49	3	3	177	178	160	159	157	175	174	176
50	5	3	180	181	163	162	160	178	177	179

SECTION B

PROPERTIES data file for region shown in figure 4.

Description of input data set for PROPERTIES is given in appendix 2, section B.

EXAMPLE PUMP TEST

100	10.0	1			
.00000100	.27000				
480	273	13	5	240	
262					
264					
266					
268					
270					
2					
150.	30.0	10	.0000005		
2					
7					
12					
17					
22					
27					
32					
37					
42					
47					
1.0	0.1	20	.000002		
1					
6					
11					
16					
21					
26					
31					
36					
41					
46					
3					
8					
13					
18					
23					
28					
33					
38					
43					
48					
-2.78	0.0	.001	.958	1.2	1000

SECTION C

OB.WELL data file used to generate figure 5.

Description of input data set for OB.WELL is given in appendix 2, section C.

```
1
 600    682.0
181
```

SECTION D

Observed field-data file used to generate figure 5.

Description of input data set for actual pump test data files is given in appendix 2, section D.

```
26 600. 138.7
1.      139.1
2.      139.33
3.      139.4
4.      139.5
5.      139.8
6.      140.
9.      140.25
12.     140.5
18.     141.1
24.     141.5
30.     141.8
45.     142.25
70.     142.9
100.    143.33
140.    143.75
220.    144.5
335.    145.3
455.    145.9
605.    146.5
695.    146.66
845.    147.
965.    147.5
1055.   147.7
1175.   147.75
1295.   147.8
1385.   148.
```

APPENDIX 5

Example of 'OUTPUT' file from MESH 'P' mode for example shown in figure 3.

CONNECTIVITY DATA

SUBREGION	SHARED BOUNDARY			
	1	2	3	4
1	2	0	0	3
2	0	0	1	4
3	4	1	0	5
4	0	2	3	6
5	6	3	0	0
6	0	4	5	0

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 1 ****

NUMBER OF INCREMENTS =

3 ROWS AND 3 COLUMNS

GLOBAL NODE NUMBERS 1 2 3 4 5 6 7 8

FINITE-ELEMENT NODE NUMBERS

8 9 1
10 11 2
12 13 3

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE NUMBERS			X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
1	10	11	9	0.4000	0.0500	0.5000	0.0500	0.5000	0.0000
2	10	9	8	0.4000	0.0500	0.5000	0.0000	0.4000	0.0000
3	11	2	1	0.5000	0.0500	0.6000	0.0500	0.6000	0.0000
4	11	1	9	0.5000	0.0500	0.6000	0.0000	0.5000	0.0000
5	12	13	11	0.4000	0.1000	0.5000	0.1000	0.5000	0.0500
6	12	11	10	0.4000	0.1000	0.5000	0.0500	0.4000	0.0500
7	13	3	2	0.5000	0.1000	0.6000	0.1000	0.6000	0.0500
8	13	2	11	0.5000	0.1000	0.6000	0.0500	0.5000	0.0500

*NOTE: COORDINATES ARE MULTIPLIED BY .001

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 2 ****

NUMBER OF INCREMENTS =

5 ROWS AND 3 COLUMNS

GLOBAL NODE NUMBERS 10 11 12 13 3 2 1 9

FINITE-ELEMENT NODE NUMBERS

12 13 3
14 15 4
16 17 5
18 19 6
20 21 7

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE NUMBERS			X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
9	14	15	13	0.4000	0.1250	0.5000	0.1250	0.5000	0.1000
10	14	13	12	0.4000	0.1250	0.5000	0.1000	0.4000	0.1000
11	15	4	3	0.5000	0.1250	0.6000	0.1250	0.6000	0.1000
12	15	3	13	0.5000	0.1250	0.6000	0.1000	0.5000	0.1000
13	16	17	15	0.4000	0.1500	0.5000	0.1500	0.5000	0.1250

14	16	15	14	0.4000	0.1500	0.5000	0.1250	0.4000	0.1250
15	17	5	4	0.5000	0.1500	0.6000	0.1500	0.6000	0.1250
16	17	4	15	0.5000	0.1500	0.6000	0.1250	0.5000	0.1250
17	18	19	17	0.4000	0.1750	0.5000	0.1750	0.5000	0.1500
18	18	17	16	0.4000	0.1750	0.5000	0.1500	0.4000	0.1500
19	19	6	5	0.5000	0.1750	0.6000	0.1750	0.6000	0.1500
20	19	5	17	0.5000	0.1750	0.6000	0.1500	0.5000	0.1500
21	20	21	19	0.4000	0.2000	0.5000	0.2000	0.5000	0.1750
22	20	19	18	0.4000	0.2000	0.5000	0.1750	0.4000	0.1750
23	21	7	6	0.5000	0.2000	0.6000	0.2000	0.6000	0.1750
24	21	6	19	0.5000	0.2000	0.6000	0.1750	0.5000	0.1750

*NOTE: COORDINATES ARE MULTIPLIED BY .001

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 3 ****

NUMBER OF INCREMENTS =

3 ROWS AND 3 COLUMNS

GLOBAL NODE NUMBERS 17 18 1 8 7 14 15 16

FINITE-ELEMENT NODE NUMBERS

22	23	8
24	25	10
26	27	12

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE NUMBERS			X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
25	24	25	23	0.2000	0.0500	0.3000	0.0500	0.3000	0.0000
26	24	23	22	0.2000	0.0500	0.3000	0.0000	0.2000	0.0000
27	25	10	8	0.3000	0.0500	0.4000	0.0500	0.4000	0.0000
28	25	8	23	0.3000	0.0500	0.4000	0.0000	0.3000	0.0000
29	26	27	25	0.2000	0.1000	0.3000	0.1000	0.3000	0.0500
30	26	25	24	0.2000	0.1000	0.3000	0.0500	0.2000	0.0500
31	27	12	10	0.3000	0.1000	0.4000	0.1000	0.4000	0.0500
32	27	10	25	0.3000	0.1000	0.4000	0.0500	0.3000	0.0500

*NOTE: COORDINATES ARE MULTIPLIED BY .001

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 4 ****

NUMBER OF INCREMENTS =

5 ROWS AND 3 COLUMNS

GLOBAL NODE NUMBERS 20 21 10 9 1 18 17 19

FINITE-ELEMENT NODE NUMBERS

26	27	12
28	29	14
30	31	16
32	33	18
34	35	20

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE NUMBERS			X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
33	28	29	27	0.2000	0.1250	0.3000	0.1250	0.3000	0.1000
34	28	27	26	0.2000	0.1250	0.3000	0.1000	0.2000	0.1000
35	29	14	12	0.3000	0.1250	0.4000	0.1250	0.4000	0.1000
36	29	12	27	0.3000	0.1250	0.4000	0.1000	0.3000	0.1000
37	30	31	29	0.2000	0.1500	0.3000	0.1500	0.3000	0.1250
38	30	29	28	0.2000	0.1500	0.3000	0.1250	0.2000	0.1250
39	31	16	14	0.3000	0.1500	0.4000	0.1500	0.4000	0.1250

40	31	14	29	0.3000	0.1500	0.4000	0.1250	0.3000	0.1250
41	32	33	31	0.2000	0.1750	0.3000	0.1750	0.3000	0.1500
42	32	31	30	0.2000	0.1750	0.3000	0.1500	0.2000	0.1500
43	33	18	16	0.3000	0.1750	0.4000	0.1750	0.4000	0.1500
44	33	16	31	0.3000	0.1750	0.4000	0.1500	0.3000	0.1500
45	34	35	33	0.2000	0.2000	0.3000	0.2000	0.3000	0.1750
46	34	33	32	0.2000	0.2000	0.3000	0.1750	0.2000	0.1750
47	35	20	18	0.3000	0.2000	0.4000	0.2000	0.4000	0.1750
48	35	18	33	0.3000	0.2000	0.4000	0.1750	0.3000	0.1750

