

**A COMPUTER PROGRAM (MODFLOWP) FOR ESTIMATING  
PARAMETERS OF A TRANSIENT, THREE-DIMENSIONAL,  
GROUND-WATER FLOW MODEL USING NONLINEAR REGRESSION**

by Mary C. Hill

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**MANUEL LUJAN, JR., Secretary**

**U.S. GEOLOGICAL SURVEY**

**Dallas L. Peck, Director**

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For additional information  
write to:

Regional Research Hydrologist  
U.S. Geological Survey  
Water Resources Division  
Box 25046, Mail Stop 413  
Denver Federal Center  
Denver, CO 80225-0046

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## PREFACE

This report presents a computer program for estimating parameters of ground-water flow simulations by using nonlinear regression. The program documented in this report is designed for incorporation into a modified version of the modular finite-difference ground-water flow model developed by the U.S. Geological Survey, which is also documented in this report. The performance of this computer program has been tested in models of both hypothetical and actual ground-water flow systems. Future applications, however, might reveal errors that were not detected in the test simulations. Users are requested to notify the originating office of any errors found in the report or in the computer program. Updates might occasionally be made to both the report and computer program. Users who wish to be added to the mailing list to receive notice of updates, if any, can send a request to:

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Telephone: (703) 648-5695

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## CONVERSION FACTORS

<u>Multiply</u>	<u>By</u>	<u>To Obtain</u>
cubic foot per second (ft <sup>3</sup> /s)	0.3048	cubic meter per second
foot (ft)	0.3048	meter
foot per second (ft/s)	0.3048	meter per second
inch (in.)	25.4	millimeter
mile (mi)	1.609	kilometer
square feet (ft <sup>2</sup> )	0.09290	square meters
square mile (mi <sup>2</sup> )	2.590	square kilometer



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ABSTRACT

This report documents a new version of the U.S. Geological Survey modular, three-dimensional, finite-difference, ground-water flow model (MODFLOW) which, with the new Parameter-Estimation Package that also is documented in this report, can be used to estimate parameters by nonlinear regression. The new version of MODFLOW is called MODFLOWP (pronounced MOD•FLOW•P), and functions nearly identically to MODFLOW when the Parameter-Estimation Package is not used. Parameters are estimated by minimizing a weighted least-squares objective function by the modified Gauss-Newton method or by a conjugate-direction method. Parameters used to calculate the following MODFLOW model inputs can be estimated: Transmissivity and storage coefficient of confined layers; hydraulic conductivity and specific yield of unconfined layers; vertical leakance; vertical anisotropy (used to calculate vertical leakance); horizontal anisotropy; hydraulic conductance of the River, Streamflow-Routing, General-Head Boundary, and Drain Packages; areal recharge rates; maximum evapotranspiration; pumpage rates; and the hydraulic head at constant-head boundaries. Any spatial variation in parameters can be defined by the user. Data used to estimate parameters can include existing independent estimates of parameter values, observed hydraulic heads or temporal changes in hydraulic heads, and observed gains and losses along head-dependent boundaries (such as streams). Model output includes statistics for analyzing the parameter estimates and the model; these statistics can be used to quantify the reliability of the resulting model, to suggest changes in model construction, and to compare results of models constructed in different ways.

## INTRODUCTION

### Terminology

Some of the terms used in this report are so fundamental to the discussion that they need to be defined before proceeding. In this report, the term 'parameter' refers to a quantity being estimated. Thus, typical parameters would be, for example, the hydraulic conductivity of defined areas of confined model layers 4 and 5, the recharge rate applied to a defined area of model layer 1 during specified time steps, or a value which, when multiplied by defined constants, produces the hydraulic conductance for selected cells listed in a River Package input file. The values produced by parameter estimation are estimates of these parameters.

In contrast, the term 'model input' refers to the properties required in the input files of MODFLOW, the U.S. Geological Survey (USGS) modular, three-dimensional finite-difference ground-water flow model. The input files are described by McDonald and Harbaugh (1988) and Prudic (1989). Typical model inputs are transmissivity of confined layers, hydraulic conductivity of unconfined layers, and recharge flux. Many model inputs can be calculated using parameters.

Use of the term 'model' in this report also might cause confusion. To coordinate with usage in the regression literature (for example, Fuller, 1987, p. 9), in this report the term model generally refers to the equations and assumptions used to represent a physical system. In this sense, a model includes not only the numerical representation of the physical equations, but also includes assumptions made to represent a physical system. To illustrate, consider linear models, which are used for illustrative purposes in this report. Linear models are of the form presented in equation (6). Assumptions required to create a linear model include how many parameters and independent variables to use. For nonlinear models, such as those constructed using the numerical representation of the ground-water flow equations as described for MODFLOW by McDonald and Harbaugh (1988) and Prudic (1989), typical assumptions concern the location and type of boundary conditions, the definition of parameters to be estimated, the inclusion or exclusion of physical features, and so on. Models of a physical system, therefore, can differ in one or several of the assumptions used in model construction. In general, models also can differ by being based on

different physical equations--for example, one model might only include flow through porous media, as in MODFLOW, whereas another also might represent flow through a fracture. No capacity to vary the physical equations, however, is provided in this report.

Confusion results because the numerical representation of the ground-water flow equation presented by McDonald and Harbaugh (1988) and Prudic (1989) (MODFLOW) also is called a model. To resolve any confusion, in this report all references to the numerical representation of the ground-water flow equation include citation of McDonald and Harbaugh (1988) and Prudic (1989) or reference to MODFLOW or MODFLOWP, and an effort has been made to clearly state that in other references to models, the more extensive definition discussed above is implied.

### Problem

Most numerical models of ground-water flow systems need to be calibrated--that is, the model needs to be made to match the physical system being modeled. The model and the physical system are compared based on calibration criteria that are defined by the user. For example, typical calibration criteria are that model parameter values are to be consistent with independent estimates of associated field parameters, and that simulated hydraulic-head values are to be similar to observed values.

Numerical models of ground-water flow systems can be calibrated by trial-and-error, in which simulated aspects of the physical system are repeatedly, manually changed until the model satisfactorily matches the physical system as measured using the defined calibration criteria. Although trial-and-error calibration is conceptually simple, it has three limitations. First, there is no way to know if the estimated parameter values satisfy the calibration criteria better than some untested set of parameter values. This lack of knowing makes it difficult to test hypotheses about a ground-water flow system because a model constructed using one hypothesis might produce better results because of the parameter values used, and not because that hypothesis is better than another. (The process of comparing different hypotheses is called model discrimination.) Second, it is difficult to determine if estimated parameters are highly correlated--that is, that coordinated changes in model parameters would

produce identical results in terms of the calibration criteria. When high correlations are present, it is impossible to uniquely estimate the parameter values. Third, the reliability of parameter estimates and simulated results can only be assessed by the tedious process of manually perturbing parameter values to perform a sensitivity analysis. The process also is inexact because results depend on how much the parameter values are perturbed, and the appropriate value is generally unknown. The lack of precision makes it difficult to evaluate whether the calibrated model is accurate enough to be used to make conclusions about the aquifer system or to predict aquifer response.

Alternatively, numerical models of ground-water flow systems can be calibrated by nonlinear regression, in which the model itself is used to determine changes in parameter values. Nonlinear regression is accomplished in the following steps:

1. Using the calibration criteria, define an objective function, which is a measure of how closely the model matches the physical system.

2. Determine the parameter values that produce the smallest value of the objective function. This is called minimization or optimization of the objective function, and, using the Parameter-Estimation Package of MODFLOWP, can be accomplished with either the modified Gauss-Newton method or a conjugate-direction method. Because the ground-water flow equation is nonlinear with respect to many of the parameters that are most commonly estimated, the optimization methods are iterative--that is, the same procedure is repeated to update parameter values until the optimal parameter values are reached.

3. Calculate statistics by which model discrimination and assessment of model reliability can be accomplished easily and objectively.

#### Purpose and Scope

This report documents the changes made to MODFLOW, the USGS modular, transient, three-dimensional, ground-water flow model, to create MODFLOWP (pronounced MOD•FLOW•P). When used in conjunction with the new Parameter-Estimation Package, which also is documented in this report, MODFLOWP is designed to estimate parameters of ground-water flow simulations that are steady-state or transient or both using nonlinear regression. When used without the Parameter-Estimation Package, MODFLOWP performs almost exactly like MODFLOW.

This report is intended to be used in conjunction with three other publications. The first two are the documentation of MODFLOW (McDonald and Harbaugh, 1988; Prudic, 1989). When applicable, their package and variable names are repeated in this report, and the reader might need to refer to those two publications for a complete discussion. The third publication is Cooley and Naff's (1990) teaching manual and documentation for a steady-state, two-dimensional, ground-water flow model with nonlinear regression. Many of the ideas presented in this report are discussed in more detail by Cooley and Naff (1990), and that publication is referenced when those ideas are discussed.

Parameters are estimated by using existing, independent estimates of parameter values (called prior estimates of the parameters), measured hydraulic heads and temporal changes in hydraulic head, and measured gains and losses along head-dependent boundaries (called observations of dependent variables). Parameters that are used to calculate the following model inputs can be estimated: properties of confined or unconfined aquifers; horizontal anisotropy; vertical anisotropy (used to calculate the model input vertical leakance); hydraulic conductance of selected cells of the River, Streamflow-Routing, General-Head Boundary, or Drain Packages (McDonald and Harbaugh, 1988; Prudic, 1989); areal recharge rates; maximum evapotranspiration; pumpage rates; and the hydraulic head at constant-head boundaries (head can vary linearly along the boundary).

The report begins with brief descriptions of numerical modeling of ground-water flow, followed by discussions of linear regression, nonlinear regression, and the calculation of sensitivity-equation sensitivities used in modified Gauss-Newton optimization and the gradient of the objective function calculated by the adjoint-state method and used in conjugate-direction optimization. Graphical and statistical methods for analyzing the discrepancies between observed and simulated dependent-variable values, and statistical methods for analyzing estimated parameter values and discriminating between different models are presented. There are detailed instructions for using the computer program, including data-entry formats. Two test cases, data listings and outputs for those cases, a brief description of all new and modified modules, and a listing of the FORTRAN program are included. An example of how regression can be applied to a transient, three-dimensional ground-water flow problem is shown in Yager (1991).

### Solving Matrix Equations

Parameter estimation requires the solution of many matrix equations with dimensions equal to the number of active cells in the finite-difference grid used to represent a ground-water flow system. These matrix equations are solved most successfully by using direct (noniterative) or conjugate-gradient solvers. The strongly implicit procedure (SIP) proved to be impractical because one iteration parameter seed (McDonald and Harbaugh, 1988, p. 12-23) did not produce convergence for all matrix equations for some test cases, and other solvers, such as slice-successive overrelaxation (SSOR) and alternating-direction implicit (ADI), tend to be slow (Trescott and Larson, 1977; Aziz and Settari, 1979, p. 281-294). A direct D4 solver module for two-dimensional problems simulated using MODFLOW was used by Hill (1990a), and is very efficient for two-dimensional problems. The D4 solver is limited, however, because round-off error becomes significant for problems with more than 500 to 1,000 active finite-difference cells. The D4 module has not been documented and is not readily available for users. Conjugate-gradient solver modules have been developed for MODFLOW by Kuiper (1987), Meyer and others (1989), Scandrett (1989), and Hill (1990b), and the first and last modules are readily available for users. Conjugate-gradient solvers generally are less efficient than D4 solvers for small problems, but can be used to accurately solve large problems (Hill, 1990a). Problems with nonlinearities such as a water-table layer or nonlinear head-dependent boundary, need an iterative solver.

### Expertise Needed to Use this Package

Parameter estimation is complicated, and use of this package with an inadequate background can easily produce fallacious conclusions. It is assumed that readers of this report are familiar with the modeling of ground-water flow and matrix addition and multiplication, and have a statistical background equivalent to one college statistics course. Readers unfamiliar with the modeling of ground-water flow need to read one of the available texts on the subject, such as Wang and Anderson (1982). Readers unfamiliar with matrix addition and multiplication need to read and do exercises from Gere and Weaver (1965). Readers unfamiliar with statistics and linear regression need to read and do exercises from Benjamin and Cornell (1970) or another basic text on statistics, and Draper and Smith (1981). Readers unfamiliar with nonlinear regression need to read and do exercises from Bard (1974), Draper and Smith (1981), and Cooley and Naff (1990).

## Notation

Throughout this report, matrices and vectors are presented using the following notation:

Capital or Greek letters underlined twice indicate matrices:  $\underline{\underline{A}}$ ,  $\underline{\underline{\omega}}$ .

A number underlined twice is a matrix, and all entries are equal to that number:  $\underline{\underline{1}}$  is a matrix of ones.

Lower-case letters underlined once indicate column vectors:  $\underline{f}$ ,  $\underline{y}$ .

A number underlined once is a column vector, and all entries are equal to that number:  $\underline{0}$  is a vector of zeros.

The element located in matrix row  $i$  and column  $j$  is designated as follows: matrix  $\underline{\underline{A}}$ , elements  $a_{i,j}$ ; matrix  $\underline{\underline{V}}$ , elements  $v_{i,j}$ .

The  $i$ th element of vector  $\underline{f}$  is  $f_i$ .

$\underline{\underline{A}}^T$  is the transpose of matrix  $\underline{\underline{A}}$ .

$\underline{e}^T$  is a row vector with the same elements as  $\underline{e}$ .

$\underline{\underline{A}}^{-1}$  is the inverse of matrix  $\underline{\underline{A}}$ .

$\underline{\underline{X}}$  is an  $N$  by  $M$  matrix if it has  $N$  rows and  $M$  columns. A column vector might be  $N$  by  $1$ , a row vector might be  $1$  by  $M$ .

$\underline{\underline{I}}$  is the identity matrix. Elements equal  $1$  along the diagonal and are zero elsewhere.

Given a square, symmetric matrix  $\underline{\underline{A}}$ ,  $\underline{\underline{A}}^2 = \underline{\underline{A}}^T \underline{\underline{A}}$ ;  $\underline{\underline{A}}^{\frac{1}{2}} = B$ , where  $B$  is defined so  $\underline{\underline{B}}^T \underline{\underline{B}} = \underline{\underline{A}}$ .

If the scalar variable  $S$  is a function of vector  $\underline{a}$  then:

$\frac{\partial S}{\partial \underline{a}}$  is a column vector with the  $i$ th element equal to  $\partial S / \partial a_i$ .

If the vector  $\underline{a}$  is a function of the scalar  $\alpha$ , then:

$\partial \underline{a} / \partial \alpha$  is a column vector with the  $i$ th element equal to  $\partial a_i / \partial \alpha$ .

Derivatives of matrices with respect to vectors produce arrays with more than two dimensions. These are discussed in detail when they are mentioned in the text.

Subscripts also are used to designate row, column, and layer number of the finite-difference grid and sequential cell number, and are defined when they are mentioned in the text.

Some module variables are used in the text to expedite relating the text to the modules. These variables are written in uppercase letters, and are defined in the text where they are introduced and in the "List of Variables" in Appendix C.

### Acknowledgments

The author would like to thank Richard M. Yager, (U.S. Geological Survey, Ithaca, New York) for using early versions of this report and computer program. His efforts toward identifying and correcting errors, and his ideas for making MODFLOWP more useful were exceptional and are greatly appreciated. The author would also like to thank David S. Morgan and Erin A. Lynch (U.S.G.S., Eugene, Oregon, and Lansing, Michigan, respectively) for helping to identify and correct errors in early versions.



# MODELING TRANSIENT, THREE-DIMENSIONAL, GROUND-WATER FLOW SYSTEMS

## Ground-Water Flow Equation

MODFLOW is documented extensively by McDonald and Harbaugh (1988) and Prudic (1989), and only those parts needed to understand MODFLOWP and the Parameter-Estimation Package are repeated here.

In their development, McDonald and Harbaugh (1988, ch. 2) discretized the ground-water flow equation spatially by using the block-centered, finite-difference method, and they implicitly differenced the equation in time. For one finite-difference cell, the discretized, differenced ground-water flow equation can be written as (McDonald and Harbaugh, 1988, p. 2-19):

$$\begin{aligned}
 & CR_{i,j-1/2,k} (h_{i,j-1,k}^n - h_{i,j,k}^n) + CR_{i,j+1/2,k} (h_{i,j+1,k}^n - h_{i,j,k}^n) \\
 & + CC_{i-1/2,j,k} (h_{i-1,j,k}^n - h_{i,j,k}^n) + CC_{i+1/2,j,k} (h_{i+1,j,k}^n - h_{i,j,k}^n) \\
 & + CV_{i,j,k-1/2} (h_{i,j,k-1}^n - h_{i,j,k}^n) + CV_{i,j,k+1/2} (h_{i,j,k+1}^n - h_{i,j,k}^n) \\
 & + P_{i,j,k}^n h_{i,j,k}^n + Q_{i,j,k}^n - S_{s,i,j,k} \frac{(\Delta r_j \Delta c_i \Delta v_k) (h_{i,j,k}^n - h_{i,j,k}^{n-1})}{t_n - t_{n-1}}
 \end{aligned} \tag{1}$$

where  $n$  is the time step at which hydraulic head is being calculated, and  $n-1$  is the previous time step;  
 $i, j, k$  are the row, column, and layer of the finite-difference cell, and, thus, identify spatial location;  
 $\Delta r_j$  is the length of the cell as measured along a row (L);  
 $\Delta c_i$  is the length of the cell as measured along a column (L);  
 $\Delta v_k$  is the length of the cell as measured perpendicular to the orientation of the layer (L);  
 $h_{i,j,k}^n$  is the hydraulic head in the center of cell  $i, j, k$  at the end of time step  $n$ ;

$CR_{i,j-1/2,k}$  and  $CR_{i,j+1/2,k}$  are the lateral hydraulic conductances between the cell at  $i, j, k$  and the two neighboring cells in row  $i$  ( $L^2/T$ );

$CC_{i-1/2,j,k}$  and  $CC_{i+1/2,j,k}$  are the lateral hydraulic conductances between the cell at  $i,j,k$  and the two neighboring cells in column  $j$  ( $L/T$ );

$CV_{i,j,k-1/2}$  and  $CV_{i,j,k+1/2}$  are the vertical hydraulic conductances between the cell at  $i,j,k$  and the two neighboring cells in adjoining model layers ( $L^2/T$ );

$P_{i,j,k}^n$  is the sum of all conductances of head-dependent boundary conditions applicable at cell  $i,j,k$  at time step  $n$  ( $L^2/T$ );

$Q_{i,j,k}^n$  is the sum of all sources or sinks or both at cell  $i,j,k$  at time step  $n$ , the conductances of head-dependent boundaries multiplied by the known hydraulic head of the head-dependent boundary condition at cell  $i,j,k$  at time step  $n$ , and terms related to constant-head boundaries ( $L^3/T$ ); and

$S_{i,j,k}$  is the specific storage, or the specific yield divided by  $\Delta v_k$ , at cell  $i,j,k$ .

The calculation of the hydraulic conductances is discussed by McDonald and Harbaugh (1988, ch. 5), and can be summarized as:

$$CR_{i,j+1/2,k} = 2\Delta c_i \frac{TR_{i,j,k} TR_{i,j+1,k}}{TR_{i,j,k} \Delta r_{j+1} + TR_{i,j+1,k} \Delta r_j}, \quad (2a)$$

$$CC_{i+1/2,j,k} = 2\Delta r_j \frac{TC_{i,j,k} TC_{i+1,j,k}}{TC_{i,j,k} \Delta c_{i+1} + TC_{i+1,j,k} \Delta c_i}, \quad (2b)$$

$$CV_{i,j,k+1/2} = \left( \frac{m \Delta z}{\sum_{g=1}^G K_g} \right)^{-1} \Delta r_j \Delta c_i, \quad (2c)$$

where  $TR_{i,j,k}$  is the transmissivity along the row at cell  $i,j,k$ , and equals the hydraulic conductivity along the row multiplied by saturated thickness ( $L^2/T$ );

$TC_{i,j,k}$  is the transmissivity along the column at cell  $i,j,k$ , and equals the hydraulic conductivity along the column multiplied by the saturated thickness ( $L^2/T$ );

$m$  is the number of strata between cell centers in model layers  $k$  and  $k+1$  that have different values of vertical hydraulic conductivity;

$\Delta z_g$  is the thickness of each of the  $m$  strata (L);

$K_g$  is the vertical hydraulic conductivity of each of the  $m$  strata (L/T).

$\left( \sum_{g=1}^m \frac{\Delta z_g}{K_g} \right)^{-1}$  is the vertical leakance (1/T).

The volume of aquifer material that is accounted for by each of the conductances is shown in figure 1.

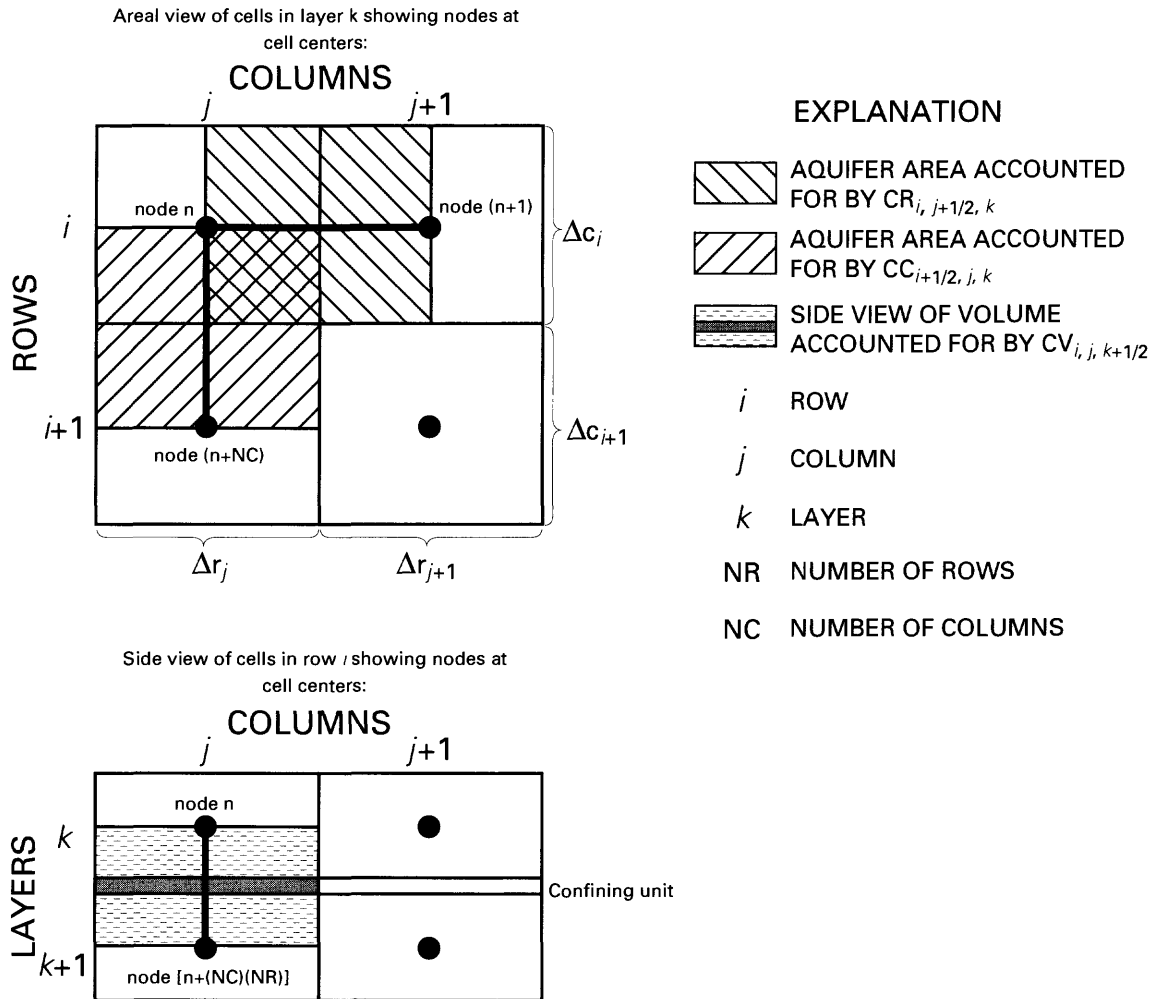


Figure 1.--Aquifer-system volumes accounted for by conductances  $CR_{i, j+1/2, k}$ ,  $CC_{i+1/2, j, k}$ , and  $CV_{i, j, k+1/2}$  in the block-centered, finite-difference method.

If equation (1) is written for each cell of a finite-difference grid, the resulting equations can be expressed in matrix form as:

$$\underline{A}(n)\underline{h}(n) - \underline{B}(n)\underline{h}(n-1) = \underline{f}(n) \quad (3)$$

where  $\underline{h}(n)$  is a vector of hydraulic heads at all grid points at the end of time step  $n$  [L];

$\underline{A}(n)$  equals  $\frac{-\underline{S}}{\Delta t(n)} + \underline{K} + \underline{P}(n)$  [ $L^2/T$ ];

$\underline{S}$  is a diagonal matrix of specific storage multiplied by cell volume, or specific yield multiplied by cell area [ $L^2$ ];

$\Delta t(n)$  is the length of time step  $n$  [T];

$\underline{K}$  is a matrix of horizontal and vertical conductances [ $L^2/T$ ];

$\underline{P}(n)$  is a diagonal matrix of conductances at head-dependent boundaries [ $L^2/t$ ];

$\underline{B}(n)$  equals  $\frac{-\underline{S}}{\Delta t(n)}$  [ $L^2/T$ ]; and

$\underline{f}(n)$  is a vector of the  $Q_{i,j,k}^n$ , and is sometimes referred to as the forcing function [ $L^3/T$ ].

Of the matrices from which  $\underline{A}$  and  $\underline{B}$  are calculated, only  $\underline{K}$  has nonzero components off the main diagonal. The structure of  $\underline{K}$  for a problem with two rows, three columns, and two layers is shown in figure 2, using subscripts to denote row, layer, and column numbers.  $\underline{K}$  is symmetric, and all nonzero components off the main diagonal occur on six off diagonals. The components,  $u_{i,j,k}$ , on the main diagonal of  $\underline{K}$  are calculated as the negative sum of the off-diagonal components for that row. For example:

$$u_{1,1,1} = CR_{1,1\neq,1} + CC_{1\neq,1,1} + CV_{1,1,1}$$

$$u_{1,2,1} = CR_{1,1\neq,1} + CR_{1,2\neq,1} + CC_{1\neq,2,1} + CV_{1,2,1}$$

The Parameter-Estimation Package can accommodate confined or unconfined model layers (LAYCON of the Block-Centered Flow Package=0 or 1), but is not designed to accommodate convertible layers (LAYCON=2 or 3). Finite-difference cells in water-table layers become inactive ('go dry') when the simulated hydraulic head declines below the bottom of a water-table layer. MODFLOW does not allow these cells to become active again within a single

$u_{1,1,1}$	$-CR_{1,1+1/2,1}^0$	$-CC_{1+1/2,1,1}^0$	$0$	$-CV_{1,1,1+1/2}^0$	$0$	$0$	$0$	$0$
$u_{1,2,1}$	$-CR_{1,2+1/2,1}^0$	$-CC_{1+1/2,2,1}^0$	$0$	$0$	$-CV_{1,2,1+1/2}^0$	$0$	$0$	$0$
$u_{1,3,1}$	$0$	$0$	$-CC_{1+1/2,3,1}^0$	$0$	$0$	$-CV_{1,3,1+1/2}^0$	$0$	$0$
$u_{2,1,1}$	$-CR_{2,1+1/2,1}^0$	$-CR_{2,1+1/2,1}^0$	$0$	$0$	$0$	$-CV_{2,1,1+1/2}^0$	$0$	$0$
$u_{2,2,1}$	$-CR_{2,2+1/2,1}^0$	$-CR_{2,2+1/2,1}^0$	$0$	$0$	$0$	$0$	$-CV_{2,2,1+1/2}^0$	$0$
$u_{2,3,1}$	$0$	$0$	$0$	$0$	$0$	$0$	$0$	$-CR_{2,3,1+1/2}^0$
$u_{1,1,2}$	$-CR_{1,1+1/2,2}^0$	$-CC_{1+1/2,1,2}^0$	$0$	$0$	$0$	$0$	$0$	$0$
$u_{1,2,2}$	$-CR_{1,2+1/2,2}^0$	$-CC_{1+1/2,2,2}^0$	$0$	$0$	$0$	$0$	$0$	$0$
$u_{1,3,2}$	$0$	$0$	$0$	$0$	$0$	$0$	$0$	$0$
$u_{2,1,2}$	$-CR_{2,1+1/2,2}^0$	$-CC_{1+1/2,1,2}^0$	$0$	$0$	$0$	$0$	$0$	$0$
$u_{2,2,2}$	$-CR_{2,2+1/2,2}^0$	$-CC_{1+1/2,2,2}^0$	$0$	$0$	$0$	$0$	$0$	$0$
$u_{2,3,2}$	$0$	$0$	$0$	$0$	$0$	$0$	$0$	$0$

symmetric

Figure 2.--Matrix  $\underline{K}$  of the finite-difference method for a problem with two rows, three columns, and two layers.

simulation (McDonald and Harbaugh, 1988, p. 5-9). The Parameter-Estimation Package, however, reactivates these cells at the beginning of each parameter-estimation iteration (see chapter in this report on nonlinear regression for a discussion of parameter-estimation iterations).

Estimated parameters can be used to calculate the model inputs listed in table 1. These model inputs are the quantities listed in the MODFLOW input instructions (McDonald and Harbaugh, 1988; Prudic, 1989). The component of equation (3) in which each model input is included also is noted.

Table 1.--Model inputs listed in the MODFLOW input instructions (McDonald and Harbaugh, 1988; Prudic, 1989) that can be calculated using parameters estimated by using the Parameter-Estimation Package, and the terms of equation (3) in which they occur

Model Inputs	Term in Equation (3)
Properties of model layers	
Confined layer	
Transmissivity <sup>1,2</sup>	$\underline{K}$
Storage coefficient <sup>1</sup>	$\underline{S}$
Unconfined layer	
Hydraulic conductivity <sup>1,2</sup>	$\underline{K}$
Specific yield <sup>1</sup>	$\underline{S}$
All layers	
Horizontal anisotropy by layer <sup>1</sup>	$\underline{K}$
Vertical leakance between layers <sup>1,2</sup>	$\underline{K}$
Vertical anisotropy between layers (used to calculate vertical leakance) <sup>1</sup>	$\underline{K}$
Head-dependent boundary conductances	$\underline{P}(n); \underline{f}(n)$
River Package <sup>1</sup>	
Streamflow-Routing Package <sup>1</sup>	
General Head-Dependent Boundary Package <sup>1</sup>	
Drain Package <sup>1</sup>	
Maximum evapotranspiration	$\underline{P}(n); \underline{f}(n)$
Constant-head boundaries	$\underline{f}(n)$
Stresses	$\underline{f}(n)$
Pumpage	
Recharge	

<sup>1</sup> Parameters can be defined by a natural-log transformation.

<sup>2</sup> One parameter can be used to calculate any combination of transmissivity of confined layers, hydraulic conductivity of unconfined layers, and vertical leakance between layers.

### Parameterization

Although the ground-water flow model permits different model-input values and, therefore, parameter values to be assigned to each model cell, and many model inputs can equal different values at different time steps, estimating this many values is impractical given the data available for most problems. Decreasing the number of parameter values permits them to be reliably estimated with the available data (the reliability of estimates is discussed later in this report). In general, the number of parameter values estimated needs to be a fraction of the number of hydraulic-head and streamflow gain-or-loss observations used to estimate them.

The number of unique parameter values to be estimated can be decreased by assuming that some of the values are known and by parameterization (Shah and others, 1978). In parameterization, a few parameter values are used to define the model-input values for many cells and time steps. Yager (1991) provides an example for a transient, three-dimensional ground-water flow system.

In the Parameter-Estimation Package, spatially varying values of model inputs can be calculated from parameters using cell-by-cell multiplicative factors, multiplication arrays, and zone arrays. Multiplication and zone arrays are used only for model inputs that are read as arrays by MODFLOW (McDonald and Harbaugh, 1988), which includes all 'Properties of model layers' listed in table 1 except horizontal and vertical anisotropy, and maximum evapotranspiration and recharge.

As an example for a model input that is not read as an array by MODFLOW, consider the conductance of the River Package. The conductance for a cell equals the hydraulic conductivity of the riverbed times the area the river occupies within the cell, divided by the riverbed thickness (McDonald and Harbaugh, 1988, p. 6-5). The Parameter-Estimation Package allows the user to define a different multiplicative factor for each river cell included in defining a parameter. Spatial variations in riverbed hydraulic conductivity, area, and thickness, therefore, can be included in multiplicative factors, and a spatially constant parameter value can be estimated. If the riverbed hydraulic conductivity can be considered to be constant for the cells, the parameter can be defined as being equivalent to that riverbed hydraulic conductivity, and the multiplicative factors would

equal the area of the river in each cell divided by the riverbed thickness. Alternatively, the initial estimates of riverbed conductance can be used as the multiplicative factors, and the parameter value initially set to 1.0. Then, any change in the parameter value would indicate the change in riverbed conductance produced by nonlinear regression. For example, a value of 0.50 would indicate a 50-percent decrease in the riverbed conductance for the included cells.

As an example for a model input read as an array by MODFLOW, consider the transmissivity of a confined model layer. If it is reasonable to assume that the hydraulic conductivity is constant, the parameter could be defined as the hydraulic conductivity. The multiplicative factor times the multiplication array would equal layer thickness; a zone array could be used if the parameter only represented the hydraulic conductivity of part of the layer. If it is known that the hydraulic conductivity is smaller in one part of the layer, this could be represented by decreasing the elements of the multiplication array in that area, or by introducing an additional parameter equal to the smaller hydraulic conductivity value. If the geohydrology of the ground-water flow system indicates that the hydraulic conductivity is applicable to parts of other model layers, they can be included in the definition.

For model inputs read as arrays by MODFLOW, the model input can be calculated as the sum of contributions from more than one parameter. As a simple example, consider the situation illustrated in figure 3. Here, it is assumed that the model input varies linearly along columns of the finite-difference grid. This variation can be represented by assigning one parameter to be equal to the model input value at row 1, and another parameter to be equal to the model input value at row 10. If the product of all multipliers for the first parameter equals 1.0 at row 1 and linearly decreases to 0.0 at row 10, and the product of all multipliers for the second parameter equals 0.0 at row 1 and linearly increases to 1.0 at row 10, the desired variation and parameter definition is obtained. Note that the values of parameters defined along the two rows of the grid are interpolated to all cells. For two-dimensional variation, two-dimensional finite-element basis functions (Segerlind, 1976) or kriging (Keidser and others, 1990) can be used to calculate multiplication arrays that perform



the desired interpolation. For kriging, a fitted or assumed variogram is used, and parameters can be defined as discussed in Appendix A. For three-dimensional variation, three-dimensional finite-element basis functions (Segerlind, 1979) can be used. Other interpolation techniques, such as polynomial interpolation and cubic splines, can also be used.

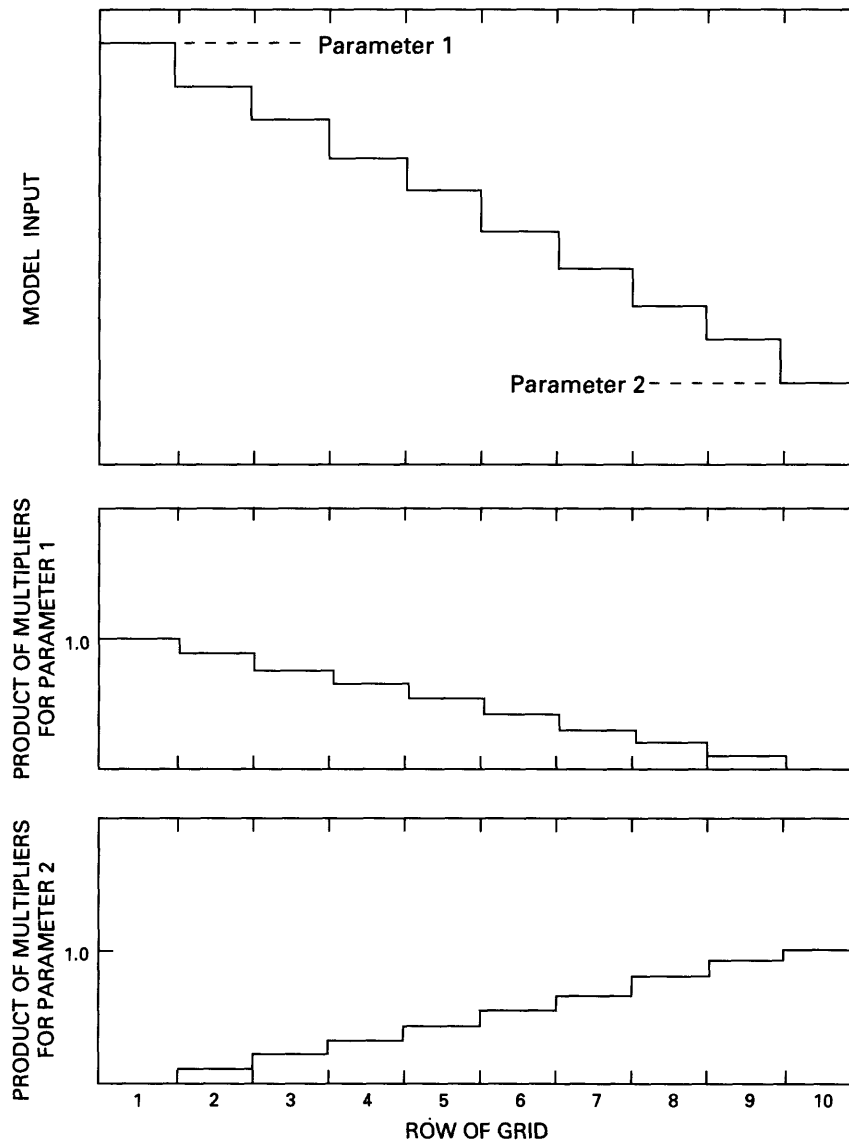


Figure 3.--Multipliers needed to define a discretized linear variation in a model input using two parameters.

The formulation provided for spatial parameterization allows a great deal of flexibility in defining parameters. It is hoped that this will allow users to define parameters that make the most physical sense in a given situation, and to realistically represent spatial variability while minimizing the number of parameters estimated. Note that any defined spatial variability is assumed to be known, and all uncertainty is related to the estimated parameters. If the spatial variability is not truly known, which is common, the results of the nonlinear regression might indicate unrealistically reliable model results.

The temporal parameterization permitted in the Parameter-Estimation Package is limited to making parameter values equal for specified time steps; the time steps can be from different stress periods and might or might not be continuous. In a sense, this is zonation applied temporally.

Some estimated parameters can be redefined by a natural-log transformation. Redefining the parameter in this way sometimes produces a better-conditioned regression problem (Carrera, 1984), always ensures that the parameter value remains positive, and, if the parameter is assumed to be lognormally distributed, allows more convenient statistics to be used to characterize the reliability of prior and final estimates. Hydraulic-conductivity estimates commonly are considered to be lognormally distributed because point hydraulic-conductivity measurements have been determined to be lognormally distributed in some geohydrologic situations (Davis, 1969, p. 76; Nielsen and others, 1973; Freeze, 1975; Neuman, 1982; Sudicky, 1986).

Some example lognormal distributions are shown in figure 4. Discussions of the lognormal distribution are available in Benjamin and Cornell (1970, p. 262-270), and Schmittroth (1979); the reader is referred to these sources for its characteristics. Here, note that if  $K$  is a lognormally distributed parameter,  $\exp[E(\ln K)]$ , equals the modal value of  $K$ , and  $\exp[E(\ln K) + \sigma^2/2]$  equals  $E(K)$ , the mean of  $K$ , where  $\sigma^2$  is the variance of  $\ln K$ . The exponential of confidence intervals on  $E(\ln K)$ , therefore, are confidence intervals on the modal value of  $K$ , and might not be symmetric about  $\exp[E(\ln K)]$ . The model inputs associated with parameters that can be redefined by a natural-log transformation are noted in table 1.

Users who prefer  $\log_{10}$  transformation can convert to  $\log_{10}$  by multiplying the log-transformed parameter value estimated by the Parameter-Estimation Package by  $\log_{10} e = 0.4342945$ . This is derived by noting that a parameter,  $b$ , can be expressed as  $b = e^{\ln b}$ . Then,  $\log_{10} b = \ln b \log_{10} e$ .

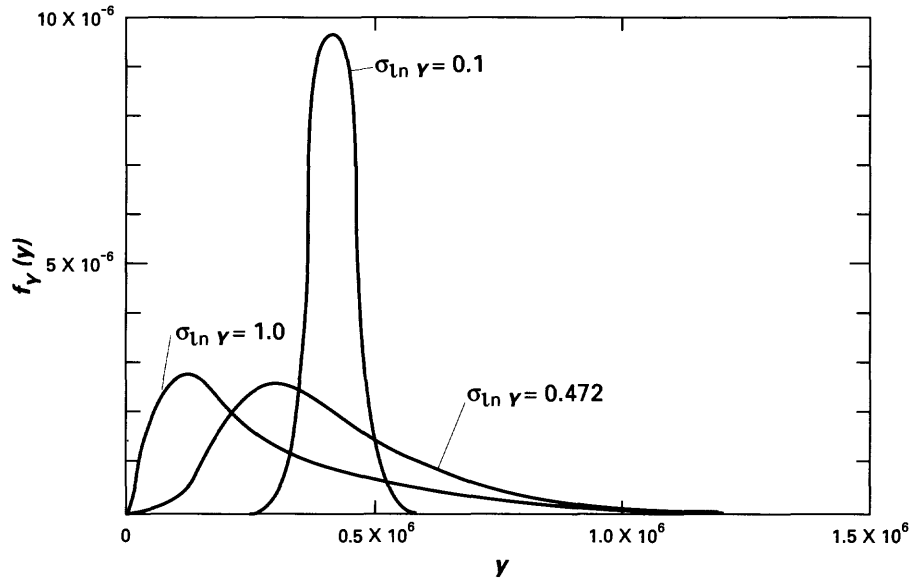


Figure 4.--Lognormal distributions with the same mean showing the effect of  $\sigma_{\ln Y}$ , where  $\ln Y$  is a normally distributed random variable. [Modified by Benjamin and Cornell (1970); used with permission of the publisher.]

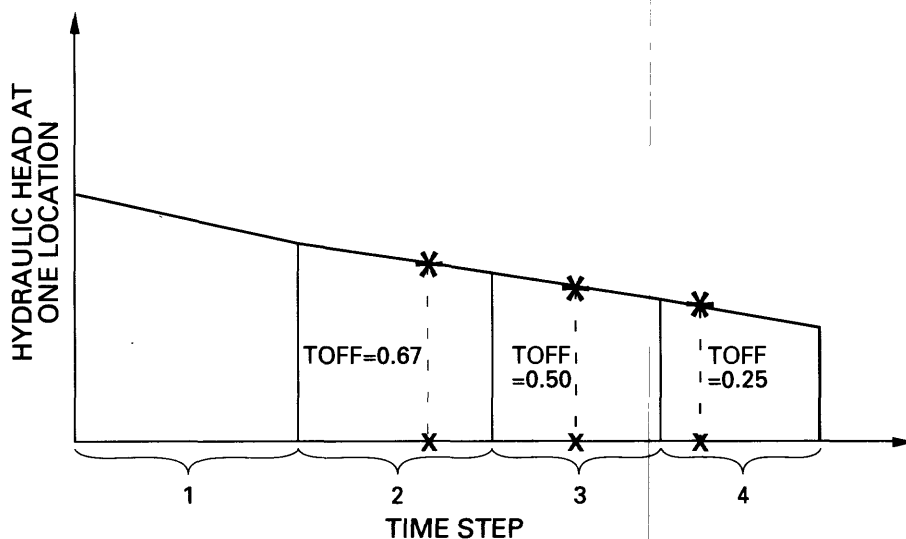
#### OBSERVATIONS

Several types of commonly available observations of dependent variables can be used to estimate parameters, including observations of hydraulic head or temporal changes in hydraulic head at arbitrary times and locations, observations of hydraulic head or temporal changes in hydraulic head averaged over several model layers, and observations of gains and losses along head-dependent boundaries, such as streamflow gains and losses. To use these observations to estimate parameters by nonlinear regression, corresponding simulated values,  $\hat{y}$ , need to be calculated so that the difference between observed and simulated values can be evaluated and minimized. Calculation of  $\hat{y}$  for the different types of observations is described in the following sections; use of  $\hat{y}$  in nonlinear regression is described later in the text.

