

DEPARTMENT OF THE INTERIOR
U.S. GEOLOGICAL SURVEY

RESULTS OF A GRAVITY SURVEY
OF
MCCARTHY'S MARSH,
SEWARD PENINSULA, ALASKA

by

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ABSTRACT

A gravity survey of McCarthy's Marsh (sometimes referred to as the Fish River Flats) was completed during August 1977 and included 80 measurements. The resulting contoured data indicate a small sedimentary basin localized in the northeastern corner of the topographic depression which forms the marsh. Faults probably border both the northern and eastern edges of the structural basin, which was probably filled by sediments eroded from the adjacent mountains. These mountains include plutons rich in radioactive minerals, which may have been locally concentrated in the sedimentary rocks within the basin; and a potentially commercial uranium deposit has now been discovered in another valley on the opposite side of the Darby Mountains. Geophysical modeling suggests a minimal sedimentary thickness of about 1 km and possibly up to 2 or even 3 km depending on the density of the sediments filling the basin. Geomorphic evidence indicates recent or active faulting at one basin boundary and might thus suggest a young age, low sediment density, and small total thickness. However, coal specimens collected near the edge of the basin may be Tertiary in age and thus suggest an older basin age, probably higher sediment density, and higher total thickness.

INTRODUCTION

McCarthy's Marsh is a tundra and lake covered topographic depression bounded by the Bendeleben Mountains on the north, the Darby Mountains on the east, and a chain of hills dominated by Mt. Wick (450 m elevation) on the southwest. The topographic relief within the depression is small and ranges from about 100 m at the northwest corner to less than 30 m. The depression is drained to the southwest by the Fish River. The abundant lakes and marshlands geomorphically suggest a continuing process of gradual subsidence combined with sedimentation from the surrounding mountain ranges. Geomorphic studies of the Bendeleben fault (Hopkins, 1963) along the northern edge of the topographic basin suggest recent or active subsidence of the lowland. In a 1967 and 1968 gravity reconnaissance of the Seward Peninsula (Barnes, 1971), a single measurement near the north-central part of the McCarthy's Marsh showed a Bouguer anomaly more than 30 mGal lower than the anomalies measured in the adjacent hills and mountains. The anomaly was interpreted as a small structural basin filled with Cenozoic sediments or sedimentary rocks. In the initial contouring and in later contouring for the reconnaissance gravity map of Alaska (Barnes, 1977), the structural basin was assumed to have the approximate area and shape of the present topographic basin, although variation of the gravity and probable basin depth within the area was recognized. The basin was considered too small to produce significant petroleum resources, and thus received little study.

Recently, Miller and Bunker (1976) studied the uranium and thorium contents of some of the plutons in the nearby mountains and found concentrations that ranged up to 58.6 ppm in the Darby pluton. The probability that some of the sediments underlying McCarthy's Marsh had been derived from the weathering of these plutons, and the possibility of local concentration of radioactive minerals suggested the desirability of drilling some exploratory holes. A gravity survey was thus planned as an initial step towards determining the configuration of the basin and locating a drilling site. Most of this report was prepared as a Technical Letter in 1977 as preparation for the proposed drilling.

Following the gravity survey, a potentially commercial uranium deposit of at least 1 million pounds U_3O_8 (Dickinson and others, 1987) was found south of Death Valley on the opposite, or eastern side, of the Darby Mountains. This deposit occurs in early Tertiary sedimentary rocks, in which coal or other carbonaceous material produced a reducing environment for uranium-bearing ground water moving downslope from the mountains. The coal contains anomalously high amounts of tungsten (Stricker and others, in press, 1988) and the Tertiary rocks are also rich in siderite (Dickinson, 1988). Coal has also been found on the flanks of McCarthy's Marsh (T.M. Miller, oral communication, 1977) where its presence suggests both a Tertiary age and possible reducing environment for some of the rocks underlying that marsh.

GRAVITY MEASUREMENTS

More than 80 gravity measurements (including two outside the mapped area) were obtained during August 1977 using a LaCoste and Romberg geodetic gravimeter. A large jet helicopter provided transportation from the operating base established at the settlement of Council a few miles west of the mapped area. The gravity base station at Council was located on the ground approximately 1 m northwest of the northwest corner of the Trading Post, where

the established gravity is 982,272.49 mGal on the U.S. Geological Survey Alaskan gravity base network (Barnes, 1968) converted to the International Gravity Standardization net 1971, IGSN-71 (Morelli and others, 1974). The data were reduced using the ellipsoid of the 1967 Geodetic Reference System (International Association of Geodesy, 1971) and include the second order terms in the free-air correction. Gravity anomalies released on the original reconnaissance map of the Seward Peninsula (Barnes, 1971) were calculated with the older datum and 1931 ellipsoid, but the more recent Seward Peninsula map (Barnes and Hudson, 1977) used the newer datum and included the data in this report.