*NOTE: COORDINATES ARE MULTIPLIED BY .001

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 5 ****

NUMBER OF INCREMENTS =

3 ROWS AND 5 COLUMNS

GLOBAL NODE NUMBERS 25 26 17 16 15 22 23 24

FINITE-ELEMENT NODE NUMBERS

36	37	38	39	22
40	41	42	43	24
44	45	46	47	26

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE	NUMBERS	X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
49	40	41 37	0.0000	0.0500	0.0500	0.0500	0.0500	0.0000
50	40	37 36	0.0000	0.0500	0.0500	0.0000	0.0000	0.0000
51	41	42 38	0.0500	0.0500	0.1000	0.0500	0.1000	0.0000
52	41	38 37	0.0500	0.0500	0.1000	0.0000	0.0500	0.0000
53	42	43 39	0.1000	0.0500	0.1500	0.0500	0.1500	0.0000
54	42	39 38	0.1000	0.0500	0.1500	0.0000	0.1000	0.0000
55	43	24 22	0.1500	0.0500	0.2000	0.0500	0.2000	0.0000
56	43	22 39	0.1500	0.0500	0.2000	0.0000	0.1500	0.0000
57	44	45 41	0.0000	0.1000	0.0500	0.1000	0.0500	0.0500
58	44	41 40	0.0000	0.1000	0.0500	0.0500	0.0000	0.0500
59	45	46 42	0.0500	0.1000	0.1000	0.1000	0.1000	0.0500
60	45	42 41	0.0500	0.1000	0.1000	0.0500	0.0500	0.0500
61	46	47 43	0.1000	0.1000	0.1500	0.1000	0.1500	0.0500
62	46	43 42	0.1000	0.1000	0.1500	0.0500	0.1000	0.0500
63	47	26 24	0.1500	0.1000	0.2000	0.1000	0.2000	0.0500
64	47	24 43	0.1500	0.1000	0.2000	0.0500	0.1500	0.0500

*NOTE: COORDINATES ARE MULTIPLIED BY .001

1

**** ARRANGEMENT OF GLOBAL NODE AND FINITE ELEMENT NODE NUMBER, IN SUBREGION 6 ****

NUMBER OF INCREMENTS =

5 ROWS AND 5 COLUMNS

GLOBAL NODE NUMBERS 28 29 20 19 17 26 25 27

FINITE-ELEMENT NODE NUMBERS

44	45	46	47	26
48	49	50	51	28
52	53	54	55	30
56	57	58	59	32
60	61	62	63	34

ELEMENT NUMBERS, FINITE-ELEMENT NODE NUMBERS, AND NODE COORDINATES

NEL	NODE	NUMBERS	X(1)	Y(1)	X(2)	Y(2)	X(3)	Y(3)
65	48	49 45	0.0000	0.1250	0.0500	0.1250	0.0500	0.1000

66	48	45	44	0.0000	0.1250	0.0500	0.1000	0.0000	0.1000
67	49	50	46	0.0500	0.1250	0.1000	0.1250	0.1000	0.1000
68	49	46	45	0.0500	0.1250	0.1000	0.1000	0.0500	0.1000
69	50	51	47	0.1000	0.1250	0.1500	0.1250	0.1500	0.1000
70	50	47	46	0.1000	0.1250	0.1500	0.1000	0.1000	0.1000
71	51	28	26	0.1500	0.1250	0.2000	0.1250	0.2000	0.1000
72	51	26	47	0.1500	0.1250	0.2000	0.1000	0.1500	0.1000
73	52	53	49	0.0000	0.1500	0.0500	0.1500	0.0500	0.1250
74	52	49	48	0.0000	0.1500	0.0500	0.1250	0.0000	0.1250
75	53	54	50	0.0500	0.1500	0.1000	0.1500	0.1000	0.1250
76	53	50	49	0.0500	0.1500	0.1000	0.1250	0.0500	0.1250
77	54	55	51	0.1000	0.1500	0.1500	0.1500	0.1500	0.1250
78	54	51	50	0.1000	0.1500	0.1500	0.1250	0.1000	0.1250
79	55	30	28	0.1500	0.1500	0.2000	0.1500	0.2000	0.1250
80	55	28	51	0.1500	0.1500	0.2000	0.1250	0.1500	0.1250
81	56	57	53	0.0000	0.1750	0.0500	0.1750	0.0500	0.1500
82	56	53	52	0.0000	0.1750	0.0500	0.1500	0.0000	0.1500
83	57	58	54	0.0500	0.1750	0.1000	0.1750	0.1000	0.1500
84	57	54	53	0.0500	0.1750	0.1000	0.1500	0.0500	0.1500
85	58	59	55	0.1000	0.1750	0.1500	0.1750	0.1500	0.1500
86	58	55	54	0.1000	0.1750	0.1500	0.1500	0.1000	0.1500
87	59	32	30	0.1500	0.1750	0.2000	0.1750	0.2000	0.1500
88	59	30	55	0.1500	0.1750	0.2000	0.1500	0.1500	0.1500
89	60	61	57	0.0000	0.2000	0.0500	0.2000	0.0500	0.1750
90	60	57	56	0.0000	0.2000	0.0500	0.1750	0.0000	0.1750
91	61	62	58	0.0500	0.2000	0.1000	0.2000	0.1000	0.1750
92	61	58	57	0.0500	0.2000	0.1000	0.1750	0.0500	0.1750
93	62	63	59	0.1000	0.2000	0.1500	0.2000	0.1500	0.1750
94	62	59	58	0.1000	0.2000	0.1500	0.1750	0.1000	0.1750
95	63	34	32	0.1500	0.2000	0.2000	0.2000	0.2000	0.1750
96	63	32	59	0.1500	0.2000	0.2000	0.1750	0.1500	0.1750

BANDWIDTH QUANTITY IS 32 CALCULATED IN ELEMENT 95

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C
C
C
C
C
C***** MAN 70
C MAN 80
C A GALERKIN FINITE-ELEMENT FLOW MODEL FOR THE TRANSIENT MAN 90
C RESPONSE OF A RADIALLY-SYMMETRIC AQUIFER (Reilly, 1984) MAN 100
C MAN 110
C PR, PZ = FT/DAY ; ZE, RE=FT ; Q=CFS ; TIME =DAYS MAN 120
C QRCH=FT/DAY (+ MEANS RECHARGE ; - MEANS DISCHARGE) MAN 130
C MAN 140
C CONSTANT DRAWDOWN NODES MUST BE NUMBERED FIRST MAN 150
C (I.E. 1,2,3,.....) MAN 160
C PPR=PRIMARY RADIAL HYDRAULIC CONDUCTIVITY MAN 170
C PPZ=PRIMARY VERTICAL HYDRAULIC CONDUCTIVITY MAN 180
C NDIF=# OF ELEMENTS WITH PROPERTIES DIFFERERER FROM THE
C PRIMARY PROPERTIES
C NE=# OF ELEMENTS; NN=# OF NODES;NCH=# OF CONSTANT DRAWDOWN NODES MAN 200
C NQ=# OF NODES DISCHARGING;NND=NODES DISCH. MAN 210
C IF NODE HAS AN 'UNCONFINED' BOUNDARY PUT A '1' IN COL. 35 MAN 220
C IF NODE HAS A RECHARGE TOP BOUNDARY PUT A '1' IN COL. 40 MAN 230
C IF NODE HAS A CONSTANT ZERO DRAWDOWN PUT A '1' IN COL. 45 MAN 240
C MAN 250
C***** MAN 260
C
C*****
C
C
C
C* NNE = # OF ELEMENTS WITH PROPERTIES DIFFERING FROM THE PRIMARY PROPERTIES
C* XBAR,YBAR = ARRAYS OF COORDINATES FOR THE CENTERS OF OBSERVATION WELL
C* SCREEN LOCATIONS, UP TO FIVE OBSERVATION WELLS
C* N1,N2,N3 = LINEAR TRIANGULAR SHAPE FUNCTIONS
C* PHI = AN ARRAY OF HEAD(S) FOR EACH OBSERVATION WELL FOR EACH ITERATION,
C* UP TO FIVE OBSERVATION WELLS.
C* POB,TOB = CUMULATIVE ARRAY OF CALCULATED HEAD(S) AT SIMULATION TIMES, FOR
C* EACH OBSERVATION WELL(S), UP TO FIVE OBSERVATION WELLS AND UP TO
C* 100 ITERATIONS AS PRESENTLY DIMENSIONED.
C* EPSI = A GAUSSIAN NORM STATISTIC COMPARING THE PREDICTED AND OBSERVED
C* DRAWDOWNS IN EACH OBSERVATION WELL(S), UP TO FIVE WELLS
C* SS = AN ARRAY CONTAINING THE SPECIFIC STORAGE VALUES FOR EACH TRIANGULAR
C* ELEMENT
C*****
C
C DIMENSION NG(480,3), PR(480), PZ(480), RE(273), ZE(273), IFLUX(273MAN 20
C 1), IQ(273), IRCH(273), NSCON(273), F(273), S1(273), S3(260), S5(26MAN 30
C 20), F2(260), WG1(260,59), WTRA1(260,59), R(3), Z(3), ZI(3), RI(3),MAN 40
C 3 L(3), W(3,3), WR(3,3), WZ(3,3), WW(3,3), WST(3,3), NND(50), TITLEMAN 50
C 4(20),SS(480) MAN
C*****
C ARRAYS THAT ARE INTRODUCED IN THE RADFLOW-S VERSION
C*****
C DIMENSION NNE(5)
C REAL N1,N2,N3,XBAR(5),YBAR(5),PHI(5)