Calculation of  $\hat{y}$  needs to be modified if water-table cells involved in the calculation 'go dry'. This problem also is discussed in this chapter.

### Hydraulic Head at One Location Observed Over Time

Hydraulic heads can be observed for any time represented by the simulation. If the observation occurs within a time step,  $\hat{y}$  is calculated by linearly interpolating values calculated at the beginning and end of the time step using TOFF, a coefficient specified by the user (Appendix A). TOFF equals the time of the observation minus the time at the beginning of the time step divided by the length of the time step. Use of TOFF is illustrated in figure 5.



#### EXPLANATION

- \* LINEARLY INTERPOLATED  
SIMULATED HYDRAULIC HEAD
- x TIME OF OBSERVED  
HYDRAULIC HEAD

Figure 5.--Use of TOFF to calculate simulated values of hydraulic heads observed within time steps by linear interpolation.

Hydraulic heads observed at one location over time can be represented in the Parameter-Estimation Package as hydraulic heads at each time of observation, or as an initial hydraulic head followed by changes in hydraulic head. The second representation permits some types of correlation in the true errors to be accurately and easily represented, as described later in this report in the section "Weighting Observations".

#### Hydraulic Head at Arbitrary Locations

The finite-difference method calculates hydraulic heads at the center of each active finite-difference cell within a layer. Observation wells, however, rarely are located at cell centers and might not be screened throughout the entire thickness represented by the model layer. In this report, hydraulic heads are assumed to be equal through the thickness of each model layer, so variations caused by limited screening of the observation well within a layer are ignored. Simulated hydraulic heads at observation locations are calculated by interpolating within the two-dimensional plane of a single layer. Six locations (A-F) for which hydraulic heads might need to be interpolated are shown in figure 6. Location A is exactly in the center of a cell, so no interpolation would be needed. Location E is exactly between two cell centers, so interpolation using two hydraulic heads would be needed. Hydraulic heads at all other locations would require interpolation using three or four hydraulic heads.

Exact interpolation of hydraulic heads is not always possible for the finite-difference method described by equations (1) and (2) because hydraulic properties that are defined for cells do not extend between locations where hydraulic head is calculated. For example, interpolation for locations C, D, or F in figure 6 could require as many as four different hydraulic-conductivity values, and, for this complicated case, no exact interpolation method is available.

Approximate geometric interpolation methods that exclude the variations in hydraulic conductivity are available. In this report, geometric interpolation based on linear, finite-element basis functions is used. Linear one-dimensional basis functions (equivalent to linear interpolation) are used for locations such as B and E in figure 6, which are adjacent to two inactive cells or are exactly between adjoining cell centers; triangular

basis functions are used for locations such as C and F in figure 6, which are within a triangle formed by the centers of three neighboring cells because the fourth neighboring cell is inactive; and quadrilateral basis functions are used for locations such as D in figure 6, which are within a rectangle formed by the centers of four active cells. All basis functions are calculated using local coordinates that are specified by the user and define where the arbitrary location is within a cell relative to the location of the cell center. These local coordinates are a row offset, ROFF, and a column offset, COFF, and their use is illustrated in figure 6. Note that ROFF is negative in the direction of decreasing row numbers, and COFF is negative in the direction of decreasing column numbers.

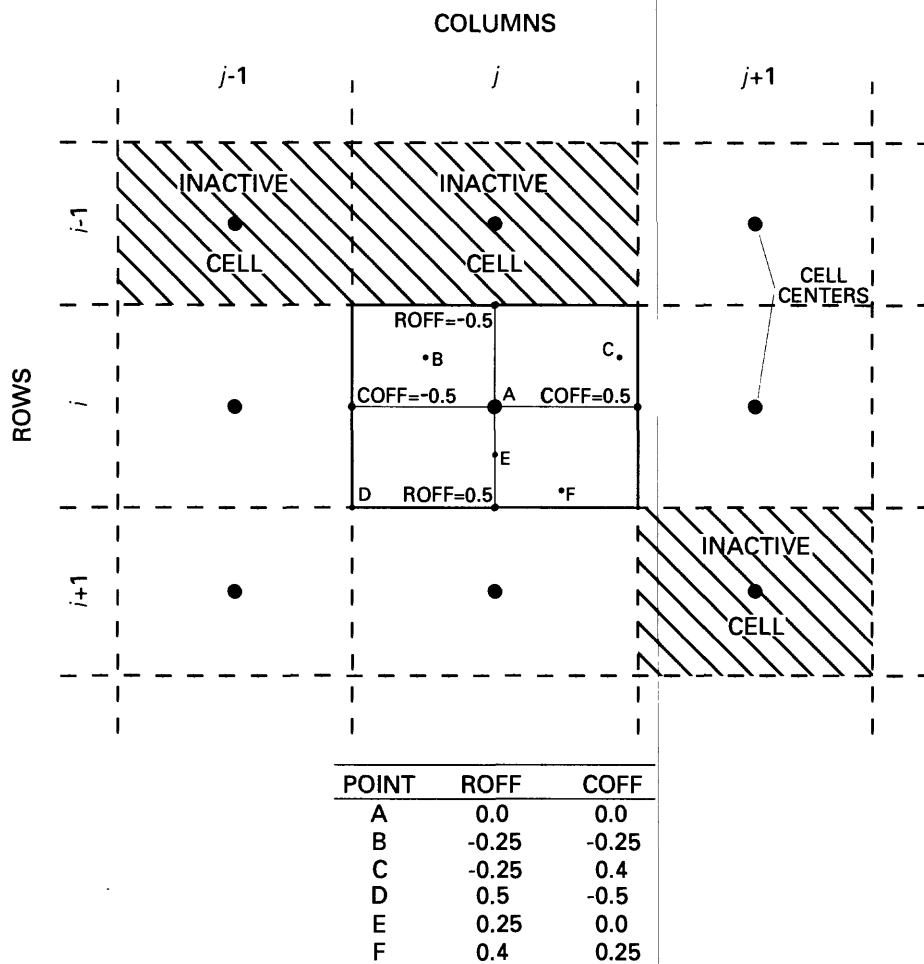


Figure 6.--Locating points within a finite-difference cell using ROFF and COFF.

The basis functions used are described in numerous texts and are not discussed in this report. They are equivalent to the one-dimensional simplex, two-dimensional simplex, and quadratic-element basis functions of Segerlind (1976, p. 24, 28, and 258), and the triangular "archetypal" and rectangular-element basis functions of Wang and Anderson (1982, p. 119 and 153). Wang and Anderson (1982) do not discuss a linear, one-dimensional basis function.

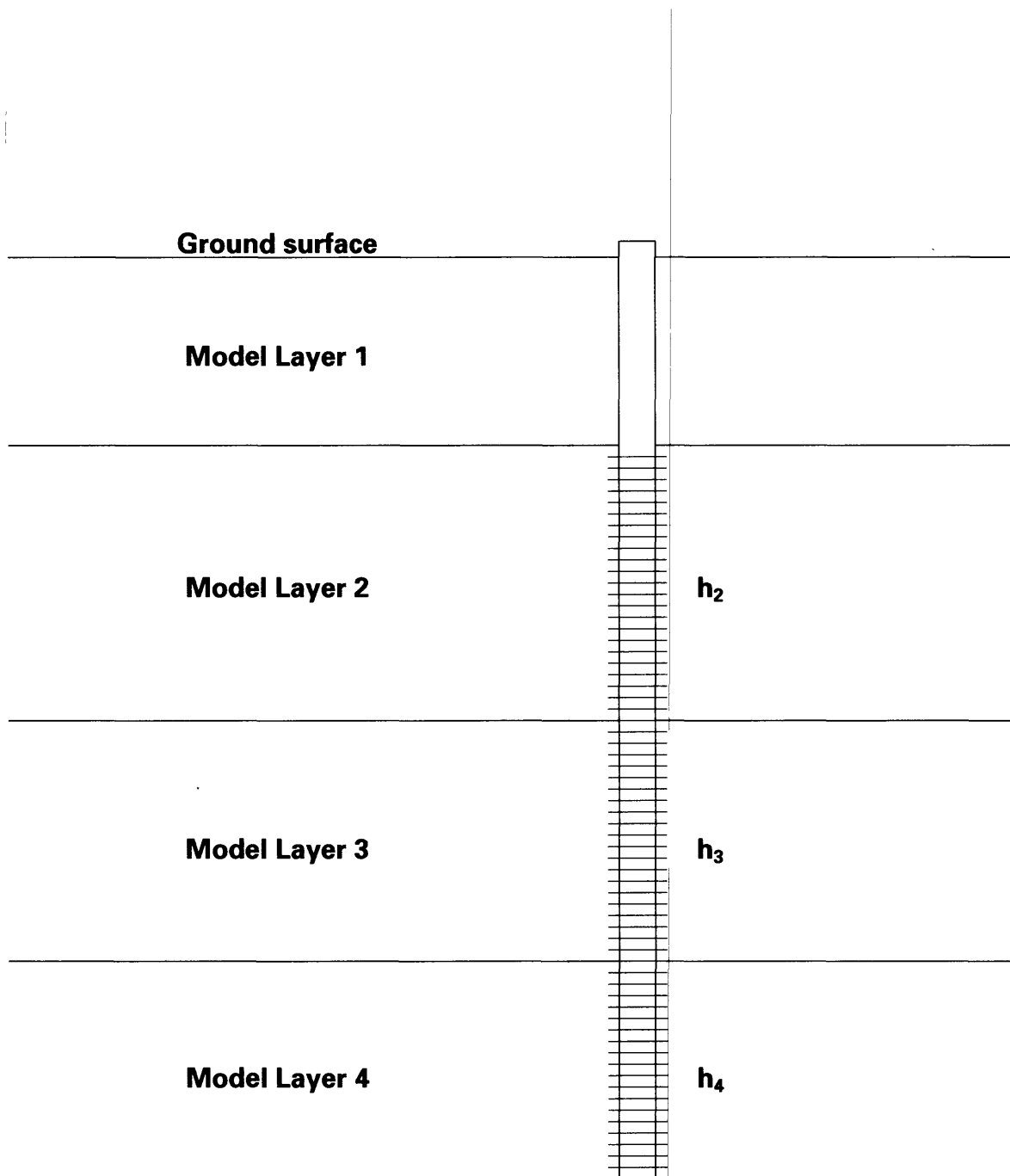
Errors introduced by using geometric interpolation might become substantial when the hydraulic properties of neighboring cells are different and cell dimensions are large. At such locations, the differences between observed and simulated hydraulic heads might be inaccurate and could produce inaccurate parameter estimates. This problem would be characterized by larger than expected differences between observed and simulated hydraulic heads.

Although this section only discusses observed hydraulic heads, identical procedures are used when an initial hydraulic head followed by temporal changes in hydraulic head are used.

#### Multilayer Hydraulic Heads

If an observation well is screened over intervals that represent more than one model layer, and the observed hydraulic head or change in hydraulic head is affected by all screened intervals, then the associated simulated value is a weighted average of the hydraulic heads or changes in hydraulic head calculated for each of the layers involved. The simulated value is calculated by multiplying the hydraulic head or change in hydraulic head in each layer by a user-specified proportion and then summing the results, as shown in figure 7. A more realistic representation of this problem would be produced by calculating the proportions based on the flow-system and aquifer characteristics, but the Parameter-Estimation Package does not do this.

Interpolation for multilayer hydraulic heads can be complicated because neighboring cells can be active or inactive, depending on the layer. In the Parameter-Estimation Package, the interpolation is defined using the IBOUND array (McDonald and Harbaugh, 1988, p. 4-2) of the first layer listed for the multilayer hydraulic-head observation (see DATA SET 6A of the INPUT



$$\hat{y} = p_2 h_2 + p_3 h_3 + p_4 h_4$$

$h_2$ ,  $h_3$ , and  $h_4$  are calculated hydraulic heads at the observation location in layers 2, 3, and 4.

$p_2$ ,  $p_3$ , and  $p_4$  are proportions defined by the user.

Figure 7.--Calculating the simulated value of hydraulic head for a multilayer observation well.



FILE, Appendix A). Thus, for each neighboring cell that is inactive in any of the other model layers, the cell in the same row and column in the first layer listed needs to be active. If no one layer contains a complete set of inactive cells, correct interpolation cannot be accomplished. This is illustrated in figure 8.

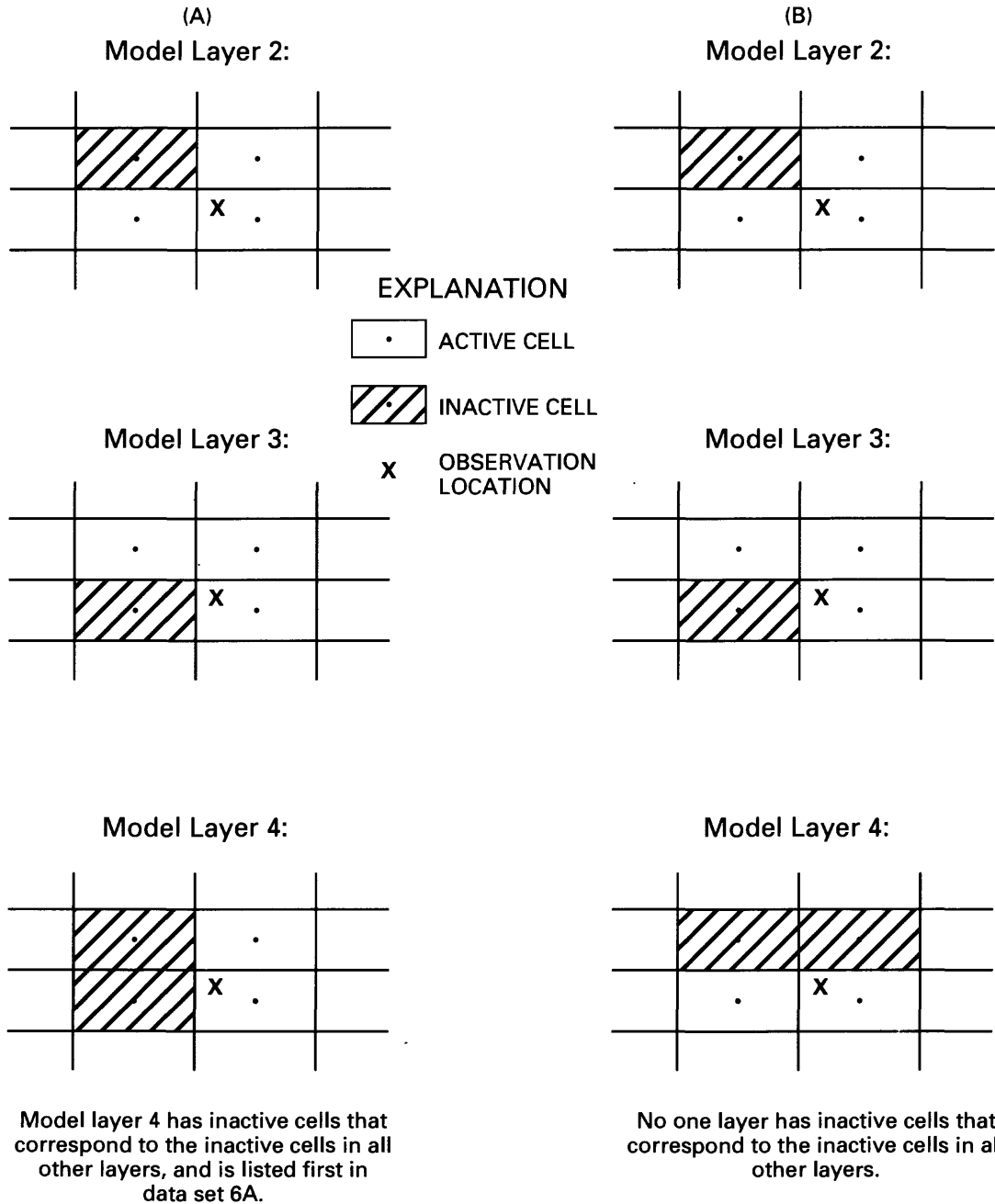


Figure 8.--Situations that do (A) and do not (B) produce correct spatial interpolation for multilayer hydraulic-head observations.

### Gains and Losses Along Head-Dependent Boundaries

Head-dependent boundaries correspond to, for example, rivers, drains and lakes, and can be simulated using the River, Drain, or General-Head Boundary Packages (McDonald and Harbaugh, 1988, ch. 6, 9, and 11), or the Streamflow-Routing Package (Prudic, 1989). Flows into or out of any part of a head-dependent boundary for which gains and losses have been observed are calculated as:

$$\hat{y} = \sum_{i=1}^{NQCL} c_i q_i = \sum_{i=1}^{NQCL} c_i \frac{K_i}{D_i} A_i (H_i - h_i), \quad (4)$$

where NQCL is the number of finite-difference cells (number of reaches for the Streamflow-Routing Package) used to simulate that part of the boundary;

$q_i$  is the simulated flow rate at one cell ( $L^3/T$ ) (negative for flow out of the aquifer);

$c_i$  is a user-defined multiplicative factor;

$K_i$  is the cell hydraulic conductivity ( $L/T$ ) of, for example, the riverbed or lakebed;

$D_i$  is the cell thickness ( $L$ ) of, for example, the riverbed or lakebed;

$A_i$  is the area of the water body within the finite-difference cell ( $L^2$ );

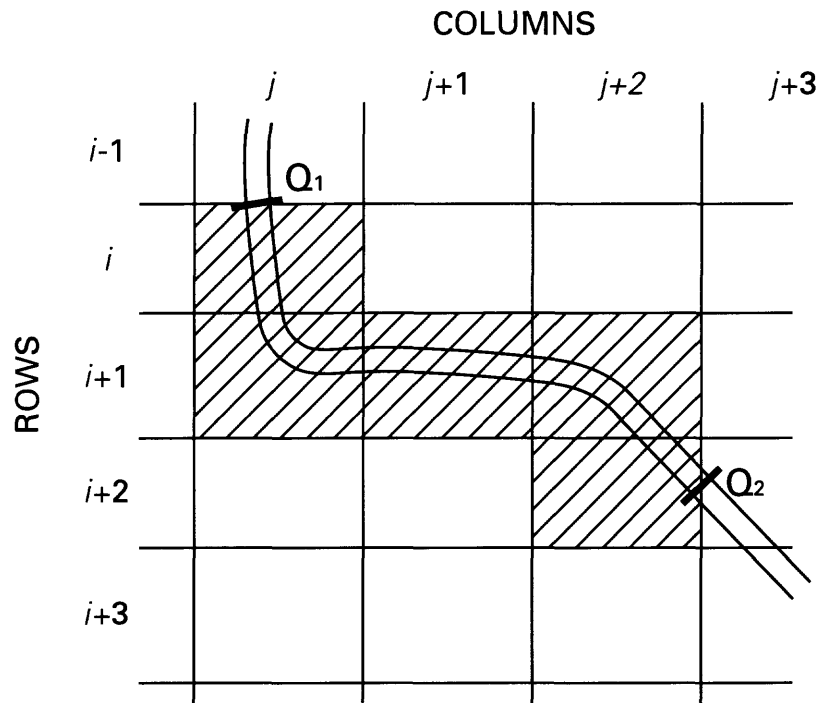
$h_i$  is the simulated hydraulic head in the ground-water system adjacent to the head-dependent boundary ( $L$ ); and

$H_i$  is the water level in the water body or the elevation of the drain.

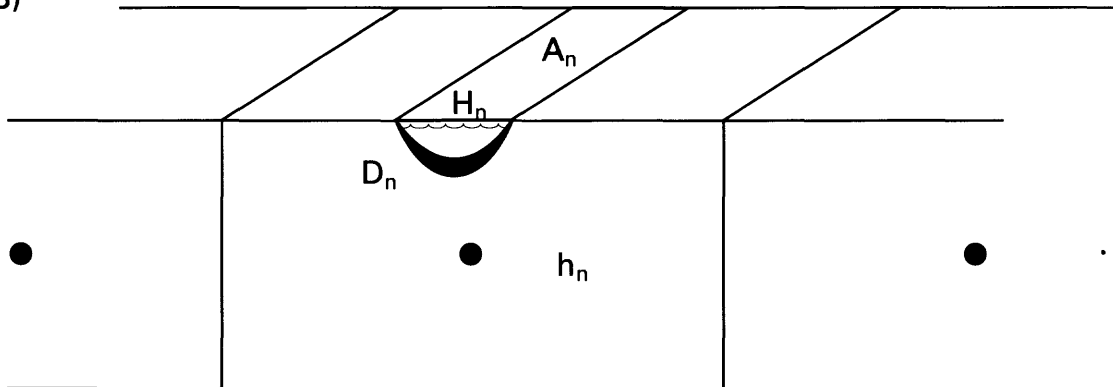
The observed equivalent of  $\hat{y}$ ,  $y$ , would equal  $Q_2 - Q_1$ , as shown in figure 9A; the related components of equation (4) are shown in figures 9A and 9B.

Generally  $c_i = 1.0$ . However, if  $Q_1$  or  $Q_2$  or both are located within a cell instead of the edges of the cells as in figure 9A,  $c_i$  needs to be less than  $\hat{1.0}$  so that only part of the flow calculated for the cell is included in  $\hat{y}$ .

(A)



(B)



#### EXPLANATION



	ONE OF THE NOCL CELLS REPRESENTING THE REACH BETWEEN $Q_1$ AND $Q_2$ IN THE MODEL	$D_n$	THICKNESS OF THE WATER-BODY BED WITHIN THE FINITE-DIFFERENCE CELL
	GAGING SITE	$H_n$	HYDRAULIC HEAD ON THE CONSTANT-HEAD SIDE OF THE HEAD-DEPENDENT BOUNDARY
$A_n$	AREA OF THE WATER-BODY BED WITHIN THE FINITE-DIFFERENCE CELL	$h_n$	CALCULATED HYDRAULIC HEAD FOR CELL $n$

Figure 9.--Representation of head-dependent boundary gain and loss observations: A, gaging sites and cells used to represent the reach between gaging sites in the model; and B, quantities used to calculate the simulated gain or loss.

There are exceptions to equation (4) in some of the model packages. In the River and Streamflow-Routing Packages, if  $h_i$  declines below the bottom of the riverbed or streambed, the flow at cell  $i$  is calculated as (figure 10A and 10C):

$$q_i = \frac{K_i}{D_i} A_i (H_i - E_i) \quad (5)$$

where  $E_i$  is the elevation of the bottom of the streambed. In the Drain Package, if  $h_i$  declines below the bottom of the drain,  $q_i=0$  (no flow is simulated between the ground-water system and the drain, as shown in figure 10B). The Streamflow-Routing Package also has the exception that if the calculated loss from a reach exceeds the flow into that reach, the loss is set equal to the flow into the reach.

The exceptions noted above result in the elimination of  $h_i$  from the calculated head-dependent boundary gains and losses, and decrease the importance of the observed gain or loss to the estimation of parameters. In the extreme, an observation might have no affect on parameter estimation, in which instance the observation is omitted for the parameter-estimation iteration being executed. Messages are printed in the output from the Parameter-Estimation Package when the exceptions listed above occur and when an observation is omitted.

#### Dry Cells in Water-Table Layers at Observation Locations

When the hydraulic head at a cell in a water-table layer declines below the bottom of the aquifer, the cell is designated as inactive and remains inactive through the last time step (McDonald and Harbaugh, 1988, p. 5-9). Such cells are said to 'go dry'. At a dry cell, hydraulic head is not calculated, and the cell cannot be used to calculate simulated hydraulic heads or head-dependent boundary gains and losses for the parameter-estimation iteration. For head-dependent boundary reaches this generally poses little problem because cells along the reaches do not tend to go dry as often as other cells. When they do go dry, these cells usually account for only a fraction of a reach. No special provisions have been made in the Parameter-Estimation Package to account for cells going dry along head-dependent boundary reaches with observed gains or losses.

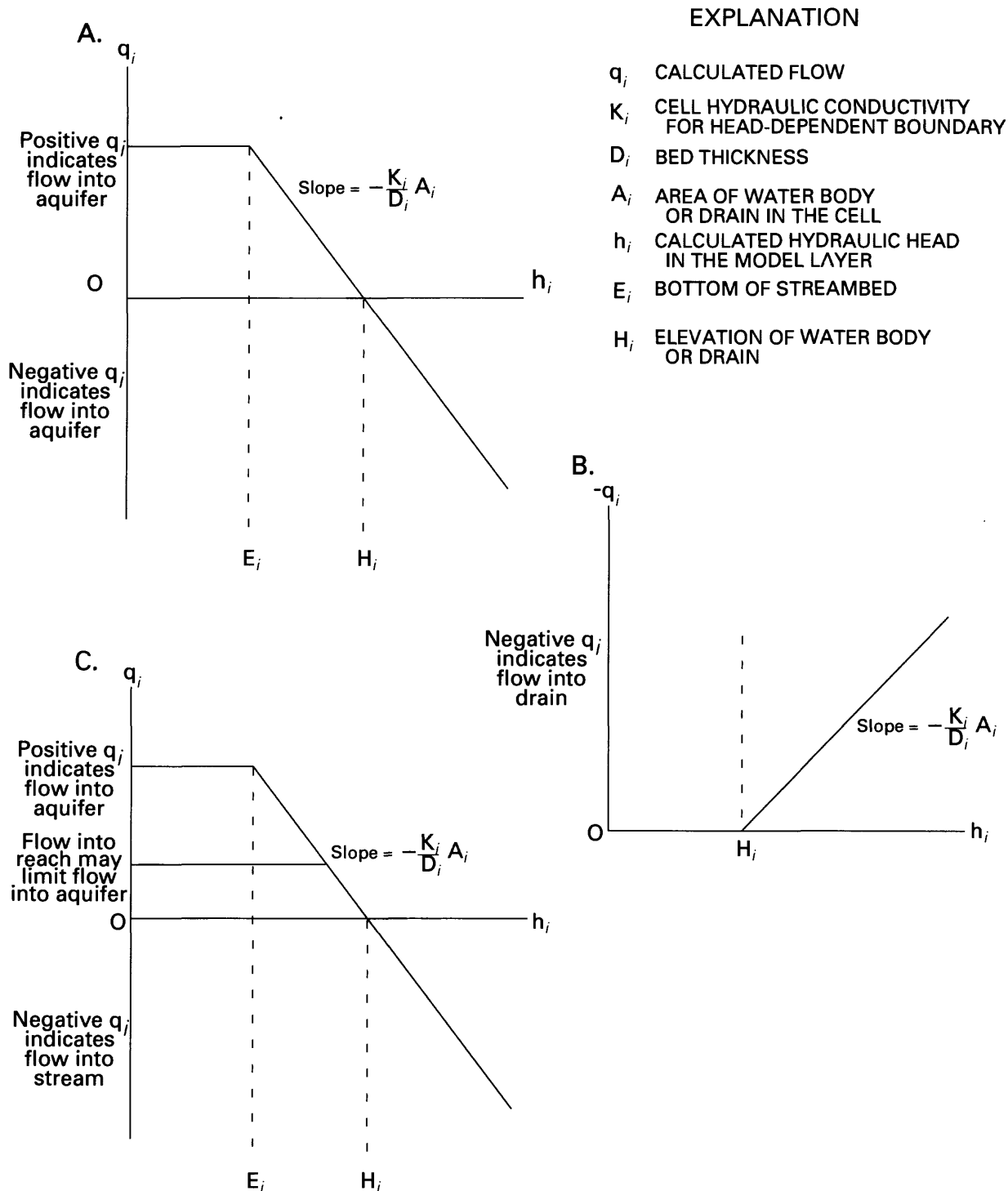


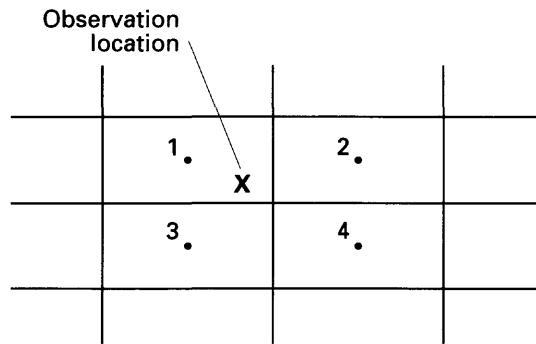
Figure 10.--The dependence of simulated gains and losses on hydraulic head in the model layer ( $h_i$ ) in: A, the River Package, B, the Drain Package, and C, the Streamflow-Routing Package.

Problems are more severe when cells go dry at or adjacent to hydraulic-head observation locations. There are three types of problems, as shown in figure 11. First, if the observation is single layer and an adjacent cell which is used in the interpolation method discussed earlier goes dry, the dry cell usually can be omitted from the interpolation without introducing too much error into the interpolated value. This procedure was adopted in the Parameter-Estimation Package. Second, if the observation is multilayer and cells used for interpolation in one or more layers go dry, the proportions used to weight the hydraulic heads from those layers probably are no longer valid. Although the cells could be omitted from the interpolation for the layers involved and a simulated hydraulic head analogous to the observed value could be calculated, the problem with the proportions can not easily be resolved. In the Parameter-Estimation Package, multilayer observations for which any cells used in the interpolation go dry are omitted from the parameter-estimation procedure. Third, if the observation is single layer or multilayer and the cell containing the observation location goes dry in any of the layers involved, the observation is omitted from the parameter-estimation procedure. The effect of omitting the observations for the last two situations is that the impetus for changing the parameters to keep the dry areas wet is lost from the parameter-estimation procedure. This loss is unfortunate, but, at this point, no practical alternative exists.

As discussed previously in the section "Ground-water flow equation", the Parameter-Estimation Package reactivates all dry cells at the beginning of each parameter-estimation iteration, so that the original interpolation and number of observations are reinstated.

#### Omitted Observations

If observations are alternately used and omitted and used again in successive parameter-estimation iterations, which might occur for hydraulic-head observations in water-table layers that go dry and for head-dependent boundary gain and loss observations, parameter estimation might not converge (see the section "The Sum-of-Squares Objective Function in Nonlinear Problems" for a discussion of parameter-estimation iterations and convergence). This problem can be addressed in the following ways:



Situation 1: Single-layer simulation; cells 2, 3, and(or) 4 go dry; recalculate interpolation.

Situation 2: Multilayer simulation; cells 2, 3, and(or) 4 go dry in any layer; omit observation from parameter-estimation procedure.

Situation 3: Single or multilayer simulation; cells 1 goes dry in any layer; omit observation from parameter-estimation procedure.

Figure 11.--Effect of dry cells on calculated hydraulic head at an observation location.

1. Eliminate the omitted observations during initial parameter estimation iterations or early in the calibration process, and try including them later when the parameter estimates are closer to the final values or the model is closer to its final form.
2. A water-table layer can be simulated as a confined layer using estimated layer thicknesses early in the calibration process, and represented as a water-table layer later when the parameter estimates are closer to the final values or the model is closer to its final form.
3. For head-dependent boundary gain-and-loss observations, small streambed or riverbed thicknesses can aggravate the problem. Increase these thicknesses if such a change is realistic.
4. Review the method used to represent the ground-water flow system and make changes if needed. This is the same process that a modeler goes through in a trial-and-error calibration, and its goal is to ensure that the physical system is being represented realistically. Unrealistic representations cause problems in nonlinear-regression parameter estimation just as they cause problems when calibrating by trial and error.

# REVIEW OF PARAMETER ESTIMATION AND ANALYSIS OF RESULTS USING LINEAR REGRESSION

A brief review of linear regression is included to provide an easier framework within which to present the concepts. Although this review is brief, extensive discussions are available in Draper and Smith (1981) and Cooley and Naff (1990), from which much of the following discussion is condensed. For the less advanced reader, Ott (1988) provides a more elementary discussion.

## Assumed Linear Model

In any type of regression procedure, a model structure needs to be assumed. In linear regression, the assumed model can be expressed as a linear function of the parameters. This assumed model is correct if the true process is a linear function of the parameters. For example,

$$\tilde{y} = \beta_1 x_1 + \beta_2 x_2 + \cdots + \beta_{NP} x_{NP} \quad (6)$$

where  $\tilde{y}$  is the true calculated dependent variable (analogous, for example, to hydraulic head in the ground-water flow equation);

$NP$  is the number of parameters;

$\beta_1 \beta_2 \cdots \beta_{NP}$  are true, unknown parameter values; and

$x_1, x_2 \cdots x_{NP}$  are independent variables (analogous to spatial dimensions and time in the ground-water flow equation). These might be functions of dependent variables in some applications.

The parameters  $\beta_1, \beta_2 \cdots \beta_{NP}$  are unknown, but can be estimated from observations,  $y_q$ , which are observed at different values of the independent variables. The data would be as follows:

$$(y_1, x_{1,1}, x_{1,2}, \cdots x_{1,NP}), (y_2, x_{2,1}, x_{2,2}, \cdots x_{2,NP}), \quad (7) \\ \cdots (y_{ND}, x_{ND,1}, x_{ND,2}, \cdots x_{ND,NP}),$$

where the added subscripts indicate the sequential number of the observation, and  $ND$  is the total number of observations. Note that the first subscript on each independent variable,  $x_{q,i}$ , is the observation



number, and the second is the number of the parameter it multiplies. These data can be substituted into the model (eq. 6) to produce ND equations of the form

$$y_q = \tilde{y}_q + \epsilon_q = \beta_1 x_{q,1} + \beta_2 x_{q,2} + \cdots \beta_{NP} x_{q,NP} + \epsilon_q \quad q = 1, ND \quad (8)$$

where  $\epsilon_q$  is the difference between observation  $y_q$  and the surface predicted by the true model, and is called the true error or disturbance.

The ND equations of (8) can be expressed using vectors and matrices as:

$$\underline{y} = \underline{X} \underline{\beta} + \underline{\epsilon} \quad (9)$$

where

$$\underline{y} = \begin{Bmatrix} y_1 \\ y_2 \\ \vdots \\ y_{ND} \end{Bmatrix}, \quad \underline{X} = \begin{bmatrix} x_{1,1} & x_{1,2} & \cdots & x_{1,NP} \\ x_{2,1} & x_{2,2} & \cdots & x_{2,NP} \\ \vdots & \vdots & \ddots & \vdots \\ x_{ND,1} & x_{ND,2} & \cdots & x_{ND,NP} \end{bmatrix}, \quad \underline{\beta} = \begin{Bmatrix} \beta_1 \\ \beta_2 \\ \vdots \\ \beta_{NP} \end{Bmatrix},$$

$$\underline{\epsilon} = \begin{Bmatrix} \epsilon_1 \\ \epsilon_2 \\ \vdots \\ \epsilon_{ND} \end{Bmatrix}.$$

The elements of  $\underline{\epsilon}$  are assumed to be random variables, and the validity of the regression procedure depends on their statistical properties. It is generally assumed that (1)  $E(\underline{\epsilon}) = \underline{0}$ , so that the model is unbiased (Benjamin and Cornell, 1970, p. 380) and (2) the variance-covariance matrix of the errors is  $V(\underline{\epsilon}) = \underline{I} \sigma^2$ , so that the elements of  $\underline{\epsilon}$  are uncorrelated and have equal variances (Draper and Smith, 1981, p. 108). Violations of the second assumption need to be accounted for by using a weight matrix, as discussed in the section "Weighting Observations".

### Parameter Estimation by Least-Squares Regression

The goal of regression is to determine estimates,  $\underline{b}$ , of the true, unknown parameter values,  $\underline{\beta}$ , so that an assumed model that approximates the true model produces calculated values,  $\hat{y}_q$ , at the observation points  $q$ , which are similar to the measured values,  $y_q$ , as measured by an objective function. Replacing  $\underline{\beta}$  with  $\underline{b}$  in equation (9) yields:

$$\underline{y} = \underline{X} \underline{b} + \underline{e} = \hat{\underline{y}} + \underline{e} \quad (10)$$

where  $\hat{\underline{y}}$  is a vector of calculated values of  $y$  and  $\underline{e}$  is a vector of residuals. The variable  $\underline{e}$  is used instead of  $\underline{\epsilon}$  to clearly indicate that the components of  $\underline{e}$  are not true errors. The elements of  $\underline{e}$  are random variables and have statistical properties that are consistent with the statistical properties of the elements of  $\underline{\epsilon}$  if the assumed model is similar to the true model.

Two objective functions commonly are used in ground-water flow parameter-estimation problems, but both reduce to the sum-of-squares objective function for any single run of the parameter-estimation procedure. The maximum-likelihood objective function is discussed in the section "Parameter Estimation and Analysis of Results Using Nonlinear Regression".

The sum-of-squares objective function is defined as:

$$\begin{aligned} S(\underline{b}) &= \sum_{q=1}^{ND} [y_q - \hat{y}_q]^2 \\ &= \sum_{q=1}^{ND} [y_q - (b_1 x_{q,1} + b_2 x_{q,2} + \dots + b_{NP} x_{q,NP})]^2 \\ &= [\underline{y} - \underline{X} \underline{b}]^T [\underline{y} - \underline{X} \underline{b}] \\ &= \underline{e}^T \underline{e}, \end{aligned} \quad (11)$$

where  $S(\underline{b})$  is a scalar, and  $\underline{e}$  is the vector of residuals. A regression problem solved using a sum-of-squares objective function is called a least-squares regression problem.

A plot of a sum-of-squares objective-function surface for a problem with two parameters,  $b_1$  and  $b_2$ , is shown in figure 12. For linear problems, the contours are elliptic, and the minimum  $S(\underline{b})$  value usually is well-defined and unique. The parameter values that produce the minimum objective-function value can be calculated by solving  $\partial S(\underline{b})/\partial \underline{b} = \underline{0}$ , which is equivalent to:

$$\frac{\partial S(\underline{b})}{\partial b_1} = 0, \quad \frac{\partial S(\underline{b})}{\partial b_2} = 0, \quad \dots \quad \frac{\partial S(\underline{b})}{\partial b_{NP}} = 0. \quad (12)$$

The minimum is called a stationary point because all the derivatives in equation (12) equal zero. Objective functions of nonlinear models can have other types of stationary points, such as maxima or inflection points (Hildebrand, 1976, p. 356-362), or relative and absolute minima. Various kinds of stationary points, in addition to alternative terminology that commonly is used to describe them, are shown in figure 13. A problem with a well-defined, unique minimum and no other stationary points on the objective-function surface is said to be well-conditioned. Although this concept can be graphically displayed only in a one- or two-dimensional parameter space, it applies for any number of parameters.

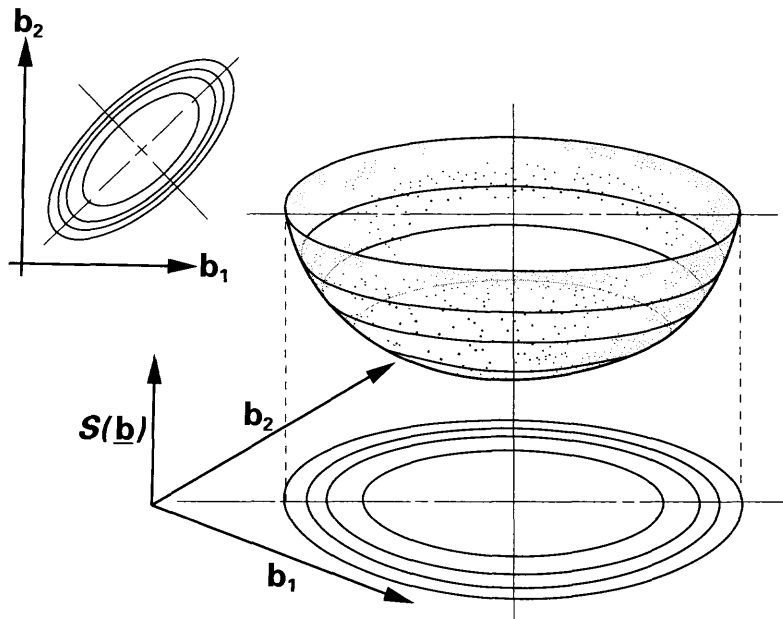


Figure 12.--Sum-of-squares objective-function surface for a linear problem with parameters  $b_1$  and  $b_2$  (modified from Himmelblau, 1972, p. 80; used with permission of the publisher).

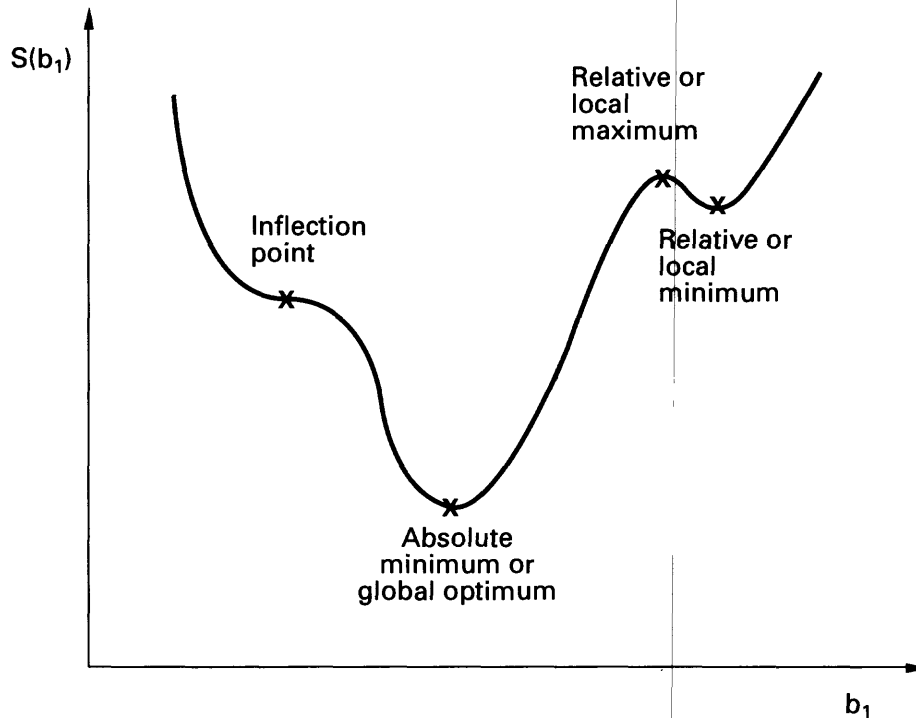


Figure 13.--Stationary points on an objective-function surface, labeled using common terminology (modified from McLaughlin, 1975, p. III-4).

In linear regression, the sensitivities, which are defined as the derivative of the calculated dependent variable,  $\hat{y}$ , with respect to the parameters, are required to calculate the  $\underline{b}$  that satisfies equation (12). The linear model is easy to use because the sensitivities are independent of the parameter values. From equation (6):

$$\frac{\partial \hat{y}}{\partial \beta_1} = x_1, \quad \frac{\partial \hat{y}}{\partial \beta_2} = x_2, \quad \dots \quad \frac{\partial \hat{y}}{\partial \beta_{NP}} = x_{NP}. \quad (13)$$

Substituting the parameter estimates,  $\underline{b}$ , for the true parameters,  $\underline{\beta}$ , sensitivities at observation-point  $q$  equal:

$$\frac{\partial \hat{y}_q}{\partial b_1} = x_{q,1}, \quad \frac{\partial \hat{y}_q}{\partial b_2} = x_{q,2}, \quad \dots \quad \frac{\partial \hat{y}_q}{\partial b_{NP}} = x_{q,NP}. \quad (14)$$

Note that  $\underline{X}$  of equations (9) and (10) is a matrix of sensitivities, and for linear problems simply equals the values of  $x_{q,1}$ ,  $x_{q,2}$ , .... When the model is nonlinear in the parameters, such as in most ground-water flow problems,  $\underline{X}$  is still a matrix of sensitivities and has the same function in the following equations. The sensitivities, however, are not as easy to calculate and they are dependent on the parameter values.

To proceed, consider a linear problem with a two-parameter model equation, and  $x_{q,1}=1$ ,  $q=1, ND$ , so the assumed model is a straight line with intercept  $b_1$  and slope  $b_2$ . Equation (12) can be solved to produce the following well-known equations, called the normal equations, for  $b_2$  and  $b_1$ :

$$b_2 = \frac{\sum x_{q,2} y_q - [(\sum x_{q,2})(\sum y_q)]/ND}{\sum x_{q,2}^2 - (\sum x_{q,2})^2/ND}, \quad (15)$$

$$b_1 = (\sum y_q)/ND - b_2(\sum x_{q,2})/ND,$$

where the summations are for the ND observations.