Altimetry was used for the elevation control, and the 100-ft elevation of the Council base was established by an average of ties to spot elevations in the survey area. There has been no leveling and minimal vertical angle-control within the survey area, but the base elevation is consistent with elevations estimated by the Federal Aviation Agency for the Council airstrip. Estimates of altimetry accuracy for similar surveys have been close to ± 5 meters, and this limitation suggests that the Bouguer anomalies have an accuracy of about ± 1 mGal. River gradients were also used as supplementary elevation control. The reduction density is a standard 2.67 g/cm^3 , which is fairly typical of the Paleozoic metamorphic rocks and younger plutons that crop out in the adjacent mountains. Tabulated data for the gravity measurements are given in the appendix, the format and source codes of which were discussed by Barnes (1972). The data were not corrected for effects of nearby terrain, which except on the margin of the basin are small in comparison with the possible errors caused by altimetry.

Results

The gravity data are summarized in the contour map of plate 1, which shows a triangular shaped low in the northeast corner of the topographic basin. This low probably represents the deepest part of the structural basin. The closely-spaced linear contours on the north and east sides of the gravity low are interpreted to be caused by high-angle faults. The gradient on the north side is approximately centered on the scarp trace of the Bendeleben fault. Geologic mapping (Miller and others, 1972, and Till and others, 1986) south of the gravity survey suggested another fault on trend with the belt of parallel contours on the east side of the basin, although the fault trace was not actually located.

Plate 2 shows aeromagnetic contours from the same area which are taken from surveys at 1000 ft elevation and with 1 mile flight line separation flown by Lockwood, Kessler, and Bartlett, Incorporated for the Department of Natural Resources, Alaska Division of Geological Survey (1971). Closely spaced magnetic contours on the edge of the gravity low are interpreted as resulting from volcanic flows within the sedimentary section. Such flows crop out on the south side of the Bendeleben fault. The remaining magnetic contours are consistent with a thick sedimentary section.

The calculated depth of the basin depends on the density of the material within it, which is probably controlled in part by the sedimentary history of the structure. Figure 1 is a computer plot of profile AB (located on plate 1), and of one possible basin cross section calculated by a simple two-dimensional iterative computer program using the method of Bott (1960) on a

profile from which a regional gradient of 15 mGal in 40 km has been subtracted. The vertical scale is enlarged eight times, exaggerating the V-like result of the calculation, which is only a preliminary approximation for a profile so close to the corner of the basin. The sediment density used in the model was 1.67 g/cm^3 (a density contrast of 1.00 g/cm^3), which is close to a minimum for uncompacted water-saturated sediments, so the calculated depth of more than 1 km might be considered a minimum depth. However, if the basin was formed and filled primarily in Quaternary time by clay and silt sediments the thickness of permafrost and ice lenses could be large, and the depth might be much smaller. However, the presence of volcanics within the section tends to diminish the possibility of a thick ice section. Figure 2 is another model of the same profile using a sediment density of 2.17 g/cc (density contrast 0.50 g/cc). Such a density would be more typical of mid-Tertiary sedimentary rocks, and the depth (2.5 km) might be considered more reasonable for a structure this large. Allowance for the inaccuracy of the two-dimensional model would also tend to increase the calculated depth.

Figure 5 is another profile which is located closer to the center of the basin, but which is supported by fewer gravity measurements. Along this line the two-dimensional gravity model is probably more valid, and the 2.00 g/cc (0.67 g/cc density contrast) sediment density of the model may be a more probable average. This profile suggests that the most probable depth is slightly less than 1.4 km, which would be increased if older sediments were assumed or if allowance were made for inaccuracies in the modeling technique.