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REAL POB(5,100),TOB(5,100),EPSI(5)
COMMON /PT/ POB,TOB
C NNE= OBSERVATION WELL ELEMENT NUMBERS
COMMON /ELEM/NG,PR,PZ
COMMON /NODES/RE,ZE,IFLUX,IQ,IRCH,NSCON,F,S1
COMMON /GLOBAL/WG1,WTRAI
COMMON /EPS/EPSI
C***** MAN 70
C MAN 80
C A GALERKIN FINITE-ELEMENT FLOW MODEL FOR THE TRANSIENT MAN 90
C RESPONSE OF A RADIALY SYMMETRIC AQUIFER MAN 100
C MAN 110
C PR, PZ = FT/DAY ; ZE, RE=FT ; Q=CFS ; TIME =DAYS MAN 120
C QRCH=FT/DAY (+ MEANS RECHARGE ; - MEANS DISCHARGE) MAN 130
C MAN 140
C CONSTANT DRAWDOWN NODES MUST BE NUMBERED FIRST MAN 150
C (I.E. 1,2,3,.....) MAN 160
C PPR=PRIMARY RADIAL HYDRAULIC CONDUCTIVITY MAN 170
C PPZ=PRIMARY VERTICAL HYDRAULIC CONDUCTIVITY MAN 180
C NDIF=# OF DIFFERING HYDRAULIC CONDUCTIVITY ELEMENTS MAN 190
C NE=# OF ELEMENTS; NN=# OF NODES;NCH=# OF CONSTANT DRAWDOWN NODES MAN 200
C NQ=# OF NODES DISCHARGING;NND=NODES DISCH. MAN 210
C IF NODE HAS AN 'UNCONFINED' BOUNDARY PUT A '1' IN COL. 35 MAN 220
C IF NODE HAS A RECHARGE TOP BOUNDARY PUT A '1' IN COL. 40 MAN 230
C IF NODE HAS A CONSTANT ZERO DRAWDOWN PUT A '1' IN COL. 45 MAN 240
C MAN 250
C***** MAN 260
C MAN 270
C MAN 271
C INPUT-OUTPUT MAN 272
C MAN 273
C*****
C FILES USED FOR I/O INTRODUCED IN RADFLOW-S
C*****
OPEN(UNIT=55,FILE='RADFLOW.INPUT',STATUS='OLD')
OPEN(UNIT=56,FILE='RAD.OUTPUT',STATUS='NEW')
OPEN(UNIT=57,FILE='OB.WELL',STATUS='OLD')
C MAN 276
C CALCULATE CONSTANTS MAN 280
C MAN 290
C TPI=3.1416*2. MAN 300
C CONV1=1440.*60. MAN 310
C MAN 320
C READ (55,11) TITLE MAN 330
11 FORMAT (20A4) MAN 340
WRITE (56,12) TITLE MAN 350
12 FORMAT (1H1,10X,20A4) MAN 360
READ (55,13) PPR,PPZ,IPP MAN 370
13 FORMAT (2F10.0,I10) MAN 380
READ (55,14) S,SY MAN 390
14 FORMAT (2F10.0) MAN 400
WRITE (56,15) S MAN 410
15 FORMAT (1H0,36H COEFFICIENT OF SPECIFIC STORAGE=,E12.5,5H 1/FT)MAN 420
WRITE (56,16) SY MAN 430

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16 FORMAT (1H0,17H SPECIFIC YIELD =,F10.4) MAN 440
   WRITE (56,17) PPR,PPZ MAN 450
17 FORMAT (1H0,38H THE PRIMARY HYDRAULIC CONDUCTIVITY = ,F10.3,12H RMAN 460
   RADIALY &,F10.3,21H VERTICALLY (FT/DAY)) MAN 470
   READ (55,18) NE,NN,NCH,NQ,NDIF MAN 480
18 FORMAT (5I5) MAN 490
   WRITE (56,19) NE,NN,NCH,NQ,NDIF MAN 500
19 FORMAT (1H0,I5,13H ELEMENTS ,I5,9H NODES ,I5,22H CONSTANT VAMAN 510
   ILUE NODES,I5,18H NODES DISCHARGING,I5,23H ELEMENTS OF DIFF. H.C.) MAN 520
   IF (NQ.EQ.0) GO TO 24 MAN 530
   WRITE (56,20) MAN 540
20 FORMAT (1H0,17H DISCHARGING NODES) MAN 550
   DO 23 I=1,NQ MAN 560
   READ (55,21) NND(I) MAN 570
21 FORMAT (I5) MAN 580
   WRITE (56,22) NND(I) MAN 590
22 FORMAT (1X,I9) MAN 600
23 CONTINUE MAN 610
24 DO 25 I=1,NE MAN 620
   PR(I)=PPR MAN 630
   PZ(I)=PPZ MAN 640
C*****
C INITIALIZE SPECIFIC STORAGE IN EACH TRIANGULAR ELEMENT
C*****
   SS(I)=S
25 CONTINUE MAN 650
C MAN 660
C*****
C DEFINE ELEMENTS OF DIFFERENT CONDUCTIVITIES MAN 670
C*****
C MAN 680
   IF (NDIF.EQ.0) GO TO 31 MAN 690
C*****
C SOME SECTION OF THE ORIGINAL RADFLOW SOURCE CODE HAVE BEEN COMMENTED
C OUT WITH AN 'CS' IN RADFLOW-S BECAUSE OF REDUNDANCIES WITH THE MESH
C PRE-PROCESSOR. THEY REMAIN AS COMMENTED STATEMENTS TO HELP THE
C PROGRAM REVIEWER
C*****
C WRITE (56,26)
CS26 FORMAT (1H0,1X,39H, ELEMENTS WITH DIFFERENT CONDUCTIVITIES)
CS WRITE (56,27) MAN 720
CS 27 FORMAT (1H0,1X,7HELEMENT,5X,11HRADIAL H.C.,5X,13HVERTICAL H.C.) MAN 730
   DO 30 K=1,NDIF MAN 740
   READ (55,28) IE,PR(IE),PZ(IE),SS(IE) MAN 750
28 FORMAT (I10,2F10.0,5X,F10.0) MAN 760
CS WRITE (56,29) IE,PR(IE),PZ(IE) MAN 770
CS 29 FORMAT (1X,I5,10X,F10.3,10X,F10.3) MAN 780
30 CONTINUE MAN 790
C MAN 800
C*****
C READ NODAL ORDER OF EACH ELEMENT MAN 810
C*****
C MAN 820
CS 31 WRITE (56,32) MAN 830