Using the matrix notation of equation (9), equation (15) is the solution of:

$$\underline{X}^T \underline{X} \underline{b} = \underline{X}^T \underline{y} \quad (16)$$

where, for the simple linear problem with two parameters,

$$\underline{X} = \begin{bmatrix} 1 & x_{1,2} \\ 1 & x_{2,2} \\ \vdots & \vdots \\ 1 & x_{ND,2} \end{bmatrix}.$$

Then,

$$\underline{X}^T \underline{X} = \begin{bmatrix} ND & \sum x_{q,2} \\ \sum x_{q,2} & \sum (x_{q,2})^2 \end{bmatrix}, \text{ and}$$

$$\underline{X}^T \underline{y} = \begin{bmatrix} \sum y_q \\ \sum x_{q,2} y_q \end{bmatrix},$$

where, again, the summations are for the ND observations. By using these definitions, it can easily be verified that equations (15) and (16) are

equivalent. Regardless of the dimensions or linearity of the problem, all least-squares regression problems are solved using normal equations of the form of equation (16).

### Weighting Observations

If the observations used in a regression analysis are (1) not equally reliable, (2) have different units, or (3) have true errors that are correlated, it cannot be assumed that the true errors have the statistical properties required to produce a valid regression even if the assumed model is correct--that is, although  $E(\epsilon) = 0$  is still valid, it cannot be assumed that the variance-covariance matrix of the true errors  $\underline{V}(\epsilon)$ , satisfies  $\underline{V}(\epsilon) = I\sigma^2$  (Draper and Smith, 1981, p. 108). As a result, the residuals used in the regression procedure need to be weighted.

Before proceeding, consider the three conditions for which weighting is required and the function the weights have in the regression for each of these conditions. Observations might not be equally reliable if, for example, they are observed with varying degrees of accuracy. In ground-water flow problems, this variability might occur if the elevations of some observation wells were determined by standard surveying methods to within a few hundredths of a foot, whereas the elevations of other observation wells were determined by an altimeter or from a topographic map to within a few feet. When performing regression with such observations, it is more important for hydraulic-head residuals to be smaller at locations with more accurate elevations than at locations with less accurate elevations, and weights are assigned that indicate this variation in importance. Observations have different units if, for example, both hydraulic heads (L) and streamflow gains and losses ( $L^3/T$ ) are observed. Weights are used to indicate that a difference of, for example, 1.0, between the observed and simulated values for the two types of observations are not equivalent, to indicate variations in observation accuracy, or both. True errors would be correlated if, for example, hydraulic head at the same well was observed at many times, and errors in determining the elevation or position of the well were common to all observations. Weighting then is used to indicate that the errors associated with those observations are correlated.

It is important to note that model error generally cannot be represented in the weight matrix. If the form and affect of model error can be evaluated, the data can be adjusted accordingly. For example, if a well penetrates only part of a pumped aquifer and the entire aquifer is represented as a model layer, the affects of partial penetration can be evaluated and the observations corrected to reflect full penetration. As the estimated transmissivity near the well changes during the calibration process, the correction can be recalculated.

#### Structure and Use of the Weight Matrix

Weighting is implemented by using a symmetric weight matrix,  $\underline{\omega}$ , that ideally would be calculated from the variance-covariance matrix of the true errors,  $\underline{V}(\underline{\epsilon})$ , as:

$$\underline{\omega} = \sigma^2 [\underline{V}(\underline{\epsilon})]^{-1}, \quad (17)$$

where  $\sigma^2$  is the user-defined common error variance of the true errors (see below). In practice,  $\underline{V}(\underline{\epsilon})$  is unknown. Its estimate,  $\hat{\underline{V}}(\underline{\epsilon})$ , is estimated by the user, and the estimated weight matrix,  $\hat{\underline{\omega}}$ , is calculated from  $\hat{\underline{V}}(\underline{\epsilon})$  as in equation (17). If  $\hat{\underline{\omega}}$  approximately equals  $\underline{\omega}$ , the weighted true errors satisfy the desired conditions,  $E(\hat{\underline{\omega}}^{\frac{1}{2}} \underline{\epsilon}) = \underline{0}$  and  $\underline{V}(\hat{\underline{\omega}}^{\frac{1}{2}} \underline{\epsilon}) = \underline{I} \sigma^2$ . If, in addition, the model is correct,  $\sigma^2$  approximately equals the estimated error variance,  $s^2$ , which is calculated as the minimized value of the objective function divided by ND-NP (divide by ND+NPR-NP if there are prior parameter estimates; see "Prior Information on Estimated Parameters"). The square root of  $s^2$  is called the standard error of estimate (Draper and Smith, 1981, p. 207). Discrepancies between  $\sigma^2$  and  $s^2$  indicated an incorrect model, an incorrect weight matrix, or biased observations; see "Adjustments Commonly Required During Parameter Estimation".

In weighted least-squares regression, the weighted residuals,  $\hat{\underline{\omega}}^{\frac{1}{2}} \underline{e}$ , replace the unweighted residuals,  $\underline{e}$ . The weighted residuals might be dimensionless or might have the units of any of the dependent variables, depending on how the modeler defines  $\sigma^2$ . The weighted sum-of-squares objective function (eq. 11) is:

$$S(\underline{b}) = \underline{e}^T (\hat{\underline{\omega}}^{\frac{1}{2}})^T \hat{\underline{\omega}}^{\frac{1}{2}} \underline{e} = \underline{e}^T \hat{\underline{\omega}} \underline{e}. \quad (18)$$

The weighted normal equations (eq. 16) are:

$$\underline{X}^T \hat{\underline{\omega}} \underline{X} \underline{b} - \underline{X}^T \hat{\underline{\omega}} \underline{y}. \quad (19)$$

If all observations have the same units (for example, if all observations are hydraulic heads), the user can define a  $\sigma^2$  such that the variance-covariance matrix of the true errors can be expressed as:

$$\underline{V}(\underline{\epsilon}) = \sigma^2 \underline{W}, \quad (20)$$

where  $\underline{W}$  is an ND by ND matrix and either  $\sigma^2$  or  $\underline{W}$  is dimensionless. Then, by equation (17):

$$\underline{\omega} = \sigma^2 (\sigma^{-2} \underline{W}^{-1}) = \underline{W}^{-1}. \quad (21)$$

The estimated matrix,  $\hat{\underline{\omega}}$ , would be of the same form. In this situation, the weight matrix and, thus, the parameter estimates produced by the regression routine are independent of the common variance, and the criterion that  $\sigma^2 \approx s^2$  is always satisfied. If  $\underline{W}$  is considered to be dimensionless, the units of the weighted residuals are the same as the units of the observations.

If there are observations with two different kinds of units (for example, if hydraulic heads and streamflow gains and losses are observed) and if it is assumed that the true errors of the two kinds of observations are statistically independent (this will be discussed in the section "Simplifying Assumptions"), the variance-covariance matrix of the true errors can be expressed as:

$$\underline{V}(\underline{\epsilon}) = \begin{bmatrix} \underline{W} \sigma_h^2 & \underline{0} \\ \underline{0} & \underline{Z} \sigma_f^2 \end{bmatrix}, \quad (22)$$

where  $\underline{W} \sigma_h^2$  is the variance-covariance matrix of errors in observed hydraulic heads and temporal changes in hydraulic head ( $\underline{\epsilon}_h$ ), and  $\underline{Z} \sigma_f^2$  is the variance-covariance matrix for errors in observed head-dependent boundary gains and losses ( $\underline{\epsilon}_f$ ). Generally,  $\sigma^2$  is defined to be equal to either  $\sigma_h^2$  or  $\sigma_f^2$  or 1.0. If  $\sigma^2$  equals  $\sigma_h^2$ , the weight matrix equals:



$$\underline{\omega} = \sigma_h^2 (\underline{V}(\underline{\epsilon}))^{-1} = \begin{bmatrix} \underline{W}^{-1} & \underline{0} \\ \underline{0} & \underline{Z}^{-1} \frac{\sigma_h^2}{\sigma_f^2} \end{bmatrix}. \quad (23)$$

Again, the estimated matrix,  $\hat{\underline{\omega}}$ , would be of the same form. The weight matrix and the parameter estimates produced by the regression routine are affected by the ratio  $\sigma_h^2/\sigma_f^2$ , and, if  $\underline{W}$  is dimensionless, the weighted residuals have the same units as the hydraulic-head observations. If  $\sigma_f^2$  is defined as the common error variance, the ratio  $\sigma_f^2/\sigma_h^2$  affects the regression routine, and, if  $\underline{W}$  is dimensionless, the weighted residuals have the same units as the head-dependent boundary gain-and-loss observations.

If  $\sigma^2$  is set equal to 1.0 and is dimensionless,  $\underline{\omega} = [\hat{\underline{V}}(\underline{\epsilon})]^{-1}$ , and the residuals are dimensionless. In this situation, if the model and  $\hat{\underline{V}}(\underline{\epsilon})$  are correct,  $s^2$  is close to 1.0.

If the true errors are all uncorrelated, the nonzero entries in  $\underline{V}(\underline{\epsilon})$ , and therefore in  $\underline{\omega}$  and  $\hat{\underline{\omega}}$ , occur on the diagonal. A diagonal weight matrix is conceptually and computationally simple, and only diagonal weight matrices are allowed in the Parameter-Estimation Package. However, a data transformation described in the following sections can be used so that some types of temporal correlations of the true errors can be included.

## Estimation of the Variance-Covariance

### Matrix of the True Errors

In transient ground-water flow problems, various dependent variables might be observed at many locations, and they might be observed at many times. The most general variance-covariance matrix of the true errors would include the following correlations: (1) Correlations between errors in observations made at different locations at the same time; (2) correlations between errors in observations made at the same location at different times; and (3) correlations between errors in observations made at different locations and different times. Such a matrix would be impossible to estimate accurately, and laborious to estimate at all. Fortunately, assumptions about the true errors that are realistic for many circumstances can be made to simplify this variance-covariance matrix. Seven assumptions

that result in a simple diagonal weight matrix are listed below and are further defined and discussed in the following section. Their validity also is noted in both parts of the text. This set of assumptions is not unique. They are presented so that one set of assumptions leading to a diagonal weight matrix can be thoroughly analyzed. The role of both measurement error and model error is included in the discussion because both commonly plague the development of ground-water flow models.

1. True error includes measurement errors and generally excludes model errors.
  - Required for a valid regression
2. Errors of different kinds of dependent variables are uncorrelated.
  - Commonly realistic for measurement errors
3. Errors of observations at different locations are uncorrelated.
  - Commonly realistic for measurement errors
4. Time-dependent deterministic components of the error are small and can be ignored.
  - Commonly realistic for measurement errors
5. At each observation location, total error for any observation =  $\epsilon_1 + \epsilon_2 + \epsilon_3$ .
  - $\epsilon_1$  = errors that are constant over time
  - $\epsilon_2$  = errors that are temporarily correlated, but not completely correlated like  $\epsilon_1$
  - $\epsilon_3$  = errors that are temporarily uncorrelated
    - Probably realistic
6. Errors are normally distributed.
  - Probably realistic
7. Either  $\epsilon_1$  or  $\epsilon_2$  or  $\epsilon_3$  errors dominate.
  - Commonly questionable

#### Simplifying assumptions

The first assumption is that the error includes measurement errors and generally excludes model errors. The sum of all measurement errors equals the  $\epsilon_q$  of equation (8); model errors are any errors that could be corrected by changes in the model given greater computer capacity, more time, or more complete information about the ground-water flow system. Measurement errors include, for example, errors in the elevation of observation wells and errors in observed streamflow. Model errors are caused by, for example,

inaccurate interpolation of calculated hydraulic heads and other problems discussed in the section "Observations" of this report, inability of the model to represent ground-water flows or fluctuations in ground-water properties that are smaller than the grid size, and parameterizations that artificially limit the spatial or temporal variability of parameters. The restrictions of the last example generally are necessary because only a limited number of parameters can be estimated, but they do produce model errors. The first assumption is required for a valid regression, and one of the goals during calibration is to reduce model error as much as possible. Model error generally cannot be accommodated using the weight matrix.

The second assumption is that errors in different kinds of dependent variables are uncorrelated. This is the assumption that was made to produce the weight matrix of equation (22), and indicates, for example, that errors in observed hydraulic heads are independent of errors in observed streamflow gains and losses. This assumption is realistic for measurement errors; for example, it is unlikely that errors incurred when observing hydraulic heads are related to errors incurred when observing streamflow. This assumption, however, might not be realistic for model errors; for example, simulated hydraulic heads and adjacent simulated streamflows generally would be affected by the same deficiencies in the model, and associated model errors would be correlated.

The third assumption is that errors in observations at different locations are uncorrelated. As with the second assumption, the third assumption is realistic for most measurement errors, but might not be realistic for model errors, especially at locations that are close to one another (Carrera, 1984, p. 37-39). One exception occurs for measurement errors of head-dependent boundary gains and losses when one flow measurement is used to calculate more than one gain or loss. For example, if flow is measured at three progressively downstream locations as  $Q_1$ ,  $Q_2$ , and  $Q_3$ , the gain or loss measurements will equal  $Q_2 - Q_1$ , and  $Q_3 - Q_2$ . If the errors in  $Q_1$ ,  $Q_2$ , and  $Q_3$  are independent, normal, and have variances equal to  $\sigma_1^2$ ,  $\sigma_2^2$ , and  $\sigma_3^2$ , the error in  $Q_2 - Q_1$  has a variance equal to  $\sigma_1^2 + \sigma_2^2$ , the error in  $Q_3 - Q_2$  has a variance equal to  $\sigma_2^2 + \sigma_3^2$ , and the covariance between the two gain-and-loss measurements equals  $-\sigma_2^2$ .

If valid, the result of the second and third assumptions is that all correlations are eliminated except for the temporal correlations at each location.

The fourth assumption is that time-dependent deterministic components of the error (Brockwell and Davis, 1987, p. 15) are small and can be ignored. Such components are more typical of model error than measurement error, so the fourth assumption probably is realistic for measurement errors.

The fifth assumption is that the remaining correlations of the true errors, which are temporal, can be categorized by thinking of the error associated with each observation at a single time and location as the sum of three statistically independent types of errors:

$$\epsilon = \epsilon_1 + \epsilon_2 + \epsilon_3, \quad (24)$$

where,  $\epsilon_1$  is constant for all time for each observation location, so the temporal correlation coefficients between this error and the errors associated with observations at other times at this location equal 1.0;

$\epsilon_2$  varies with time and has correlation coefficients between this error and the errors associated with observations at other times at this location between 0.0 and 1.0, exclusive; and

$\epsilon_3$  varies independently over time and has correlation coefficients between this error and the errors associated with observations at other times at this location equal to zero.

Examples of observations with these types of errors are shown in figure 14. Considering their definitions, the assumed independence of  $\epsilon_1$ ,  $\epsilon_2$ , and  $\epsilon_3$  is realistic, and this method of characterizing errors probably is valid for all ground-water flow models. The autocorrelated temporal errors considered by Sadeghipour and Yeh (1984), Carrera and Neuman (1986a, p. 203), and Watson and others (1990a,b) would be classified as  $\epsilon_2$ , as defined above. Lu and others (1988, p. 675) introduced a constant error similar to  $\epsilon_1$  to describe spatial correlations of errors in an estimated transmissivity field.

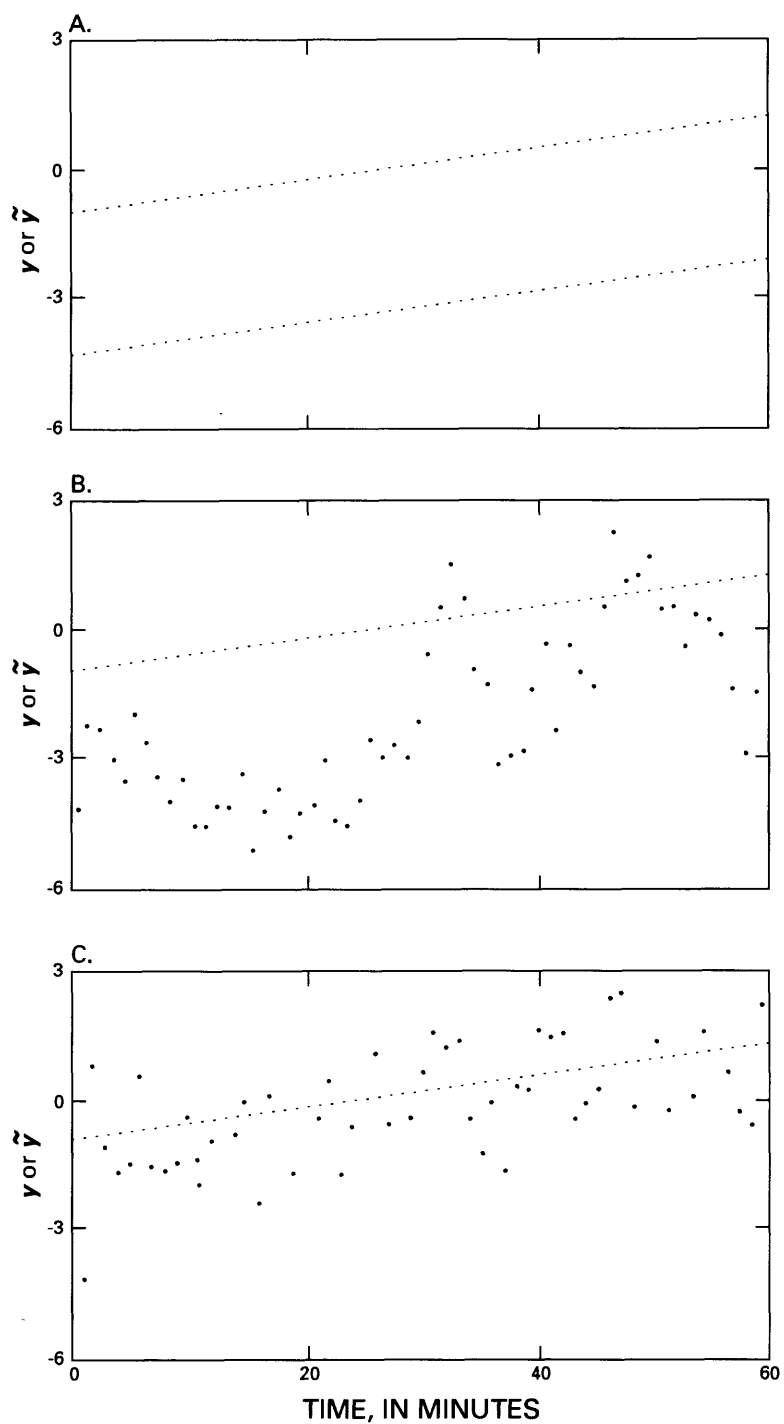


Figure 14. Paired observed and true values for which the errors,  $y - \tilde{y}$ , are (A)  $\epsilon_1$  errors, (B)  $\epsilon_2$  errors, and (C)  $\epsilon_3$  errors.

Processes that are likely to produce the three error types are different for measurement errors and model errors. For measurement errors,  $\epsilon_1$  might be the error in the measured elevation of the well;  $\epsilon_2$  might be an autocorrelated error in the recording device; and  $\epsilon_3$  might be random, uncorrelated inaccuracy in the recording device. From a practical viewpoint,  $\epsilon_1$  and  $\epsilon_3$  errors probably dominate measurement errors. For model errors,  $\epsilon_1$  might be the error produced because constant pumpage at a well near the observation location is not accounted for in the model;  $\epsilon_2$  might be the error produced because the parameterization of transmissivity is not realistic; and  $\epsilon_3$  errors probably would be small or equal to zero.

When written for a series of observations over time at an arbitrary observation location  $l$ , equation (24) becomes:

$$\underline{\epsilon}_l = \underline{\epsilon}_{1l} + \underline{\epsilon}_{2l} + \underline{\epsilon}_{3l}, \quad (25)$$

where the length of each vector equals the number of temporal measurements at observation location  $l$ . If only temporal correlations are nonzero and the observations are ordered by location,  $\underline{V}(\underline{\epsilon})$  is a block-diagonal matrix with the size of the blocks equal to the length of the vectors in equation (25), which might be different for different locations.

The variance-covariance matrices associated with the  $\epsilon_1$  and  $\epsilon_3$  errors have structures determined by their definitions.  $\underline{V}(\underline{\epsilon}_{1l})$  is a matrix with all elements equal to the variance of the error. Thus,  $\underline{V}(\underline{\epsilon}_{1l}) = \underline{1} \sigma_{1l}^2$ , where  $\underline{1}$  is a matrix of ones and  $\sigma_{1l}^2$  is the error variance associated with observation location  $l$ .  $\underline{V}(\underline{\epsilon}_{1l})$  can be simplified if changes in the dependent variable over time are used in the regression instead of the actual values. For example, if hydraulic head is observed multiple times at one location, the first observation would be the initial hydraulic head, and subsequent observations would be changes from that initial hydraulic head. Because the  $\epsilon_1$  error is considered to be constant over time, it would be included only in the initial observation; the subtraction would eliminate this error from subsequent observations. Thus, by this simple transformation,  $\underline{V}(\underline{\epsilon}_{1l})$  would have one nonzero variance equal to  $\sigma_{1l}^2$  associated with the first observation at observation location  $l$ , and all

other variances and covariances in the matrix would equal zero. To invert this matrix to calculate  $\underline{\omega}$ , the zero diagonal elements would have to be replaced by small, nonzero values.

$\underline{V}(\underline{\epsilon}_{3\ell})$  is a diagonal matrix because the  $\epsilon_3$  errors are uncorrelated. If, in addition, these errors are thought to have the same variance,  $\underline{V}(\underline{\epsilon}_{3\ell}) = \underline{I} \sigma_{3\ell}^2$ , where  $\underline{I}$  is the identity matrix and  $\sigma_{3\ell}^2$  is the error variance. Under the transformation discussed above for  $\epsilon_1$  errors,  $\underline{V}(\underline{\epsilon}_{3\ell})$  becomes more complicated. The variance associated with the first observation at observation location  $\ell$  remains unchanged, but the covariances associated with the first observation equal  $-\sigma_{3\ell}^2$ , all other covariances equal  $\sigma_{3\ell}^2$ , and all other variances equal  $2\sigma_{3\ell}^2$ .

The variance-covariance matrix of the  $\epsilon_2$  errors depends on the correlation between the errors. If the correlation can be expressed by an autoregressive process (Brockwell and Davis, 1987, p. 79) and the observations are made at equally spaced times, differencing can be used to produce an independent set of observations and a diagonal variance-covariance matrix. Sadegui pour and Yeh (1984) use differencing of a one-step autoregressive process and apply it to parameter estimation in a ground-water flow problem.

The sixth assumption is that the sources of error are numerous and varied enough that, by the central-limit theorem (Benjamin and Cornell, 1970, p. 251-253), the joint probability distribution function (pdf) of the errors of equation (25) are normal, so:

$$\underline{\epsilon}_\ell \sim N[\underline{0}, \underline{V}(\underline{\epsilon}_\ell)] = N[\underline{0}, \underline{V}(\underline{\epsilon}_{1\ell}) + \underline{V}(\underline{\epsilon}_{2\ell}) + \underline{V}(\underline{\epsilon}_{3\ell})], \quad (26)$$

where  $\sim$  means "distributed as", and the three variance-covariance matrices are summable because of the assumed normality and independence of  $\underline{\epsilon}_{1\ell}$ ,  $\underline{\epsilon}_{2\ell}$ , and  $\underline{\epsilon}_{3\ell}$ . By using the expressions for  $\underline{V}(\underline{\epsilon}_{1\ell})$  and  $\underline{V}(\underline{\epsilon}_{3\ell})$  described above (assuming all  $\epsilon_3$  errors have the same variance), the joint pdf can be expressed as:

$$\epsilon_{\ell} \sim N[0, \underline{1} \sigma_{1\ell}^2 + \underline{V}(\epsilon_{2\ell}) + \underline{1} \sigma_{3\ell}^2]. \quad (27)$$

The sixth assumption probably is realistic for all ground-water flow problems.

If changes in the dependent variable were considered,  $\underline{1} \sigma_{1\ell}^2$  would be simplified further, but  $\underline{1} \sigma_{3\ell}^2$  would become more complicated, as discussed above. If  $\sigma_{3\ell}^2$  is small compared to  $\sigma_{1\ell}^2$ , an approximate diagonal matrix with the first variance equal to  $\sigma_{1\ell}^2$  and variances for subsequent observations equal to  $2\sigma_{3\ell}^2$  can produce valid regression results. If  $\epsilon_2$  errors are important and autoregressive, and the times between observations are constant, differencing methods can be used to make  $\underline{V}(\epsilon_{2\ell})$  diagonal. However,  $\underline{V}(\epsilon_{1\ell})$  and  $\underline{V}(\epsilon_{3\ell})$  would then become more complicated.

The seventh assumption is that either  $\epsilon_1$  or  $\epsilon_2$  or  $\epsilon_3$  errors dominate, and if  $\epsilon_2$  errors dominate, the errors are autoregressive and the time between observations is constant. Although, as discussed above, it could be argued that  $\epsilon_2$  errors generally are a small part of the total measurement error, the assumption that one type of error dominates is questionable under most circumstances.

If all seven assumptions are valid, no flow observations are used to calculate more than one head-dependent boundary gain or loss, and the appropriate transformation is used, the variance-covariance matrix and, therefore, the weight matrix is diagonal. This structure is advantageous computationally and because the effect of a diagonal weight matrix on parameter estimation is easy for users to understand.

In practice, the seventh assumption is most likely to be violated. Violation of the seventh assumption means that more than one classification of error is significant and off-diagonal terms in the weight matrix are needed.

#### Estimation Procedure

For a diagonal variance-covariance matrix, the quantities that need to be estimated for each observation location are  $\sigma_{1\ell}^2$  and the diagonal elements



of  $\underline{V}(\epsilon_{3\ell})$  or, if the  $\epsilon_3$  errors are assumed to have equal variances,  $\sigma_{3\ell}^2$ . If  $\sigma_{1\ell}^2 \neq 0.0$ ,  $\sigma_{1\ell}^2$  is only applied to the first observation at location  $\ell$ , and subsequent observations need to be calculated as the change from the first observation. If only one observation is made at an observation location,  $\underline{V}(\epsilon_{1\ell})$  and  $\underline{V}(\epsilon_{3\ell})$  are scalars.

Estimation of  $\sigma_{1\ell}^2$  is based on knowledge of errors that are constant over time. For example, perhaps the elevation of an observation well was determined by an altimeter and is considered to be accurate to within 3 ft. To estimate  $\sigma_{1\ell}^2$ , this statement needs to be quantified to, for example, the probability that the true elevation is within 3 ft of the measured elevation is 95 percent. Using the sixth assumption--that the  $\epsilon_{1\ell}$  are normally distributed--a table of the cumulative distribution of a standardized normal distribution (Cooley and Naff, 1990, p. 44, or any basic statistical text, such as Benjamin and Cornell, 1970, p. 655) can be used to determine that  $1.96 \hat{\sigma}_{1\ell} = 3.0$  ft, or  $\hat{\sigma}_{1\ell} = 1.53$ , where  $\hat{\sigma}_{1\ell}$  is the estimated standard deviation. The variance is calculated as the square of the standard deviation, so  $\hat{\sigma}_{1\ell}^2 = 2.34$  ft<sup>2</sup>. If elevations of wells are obtained from USGS topographic maps, the accuracy standards of the USGS can be used to quantify errors in elevation. The USGS (1980, p. 6) states that on their topographic maps, "\*\*\*not more than ten percent of the elevations tested shall be in error more than one-half the contour interval."

Estimation of each diagonal element of  $\underline{V}(\epsilon_{3\ell})$  can be accomplished by using a similar procedure. For example, consider a loss in streamflow between two gaging stations. The upstream and downstream streamflow measurements are 3.0 ft<sup>3</sup>/s and 2.5 ft<sup>3</sup>/s, the measurements are each thought to be accurate to within 5 percent (using, for example, Carter and Anderson, 1963, as in Hill and others, in press), and the errors in the two measurements are considered to be independent. Stated quantitatively, perhaps the hydrologist is 90 percent certain that the first measurement is within 0.15 ft<sup>3</sup>/s of the true value, and 95 percent certain that the second measurement is within 0.125 ft<sup>3</sup>/s of the true value. Assuming that the errors are independent and normally distributed, the standard deviation of the first measurement is calculated from  $1.65 \hat{\sigma}_1 = 0.15$  ft<sup>3</sup>/s, so  $\hat{\sigma}_1^2 = 0.083$  (ft<sup>3</sup>/s)<sup>2</sup>. The standard deviation of the second measurement is calculated from  $1.96 \hat{\sigma}_2 = 0.125$  ft<sup>3</sup>/s, so  $\hat{\sigma}_2^2 = 0.0041$  (ft<sup>3</sup>/s)<sup>2</sup>. The variance of the

loss of  $0.5 \text{ ft}^3/\text{s}$  equals  $\hat{\sigma}_1^2 + \hat{\sigma}_2^2 = 0.0124 (\text{ft}^3/\text{s})^2$ . The coefficient of variation (standard deviation,  $0.0124^{1/2}$ , divided by the loss,  $0.5 \text{ ft}^3/\text{s}$ ) for the loss in streamflow is, therefore, 0.22, which indicates a moderately reliable value.

It generally is impossible to identify all errors that contribute to the variance-covariance matrix, and the variances calculated by using the methods discussed in this section are clearly approximate. In the Parameter-Estimation Package,  $\hat{\sigma}_h^2$ ,  $\hat{\underline{W}}$ ,  $\hat{\sigma}_f^2$ , and  $\hat{\underline{Z}}$  of the estimated equivalent of equation (22) are specified independently to allow the user to conveniently change the weight matrix for all hydraulic-head observations and temporal change in hydraulic-head observations, or all head-dependent boundary gain-and-loss observations. This might be necessary if all the weighted residuals of one type of data are larger than for the other, as discussed in the section "Adjustments Commonly Required During Parameter Estimation". It commonly is most convenient initially to define  $\hat{\underline{W}}$  and  $\hat{\underline{Z}}$  as variance-covariances matrices, and set  $\hat{\sigma}_h^2 = 1.0$  and  $\hat{\sigma}_f^2 = 1.0$ . Changes in  $\hat{\sigma}_h^2$  or  $\hat{\sigma}_f^2$  can then easily be interpreted as changes in the initial estimate of  $V(\underline{\epsilon})$ . An additional simplification can be achieved by keeping the estimated common variance equal to 1.0 and making all changes to the other variance. Then, the final estimated error variance would ideally equal 1.0 and, if the residuals are nearly independent, they would resemble realizations from a standard normal,  $N(0,1)$ , distribution.

Data interpolated from observed dependent-variable values are sometimes used to calibrate regression models. Neuman (1982), Clifton and Neuman (1982), Neuman and Jacobson (1984), and Carrera and Neuman (1986a) suggest that kriging can be used to interpolate observed hydraulic-head values, and the kriging variances and variogram can be used to calculate the variance-covariance matrix. The advantage of interpolation methods is that more hydraulic-head values are available for the regression. The disadvantage of interpolation methods is that they are not based on the physics of ground-water flow, and interpolated values might not be realistic. This problem is most severe if aquifer properties change rapidly; the interpolation method might make the hydraulic-head distribution unrealistically smooth. Use of interpolated values in the regression procedure produces correlation between the errors, so the third assumption stated above is not valid, and nonzero

off-diagonal components of  $\underline{V}(\underline{\epsilon})$  are required. The computer program presented in this report is not designed to accommodate nonzero off-diagonal components of  $\underline{V}(\underline{\epsilon})$ .

#### Prior Information on the Estimated Parameters

Data on model parameters that are independent of the observations of dependent variables used in the regression exist in most problems. These data are called prior information on the estimated parameters and can be included in the regression if they can be expressed in a form similar to equation (6) (Neuman and Yakowitz, 1979; Cooley, 1983a). Generally, such an expression is not difficult. If, for example, an independent estimate,  $P$ , exists for parameter  $\beta_2$ ,  $P$  generally can be expressed as:

$$P = a_2 \beta_2 + u, \quad (28)$$

where  $a_2$  is analogous to  $x_2$ , the NP-1 other coefficients equal zero, and  $u$  is the true error of the prior estimate of the parameter and is analogous to  $\epsilon$  in equation (6). The new notation is used to emphasize the difference between the variables in equation (28) and those of equation (6). Prior information also might apply to a combination of estimated parameters, so, for example:

$$P = a_2 \beta_2 + a_4 \beta_4 + u. \quad (29)$$

This might be useful, for example, if seasonal recharge rates are being estimated and measurements of annual recharge are available; or if storage coefficients of two model layers are being estimated, and an aquifer test was conducted that measured the combined storage coefficient. Although nonlinear prior relations also could be considered by nonlinear regression, this option is not included in the Parameter-Estimation Package.

In some situations, many approximately equally reliable estimates of a parameter might exist within its applicable region, as defined by parameterization. For example, a parameter equal to the hydraulic conductivity of a large area of an aquifer can be estimated using the results of many specific-capacity tests (if the parameter is log-transformed, the natural log of the estimates needs to be used). The goal

is to use the individual estimates to obtain an estimate of the hydraulic conductivity of the entire region and a variance that represents the reliability of this estimate. One way to achieve this goal is to use the arithmetic mean of the individual estimates and calculate the variance of the estimate as the variance of the mean,  $s_p^2/n$ , where  $s_p^2 = (\sum_{i=1}^n (p_i - \bar{p})^2)/(n-1)$ ,  $n$  is the number of individual estimates,  $p_i$  is an individual estimate, and  $\bar{p} = \sum_{i=1}^n p_i/n$  (Benjamin and Cornell, p. 11 and 385). There are two problems related to this method. First, recent literature (Gómez-Hernández and Gorelick, 1989) has indicated that the arithmetic mean is not always the correct averaging method to use, and the reader might want to consider alternatives, such as the geometric mean. Note that if the parameter is log-transformed,  $\bar{p}$  is the geometric mean of the untransformed parameter. Second, if  $n$  is very large,  $s_p^2$  might be so small that its use would make the parameter value virtually equal to its prior estimate. In such cases, there might be a discrepancy between what is being observed and what is represented by the model parameter, and a larger variance might be justified.

If estimates that are not approximately equally reliable exist, as would occur if hydraulic-conductivity estimates were available from aquifer and specific-capacity tests, several options exist. First, if the two types of data represent the same part of the ground-water flow system, the less accurate values can be ignored. If the two types of data represent different parts of the system and the two mean values of hydraulic conductivity are quite different, reparameterization might be justified. Other options can be developed based on the situation involved, but in no situation can the data be combined into one mean estimate using the equations from the preceding paragraph.

If many prior estimates on the estimated parameters exist, they can be expressed similarly to equation (7):

$$\begin{aligned} & (P_1, a_{1,1}, a_{1,2} \dots a_{1,NP}), (P_2, a_{2,1}, a_{2,2} \dots a_{2,NP}), \\ & \dots (P_{NPR}, a_{NPR,1}, a_{NPR,2} \dots a_{NPR,NP}), \end{aligned} \quad (30)$$

where the added subscripts indicate the sequential number of the prior estimate, and NPR is the total number of prior estimates on the parameters. (Note that NPR as used in this part of the report equals NPR+MPR as defined in Appendix A and used in the FORTRAN code.) Once in this form, the NPR equations can be added to equation (9) by augmenting  $\underline{y}$ ,  $\underline{X}$ ,  $\hat{\underline{y}}$  and  $\underline{e}$ .

A regression equation analogous to equation (10) is produced by replacing the true, but unknown, vector  $\underline{\beta}$  with the vector of estimated parameters,  $\underline{b}$ , and substituting the residual vector,  $\underline{e}$ , for the vector of true errors,  $\underline{\epsilon}$ . The regression equation augmented to include prior information on the parameters can be expressed as:

$$\underline{y} - \underline{X} \underline{b} + \underline{e} = \hat{\underline{y}} + \underline{e} \quad (31)$$

where,

$$\underline{y} = \begin{pmatrix} y_1 \\ y_2 \\ \vdots \\ y_{ND} \\ \hline p_1 \\ p_2 \\ \vdots \\ p_{NPR} \end{pmatrix}, \quad \underline{X} = \begin{pmatrix} x_{1,1} & x_{1,2} & \cdots & x_{1,NP} \\ x_{2,1} & x_{2,2} & \cdots & x_{2,NP} \\ \vdots & \vdots & \ddots & \vdots \\ x_{ND,1} & x_{ND,2} & \cdots & x_{ND,NP} \\ \hline a_{1,1} & a_{1,2} & \cdots & a_{1,NP} \\ a_{2,1} & a_{2,2} & \cdots & a_{2,NP} \\ \vdots & \vdots & \ddots & \vdots \\ a_{NPR,1} & a_{NPR,2} & \cdots & a_{NPR,NP} \end{pmatrix},$$

$$\hat{\underline{y}} = \begin{pmatrix} \hat{y}_1 \\ \hat{y}_2 \\ \vdots \\ \hat{y}_{ND} \\ \hline \hat{p}_1 \\ \hat{p}_2 \\ \vdots \\ \hat{p}_{NPR} \end{pmatrix}, \quad \underline{e} = \begin{pmatrix} e_1 \\ e_2 \\ \vdots \\ e_{ND} \\ \hline u_1 \\ u_2 \\ \vdots \\ u_{NPR} \end{pmatrix}$$

where the true errors,  $u$ , have been replaced by the residuals,  $u$ . The  $\underline{b}$  is the same as in equation (10).

The unweighted sum-of-squares objective function (eq. 11) now becomes:

$$S(\underline{b}) = \sum_{q=1}^{ND} (y_q - \hat{y}_q)^2 + \sum_{p=1}^{NPR} (P_p - \hat{P}_p)^2. \quad (32)$$

In a sense, a penalty function has been introduced that increases the objective-function value as the parameter estimates produced by the regression routine diverge from the prior estimates. By using the augmented vectors and matrices of equation (32),  $S(\underline{b})$  still can be expressed as  $(\underline{y} - \underline{X}\underline{b})^T(\underline{y} - \underline{X}\underline{b})$  or  $\underline{e}^T \underline{e}$ , and the unweighted normal equations are still as in equation (16).

Prior estimates of the parameters are weighted to indicate their reliability relative to each other and relative to the observations of dependent variables, and to accommodate the different units the prior estimates might have. Assuming that the errors on the hydraulic head, streamflow gain-and-loss, and parameter data are uncorrelated, the weight matrix of equation (23), in which  $\sigma_h^2$  is assumed to be the common error variance, can be augmented to become:

$$\underline{W} = \begin{bmatrix} \underline{W}^{-1} & \underline{0} & \underline{0} \\ \underline{0} & \underline{Z}^{-1} \frac{\sigma_h^2}{\sigma_f^2} & \underline{0} \\ \underline{0} & 0 & \underline{U}^{-1} \sigma_h^2 \end{bmatrix}, \quad (33)$$

where  $\underline{U}$  is the variance-covariance matrix for true errors in the prior estimates of the parameters.

The most general form of  $\underline{U}$  could be as complicated as the most general form of the variance-covariance matrix on observations of dependent variables, which was discussed in previous sections of this report.  $\underline{U}$  can be simplified by using assumptions that are nearly identical to the seven assumptions discussed in those earlier sections. The resulting  $\underline{U}$  has nonzero elements only on its main diagonal, and these elements equal the variances of the measurement errors of the prior information on the estimated parameters.  $\underline{U}$  can be estimated by using methods similar to those presented in the earlier sections.

If the parameters with prior information are divided into groups with the same units (for example, one group might be hydraulic-conductivity values and another might be recharge rates), the variance-covariance matrix for each group can be expressed as a dimensionless matrix multiplied by a group variance. For example, with three groups,  $\underline{U}$  can be expressed as:

$$\underline{U} = \begin{bmatrix} \underline{U}_{p_1} \sigma_{p_1}^2 & 0 & 0 \\ 0 & \underline{U}_{p_2} \sigma_{p_2}^2 & 0 \\ 0 & 0 & \underline{U}_{p_3} \sigma_{p_3}^2 \end{bmatrix}, \quad (34a)$$

and  $\underline{U}^{-1} \sigma_h^2$  can be expressed as:

$$\underline{U}^{-1} \sigma_h^2 = \begin{bmatrix} \underline{U}_{p_1}^{-1} \frac{\sigma_h^2}{\sigma_{p_1}^2} & 0 & 0 \\ 0 & \underline{U}_{p_2}^{-1} \frac{\sigma_h^2}{\sigma_{p_2}^2} & 0 \\ 0 & 0 & \underline{U}_{p_3}^{-1} \frac{\sigma_h^2}{\sigma_{p_3}^2} \end{bmatrix}, \quad (34b)$$

where  $\sigma_{p_1}^2$ ,  $\sigma_{p_2}^2$ , and  $\sigma_{p_3}^2$  are the variances for groups  $p_1$ ,  $p_2$ , and  $p_3$ , respectively. This representation is sometimes helpful when trying to estimate the weight matrix of the prior parameter estimates.

The weighted sum-of-squares objective function is still expressed by equation (18), except that  $\underline{e}$  is augmented as in equation (31), and  $\underline{\omega}$  is augmented as in equation (33). Similarly, the weighted normal equations can be calculated by using equation (19) with the augmented vectors and matrices of equations (31) and (33).

### Input Data Used by the Parameter-Estimation Package to Calculate the Complete Weight Matrix

In the Parameter-Estimation Package, diagonal elements of  $\hat{V}(\epsilon)$  are calculated using  $\hat{\sigma}_h^2$ ,  $\underline{W}$ ,  $\hat{\sigma}_f^2$ ,  $\underline{Z}$  and  $\underline{U}$ , which are estimated equivalents of the terms in equations (22) and (34). From a practical perspective,  $\hat{\sigma}_h^2$  and  $\hat{\sigma}_f^2$  can be thought of as scaling factors, so that the diagonal elements of  $\underline{W}$  and  $\underline{Z}$  are scaled variances. These scaled variances can be specified directly, or the user can specify scaled standard deviations or scaled coefficients of variation. When scaled standard deviations are specified, the scaled variances are calculated as the square of the scaled standard deviation; when scaled coefficients of variation are specified, the scaled variances are calculated as  $(\gamma y)^2$ , where  $\gamma$  is the scaled coefficient of variation and  $y$  is the observed value of hydraulic head, temporal change in hydraulic head, or head-dependent boundary gain or loss. The diagonal weight matrix is calculated from the variances using equation (17), (23), or (33) and (34b), where the common error variance is set equal to  $\sigma_h^2$  or  $\sigma_f^2$ .

Components of the diagonal weight matrix related to prior parameter estimates are calculated similarly, but the variances, standard deviations, or coefficients of variation specified by the user are not scaled. For example, the  $\sigma_{p_i}^2$ ,  $i = 1, 3$ , of equation (34a) would be included in the value specified by the user.

### Analysis of Results for Linear Problems

Analysis of final parameter estimates and the assumed model are required to: (1) Discriminate between models that use different parameterizations, boundary conditions, or other choices of model construction by comparing the results achieved from the different models, and (2) determine if the simulated results are similar enough to observed values and if the parameter estimates are reliable enough to justify using the calibrated model to draw conclusions about the aquifer system or to predict aquifer response. The second objective would benefit from calculation of confidence intervals on the predicted quantities (Draper and Smith, 1981, p. 94), but these confidence intervals are not included in the Parameter-Estimation Package.



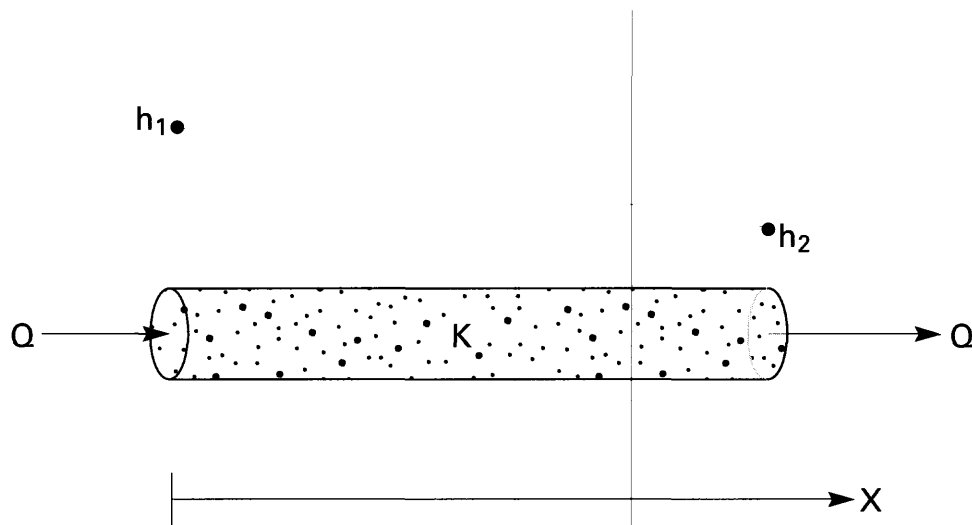
Many of the methods discussed in this section are discussed in more detail in Cooley and Naff (1990, ch. 5). See Cooley and others (1986) for an example of how the methods can be used.