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STAT. NOS.	LOC.	MT- REF	ELEV ELEV	ELEV ELEV	OBSV TIME	OBSV MILLIGALS	GRAV TYPE	GRAV TYPE	FAA MGALS	SRA 2.20	ANOM ACC.	SRA 2.67	STAT NUMH	OTHER ELEV	SRA ELEV.			
MAIN_AUX.	LATITUDE	LONGITUDE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE	TYPE		
BL31	61 10.54	149 50.87	A	0	0	88	A	540	981906.77	A	-93.2	-95.6	6	-96.2	6	BL31	R	0.0000
NOMF	64 30.55	165 26.12	A	0	16	A	A	755	982260.06	A	7.8	7.4	6	7.3	6	NOMF	R	0.0000
NOMF	64 30.55	165 26.12	A	0	16	A	A	755	982259.82	A	7.6	7.1	6	7.0	6	NOMF	R	0.0000
NOMF	64 30.55	165 26.12	A	0	16	C	C	1317	982259.82	A	7.6	7.1	6	7.0	6	NOMF	R	0.0000
COUN	64 53.60	163 39.92	A	0	100	H	B	1529	982272.47	B	1.2	-1.6	7	-2.2	7	COUN	100	R -2.2
COUN	64 53.60	163 39.92	A	0	100	H	B	1529	982272.44	B	1.2	-1.7	7	-2.3	7	COUN	100	R -2.3
MM01	64 56.04	163 28.25	A	0	1501	T	C	1555	982188.33	C	46.0	3.8	7	-5.2	7	MM01	1440	G -9.0
MM02	64 59.02	163 26.80	A	0	869	T	C	1605	982229.79	C	24.5	0.1	7	-5.1	7	MM02	840	M -6.9
MM03	65 3.70	163 29.15	A	0	473	T	C	1615	982247.77	C	-0.1	-13.4	7	-16.3	7	MM03	455	M -17.4
MM04	65 5.98	163 28.85	A	0	333	T	C	1625	982246.56	C	-17.1	-26.5	7	-28.5	7	MM04	309	J -30.0
MM05	65 4.35	163 20.52	A	0	344	T	C	1634	982239.12	C	-21.6	-31.3	7	-33.4	7	MM05	319	M -34.9
MM06	65 8.21	163 15.42	A	0	224	T	C	1643	982235.45	C	-41.1	-47.4	7	-48.7	7	MM06	225	J -48.7
MM07	65 13.01	163 11.62	A	0	446	T	C	1654	982244.07	C	-17.2	-29.7	7	-32.4	7	MM07	470	M -30.9
MM08	65 10.52	163 7.72	A	0	361	T	C	1705	982248.92	C	-17.4	-27.5	7	-29.7	7	MM08	320	M -32.2
MM09	65 7.68	163 6.15	A	0	182	T	C	1712	982228.61	C	-51.3	-56.4	7	-57.5	7	MM09	174	M -58.0
MM10	65 9.30	162 56.62	A	0	20	380	T	1722	982232.82	C	-30.3	-41.0	7	-43.3	7	MM10	355	M -44.8
MM11	65 10.28	162 43.00	A	0	-3	1192	T	1735	982196.42	C	8.5	-25.0	7	-32.2	7	MM11	1172	G -33.4
MM12	65 7.40	162 48.60	A	0	210	T	C	1744	982249.11	C	-27.8	-33.7	7	-35.0	7	MM12	204	J -35.4
MM13	65 4.82	162 53.45	A	0	110	T	C	1753	982231.77	C	-51.6	-54.7	7	-55.3	7	MM13	105	J -55.6
MM14	65 3.68	162 58.15	A	0	1	88	T	1801	982229.10	C	-55.0	-57.5	7	-58.0	7	MM14	84	J -58.3
MM15	65 3.25	163 5.95	A	0	106	T	C	-41.9	982239.96	C	-13.1	-15.1	7	-15.5	7	MM15	115	J -45.0
MM16	64 59.50	163 5.92	A	0	71	T	C	1819	982267.76	C	-13.1	-15.1	7	-15.5	7	MM16	58	J -1.3
MM17	64 56.08	163 9.25	A	0	56	T	C	-5.2	982273.04	C	-3.9	-6.8	7	-7.2	7	MM17	46	J -7.8
MM18	64 53.90	163 13.65	A	0	42	T	C	-3.9	982273.13	C	-3.9	-5.1	7	-5.3	7	MM18	38	J -5.6
COUN	64 53.60	163 39.92	A	0	100	H	B	1856	982272.47	B	1.2	-1.6	6	-2.2	6	COUN		

DATA SUMMARY

BANGES OF	LATITUDE	LONGITUDE	ELEVATION	OBSV GRAY	FAA	SRA=2.67
MINIMUM:	61 10.54	149 50.87	16	981906.77	-93.2	-96.2
MAXIMUM:	65 13.01	165 26.12	1501	982273.13	46.0	7.3