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CS 32 FORMAT (1H0,7HELEMENT,10X,11HNODAL ORDER) MAN 840
31 DO 35 I=1,NE MAN 850
    READ (55,33) IE,NG(IE,1),NG(IE,2),NG(IE,3) MAN 860
33 FORMAT (4I5) MAN 870
CS WRITE (56,34) IE,NG(IE,1),NG(IE,2),NG(IE,3) MAN 880
CS 34 FORMAT (5X,I5,5X,3(2X,I5)) MAN 890
35 CONTINUE MAN 900
C*****
C READ # OF OBSERVATION WELLS
C MAXIMUM OF 5 OBSERVATION WELLS
C*****
    READ(57,221) NNO
221 FORMAT(5(1X,I4))
C*****
C READ LOCATION FOR OBSERVATION WELLS IN EACH ELEMENT
C*****
    DO 223 I=1,NNO
        READ(57,222) XBAR(I),YBAR(I)
222 FORMAT (2(1X,F6.0))
223 CONTINUE
C*****
C READ ELEMENT NUMBERS FOR OB. WELLS
C*****
    DO 224 I=1,NNO
        READ(57,225) NNE(I)
225 FORMAT(5(1X,I4))
224 CONTINUE
C*****
C MAN 910
C READ NODAL COORDINATES FOR EACH NODE MAN 920
C MAN 930
C*****
CS WRITE (56,36) MAN 940
CS 36 FORMAT (1H0,17HNODAL INFORMATION) MAN 950
CS WRITE (56,37) MAN 960
CS 37 FORMAT (1X,4HNODE,10X,1HR,10X,1HZ,10X,10HUNCONFINED,10X,16HSURFACEMAN 970
CS 1 RECHARGE,10X,13HCONSTANT HEAD) MAN 980
    DO 40 J=1,NN MAN 990
        IQ(J)=0 MAN1000
        READ (55,38) IND,RE(IND),ZE(IND),IFLUX(IND),IRCH(IND),NSCON(IND) MAN1010
38 FORMAT (I10,2F10.0,3I5) MAN1020
CS WRITE (56,39) IND,RE(IND),ZE(IND),IFLUX(IND),IRCH(IND),NSCON(IND) MAN1030
CS 39 FORMAT (1X,I5,2F10.2,3(15X,I5)) MAN1040
40 CONTINUE MAN1050
C MAN1060
C*****
C CHECK INPUT DATA FOR CONSISTENCY MAN1070
C*****
C MAN1080
    CALL CHECK(NE,NN,NCH,NG,RE,ZE,NSCON,IERR) MAN1090
    IF (IERR.EQ.1) GO TO 91 MAN1100
C MAN1110
C*****
C DEFINE DISCHARGING NODES MAN1120

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C*****
C
    IF (NQ.EQ.0) GO TO 46
    DO 41 K=1,NQ
    IQ(NND(K))=1
41 CONTINUE
C
C*****
C    DEFINE TOTAL TRANSMISSIVITY OF SCREEN LENGTH
C*****
C
    TRTOT=0.
    DO 45 J=1,NE
    DO 44 I=1,3
    IF (IQ(NG(J,I)).NE.1) GO TO 44
    IF (I.EQ.1) GO TO 42
    IF (IQ(NG(J,I-1)).NE.1) GO TO 44
    TI=PR(J)*ABS(ZE(NG(J,I))-ZE(NG(J,I-1)))
    GO TO 43
42 IF (IQ(NG(J,3)).NE.1) GO TO 44
    TI=PR(J)*ABS(ZE(NG(J,1))-ZE(NG(J,3)))
43 TRTOT=TRTOT+TI
44 CONTINUE
45 CONTINUE
C
C*****
C    DETERMINE HALF BAND WIDTH AND NEEDED MATRIX WIDTH
C*****
C
46 IHBW1=0
    DO 50 I=1,NE
    DO 49 J=1,3
    IF (J.EQ.1) GO TO 47
    IF (NSCON(NG(I,J-1)).EQ.1) GO TO 49
    IF (NSCON(NG(I,J)).EQ.1) GO TO 49
    IHBW=IABS(NG(I,J)-NG(I,J-1))
    GO TO 48
47 IF (NSCON(NG(I,1)).EQ.1) GO TO 49
    IF (NSCON(NG(I,3)).EQ.1) GO TO 49
    IHBW=IABS(NG(I,1)-NG(I,3))
48 IF (IHBW.LT.IHBW1) GO TO 49
    IHBW1=IHBW
49 CONTINUE
50 CONTINUE
    M=2*IHBW1+1
    WRITE (56,51) IHBW1,M
51 FORMAT (1H0,22H THE HALF BAND WIDTH IS,15,32H AND THE WIDTH OF THE
1 MATRIX IS,15)
    DO 52 II=1,NN
    S1(II)=0.0
52 CONTINUE
    MM=NN-NCH
C
C    SET UP PUMPING PERIOD