Parameter estimates are analyzed to determine: (1) How reliably they are estimated by the available data; and (2) whether some of the parameters are strongly correlated. A parameter cannot be reliably estimated if the values of the dependent variables at all observation locations are insensitive to that parameter and prior estimates are missing or inaccurate. This might occur, for example, when trying to estimate hydraulic conductivity in an area of an aquifer that is remote from all observation locations. Strong correlation between parameters occurs when similar values of the dependent variables at the observation locations are produced by numerous, different combinations of parameter values and prior estimates of the parameters do not exist or are inaccurate. For example, consider a Darcy cylinder (fig. 15) packed with sand that has a known hydraulic head,  $h_1$ , at  $X=0$ , and the unknown parameters  $K$ , the hydraulic conductivity of the sand, and  $Q$ , the flow through the cylinder. Hydraulic head at any distance,  $X$ , along the cylinder can be calculated as  $h=h_1-\frac{Q}{KA} X$ . As long as the ratio  $Q/K$  is constant, the hydraulic-head distribution along the length of the cylinder will be the same. Thus,  $Q$  and  $K$  are perfectly correlated and cannot be estimated independently by using observed hydraulic heads.

The reliability and correlation of parameter estimates can be analyzed by using the variance-covariance matrix,  $\underline{V}(\underline{b}')$ , for the final estimated parameters,  $\underline{b}'$  (Bard, 1974, p. 59):

$$\underline{V}(\underline{b}') = s^2 (\underline{X}^T \underline{\omega} \underline{X})^{-1} \quad (35)$$

where  $\underline{V}(\underline{b}')$  is an NP by NP matrix;  $s^2$ , the estimated error variance, is the minimized value of the objective function divided by  $ND+NPR-NP$ ; and  $\underline{X}$  and  $\underline{\omega}$  are augmented as in equations (31) and (33) if there is prior information on the parameters. The validity of equation (35) depends on the model being nearly linear in the vicinity of  $\underline{b}'$ .



#### EXPLANATION

$h_1, h_2$	HYDRAULIC-HEAD AT THE TWO ENDS OF THE DARCY CYLINDER
$Q$	FLOW THROUGH THE CYLINDER
$K$	HYDRAULIC CONDUCTIVITY OF THE MATERIAL FILLING THE CYLINDER
$X$	DISTANCE ALONG THE CYLINDER

Figure 15.--Darcy cylinder.

Each element along the main diagonal of the variance-covariance matrix,  $v_{ii}$ , equals the estimated variance of final parameter estimate  $b'_i$ . The square root of each variance is the standard deviation of the parameter estimate, and the coefficient of variation equals  $(v_{ii})^{1/2}/b'_i$ , which is dimensionless. The coefficient of variation is the easiest statistic by which to compare the reliability of different parameters estimated in a single parameter-estimation run. However, as discussed in item 2 in the section "Output for Test Case 1" in Appendix A, interpretation of the coefficients of variation can be confusing if there are log-transformed parameters. For linear problems, the variances calculated by using equation (35) can be used to calculate confidence intervals on the estimated parameters (Draper and Smith, 1981, p. 94) as:

$$b_i \pm (v_{ii})^{1/2} \times t(\text{ND+NPR-NP}, 1.0-\alpha/2) \quad (36)$$

where,  $t(\cdot, \cdot)$  is a student-t probability distribution in which the first argument equals the degrees of freedom, the second argument equals the probability that  $\beta_i$  occurs within the confidence interval, and  $\alpha$  equals the probability that  $\beta_i$  occurs outside the confidence interval. The student-t probability distribution is presented in table 2. For log-transformed parameters, the confidence interval needs to be calculated on the log-transformed parameter estimate. The exponential of the estimate equals the mode of the lognormal probability distribution; the exponential of the confidence limits are confidence limits on the mode, which might not be symmetric about the mode.

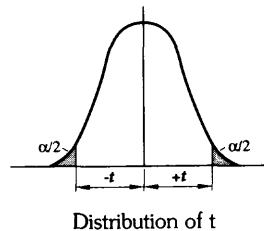
Parameter reliability also can be characterized by using the eigenvalues and eigenvectors of  $\underline{V}(\underline{b}')$  (Carrera and Neuman, 1986c). Unlike the previous work, in the Parameter-Estimation Package  $\underline{V}(\underline{b}')$  is scaled with the final estimated parameter values before eigenvalues and eigenvectors are calculated. This is necessary to ensure that the eigenvalues and eigenvectors, when used as described below, are indicative of parameter reliability instead of differences in parameter values. Elements of the scaled matrix are calculated as  $(v_{ij})/b'_i b'_j$ . The least reliable parameter values can be identified by inspecting the eigenvectors associated with the largest eigenvalues. The parameters with the largest elements of these eigenvectors are estimated least reliably. The most reliable parameter values can be identified by inspecting the eigenvectors associated with the smallest eigenvalues. The parameters related to the largest elements of these eigenvectors are estimated most reliably.

Parameter reliability can be characterized by using either the coefficient of variation or eigenvalues and eigenvectors, but the conclusions generally are identical. Use of the coefficient of variation is easier, so its use is encouraged.

Table 2.--Student *t* probability distribution

[Modified from Draper and Smith (1981, p. 532) with permission from publisher]

Degrees of freedom	Probability <sup>1</sup>									
	0.9	0.7	0.5	0.3	0.2	0.1	0.05	0.02	0.01	0.001
1	0.158	0.510	1.000	1.963	3.078	6.314	12.706	31.821	63.657	636.619
2	0.142	0.445	0.816	1.386	1.886	2.920	4.303	6.965	9.925	31.598
3	0.137	0.424	0.765	1.250	1.638	2.353	3.182	4.541	5.841	12.924
4	0.134	0.414	0.741	1.190	1.533	2.132	2.776	3.747	4.604	8.610
5	0.132	0.408	0.727	1.156	1.476	2.015	2.571	3.365	4.032	6.869
6	0.131	0.404	0.718	1.134	1.440	1.943	2.447	3.143	3.707	5.959
7	0.130	0.402	0.711	1.119	1.415	1.895	2.365	2.998	3.499	5.408
8	0.130	0.399	0.706	1.108	1.397	1.860	2.306	2.896	3.355	5.041
9	0.129	0.398	0.703	1.100	1.383	1.833	2.262	2.821	3.250	4.781
10	0.129	0.397	0.700	1.093	1.372	1.812	2.228	2.764	3.169	4.587
11	0.129	0.396	0.697	1.088	1.363	1.796	2.201	2.718	3.106	4.437
12	0.128	0.395	0.695	1.083	1.356	1.782	2.179	2.681	3.055	4.318
13	0.128	0.394	0.694	1.079	1.350	1.771	2.160	2.650	3.012	4.221
14	0.128	1.393	0.692	1.076	1.345	1.761	2.145	2.624	2.977	4.140
15	0.128	1.393	0.691	1.074	1.341	1.753	2.131	2.602	2.947	4.073
16	0.128	0.392	0.690	1.071	1.337	1.746	2.120	2.583	2.921	4.015
17	0.128	0.392	0.689	1.069	1.333	1.740	2.110	2.567	2.898	3.965
18	0.127	1.392	0.688	1.067	1.330	1.734	2.101	2.552	2.878	3.922
19	0.127	1.391	1.688	1.066	1.328	1.729	2.093	2.539	2.861	3.883
20	0.127	1.391	0.687	1.064	1.325	1.725	2.086	2.528	2.845	3.850
21	0.127	0.391	0.686	1.063	1.323	1.721	2.080	2.518	2.831	3.819
22	0.127	0.390	0.686	1.061	1.321	1.717	2.074	2.508	2.819	3.792
23	0.127	0.390	0.685	1.060	1.319	1.714	2.069	2.500	2.807	3.767
24	0.127	0.390	0.685	1.059	1.318	1.711	2.064	2.492	2.797	3.745
25	0.127	0.390	0.684	1.058	1.316	1.708	2.060	2.485	2.787	3.725
26	0.127	0.390	0.684	1.058	1.315	1.706	2.056	2.479	2.779	3.707
27	0.127	0.389	0.684	1.057	1.314	1.703	2.052	2.473	2.771	3.690
28	0.127	0.389	0.683	1.056	1.313	1.701	2.048	2.467	2.763	3.674
29	0.127	0.389	0.683	1.055	1.311	1.699	2.045	2.462	2.756	3.659
30	0.127	0.389	0.683	1.055	1.310	1.697	2.042	2.457	2.750	3.646
40	0.126	0.388	0.681	1.050	1.303	1.684	2.021	2.423	2.704	3.551
60	0.126	0.387	0.679	1.046	1.296	1.671	2.000	2.390	2.660	3.460
120	0.126	0.386	0.677	1.041	1.289	1.658	1.980	2.358	2.617	3.373
∞	0.126	0.385	0.674	1.036	1.282	1.645	1.960	2.326	2.576	3.291

<sup>1</sup>Probability = Area in two tails of distribution outside  $\pm t$ -value in table.Table 2. Student-*t* probability distribution.

The elements off the main diagonal of  $\underline{V}(\underline{b}')$ ,  $v_{ij}$ ,  $i \neq j$ , are the covariances. The correlation between any two parameters is measured by correlation coefficients, which are calculated as  $(v_{ij}) / (v_{ii})^{1/2} (v_{jj})^{1/2}$ . Correlation coefficients can have values ranging from -1.0 to +1.0: values of about zero indicate no correlation between  $b'_i$  and  $b'_j$ ; values of about -1.0 or +1.0 indicate strong correlation. In the simple, two-parameter problem presented at the beginning of this section, the correlation between Q and K was +1.0.

Correlations also might occur between groups of parameters. If these correlations are strong, similar dependent-variable values are produced by different combinations of values of all the parameters in the group. For example, in the two-layer aquifer system described as test case 1 in Appendix A, doubling all hydraulic-conductivity values and all fluxes produces an identical hydraulic-head distribution. The correlation coefficients between pairs of parameters from a group of parameters that are correlated generally are about 1.0 or -1.0, but it might not be obvious from the correlation coefficients that the parameters form a group. Such a group can be identified by using the eigenvectors of  $\underline{V}(\underline{b}')$  scaled as described above. Parameters in such groups are associated with nearly equal elements within individual eigenvectors. The implied functional dependence is stronger if the elements associated with the parameters are nearly equal in several eigenvectors, and if the eigenvector elements and the eigenvalue associated with each eigenvector are large.

The assumed model also is analyzed to determine if the simulated dependent-variable values are as expected--that is, are indicative of a valid regression. Unexpected results would indicate that the assumed model is biased. Evaluation of the assumed model is accomplished through statistical and graphical analyses of the weighted observations,  $\underline{\omega}^h \underline{y}$ , the weighted final simulated values,  $\underline{\omega}^h \hat{\underline{y}}$ , and the weighted final residuals,  $\underline{\omega}^h \underline{e} = \underline{\omega}^h (\underline{y} - \hat{\underline{y}})$ . Three commonly used statistics are the average weighted residual, the estimated error variance, and the correlation coefficient. The average weighted residual is calculated as the sum of the weighted residuals divided by the number of weighted residuals, and needs to be about zero. The estimated error variance,  $s^2$ , was discussed after equation (35) and is a measure of how similarly the final simulated values match the

observed values. For simulations with the same weight matrix, smaller values of  $s^2$  indicate a better match;  $s^2$  cannot be used to compare regressions which use different weight matrices. The correlation coefficient,  $R$ , measures how closely trends in the simulated values match trends in the observed values and is calculated as (Cooley and Naff, 1990, p. 166):

$$R = \frac{(\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{y} - \underline{\underline{m}}_y)^T (\underline{\hat{\omega}}^{-\frac{1}{2}} \hat{\underline{y}} - \underline{\underline{m}}_y^{\hat{}})}{[(\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{y} - \underline{\underline{m}}_y)^T (\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{y} - \underline{\underline{m}}_y) (\underline{\hat{\omega}}^{-\frac{1}{2}} \hat{\underline{y}} - \underline{\underline{m}}_y^{\hat{}})^T (\underline{\hat{\omega}}^{-\frac{1}{2}} \hat{\underline{y}} - \underline{\underline{m}}_y^{\hat{}})]^{\frac{1}{2}}} \quad (37)$$

where  $\underline{y}$ ,  $\hat{\underline{y}}$ , and  $\underline{\hat{\omega}}$  are defined in equations (9), (10), and (23).

$$\underline{\underline{m}}_y = \left[ \left( \sum_{q=1}^{ND} (\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{y})_q \right) / ND \right] \underline{1},$$

$$\underline{\underline{m}}_y^{\hat{}} = \left[ \left( \sum_{q=1}^{ND} (\underline{\hat{\omega}}^{-\frac{1}{2}} \hat{\underline{y}})_q \right) / ND \right] \underline{1},$$

and  $\underline{1}$  is a vector of length  $ND$  with each element equal to 1. Note that  $\underline{\underline{m}}_y$  is simply a vector with each component equal to the average value of the weighted dependent-variable observations, and that  $\underline{\underline{m}}_y^{\hat{}}$  is an analogous vector using the weighted calculated dependent-variable values. Generally  $R$  needs to be greater than 0.90.  $R$  also is calculated with  $\underline{y}$ ,  $\hat{\underline{y}}$ , and  $\underline{\hat{\omega}}$  augmented as in equations (31) and (33), in which case  $ND+NPR$  replaces  $ND$  when calculating  $\underline{\underline{m}}_y$  and  $\underline{\underline{m}}_y^{\hat{}}$ .

The statistical properties of the weighted residuals are checked against their expected statistical properties to identify unexpected patterns that would indicate bias in the model. One might expect that if the weighted true errors satisfied the conditions  $E(\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{\epsilon}) = \underline{0}$  and  $V(\underline{\hat{\omega}}^{-\frac{1}{2}} \underline{\epsilon}) = \underline{I}\sigma^2$ , the same would be true of the weighted residuals. If this were the situation, the weighted residuals would be independent and have equal variances. Although they actually might be correlated, as discussed below, a first step toward analyzing the weighted residuals is accomplished by testing whether they satisfy these properties. For the purposes of the first of the two tests performed, as described below, it also is assumed

that  $\underline{\epsilon}$  and, therefore,  $\underline{e}$  are normally distributed. If the tests indicate that the residuals are normal, independent, and have equal variance, the model probably is unbiased.

The correlation coefficient between the weighted residuals ordered from smallest to largest and the order statistics from a  $N(0,1)$  probability distribution function (Brockwell and Davis, 1987, p. 304) is the first statistic used to test for independent, normally distributed weighted residuals. This statistic was chosen instead of other statistics, such as chi-squared and Kolomogorov-Smirnov, because it is more powerful for commonly used sample sizes (Shapiro and Francia, 1972). The correlation coefficient,  $R_N^2$ , is calculated as:

$$R_N^2 = \frac{[(\underline{e}_o - \underline{m})^T \underline{r}]^2}{[(\underline{e}_o - \underline{m})^T (\underline{e}_o - \underline{m})](\underline{r}^T \underline{r})}, \quad (38)$$

where all vectors are of length ND,  $\underline{m}$  is a vector with all components equal to the average of the weighted residuals,  $\underline{e}_o$  are the weighted residuals ordered from smallest to largest, and  $\underline{r}$  is a vector with the  $i$ th element equal to the ordinate value of a  $N(0,1)$  probability distribution function for a cumulative probability equal to  $u_i = (i-0.5)/ND$ . If, for example,  $u_i = 0.8531$ ,  $r_i = 1.05$ .

The hypothesis that the weighted residuals are derived from an independent, normal distribution is rejected if  $R_N^2$  is too much smaller than its ideal value of 1.0. The critical value below which the hypothesis is rejected depends on the value of ND and on the significance level (Benjamin and Cornell, 1970, p. 406) chosen by the user (table 3). If  $R_N^2$  indicates that the weighted residuals are not independent and normally distributed, the hypothesis that they are correlated and normally distributed needs to be tested, as discussed below. In any case, the three graphical analyses described below need to be performed.

Table 3: Critical values of  $R_N^2$  below which the hypothesis that the weighted residuals are independent and normally distributed is rejected (From Shapiro and Francia, 1972; Brockwell and Davis, 1987, p. 304)

ND or ND+NPR+MPR	<u>Significance level</u>		ND or ND+NPR+MPR	<u>Significance level</u>	
	0.05	0.10		0.05	0.10
35	0.943	0.952	81	0.970	0.975
			83	0.971	0.976
50	0.953	0.963	85	0.972	0.977
51	0.954	0.964	87	0.972	0.977
53	0.957	0.964	89	0.972	0.977
55	0.958	0.965			
57	0.961	0.966	91	0.973	0.978
59	0.962	0.967	93	0.973	0.979
			95	0.974	0.979
61	0.963	0.968	97	0.975	0.979
63	0.964	0.970	99	0.976	0.980
65	0.965	0.971			
67	0.966	0.971	131	0.980	0.983
69	0.966	0.972	200	0.987	0.989
71	0.967	0.972			
73	0.968	0.973			
75	0.969	0.973			
77	0.969	0.974			
79	0.970	0.975			

The correlation coefficient of equation (38) is also calculated using the vector of weighted residuals augmented for prior parameter estimates. The augmented residual vector is shown after equation (31); the weight matrix is shown in equation (33); all vectors of equation (38) would be of length ND+NPR. Inconsistency between the dependent-variable data and the prior parameter estimates is indicated if this second evaluation of  $R_N^2$  is smaller than the value calculated using only dependent-variable weighted residuals.

The runs test (Draper and Smith, 1981, p. 157-162) is used to test for independent residuals. In the runs test, the number of sequences of residuals of the same sign ( $u$ ) is counted, along with the total number of positive residuals ( $n_1$ ), and the total number of negative residuals ( $n_2$ ). The expected number of runs equals  $\mu = [2n_1n_2/(n_1+n_2)]+1.0$ , and the variance equals  $\sigma^2 = [2n_1n_2(2n_1n_2-n_1-n_2)]/[(n_1+n_2)^2(n_1+n_2-1)]$ . The test statistic for too few runs equals  $z_f = (u-\mu+0.5)/\sigma$ ; the test statistic for too many



runs equals  $z_m = (u - \mu - 0.5) / \sigma$ . If  $n_1 > 10$  and  $n_2 > 0$ ,  $u$  is normally distributed and critical values for  $z_f$  and  $z_m$  are printed by the Parameter-Estimation Package. Otherwise, a table such as the table in Draper and Smith (1981, p. 160-161) needs to be used to evaluate whether  $u$  is too small or too large.

The runs test is included in the Parameter-Estimation Package because it takes the order of the residuals into account, which is ignored in the correlation coefficient of equation (38). Normally, observations are grouped by location in transient simulations, and too few runs commonly indicates positive serial correlation between residuals at individual locations.

Except when  $ND \gg NP$  (Draper and Smith, 1981, p. 152; Cooley and others, 1986, p. 1771) the weighted residuals generally are correlated, even if the weighted true errors are not. The expected variance-covariance matrix for the weighted residuals is  $V(\underline{\omega}^{-1/2} \underline{e}) = (\underline{I} - \underline{X}(\underline{X}^T \underline{\omega} \underline{X})^{-1} \underline{X}^T \underline{\omega}) \sigma^2$  (Bard, 1974, p. 194; Cooley and Naff, 1990, p. 168), and graphical analyses of the weighted residuals is done by comparing plots of the weighted residuals to plots of realizations that have the same variance-covariance matrix. Assuming that the weighted true errors are normally distributed, the realizations would be derived from the joint normal probability distribution function  $N(0, (\underline{I} - (\underline{X}(\underline{X}^T \underline{\omega} \underline{X})^{-1} \underline{X}^T \underline{\omega}) \sigma^2))$ . A slightly modified version of the FORTRAN program presented by Cooley and Naff (1990, p. 176-183) can be used to produce realizations from this probability distribution function. The modifications are described in Appendix B of this report.

Three graphical analyses of the residuals are: (1) Plot the weighted residuals and several realizations on maps of each of the simulated model layers; (2) plot the weighted residuals and several realizations against their respective  $\hat{y}_q$  values on graph paper; and (3) plot the weighted residuals and several realizations on probability paper. See Cooley and Naff (1990, p. 168-170) for more information about graphical analyses.

Model discrimination can be performed by using the methods described above to compare the results from alternative models. Models with smaller parameter coefficients of variation, parameter correlations less than 0.95,

smaller values of  $s^2$  (if the weight matrices are identical), larger values of  $R^2$ , and weighted residuals that more closely match their expected statistical characteristics are considered to be better. Additional statistics are presented in the section "Analysis of Results for Nonlinear Problems". Model discrimination is difficult because usually no one model is the best for all the measures indicated above. If several models appear to be equally good, it might be helpful to perform some predictive runs by using all of these models.

#### Adjustments Commonly Required During Parameter Estimation

As the modeler learns about the physical system, the model, and the data through modeling and parameter estimation, adjustments commonly are made to the model, parameter definition, weight matrix, and observation data sets. In part, this is the same process a modeler goes through when calibrating by trial and error, but use of regression allows hypotheses to be tested more rigorously and provides more information about the effects of the data on parameter estimates and the reliability of the estimates.

For a model to be satisfactory, the weighted residuals produced by the final model need to satisfy two criteria: (1) The estimated common error variance ( $\hat{\sigma}_h^2$  or  $\hat{\sigma}_f^2$ ) needs to approximately equal the calculated error variance,  $s^2$ ; and (2) the weighted residuals need to satisfy  $E(\underline{\omega}^w \underline{e}) = 0$  and  $V(\underline{\omega}^w \underline{e}) = (\underline{I} - \underline{X}(\underline{X}^T \underline{\omega} \underline{X})^{-1} \underline{X}^T \underline{\omega}) \hat{\sigma}^2$ . As discussed in the previous section, violation of the second criterion is indicative of bias in the model.

One conspicuous indication of a problem is the presence of weighted residuals at convergence of parameter estimation (or after several parameter-estimation iterations if convergence is not achieved) that are so large that they dominate the regression, or so small that they are ignored by the regression. In such situations, the model needs to be evaluated to determine whether: (1) Some aspect of model construction is incorrect; (2) the parameter definition needs to be modified; (3) the weight matrix needs to be changed so that the data affect the regression more equally; or (4) dependent-variable observations or prior parameter estimates need to be eliminated or corrected because they are clearly biased.

Model construction can be modified, for example, by changing the representation of physical boundary conditions, such as conversion of an overlying constant-head boundary to a recharge boundary; and correction of input data, such as known pumpage. Many of these are the same kind of changes a modeler would consider as part of trial and error calibration.

Parameter definition can be modified, for example, by adding, omitting, dividing, or combining parameters, or making other changes in the parameterization. Note that the final parameterization needs to be consistent with what is known about hydrogeology of the ground-water flow system.

Changes to the weight matrix are common because  $\hat{\sigma}_h^2$ ,  $\hat{\sigma}_f^2$ , and  $\hat{\sigma}_{p_i}^2$  commonly are unknown, and there might be some question about the values in  $\hat{\underline{W}}$ ,  $\hat{\underline{Z}}$ , and  $\hat{\underline{U}}_{p_i}$  (see equations 17, 23, or 33 and 34). If all the weighted residuals for one data type, such as head-dependent boundary gains and losses, are extremely large or extremely small,  $\hat{\sigma}_h^2$ ,  $\hat{\sigma}_f^2$ , and  $\hat{\sigma}_{p_i}^2$  might need to be adjusted to achieve a more even distribution. To adjust  $\hat{\sigma}_h^2$ ,  $\hat{\sigma}_f^2$ , and  $\hat{\sigma}_{p_i}^2$  such that the desired effect on the weights is achieved, consider how the weights are calculated. If  $\hat{\sigma}_h^2$  is the common variance,  $\hat{\sigma}^2$ , the weighting of hydraulic heads and temporal changes in hydraulic heads can be adjusted only by adjusting components of  $\hat{\underline{W}}$ . The weighting of head-dependent boundary gains and losses would be sensitive to the ratio  $\hat{\sigma}_h^2/\hat{\sigma}_f^2$ . For example, if  $\hat{\sigma}_f^2$  is increased by a factor of 4 the weighting of all gains and losses would be decreased by a factor of 2. The weighting of prior parameter estimates would be sensitive to the ratio  $\hat{\sigma}_f^2/\hat{\sigma}_{p_i}^2$ .

If  $\hat{\underline{\omega}}$  is realistic and the weighted residuals have all desired properties, but the estimated common error variance does not equal the calculated error variance ( $\hat{\sigma}^2 \neq s^2$ ), the following procedure can be followed if changing  $\hat{\underline{W}}$  or  $\hat{\underline{Z}}$ , and  $\hat{\underline{U}}$  of equation (33) is acceptable. Set the estimated common error variance equal to  $s^2$  and multiply all elements of  $\hat{\underline{U}}$  and either  $\hat{\underline{W}}$  or  $\hat{\underline{Z}}$  (depending on whether  $\hat{\sigma}_f^2$  or  $\hat{\sigma}_h^2$  is defined as the common error variance, respectively) by  $s^2/\hat{\sigma}_{OLD}^2$ . These changes will produce an identical weight matrix, so that the regression will be the same.

In some cases, individual observations dominate the regression or are ignored. Components of  $\hat{\underline{W}}$ ,  $\hat{\underline{Z}}$ , and  $\hat{\underline{U}}_{\underline{p}_i}$  can be adjusted to achieve a more even distribution, but the reason for the problem needs to be considered before making such adjustments. For example, Cooley and others (1986, p. 1764) anticipated that the small error with which shallow wells could be measured would produce accurate hydraulic-head observations at these points, and thus assigned them large weights. During calibration it was determined that "the model fit no better at these points than elsewhere." (Cooley and others, 1986, p. 1772). Apparently, the shallow wells were affected by shallow, local flow systems not represented in the regional-scale model, and this situation produced residuals that were as large as those associated with inaccurately observed deep wells. Decreasing the weights for observations from shallow wells produced more satisfactory results.

Although the process described above can become mechanical, the user needs to remember that the weight matrix reflects data accuracy. The final weight matrix needs to be justifiable in terms of known errors and inadequacies of the data.

Dependent-variable observations or prior parameter estimates from the regression can be eliminated only if careful consideration of the problem indicates that they are clearly biased. The danger is in eliminating data that is indicative of a legitimate problem in the model.

Once residuals are fairly evenly distributed, most of the anticipated changes have been made to the model, and parameter estimates are close to satisfactory, an attempt needs to be made to test whether the goals stated in the beginning of this section--that is, the estimated common error variance needs to approximately equal the calculated error variance, and the weighted residuals should satisfy  $E(\hat{\underline{\omega}}^{\frac{1}{2}} \underline{e}) = 0$  and  $V(\hat{\underline{\omega}}^{\frac{1}{2}} \underline{e}) = (\underline{I} - \underline{X}(\underline{X}^T \hat{\underline{\omega}} \underline{X})^{-1} \underline{X}^T \hat{\underline{\omega}}) \sigma^2$ --are satisfied by using the tests described in the previous section. More changes in the model and the weight matrix might be required.

With so many things that might be changed, the user might wonder about the uniqueness of the final model. Even if any single run of the regression routine produces a unique set of estimates (and this has its own set of

problems, as discussed by many authors such as Carrera and Neuman, 1986b), there is no guarantee that the final model is unique. The enhanced capability of regression modeling does, however, provide the modeler with an effective means of evaluating and discriminating between different possible models.

#### PARAMETER ESTIMATION AND ANALYSIS OF RESULTS USING NONLINEAR REGRESSION

In nonlinear regression, the assumed model need not be a linear function of the parameters, as in equation (6). Nonlinear regression needs to be used for ground-water flow problems because hydraulic head, as the solution of the ground-water flow equation, is a nonlinear function of many of the parameters a modeler would want to estimate. In contrast, for confined aquifers, the ground-water flow equation is classified as linear because hydraulic head is a linear function of time and space. An example is discussed in the next section.

##### Nonlinearity of the Ground-Water Flow Equation

The nonlinearity of the ground-water flow equation can be illustrated by considering Darcy's Law, the constitutive relation on which the ground-water flow equation is based. The differential form of Darcy's Law as applied to the Darcy cylinder shown in figure (15) is:

$$Q = -KA \frac{\partial h}{\partial X} , \quad (39)$$

where

Q is the flux [ $L^3/T$ ];

K is the hydraulic conductivity of the saturated material [ $L/T$ ];

A is the cross-sectional area [ $L^2$ ];

h is hydraulic head [ $L$ ]; and

X is distance along an axis parallel to the direction of flow [ $L$ ].

Equation (39) can be solved for the hydraulic head at any distance, X, along the cylinder to achieve:

$$h = h_1 - \frac{Q}{KA} X, \quad (40)$$

where  $h_1$  is the hydraulic head at  $X = 0$ . The derivatives of equation (40) with respect to  $X$ ,  $Q$  and  $K$  are:

$$\begin{aligned}\frac{\partial h}{\partial X} &= -\frac{Q}{KA} \\ \frac{\partial h}{\partial Q} &= -\frac{1}{KA} X \\ \frac{\partial h}{\partial K} &= -\frac{Q}{K^2 A} X.\end{aligned}\tag{41}$$

Thus, the hydraulic head is a linear function of  $X$  because  $\partial h/\partial X$  is independent of  $X$ . Hydraulic head also is a linear function of  $Q$ , but is a nonlinear function of  $K$ ;  $\partial h/\partial Q$  and  $\partial h/\partial K$  are both functions of  $K$ . The derivatives  $\partial h/\partial Q$  or  $\partial h/\partial K$  would be sensitivities in a parameter-estimation problem in which  $Q$  or  $K$  were being estimated. As in this simple example, sensitivities with respect to flows, such as  $Q$ , are nearly always functions of aquifer properties; sensitivities with respect to aquifer properties, such as  $K$ , are nearly always functions of the aquifer properties and the flows.

It is interesting to note that the example discussed above is linear if the ratio  $Q/K$  is considered. That is,

$$\frac{\partial h}{\partial (Q/K)} = -\frac{X}{A}\tag{42}$$

which is independent of any parameters. In this case, simple linear regression could be used to estimate  $Q/K$ . Ground-water flow problems can sometimes be linearized by redefining parameters in this way, but the prospects become less likely as the flow system becomes more complicated.

#### Assumed Nonlinear Model

For the nonlinear regression considered in this report, the true model can be expressed as:

$$\tilde{y} = g^* (\xi_1, \xi_2 \cdots \xi_k; \beta_1, \beta_2 \cdots \beta_{NP})\tag{43}$$

where

$\tilde{y}$  is a dependent variable, such as simulated hydraulic head, temporal change in hydraulic head, or head-dependent boundary gain or loss;

$g^*(\cdot)$  is general notation for a function of the values in the parentheses, and represents the true model;

$\xi_1$  is an independent variable, such as spatial dimension or time; and

$\beta_1$  is a true, unknown parameter value.

By using the same reasoning applied after equation (6) to linear problems, a vector of observations of dependent variables,  $y$ , can be expressed in terms of parameter estimates  $\underline{b}$  and model estimate  $g(\cdot)$  as:

$$y = g(\xi, \underline{b}) + \underline{e} = \hat{y} + e \quad (44)$$

which is analogous to equation (10) of this report and equivalent to equation (3.3-3) of Cooley and Naff (1990, p. 61).

Although the function,  $g(\cdot)$ , of equation (44) commonly is thought of as an analytical function of the independent variables and parameters, it also might be a numerical model. In this report  $g(\cdot)$  is calculated using the ground-water flow model presented by McDonald and Harbaugh (1988) and Prudic (1989), which was described briefly in the first part of this report. The model inputs that can be calculated with parameters estimated by nonlinear regression are listed in table 1; other model inputs need to be specified by the modeler.

#### Maximum-Likelihood Objective Function

The maximum-likelihood objective function has been used extensively in the time-series literature (Brockwell and Davis, 1987, ch. 8), and also has been used to estimate parameters in ground-water flow problems (Carrera and Neuman, 1986a). Although, as indicated below, it reduces to the least-squares objective function for the parameter-estimation procedure, the maximum-likelihood objective function can be used to calculate statistics with which different models can be compared. The statistics are discussed in the section "Analysis of Results for Nonlinear Problems".

The maximum-likelihood objective function is developed by considering the random nature of  $y$ , the observations. This random nature is a consequence of conceptualizing measurement error as random, as discussed in the section "Weighting Observations". If  $\underline{Y}$  is the vector of jointly distributed random variables of which  $y$  is a realization, the joint probability distribution function (pdf),  $f_{\underline{Y}}(y)$ , depends on the true model and true parameter values. For the purpose of estimating parameters for a given assumed model, consider the joint pdf conditioned on a particular set of parameter values,  $f_{\underline{Y}}(y|\underline{b})$ . This joint pdf can be thought of as the probability that different sets of possible observations would occur given the parameter values  $\underline{b}$ . In parameter estimation, the elements of  $y$  are known and we would like to estimate  $\underline{b}$ . A reasonable requirement of the estimates is that they maximize the probability of obtaining the observations,  $y$ . This requirement is imposed by defining the objective function using the likelihood function,  $\ell(\underline{b}|y)$ , which is:

$$\ell(\underline{b}|y) = f_{\underline{Y}}(y|\underline{b}). \quad (45)$$

If the true errors are from a joint, normal distribution, the likelihood function equals (Brockwell and Davis, 1987, p. 247):

$$\ell(\underline{b}|y) = \left(\frac{1}{2\pi}\right)^{ND/2} |\underline{V}(\underline{\epsilon})|^{-1/2} \exp\left\{-\frac{1}{2} \underline{e}^T (\underline{V}(\underline{\epsilon}))^{-1} \underline{e}\right\}, \quad (46)$$

where, by equation (44),  $\underline{e} = y - \hat{y}$ ,  $\hat{y}$  is a function of  $\underline{b}$ , and  $ND$  is the number of observations. Replacing  $\underline{V}(\underline{\epsilon})$  using equation (17), taking the natural log, and multiplying by  $-2$  produces the maximum-likelihood objective function:

$$S'(\underline{b}) = -2\ln(\ell(\underline{b}|y)) = ND \ln 2\pi - \ln\left|\frac{1}{\sigma^2} \underline{\omega}\right| + \underline{e}^T \left[\frac{1}{\sigma^2} \underline{\omega}\right] \underline{e}, \quad (47)$$

where  $\sigma^2$  is the common variance, which was defined after equation (17) of this report. Because of the multiplication by a negative number, the maximization problem becomes a minimization problem, and the objective is to determine the parameter estimates that minimize equation (47). To include prior estimates of the parameters,  $\underline{e}$  and  $\underline{\omega}$  are augmented as in equations



(31) and (33), and ND is replaced by ND+NPR. To calculate equation (47), the determinant is expanded by using equation (33) to yield:

$$S'(\underline{b}) = (ND+NPR) \ln 2\pi + (ND+NPR) \ln \sigma^2 \\ - \ln |\underline{\omega}_d| - \ln |\underline{\omega}_p| + \underline{e}^T \left( \frac{1}{\sigma^2} \underline{\omega} \right) \underline{e}, \quad (48)$$

where  $\underline{\omega}_d$  and  $\underline{\omega}_p$  are the sections of the weight matrix applicable to dependent variable observations and prior estimates of the parameters, respectively.

For any assumed model, set of observations, and estimated weight matrix used in the parameter-estimation procedure,  $\underline{\omega}$  is replaced by  $\hat{\underline{\omega}}$ , and ND,  $\sigma^2$ , and  $\underline{\omega}$  are constant. Eliminating terms of equation (48) that do not depend on  $\underline{b}$  and multiplying by  $\sigma^2$  yields:

$$S(\underline{b}) = \underline{e}^T \hat{\underline{\omega}} \underline{e}. \quad (49)$$

Thus, for the optimization process, the maximum-likelihood objective function equals the sum-of-squares objective function (eq. 18).

The development of the least-squares objective function from the maximum-likelihood objective function differs from the development of equations (11) or (18) because equation (46) requires that the true errors be from a joint, normal distribution.

### The Sum-of-Squares Objective Function in Nonlinear Problems

In nonlinear problems, the sum-of-squares objective function generally is not elliptical as it was for linear problems, as shown in figures 16 and 17. The minimum cannot be determined in one solution of the normal equations, as was possible in linear regression, because the sensitivities change as the parameter values change. Thus, optimal parameter values are determined by an iterative process comprised of repeatedly solving the normal equations. How two parameter values changed in one ground-water flow problem for eight parameter-estimation iterations is shown in figure 17. As discussed in the following sections, the iterations stop when specified convergence criteria are met.

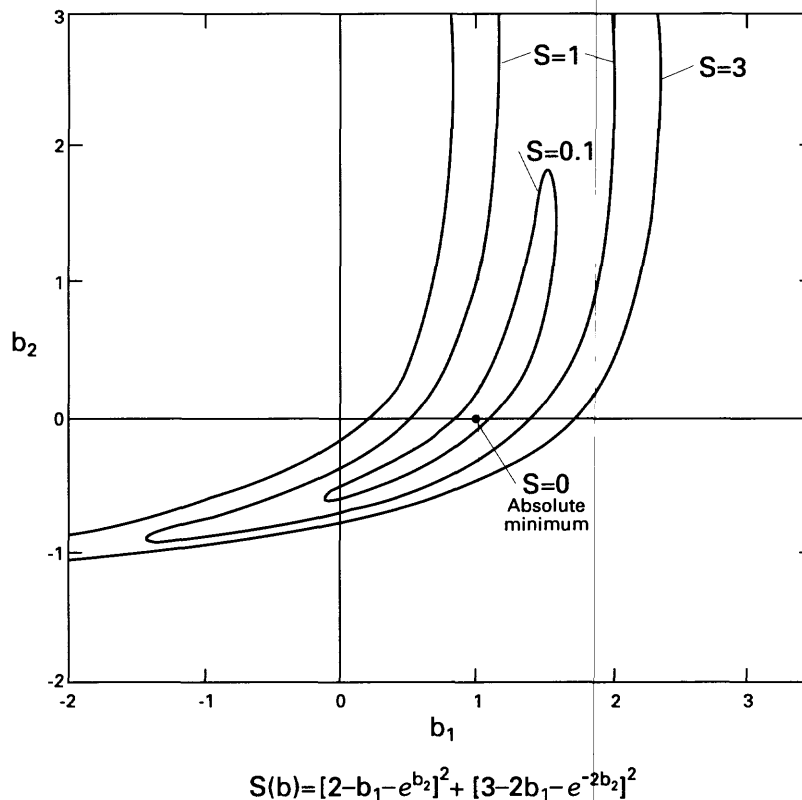
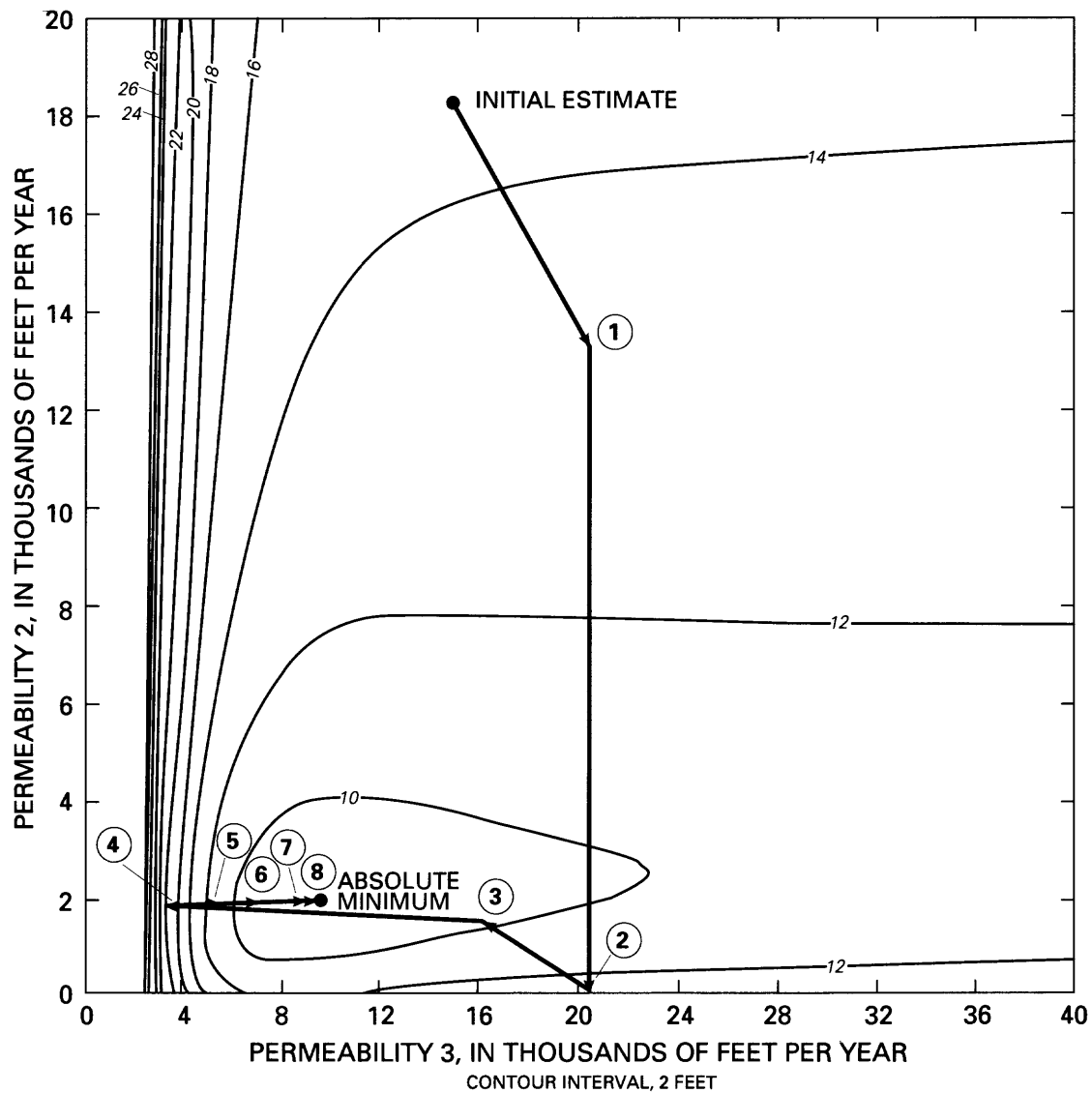


Figure 16.--Sum-of-squares objective function  $[S(\underline{b})]$  surface for a problem that is nonlinear in parameters  $\beta_1$  and  $\beta_2$  (modified from Beck and Arnold, 1977, p. 347; used with permission of the publisher).



#### EXPLANATION

- ③ PARAMETER ESTIMATES AFTER THE THIRD  
PARAMETER-ESTIMATION ITERATION

Figure 17.--Sum-of-squares objective function surface for a nonlinear problem showing parameter estimates at parameter-estimation iterations (modified from McLaughlin, 1975, p. VI-9).

## The Modified Gauss-Newton Optimization Method and Quasi-Newton Updating

The Parameter-Estimation Package is designed to perform modified Gauss-Newton optimization for any of the problems that the package can represent. Problems with observed head-dependent boundary flow gains and losses and problems with water-table aquifers that go dry at some finite-difference cells for any of the estimated parameter values are included. Modified Gauss-Newton optimization and related methods are discussed by Himmelblau (1972), Bard (1974), Beck and Arnold (1977), Cooley (1983b), and Cooley and Naff (1990), and much of this section is condensed from their discussions.

### Iterative Equations

The normal equations and the iterative process for the modified Gauss-Newton optimization method are discussed by Cooley and Naff (1990, ch. 3), and can be expressed as:

$$(\underline{C}^T \underline{X}_r^T \hat{\omega} \underline{X}_r \underline{C} + \underline{I} \mu_r) \underline{C}^{-1} \underline{d}_r = \underline{C}^T \underline{X}_r^T \hat{\omega} (y - \hat{y}_r) \quad (50a)$$

$$\underline{b}_{r+1} = \rho_r \underline{d}_r + \underline{b}_r \quad (50b)$$

where

$\underline{C}$  is a diagonal scaling matrix with element  $c_{ii}$  equal to  $(\underline{X}_r^T \hat{\omega} \underline{X}_r)^{-1/2}_{ii}$ , which produces a scaled matrix with the smallest possible condition number (Forsythe and Strauss, 1955);

$\underline{X}_r$  is the sensitivity matrix evaluated at parameter estimates  $\underline{b}_r$ ;

$\hat{r}$  is the parameter-estimation iteration number;

$\hat{\omega}$  is the weight matrix;

$\underline{d}_r$  is a vector used to update the parameter estimates;

$\mu_r$  is the Marquardt parameter (Marquardt, 1963); and

$\rho_r$  is a damping parameter.