NUMBER OF STATIONS: 25

STAT. NOS.	LOC.		HT- FEET	ELEV FEET	FLEV FEET	MILLIGALS	ORSV TIME	ORSV GRAV	ORSV TYPE	FAA MGALS	SRA ACC.	ANOM SBA	STAT NUMB	OTHER ELEV	SBA TYPE				
	MAIN	AUX																	
COUN	64	53.60	163	39.92	A	0	U	100	H	0	849	982727.47	H	0	100	R	-2.2		
MM19	64	54.76	163	11.88	A	0	0	53	T	0	941	982773.36	C	0	MM19	0	42	J	-6.2
MM20	64	56.72	163	8.70	A	0	0	62	T	0	949	982727.76	C	0	MM20	0	48	J	-8.7
MM21	64	58.08	163	6.50	A	0	0	71	T	0	956	982727.33	C	0	MM21	0	52	J	-10.4
MM22	64	59.68	163	0.80	A	0	0	131	T	0	1004	982763.96	C	0	MM22	0	130	M	-14.9
MM23	64	54.03	162	57.80	A	0	0	120	T	0	1011	98259.08	C	0	MM23	0	126	M	-20.4
MM24	64	57.17	162	52.15	A	0	0	171	T	0	1029	98250.32	C	0	MM24	0	155	M	-25.2
MM25	64	54.73	162	47.53	A	0	0	254	T	0	1020	98254.22	C	0	MM25	0	235	M	-13.7
MM26	64	55.68	162	41.35	A	0	0	525	T	0	1040	98231.85	C	0	MM26	0	500	M	-21.3
MM27	64	58.69	162	42.80	A	0	0	313	T	0	1048	98227.80	C	0	MM27	0	295	M	-41.1
MM28	65	0.30	162	39.40	A	0	0	578	T	0	1057	98234.86	C	0	MM28	0	550	M	-20.7
MM29	65	2.15	162	41.20	A	0	0	494	T	0	1104	98239.85	C	0	MM29	0	520	M	-19.6
MM30	65	2.24	162	49.30	A	0	0	154	T	0	1145	98228.95	C	0	MM30	0	185	M	-50.7
MM31	65	2.74	162	58.25	A	0	0	90	T	0	1155	98232.53	C	0	MM31	0	80	J	-54.0
MM32	65	1.65	163	1.75	A	0	0	85	T	0	1201	98247.46	C	0	MM32	0	72	J	-38.3
MM33	65	2.52	163	3.55	A	0	0	96	T	0	1207	982241.57	C	0	MM33	0	99	J	-43.5
MM34	65	3.66	163	9.05	A	0	0	125	T	0	1214	98241.92	C	0	MM34	0	125	J	-42.9
MM35	65	5.29	163	10.70	A	0	0	156	T	0	1220	98236.65	C	0	MM35	0	156	J	-48.2
MM36	65	6.40	163	8.65	A	0	0	243	T	0	1227	98221.80	C	0	MM36	0	235	M	-59.7
MM37	65	7.28	163	11.60	A	0	0	196	T	0	1234	98226.24	C	0	MM37	0	198	J	-58.4
MM38	65	6.08	163	19.88	A	0	0	271	T	0	1242	98243.72	C	0	MM38	0	270	M	-37.6
MM39	65	4.47	163	24.80	A	0	0	297	T	0	1249	98247.49	C	0	MM39	0	266	J	-2.6
COUN	64	53.60	163	39.92	A	0	0	100	R	0	1304	98272.47	B	0	COUN	0	100	R	-2.2
COUN	64	53.60	163	39.92	A	0	0	100	R	0	1401	98272.47	B	0	COUN	0	101	R	-2.2
MM40	64	55.32	163	10.95	A	0	0	52	T	0	1431	98273.13	C	0	MM40	0	44	J	-6.9
MM41	64	57.32	163	7.22	A	0	0	61	T	0	1440	98272.68	C	0	MM41	0	50	J	-9.3
MM42	64	56.38	162	57.50	A	0	0	146	T	0	1450	98264.62	C	0	MM42	0	147	M	-10.5
MM43	64	57.83	162	53.20	A	0	0	152	T	0	1457	98251.43	C	0	MM43	0	145	M	-25.5
MM44	64	56.33	162	51.35	A	0	0	183	T	0	1503	98250.47	C	0	MM44	0	180	M	-22.6
MM45	64	55.44	162	49.75	A	0	0	215	T	0	1518	98255.26	C	0	MM45	0	208	M	-15.1
MM46	64	58.19	162	54.90	A	0	0	129	T	0	1524	98256.44	C	0	MM46	0	137	M	-21.4
MM47	64	56.52	162	56.52	A	0	0	119	T	0	1524	98256.92	C	0	MM47	0	130	M	-19.4
MM48	64	59.78	163	0.35	A	0	0	94	T	0	1536	98259.62	C	0	MM48	0	108	M	-21.8
MM49	65	0.85	163	2.00	A	0	0	80	T	0	1542	98253.63	C	0	MM49	0	68	J	-31.4
MM50	65	1.67	163	1.10	A	0	0	87	T	0	1542	98245.42	C	0	MM50	0	73	J	-40.3
MM51	65	2.24	163	0.20	A	0	0	86	T	0	1547	98238.38	C	0	MM51	0	76	J	-47.8
MM52	65	6.48	162	50.95	A	0	0	142	T	0	1556	98237.16	C	0	MM52	0	123	J	-51.1
MM53	65	8.24	162	48.35	A	0	0	280	T	0	1604	98245.17	C	0	MM53	0	279	J	-35.8
MM54	65	9.08	162	46.90	A	0	0	354	T	0	1610	98247.99	C	0	MM54	0	360	J	-29.1
MM55	65	8.12	162	59.88	H	0	0	176	T	0	1620	98233.02	C	0	MM55	0	165	M	-53.4
MM56	65	7.10	163	2.10	A	0	0	218	T	0	1629	98223.18	C	0	MM56	0	202	M	-61.1
MM57	65	5.43	163	11.55	A	0	0	107	T	0	1636	98226.91	C	0	MM57	0	98	J	-61.6
MM58	65	8.00	163	2.70	A	0	0	204	T	0	1645	98231.81	C	0	MM58	0	170	J	-53.2
MM59	65	4.32	163	10.30	A	0	0	152	T	0	1700	98239.65	C	0	MM59	0	209	J	-54.8
MM60	65	0.32	163	13.75	A	0	0	119	T	0	1709	98237.22	C	0	MM60	0	143	J	-44.9
MM61	64	58.53	163	5.58	A	0	0	67	T	0	1716	98270.60	C	0	MM61	0	133	J	-7.3
MM62	64	53.60	163	39.92	A	0	0	100	H	0	1746	98272.47	B	0	MM62	0	54	J	-15.6
COUN	64	53.60	163	39.92	A	0	0	100	H	0	1746	98272.47	B	0	COUN	0	100	R	-2.2