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```

MAN1130
MAN1140
MAN1150
MAN1160
MAN1170
MAN1180
MAN1190
MAN1200
MAN1210
MAN1220
MAN1230
MAN1240
MAN1250
MAN1260
MAN1270
MAN1280
MAN1290
MAN1300
MAN1310
MAN1320
MAN1330
MAN1340
MAN1350
MAN1360
MAN1370
MAN1380
MAN1390
MAN1400
MAN1410
MAN1420
MAN1430
MAN1440
MAN1450
MAN1460
MAN1470
MAN1480
MAN1490
MAN1500
MAN1510
MAN1520
MAN1530
MAN1540
MAN1550
MAN1560
MAN1570
MAN1580
MAN1590
MAN1600
MAN1610

```


C		MAN1620
	TITO=0.0	MAN1630
	DO 90 NPP=1,IPP	MAN1640
	DO 53 II=1,NN	MAN1650
	F(II)=0.0	MAN1660
53	CONTINUE	MAN1670
	READ (55,54) Q,QRCH,DELT,TMAXF,TSM,NTS	MAN1680
54	FORMAT (5F10.0,I10)	MAN1690
	DT=DELT	MAN1700
	TM=0.0	MAN1710
	DO 55 I=1,NTS	MAN1720
	TM=TM+DT	MAN1730
	IF (TM.GE.TMAXF) GO TO 56	MAN1740
	DT=TSM*DT	MAN1750
55	CONTINUE	MAN1760
	GO TO 57	MAN1770
56	DELT=TMAXF/TM*DELT	MAN1780
	NTS=I	MAN1790
57	WRITE (56,58) NPP,DELT,NTS	MAN1800
58	FORMAT (1H1,14HPUMPING PERIOD,I10,/,20H INITIAL TIME STEP =,F10.5,15H DAYS,/,46H NUMBER OF TIME STEPS IN THIS PUMPING PERIOD =,I10)	MAN1810
	WRITE (56,59) Q	MAN1830
59	FORMAT (1H0,11HDISCHARGE=,E12.5,6H CFS)	MAN1840
	WRITE (56,60) QRCH	MAN1850
60	FORMAT (1H0,10HRECHARGE=,F7.2,8H FT/DAY)	MAN1860
	Q=Q*CONVL	MAN1870
C		MAN1880
C	VALUE OF SINK MATRIX	MAN1890
C		MAN1900
	QTOT=0.0	MAN1910
	DO 65 K=1,NE	MAN1920
	DO 61 J=1,3	MAN1930
	L(J)=NG(K,J)	MAN1940
	R(J)=RE(L(J))	MAN1950
	Z(J)=ZE(L(J))	MAN1960
61	CONTINUE	MAN1970
	DO 64 I=1,3	MAN1980
	DO 63 J=1,3	MAN1990
	IF (IQ(L(J)).NE.1) GO TO 62	MAN2000
	IF (IQ(L(I)).NE.1) GO TO 62	MAN2010
	BLEN=SQRT((ABS(R(I)-R(J)))**2+(ABS(Z(I)-Z(J)))**2)	MAN2020
	F(L(I))=Q*PR(K)*BLEN/(2.*TRTOT)+F(L(I))	MAN2030
	QTOT=Q*PR(K)*BLEN/(2.*TRTOT)+QTOT	MAN2040
62	IF (IRCH(L(J)).NE.1) GO TO 63	MAN2050
	IF (IRCH(L(I)).NE.1) GO TO 63	MAN2060
	AREA=3.1416*ABS(R(J)**2-R(I)**2)	MAN2070
	F(L(I))=QRCH*AREA/2.+F(L(I))	MAN2080
63	CONTINUE	MAN2090
64	CONTINUE	MAN2100
65	CONTINUE	MAN2110
	DO 66 I=1,MM	MAN2120
	F2(I)=F(I+NCH)	MAN2130
66	CONTINUE	MAN2140
C		MAN2150

C	CHECK DISCHARGE	MAN2160
C		MAN2170
	QTOT=QTOT/CONV1	MAN2180
	WRITE (56,67) QTOT	MAN2190
	67 FORMAT (1H0,28H CALCULATED WELL DISCHARGE =,F10.2,4H CFS)	MAN2200
C		MAN2210
C	START TIME LOOP	MAN2220
C	*****	
	TIME=0.0	MAN2240
C	*****	
C	NIT= IS COUNTER FOR PRINT ROUTINE	
C	*****	
	NIT=0	
	DO 89 IT=1,NTS	MAN2250
C	*****	
C	INITIALIZE VARIABLES	MAN2270
C	*****	
C		MAN2280
	DO 69 I=1,MM	MAN2290
	DO 68 J=1,M	MAN2300
	WTRA1(I,J)=0.0	MAN2310
	WG1(I,J)=0.0	MAN2320
	68 CONTINUE	MAN2330
	69 CONTINUE	MAN2340
	DO 79 K=1,NE	MAN2350
C	*****	
C	ASSIGN SPECIFIC STORAGE FOR EACH ELEMENT DURING CONDUCTIVITY	
C	MATRIX ASSEMBLY	
C	*****	
	S=SS(K)	
	DO 70 J=1,3	MAN2360
	L(J)=NG(K,J)	MAN2370
	R(J)=RE(L(J))	MAN2380
	Z(J)=ZE(L(J))	MAN2390
	70 CONTINUE	MAN2400
C		MAN2410
C	AVERAGE DISTANCE R OF ELEMENT	MAN2420
C		MAN2430
	RBAR=(R(1)+R(2)+R(3))/3.	MAN2440
C		MAN2450
	DO 72 I=1,3	MAN2460
	DO 71 J=1,3	MAN2470
	W(I,J)=0.0	MAN2480
	71 CONTINUE	MAN2490
	72 CONTINUE	MAN2500
	ZI(1)=Z(2)-Z(3)	MAN2510
	ZI(2)=Z(3)-Z(1)	MAN2520
	ZI(3)=Z(1)-Z(2)	MAN2530
	RI(1)=R(3)-R(2)	MAN2540
	RI(2)=R(1)-R(3)	MAN2550
	RI(3)=R(2)-R(1)	MAN2560
	DEL=(ZI(1)*R(1)+ZI(2)*R(2)+ZI(3)*R(3))/2.	MAN2570
C		MAN2580
C	CALCULATE ELEMENT MATRICIES	MAN2590

C		MAN2600
	DO 78 I=1,3	MAN2610
	DO 77 J=1,3	MAN2620
	WR(I,J)=TPI*RBAR*PR(K)*ZI(I)*ZI(J)/(4.*DEL)	MAN2630
	WZ(I,J)=TPI*RBAR*PZ(K)*RI(I)*RI(J)/(4.*DEL)	MAN2640
	IF (I.EQ.J) GO TO 73	MAN2650
	WST(I,J)=S*TPI*R(I)*DEL/(DELT*12.)	MAN2660
	GO TO 74	MAN2670
73	WST(I,J)=S*TPI*R(I)*DEL/(DELT*6.)	MAN2680
74	WW(I,J)=WR(I,J)+WZ(I,J)	MAN2690
	IF (I.NE.J) GO TO 76	MAN2700
	IF (IFLUX(L(I)).NE.1) GO TO 76	MAN2710
	AREA=0.0	MAN2720
	DO 75 KK=1,3	MAN2730
	IF (KK.EQ.I) GO TO 75	MAN2740
	IF (IFLUX(L(KK)).NE.1) GO TO 75	MAN2750
	AREA=3.1416*ABS(R(I)*R(I)-R(KK)*R(KK))	MAN2760
75	CONTINUE	MAN2770
	W(I,J)=-SY*AREA/(2.*DELT)	MAN2780
C		MAN2790
C	ASSEMBLE ELEMENT MATRICIES INTO GLOBAL	MAN2800
C		MAN2810
76	IF (NSCON(L(J)).EQ.1) GO TO 77	MAN2820
	IF (NSCON(L(I)).EQ.1) GO TO 77	MAN2830
	II=NG(K,I)-NCH	MAN2840
	JJ=NG(K,J)-NCH	MAN2850
	MTRAN=JJ-II+(M+1)/2	MAN2860
C		MAN2870
C	GLOBAL TRANSIENT MATRIX	MAN2880
C		MAN2890
	WTRA1(II,MTRAN)=WST(I,J)+W(I,J)+WTRA1(II,MTRAN)	MAN2900
C		MAN2910
C	GLOBAL MATRIX	MAN2920
C		MAN2930
	WG1(II,MTRAN)=WW(I,J)+WG1(II,MTRAN)	MAN2940
77	CONTINUE	MAN2950
78	CONTINUE	MAN2960
79	CONTINUE	MAN2970
C		MAN2980
C		MAN2990
C	SUM OF GLOBAL AND TRANSIENT COEFFICIENT MATRICIES	MAN3000
C	ON LEFT HAND SIDE	MAN3010
C		MAN3020
	DO 81 I=1,MM	MAN3030
	DO 80 J=1,M	MAN3040
	WG1(I,J)=WTRA1(I,J)+WG1(I,J)	MAN3050
80	CONTINUE	MAN3060
81	CONTINUE	MAN3070
C		MAN3080
C	MULT. OF MATRICIES ON RIGHT HAND SIDE	MAN3090
C		MAN3100
	DO 82 I=1,MM	MAN3110
	S3(I)=S1(I+NCH)	MAN3120
	S5(I)=0.0	MAN3130

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82 CONTINUE MAN3140
CALL MLTBM(WTRAl,S3,S5,MM,M) MAN3150
DO 83 I=1,MM MAN3160
S5(I)=S5(I)+F2(I) MAN3170
83 CONTINUE MAN3180
C MAN3190
C SOLUTION MAN3200
C MAN3210
CALL SOLVE(1,WG1,S5,MM,IHBW1,MM,M) MAN3220
CALL SOLVE(2,WG1,S5,MM,IHBW1,MM,M) MAN3230
NNN=NCH+1 MAN3240
DO 84 I=NNN,NN MAN3250
S1(I)=S5(I-NCH) MAN3260
84 CONTINUE MAN3270
C
TIME=TIME+DELT MAN3280
TIMM=TIME*1440. MAN3290
ACTT=TIME+TITO MAN3300
C*****
C WRITE OUT OBSERVATION WELL RESULTS AFTER EACH ITERATION
C*****
DO 801 KK=1,NNO
LN=NNE(KK)
XBARE=XBAR(KK)
YBARE=YBAR(KK)
DO 802 JJ=1,3
L(JJ)=NG(LN,JJ)
R(JJ)=RE(L(JJ))
802 Z(JJ)=ZE(L(JJ))
A1=R(2)*Z(3)-R(3)*Z(2)
A2=R(3)*Z(1)-R(1)*Z(3)
A3=R(1)*Z(2)-R(2)*Z(1)
B1=Z(2)-Z(3)
B2=Z(3)-Z(1)
B3=Z(1)-Z(2)
C1=R(3)-R(2)
C2=R(1)-R(3)
C3=R(2)-R(1)
DELT2=(B1*R(1)+B2*R(2)+B3*R(3))
N1=(A1+B1*XBARE+C1*YBARE)/DELT2
N2=(A2+B2*XBARE+C2*YBARE)/DELT2
N3=(A3+B3*XBARE+C3*YBARE)/(2*DELT2)
PHI(KK)=N1*S1(L(1))+N2*S1(L(2))+N3*S1(L(3))
801 CONTINUE
C*****
C PRINT OUT OBSERVATION WELL DATA FOR EACH ITERATION
C*****
WRITE(56,850) ACTT
850 FORMAT(1X,'THE OBSERVATION WELL DATA AT TIME =',F10.3,' DAYS')
DO 860 KK=1,NNO
WRITE (56,851) KK,PHI(KK)
851 FORMAT(1X,'AT OBS WELL #',I2,2X,'THE DRAWDOWN IS ',F6.3,1X,
1' FEET')
POB(KK,IT)=PHI(KK)

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      TOB(KK,IT)=ACTT*1440
860  CONTINUE
C*****
C  AN ARITHMETIC LOGICAL TEST FOR PRINTING OUTPUT FOR ENTIRE FLOW FIELD
C  EVERY TENTH ITERATION OR LAST ITERATION
C*****
      IF (IT .EQ. NTS) GO TO 998
      NIT=NIT+1
      NITT=NIT/10
      NIP=NITT*10
      IF(NIT .NE. NIP) GO TO 999

C
C      OUTPUT
C
998  WRITE (56,85) ACTT
      85  FORMAT (1H1,30HTOTAL TIME IN THE SIMULATION =,F10.3,5H DAYS)
      WRITE (56,86) TIME,TIMM
      86  FORMAT (1H0,18HTHE DRAWDOWN AFTER,E10.3,9H  DAYS OR,E10.3,26HMIN.
      1IN THE PUMPING PERIOD)
      WRITE (56,87)
      87  FORMAT (1H0,10X,12H NODE NUMBER,5X,8HDRAWDOWN,10X,12H NODE NUMBER,
      15X,8HDRAWDOWN,10X,12H NODE NUMBER,5X,8HDRAWDOWN)
      WRITE (56,88) (I,S1(I),I=1,NN)
      88  FORMAT (10X,I5,10X,F10.3,10X,I5,10X,F10.3,10X,I5,10X,F10.3)
999  DELT=DELT*TSM
      89  CONTINUE
      TITO=TIME+TITO
      90  CONTINUE
      GO TO 93
      91  WRITE (56,92)
      92  FORMAT (1H1,49H**TERMINATION OF PROGRAM DUE TO INPUT DATA ERRORS)
      GO TO 935
C*****
C  CALL DRAWDOWN PLOTTING ROUTINE FOR SIMULATION AND FOR TEST
C  DATA AT THE OBSERVATION WELL
C*****
93   DO 931 NPLT=1,NNO
931  CALL PTPLOT(NPLT,NTS)
      WRITE(56,993) (EPSI(I),I=1,NNO)
993  FORMAT(1X,5(/,F10.5))
935  STOP
      END
      SUBROUTINE CHECK(NE,NN,NCH,NG,RE,ZE,NSCON,IERR)
      DIMENSION NG(NE,3),RE(NN),ZE(NN),NSCON(NN)

C
C      THIS SUBROUTINE CHECKS THE ELEMENT INPUT DATA FOR CONSISTANCY
C
      IERR=0
      NCK=0

C
C      CHECK NUMBER AND ORDER OF CONSTANT HEAD NODES
C
C      FIRST CHECK IF CONSTANT HEAD NODES ARE THE FIRST NODES NUMBERED
C