Calculation of the elements of  $\underline{X}_r$  is described in the section of this report "Sensitivity-Equation Method of Calculating Sensitivities".

For problems with large residuals and a large degree of nonlinearity, Dennis, Gay, and Welsch (1981) suggested substituting  $\underline{X}_r^T \hat{\omega} \underline{X}_r + \underline{R}_r$  for  $\underline{X}_r^T \hat{\omega} \underline{X}_r$  in equation (50a) at selected iterations, where  $\underline{R}_r$  is an estimate of the difference between  $\underline{X}_r^T \hat{\omega} \underline{X}_r$  and the Hessian matrix, and is calculated by quasi-Newton updating as (Dennis, Gay, and Welsch, 1981):

$$\begin{aligned} \underline{R}_r &= \underline{0} & r &= 0 \\ \underline{R}_r &= t\underline{R}_{r-1} + \frac{\underline{u} \Delta \underline{g}_r^T + \Delta \underline{g}_r \underline{u}^T}{\underline{d}_{r-1}^T \Delta \underline{g}_r} - \frac{\underline{d}_{r-1}^T \underline{u} \Delta \underline{g}_r \Delta \underline{g}_r^T}{\left( \underline{d}_{r-1}^T \Delta \underline{g}_r \right)^2} & r &> 0 \end{aligned} \quad (51)$$

where

$$\begin{aligned} \Delta \underline{g}_r &= \underline{g}_r - \underline{g}_{r-1} \\ \underline{g}_r &= - \underline{X}_r^T \hat{\omega} \underline{e}_r \\ \underline{u} &= (\underline{X}_r - \underline{X}_{r-1})^T \hat{\omega} \underline{e}_r - t\underline{R}_{r-1} \underline{d}_{r-1} \\ t &= \min \left\{ \left| \underline{d}_{r-1}^T (\underline{X}_r - \underline{X}_{r-1})^T \hat{\omega} \underline{e}_r / (\underline{d}_{r-1}^T \underline{R}_{r-1} \underline{d}_{r-1}) \right|; 1.0 \right\}, \end{aligned}$$

and all other variables are defined after equations (10) and (50).

$\underline{R}_r$  is calculated starting at  $r=1$ , but is only included in equation (50a) in later iterations. Performance of the method depends on when  $\underline{R}_r$  is included. R.L. Cooley and M.C. Hill (in press) found that generally it is best to include  $\underline{R}_r$  after the sum of squared, weighted residuals is no longer changing very much at each parameter-estimation iteration. In the Parameter-Estimation Package,  $\underline{R}_r$  is included for all iterations after the sum of squared, weighted residuals decreases by less than a user-defined percentage over two iterations (see SOSR of DATA SET 13 of the INPUT FILE instructions in DATA SET 13), or after a user-specified number of iterations (NFIT of DATA SET 13). The more elaborate criteria for inclusion of  $\underline{R}_r$  suggested by Dennis, Gay and Welsch (1981) require additional model simulations. Considering the large problems that are expected to be simulated with MODFLOWP, the more elaborate criteria seemed impractical and were not included in the Parameter-Estimation Package. When  $\underline{R}_r$  is included

in equation (50a), the elements of the diagonal scaling matrix,  $\underline{C}$ , are calculated as  $(\underline{X}_r^T \hat{\omega} \underline{X}_r + \underline{R})_{ii}^{-1/2}$ .

In the Parameter-Estimation Package, initially  $\mu_r = 0$  for each parameter-estimation iteration  $r$ . For iterations in which the condition described by Cooley and Naff (1990, p. 71-72) is met using  $\mu_r = 0$ ,  $\mu_r$  is increased according to  $\mu_r^{\text{new}} = 1.5 \mu_r^{\text{old}} + 0.001$  until the condition is no longer met.

The damping parameter,  $\rho_r$ , can vary in value from 0.0 to 1.0, and changes the magnitude, but not the direction of  $\underline{d}_r$ . The damping parameter is used to ensure that the absolute values of fractional parameter value changes, defined for any parameter  $i$  as  $(b_i^{r+1} - b_i^r)/b_i^r$ , where  $b_i^r$  is the  $i$ th element of vector  $\underline{b}_r$ , are all less than a value specified by the user (DMAX of Appendix A and C), and to damp oscillations that occur when elements in  $\underline{d}_r$  and  $\underline{d}_{r-1}$  define opposite directions.

For log-transformed parameter  $i$ , requiring that the absolute value of  $(b_i^{r+1} - b_i^r)/b_i^r$  be less than DMAX produces inconsistent results, as illustrated by the following example. If the estimated parameter is  $\ln K$ , where  $K$  is hydraulic conductivity, and  $\text{DMAX} = 2.0$ , placing the restriction on  $\ln K$  would require that  $(\ln K)^{r+1}$  be between  $(\ln K)^r - 2.0(\ln K)^r$  and  $(\ln K)^r + 2.0(\ln K)^r$ . If  $K$  at parameter-estimation iteration  $r$  is close to 1.0, say  $K = 1.1$ , the restriction would require  $(\ln K)^{r+1}$  to be between -0.95 and 2.85, so that  $K^{r+1}$  would be required to be within the narrow range 0.91 and 1.33. If  $K$  at parameter-estimation iteration  $r$  is far from 1.0, say  $K = 1 \times 10^{-4}$ , the restriction requires that  $(\ln K)^{r+1}$  be between -27.63 and 9.21, so that  $K^{r+1}$  would be allowed to vary within the very wide range of  $1 \times 10^{-12}$  and 2.22. More physically meaningful limitations are produced if the restriction is placed on the exponential of the estimated parameter, which, in this example, is  $\exp(\ln K) = K$ . Then, in the first situation,  $\text{DMAX} = 2.0$  would require  $K$  to be between 0.0 and 3.3, where the lower limit of 0.0 is a result of estimating a log-transformed parameter, and is always the lower limit for a log-transformed parameter when  $\text{DMAX} \geq 1.0$ . In the second situation,  $\text{DMAX} = 2.0$  would require  $K$  to be between 0.0 and  $3 \times 10^{-4}$ .

Calculation of the damping parameter is based on the method described by Cooley (1983b, p. 1274), modified for when one or more of the parameters are

log-transformed. In this method,  $ADMX_r$  is defined as the maximum absolute value of the fractional parameter changes defined by  $\underline{d}_r$ . Thus,

$$ADMX_r = \max_i \begin{cases} |d_i^r/b_i^r| & \text{for untransformed parameters} \\ |\exp(d_i^r)-1.0| & \text{for log-transformed parameters} \end{cases} \quad (52)$$

where  $d_i^r$  is the  $i$ th element of vector  $\underline{d}_r$ ,  $b_i^r$  is the  $i$ th element of vector  $\underline{b}_r$ , and  $b_i^0$  replaces  $b_i^r$  if  $|b_i^r| < |b_i^0|/10^3$ . The expression for log-transformed parameters is derived by noting that the fractional change of the physically relevant parameter equals  $(\exp(b_i^{r+1}) - \exp(b_i^r))/\exp(b_i^r)$ , which equals  $(\exp(b_i^{r+1})/\exp(b_i^r))-1.0$ . Substituting  $\exp(d_i^r) = \exp(b_i^{r+1})/\exp(b_i^r)$ , which is derived from equation (50b) with  $\rho_r = 1.0$ , yields the expression for log-transformed parameters. An exception to equation (52) occurs if  $DMAX \geq 1.0$ , because, as mentioned previously, the exponential of a log-transformed parameter is always greater than 0.0, and can never decrease enough to require  $\rho_r$  to be less than 1.0 if  $DMAX \geq 1.0$ . Thus, if  $d_i^r < 0$  for a log-transformed parameter and  $DMAX \geq 1.0$ , parameter  $i$  is excluded from consideration in equation (52).

If  $j$  is the parameter for which  $ADMX_r$  is a maximum,  $DMX_r$  is defined as  $d_j^r/b_j^r$  if parameter  $j$  is untransformed (again,  $b_j^0$  is used if  $|b_j^r| < |b_j^0|/10^3$ ), and  $\exp(d_j^r)-1.0$  if parameter  $j$  is log-transformed. A preliminary damping parameter,  $\rho_r^*$ , is calculated to minimize oscillations according to:

$$\rho_r^* = 1 \quad \begin{array}{l} r=0 \text{ or } j \text{ is not the same for} \\ \text{iterations } r \text{ and } r+1 \end{array} \quad (53a)$$

$$\left. \begin{array}{ll} s = DMX_r/(\rho_{r-1} DMX_{r-1}) \\ \text{If } s \geq -1 & \rho_r^* = \frac{3+s}{3+|s|} \\ \text{If } s < -1 & \rho_r^* = 1/(2|s|) \end{array} \right\} \begin{array}{l} r > 0 \text{ and } j \text{ is the same for} \\ \text{iterations } r \text{ and } r+1, \end{array} \quad (53b)$$

where the condition on  $j$  has been added to Cooley's (1983b) method. The damping parameter is then calculated as:

$$\begin{aligned} \rho_r &= \rho_r^* & \text{if } \rho_r^* \text{ ADMX}_r \leq \text{DMAX} \\ \rho_r &= \text{DMAX}/\text{ADMX}_r & \text{if } \rho_r^* \text{ ADMX}_r > \text{DMAX} \end{aligned} \quad (54a)$$

if parameter j is untransformed, and

$$\begin{aligned} \rho_r &= \rho_r^* & \text{if } d_j^r > 0.0 \text{ and } \rho_r^* d_j^r \leq \ln(\text{DMAX}+1.0), \\ & & \text{or } d_j^r < 0.0, \rho_r^* d_j^r \leq \ln(1.0-\text{DMAX}), \\ & & \text{and } \text{DMAX} < 1.0 \end{aligned} \quad (54b)$$

$$\rho_r = (\ln(\text{DMAX}+1.0))/d_j^r \quad \text{if } d_j^r > 0.0 \text{ and } \rho_r^* d_j^r > \ln(\text{DMAX}+1.0),$$

$$\rho_r = (\ln(1.0-\text{DMAX}))/d_j^r \quad \text{if } d_j^r < 0.0, \rho_r^* d_j^r > \ln(1.0-\text{DMAX}), \\ \text{and } \text{DMAX} < 1.0.$$

if parameter j is log-transformed. The expressions for log-transformed parameters are derived using the properties discussed after equation (52): the DMAX restriction requires that, if  $d_j^r > 0.0$ ,  $(\exp(b_j^{r+1})/\exp(b_j^r))-1.0 \leq \text{DMAX}$ , or  $\rho_r d_j^r \leq \ln(\text{DMAX}+1.0)$ ; if  $d_j^r < 0.0$  and  $\text{DMAX} < 1.0$ ,  $(\exp(b_j^{r+1})/\exp(b_j^r))-1.0 > -\text{DMAX}$ , or  $\rho_r d_j^r > \ln(1.0-\text{DMAX})$ . No special restrictions are required to prohibit a large decrease in a log-transformed parameter for  $\text{DMAX} \geq 1.0$  because the log-transform itself restricts the physical value of the parameter to positive values.'

Typically DMAX is larger than 1.0 and less than about 2.0. Values less than 1.0 can be used if parameter-value oscillations are a problem, but note that values less than 1.0 prohibit parameter values from changing sign.

As discussed by Cooley and Naff (1990, p. 70), modified Gauss-Newton optimization typically converges within "\*\*\*a number of iterations equal to five or twice the number of parameters, whichever is greater." Convergence will tend to occur sooner for well-conditioned problems, and later for poorly conditioned problems.

Using double precision as suggested by Stewart (1972, p. 226-227), equation (50a) has been solved accurately and efficiently in many



applications of MODFLOWP using Cholesky  $LDL^T$  decomposition (Dennis and Schnabel, 1983, p. 50-51). Exceptions were plagued by strong correlations between parameters or insensitive parameters, and were resolved by reparameterization. Dennis and Schnabel (1983, p. 221) and Seber and Wild (1989, p. 621) suggest that solving the alternative formulation  $\underline{X} \underline{d} = (\underline{y} - \hat{\underline{y}})$  using QR or singular-value decomposition (Dennis and Schnabel, 1983, p. 49-51; Seber and Wild, 1989, p. 680-681; Press and others, 1989, p. 52-63) is more stable, but it is unclear whether or not they used the scaling and Marquardt parameter which adds stability to equation (50a). Press and others (1989, p. 515-520) suggest using singular-value decomposition for linear regression, but use Gauss-Jordan elimination to solve a variation of equation (50a) that includes similar scaling and implementation of the Marquardt parameter for nonlinear regression. Considering the success experienced using Cholesky decomposition and the lack of any clear indication that the alternatives are better, Cholesky decomposition is used in the Parameter-Estimation Package of this report.

#### Convergence Criteria

Convergence of the modified Gauss-Newton iterative process is achieved when either of two criteria are satisfied. The first convergence criterion is based on the fact that, for well-posed problems, the iterative process defined by equations (50a) and (50b) produces parameter estimates,  $\underline{b}_r$ , that are progressively closer to the values associated with the minimum of the sum-of-squares objective function. As this minimum is reached, the right-hand side of (50a) and, therefore,  $\underline{d}_r$  approach zero. Thus, the first criterion is that the largest absolute value of  $d_i/b_i$ ,  $i=1, NP$ , is less than a user-defined convergence criterion (TOL of Appendices A and C), where  $d_i$  is the  $i$ th element of  $\underline{d}_r$  and  $b_i$  is the  $i$ th element of  $\underline{b}_r$  (eq. 50a). For log-transformed parameters, a process similar to the one described above produces the requirement that the largest absolute value of  $\exp(d_i)-1$ ,  $i=1, NP$ , needs to be less than the convergence criterion.

The second convergence criterion is satisfied if the sum of squared, weighted residuals does not change by more than a user-defined percentage over three consecutive iterations. This criterion allows parameter estimation to be completed and final statistics to be printed when parameters vary in the vicinity of the minimum, but never quite satisfy the

first convergence criterion. This most frequently occurs when there is at least one insensitive parameter. Insensitive parameters generally have large variances, and the user needs to consider reparameterizing the problem if there are insensitive parameters.

### Conjugate-Direction Optimization Methods

The Parameter-Estimation Package is designed to perform conjugate-direction optimization when hydraulic heads or changes in hydraulic heads are the only dependent-variable observations, and water-table aquifers remain saturated at all finite-difference cells for all estimated parameter values. These restrictions are not required for conjugate-direction methods, but the program presented in this report does not support the use of conjugate-direction methods on these more complicated problems. Conjugate-direction optimization is discussed by Himmelblau (1972), Neuman (1980, 1982), Cooley (1985), and Carrera and Neuman (1986b), and this section is condensed from their discussions.

Neuman (1980, 1982) and Carrera and Neuman (1986b) use the term conjugate gradient to describe the methods classified as conjugate direction in this report. A change in terminology is justified because the methods are not truly conjugate-gradient methods, as defined by Himmelblau (1972, p. 88). The choice of the term conjugate direction is derived from Himmelblau (1972, p. 105).

### Iterative Equations

Conjugate-direction optimization is accomplished by using the gradient vector,  $\mathbf{g}_r$ , which has components equal to:

$$g_i = \frac{\partial S(\underline{b}_r)}{\partial b_i} \quad i = 1, NP \quad (55)$$

where  $r$  is the parameter-estimation iteration number. The gradient is equivalent to the unscaled right-hand side of equation (50a) multiplied by -2, but is calculated by the adjoint-state method, which is discussed in the section of this report "Adjoint-State Method of Calculating the Gradient of the Objective Function". The adjoint-state method of calculating the gradient takes much less computer time in most problems than using a method

that requires the sensitivity matrix,  $\underline{X}$ . To define the direction of parameter change,  $\underline{d}_r$ , the gradient vector is modified by an approximation of  $(\underline{X}^T \hat{\omega} \underline{X})^{-1}$ , the inverse of the unscaled matrix on the left-hand side of equation (50a) with  $\mu_r=0$ . An approximation is used to avoid calculating the sensitivity matrix,  $\underline{X}$ . The Fletcher-Reeves and quasi-Newton methods discussed below differ in how the matrix inverse is approximated. Carrera and Neuman (1986b) also discuss a combined method in which the Fletcher-Reeves method is used in the first parameter-estimation iterations, and the quasi-Newton method is used in later iterations. In the Parameter-Estimation Package, the user can specify how many Fletcher-Reeves iterations to use in the combined method.

To produce a better-conditioned problem,  $\underline{g}$  is scaled as  $\underline{C} \underline{g}$ ,  $\underline{d}$  is scaled as  $\underline{C}^{-1} \underline{d}$ , and the matrix to be approximated is scaled as  $(\underline{C}^T \underline{X}_r^T \hat{\omega} \underline{X}_r \underline{C})^{-1}$  where the diagonal elements of the scaling matrix,  $\underline{C}$ , are defined by the user. The performance of the conjugate-direction methods is substantially affected by the scaling. Ideally, the  $c_{ii}$  would be equal to the values used in modified Gauss-Newton optimization (discussed after eq. 50a), but because  $\underline{X}$  is unknown, those values can not be calculated for conjugate-direction optimization. Scale factors are similar in value to the related parameter (Cooley, 1985, tables 1, 4, and 9), but optimal values can be determined only by trial and error. Taking the natural log of the parameter also is a form of scaling and might decrease the number of parameter-estimation iterations required for some problems.

For each parameter-estimation iteration, the updated parameter estimates are calculated as:

$$\underline{b}_{r+1} = \rho_r \underline{d}_r + \underline{b}_r, \quad (56)$$

where  $\rho_r$  is calculated by Newton's method, as described below. If the maximum fractional parameter change calculated by equation (56) is greater than the value specified by DMAX of the INPUT FILE (see Appendix A),  $\rho_r$  is decreased using the method described for the modified Gauss-Newton method (eqs. 52, 53, and 54), except that  $\rho_r^* = 1.0$  for all iterations.

Conjugate-direction optimization typically requires many more iterations than is required by modified Gauss-Newton optimization. Even simple problems might require about 50 iterations (Cooley, 1985; Hill, 1990a), and 100 iterations might not be excessive for some problems.

#### Fletcher-Reeves Method of Approximating the Matrix Inverse

In the Fletcher-Reeves method, the scaled direction of parameter change is calculated as:

$$\underline{C}^{-1} \underline{d}_{r+1} = - \underline{C} \underline{g}_r + \alpha_r \underline{C}^{-1} \underline{d}_r \quad (57)$$

$$\alpha_r = 0 \quad r = n \times NP$$

$$\alpha_r = \frac{(\underline{C} \underline{g}_r)^T \underline{C} \underline{g}_r}{(\underline{C} \underline{g}_{r-1})^T \underline{C} \underline{g}_{r-1}} \quad r \neq n \times NP,$$

where

$\underline{g}_r$  is the gradient calculated by using parameter estimates  $\underline{b}_r$ ;

$\underline{d}_r$  is the direction of parameter change for iteration  $r$ ;

$\alpha_r$  is an iteration parameter for iteration  $r$ ;  $n=0,1,2 \dots$ ; and

$NP$  is the number of estimated parameters.

Equation (57) can be rewritten as (modified from Cooley, 1985, p. 1531):

$$\underline{C}^{-1} \underline{d}_{r+1} = - \left[ \underline{I} - \frac{\underline{C}^{-1} \underline{d}_r (\underline{C} \underline{g}_r)^T}{(\underline{C} \underline{g}_{r-1})^T \underline{C} \underline{g}_{r-1}} \right] \underline{C} \underline{g}_r, \quad (58)$$

where  $\underline{I}$  is an  $NP$  by  $NP$  identity matrix. The approximation of the inverse of the matrix on the left-hand side of equation (50a) with  $\mu_r=0$  is the expression multiplying  $\underline{C} \underline{g}_r$  on the right-hand side of equation (58).

#### Quasi-Newton Method of Approximating the Matrix Inverse

In the quasi-Newton method, the direction of parameter change is calculated as:

$$\underline{C}^{-1} \underline{d}_{r+1} = - \underline{H}_r \underline{C} \underline{g}_r, \quad (59)$$

where

$$\underline{H}_r = \text{diag}((b_1/c_{1,1})^2, (b_2/c_{2,2})^2, \dots (b_{NP}/c_{NP,NP})^2) \quad r = 0$$

$$\begin{aligned} \underline{H}_r = & \left[ \underline{H}_{r-1} - \frac{\underline{H}_{r-1} \underline{C}(\Delta \underline{g}_r) \underline{d}_r^T \underline{C}^{-1} + \underline{C}^{-1} \underline{d}_r (\Delta \underline{g}_r)^T \underline{C} \underline{H}_{r-1}}{\underline{d}_r^T (\Delta \underline{g}_r)} \right] \gamma_r \\ & + \left[ \rho_{r-1} + \frac{\gamma_r (\Delta \underline{g}_r)^T \underline{C} \underline{H}_{r-1} \underline{C}(\Delta \underline{g}_r)}{\underline{d}_r^T (\Delta \underline{g}_r)} \right] \frac{\underline{C}^{-1} \underline{d}_r^T \underline{d}_r \underline{C}^{-1}}{\underline{d}_r^T (\Delta \underline{g}_r)} \quad r > 0 \end{aligned}$$

$$\Delta \underline{g}_r = \underline{g}_r - \underline{g}_{r-1}$$

$$\gamma_r = \frac{\rho_{r-1} \underline{d}_r^T (\Delta \underline{g}_r)}{(\Delta \underline{g}_r)^T \underline{C} \underline{H}_{r-1} \underline{C}(\Delta \underline{g}_r)} \quad r = 1$$

$$\gamma_r = 1 \quad r > 1,$$

and  $\rho_{r-1}$  is the iteration parameter calculated using Newton's method, as described below.

#### Newton's Method of Calculating the Iteration Parameter

Once the direction of parameter change is calculated, the updated parameter values are calculated using equation (56). Calculation of  $\rho_r$  by Newton's method (Neuman, 1980, p. 337) is accomplished in three steps. First,  $\partial \underline{h} / \partial \rho_r$ , the derivative of hydraulic head with respect to the iteration parameter, is calculated by solving:

$$\underline{A}(n) \frac{\partial \underline{h}(n)}{\partial \rho_r} - \underline{B}(n) \frac{\partial \underline{h}(n-1)}{\partial \rho_r} = \underline{a}(n), \quad (60)$$

where  $\underline{A}(n)$ ,  $\underline{h}(n)$ , and  $\underline{B}(n)$  were defined after equation (3), and

$$\underline{a}(n) = \sum_{i=1}^{NP} d_i \left[ \frac{-\partial \underline{A}(n)}{\partial b_i} \underline{h}(n) + \frac{\partial \underline{B}(n-1)}{\partial b_i} \underline{h}(n-1) - \frac{\partial \underline{f}(n)}{\partial b_i} \right], \quad (61)$$

where,  $d_i$  is the  $i^{\text{th}}$  element of  $\underline{d}_r$ . For steady-state conditions ( $n=0$ ),  $\underline{B}(n)$  of equations (60) and (61) equals zero, and the storage terms in  $\underline{A}$  equal zero.

In the second step, the  $\partial \hat{h}/\partial \rho_r$  are used to calculate  $\partial \hat{y}/\partial \rho_r$  by using the methods used to calculate  $\hat{y}$  from  $\hat{h}$  discussed in the "Observations" section of this report, where the  $\partial \hat{h}/\partial \rho_r$  and  $\partial \hat{y}/\partial \rho_r$  are substituted for  $\hat{h}$  and  $\hat{y}$ . The resulting ND-length vector is used to accomplish the third step of Newton's method, in which:

$$\rho_r = \frac{\underline{t}_r^T \hat{\underline{\omega}}_d \underline{e}_d + \underline{d}_{r+1}^T \hat{\underline{\omega}}_p \underline{e}_p}{\underline{t}_r^T \hat{\underline{\omega}}_d \underline{t}_r + \underline{d}_{r+1}^T \hat{\underline{\omega}}_p \underline{C}_{d_{r+1}}}, \quad (62)$$

where,  $\underline{t}_r = \partial \hat{y}/\partial \rho_r$ ;  $\underline{e}_d$  is the partition of  $\underline{e}$  which relates to the dependent-variable data;  $\hat{\underline{\omega}}_d$  is the partition of  $\hat{\underline{\omega}}$  which relate to the dependent variable data;  $\underline{e}_p$  is the partition of  $\underline{e}$  which relates to the prior estimates of the parameters; and  $\hat{\underline{\omega}}_p$  is the partition of  $\hat{\underline{\omega}}$ , which relates to the prior estimates of the parameters (see section "Prior Information on the Estimated Parameters").

#### Convergence Criteria and Iteration Control

The conjugate-direction optimization methods are said to converge when the absolute value of the largest element of  $\underline{g}_r$  (eq. 55) and the absolute value of the largest element of  $\rho_r \underline{d}_r$  divided by the corresponding element of  $\underline{b}$ , (eq. 56) are smaller than a user-defined convergence criterion.

At each conjugate-direction iteration, two items are checked to ensure that the parameter-estimation procedure is progressing satisfactorily. First, the value of the objective function is checked. If the value increases by more than 0.0001 (a small nonzero value is used to accommodate round-off error), it is assumed that the iteration parameter calculated by Newton's method is too large. A new set of parameters is calculated as:

$$\underline{b}'_{r+1} = \underline{b}_{r+1} - \sum_{m=1}^n \frac{1}{2^m} \rho_r \underline{d}_r, \quad (63)$$

where  $n$  is the number of times that the change in the parameters has been reduced and  $m$  is a dummy variable used in the summation. As many as five reductions might occur within a single parameter-estimation iteration. The iteration process continues if the new parameters produce an objective-function value that is no more than 0.0001 larger than the objective-

function value from the previous iteration. If the objective-function value has not satisfied this criterion after five reductions, execution stops.

[The above discussion is modified from Neuman (1980) and R. L. Cooley (U.S. Geological Survey, written commun., 1989.)

Second, the progress of quasi-Newton iterations is checked by comparing the change in the gradient between iterations ( $\underline{g}_r - \underline{g}_{r-1}$ ) and the parameter change direction vector,  $\underline{d}_{r-1}$ . If the value of  $(\underline{g}_r - \underline{g}_{r-1})^T \underline{d}_{r-1}$  is zero or negative,  $\underline{d}_{r-1}$  is not a descent direction, and  $\underline{H}$  is not updated for that iteration (Shanno, 1978; R.L. Cooley, written commun., 1989).

#### Relative Efficiency of the Optimization Methods

The modified Gauss-Newton and conjugate-direction optimization methods discussed in this report have been compared by using steady-state ground-water flow test cases (Cooley, 1985), and using steady-state and transient ground-water flow test cases (Hill, 1990a). Their results indicate that the modified Gauss-Newton method estimates parameters by using much less computer processing time (less than 50 percent with a direct D4 solver; less than 80 percent with a conjugate-gradient solver with the modified incomplete Cholesky preconditioner), and slightly more computer storage (as much as 6 percent) than the conjugate-direction optimization methods. The decrease in computer storage is lost if statistics requiring the calculation of the sensitivity matrix,  $\underline{X}_r$ , are calculated for the conjugate-direction methods. The modified Gauss-Newton method also has the advantage of not requiring user-defined scaling. Despite its apparent inefficiency and disadvantages, conjugate-direction optimization was retained in the Parameter-Estimation Package so it could be compared with the modified Gauss-Newton method for a greater range of problems.

Odenwald and Herrling (1990) optimized a regression problem using several iterations of a conjugate-direction optimization method followed by modified Gauss-Newton optimization iterations. For the final iterations, a full Newton optimization method (Gill and others, 1981) was used. Although Odenwald and Herrling (1990) did not compare this optimization procedure with using each method individually, it is likely that combined methods produce more efficient optimization, and this is a promising area of further research.

R.L. Cooley and M.C. Hill (in press) showed that using the quasi-Newton updating of equation (51) can dramatically reduce the number of iterations required to estimate parameters for problems in which modified Gauss-Newton converges slowly. Convergence is considered to be slow if the number of parameter-estimation iterations required exceeds the number of estimated parameters. If modified Gauss-Newton converges quickly, there is no advantage to using the quasi-Newton updating.

#### Analysis of Results for Nonlinear Problems

When using nonlinear regression, final parameter estimates and the assumed model can be analyzed by using the same methods used for linear models (see "Analysis of Results for Linear Problems" of this report). When optimizing with the modified Gauss-Newton method, the statistics calculated by using the sensitivity matrix,  $\underline{X}$ , such as variance-covariance matrix for the final parameters (eq. 35), are generally calculated by using the sensitivity matrix from the last parameter-estimation iteration ( $\underline{X}_r$  of eq. 50a). When optimizing with a conjugate-direction method, these statistics are available only if the sensitivity matrix is calculated by using the final parameter estimates. This capability is provided as an option in the Parameter-Estimation Package.

Nonlinearity produces several problems in the analysis of results. First, in nonlinear problems, the estimated error variance,  $s^2$ , might not be an unbiased estimate of the true error variance, even if the model is correct (Draper and Smith, 1981, p. 484), and unbiasedness generally is not possible in nonlinear problems (Bard, 1974, p. 40). Fortunately, for typical ground-water flow problems the bias caused by nonlinearity is not large, and  $s^2$  can be used as described for linear problems. Second, the confidence intervals on parameter values for linear problems (eq. 36) might not be valid (Donaldson and Schnabel, 1987), and alternative methods, such as those described by Vecchia and Cooley (1987) might need to be used. The alternative methods are not included as part of the Parameter-Estimation Package presented in this report.

Additional statistics developed with the maximum-likelihood objective function can be used for model discrimination. The first statistic is the value of the maximum-likelihood objective function itself (eq. 48),



evaluated at the minimized parameter values,  $b'$ . In many circumstances, smaller values of  $S'(b')$  indicate better models. As more parameters are added, however, the residuals,  $e$ , and, therefore,  $S'(b)$ , generally become smaller, and the user might draw the incorrect conclusion that models with more parameters generally are better. To reflect the fact that adding too many parameters produces unreliable parameter estimates, two additional statistics have been developed that are equal to the sum of  $S'(b')$  and terms that become large as more parameters are added. Although these statistics were developed for time-series problems, Carrera and Neuman (1986a and c) successfully used them to discriminate between different parameterizations of a test case of ground-water flow. The statistics are stated below; see the cited references for their derivations and additional discussion.

The second statistic (AIC) was developed by Akaike (1974) and equals:

$$AIC(b') = S'(b') + 2 \times NP. \quad (64)$$

The third statistic (BIC) also was developed by Akaike (1978) as a response to concern that  $AIC(b')$  sometimes promoted use of more parameters than was required. The version of this statistic used by Carrera and Neuman (1986a and c) is:

$$BIC(b') = S'(b') + NP \times \ln(ND+NPR+MPR). \quad (65)$$

For both statistics, smaller values indicate a more accurate model. If the statistics for a model with fewer parameters are only slightly larger than the statistics of another model, however, it might be better to select the model with fewer parameters, unless the investigator has other information indicating the validity of the more complicated model.

#### Dry Cells in Water-Table Layers

If the top model layer is designated as a water-table layer (Block-Centered Flow Package: LAYCON=1), some cells might go dry and become inactive. In the Parameter-Estimation Package, only the modified Gauss-Newton optimization method with ISN=-1 (LINE 6 of the INPUT FILE) is designed to accommodate dry cells. At the beginning of each parameter-estimation iteration, the hydraulic-conductance and IBOUND arrays (McDonald

and Harbaugh, 1988) are adjusted to make all dry cells active again, so conditions are the same at the beginning of each parameter-estimation iteration.

#### CALCULATING SENSITIVITY-EQUATION SENSITIVITIES AND THE GRADIENT OF THE OBJECTIVE FUNCTION

Modified Gauss-Newton optimization requires ND derivatives with respect to each of the parameters. These derivatives, or sensitivities, can be expressed as  $\partial \hat{y}_q / \partial b_\ell$ ,  $q=1, ND$ ,  $\ell=1, NP$ , and are the elements of an ND by NP matrix. Conjugate-direction optimization requires one derivative with respect to each of the parameters. These derivatives can be expressed as  $\partial S(\underline{b}) / \partial b_\ell$ ,  $\ell=1, NP$ , and are the elements of the gradient of the objective function,  $\underline{g}_r$  (eq. 55), which is a vector. Yeh (1986) showed that when the required number of derivatives with respect to each parameter was greater than the number of parameters, the derivatives could be calculated most efficiently using the sensitivity-equation method. Thus, the sensitivity-equation method is used to calculate the derivatives required for modified Gauss-Newton optimization. When the required number of derivatives with respect to each parameter is less than or equal to the number of parameters, Yeh (1986) showed that the adjoint-state method is most efficient. Thus, the adjoint-state method is used to calculate the derivatives required for conjugate-direction optimization. The sensitivity-equation method and the adjoint-state method are described in the following sections.

#### Sensitivity-Equation Method of Calculating Sensitivities

In modified Gauss-Newton optimization, the elements of the first ND rows of the sensitivity matrix ( $\underline{X}_r$  of eq. 50a) equal  $\partial \hat{y}_q / \partial b_\ell$ ,  $q=1, ND$ ,  $\ell=1, NP$ , where  $\hat{y}_q$  is an element of vector  $\hat{\underline{y}}$  (eq. 44). The columns of this partition of  $\underline{X}_r$  can each be expressed as the vector  $\partial \hat{\underline{y}} / \partial b_\ell$ . For simplicity in the following discussion, the subscript  $q$  is omitted, and a single component of the vector  $\partial \hat{\underline{y}} / \partial b_\ell$  is represented by  $\partial \hat{y} / \partial b_\ell$ . In the sensitivity-equation method, these elements are calculated from sensitivity-equation sensitivities,  $\partial \underline{h} / \partial b_\ell$ ,  $\ell=1, NP$ , where  $\underline{h}$  is defined after equation (3) and is a vector of hydraulic heads at every grid cell center and time step. For observations of hydraulic heads and changes in hydraulic heads, the  $\partial \hat{\underline{y}} / \partial b_\ell$  are calculated from the  $\partial \underline{h} / \partial b_\ell$  exactly as the  $\hat{\underline{y}}$  are calculated from the  $\underline{h}$ , as described in the section entitled "Observations".

For observations of head-dependent boundary gains and losses, the sensitivities are calculated by taking the derivative of equation (4). For parameters, such as transmissivity, that are not directly involved in the calculation of a gain or loss along the head-dependent boundary:

$$\hat{\partial y / \partial b}_\ell = \sum_{i=1}^{NQCL} \frac{\partial q_i}{\partial b_\ell} = - \sum_{i=1}^{NQCL} \frac{K_i}{D_i} A_i \frac{\partial h_i}{\partial b_\ell} \quad (66)$$

where all terms were defined after equation (4). Two examples are used to illustrate how  $\hat{\partial y / \partial b}_\ell$  is calculated when  $b_\ell$  is a function of  $K_i$  ( $b_\ell = f(K_i)$ ). First, if  $b_\ell = K_i$  for all NQCL cells of the head-dependent boundary:

$$\hat{\partial y / \partial b}_\ell = \sum_{i=1}^{NQCL} \left[ - \frac{K_i}{D_i} A_i \frac{\partial h_i}{\partial b_\ell} + \frac{A_i}{D_i} (H_i - h_i) \right]. \quad (67)$$

Second, if  $b_\ell = K_i / D_i$  for all NQCL cells of the head-dependent boundary:

$$\hat{\partial y / \partial b}_\ell = \sum_{i=1}^{NQCL} \left[ - \frac{K_i}{D_i} A_i \frac{\partial h_i}{\partial b_\ell} + A_i (H_i - h_i) \right]. \quad (68)$$

Three circumstances can affect the calculated  $\hat{\partial y / \partial b}_\ell$ , all of which decrease the effect of the head-dependent boundary gain-or-loss observation on parameter estimation.

First, if the head-dependent boundary is simulated using the Streamflow-Routing or River Package, and the simulated hydraulic head,  $h_i$ , is below the bottom of the streambed, the  $i$ th term of  $\hat{\partial y / \partial b}_\ell$  equals 0.0 unless  $b_\ell$  is a function of  $K_i$  ( $b_\ell = f(K_i)$ ). If  $b_\ell = K_i$ , the  $i$ th term of  $\hat{\partial y / \partial b}_\ell$  equals  $(A_i / D_i)(H_i - \text{RBOT}_i)$ , where  $\text{RBOT}_i$  is the elevation of the bottom of the streambed.

Second, if the head-dependent boundary is simulated using the Drain Package, and the simulated hydraulic head,  $h_i$ , is below the elevation of the drain, the  $i^{\text{th}}$  term of  $\hat{\partial y / \partial b}_\ell$  equals 0.0 for all  $b_\ell$ .

Third, if the head-dependent boundary is simulated by using the Streamflow-Routing Package, and the loss in streamflow exceeds the flow entering reach  $i$ , the  $i$ th term of  $\hat{\partial y / \partial b}_\ell$  equals 0.0 for all  $b_\ell$ .

In the extreme, these conditions can eliminate the effect of the head-dependent boundary gain-or-loss observation on parameter estimation. For example, if the simulated hydraulic heads at all cells or reaches used to simulate a head-dependent boundary are below the bottom of the streambed, or drain, the observation has no effect on estimated parameter values unless  $b_\ell = f(K_i)$ , in which case only the estimation of parameter  $b_\ell$  would be affected.

The  $\partial \underline{h} / \partial b_\ell$  are calculated from the numerical solution of the sensitivity equation. If the temporal discretization of the ground-water flow equation is fully implicit, as in MODFLOW and MODFLOWP, the matrix form of the sensitivity equations for the  $\ell^{\text{th}}$  parameter of a problem in which all aquifers are confined is:

$$\underline{A}(0) \frac{\partial \underline{h}(0)}{\partial b_\ell} = - \frac{\partial \underline{A}(0)}{\partial b_\ell} \underline{h}(0) - \frac{\partial \underline{f}(0)}{\partial b_\ell} \quad n = 0, \quad (69a)$$

and

$$\begin{aligned} \underline{A}(n) \frac{\partial \underline{h}(n)}{\partial b_\ell} = & - \frac{\partial \underline{B}(n)}{\partial b_\ell} \underline{h}(n-1) + \underline{B}(n) \frac{\partial \underline{h}(n-1)}{\partial b_\ell} \\ & - \frac{\partial \underline{A}(n)}{\partial b_\ell} \underline{h}(n) - \frac{\partial \underline{f}(n)}{\partial b_\ell} \quad n \geq 1, \end{aligned} \quad (69b)$$

where  $\underline{A}(0)$  equals  $\underline{K} + \underline{P}(0)$  [ $L^2/T$ ];

$b_\ell$  is the  $\ell^{\text{th}}$  parameter;

$\underline{f}(0)$  is the forcing function of the steady-state problem ( $n=0$ ); and

$\underline{f}(n)$  is the forcing function at the  $n^{\text{th}}$  time step.

All terms except  $b_\ell$  were defined after equation (3). Note that  $\underline{A}(0)$ ,  $\underline{h}(0)$ , and  $\underline{f}(0)$  are just  $\underline{A}(n)$ ,  $\underline{h}(n)$ , and  $\underline{f}(n)$  evaluated for  $n=0$  (steady state).

The boundary conditions are:

$$\left. \frac{\partial \underline{h}}{\partial b_\ell} \right|_{\Gamma_1} = 0, \quad (70)$$

$$\underline{h} \Big|_{\Gamma_2} = 0,$$

where  $\Gamma_1$  are the constant-head boundaries of the physical system, except when  $b_\ell$  is used to define the hydraulic head along a constant-head boundary. In that situation,  $\partial h / \partial b_\ell$  along the boundary is calculated from the relation between the constant heads and  $b_\ell$ .  $\Gamma_2$  are the head-dependent boundaries and  $H$  is the constant head on one side of the boundary.

By using equation (69) and (70),  $\partial h / \partial b_\ell$  for each time step can be calculated for all parameters before progressing to the next time step. By using this method,  $\underline{A}$  is formulated only once for each time step, but solutions of hydraulic heads and sensitivities for all parameters needs to be saved for use in the next time step. Alternatively, sensitivities for all time steps can be calculated for each parameter before progressing to the next parameter. By using this method,  $\underline{A}$  is formulated more times, but the quantity of computer temporary storage required is smaller if the number of parameters is less than the number of time steps. Both methods are available in the Parameter-Estimation Package by appropriate specification of ISN of LINE 6 of the INPUT FILE (Appendix A).

If any of the layers are unconfined,  $\underline{K}$ , and, therefore, the  $\underline{A}$  are functions of  $\underline{h}$  and  $\underline{h}(\underline{h})$ , and the first term on the right-hand side of equation (69a) and the third term on the right-hand side of equation (69b) need to be expanded. By using iterative updating as suggested by Shah and others (1978), to avoid solving a problem with an unsymmetric matrix, the equations for problems with unconfined aquifers are:

$$\underline{A}(0) \left( \frac{\partial \underline{h}(0)}{\partial b_\ell} \right)^r = - \frac{\partial \underline{A}(0)}{\partial \underline{h}(0)} \left( \frac{\partial \underline{h}(0)}{\partial b_\ell} \right)^{r-1} \underline{h}(0) - \frac{\partial \underline{A}(0)}{\partial b_\ell} \underline{h}(0) - \frac{\partial \underline{f}(0)}{\partial b_\ell}, \quad n = 0, \quad (71a)$$

and

$$\begin{aligned} \underline{A}(n) \left( \frac{\partial \underline{h}(n)}{\partial b_\ell} \right)^r = & - \frac{\partial \underline{A}(n)}{\partial \underline{h}(n)} \left( \frac{\partial \underline{h}(n)}{\partial b_\ell} \right)^{r-1} \underline{h}(n) + \frac{\partial \underline{B}(n)}{\partial b_\ell} \underline{h}(n-1) + \\ & \underline{B}(n) \frac{\partial \underline{h}(n-1)}{\partial b_\ell} - \frac{\partial \underline{A}(n)}{\partial b_\ell} \underline{h}(n) - \frac{\partial \underline{f}(n)}{\partial b_\ell}, \quad n \geq 1, \quad (71b) \end{aligned}$$

where the equations need to be solved with an iterative solver such as PCG2 (Hill, 1990b), and  $r$  is the solver iteration. All other variables were defined after equations (3) or (69). By using index notation to clarify the multiplications involved, the first term on the right-hand side of equations (71a) and (71b) equal:

$$\frac{\partial \underline{A}(0)}{\partial \underline{h}(0)} \left( \frac{\partial \underline{h}(0)}{\partial b_\ell} \right)^{r-1} \underline{h}(0) = \frac{\partial A_{ij}(0)}{\partial h_m(0)} \left( \frac{\partial h_m(0)}{\partial b_\ell} \right)^{r-1} h_j(0) \quad (72a)$$

and

$$\frac{\partial \underline{A}(n)}{\partial \underline{h}(n)} \left( \frac{\partial \underline{h}(n)}{\partial b_\ell} \right)^{r-1} \underline{h}(n) = \frac{\partial A_{ij}(n)}{\partial h_m(n)} \left( \frac{\partial h_m(n)}{\partial b_\ell} \right)^{r-1} h_j(n), \quad (72b)$$

which are vectors.

Sensitivity-equation sensitivities for different parameters might vary from hydraulic-head values and from each other by several orders of magnitude. When using an iterative solver, the convergence criteria specified for hydraulic head needs to be adapted for each parameter. In this report, the convergence criteria for the sensitivity-equation sensitivities for a parameter  $b_\ell$  are calculated as  $\text{CONV}/(|b_\ell^0| \times 100)$ , where CONV is a convergence criterion for hydraulic head, and  $b_\ell^0$  is the initial estimate of the parameter. For example, when using PCG2 (Hill, 1990b), the convergence criteria for  $b_\ell$  are calculated as  $\text{HCLOSE}/(|b_\ell^0| \times 100)$  and  $\text{RCLOSE}/(|b_\ell^0| \times 100)$ .