DATA SUMMARY RANGES: UEL - LATITUDE - LONGITUDE - ELEVATION - OBSV GRAY - FAA - SBA-2.67

MINIMUM: 64 53.60 162 39.40 52 982721.80 -57.4 -61.1
 MAXIMUM: 65 9.08 163 39.92 578 98273.16 1.2 -2.2

NUMBER OF STATIONS: 40

USGS GRAVITY DATA FROM: SEWARD PEN ALASKA; TRAVELER: FISHER-HIV-J PROJ CHIEF: HANNES DATUM: HANNES 1975 DATA SET: AY63
 DATE: 08/11/77 MFLEK: G192 OBSRVENS: MORTN * MAIN BASE: COUN VALUE: 98272.47 DRIFT: 0.07 OTHER BASES: NOMF

STAT. NOS.	MAIN_AVAL	LATITUDE	LONGITUDE	LUC.	MT-REF	ELEV	ELEV	MT-ELEV	MT-ELEV	OBSV TIME	GRV MLLGALS	GRAV TYPE	FAA MGALS	SRA ANDM	SRA ACC	SRA	STAT	OTHER ELEV	SBA	
						ELEV	ELEV										NUMB	ELEV	TYPE	
COUN	64	53.60	163 39.42	A	0	100	H	0	850	98272.47	H	0	1.2	-1.6	6	-2.2	COUN	100	R	-2.2
MM63	64	58.60	163 38.75	A	0	172	T	0	923	98270.85	C	0	0.6	-4.3	7	-5.3	MM63	185	M	-4.6
MM64	65	6.68	163 33.42	A	0	341	T	0	942	98247.38	C	0	-16.4	-26.0	7	-28.0	MM64	352	J	-27.4
MM65	65	7.38	163 26.12	A	0	431	T	0	950	98233.36	C	0	-22.7	-34.9	7	-37.4	MM65	425	M	-37.8
MM66	65	12.18	163 28.48	A	0	646	T	0	1000	98232.39	C	0	-9.0	-27.2	7	-31.1	MM66	650	M	-30.9
MM67	65	11.24	163 26.75	A	0	554	T	0	1007	98238.11	C	0	-11.0	-26.5	7	-29.9	MM67	560	M	-29.5
MM68	65	10.65	163 26.30	A	0	504	T	0	1012	98241.01	C	0	-12.0	-26.2	7	-29.2	MM68	490	M	-30.1
MM69	65	9.34	163 24.57	A	0	372	T	0	1019	98247.48	C	0	-16.4	-26.9	7	-29.1	MM69	358	M	-30.0
MM70	65	8.72	163 22.91	A	0	307	T	0	1025	98242.25	C	0	-27.1	-35.7	7	-37.5	MM70	315	M	-37.1
MM71	65	8.72	163 20.68	A	0	242	T	0	1032	98242.28	C	0	-33.2	-40.0	7	-41.4	MM71	258	M	-40.5
MM72	65	8.13	163 18.85	A	0	221	T	0	1039	98239.65	C	0	-37.0	-43.3	7	-44.6	MM72	235	M	-43.8
MM73	65	4.55	163 16.55	A	0	5	T	0	1047	98240.50	C	0	-30.2	-37.0	7	-38.5	MM73	253	M	-37.8
MM74	65	1.80	163 19.08	A	0	140	T	0	1055	98271.74	C	0	-5.2	-9.2	7	-10.0	MM74	158	J	-9.0
MM75	65	1.45	163 13.40	U	0	131	T	0	1105	98262.96	C	0	-14.6	-18.3	7	-19.1	MM75	141	M	-17.4
MM76	65	1.82	163 7.40	A	0	122	T	0	1115	98251.58	C	0	-27.1	-30.6	7	-31.3	MM76	141	M	-30.2
MM77	64	54.25	163 4.02	A	0	60	T	0	1123	98265.29	C	0	-16.2	-17.9	7	-18.3	MM77	75	M	-17.5
MM78	65	0.35	163 3.15	A	0	62	T	0	1130	98256.94	C	0	-25.7	-27.5	7	-27.8	MM78	66	J	-27.6
MM79	65	1.20	162 54.48	A	0	125	T	0	1141	98231.10	C	0	-46.6	-50.2	7	-50.9	MM79	140	P	-50.0
MM80	65	3.82	162 56.92	A	0	86	T	0	1152	98226.79	C	0	-57.6	-60.0	7	-60.6	MM80	120	M	-58.6
MM81	65	4.50	162 55.60	A	0	85	T	0	1200	98226.04	C	0	-57.3	-59.7	7	-60.2	MM81	120	M	-58.1
MM82	65	5.49	163 5.70	A	0	139	T	0	1211	98272.51	C	0	-56.0	-59.9	7	-60.8	MM82	150	M	-61.2
COUN	64	53.60	163 39.42	A	0	100	H	0	1249	98272.47	B	0	1.2	-1.6	6	-2.2	COUN	100	R	-2.2
COUN	64	53.60	163 39.42	A	0	100	H	0	1249	98272.47	B	0	1.2	-1.6	6	-2.2	COUN	100	R	-2.2
COUN	64	30.55	165 26.12	A	0	16	A	0	1508	98259.74	A	0	7.5	7.0	6	7.0	NOMF	100	R	-2.2
NOMF	64	30.55	165 26.12	A	0	16	A	0	1508	98259.74	A	0	7.6	7.1	6	7.0	NOMF	100	R	-2.2