```

```

MAN3310
MAN3320
MAN3330
MAN3340
MAN3350
MAN3360
MAN3370
MAN3380
MAN3390
MAN3400
MAN3410
MAN3420
MAN3430
MAN3440
MAN3450
MAN3460
MAN3470
MAN3480
MAN3490
MAN3500
MAN3520-
CHK 010
CHK 020
CHK 030
CHK 040
CHK 050
CHK 060
CHK 070
CHK 080
CHK 090
CHK 100
CHK 110
CHK 120

```

	DO 10 I=1,NCH	CHK 130
	NCK=NSCON(I)+NCK	CHK 140
10	CONTINUE	CHK 150
	IF(NCK.EQ.NCH) GO TO 30	CHK 160
	IERR=1	CHK 170
	WRITE(56,20) NCH,NCK	CHK 180
20	FORMAT(1H1,20H*** PROGRAM EXPECTED,15,39H CONSTANT HEAD NODES BUT	CHK 190
	1ONLY THE FIRST,15,28H NODES WERE FLAGGED AS SUCH)	CHK 200
C		CHK 210
C	THEN CHECK THE TOTAL NUMBER OF CONSTANT HEAD FLAGS	CHK 220
C		CHK 230
30	NCK=0	CHK 240
	DO 40 I=1,NN	CHK 250
	NCK=NSCON(I)+NCK	CHK 260
40	CONTINUE	CHK 270
	IF(NCK.EQ.NCH) GO TO 60	CHK 280
	IERR=1	CHK 290
	WRITE(56,50)	CHK 300
50	FORMAT(1H0,71H***TOTAL NUMBER OF CONSTANT HEAD FLAGS DOES NOT AGRECHK 310	
	1E WITH NCH(# CODED))	CHK 320
C		CHK 330
C	NEXT CHECK IS TO INSURE THAT ALL ELEMENTS ARE NUMBERED	CHK 340
C	COUNTERCLOCKWISE	CHK 350
C		CHK 360
60	DO 100 K=1,NE	CHK 370
	L=NG(K,1)	CHK 380
	M=NG(K,2)	CHK 390
	N=NG(K,3)	CHK 400
	A=(RE(L)-RE(N))*ZE(M)+(RE(M)-RE(L))*ZE(N)+(RE(N)-RE(M))*ZE(L)	CHK 410
	IF(A.LT.0.) GO TO 100	CHK 420
	IERR=1	CHK 430
	WRITE(56,70) K	CHK 440
70	FORMAT(1H0,17H***EITHER ELEMENT,15,23H IS NUMBERED CLOCKWISE,/,11CHK 450	
	1X,92HOR THE VERTICAL COORDINATES ARE NOT POSITIVE DOWNWARD STARTINCHK 460	
	2G WITH ZERO AT THE TOP BOUNDARY)	CHK 470
100	CONTINUE	CHK 480
	RETURN	CHK 490
	END	CHK 500-
	SUBROUTINE MLTBM(A,B,R,MM,M)	MLT 010
	DIMENSION A(MM,M),B(MM),R(MM)	MLT 020
C		MLT 030
C	MULT. OF A BANDED MATRIX(ORIGINALLY MM*MM)	MLT 040
C	WITH A VECTOR MATRIX	MLT 050
C	(COMPACTED BANDED MATRIX OF M*MM AND VECTOR OF MM*1)	MLT 060
C		MLT 070
	DO 1 I=1,MM	MLT 080
	R(I)=0.	MLT 090
	DO 2 J=1,M	MLT 100
	K=J+I-(M+1)/2	MLT 110
	IF(K.LT.1) GO TO 2	MLT 120
	IF(K.GT.MM) GO TO 2	MLT 130
	R(I)=A(I,J)*B(K)+R(I)	MLT 140
2	CONTINUE	MLT 150
1	CONTINUE	MLT 160