#### Adjoint-State Method of Calculating the Gradient of the Objective Function

In adjoint-state theory, adjoint states are calculated first, and then are used to calculate the gradient. Adjoint states are obtained by solving differential equations that are developed from, and are very similar to, the ground-water flow equations. If the temporal discretization of the ground-water flow equation is fully implicit, as in MODFLOW and MODFLOWP, the matrix form of the adjoint-state equations are (after Townley and Wilson, 1985):

$$\underline{A}(n) \phi(n-1) = \underline{B}(n+1) \phi(n) + \frac{\partial S(\underline{b})}{\partial \underline{h}(n)} \quad n > 0 \quad (73a)$$

$$\underline{A}(0) \phi(-1) = \underline{B}(1) \phi(0) + \frac{\partial S(\underline{b})}{\partial \underline{h}(0)} \quad n = 0, \quad (73b)$$

where  $S(\underline{b})$  is the objective function;

$\frac{\partial S(\underline{b})}{\partial \underline{h}(n)}$  is a vector of zeros unless components of  $S(\underline{b})$  are at time step  $n$ ; and

$\phi(n)$  is the adjoint state at the end of the  $n^{\text{th}}$  time step  $[T/L^2]$ .

All other terms were defined after equation (3). The boundary conditions are:

$$\begin{aligned} \phi \Big|_{\Gamma_1} &= 0 \\ \left( \frac{\partial \phi}{\partial x} n_x + \frac{\partial \phi}{\partial y} n_y + \frac{\partial \phi}{\partial z} n_z \right) \Big|_{\Gamma_2} &= 0, \end{aligned} \quad (74)$$

where  $\Gamma_1$  are the constant-head boundaries of the physical system;  
 $\Gamma_2$  are the defined-flux boundaries of the physical system; and  
 $n_x, n_y, n_z$  are the components of an inward-looking unit vector along  $\Gamma_2$ .

The initial condition is  $\phi(N)=0$ , where  $N$  is the latest time step at which a component of  $S(\underline{b})$  occurs. Equations (73) and (74) are solved by starting at  $n=N$ , and working backwards to  $\phi(-1)$ . In a sense, the system is solved backwards in time, except that different time-step lengths are used on the two sides of the equation.

The derivative with respect to the  $\ell^{\text{th}}$  parameter is calculated by (Townley and Wilson, 1985):

$$\begin{aligned} \frac{\partial S(\underline{b})}{\partial b_\ell} &= \frac{\partial S_f(\underline{b})}{\partial b_\ell} + \frac{\partial S_p(\underline{b})}{\partial b_\ell} + \phi(-1) \left\{ - \frac{\partial \underline{A}(0)}{\partial b_\ell} \underline{h}(0) - \frac{\partial \underline{f}(0)}{\partial b_\ell} \right\} \\ &+ \sum_{n=1}^N \phi(n-1) \left\{ - \frac{\partial \underline{A}(n)}{\partial b_\ell} \underline{h}(n) + \frac{\partial \underline{B}(n)}{\partial b_\ell} \underline{h}(n-1) - \frac{\partial \underline{f}(n)}{\partial b_\ell} \right\}, \end{aligned} \quad (75)$$

where  $S(\underline{b}) = S_h(\underline{b}) + S_f(\underline{b}) + S_p(\underline{b})$ ;

$S_h(\underline{b})$  are terms of the objective function related to observed hydraulic heads or changes in hydraulic head;

$S_f(\underline{b})$  are terms of the objective function related to head-dependent boundary gain and loss observations; and

$S_p(\underline{b})$  are terms of the objective function related to prior estimates of the parameters.

All other terms were defined after equations (3) or (69). A clear derivation of equations (73), (74) and (75) is presented by Townley and Wilson (1985, p. 1854-1855), and is not repeated in this report.

A simplistic understanding of the adjoint states can be developed by considering equations (73) and (74) when  $h_u(\underline{b})$  is substituted for  $S(\underline{b})$ , where  $h_u(\underline{b})$  is a single hydraulic head, and  $u$  indicates its time and location. In this circumstance,  $\partial h_u(\underline{b})/\partial b_\ell$ ,  $\ell=1, NP$ , would be calculated. In a steady-state system, the adjoint states are the solution of:

$$\underline{A}(\underline{Q}) \underline{\phi} = \frac{\partial h_u(\underline{b})}{\partial \underline{h}}. \quad (76)$$

The right-hand side is equal to a vector of zeros except for a 1.0 in the location of  $u$ . The adjoint states  $\underline{\phi}$  then could be interpreted as the change in hydraulic head at each grid node caused by a unit recharge at location  $u$ . An equally valid interpretation is that each value in  $\underline{\phi}$  is the change in  $h_u(\underline{b})$  that would occur because of a unit recharge at the grid node associated with the value of  $\underline{\phi}$ . The latter interpretation was presented by Wilson and Metcalfe (1985), and is consistent with the view that the adjoint states relate changes in ground-water flow to the sensitivities.

For a simplistic understanding of the transient adjoint states, consider first  $\underline{\phi}(N-1)$ , where  $N$  is the time step at which  $h_u(\underline{b})$  occurs. Because  $\underline{\phi}(N)=0$ ,  $\underline{\phi}(N-1)$  is the solution of:

$$\underline{A}(N-1) \underline{\phi}(N-1) = \frac{\partial h_u(\underline{b})}{\partial \underline{h}(N)}. \quad (77)$$



The right-hand side of (77) is a vector of zeros, except for a 1 in the location identified by  $u$ . If all time steps are the same length and the direction of the time sequence is disregarded, it is simple to imagine that  $\phi(N-2)$ ,  $\phi(N-3)$ , ...  $\phi(0)$  represent the dissipation of this unit recharge over time. This representation is not correct when the time steps are of different lengths.

In equation (75),  $\phi(-1)$  is used to relate the initial conditions of the problem to the calculated derivative. In solving for  $\phi(-1)$  (eq. 73), the storage term is deleted from the left-hand side of the equation. Thus,  $\phi(-1)$  is larger than  $\phi(n)$ ,  $n > -1$ , which indicates the enduring importance of the initial conditions. As  $N$  increases,  $\lambda(-1)$  becomes smaller, and the initial conditions become less important.

When  $h_u(\underline{b})$  is substituted for  $S(\underline{b})$ , the sum of the adjoint states for transient problems equals the steady-state adjoint state ( $\phi_{ss}$ ). That is, for any  $N$ :

$$\sum_{i=-1}^N \phi(i) = \phi_{ss}. \quad (78)$$

This equality means that the same total weighting is used to relate changes in ground-water flow to the sensitivities (see discussion after eq. 76), but that the weighting is spread out over the time steps involved. This property does not apply when calculating the gradient.

To calculate the gradient for problems with water-table layers, which are nonlinear,  $\underline{A}(n)$  and  $\underline{A}(0)$  of equation (73) would be replaced by  $\frac{\partial \underline{A}(n)}{\partial \underline{h}(n)} \underline{h}(n) + \underline{A}(n)$  and  $\frac{\partial \underline{A}(0)}{\partial \underline{h}(0)} \underline{h}(0) + \underline{A}(0)$ , respectively. Although iterative updating, as discussed above, perhaps could be used to solve the resulting equations; this was not done in the Parameter-Estimation Package. Thus, for problems with water-table layers, parameter estimation needs to be accomplished by using modified Gauss-Newton optimization.

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## APPENDIX A: MODFLOWP INPUT AND OUTPUT

### Input Instructions

These input instructions are intended to be used in conjunction with the documentation for the modular, three-dimensional, ground-water flow model (MODFLOW) presented by McDonald and Harbaugh (1988) and the Streamflow-Routing Package presented by Prudic (1989). As needed, their variable names are used here with their lower- and upper-case lettering conventions. If the Parameter-Estimation Package is not activated, MODFLOWP operates identically to MODFLOW, with a minor exception discussed in the section "Hydraulic Heads," Appendix C.

In the following discussion, the input file for the Parameter-Estimation Package will be referred to as the INPUT FILE. IUNIT(15), which is read from the Basic Package input file, is used to store the input unit number for the INPUT FILE. If desired, another element of IUNIT can be used by changing all references to IUNIT(15); see text in the first section of Appendix B.

The Parameter-Estimation Package can be used to: (1) calculate hydraulic heads and flows like MODFLOW, but using the parameter values specified in the INPUT FILE; (2) calculate hydraulic heads, and sensitivity-equation sensitivities of simulated hydraulic heads by using equations (69), (70), and (71), or the adjoint states and the gradient of the objective function by using equations (73), (74), and (75); or (3) perform parameter estimation by nonlinear regression. Nonlinear regression can be accomplished by modified Gauss-Newton optimization by using sensitivity-equation sensitivities, or by conjugate-direction optimization by using the gradient of the objective function calculated by using adjoint states. When parameter estimation converges, final calculated hydraulic heads and flows can be printed and saved as they are for MODFLOW by specifying KPRINT=1 in DATA SET 13 of the INPUT FILE.

### Calculating Hydraulic Heads and Flows

Hydraulic heads and flows first need to be calculated without the Parameter-Estimation Package [IUNIT(15)=0]. Without the Parameter-Estimation Package, MODFLOWP performs almost exactly like MODFLOW and requires the same input files. Constructing the MODFLOW input files and simulating hydraulic heads and flows, and then constructing an INPUT FILE that is supposed to produce the same hydraulic heads and flows produces an effective check on the parts of the INPUT FILE used to calculate model inputs from the parameter values.

Calculating hydraulic heads and flows by using the Parameter-Estimation Package [IUNIT(15)≠0] involves modifying the MODFLOW input files as described in the following section, constructing the INPUT FILE as described below, and setting IPAR of LINE 6 of the INPUT FILE equal to -1. Calculating hydraulic heads and flows by using the Parameter-Estimation Package differs from calculating hydraulic heads and flows with MODFLOW in three ways. First, problems with both steady-state and transient conditions are simulated with one model run and one set of input files. This change was required for parameter estimation and alleviates problems related to keeping the data sets for the two types of problems consistent. Second, the parameter values defined in DATA SET 8 of the INPUT FILE are used in the simulation. This feature makes the parameter values easy for the user to change, and this feature can be used to help determine the initial parameter values of the parameter-estimation procedure or to facilitate trial-and-error calibration for models that are not calibrated by nonlinear regression. Calibration by nonlinear regression might not be possible, for example, if most of the available computer storage or execution capacity is used just to calculate hydraulic heads. Third, the simulation continues only for as many time steps as are needed to include all the time steps at which there are observations (see DATA SETS 6, 6C, and 7A).

The hydraulic heads and flows calculated with IUNIT(15)=0 and with IUNIT(15)≠0 need to be nearly identical. Discrepancies generally indicate errors in DATA SETS 2, 2A, 2B, 3, and 4 of the INPUT FILE, which are used to define the parameterization and are described below.

#### Calculating Sensitivity-Equation Sensitivities and the Gradient of the Objective Function and Performing Parameter Estimation

Use of the Parameter-Estimation Package involves modifying the input files from other packages and constructing the INPUT FILE as described below.

#### Changes to input files from other packages

When used with the Parameter-Estimation Package, the input files for some of the packages described by McDonald and Harbaugh (1988) and the package described by Prudic (1989) need to be changed slightly. For steady-state



problems, these changes are made to the files used to calculate steady-state hydraulic heads with IUNIT(15)=0; for problems that include steady-state and transient or just transient conditions, these changes are made to the files used to calculate transient hydraulic heads with IUNIT(15)=0. Examples are included for the test cases at the end of Appendix A. The needed changes are as follows:

1. The Basic Package input file needs to be changed in the following ways:

- a. NPER needs to be equal to or greater than the time step of the latest observation (see DATA SETS 6, 6C, and 7A in the INPUT FILE). (In MODFLOWP, time steps are numbered from the beginning of the simulation, so remember to include all the time steps from preceding stress periods when calculating the time step of the latest observation). If TOFF (DATA SETS 6, 6C, and 7A) of the latest observation is greater than zero, NPER needs to be equal to or greater than the latest time step plus 1. NPER=0 can be used for steady-state problems.

- b. IUNIT(15) needs to equal the FORTRAN unit number from which the INPUT FILE is read.

- c. Starting hydraulic heads (Shead) from the steady-state Basic Package input file need to be used in the Basic Package input file.

2. For transient simulations, input files for the River, Recharge, Well, Drain, Evapotranspiration, General-Head Boundary, and Streamflow-Routing Packages need to include the data "FOR EACH STRESS PERIOD" (McDonald and Harbaugh, 1988; Prudic, 1989) from the steady-state simulation, followed by the data "FOR EACH STRESS PERIOD" from the transient simulation. The Output Control input file needs to include the data "FOR EACH TIME STEP" from the steady-state simulation, followed by the data "FOR EACH TIME STEP" from the transient simulation. For steady-state simulations, these input files need not be changed.

3. For transient simulations, if the IBOUND array of the Basic Package input file is different for steady-state and transient conditions, a new input file is needed. This input file contains the steady-state IBOUND array followed by the transient IBOUND array and is read from FORTRAN unit IUBD (LINE 7 of the INPUT FILE). These IBOUND arrays replace the IBOUND array read

from the Basic Package input file. Note that any cells that are inactive in the steady state IBOUND array must be inactive in the transient array. If any layers are unconfined, only the steady-state IBOUND array is read from IUBD.

4. If the top simulated layer is a water-table layer (Block-Centered Flow Package: LAYCON=1), and any cells go dry for any of the sets of parameter values that occur in the parameter-estimation iterations, the IBOUND array needs to be read from a new input file, as described in item 3 above. For a steady-state simulation, this input file contains the IBOUND array for steady-state conditions. For transient problems, this input file needs to contain two IBOUND arrays; repeat the steady-state IBOUND array if it is used for steady-state and transient conditions.

5. Many packages of MODFLOW permit arrays to be read from separate files using subroutines U2DREL and U2DINT (McDonald and Harbaugh, 1988, ch. 14). The Parameter-Estimation Package also permits arrays to be read from separate files using U2DREL and U2DINT, and care needs to be taken that one file is not read by two packages, which results in an end-of-file error. A common example occurs when defining a transmissivity parameter and U2DREL is called to read cell values of aquifer thickness from a separate file. The user might try to read the same separate file from the Parameter-Estimation Package that has already been read from the Block-Centered Flow Package. The problem can be resolved by creating a new copy of the file, or by realizing that the parameter values specified by the INPUT FILE (DATA SET 8) are used to replace the values read from the Block-Centered Flow Package. Thus, the Block-Centered Flow Package input file can be changed to assign an arbitrary constant value of transmissivity [positive, nonzero values are needed so that submodule SBCFIN (McDonald and Harbaugh, 1988, p. 5-68) will not change IBOUND values to zero], and the separate file is read only from the Parameter-Estimation Package.

6. Output Control input-file variables IHEDFM, IHEDUN, IHDDFL, Hdpr, and Hdsv are used to control the printing and saving of hydraulic heads, adjoint states, and sensitivity-equation sensitivities for all cells when using the Parameter-Estimation Package. Read the instructions for IPAR of LINE 6 of the INPUT FILE and change the listed variables as needed to produce the desired output.

7. Superposition simulations, in which changes in hydraulic head are calculated, can conform to the input-file specifications described above by including steady-state conditions in which all hydraulic heads equal zero.

8. To estimate parameters for NSIM simulations of one flow system (for example, if there are NSIM aquifer tests), begin by estimating the parameters for each individual simulation using the directions in this appendix. To combine the simulations, the Basic Package input file from the first simulation needs to be modified in the following ways:

a. NPER needs to equal the sum of the NPER values from each of the simulations, plus NSIM-1. The NSIM-1 time steps account for the steady-state conditions for all but the first simulation.

b. Add the data lines from the other NSIM-1 Basic Package input files that specify PERLEN, NSTP, and TSMULT. Preceding the lines for all but the first simulation, add a line with PERLEN=1.E23, NSTP=1, TSMULT=1.0. The added lines specify the large time step needed to simulate steady-state conditions.

The following changes involve the INPUT FILE, which is discussed in the following sections. These changes are listed here to keep all changes together, but the following sections need to be read first.

c. Simulations with different known hydraulic heads at constant hydraulic-head boundaries can be represented using the methods discussed in the section "IUNHEA."

d. If the NSIM simulations are superposition simulations, the hydraulic heads and sensitivities at the beginning of all but the first simulation can be set to zero using NZER of LINE 8 and IZER of DATA SET 1B of the INPUT FILE. The time-step numbers of NZER equal the time step associated with what was steady state when the simulations were considered separately. Thus, the time step of the steady state preceding the second simulation equals NPER of the first simulation plus 1; the time step of the steady state preceding the third simulation equals NPER of the first simulation, plus 1, plus NPER of the second simulation, plus 1. This process is continued until all simulations are included.

e. The time steps of the observations in the INPUT FILE (see discussion of DATA SETS 6, 6C, and 7A of the section "Data entry format and instructions for the INPUT FILE") for all but the first simulation need to be changed. For the second simulation, add NPER of the first simulation to all time-step numbers. For the third simulation, add NPER of the first simulation plus 1+NPER of the second simulation; the 1 accounts for the steady-state conditions of the second simulation. For the fourth simulation, add NPER of the first simulation, plus 1+NPER of the second simulation, plus 1+NPER of the third simulation. Continue until all simulations are included. Once these changes are made, all observations need to be included in one INPUT FILE, and NH, MOBS, MAXM, NQ, NQC, and NQT of DATA LINE 5 need to be changed to accommodate the total number of observations.

#### Discussion of the INPUT FILE

The INPUT FILE is described below. Some of the more complicated variables are discussed first, and the data entry and format instructions follow.

#### ISN

ISN (LINE 6) is used to select between the different optimization and numerical methods available in the Parameter-Estimation Package, and computer-storage allocation depends on ISN. Usually ISN=-1; the other values discussed in this section need to be considered only under special circumstances.

If ISN<0, sensitivity-equation sensitivities are calculated (see section "Sensitivity-Equation Method of Calculating Sensitivities), and modified Gauss-Newton optimization is performed. Two options are available for calculating the sensitivity-equation sensitivities:

1. If ISN=-1, all sensitivities are calculated at each time step before progressing to the next time step. This method permits matrix  $\underline{A}$  on the left-hand side of equation (69) or (71) to be calculated only once for each time step, so if a direct solver, such as the D4 solver (S.A. Leake, U.S. Geological Survey, written commun., 1989), is used,  $\underline{A}$  only needs to be decomposed once for each time step. Because decomposition of direct solvers might use more than 75 percent of the computer time required by a direct solver, using one decomposition can be advantageous. When ISN=-1, NP files

numbered starting with IUHEAD are used to store nodal arrays of sensitivities (NP and IUHEAD are read from LINES 3 and 7 of the INPUT FILE, respectively). If the number of parameters is less than the number of time steps, the number of files will be smaller with ISN=-1 than with ISN=-2.

2. If ISN=-2, sensitivities for each parameter are calculated for all time steps before progressing to the next parameter. Unless the problem is steady state or  $\underline{A}$  is the same for all time steps (constant time-step length),  $\underline{A}$  needs to be decomposed at each time step when using a direct solver, and direct solvers generally are not as efficient with ISN=-2 as with ISN=-1. Thus, a conjugate-gradient solver probably needs to be used for most problems with ISN=-2. When ISN=-2, files numbered starting with IUHEAD of LINE 3 are used to store nodal arrays of hydraulic head for each time step. If the number of time steps is less than the number of parameters, the number of files will be smaller with ISN=-2 than with ISN=-1.

If ISN>0, the gradient of the objective function is calculated by the adjoint-state method, and parameter estimates are calculated by a conjugate-direction method. NFIT of DATA SET 13 of the INPUT FILE is used to designate the number of Fletcher-Reeves iterations that precede quasi-Newton iterations, and NFIT needs to be coordinated with ISN. Options for ISN are as follows:

1. If ISN=1, enough computer storage is allocated to permit quasi-Newton iterations, which need slightly more computer storage than Fletcher-Reeves iterations. Fletcher-Reeves iterations can be performed with ISN=1, so that NFIT can be greater than zero.

2. If ISN=2, enough computer storage is allocated to permit Fletcher-Reeves iterations. The allocated computer storage is insufficient for quasi-Newton iterations, so NFIT needs to be greater than or equal to ITMXP of DATA SET 13 to ensure that no quasi-Newton iterations are executed.

3. If ISN=4, enough computer storage is allocated to permit quasi-Newton and, therefore, Fletcher-Reeves iterations, and to calculate statistics that need the sensitivity matrix,  $\underline{X}_r$ . The statistics are calculated if parameter estimation converges and LASTX of DATA SET 13 of the INPUT FILE is larger than zero.

## IPAR

IPAR (LINE 6) is used to identify whether to (1) just calculate hydraulic heads and flows, (2) calculate hydraulic heads and flows and sensitivity-equation sensitivities ( $ISN < 0$ ) or adjoint states and the gradient of the objective function ( $ISN > 0$ ), or (3) perform parameter estimation.

If  $IPAR < 0$ , hydraulic heads are calculated. Hydraulic-head arrays at each time step are printed or saved or both as specified by the Output Control Package input file; calculated and observed hydraulic heads or changes in hydraulic heads at the NH times and locations (see DATA SETS 6 and 6C) and flows at the NQT times and head-dependent boundaries (see DATA SET 7A) are printed.

If  $IPAR = 0$ , hydraulic heads and sensitivity-equation sensitivities ( $ISN < 0$ ) or adjoint states ( $ISN > 0$ ) are calculated. If  $ISN < 0$ , hydraulic head and sensitivity-equation sensitivity arrays are printed or saved or both for time steps when at least one of the NH hydraulic heads or NQT flows occurs and Hdpr and Hdsv of the Output Control input file are set to allow the output. If  $ISN > 0$ , hydraulic heads and adjoint states are printed or saved or both for all time steps indicated by Hdpr and Hdsv. Adjoint states are calculated backwards in time (eq. 73), but the Output Control Package input file is read forward in time, so the Hdpr and Hdsv values for time step KSTP are used to print the adjoint states  $\phi(N-KSTP)$ , where N is the latest time step at which a component of  $S(b)$  occurs. (See the sections "Adjoint-State Method of Calculating the Gradient of the Objective Function" and "Calculated Values and Volumetric Budgets for the Entire Model" for more information.) In addition, the following values are printed: calculated and observed hydraulic heads at the NH times and locations and flows at the NQT times and boundaries; for  $ISN < 0$ , NH+NQT sensitivities; for  $ISN > 0$ , the gradient of the objective function.

If  $IPAR = 1$ , parameter estimation by nonlinear regression is performed. The following values are printed: calculated and observed hydraulic heads or changes in hydraulic head at the NH times and locations; NQT calculated and observed gains and losses at head-dependent boundaries; NH+NQT sensitivities ( $ISN < 0$ ) or the gradient of the objective function ( $ISN > 0$ ); and data from the

regression procedure. IPRINT of DATA SET 13 of the INPUT FILE controls whether or not all of these items are printed at every iteration of the parameter-estimation procedure. If parameter estimation converges, the printing or saving or both of final hydraulic heads is controlled by KPRINT of DATA SET 13 and Hdpr and Hdsv of the Output Control Package input file.

#### IUNHEA

IUNHEA (LINE 7) is used to indicate that there are temporal changes in known hydraulic heads at constant hydraulic-head boundaries. Known hydraulic heads at constant hydraulic-head boundaries are specified by the user and are not affected by the parameters defined by using the CH identifier (see DATA SETS 2 and 2A of the INPUT FILE). Known hydraulic heads can be changed at time steps specified by the user by defining IUNHEA $\neq$ 0. Module SEN1RH (see Appendix C) is called from MAIN when IUNHEA $\neq$ 0, and the present version functions as described below. Although this version is general, it requires an input file that might be extremely large for some problems. Users are encouraged to modify SEN1RH to coordinate with their problems and to decrease the size of or eliminate the input file.

The present version of SEN1RH reads from unit number IUNHEA. The first data card of the input file is a list of as many as 16 time steps at which the known hydraulic heads at constant hydraulic-head boundaries change. The format is 16F5.0 (note that integers can be read using this format; they need to be right-justified). For every nonzero time-step number (all nonzero numbers need to be to the left of blanks or zeros), the input file contains an array of hydraulic heads for each of the NLAY model layers. These arrays are read using U2DREN (Appendix C), a utility module that operates like U2DREL (McDonald and Harbaugh, 1988, p. 14-26) but prints nothing; use the instructions for U2DREL to construct this part of the input file. At each of the time steps listed on the first data card, the hydraulic heads at all constant hydraulic-head boundaries are replaced using values from the associated arrays of hydraulic heads. The first set of NLAY arrays read is associated with the first time step listed, the second set of NLAY arrays read is associated with the second time step, and so forth.

Parameter Definition: DATA SETS 2, 2A, 2B, 3, and 4

DATA SETS 2, 2A, 2B, 3, and 4 define how parameters (with values initially specified in DATA SET 8 and subsequently calculated by nonlinear regression) are used to calculate the model inputs described in the MODFLOW input instructions (McDonald and Harbaugh, 1988; Prudic, 1989), and listed in table 1. A DATA SET 2 is repeated for each parameter except for parameters used to define constant hydraulic-head boundaries, in which instance many parameters can be defined under one DATA SET 2. The model input(s) involved are identified by PID, the first variable of DATA SET 2. PID is a character variable; available options and their associated model inputs are listed in table A1. Use of array NLL, which is part of DATA SET 2, and DATA SETS 2A and 2B is mentioned in table A1, and is discussed in detail in the following paragraphs.

For PID=ANI and ANIV, array NLL is used to specify layer numbers. The parameter needs to equal the quantity specified as the model input in table A1, and only DATA SET 2 is needed.

DATA SET 2 is followed by DATA SET 2A if the MODFLOW input instructions specify that the model input indicated by PID be defined by a list of cells. This occurs for pumpage (called the volumetric recharge rate by McDonald and Harbaugh, 1988) of the Well Package (PID=Q), and the conductances of the River, Drain, Streamflow-Routing, and General-Head Boundary Packages (PID=KRB, KDR, KST, and GHb). DATA SET 2A is a list of cells (specified by layer, row, and column or, for the Streamflow-Routing Package, by reach and segment) where the parameter applies, and can include cell-by-cell multiplicative factors that allow the user to define the parameter to be the most physically significant quantity. For example, noting that the conductance for a cell equals  $(K_i/D_i)A_i$  (eq. 4), the parameter can be defined as  $K_i$  if  $K_i$  can be considered to be constant for all listed cells. Then the multiplicative factors would equal  $(A_i/D_i)$ , which might be different for each cell. As a default, all multiplicative factors can be set to 1.0 using NLL(1) of DATA SET 2, which implies that the parameter equals the required model input for all listed cells.



Table A1:--Available options for the parameter identifier (PID), the INPUT FILE data sets used to calculate the contribution of this parameter to the MODFLOW model input (McDonald and Harbaugh, 1988; Prudic, 1989), and the MODFLOW model input

PID	Multipliers and spatial extent defined by	Time defined by	MODFLOW Model input
Q	NLL(1); DATA SET 2A	NLL(I)	Volumetric recharge rate of the Well Package.
KRB <sup>1</sup>	NLL(1); DATA SET 2A	NLL(I)	Conductance of the River Package.
KDR <sup>1</sup>	NLL(1); DATA SET 2A	NLL(I)	Conductance of the Drain Package.
KST <sup>1</sup>	NLL(1); DATA SET 2A	NLL(I)	Conductance of the Streamflow-Routing Package.
GHB <sup>1</sup>	NLL(1); DATA SET 2A	NLL(I)	Conductance of the General-Head Boundary Package.
CH	NLL(I); DATA SET 2A	NLL(2)	Constant hydraulic head linearly interpolated between specified nodes.
T <sup>1</sup>	NLL(I); DATA SET 2B		Horizontal hydraulic conductivity or transmissivity of the Block-Centered Flow Package <sup>2</sup> .
ANI <sup>1</sup>	NLL(I)		Horizontal anisotropy of the Block-Centered Flow Package.
KV <sup>1</sup>	NLL(I); DATA SET 2B		Leakance of the Block-Centered Flow Package.
TKV <sup>1</sup>	NLL(I); DATA SET 2B		Model inputs described for PID=T and KV.
ANIV <sup>1</sup>	NLL(I)		Vertical anisotropy used to calculate leakance of the Block-Centered Flow Package.
S1 <sup>1</sup>	NLL(I); DATA SET 2B		Storage coefficient or specific yield of the Block-Centered Flow Package <sup>3</sup> .
RCH	NLL(1); DATA SET 2B	NLL(I)	Recharge rate of the Recharge Package.
ETM	NLL(1); DATA SET 2B	NLL(I)	Maximum ET rate of the Evapotranspiration Package.

<sup>1</sup>The natural log of the indicated quantity can be defined as the parameter to be estimated using LN in DATA SET 2 of the INPUT FILE.

<sup>2</sup>If LAYCON of the Block-Centered Flow Package=0, the T model input is transmissivity. If LAYCON=1, the T model input is hydraulic conductivity.

<sup>3</sup>If LAYCON of the Block-Centered Flow Package=0, the S1 model input is the storage coefficient. If LAYCON=1, the S1 model input is specific yield.

DATA SET 2A is also required for parameters used to define constant hydraulic-head boundaries (PID=CH). In this circumstance, only row and column numbers are read from DATA SET 2A, and the multiplicative constants are replaced with numbers that indicate cells at which constant hydraulic head is to be linearly interpolated from specified end points, the end points, and the constant hydraulic-head parameters defined at the end points. The linear interpolation is only allowed along rows or columns, as shown in figure A1. Interpolation along diagonals and around corners is prohibited. The model layers in which the constant hydraulic-head cells occur are listed in part of array NLL, of DATA SET 2. There are restrictions on how constant hydraulic-head boundaries that span multiple model layers can be defined by the Parameter-Estimation Package, as shown in figure A2. The relevant rules

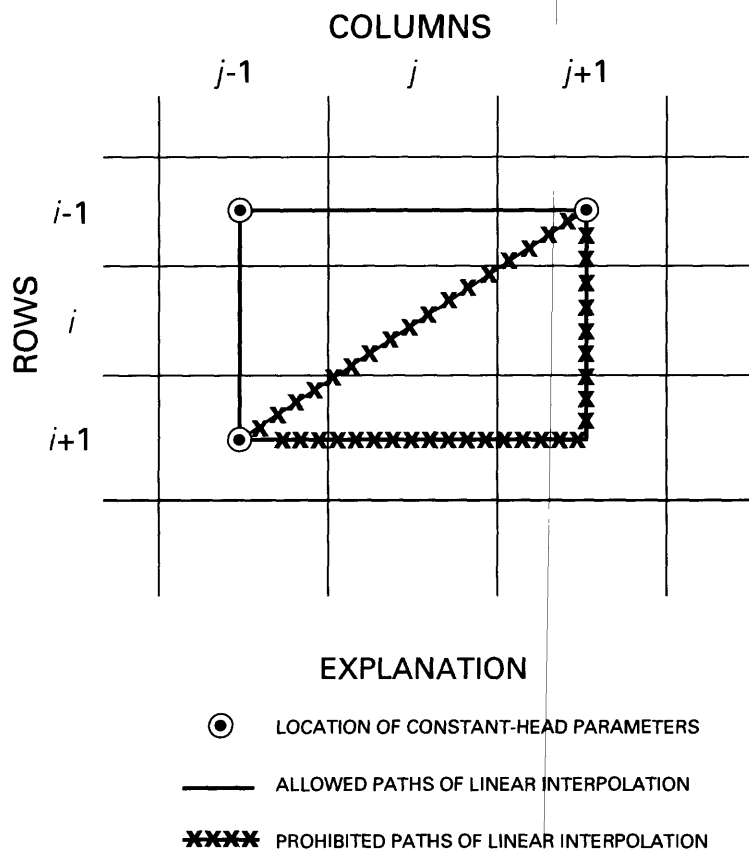
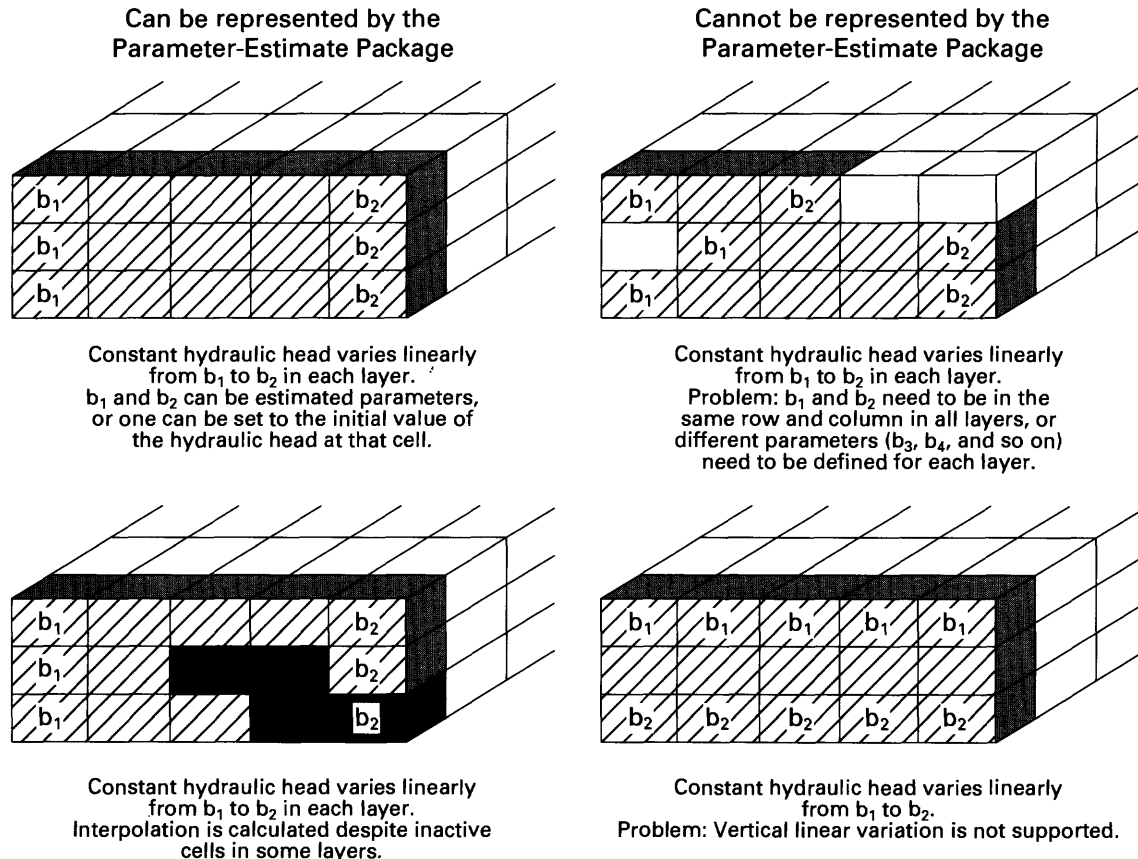


Figure A1.--Allowed and prohibited paths of linear interpolation for constant hydraulic-head parameter definition.

portrayed are: (1) A constant hydraulic-head parameter affects the constant hydraulic-head cells at rows and columns listed in DATA SET 2A; (2) as a consequence of (1), a constant hydraulic-head parameter affects cells in the same rows and columns in all layers involved; (3) affected cells can be specified as constant hydraulic head or inactive, but cannot be active (McDonald and Harbaugh, 1988, p. 4-2); and (4) vertical linear variations are not allowed.



#### EXPLANATION

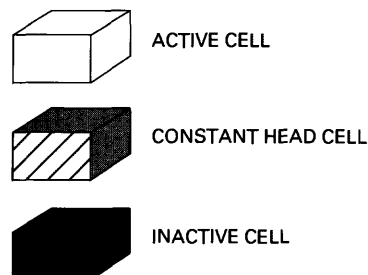


Figure A2.--Circumstances that can and cannot be represented by the Parameter-Estimation Package using PID=CH (DATA SET 2A).

If the MODFLOW input instructions specify that the model input be defined by arrays, as occurs for most aquifer properties (PID=T, KV, TKV, and S1), recharge (PID=RCH), and maximum evapotranspiration (PID=ETM), repetitions of DATA SET 2B can follow the applicable DATA SET 2. The number of repetitions of DATA SET 2B depends on how many model layers are affected by this parameter and whether defaults that can be activated using array NLL of DATA SET 2 are used. A more detailed discussion of how model inputs are calculated from parameters using DATA SET 2B follows the discussion of DATA SETS 3 and 4.

DATA SET 3 is composed of  $NROW \times NCOL$  (number of rows in the finite-difference grid by number of columns) multiplication arrays. Multiplication arrays can be used to calculate model inputs defined by PID = T, KV, TKV, S1, RCH, and ETM. Multiplication array 1 is the first array in DATA SET 3, multiplication array 2 is the second, and so on. Multiplication arrays are referred to in DATA SET 2B. A multiplication array can, for example, equal the cell-by-cell thickness of a confined model layer with homogeneous hydraulic conductivity. If the parameter equals the hydraulic conductivity, the parameter times the multiplication array would equal the transmissivity array, which is the required model input.

DATA SET 4 is composed of  $NROW \times NCOL$  zone arrays. Zone arrays can be used to define the areas in which parameters are used to calculate model inputs defined by PID = T, KV, TKV, S1, RCH, and ETM. Zone array 1 is the first array in DATA SET 4, zone array 2 is the second, and so on. Zone arrays are referred to in DATA SET 2B. A zone array can, for example, be used to indicate that a parameter representing one hydraulic conductivity is to be used to calculate transmissivity in part of a confined model layer, and that a parameter representing another hydraulic conductivity is to be used to calculate transmissivity in the rest of that layer. Note that a multiplication array with elements equal to cell-by-cell layer thickness would be used to calculate transmissivity from the hydraulic conductivities.

The calculation of model inputs from parameters with PID=T, KV, TKV, S1, RCH, and ETM is defined using array NLL of DATA SET 2, variables SFAC, LM, and LZA, and array LZ of DATA SET 2B, multiplication arrays from DATA SET 3, and zone arrays from DATA SET 4. These variables and arrays are described in the

section "Instructions for the INPUT FILE," and their use is illustrated in figures A3A, A3B, and A3C for a model with five rows and five columns. Note that for subsequent parameter-estimation iterations, the parameter value changes but the other values stay the same. If the same cell is included under too many equivalent PID's, computed sensitivities will be wrong. This error is checked for by the program when ICHECK of LINE 4 is greater than zero.

#### EXAMPLE A

- 1) From DATA SET 2: PID=RCH
- 2) From DATA SET 8: Parameter value = 1.0
- 3) From DATA SET 2: NLL(1)=1  
(One value > 0, so one DATA SET  
2B follows this DATA SET 2)
- 4) From DATA SET 2B: SFAC= $1 \times 10^{-8}$
- 5) From DATA SET 2B: LM=0 and LZA=0
- 6) Combining (1) through (5), the recharge rates  
calculated from this parameter are:

$$\begin{bmatrix} 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} \\ 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} \\ 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} \\ 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} \\ 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} & 1 \times 10^{-8} \end{bmatrix}$$

Figure A3.--Three examples of calculating model-input values from parameter values by using PID and NLL(I) from DATA SET 2; SFAC, LM, LZA, and LZ(I) from DATA SET 2B; multiplication and zone arrays from DATA SETS 3 and 4; and parameter values from DATA SET 8 for a model with five rows and five columns. (A zero in the final array indicates that the parameter does not affect the model-input value at that cell.)

# EXAMPLE B

1) From DATA SET 2: PID=T

2) From DATA SET 8: Parameter value = 2.0

3) From DATA SET 2: NLL(1)=4  
(One value > 0, so one DATA SET  
2B follows this DATA SET 2)

4) From DATA SET 2B: SFAC=10.0

5) From DATA SET 2B: Use multiplication array LM=2  
Multiplication array 2 from DATA SET 3:

10.	10.	10.	10.	10.
9.	9.	9.	9.	9.
8.	8.	8.	8.	8.
7.	7.	7.	7.	7.
6.	6.	6.	6.	6.

6) From DATA SET 2B: Use zone array LZA=1, zones LZ(1)=3 and LZ(2)=4  
Zone array 1 from DATA SET 4:

1	2	3	4	5
1	2	3	4	5
1	2	3	4	5
1	2	3	4	5
1	2	3	4	5

7) Combining (1) through (6), the transmissivity values  
calculated from this parameter for layer 4 are:

0.	0.	200.	200.	0.
0.	0.	180.	180.	0.
0.	0.	160.	160.	0.
0.	0.	140.	140.	0.
0.	0.	120.	120.	0.

Figure A3.--Three examples of calculating model-input values from parameter values by using PID and NLL(I) from DATA SET 2; SFAC, LM, LZA, and LZ(I) from DATA SET 2B; multiplication and zone arrays from DATA SETS 3 and 4; and parameter values from DATA SET 8 for a model with five rows and five columns. (A zero in the final array indicates that the parameter does not affect the model-input value at that cell.)--Continued.

# EXAMPLE C

- 1) From DATA SET 2: PID=TKV
- 2) From DATA SET 8: Parameter value = 1.0
- 3) From DATA SET 2: NLL(1)=2, NLL(2)=-2, NLL(3)=-2  
(One value > 0, so one DATA SET  
2B follows this DATA SET 2)
- 4) From DATA SET 2B: SFAC=0.01
- 5) From DATA SET 2B: LM=0
- 6) From DATA SET 2B: Use zone matrix LZA=1, zone LZ(1)=2  
Zone array 1 from DATA SET 4:

$$\begin{bmatrix} 1 & 1 & 1 & 2 & 2 \\ 1 & 1 & 1 & 2 & 2 \\ 1 & 1 & 1 & 2 & 2 \\ 1 & 1 & 1 & 2 & 2 \\ 1 & 1 & 1 & 2 & 2 \end{bmatrix}$$

- 7) Combining (1) through (6), this parameter contributes to the model inputs as follows:

Vertical leakance between  
layers 1 and 2:

$$\begin{bmatrix} 0. & 0. & 0. & .01 & .01 \\ 0. & 0. & 0. & .01 & .01 \\ 0. & 0. & 0. & .01 & .01 \\ 0. & 0. & 0. & .01 & .01 \\ 0. & 0. & 0. & .01 & .01 \end{bmatrix}$$

Layer 2 transmissivity:

$$\begin{bmatrix} 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \end{bmatrix}$$

Vertical leakance between  
layers 2 and 3:

$$\begin{bmatrix} 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \\ 1. & 1. & 1. & 1. & 1. \end{bmatrix}$$

Figure A3.--Three examples of calculating model-input values from parameter values by using PID and NLL(I) from DATA SET 2; SFAC, LM, LZA, and LZ(I) from DATA SET 2B; multiplication and zone arrays from DATA SETS 3 and 4; and parameter values from DATA SET 8 for a model with five rows and five columns. (A zero in the final array indicates that the parameter does not affect the model-input value at that cell.)--Continued.

Parameters with PID=T, TKV, and S1 can be defined over several layers that might not have the same LAYCON value (see footnotes of table A1), but the defined parameter needs to be the same in all the layers. For example, if PID=T, and a confined and unconfined layer are included, the estimated parameter could be hydraulic conductivity. SFAC of DATA SETS 2B and multiplication arrays from DATA SET 3 are used to calculate the model input appropriate for each model layer from the parameter.

If hydrogeologic units pinch out, but the numerical layers continue into the pinched-out areas to maintain the hydraulic connection between underlying and overlying layers, the aquifer properties of the pinched-out areas generally are not included under an estimated parameter.

The model input identified by PID=TKV includes the model inputs identified by PID=T and PID=KV. This option enables the modeler to define a functional relation between the horizontal hydraulic conductivity (LAYCON=1) or transmissivity (LAYCON=0) of one or more model layers and the overlying vertical leakance, the underlying vertical leakance, the vertical leakance between layers (if there is more than one layer), or all of these. PID=ANIV is provided to enhance the applicability of the TKV option. To illustrate the use of PID=KV, TKV, and ANIV, consider the physical situations that vertical leakance is intended to represent, as discussed by McDonald and Harbaugh (1988, p. 5-11 to 5-18) and shown in figure A4.