Figure Captions

Figure 1. Gravity profile AB and cross section computed with a density contrast of 1.00 gm/cm^3 representing a porous-sediment density of 1.67 gm/cm^3 . Horizontal and vertical scale units in kilometers (vertical exaggeration: 8X). Small circles represent observed Bouguer gravity values in milligals; small crosses represent data calculated by the iterative program of Bott (1960).

Figure 2. Gravity profile AB and cross section computed with a density contrast of 0.50 gm/cm^3 representing a sedimentary rock density of 2.17 gm/cm^3 and basement rock density of 2.67 gm/cm^3 . Horizontal and vertical scale units in kilometers (vertical exaggeration: 8X). Small circles represent observed Bouguer gravity values in milligals; small crosses represent data calculated by the iterative program of Bott (1960).

Figure 3. Gravity profile CD and cross section computed with a density contrast of 0.67 gm/cm^3 representing primarily a sedimentary density of 2.00 and basement rock density of 2.67 gm/cm^3 . Horizontal and vertical scale units in kilometers (vertical exaggeration: 8X). Small circles represent observed Bouguer gravity values in milligals; small crosses represent data calculated by the iterative program of Bott (1960).

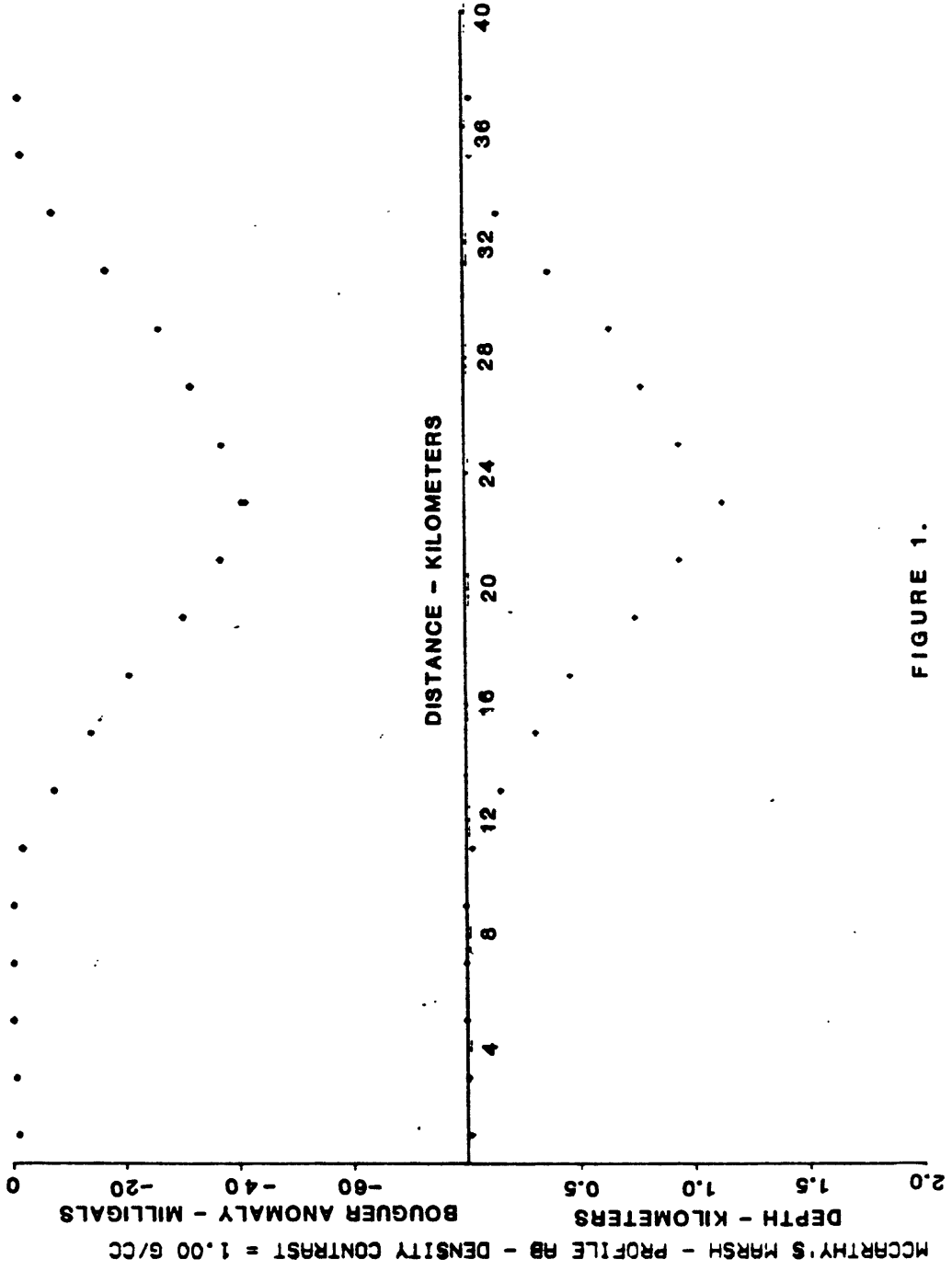


FIGURE 1.