RETURN	MLT 170
END	MLT 180-
SUBROUTINE SOLVE(KKK,B,R,NEQ,IHALFB,NDIM,MDIM)	SOL 10
*****	SOL 20
C	SOL 30
C ASYMMETRIC BAND MATRIX EQUATION SOLVER	SOL 40
C ORIGINALLY PROGRAMED BY JAMES O. DUGUID	SOL 50
C	SOL 60
C KKK=1 TRIANGULARIZES THE BAND MATRIX B	SOL 70
C KKK=2 SOLVES FOR RIGHT SIDE R, SOLUTION RETURNS IN R	SOL 80
C	SOL 90
DIMENSION B(NDIM,MDIM), R(NDIM)	SOL 100
NRS=NEQ-1	SOL 110
IHBP=IHALFB+1	SOL 120
IF (KKK.EQ.2) GO TO 30	SOL 130
C	SOL 140
C TRIANGULARIZE MATRIX A USING DOOLITTLE METHOD	SOL 150
C	SOL 160
DO 20 K=1,NRS	SOL 170
PIVOT=B(K,IHBP)	SOL 180
KK=K+1	SOL 190
KC=IHBP	SOL 200
DO 10 I=KK,NEQ	SOL 210
KC=KC-1	SOL 220
IF (KC.LE.0) GO TO 20	SOL 230
C=-B(I,KC)/PIVOT	SOL 240
B(I,KC)=C	SOL 250
KI=KC+1	SOL 260
LIM=KC+IHALFB	SOL 270
DO 10 J=KI,LIM	SOL 280
JC=IHBP+J-KC	SOL 290
10 B(I,J)=B(I,J)+C*B(K,JC)	SOL 300
20 CONTINUE	SOL 310
GO TO 100	SOL 320
C	SOL 330
C MODIFY LOAD VECTOR R	SOL 340
C	SOL 350
30 NN=NEQ+1	SOL 360
IBAND=2*IHALFB+1	SOL 370
DO 70 I=2,NEQ	SOL 380
JC=IHBP-I+1	SOL 390
JI=1	SOL 400
IF (JC.LE.0) GO TO 40	SOL 410
GO TO 50	SOL 420
40 JC=1	SOL 430
JI=I-IHBP+1	SOL 440
50 SUM=0.0	SOL 450
DO 60 J=JC,IHALFB	SOL 460
SUM=SUM+B(I,J)*R(JI)	SOL 470
60 JI=JI+1	SOL 480
70 R(I)=R(I)+SUM	SOL 490
C	SOL 500
C BACK SOLUTION	SOL 510
C	SOL 520

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R(NEQ)=R(NEQ)/B(NEQ,IHBP) SOL 530
DO 90 IBACK=2,NEQ SOL 540
I=NN-IBACK SOL 550
JP=I SOL 560
KR=IHBP+1 SOL 570
MR=MINO(IBAND,IHALFB+IBACK) SOL 580
SUM=0.0 SOL 590
DO 80 J=KR,MR SOL 600
JP=JP+1 SOL 610
80 SUM=SUM+B(I,J)*R(JP) SOL 620
90 R(I)=(R(I)-SUM)/B(I,IHBP) SOL 630
100 RETURN SOL 640
END SOL 650-

C
C*****
C SUBROUTINE PTPLOT WRITTEN BY A. PUCCI AND D. POPE 1/2/87
C USGS WEST TRENTON ,NEW JERSEY
C (609) 771-3900
C*****
SUBROUTINE PTPLOT(NPLT,NTS)
C*****
C PROGRAM TO PLOT PUMPING TEST DATA. FROM RADFLOW MODEL OUTPUT AT EACH
C OBSERVATION WELL, AND FROM THE OBSERVATION WELL DATA AT EACH SITE.
C*****
C GLOSSARY
C
C GXMAX,GYMAX,GYMIN,GXMIN = USER SUPPLIED LIMITS TO LOG-LOG GRAPH OF ****
C WATER LEVEL CHANGES AGAINST REDUCED TIME ****
C*****
CHARACTER INPUT*10,OUTPUT*10,TITLE1*50,TITLE2*50,ANS*1
REAL GXMAX,GXMIN,GYMAX,GYMIN,XAXIS,YAXIS
REAL POB(5,100),TOB(5,100),EPSI(5)
INTEGER CHOICE

C GDIU INITIALIZE VARIABLES FOR GDIU DEVICE CALLS
CHARACTER*1 OPT /* DEVICE OPTION CODE
CHARACTER*50 DES /* DEVICE DESCRIPTION
CHARACTER*32 PALET /* DEVICE PALET
LOGICAL FLAGS(3) /* DEVICE OPTION FLAGS
C GDIU /* 1-PLOT FILE REQUIRED
C GDIU /* 2-DEVICE IS NOT A GRAPHIC TERMINAL
C GDIU /* 3-DEVICE HAS GRAPHIC INPUT
REAL SIZE(2) /* OPTIONAL MAX WIDTH AND HEIGHT OF PLOT
CHARACTER*128 PLTFIL /* NAME OF PLOT FILE, IF NEEDED
INTEGER LUPLLOT /* LOGICAL UNIT TO OPEN PLOT FILE ON
INTEGER NDEV /* DEVICE NUMBERS
CHARACTER*8 COLOR /* PLOT COLOR
COMMON /PT/ POB,TOB
COMMON /EPS/ EPSI
C*****
C** EACH OUTPUTFILE WILL BE SEPARATE FOR AN OBSERVATION WELL
C** WITH THE TEST DATA
C*****
C
C*****

```



```

C      TERMINAL PROMPTS TO USER FOR OUTPUT CONTROL
C*****
C**      OUTPUT FILE NAMES FOR EACH OBSERVATION WELL PLOT MUST BE UNIQUE
C
      PRINT *, 'BEGIN PLOTTING SECTION'
      PRINT *, '
      PRINT *, 'ENTER TITLE FIRST LINE'
      PRINT *, 'FORMAT  ''title words$'''
      READ(1,*) TITLE1
      PRINT *, 'ENTER TITLE SECOND LINE'
      PRINT *, 'FORMAT  '' second title$'''
      READ(1,*) TITLE2
      WRITE(1,*) ' THE NEXT FOUR INPUTS: XMAX,XMIN,YMAX,YMIN, REFER'
      WRITE(1,*) ' TO THE LOG CYCLES THAT ARE CHOSEN FOR PLOTTING '
      WRITE(1,*) ' DATA AND CALCULATED DRAWDOWNS AT THE OBSERVATION'
      WRITE(1,*) ' WELLS AS TYPE CURVES, USING LOG-LOG PLOTS.'
      WRITE(1,*) ' USE 5 LOG CYCLES FOR X-AXIS, 3 FOR Y AXIS.'
      WRITE(1,*) ' I.E. MAX X =0., MIN X=-5., MAX Y= 1., MIN Y=-2.'
      PRINT *, 'MAX-X VALUE ='
      READ(1,*) GXMAX
      PRINT *, 'MIN -X VALUE ='
      READ(1,*) GXMIN
      PRINT *, 'MAX Y VALUE ='
      READ(1,*) GYMAX
      PRINT *, 'MIN Y VALUE='
      READ(1,*) GYMIN
      PRINT *, 'NAME THE INPUT FILE'
      READ '(A)', INPUT
C*****
C      OPEN OBSERVATION-WELL DATA FILE
C*****
      OPEN (61, FILE=INPUT, STATUS='OLD')
      PRINT *, 'TYPE OF DRAWDOWN DATA?(1=DRAWDOWN,2=WATER LEVEL)'
      READ (1,*) CHOICE2
C*****
C      SET CONTROL COUNTER FOR EPSILON SUBROUTINE ,SO THAT THE EPSILON
C      STATISTIC IS CALCULATED ONLY ONCE.
C*****
      NEP=0
7      NEP=NEP+1
8      NDEV = 0
      LUPLT = 13
C**      SUBROUTINE TO QUERY USER FOR DEVICE
      CALL G_QRDV(NDEV)
C
C**      SUBROUTINE RETURNS ATTRIBUTES FOR SELECTED DEVICE
      CALL G_DVDF(OPT,DES,PALET,FLAGS,SIZE,-NDEV,IRTN)
      IF (IRTN .NE. NDEV) GO TO 8
C
C      SET FLAG SPECIFYING THAT A ZETA PLOT HAS BEEN PRODUCED
      IF(FLAGS(1)) THEN
        NOZETA = 1
        PRINT *, 'TYPE IN THE NAME OF THE OUTPUT FILE'
        READ '(A)', OUTPUT

```