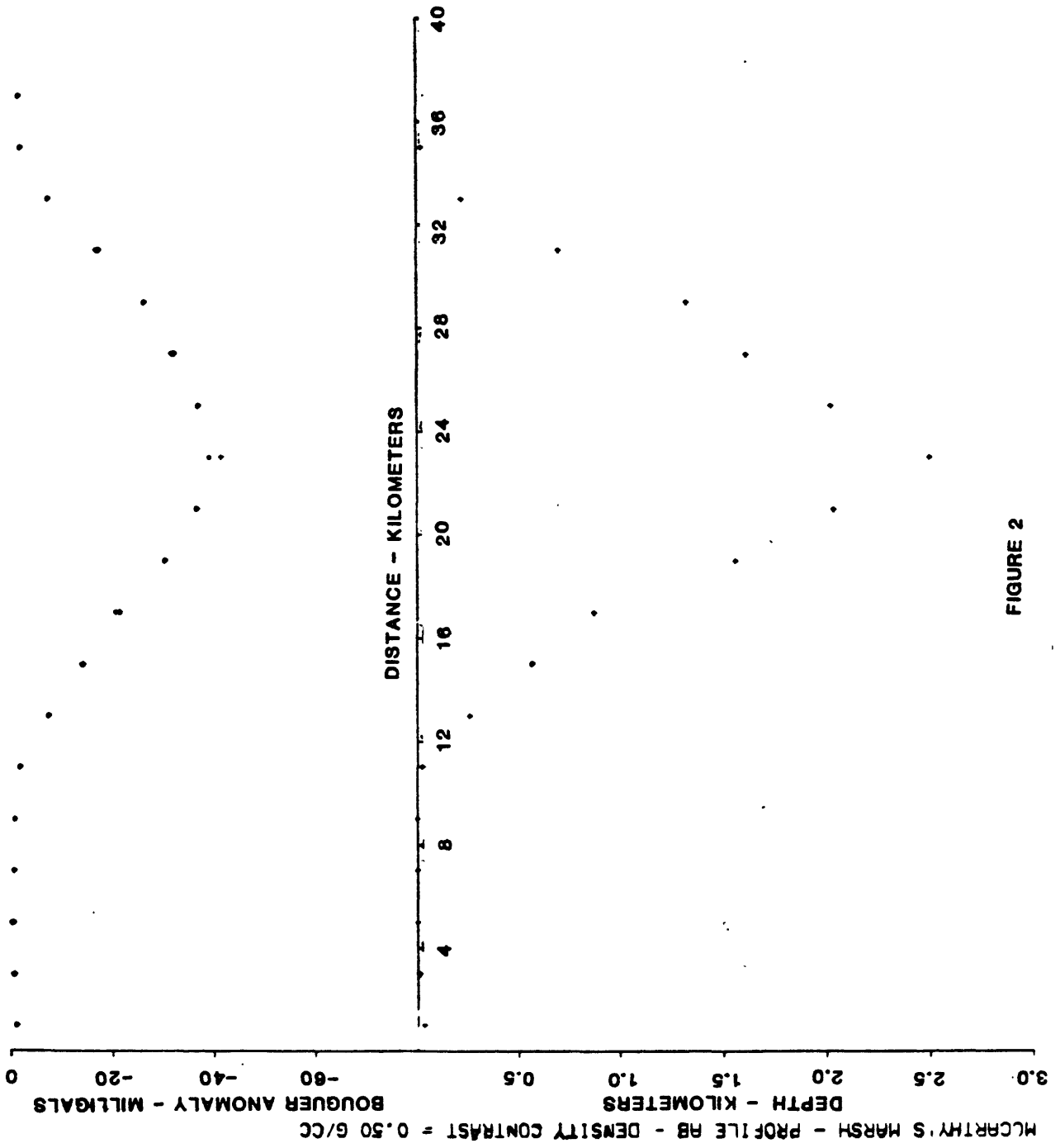


FIGURE 2