```

        OPEN(LUPLT,FILE=OUTPUT,STATUS='NEW')
    ELSE
        NOZETA = 0
    ENDIF
C** SUBROUTINE TO INITIALIZE SELECTED DEVICE    **
    CALL G_INIT(NDEV,1,1,LUPLT,IERR)
    IF(IERR.NE.0) STOP 'ERROR TRYING TO INITIALIZE GRAPHIC DEVICE'
C** SUBROUTINE TO PUT TERMINAL IN GRAPHIC MODE    **
    CALL G_GRMO(NDEV,1,1,LUPLT,IERR)
    IF(IERR.NE.0) STOP 'ERROR TRYING TO GO TO GRAPHIC MODE'
C
C    BASIC DISSPLA GRAPH SETUP
    CALL PAGE(11.5,9.5)
    CALL AREA2D(9.0625,5.5)
    CALL HEADIN( TITLE1,100,1.4,2 )
    CALL HEADIN( TITLE2,100,1.2,2 )
    CALL XNAME('LOG T/R**2$',100)
    CALL YNAME('LOG S$',100)
10    CALL GRAF(GXMIN,1.,GXMAX,GYMIN,1.,GYMAX)
C*****
C**    CALL DATA-PLOTTING SUBROUTINE
C*****
    CALL PUMPLT(61,NPLT,NTS,CHOICE2,N)
    CALL ENDPL(0)
C** RETURN SCREEN TO TEXT MODE
    CALL G_TXMO(NDEV,1,1,LUPLT,IERR)
C** GDIU CALL WHICH IS THE EQUIVALENT OF THE DISSPLAY DONEPL CALL
    CALL G_DNPL(NDEV,1,1,LUPLT,IERR)
C*****
C    CALL SUBROUTINE EPSILON IF THIS IS THE FIRST PLOT OF THIS DATA
C*****
    IF (NEP .EQ. 1) THEN
        CALL EPSILON(NPLT,N,NTS)
        WRITE(1,*) 'EPSI= ',EPSI(NPLT)
    ENDIF
C*****
C    GIVES OPTION TO MAKE A ZETA PLOT IF A PLOT TO THE TERMINAL WAS
C    PRODUCED FIRST
C*****
    IF (NOZETA .EQ. 1) GO TO 40
    WRITE(1,*) 'DO YOU WANT ANOTHER PLOT? (Y OR N)'
    READ(1,20) ANS
20    FORMAT(A1)
    IF (ANS .EQ. 'N') GO TO 40
    CLOSE (13)
    REWIND (61)
    GO TO 7
40    CLOSE (61)
    RETURN
END
C
C
C*****
SUBROUTINE PUMPLT(F,NPLT,NTS,CHOICE2,N)

```

```

C*****
C
C*****
C**          GLOSSARY
C**
C**    XT,YT = LOGARITHMS OF OBSERVED REDUCED TIME AND RESIDUAL WATER
C**          LEVELS FOR EACH OBSERVATION WELL
C**    XPT,YPT = LOGARITHMS OF SIMULATED REDUCED TIME AND RESIDUAL WATER
C**          LEVELS FOR EACH OBSERVATION WELL
C**    N = NUMBER OF WATER LEVEL OVSRVATIONS
C**    R = DISTANCE OF OBSERVATION WELLS FROM PUMPING WELL
C**    RE = REFERENCE ELEVATION FOR WATER LEVEL ELEMENTS (0 IS DUMMY
C**          VALUE FOR DATA WITH RESIDUAL WATER LEVELS
C*****
      INTEGER CHOICE2,N,F
      REAL S(100),T(100),XT(100),YT(100),R,RE
      REAL XPT(100),YPT(100)
      REAL POB(5,100),TOB(5,100)
      COMMON /PT/POB,TOB
      COMMON /TS/ T,S
C*****
C    READ ACTUAL TEST DATA FROM DATA FILE
C*****
      READ(F,10) N,R,RE
10    FORMAT(1X,I3,1X,F5.0,1X,F5.1)
      WRITE(1,10) N,R,RE
      DO 20 I=1,N
          READ(F,15) T(I),S(I)
C      WRITE(1,15)T(I),S(I)
15    FORMAT(F10.0,F10.3)
20    CONTINUE
C*****
C    WHAT KIND OF DRAWDOWN?
C*****
      TP=0.0
      IF (CHOICE2.EQ.1) GO TO 50
      TP=RE
50    DO 105 J=1,N
          S(J)=S(J)-TP
          XT(J)=LOG10(T(J)/(R*R))
105    YT(J)=LOG10(S(J))
C*****
C    PREPARE MODEL DATA FOR PLOTTING
C*****
      DO 106 J=1,NTS
          XPT(J)=LOG10(TOB(NPLT,J)/(R*R))
106    YPT(J)=LOG10(POB(NPLT,J))
C*****
C    PLOT OBSERVED TEST DATA
C*****
      CALL MARKER(16)
      CALL CURVE(XT,YT,N,-1)
C*****
C    PLOT MODEL OUTPUT DATA

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C*****
  CALL MARKER(2)
  CALL CURVE(XPT,YPT,NTS,+1)
  RETURN
  END
C
C
C*****
  SUBROUTINE EPSILON(NPLT,N,NTS)
C
  REAL POB(5,100),TOB(5,100),T(100),S(100),EPSI(5)
  COMMON /PT/POB,TOB
  COMMON /TS/T,S
  COMMON /EPS/ EPSI
C*****
C 'NPLT' IS THE OBSERVATION WELL BEING PLOTTED
C 'N' IS THE NUMBER OF DATA POINTS AT EACH OBSERVATION WELL
C 'NTS' IS THE NUMBER OF CALCULATION POINTS FROM RADFLOW
C THE FIRST DATA POINT SHOULD BE AFTER THE FIRST CALCULATED POINT
C*****
  DO 10 K=1,N
    DO 15 J=1,NTS
      TOBJ=TOB(NPLT,J)
      TK=T(K)
      TEST=TOBJ-TK
      IF(TEST.GE.0.) THEN
        GO TO 11
      END IF
15    CONTINUE
      IF (TOB(NPLT,J) .LT. T(K)) RETURN
C*****
C  INTERPOLATE SIMULATED RESIDUAL WATER LEVELS TO SAME TIME AS OBSERVED
C  WATER LEVELS FOR COMPARISON
C*****
11    IF (J .EQ. 1) GO TO 10
      T1=TK-TOB(NPLT,J-1)
      T2=TOBJ-TOB(NPLT,J-1)
      TT=T1/T2
      HIP=POB(NPLT,J)-POB(NPLT,J-1)
      HIP=HIP*TT + POB(NPLT,J-1)
      EPSI(NPLT)=EPSI(NPLT)+(HIP - S(K))*2/S(K)**2
10    CONTINUE
  RETURN
  END

```