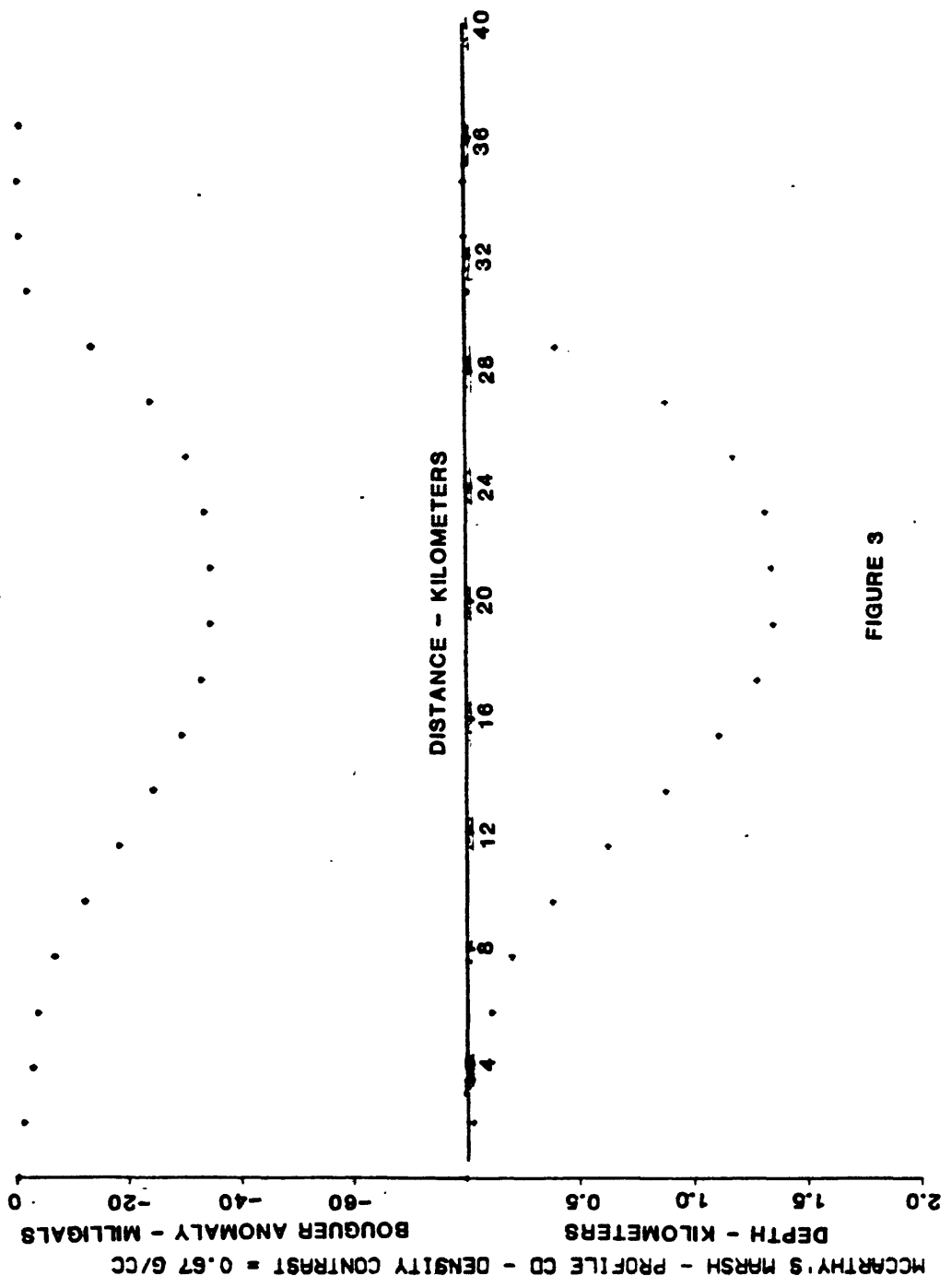


FIGURE 3