In situation (A) of figure A4, the vertical leakance between layers  $k$  and  $k+1$  is calculated as (McDonald and Harbaugh, 1988, p. 5-17):

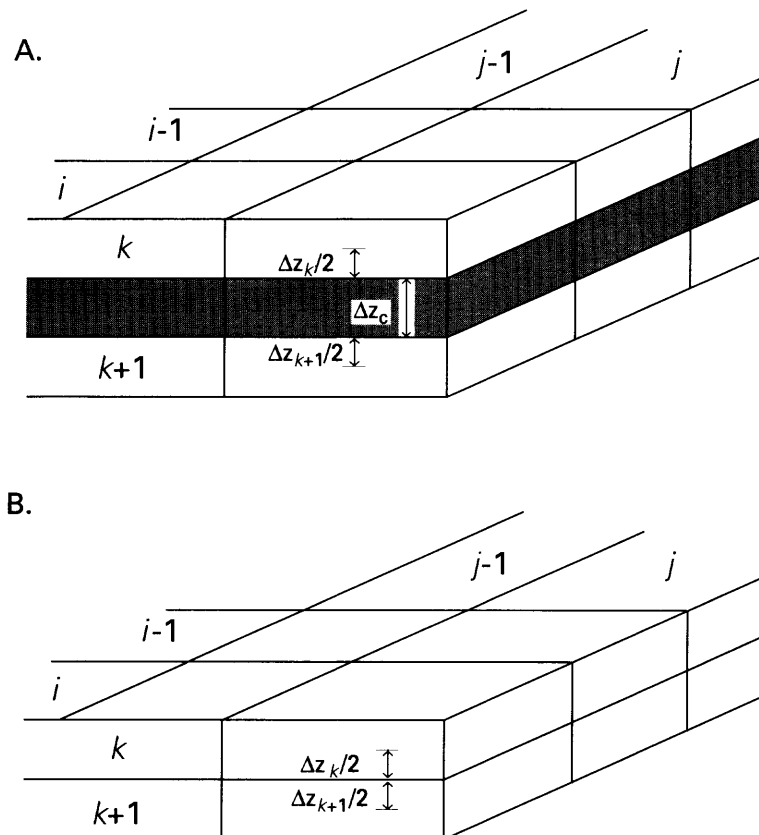
$$V_{cont\ i,j,k+\frac{1}{2}} = \left( \frac{\Delta z_k/2}{a_1 K_{i,j,k}} + \frac{\Delta z_c}{KZ_{c\ i,j,k+\frac{1}{2}}} + \frac{\Delta z_{k+1}/2}{a_2 K_{i,j,k+1}} \right)^{-1} \quad (A1)$$

where  $K_{i,j,k}$  is the horizontal hydraulic conductivity of the cell at row  $i$ , column  $j$ , and layer  $k$ ;

$a_1$  and  $a_2$  are vertical to horizontal anisotropies; and

$KZ_{c\ i,j,k+\frac{1}{2}}$  is the vertical hydraulic conductivity of the confining unit between layers  $k$  and  $k+1$ .





#### EXPLANATION

$i, j, k$	CELL ROW, COLUMN, AND LAYER NUMBER, RESPECTIVELY
$\Delta z_k, \Delta z_{k+1}$	THICKNESS OF MODEL LAYER $k$ and $k+1$ , RESPECTIVELY
$\Delta z_c$	THICKNESS OF CONFINING UNIT

Figure A4.--Subsurface layering represented by vertical leakage  
(A) with, and (B) without a distinct confining unit.

If  $a_1$  and  $a_2$  are known, and  $K_{i,j,k}$ ,  $KZ_{c_{i,j,k+\frac{1}{2}}}$ , and  $K_{i,j,k+1}$  are estimated independently, two TKV identifiers and one KV identifier need to be used. The two TKV identifiers are used to represent the contribution of  $K_{i,j,k}$  and  $K_{i,j,k+1}$  to  $V_{cont_{i,j,k+\frac{1}{2}}}$ , and the KV identifier is used to represent the contribution of  $KZ_{c_{i,j,k+\frac{1}{2}}}$ . For the two TKV identifiers, the product of the two parameter values and all multiplicative factors need to equal the individual leakances  $(a_1 K_{i,j,k})/(\Delta z_k/2)$  and  $(a_2 K_{i,j,k+1})/(\Delta z_{k+1}/2)$ , and the appropriate position, I, of  $NLL(I)$  needs to be used (see explanation for DATA SET 2 in "Instructions for the INPUT FILE"). For the KV identifier, the product of the parameter value and all multiplicative factors need to equal  $KZ_{c_{i,j,k+\frac{1}{2}}}/\Delta z_c$ . Terms from the three identifiers are combined correctly by the Parameter-Estimation Package to produce equation (A1).

Alternatives to the above scenario depend on what is known about the components of equation (A1). If  $a_1$  or  $a_2$  or both are unknown, they cannot be estimated uniquely because then a single value of  $V_{cont_{i,j,k+\frac{1}{2}}}$  could be produced by many different combinations of values of  $KZ_{c_{i,j,k+\frac{1}{2}}}$ , and  $a_1$  or  $a_2$  or both. ( $K_{i,j,k}$  and  $K_{i,j,k+1}$  are not included because they are used to calculate the transmissivities of the adjoining layers and thus independently impact the flow system if horizontal flow in the layers is significant.) Although individual components of equation (A1) cannot be estimated if  $a_1$  or  $a_2$  or both are unknown, an effective vertical hydraulic conductivity or leakance can be estimated. For example, if  $a_1$  is unknown, equation (A1) can be expressed as:

$$V_{cont_{i,j,k+\frac{1}{2}}} = \left( \frac{\Delta z_E}{KZ_{E_{i,j,k+\frac{1}{2}}}} + \frac{\Delta z_{k+1}/2}{a_2 K_{i,j,k+1}} \right)^{-1} \quad (A2)$$

where  $\Delta z_E$  is an effective thickness, and  $KZ_{E_{i,j,k+\frac{1}{2}}}$  is an effective vertical hydraulic conductivity. In this circumstance, one KV identifier and one TKV identifier are used to define the parameters. For the KV identifier, the product of the parameter value and all multiplicative factors needs to equal  $KZ_{E_{i,j,k+\frac{1}{2}}}/\Delta z_E$ . For the TKV identifier, the product of the parameter value and all multiplicative factors needs to equal  $(a_2 K_{i,j,k+1})/(\Delta z_{k+1}/2)$ .

If  $a_2$  also is unknown, one KV identifier is used to estimate one effective vertical hydraulic conductivity or leakance. The product of the parameter value and all multiplicative factors needs to equal  $KZ_{E_{i,j,k+\frac{1}{2}}}/\Delta z_E$ .

If it is known that the  $KZ_{C_{i,j,k+\frac{1}{2}}}$  term dominates  $Vcont_{i,j,k+\frac{1}{2}}$ , the smaller terms can be neglected and one KV identifier can be used. The product of the parameter and all multiplicative factors needs to equal  $KZ_{C_{i,j,k+\frac{1}{2}}}/\Delta z_C$ .

In situation (B) of figure A4, the vertical leakance is calculated as (McDonald and Harbaugh, 1988, p. 5-13):

$$Vcont_{i,j,k+\frac{1}{2}} = \left( \frac{\Delta z_k/2}{a_1 K_{i,j,k}} + \frac{\Delta z_{k+1}/2}{a_2 K_{i,j,k+1}} \right)^{-1}. \quad (A3)$$

If  $a_1$  and  $a_2$  are known and  $K_{i,j,k}$  and  $K_{i,j,k+1}$  are estimated independently, two TKV identifiers are used, as discussed previously.

If  $a_1$  and  $a_2$  are known and one parameter is used to estimate both  $K_{i,j,k}$  and  $K_{i,j,k+1}$ , one TKV identifier is used. For example, if  $cK_{i,j,k} = K_{i,j,k+1}$ , where  $c$  is a known constant and  $K_{i,j,k}$  is the parameter,

$$Vcont_{i,j,k+\frac{1}{2}} = K_{i,j,k} [(\Delta z_k/2a_1) + (\Delta z_{k+1}/2a_2c)]^{-1}. \quad (A4)$$

The product of the parameter value and the multiplicative factors need to equal equation (A4).

If  $a_1$  and  $a_2$  are unknown but satisfy  $ca_1=a_2$ ,

$$Vcont_{i,j,k+\frac{1}{2}} = a_1 \left[ \frac{\Delta z_k/2}{K_{i,j,k}} + \frac{\Delta z_{k+1}/2}{cK_{i,j,k+1}} \right]^{-1}, \quad (A5)$$

and the ANIV parameter identifier can be used to define  $a_1$  as a parameter.

In the Parameter-Estimation Package, the TKV identifier(s) (one if  $K_{i,j,k}$  and  $K_{i,j,k+1}$  are calculated using one parameter; two if they are not) are used to calculate the term in the brackets, which is then multiplied by the parameter value of the ANIV identifier. Under the TKV identifier(s), the product of all multiplicative factors used to define vertical leakance and the relevant parameter value needs to equal  $K_{i,j,k}/(\Delta z_k/2)$  or  $cK_{i,j,k+1}/(\Delta z_{k+1}/2)$ . Note that the multiplicative factor which relates the two anisotropies is included in a TKV identifier.

If either  $a_1$  or  $a_2$  is unknown in situation B of figure (A4), it could be uniquely estimated, but the Parameter-Estimation Package is not designed to solve this problem. In this situation, an effective vertical hydraulic conductivity or vertical leakance defined using a KV identifier needs to be estimated, as discussed above.

If  $a_1$  and  $a_2$  are unknown and are not related as above, they cannot be uniquely estimated. An effective vertical leakance defined using a single KV identifier needs to be estimated.

For PID=T, S1, RCH and ETM, the final model-input value can be calculated by summing the contributions from more than one parameter, as illustrated for a simple case in figure 3 and discussed in the section "Parameterization". Additions are performed differently for vertical leakances, as discussed above, but the following procedure still is used. To allow for additive options, the following procedure is implemented whether or not an additive option is used for a particular model input. If any PID=T, KV, TKV, S1, RCH, or ETM, the Parameter-Estimation Package sets the associated model input to zero at all cells, and then calculates values using DATA SETS 2 and 2B and initial (DATA SET 8) or estimated parameter values. Thus, if PID=T for any parameter, transmissivity is set to zero at all cells in confined layers and hydraulic conductivity is set to zero at all cells in unconfined layers. For parameters that can be time dependent (PID=RCH or ETM), the model input is set to zero at all time steps. If some of the additive contributions are assumed to be known and, therefore, are not to be estimated, they still need to be defined using DATA SETS 2 and 2B, and need to be among the last repetitions of these data sets. A negative group number in DATA SET 9 (see section "IWPG") is used to exclude the related parameter from updating by nonlinear regression. With the additive option, the same cell can appear under more than one DATA SET 2. The check initiated using ICHECK of LINE 4 of the INPUT FILE can be used to verify that cells are repeated as many times as expected.

Parameters defined using PID=Q, KRB, KDR, KST, GHB, CH, RCH, and ETM apply at time steps specified by the user. Except for PID=CH, the time steps are specified using all but the first element of array NLL of DATA SET 2 and can be continuous or discontinuous. Parameters defined using PID=CH can only apply at steady state, under transient conditions, or both, as specified by NLL(2).

Kriging can be used to parameterize spatially variable model inputs by producing multiplication matrices using a kriging algorithm. If the kriging is to be accomplished using estimated and known point values (de Marsily and others, 1984; Keidser and others, 1990), the known point values are included in the last repetitions of DATA SET 2, and the related IWPG value is negative (see section "IWPG" and the instructions for DATA SET 9). The multiplication array for this unestimated parameter can be produced by a kriging routine using a data set that includes the known point values and zeros for the estimated point values. The value of the unestimated parameter in DATA SET 8 would equal 1.0. For estimated point values that are estimated independently, each needs to be included in a repetition of DATA SET 2. The associated multiplication arrays can be produced by a kriging routine using a data set in which the point of interest has a value equal to one, and all other points have values equal to zero. After estimating point values, an experimental variogram using the measured and estimated point values needs to be produced and compared with the variogram used to do the kriging.

A second method of parameterization with kriging combines kriging with zonation (Keidser and others, 1990). In this method, the final estimated model-input values at a grid cell are calculated as the initial kriged value plus  $b_{\ell}\sigma^*$ , where  $b_{\ell}$  is a zoned, estimated parameter, and  $\sigma^*$  is the cell variance calculated by kriging using the initial set of point values of the model input. In this situation, the multiplication array for  $b_{\ell}$  is the variance map produced by kriging, and a zonation array is used to define its applicable area. The parameter  $b_{\ell}$  can be negative or positive, and the associated parameter number needs to be included in DATA SET 1C if the PID=T, KV, TKV, S1, or ETM. The initial kriged model-input distribution is included by using one of the last repetitions of DATA SET 2; set the associated parameter value of DATA SET 8 to 1.0, set the associated IWPG value of DATA SET 9 to a negative number, and set the associated multiplication array equal to the kriged model-input values.

Keidser and Rosbjerg (1991) used the two kriging methods discussed above and zonation to parameterize transmissivity in a transport problem. In their examples, they found that the first kriging method, in which individual point values are estimated, produced excessive small-scale variations in the transmissivity field caused by local overfitting. Including zonation resolved this problem.

EVH, EVF, and EV

EVH, EVF, and EV of DATA SET 5 are the estimated values of  $\sigma^2$ ,  $\sigma_h^2$ , and  $\sigma_f^2$  ( $\sigma^2$  needs to equal  $\sigma_h^2$  or  $\sigma_f^2$ ) of equations (17) and (22), and are used to calculate the weights of the dependent-variable observations as described in the explanations for DATA SETS 6 and 7A in "Instructions for the Input File." As discussed in the section "Structure and Use of the Weight Matrix", the calculated error variance printed at the end of the output of the Parameter-Estimation Package needs to approximately equal EV.

TOFF

TOFF (DATA SETS 6, 6C and 7A of the INPUT FILE) is the time-step offset that identifies a time after the end of the time step read as NDER(4) in DATA SETS 6 or 6C, or IQOB in DATA SET 7A, but before the end of the following time step. TOFF equals the fraction of the next time step that would have to occur to reach the desired time, and values of TOFF need to range from 0.0 to 1.0. As an example, consider a time 1.2 days into a simulation in which time step 3 ends at 1 day, and time step 4 ends at 1.3 days. In this example, the time step (NDER(4) or IQOB) equals 3 and TOFF=0.67. Values for the desired time are calculated by linearly interpolating between the values calculated at the end of the two time steps (fig. 5).

IWPG

The group numbers of DATA SET 9 are used to print residuals of prior parameter estimates specified using DATA SET 10, or to omit a defined parameter from parameter estimation. The latter is accomplished by making the group number negative. All group numbers larger than or equal to zero need to precede any negative group numbers, and the parameters are omitted from regression in the Parameter-Estimation Package by reducing NP, which is initially read from LINE 3.

TOL

TOL is the first parameter-estimation closure criterion discussed in the section "Convergence Criteria." Modified Gauss-Newton optimization converges if the fractional change of all parameters, as calculated by equation (50a), is less than or equal to TOL. TOL commonly equals 0.01 or 0.001 (each

calculated change cannot exceed 1.0 or 0.1 percent of the parameter value), but is problem dependent. Too small a value will have little impact on estimated parameters and might substantially increase execution time. If TOL is greater than the coefficients of variation of the parameters, the calculated standard deviation might be too small.

#### LPRINT

If LPRINT>0, eigenvalues and eigenvectors of the variance-covariance matrix scaled by the parameter values (see section "Analysis of results for linear problems") are calculated and printed. If LPRINT=1, subroutines DE2CSF and DEPISF from the IMSL(1987) library are used to do the calculation and compute a performance index; the IMSL library needs to be included when compiling MODFLOWP (see section, "Compiling and Loading MODFLOWP" of Appendix B).

If LPRINT=2 or 3, subroutines TRED2, TQLI, and EIGSRT from Press and others (1989) are used to calculate eigenvalues and eigenvectors; these routines are included in the Parameter-Estimation Package. If LPRINT=3, the accuracy of the eigenvalues and eigenvectors from TRED2, TQLI, and EIGSRT is tested using the basic definition of eigenvalues and eigenvectors, as suggested in an example on the FORTRAN example diskette associated with Press and others (1989). Given a matrix  $\underline{A}$  of order  $n$ ,  $n$  sets of eigenvalues and the associated eigenvectors need to satisfy  $\underline{A} \underline{x}_j = \lambda_j \underline{x}_j$ ,  $j=1,n$ , where  $\lambda_j$  is an eigenvalue, and  $\underline{x}_j$  is the associated eigenvector. The accuracy of the eigenvalues and eigenvectors is tested by calculating the product of the scaled variance-covariance matrix on the parameters and the eigenvectors (equivalent to  $\underline{A} \underline{x}_j$  above), and comparing each element of the resulting vector to the corresponding element of  $\underline{x}_j$ . If the ratio equals the eigenvalue,  $\lambda_j$ , the calculated eigenvalue and eigenvector are accurate.

The performance index from the IMSL library is more convenient than the test conducted when TRED2, TQLI, and EIGSRT are used, so use of LPRINT=1 is suggested when the IMSL library is available.

### Checking the INPUT FILE

To ensure that parameters are properly defined in the INPUT FILE, the following procedure can be used as a check and is STRONGLY RECOMMENDED FOR ALL APPLICATIONS OF THIS PACKAGE.

1. Construct MODFLOW package input files and run MODFLOWP without the Parameter-Estimation Package (IUNIT(15)=0).
2. Modify the MODFLOW input files (see section, "Changes to Input Files from Other Packages"), construct the INPUT FILE, and run MODFLOWP with the Parameter-Estimation Package (IUNIT(15)=the FORTRAN unit number of the INPUT FILE) and IPAR<0 (LINE 6 of the INPUT FILE).
3. The hydraulic heads and volumetric budgets for the entire model produced by (1) and (2) need to be IDENTICAL except for changes that are smaller in magnitude than the convergence criteria of the solver used. If they differ by more, an inconsistency exists between the two simulations and generally indicates errors in DATA SETS 2, 2A, 2B, 3, and 4 of the INPUT FILE, which are used to define the parameterization. Resolve all inconsistencies to ensure that the INPUT FILE is correct before proceeding!

To help in debugging, the model-input arrays produced by the Parameter-Estimation Package using the initial parameter estimates for PID=T, KV, TKV, S1, RCH, and ETM can be printed using IPRNP of LINE 4 of the INPUT FILE. If IPRNP equals IPRN used when reading the arrays for the model run without parameter estimation (McDonald and Harbaugh, 1988, p. E-1), the arrays printed from the two runs need to be identical to four or five significant digits.

### Outline of the INPUT FILE

The following outline briefly reviews the purpose and order of the lines and data sets of the INPUT FILE. The test cases at the end of this appendix provide examples of how the INPUT FILE is constructed.

LINE	Description	Number of repetitions
1	Title	1
2	Title	1
3	Data used to dimension arrays for parameterization	1
4	Data used in checking the parameterization	1
5	Data used to dimension arrays for observations	1
6	Data used to define what is to be calculated and how it is to be calculated	1
7	FORTTRAN unit numbers for input or output files	1
8	Data that indicate if DATA SETS 1A, 1B, and 1C are read	1



# Outline of the INPUT FILE--Continued

DATA SET	Description	Number of repetitions
1A	FORTTRAN input unit numbers identified within the Recharge or Evapotranspiration Packages.	1
1B	List of time steps at which all hydraulic heads and sensitivities are set to 0.0.	1
1C	List of usually positive parameters which are allowed to be negative.	1
2; immediately followed by associated 2A or repetitions of 2B, as needed.	Parameter definitions used to calculate model inputs from parameters. A typical sequence of data sets would be: 2, 2A, 2, 2B, 2B, 2, 2, 2A.	As many as are needed to define the NP parameters; NP if there are no CH parameters.
3	Multiplication arrays used to define parameters. Referred to in DATA SET 2B.	NMM times (LINE 3). Array 1 is first, 2 is second, and so on.
4	Zone arrays used to define parameters. Referred to in DATA SET 2B.	NZM times (see LINE 3). Array 1 is first, 2 is second, and so on.
5	$\sigma_h^2$ , $\sigma_f^2$ , unit numbers for reading observations, and $\sigma^2$ .	1
6; immediately followed by associated 6A, 6B, and 6C, as needed.	Observations of hydraulic head or temporal changes in hydraulic head. DATA SET 6 defines the observation location, and, unless DATA SETS 6B and 6C follow, the observation and its time and statistic. DATA SET 6A is used for multilayer observations. A typical sequence of data sets would be: 6, 6, 6, 6A, 6, 6B, 6C, 6.	DATA SET 6 needs to be repeated for each observation location, and can be repeated as many as NH times.
7; immediately followed by 7A and 7B.	Observations of head-dependent boundary gains and losses. A typical sequence of data sets would be: 7, 7A, 7B, 7, 7A, 7B. Note that each DATA SET 7 is always followed by a DATA SET 7A and 7B.	These three DATA SETS are repeated as a group NQ times (LINE 5).

Outline of the INPUT FILE--Continued

DATA SET	Description	Number of repetitions
8	Initial parameter values.	1
9	Parameter group numbers.	1
10	Allows initial parameter values to be used as prior estimates on the parameters (see eq. 28).	1
11	Flag that indicates whether the statistics of DATA SETS 9 and 12 are variances, standard deviations, or coefficients of variation.	1
12	Prior estimates that include more than one parameter (eq. 29) or that are independent of the initial parameter values.	MPR (LINE 5).
13	Data for the nonlinear regression.	1
14	Factors used to scale parameters for conjugate-direction optimization methods.	1

## Instructions for the INPUT FILE

FOLLOW PROCEDURE DESCRIBED IN THE PRECEDING SECTION TO CHECK THE INPUT FILE

LINE	COLUMN	FORMAT	VARIABLE	DEFINITION
1	1-80	A80	TITLE	Title printed when the SEN part of the Parameter-Estimation Package is first active.
2	1-80	A80	TITLE	

Data used to dimension arrays for parameterization. Usually it is best to construct the repetitions of DATA SET 2 before trying to determine NSM, NSN, NLLI1, and LZI1.

3	1-5	I5	NP	Number of parameters (includes estimated parameters and parameters that are not modified by the regression).
	6-10	I5	NSM	Total number of NLL values larger than zero for PID=T, KV, TKV, and S1, (see DATA SET 2). Add one for any PID=RCH or ETM with NLL(1)>0.
	11-15	I5	NSN	Number of cell locations listed for parameter definition in the INPUT FILE.  NSN equals the sum of the absolute values of NLL(1) for PID=GHB, Q, KRB, KDR, KST, and CH in DATA SET 2.
	16-20	I5	NLLI1	Largest number of values used for any NLL vector of DATA SET 2.
	21-25	I5	LZI1	Largest number of values used for any LZ vector of DATA SET 2B.
	26-30	I5	NMM	Number of multiplication arrays in DATA SET 3. NMM=0 if there are no multiplication arrays.
	31-35	I5	NZM	Number of zone arrays in DATA SET 4. NZM=0 if there are no zone arrays.

Data used in checking the parameterization.

4	1-5	I5	IPRNP	Output format code (see table A2) for model-input array produced by using initial parameter estimates for PID=T, KV, TKV, S1, RCH, or ETM. If IPRNP<0, no arrays are printed.
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Arrays are only printed if parameter estimates are used in their calculation, and in DATA SET 2, NLL>0. See section "Model-Input Arrays Produced with the Initial Parameter Estimates."

# Instructions for the INPUT FILE--Continued

LINE	COLUMN	FORMAT	VARIABLE	DEFINITION
4	6-10	I5	ICHECK	Flag used to indicate whether to check (ICHECK>0) or not to check (ICHECK=0) for cells that are repeated more than NUMR times (see below) in DATA SET 2 for model inputs defined by arrays.  Check involves parameters with PID=T, KV, TKV, S1, RCH, and ETM.  This check is useful in determining whether cells have been repeated under different PIDs as many times as intended. Also can be used to check that all cells in the applicable layers are included as needed (see fifth paragraph from end of section "Parameter Definition: DATA SETS 2, 2A, 2B, 3, and 4"). Set ICHECK=0 when not being used to reduce computer execution time.
11-15	I5	NUMR	NUMR	Number of times a cell can be repeated to define a single model input before an error message is printed.  Suggested usage: first set NUMR=1, and make sure repeated cells are as expected; then set NUMR=2, and make sure cells repeated more than once are as expected. Continue incrementing by 1 until the maximum number of repetitions is reached.
Data used to dimension arrays for observations.				
5	1-5	I5	NH	Number of observations of hydraulic head or changes in hydraulic head.
	6-10	I5	MOBS	Number of the NH locations and times that are multilayer (see section "Multilayer Hydraulic Heads" and instructions for DATA SET 6A).
	11-15	I5	MAXM	Maximum number of layers used for any of the MOBS locations (see instructions for DATA SET 6A).
	16-20	I5	NQ	Number of cell groups for which there are head-dependent boundary flow observations.
	21-25	I5	NQC	Total number of individual cells in the NQ groups (sum of absolute values of all NQCL in repetitions of DATA SET 7).
	26-30	I5	NQT	Total number of head-dependent flow observations (sum of all values of NQOB in repetitions of DATA SET 7).
	31-35	I5	MPR	Number of equations of prior information on the parameters that include more than one parameter (see eq. 29).

## Instructions for the INPUT FILE--Continued

LINE	COLUMN	FORMAT	VARIABLE	DEFINITION
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Data used to define what is calculated and how it is calculated.

6	1-5	I5	IPAR	Flag identifying what to calculate. If IPAR<0, hydraulic heads are calculated; if IPAR=0, hydraulic heads and sensitivity equations (ISN<0) or adjoint states (ISN>0) are calculated; if IPAR>0, parameter-estimation is performed. See section "IPAR".
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For all IPAR values, model inputs calculated using the parameter values of DATA SET 8 replace the values from the input files for other packages, where applicable.

6-10	I5	ISN	Flag identifying which optimization and numerical methods are used. See section "ISN". Generally, ISN=-1.
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If ISN<0, sensitivity-equation sensitivities are calculated, and parameter estimation is performed by the modified Gauss-Newton method. ISN can equal -1 or -2.

If ISN>0, the adjoint-state method is used to calculate the gradient of the objective function, and parameter estimation is performed by the conjugate-direction method. ISN can equal 1, 2, or 4.

ISN=-1 worked most efficiently for the test problems considered by Cooley (1985) and Hill (1990).

**\*\*ISN>0 cannot be used if there are any water-table layers or if NQT>0\*\***

**\*\*Use ISN=-1 if there are water-table layers and if cells go dry for any parameter-estimation iteration\*\***

11-15	I5	ISCALS	If ISCALS>0 or KPRINT>0 in DATA SET 13, printed sensitivity-equation sensitivities are scaled by multiplying by the parameter value and the square root of the weight. Scaled sensitivities can be used to compare the relative influence of different parameters.
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16-20	I5	NOPT	When NOPT=1 and ISN<0, $R$ of equation (51) is included in equation (50a) after NFIT (DATA SET 13) modified Gauss-Newton iterations or after two iterations fail to reduce the sum of squared, weighted residuals by SOSR×100 percent (DATA SET 13).
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# Instructions for the INPUT FILE--Continued

LINE	COLUMN	FORMAT	VARIABLE	DEFINITION
FORTRAN unit numbers for input or output files.				
7	1-5	I5	IUHEAD	First output/input unit for hydraulic heads or sensitivity-equation sensitivities stored in binary format.
This unit and NP (LINE 3) or NPER (as specified in the Basic Package input file) sequentially numbered additional units are opened in MODFLOWP. An error message is printed and execution stops if the units are already open.				
6-10	I5	IOUB	IOUB	Output unit number for estimated parameter values.
File IOUB is used to print parameter estimates and selected statistics from all parameter-estimation iterations at the end of the output file, and to provide parameter values with which to restart the parameter-estimation routine (see section "Restarting the Parameter-Estimation Routine"). If IOUB=0, the parameter estimates and statistics are not written on a separate file and are not printed at the end of the output file. Generally, IOUB≠0.				
11-15	I5	IUBD	IUBD	Input unit for IBOUND arrays.
See items 3 and 4 of the section "Changes to Input Files from Other Packages."				
If IUBD>0, NPER>1 in the Basic Package input file, and all layers are confined, two IBOUND arrays are read from FORTRAN unit IUBD by using U2DINN, which functions like U2DINT (McDonald and Harbaugh, 1988, p. 14-30) except that nothing is printed. The first IBOUND array is for steady-state conditions; the second IBOUND array is for transient conditions. If IUBD>0, and NPER<1 or there are water-table layers, one IBOUND array is read. If IUBD=0, the IBOUND array specified in the Basic Package input file is used, and no other input file is required.				
** If there are any water-table layers and cells go dry for any parameter-estimation iteration, use IUBD>0 **.				
16-20	I5	IUNHEA	IUNHEA	IUNHEA≠0 if known hydraulic heads at constant hydraulic-head boundaries change during the simulation. See text in section "IUNHEA".

# Instructions for the INPUT FILE--Continued

LINE	COLUMN	FORMAT	VARIABLE	DEFINITION
Data that indicate if DATA SETS 1A, 1B, and 1C are read.				
8	1-5	I5	NRWD	Number of FORTRAN input units identified from within the Recharge and Evapotranspiration Packages using LOCAT. If NRWD>0, DATA SET 1A is read.
Files used as multiplication arrays (DATA SET 3) cannot be read by other packages and cannot be included here and in DATA SET 1A.				
	6-10	I5	NZER	Number of time steps >0 at which hydraulic head equals zero. If NZER>0, DATA SET 1B is read.
	11-15	I5	NPNG	Number of parameters with PID=T, KV, TKV, S1, or ETM that can have negative values. If NPNG>0, DATA SET 1C is read.

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
Omit DATA SET 1A if NRWD=0 (LINE 8).				
1A	1 or more	16I5	IRWD	NRWD FORTRAN input unit numbers that are identified from within the Recharge or Evapotranspiration Packages using LOCAT.
Omit DATA SET 1B if NZER=0 (LINE 8).				
1B	1 or more	16I5	IZER	NZER time steps at which all hydraulic heads and sensitivities are set to 0.0.
Used when estimating parameters with multiple superposition simulations (see item 8d in section "Changes to Input Files from Other Packages").				
Omit DATA SET 1C if NPNG=0 (LINE 8).				
1C	1 or more	16I5	IPNG	NPNG parameter numbers for which PID=T, KV, TKV, S1, or ETM, and parameters are defined with the second kriging method discussed at the end of section "Parameter Definition: DATA SETS 2, 2A, 2B, 3, and 4."

## Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
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DATA SETS 2, 2A, 2B, 3, and 4 are used to calculate model inputs from the parameters. See section "Parameter Definition: DATA SETS 2, 2A, 2B, 3 and 4." Repeat DATA SET 2, and DATA SET 2A or 2B, when required, until all NP parameters are defined.

NOTE: A parameter cannot be reliably estimated if the values calculated at all observation points are insensitive to that parameter, prior estimates are missing or inaccurate, or if the parameter is highly correlated with one or more other parameters (see "Analysis of Results for Linear Problems"). To avoid these problems, MINIMIZE THE NUMBER OF ESTIMATED PARAMETERS.

2	1	A4,I1, 11I5 For ad- ditional lines, Use 16I5	PID, LN, NLL(I), I=1,NLLI1	Parameter identifier, natural log indicator, and vector used as described below. NLLI1 is specified on LINE 3.
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PID needs to be left-justified and in upper-case letters. PID options are listed in table A1.

LN>0 indicates that the parameter to be estimated is the natural log of the defined quantity. Valid only for PID=GHB, KRB, KDR, KST, T, KV, TKV, and S1.

NLLI1 (LINE 3) values are read for the NLL array.

DATA SET	EXPLANATION
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2	PID = ANI: The NLL(I) values equal the model-layer numbers to which this horizontal anisotropy applies; no additional records follow.
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PID = Q, KRB, KDR, KST, and GHB: The absolute value of NLL(1) equals the number of cell locations that follow in DATA SET 2A. NLL(1)<0 indicates that FACTOR of DATA SET 2A will be set to 1.0 for all listed cells.

NLL(I), I=2, NLLI1, are used to indicate the time steps at which the pumpage rate or head-dependent boundary condition applies. The parameter starts at the beginning of time step NLL(2), and stops at the end of time step NLL(3); the parameter starts again at the beginning of time step NLL(4), and stops at the end of NLL(5); and so forth. If applied at one time step, NLL(I)=NLL(I+1), where I is an even number. For steady state, use zero.

For Q, KRB, KDR, KST, and GHB, unused values of NLL(I) (for example, if 3 values are needed to define the parameter, but NLLI1=6, there would be 3 unused values) need to be negative because a zero or blank is interpreted as steady state.



## Instructions for the INPUT FILE--Continued

### DATA SET

### EXPLANATION

- 2 PID = CH: NLL(1) needs to be positive and equals the number of cells that follow in DATA SET 2A. NLL(2) equals the number of parameters defined under this identifier. NLL(3) indicates when the constant hydraulic-head boundary applies and is used as follows:

<u>NLL(3)</u>	<u>When CH applies</u>
0	Steady state only.
1	Transient only.
2	Both steady state and transient.

NLL(I), I=4,NLLI1, equal the layers in which this constant hydraulic-head boundary condition applies. Unused values need to be blank or zero; nonzero values need to precede blanks and zeros. See figures A1 and A2 for situations that can and cannot be represented with PID=CH.

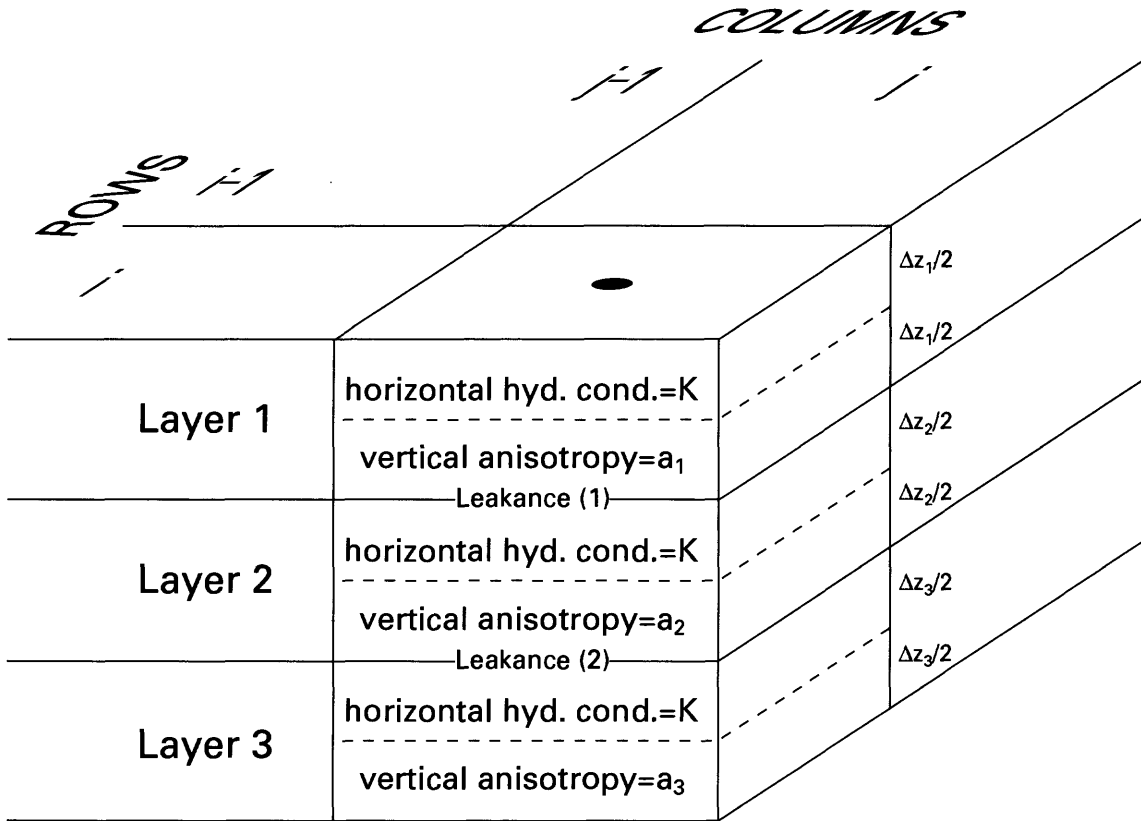
PID = RCH and ETM: The components of NLL are not layer numbers; layer numbers are determined by using NRCHOP and array INRECH of the Recharge Package input file or by using NEVTOP and array IEVT of the Evapotranspiration Package input file (McDonald and Harbaugh, 1988, ch. 7 and 10). The components of NLL are used as follows: NLL(1)<0 indicates that the parameter equals the recharge or maximum evapotranspiration rate at all active cells where recharge or evapotranspiration apply, and no additional records follow; NLL(1)>0 indicates that the parameter is a multiplicative constant, applies over part of the modeled area, or both, and DATA SET 2B follows. NLL(I),I=2,NLLI1 are used for temporal definition as explained above for Q, KRB, KDR, KST, and GHB.

As above, unused values of NLL(I) need to be negative.

PID = T, KV, and S1: NLL is a list of layer numbers where: NLL(I)<0 indicates that the parameter equals the model-input value at all active cells of layer |NLL(I)|, and no additional records follow; NLL(I)>0 indicates that the parameter is a multiplicative constant, applies to only part of layer NLL(I), or both, and DATA SET 2B is read for each NLL(I)>0 in the order in which these positive values occur. Nonzero NLL values need to precede zeros and blanks.

# Instructions for the INPUT FILE--Continued

DATA SET	EXPLANATION
2	<p>PID = TKV: NLL is a list of layer numbers where positive and negative values are used as described for PID = S1, T, and KV. When I equals <math>1+3k</math>, where <math>k=0,1,2,\dots</math>, so that <math>I=1,4,7,\dots</math>, NLL(I) is used to define vertical leakance between layer NLL(I) and the layer above (last term of eq. A1 or A2); when I equals <math>2+3k</math>, so that <math>I=2,5,8,\dots</math>, NLL(I) is used to define horizontal hydraulic conductivity or transmissivity; when I equals <math>3+3k</math>, so that <math>I=3,6,9,\dots</math>, NLL(I) is used to define vertical leakance between layer NLL(I) and the layer below (first term of eq. A1 and A2). To allow full generality, nonzero numbers can be preceded by zeros or blanks; no DATA SET 2B is read for a zero or blank. For example, NLL(I)=0,1,1,2,2,2,3,3 indicates that the horizontal hydraulic conductivity or transmissivity of layers 1, 2, and 3 are related to each other and to the vertical leakances between these three layers, and seven repetitions of DATA SET 2B would be read. If the parameter is defined as the horizontal hydraulic conductivities of the three layers, which are considered to be equal, and <math>a_1</math>, <math>a_2</math>, and <math>a_3</math> are vertical anisotropies of the three layers, the seven repetitions would be defined as shown in figure A5.</p> <p>PID = ANIV: The NLL(I) values equal the layer numbers above the applicable vertical leakance. Vertical leakance is calculated using TKV identifiers, and then is multiplied by the value of the ANIV parameter. See equation A5.</p>



Layer 1 is a water-table layer; therefore  $\Delta z_1$  is approximate.

K is the parameter. The eight components of array  
NLL are 0,1,1,2,2,2,3,3.

Seven repetitions of DATA SET 2B are required. For each repetition,  
K times SFAC of DATA SET 2B, and CNSTNT and the elements  
of the multiplication array of DATA SET 3 must equal:  
(description of required model inputs are in brackets)

- 1) K [horizontal hydraulic conductivity of layer 1]
- 2)  $a_1 K / (\Delta z_1 / 2)$
- 3)  $a_2 K / (\Delta z_2 / 2)$  }  $\left[ \text{Leakance (1)} = \left( (\Delta z_1 / 2) / a_1 K + (\Delta z_2 / 2) / a_2 K \right)^{-1} \right]$
- 4)  $K \Delta z_2$  [transmissivity of layer 2]
- 5)  $a_2 K / (\Delta z_2 / 2)$
- 6)  $a_3 K / (\Delta z_3 / 2)$  }  $\left[ \text{Leakance (2)} = \left( (\Delta z_1 / 2) / a_2 K + (\Delta z_3 / 2) / a_3 K \right)^{-1} \right]$
- 7)  $K \Delta z_3$  [transmissivity of layer 3]

Figure A5.--Use of repetitions of DATA SET 2B when PID=TKV.

## Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
2A	Absolute value of NLL(1)	See below	CELS(I), I=1,3, FACTOR	List of cells where the parameter is used to calculate a model input.

Four format options are available to read DATA SET 2A to permit files developed for other packages of MODFLOW to be used more directly. The format is selected based on PID (DATA SET 2).

PID = Q: 4F10.0 is used to read the layer, row, column, and FACTOR of a cell.

PID = GHB, KRB, and KDR: 3F10.0, 10X, F10.0 is used to read the layer, row, column, and FACTOR of a cell.

PID = KST: 15X, 2F5.0, 25X, F10.0 is used to read the segment, reach, and FACTOR of a cell.

PID = CH: 10X, 3F10.0 is used to read the row, column, and FACTOR of a cell.

Note that integers and real numbers with digits to the right of the decimal point can be read using F10.0 and F5.0 formats.

FACTOR is used to calculate the model input for the PID in the preceding DATA SET 2 (see table A1) from the parameter value.

PID = Q, KRB, KDR, KST, and GHB: If NLL(1)>0, the model input equals the parameter value multiplied by the FACTOR of DATA SET 2A; if NLL(1)<0, the parameter is equivalent to the model input, and FACTOR is set to 1.0 by the program, regardless of the value specified in DATA SET 2A. The order of cells in DATA SET 2A needs to match the order of cells in the associated package input file; if cell 1 precedes cell 10 in the package input file, it needs to precede cell 10 in DATA SET 2A.

PID = CH: Values along a constant hydraulic-head boundary are linearly interpolated between cells with FACTOR>1.0 or FACTOR<0.0; at all other cells, FACTOR needs to equal zero. The parameters are the hydraulic heads at the center of the cells with FACTOR>1.0. Equal positive FACTORS indicate that the constant hydraulic heads at these and intervening cells are equal. Equal positive FACTORS need to be grouped; that is, they can be separated only by zeros. The head at a cell with FACTOR<0.0 remains at the value specified in Shead of the Basic Package input file.

All cells listed under a CH identifier need to be designated as constant head in the IBOUND array read from the Basic Package input file, or the appropriate IBOUND array(s) read from FORTRAN unit IUBD (LINE 7). See figures A1 and A2 for additional restrictions.

# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
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Repeat DATA SET 2B once for each  $NLL(I) > 0$  in the preceding DATA SET 2 for  $PID=RCH, ETM, S1, T, KV, \text{ or } TKV$ . The first DATA SET 2B is associated with the first  $NLL(I) > 0$ , the second is associated with the second  $NLL(I) > 0$ , and so on.

2B	Number of $NLL(I) > 0$ in preceding DATA SET 2 for $PID$ 's listed above.	F10.0,I5, 14I5 After first line, use 16I5.	SFAC, LM, LZA, LZ(I), I=1, LZI1	Factor, multiplication array number (DATA SET 3), zone array number (DATA SET 4), and zone numbers (LZ(I), $I=1, LZI1$ ). LZI1 is specified on LINE 3. The F10.0 format allows the decimal point to be specified anywhere in the field.
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For information about the use of SFAC, LM, LZA, and LZ(I), and a discussion of which cells need to be included in a DATA SET 2 and 2B if  $PID=T, KV, TKV, S1, RCH, \text{ or } ETM$  for any parameter, see section "Parameter Definition: DATA SETS 2, 2A, 2B, 3, and 4."

If  $LM=0$ , a default multiplication array with all elements equal to 1.0 is used.

If  $LZA=0$ , zonation is not used to limit the areal extent of the parameter. The parameter will apply to all active cells with nonzero values in the multiplication array in the layer specified in DATA SET 2.

Zone numbers need to be positive, nonzero integers; in LZ(I), nonzero numbers need to precede blanks or zeros.

## Instructions for the INPUT FILE--Continued

DATA SET	EXPLANATION
Omit DATA SET 3 if no multiplication arrays are used (LINE 3: NMM=0).	
3	NMM (LINE 4) NROW×NCOL multiplication arrays. Read by using module U2DREL of McDonald and Harbaugh (1988, p. 14-26 to 14-29; E-1).  Multiplication array numbers are referenced by variable LM of DATA SET 2B. Multiplication array number 1 needs to be first, number 2 needs to be second, and so on.  If the parameter is to be used to calculate the model input in only part of the area, zeros can appear in the multiplication array for uninvolved cells, or zonation (see DATA SET 4) can be used to limit the areal extent of the parameter. The product of the parameter, SFAC of DATA SET 2B, CNSTNT of U2DREL, and the nonzero entries of the multiplication array, needs to equal the model input described in table A1 (see also the section "Parameter Definition: DATA SETS 2, 2A, 2B, 3, and 4"). See figure A3 for an example of how multiplication arrays are used.
Omit DATA SET 4 if no zone arrays are used (LINE 3:NZM=0).	
4	NZM (LINE 4) NROW×NCOL zone arrays. Read by using module U2DINT of McDonald and Harbaugh (1988, p. 14-30 to 14-34; E-1).  Zone array numbers are referenced by LZA of DATA SET 2B; zone numbers are referenced by LZ of DATA SET 2B. Zone array number 1 needs to be first, number 2 needs to be second, and so forth. Each zone array can include many zone numbers.  For each DATA SET 2B, the specified zone array, LZA, needs to include all zone numbers referenced in the array LZ. See figures A3.A and A3.B for examples of how zone arrays are used.

# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
5	1	2F10.0, 2I5, F10.0	EVH, EVF, IUH, IUF, EV	Factors $\sigma_h^2$ , $\sigma_f^2$ of equation (22), input unit numbers for hydraulic head and head-dependent boundary flow gain or loss observations (DATA SETS 6 and 7), and the estimated common error variance ( $\sigma^2$ of eq. 17).

Either EVH or EVF needs to equal EV.

If equal to zero, IUH and IUF are set equal to the input unit number of the INPUT FILE.

DATA SET 6 and, if required, 6A and(or) 6B and 6C are read from input unit IUH (DATA SET 5), and needs to be repeated for each hydraulic-head observation location.

Transient data can be included by repeating DATA SET 6 or by using DATA SETS 6B and 6C.

Omit these DATA SETS if NH=0 (LINE 5).

6	1	A4,1X, 4I5, 3F8.0, F10.0, F8.0,I5	DID, NDER(I), I=1,4; ROFF,COFF, TOFF, HOBS, WT, IWT	Data identifier (any four characters the user chooses), layer, row, column, time step (zero for steady-state), row and column offsets used to locate the observation point within a cell (must range from -0.5 to 0.5; see fig. 6), time-step offset (must range from 0.0 to 1.0; see fig. 5 and section "TOFF"), observed head, the value from which the weight of the observed head is calculated, and a flag to indicate whether WT is a scaled variance (IWT=0), a scaled standard deviation (IWT=1), or a scaled coefficient of variation (IWT=2).
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When IPAR<0 (LINE 6), HOBS, WT, and IWT are printed and used to calculate weighted residuals. WT needs to be greater than zero.

If NDER(1)<0, The observation is multilayer, and DATA SET 6A is read.

If NDER(4)<0, -NDER(4) time steps are involved, and DATA SETS 6B and 6C are read. DID, HOBS, and WT of DATA SET 6 are replaced when DATA SET 6C is read.

Weights are calculated as  $EV/(WT \times EVH)$  for IWT=0,  $EV/(WT^2 \times EVH)$  for IWT=1, and  $EV/((WT \times HOBS)^2 \times EVH)$  for IWT=2. EVH and EV are read from DATA SET 5.

In transient simulations, the steady-state IBOUND array is used to identify inactive cells for the interpretation with ROFF and COFF (fig. 6).

# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
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Omit DATA SET 6A if  $NDER(1) > 0$  in the preceding repetition of DATA SET 6.

6A	1	8(I5, F5.0)	(MLAY(I), PR(I)), I=1, -NDER(1)	Layer numbers for a multilayer observation well, and the proportions assigned to each layer.
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There can be as many as MAXM (LINE 5) layers; the proportions need to sum to 1.0.

The first layer is used to calculate interpolation coefficients for arbitrary locations within the finite-difference cell (see figs. 7 and 8).

Omit DATA SETS 6B and 6C if  $NDER(4) > 0$  in the preceding DATA SET 6.

6B	1	I5	ITT	Flag for transient observations.
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ITT	Description
1	Observed hydraulic heads are used for parameter estimation.
2	Observed initial hydraulic head and subsequent changes in hydraulic head are used for parameter estimation.

6C	-NDER(4) from DATA SET 6	A4,1X I5, F8.0, 3F10.0, I5	DID, NDER(4), TOFF, HOBS,WT <sub>h</sub> , WT <sub>DD</sub> , IWT	Data identifier, time step, time-step offset, observed head, values from which the weight for head or for drawdown (used when ITT=2) is calculated, and a flag that is used as described for DATA SET 6.
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The first line of this DATA SET needs to be the earliest observed hydraulic head at this location used for parameter estimation.  
WT<sub>h</sub> is always used for the first observation.

The time step read as NDER(4) in the first line of DATA SET 6C replaces the value of NDER(4) read in DATA SET 6.

When  $IPAR < 0$ , HOBS, WT<sub>h</sub>, WT<sub>DD</sub>, and IWT are printed and used to calculate weighted residuals. WT<sub>h</sub> and WT<sub>DD</sub> need to be greater than zero.



# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
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DATA SETS 7, 7A, and 7B are read from input unit IUF (DATA SET 5), and are repeated for each of the NQ cell groups (LINE 5) that define head-dependent boundaries with observed gains or losses. Omit these DATA SETS if NQ=0.

7	1	3I5	IBT, NQOB,NQCL	Boundary type, number of times at which head-dependent boundary gains or losses are observed for this group, and number of cells in this group (fig. 9).
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If NQCL<0, the FACTORS of DATA SET 7B are set equal to 1.0, and the number of cells is set equal to -NQCL.

IBT values: 1, River Package; 2, General-Head Boundary Package; 3, Stream Package; 4, Drain Package. If IBT=3, NQCL equals the number of reaches in the group.

7A	NQOB	A4,1X, I5,F8.0 2F10.0, I5	DID,IQOB, TOFF, HOBS,WT, IWT	Data identifier (any four characters the user chooses), time step (zero for steady state), time-step offset (must range from 0.0 to 1.0; see fig. 5 and section "TOFF"), observed head-dependent boundary gain or loss (in L <sup>3</sup> /T; losses indicate flow into the aquifer and are positive), the value from which the weight for observed flux is calculated, and a flag that is used as in DATA SET 6.
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When IPAR<0, HOBS, WT, and IWT are printed and used to calculate weighted residuals. WT needs to be greater than zero.

Weights are calculated as EV/(WT×EVF) for IWT=0, EV/(WT<sup>2</sup>×EVF) for IWT=1, and EV/((WT×HOBS)<sup>2</sup>×EVF) for IWT=2. EVF and EV are read from DATA SET 5.

7B	NQCL	See definition	QCLS(I), I=1,3, FACTOR	For IBT=1, 2, or 4 (DATA SET 7) 4F10.0 is used to read the layer, row, column, and FACTOR of each cell in the group. For IBT=3, 15X, 2F5.0, F10.0 is used to read segment, reach, and FACTOR.
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Note that integers and real numbers with digits to the right of the decimal point can be read using F10.0 or F5.0 format.

FACTOR needs to be set to 1.0 unless only part of the gain or loss for the cell is to be included; then FACTOR is used to allocate the calculated gain or loss in this cell or reach (see eq. 4 and fig. 9).

If NQCL of DATA SET 7 is negative or FACTOR = 0.0, FACTOR is set to 1.0.

# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
8	1 or more	8F10.0	B(I), I=1,NP	Initial parameter values. B(1) is the initial value of the first parameter defined under the first repetition of DATA SET 2; B(2) is the initial value of the second parameter defined under a DATA SET 2, and so on.

Parameter values specified here are used to replace model-input values read from the input files for other packages.

Even if LN of the associated DATA SET 2 is not 0, do not log transform the value of the parameter specified in DATA SET 8; log transformations are done by the Parameter-Estimation Package.

\*\*Convergence of parameter estimation can depend on the initial values used. If problems with convergence occur, see section "Common Problems" \*\*

9	1 or more	8I10	IWPG(I), I=1,NP	Parameter group numbers. See section "IWPG." IWPG(1) is the group number of the first parameter defined under the first repetition of DATA SET 2; IWPG(2) is the group number of the second parameter defined under a DATA SET 2, and so on.
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Positive group numbers: Residuals related to prior information listed in DATA SET 8 are printed by group. Group numbers need to be less than or equal to the number of estimated parameters.

Negative group numbers: Parameter values are substituted into model arrays but are not estimated by regression.

\*\*All positive group numbers need to precede any negative group numbers.\*\*

DATA SETS 10 through 14 are read only if IPAR>0 (LINE 6).

10	1 or more	8F10.0	WP(I), I=1,NP	If WP(I)≠0.0, the Ith initial value of DATA SET 8 is used as the prior estimate of the parameter (eq. 28).
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Weights of the prior estimates are calculated for WP(I)≠0.0, as indicated by IWP of DATA SET 11. If IWP=0, the nonzero WP(I) are variances; if IWP=1, they are standard deviations; and if IWP=2, they are coefficients of variation.

If LN(I)≠0 (see DATA SET 2), WP(I) describes the probability distribution function of the natural log of the parameter.

# Instructions for the INPUT FILE--Continued

DATA SET	NUMBER OF LINES	FORMAT	VARIABLE	DEFINITION
11	1	I10	IWP	Flag to indicate how the WP of DATA SETS 10 and 12 are used to calculate weights.

Weights are calculated as  $EV/WP(I)$  for  $IWT=0$ ,  $EV/(WP(I))^2$  for  $IWT=1$ , or  $EV/(WP(I) \times B(I))^2$  for  $IWT=2$ .  $EV$  is the estimated common error variance from DATA SET 5;  $B(I)$  is the initial value of the  $I$ th parameter from DATA SET 8. When  $IWT=2$ , a value of 1.0 is used when  $B(I)=0.0$ , and  $\ln B(I)$  replaces  $B(I)$  when  $LN(I) \neq 0$  (DATA SET 2).

DATA SET 12 needs to be repeated  $MPR$  times (LINE 5). Omit if  $MPR=0$ .

12	1 or more	8F10.0	PRM(I), I=1,NP, PRE, WP	NP coefficients, the prior estimate, and the value from which the weight of the prior estimate is to be calculated.
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See section "Restarting the Parameter-Estimation Routine" for an example of how DATA SET 12 can be used.

$PRM(I)$  is the coefficient of the  $I$ th parameter; if  $PRM(I)=0.0$ , the  $I$ th parameter is not included.

$WP$  is used to calculate a weight by using  $IWP$  of DATA SET 11 and the equations stated there, with  $WP$  replacing  $WP(I)$ . For  $IWP=2$ ,  $PRE$  replaces  $B(I)$ .

If  $ISN>0$  (LINE 6), either the  $SCL(I)$  (DATA SET 14) related to all  $PRM(I) \neq 0$  need to be equal, or only one  $PRM(I) \neq 0$ .

If  $PRM(I) \neq 0.0$  for more than one  $I$ , no log-transformed parameters can be included.

For log-transformed parameters,  $PRE$  needs to be untransformed, but  $WP$  describes the normal probability distribution function of the natural log of the parameter. Thus, the definition of  $PRE$  and  $WP$  of DATA SET 12 are consistent with the definition of  $B(I)$  and  $WP(I)$  of DATA SETS 8 and 10, respectively.

# Instructions for the INPUT FILE--Continued

DATA SET	COLUMN	FORMAT	VARIABLE	DEFINITION
13	1-5	F5.0	DMAX	Maximum fractional change for parameter values in one iteration. Used to calculate $\rho_r$ of equation (50b).  If DMAX<1.0, parameters cannot change sign (see discussion after eq. 54).
6-10	F5.0	CSA	Search direction adjustment parameter used in Marquardt procedure.  CSA=0.08 is the value suggested by Cooley and Naff (1990, p. 71-72, 91). Used only in modified Gauss-Newton optimization.	
11-15	F5.0	TOL	Parameter-estimation closure criterion. See "TOL." Commonly equals 0.01 or 0.001.	
16-20	I5	ITMXP	Maximum number of parameter-estimation iterations. Commonly equal to 1.5 times the number of estimated parameters for modified Gauss-Newton optimization.	
21-25	F5.0	FCONV	If FCONV>0, coarser solver convergence criteria are used when calculating hydraulic heads and sensitivities for the earlier parameter-estimation iterations.  Commonly, FCONV=0.0. Typical nonzero values of FCONV would be 5.0 or 10.0. See the section, "Reducing Computer Execution Time of Modified Gauss-Newton Optimization" for additional information.	
26-30	I5	IPRIOR	If IPRIOR=0, prior information from DATA SETS 10 and 12 is disregarded.	
30-35	I5	IOUR	Output unit for unformatted data to be used by RESAN.MODP, a residual analysis program. If IOUR=0, nothing is output.	
36-40	I5	IPRC	Format code with which the variance-covariance and correlation matrices are printed when parameter estimation converges. Options are listed in table A2; IPRC=2 usually produces a satisfactory printout.	

## Instructions for the INPUT FILE--Continued

DATA SET	COLUMN	FORMAT	VARIABLE	DEFINITION
13	41-45	I5	IPRINT	Controls printing of selected items at each iteration.  The controlled items are: for $ISN < 0$ , the scaled least-squares matrix (eq. 50a), observation data and sensitivities, and prior-estimate data; for $ISN > 0$ , the observation and prior-estimate data. Runs-test statistics (see "Analysis of Results for Linear Problems") are printed with the observation and prior-estimate data.  If $IPRINT > 0$ , the items are printed at each iteration.  If $IPRINT = 0$ , the observation-point and prior-estimate data and, for $ISN < 0$ , sensitivities, are printed at the first and last iterations.
46-50	I5	KPRINT		If $KPRINT = 1$ , hydraulic-head arrays for the parameter values for which parameter estimation converges are printed and saved, as specified in the Output Control input file. Otherwise, set $KPRINT = 0$ .
51-55	I5	LPRINT		If $LPRINT > 0$ , the eigenvalues and eigenvectors of the variance-covariance matrix scaled with the final parameters are printed upon convergence of parameter estimation.  Used only when the covariance matrix is calculated (on LINE 6, $ISN < 0$ or, in DATA SET 13, $LASTX > 0$ ). $LPRINT$ may equal 0, 1, 2, or 3; see section "LPRINT."
56-60	I5	LASTX		Controls calculation of sensitivity-equation sensitivities used to calculate the variance-covariance matrix on the parameters (eq. 35) when parameter estimation converges.

When  $ISN < 0$ : If  $LASTX = 0$ , sensitivities from the last parameter-estimation iteration are used. If  $LASTX > 0$ , sensitivities calculated by using the final parameter estimates are used.  $LASTX = 0$  saves computer time and usually produces a satisfactory variance-covariance matrix.

When  $ISN > 0$ : If  $LASTX = 0$ , the variance-covariance matrix is not calculated. If  $LASTX > 0$ , the variance-covariance matrix (eq. 35) and the correlation matrix are calculated and printed, and  $-LASTX$  is used in the same way as  $ISN$  when  $ISN < 0$  to define the method used to calculate the sensitivities (see  $ISN$  on LINE 6).

# Instructions for the INPUT FILE--Continued

DATA SET	COLUMN	FORMAT	VARIABLE	DEFINITION
13	61-65	I5	NFIT	Number of Fletcher-Reeves (ISN=2) or Gauss-Newton (ISN<0; NOPT=1) iterations. If ISN=2, NFIT needs to be equal to or greater than ITMXP. (ISN and NOPT are on LINE 6). See section "Parameter Estimation and Analysis of Results using Nonlinear Regression."
	66-70	F5.0	SOSC	The second convergence criterion discussed in the section "Convergence Criteria." Parameter estimation using the modified Gauss-Newton method converges if the percentage change in the sum of squared, weighted residuals does not exceed SOSC×100 in three parameter-estimation iterations.
	71-75	F5.0	SOSR	A criteria for using $\underline{R}$ of equation (51) in equation (50a). $\underline{R}$ is used if the percentage change in the sum of squared, weighted residuals does not exceed SOSR×100 in two parameter-estimation iterations.

DATA SET 14 is read only if ISN>0.

14	1 or more	8F10.0	SCL (I), I=1,NP	Factors used to scale parameters for conjugate-direction methods.
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Generally,  $SCL(I) \cong B(I)$  of DATA SET 8. If  $LN(I)>0$  (DATA SET 2), the Parameter-Estimation Package replaces  $SCL(I)$  with  $\ln [SCL(I)]$ , and the transformed value is printed.

Table A2.--Format code (IPRC in DATA SET 13 of the INPUT FILE)  
options for printing the variance-covariance and  
correlation matrices of the parameters

IPRC	FORMAT	IPRC	FORMAT
1	11G10.3	7	20F5.0
2	9G13.6	8	20F5.1
3	15F7.1	9	20F5.2
4	15F7.2	10	20F5.3
5	15F7.3	11	20F5.4
6	15F7.4	12	10G11.4

## Description of Output

### Printing and Checking of the INPUT FILE

The input file is read and then printed on output unit IOUT (IOUT is specified as 6 in the beginning of MAIN, but can be changed if needed). If  $ISN < 0$ , convergence criteria are calculated for the solution of equations (69) or (71), as described in the section "Sensitivity-Equation Method of Calculating Sensitivities" after equation (72), and are printed with the initial parameter values.

### Error Messages

The Parameter-Estimation Package prints error messages to output unit IOUT. These messages indicate errors in the INPUT FILE and problems in program execution, and are followed by the name of the module or submodule (see Appendix C) from which they are printed in parentheses.

Most INPUT FILE errors will stop execution of the program. "FORMAT/DATA MISMATCH" or "END-OF-FILE" errors originate from the computer, and execution stops as soon as the error is detected. A few errors detected by checks within the Parameter-Estimation Package also will stop execution as soon as the error is detected, but for most package-detected errors, the entire INPUT FILE is read and printed before execution stops. Then "EXECUTION TERMINATED DUE TO ERRORS IN PARAMETER-ESTIMATION PACKAGE INPUT FILE--SEARCH ABOVE FOR STOP EXECUTION TO FIND ERROR MESSAGES (SEN10T)" is printed at the end of the output file. Error messages can be located by searching the output file for the words "STOP EXECUTION."

Once the INPUT FILE has been read successfully, execution problems can occur when, for example, a negative hydraulic-conductivity value is calculated, thus activating the option of the Parameter-Estimation Package which writes an error message to IOUT and resets the value to a small, positive number. Most execution problems will not stop the program, but their presence generally indicates that the parameter-estimation problem being considered is not well-conditioned. Check scaled sensitivity-equation sensitivities or the gradient of the objective function scaled by dividing through by the relevant parameter values for parameters that are insensitive to the observed data.

Most error messages are self-explanatory and are not discussed here. However, the following need additional explanation. Underlined items are variables which are specified in the INPUT FILE.

Error message:

HEAD OBS# 4321, ID OAK5 IS DRY -- OMIT (SSEN1U)

Explanation:

The observation is omitted because of conditions represented in figure 11, and the number of observations used to calculate the estimated error variance (ND of eq. 7 and in the text after eq. 17 and 35) is reduced by one. The observation is restored and ND is reset to its original value at the beginning of the next parameter-estimation iteration. SSEN1U is the submodule from which the error message is printed (see Appendix C).

Error Message:

INTERPOLATION FOR HEAD OBS# 4321, ID OAK5 CHANGED BECAUSE AT LEAST ONE NEIGHBORING CELL IS DRY (SSEN1U)

Interpolation is recalculated because at least one of the neighboring cells used in the interpolation (see figs. 6 and 11) is dry. Although the row, column, and layer of the dry cell are not specified in the error message, dry cells are listed elsewhere in the output from a MODFLOW submodule. At the beginning of the next parameter-estimation iteration, the inactive dry cell is reactivated, and the interpolation is reset to its original form.

#### Model-Input Arrays Produced with the Initial Parameter Estimates

For PID = T, KV, TKV, S1, RCH, and ETM, the model-input arrays produced with the initial parameter estimates (DATA SET 8) are printed if IPRNP>0 (LINE 4 of the INPUT FILE) and the associated NLL value(s) (DATA SET 2) are positive. To check that the initial model-input arrays produced by MODFLOWP with the Parameter-Estimation Package (IUNIT (15)≠0) are the same as those read from the Block-Centered Flow, Recharge, and Evapotranspiration input files for a run without the Parameter Estimation Package (IUNIT (15)≠0), set IPRNP equal to IPRN used in those input files. The arrays printed from the two runs need to be identical to four or five significant digits.



Calculated Values and Volumetric Budgets  
for the Entire Model

If IPAR=0 on LINE 6 of the INPUT FILE equals zero, the following arrays are calculated using the parameter values of DATA SET 8, and can be printed, saved on an unformatted file, or both by using the specifications from the Output Control input file (McDonald and Harbaugh, 1988, p. 4-14 to 4-7): hydraulic heads and drawdowns, and, for ISN<0 (LINE 6 of the INPUT FILE), sensitivity-equation sensitivities, or for ISN>0, adjoint states and the derivative of hydraulic head with respect to Newton's iteration parameter. Arrays are printed in the order shown in figure A6. For IPAR=0, the flags of the Output Control input file need to be set such that drawdowns are neither printed nor saved.

[print/save time step : a time step at which Hdpr and Hdsv of Output Control (McDonald and Harbaugh, 1988, p. 4-14) indicate that results are to be printed and (or) saved and for which there is at least one dependent-variable observation. NPER : the total number of time steps.]

---

ISN=-1	ISN=-2	ISN>0
First print/save time step:	Hydraulic heads for all print/save time steps	Hydraulic heads for all print/save time steps
Hydraulic heads		
Sensitivity-equation sensitivities for all parameters	First parameter sensitivity-equation sensitivities for all print/save time steps	Adjoint states for NPER minus the print/save time step numbers
Repeat for all print/save time steps	Repeat for all parameters	

---

Figure A6.--Order of arrays printed, saved, or both when IPAR of the INPUT FILE equals zero.

Volumetric budgets of the entire model (McDonald and Harbaugh, 1988, p. 4-7) are printed with solutions of hydraulic heads, if indicated by the Output Control input file. When PCG2 (Hill, 1990b) is used with MXITER>1, simplified volumetric budgets of the entire model are printed with solutions of sensitivity-equation sensitivities and adjoint states. Only the budgets related to hydraulic heads make obvious physical sense, but the others are included to check solver accuracy. Excessive errors (generally larger than 1 percent) indicate that the solution is inaccurate. Smaller convergence criteria, smaller time steps, or a smaller grid spacing might be needed to resolve the problem. Cumulative budget terms printed for solutions of steady-state hydraulic head and drawdown are very large because the time-step length is set equal to  $1.0 \times 10^{22}$  for steady-state simulations.

#### Plotting Calculated Values

Routines such as those by Leake (1990; U.S. Geological Survey, written commun., 1989) and Harbaugh (1990) have been developed to contour calculated hydraulic heads and drawdowns (Leake, 1990, also plots fluxes) from unformatted files produced by MODFLOW (McDonald and Harbaugh, 1988, p. E-3). In general, these routines or appropriate preprocessors identify the array to be contoured using values of TEXT, ILAY, KSTP, and KPER, which are written just before the array by ULASAV of MODFLOW (McDonald and Harbaugh, 1988, p. 14-9). TEXT is a label (HEAD or DRAWDOWN); ILAY is the layer number; and KSTP and KPER are the time step and stress period of the data, with KSTP measured from the beginning of the stress period.

The contouring routines also can be used to contour calculated hydraulic heads, drawdowns, and sensitivity-equation sensitivities (ISN<0) or adjoint states (ISN<0) produced by the Parameter-Estimation Package (MODFLOWP with IUNIT(15)≠0) with IPAR=0 (heads and drawdowns also can be saved when IPAR<0, and when IPAR>0 if KPRINT=1 in DATA SET 13). The only difference is that when using the Parameter-Estimation Package, KSTP is measured from the beginning of the simulation, with KSTP=0 indicating steady state, and KPER is used as noted on table A3 to indicate what the values represent. For sensitivity-equation sensitivities and adjoint states, TEXT=HEAD.

Table A3.--The use of KSTP and KPER in unformatted files produced by the computer programs MODFLOW and MODFLOWP

[--, plotted quantity indicated not calculated when IUNIT(15)=0]

Plotted quantity	MODFLOW or MODFLOWP with IUNIT(15)=0		MODFLOWP with IUNIT(15)≠0	
	KSTP	KPER	KSTP	KPER
Hydraulic heads Drawdowns Fluxes	Time step since beginning of stress period.	stress period	Time step since begin- ning of simulation. KSTP=0 for steady state.	0
Sensitivity- equation sensitivities.	--	--	.....do.....	Parameter number
Adjoint states	--	--	.....do.....	1

## Nonlinear Regression

Nonlinear regression is performed when IPAR of LINE 6 of the INPUT FILE is greater than zero. At each parameter-estimation iteration, items are printed on output unit IOUT to permit the modeler to monitor the progress of the optimization. For modified Gauss-Newton optimization, these items are the determinant of the scaled least-squares matrix (small values indicate a poorly conditioned parameter-estimation problem), the Marquardt parameter (labeled AMP on the printout; nonzero values indicate a poorly conditioned parameter-estimation problem), the factor used to scale the parameter-change vector ( $\rho_r$  of eq. 50b; labeled AP on the printout), the maximum fractional parameter change calculated using equation (50a) (labeled DMX on the printout; modified Gauss-Newton optimization converges when the absolute value of DMX is less than TOL of DATA SET 13 of the INPUT FILE), and the number of the parameter for which the maximum fractional change occurred (j of eq. 54).

For conjugate-direction optimization, these items are the iteration parameter calculated by Newton's method, the factor used to reduce the iteration parameter (labeled AP on the printout; discussed after eq. 56), the maximum fractional parameter change prior to reduction of the iteration parameter (labeled DMX on the printout), the parameter for which the maximum fractional change occurred, and the absolute value of the component of the gradient vector that has the largest magnitude. Conjugate-direction optimization converges when the last item and the absolute value of the maximum fractional parameter change are less than TOL of DATA SET 13 of the INPUT FILE.

For both optimization methods, the updated parameter estimates are printed at each parameter-estimation iteration and in a table at the end of the simulation (see section "Parameter Values for Restarting Parameter Estimation"). The table is printed whether or not parameter estimation converges and includes some of the items mentioned above and the sum of squared residuals for each iteration. Printing the values together in a table is intended to make it easier for the user to determine how individual parameter values are changing, and whether the changes indicate a problem. If problems occur, see the section "Common Problems." If  $LN(I) \neq 0$ , the value printed for parameter I equals  $e^b$ , where b is the log-transformed value estimated by the parameter-estimation routine, and  $e^b$  equals the mode of the lognormal distribution (see section "Parameterization").

The printing of other items at each parameter-estimation iteration is controlled by IPRINT of DATA SET 13 of the INPUT FILE; see the section "Instructions for the INPUT FILE" for additional information.

The following additional items are printed toward the end of the output file if parameter estimation converges.

- (1) For all optimization methods, tables of information related to the dependent-variable observations and prior parameter estimates are printed, in addition to the final sum of squared weighted residuals, the calculated error variance (defined after eq. 17 and 35),  $R$  (eq. 37), the total number of parameter-estimation iterations, and  $R_N^2$  (eq. 38). The latter three are printed excluding and including prior estimates of the parameters.
- (2) If optimization is accomplished by the modified Gauss-Newton method or if LASTX>0 in DATA SET 13 of the INPUT FILE, the variance-covariance matrix (eq. 35) of the parameters and related statistics are printed, and a table containing the following is printed: The estimated parameter values, the exponential of transformed parameters (zeros are printed for parameters that are not log-transformed), the standard derivations and coefficients of variation of the estimates, and the estimates plus and minus two standard derivations. Equation (36) needs to be used to calculate accurate linear confidence intervals on the parameters, but the estimated values plus or minus two standard deviations provide the user with an estimate of a linear 95-percent confidence interval. Possible inaccuracies in linear confidence intervals in the parameters were mentioned in the section "Analysis of Results for Nonlinear Problems." Eigenvalues and eigenvectors of the variance-covariance matrix scaled with the final parameter values are calculated and printed depending on the value of LPRINT of DATA SET 13.
- (3) If the quasi-Newton method is used and LASTX=0, the final approximate quasi-Newton inverse Hessian matrix is printed.
- (4) Nodal hydraulic heads are printed, saved, or both, depending on the value of KPRINT of DATA SET 13 of the INPUT FILE.

## Parameter Values for Restarting Parameter Estimation

Parameter values from each parameter-estimation iteration are printed on the FORTRAN unit number specified by IOUB of LINE 7 of the INPUT FILE. These parameter values are printed in a format consistent with DATA SET 8 of the INPUT FILE, so they can be used to restart the parameter-estimation routine, as discussed in the section "Restarting the Parameter-Estimation Routine" of Appendix B. File IOUB also is used to print the table of parameter values and other items for each parameter-estimation iteration discussed above.

## Input for the Residual Analysis Program

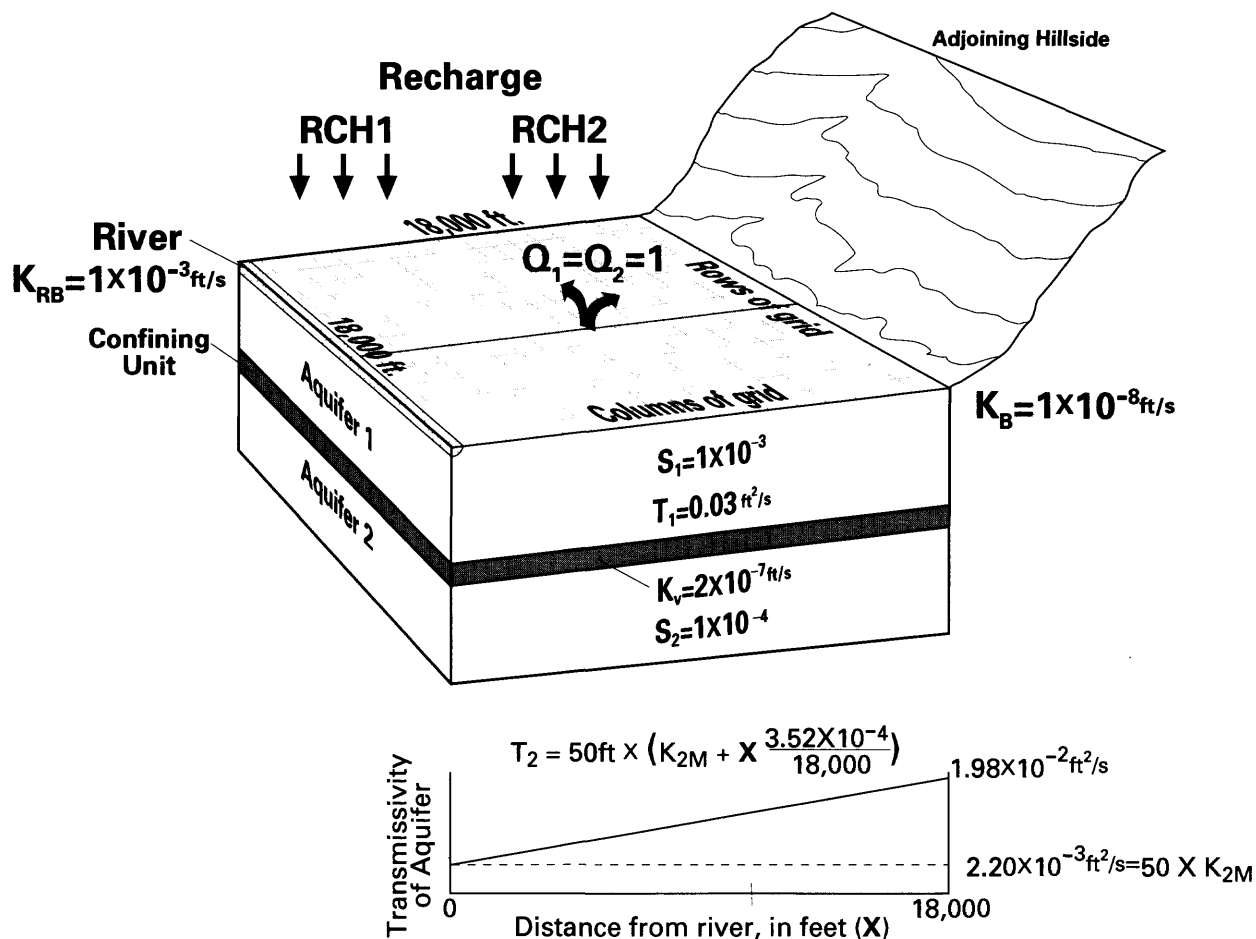
A file that is to be used as input for RESAN.MODP, a slightly modified version of Cooley and Naff's (1990) residual analysis program (see Appendix B), is produced on the FORTRAN unit number specified by IOUR of DATA SET 13 of the INPUT FILE.

## Sample INPUT FILES and Output

Sample INPUT FILES and output for two test cases are presented. The two test cases were presented previously by Cooley (1985), Hill (1989), and Cooley and Naff (1990).

### Test Case 1

The physical system for test case 1 is shown in figure A7. The system is comprised of two confined aquifers separated by a confining unit. The system is affected by head-dependent boundaries at the stream and along the boundary farthest from the stream. The aquifer properties shown in figure A7 are the storage coefficient and transmissivity of aquifer 1 ( $S_1$  and  $T_1$ ), the vertical hydraulic conductivity of the confining unit ( $K_v$ ), the storage coefficient and a multiplicative factor for transmissivity of aquifer 2 ( $S_2$  and  $K_{2M}$ ), and the hydraulic conductivity of the material bounding the aquifers on the side of the physical system farthest from the stream ( $K_B$ ). Storage in the confining unit is assumed to be negligible. Stresses on the system include areal recharge in the area near the stream (RCH1), areal recharge in the area farther from the stream (RCH2), and pumpage from each of the two layers ( $Q_1$  and  $Q_2$ ). The two pumpage rates are equal, so  $Q_1=Q_2$ . The hydraulic conductivity of the riverbed is  $K_{RB}$ .



Riverbed characteristics: width=10 feet; thickness = 10 feet

Figure A7.--Physical system for test case 1, with the true values of all model inputs except RCH1 and RCH2.

For the finite-difference method, the system is discretized into square 1,000-ft by 1,000-ft cells, so that the grid has 18 rows and 18 columns. The river is in column 1. RCH1 applies to cells in columns 1 through 9; RCH2 to cells in columns 10 through 18. The wells are located at the center of the cell at row 9, column 10. The simulation begins from steady-state initial conditions with no pumpage, and a constant rate of pumpage is maintained throughout the simulation. Four stress periods are simulated: the first three are 1, 3, and 6 days long, and each has one time step; the fourth is 272.8 days long, has 9 time steps, and each time-step length is 1.2 times the length of the previous time-step length.

The following nine parameters are estimated:  $Q_1$  and  $Q_2$ ,  $K_1$  ( $T_1 = K_1 \times 50$  ft),  $S_1$ ,  $K_{RB}$ ,  $K_z$  ( $K_v = K_z/10$  ft),  $K_{2M}$  (see graph in figure A7 for calculation of  $T_2$  from  $K_{2M}$ ),  $S_2$ , RCH1, and RCH2. Parameters  $K_1$ ,  $S_1$ ,  $K_{RB}$ ,  $K_z$ , and  $K_{2M}$  and  $S_2$  are log-transformed. The true values of most of these parameters are shown in figure A7; the true values of RCH1 and RCH2 are  $1.0 \times 10^{-8}$  ft/s and  $1.5 \times 10^{-8}$  ft/s (3.78 and 5.76 in/yr), respectively. The true values are known because the test case is synthetic. Hydraulic-head data were produced by using the true parameter values, and then were corrupted by adding two realizations of normally distributed noise. The first realization had a standard deviation of 1.0 ft, and the same value was used to corrupt all hydraulic-head observations at a single location; thus  $\epsilon_1$  errors were imposed. The second realization had a standard deviation of 0.05 ft, and independent values were used to corrupt all hydraulic-head observations; thus  $\epsilon_3$  errors were superimposed. In repetitions of DATA SET 6B, IIT=2, so that initial hydraulic heads and subsequent changes in hydraulic head were used in the regression. Head-dependent boundary gain and loss data also were produced by using the true parameter values, and were corrupted by adding normally distributed noise with a standard deviation equal to 0.10 times the true gain along the stream.

#### INPUT FILE and Input Files from other Packages for Test Case 1

The INPUT FILE used for test case 1 is shown on the following pages. Note that although the presence of nonzero values in DATA SET 10 indicates the use of prior estimates of the parameters, the designation of IPRIOR=0 in DATA SET 13 means that these prior estimates are not used.

#### INPUT FILE

##### TWO-LAYER EXAMPLE - TRANSIENT

9	5	56	4	2	1	1
2	1	1				
32	0	0	1	18	3	0
1	-1	1	0			
40	33	0	0			
1	0	0				
30						
Q	0	-2	1	15	-1	
		1		9		10
		2		9		10
S1	1	-1				
T	1	1				
		50.				

LINE 1
LINE 2
LINE 3
LINE 4
LINE 5
LINE 6
LINE 7
LINE 8
DATA SET 1A
DATA SET 2
DATA SET 2A
DATA SET 2
DATA SET 2
DATA SET 2B



DATA SET 2	
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
90	95
DATA SET 2	
DATA SET 2B	
DATA SET 2	
DATA SET 2	
DATA SET 2B	
DATA SET 2	
DATA SET 2B	
DATA SET 2	
DATA SET 2B	
DATA SET 3	

16	1(9I8)					DATA SET 4			
1	1	1	1	1	1	1	1	1	1
2	2	2	2	2	2	2	2	2	2
1	1	1	1	1	1	1	1	1	2
2	2	2	2	2	2	2	2	2	3
1	1	1	1	1	1	1	1	1	4
2	2	2	2	2	2	2	2	2	5
1	1	1	1	1	1	1	1	1	6
2	2	2	2	2	2	2	2	2	7
1	1	1	1	1	1	1	1	1	8
2	2	2	2	2	2	2	2	2	9
1	1	1	1	1	1	1	1	1	2
2	2	2	2	2	2	2	2	2	11
1	1	1	1	1	1	1	1	1	12
2	2	2	2	2	2	2	2	2	13
1	1	1	1	1	1	1	1	1	14
2	2	2	2	2	2	2	2	2	15
1	1	1	1	1	1	1	1	1	16
2	2	2	2	2	2	2	2	2	17
1	1	1	1	1	1	1	1	1	18
2	2	2	2	2	2	2	2	2	2

	1.0		1.0	0	0	1.0			DATA SET 5
1.0	1	3	1	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
1.0	0	0.00		101.804	1.0025	0.0025	0		DATA SET 6C
1.1	1	0.00		101.775	1.0025	0.0025	0		
1.12	12	0.00		101.675	1.0025	0.0025	0		
2.0	1	4	4	-5	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
2.0	0	0.00		128.117	1.0025	0.0025	0		DATA SET 6C
2.1	1	0.00		128.076	1.0025	0.0025	0		
2.2	2	0.00		127.560	1.0025	0.0025	0		
2.8	8	0.00		116.586	1.0025	0.0025	0		
2.12	12	0.00		113.933	1.0025	0.0025	0		
3.0	1	10	9	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
3.0	0	0.00		156.678	1.0025	0.0025	0		DATA SET 6C
3.1	1	0.00		152.297	1.0025	0.0025	0		
3.12	12	0.00		114.138	1.0025	0.0025	0		
4.0	1	13	4	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
4.0	0	0.00		124.893	1.0025	0.0025	0		DATA SET 6C
4.1	1	0.00		124.826	1.0025	0.0025	0		
4.12	12	0.00		110.589	1.0025	0.0025	0		
5.0	1	14	6	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
5.0	0	0.00		140.961	1.0025	0.0025	0		DATA SET 6C
5.1	1	0.00		140.901	1.0025	0.0025	0		
5.12	12	0.00		119.285	1.0025	0.0025	0		
6.0	2	4	4	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
6.0	0	0.00		126.537	1.0025	0.0025	0		DATA SET 6C
6.1	1	0.00		126.542	1.0025	0.0025	0		
6.12	12	0.00		112.172	1.0025	0.0025	0		
7.0	2	10	1	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
7.0	0	0.00		101.112	1.0025	0.0025	0		DATA SET 6C
7.1	1	0.00		101.160	1.0025	0.0025	0		
7.12	12	0.00		100.544	1.0025	0.0025	0		
8.0	2	10	9	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
8.0	0	0.00		158.135	1.0025	0.0025	0		DATA SET 6C
8.1	1	0.00		152.602	1.0025	0.0025	0		
8.12	12	0.00		114.918	1.0025	0.0025	0		
9.0	2	10	18	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
9.0	0	0.00		176.374	1.0025	0.0025	0		DATA SET 6C
9.1	1	0.00		176.373	1.0025	0.0025	0		
9.12	12	0.00		138.132	1.0025	0.0025	0		
0.0	2	18	6	-3	0.00	0.00	0.00	0.000	0.00 0 DATA SET 6
2									DATA SET 6B
0.0	0	0.00		142.020	1.0025	0.0025	0		DATA SET 6C
0.1	1	0.00		142.007	1.0025	0.0025	0		
0.12	12	0.00		122.099	1.0025	0.0025	0		

										DATA SET 7				
										DATA SET 7B				
SS	3	0	0.0	-4.4	.400000	1								
TR3	3	0.0	-4.1	.380000	1									
TR12	12	0.0	-2.2	.210000	1									
1	1	1	1	1	10.0	100	1000.	90	95	DATA				
1	2	1	1	2	0.0	100	1000.	90	95	SET				
1	3	1	1	3	0.0	100	1000.	90	95	7C				
1	4	1	1	4	0.0	100	1000.	90	95					
1	5	1	1	5	0.0	100	1000.	90	95					
1	6	1	1	6	0.0	100	1000.	90	95					
1	7	1	1	7	0.0	100	1000.	90	95					
1	8	1	1	8	0.0	100	1000.	90	95					
1	9	1	1	9	0.0	100	1000.	90	95					
1	10	1	1	10	0.0	100	1000.	90	95					
1	11	1	1	11	0.0	100	1000.	90	95					
1	12	1	1	12	0.0	100	1000.	90	95					
1	13	1	1	13	0.0	100	1000.	90	95					
1	14	1	1	14	0.0	100	1000.	90	95					
1	15	1	1	15	0.0	100	1000.	90	95					
1	16	1	1	16	0.0	100	1000.	90	95					
1	17	1	1	17	0.0	100	1000.	90	95					
1	18	1	1	18	0.0	100	1000.	90	95					
	-1.1	1.3E-3	3.00E-4	1.2E-3	1.E-7	2.E-4	4.0E-5	2.E-8						
1.0E-8														
2	3	4	5	6	3									
7														
.1	1.0E-4	4.00E-5	1.0E-4	0.	0.									
1.5E-9														
1														
2.0	.08	.010	10	0.	0	0	12	0	0					
DMAX	CSA	TOL	ITMX	FCONV	IOUR	IPRINT	LPRINT	NFIT	SOSR	12				
					IPRIOR	IPRC	KPRINT	LASTX	SOSC					

Input files from other packages used without (labeled "Steady State" and "Transient") and with the Parameter-Estimation Package are shown on the following pages. The true model input values are included in these files.

# Basic Package Input Files

## Without the Parameter-Estimation Package

### Steady-State

#### MODULAR MODEL - TWO-LAYER EXAMPLE PROBLEM

		2				18			18			1			1		
7	8	0	0	0	0	12	31	0	0	0	11	9	0	0	0	0	13
		0				1											
		0				1									-1		
		0				1									-1		
		0.															
		0				200.									-1		
		0				200.									-1		
86400.						1			1								

### Transient

#### MODULAR MODEL - TWO-LAYER EXAMPLE PROBLEM

		2				18			18			4			1		
7	8	0	0	0	0	12	31	0	0	0	11	9	0	0	0	0	13
		0				1											
		0				1									-1		
		0				1									-1		
		0.															
		-13				1.									-1		
		-13				1.									-1		
87162.						1			1.2								
261486.						1			1.2								
522972.						1			1.2								
23567441.						9			1.2								

## With the Parameter-Estimation Package

#### MODULAR MODEL - TWO-LAYER EXAMPLE PROBLEM

		2				18			18			12			1		
7	8	0	0	0	0	12	31	0	0	0	11	9	0	16	0	0	13
		0				1											
		0				1									-1		
		0				1									-1		
		0.															
		0				200.									-1		
		0				200.									-1		
87162.						1			1.2								
261486.						1			1.2								
522972.						1			1.2								
23567441.						9			1.2								

# Output Control Package Input Files

## Steady-State

2	0	19	00
0	1	1	0
0	0	0	0

## Transient

2	0	19	00
0	1	1	0
0	0	0	0
-1	1	1	0
0	1	1	0
0	0	0	0
-1	1	1	0
-1	1	1	0
0	1	1	0
0	0	0	0
-1	1	0	0
-1	1	0	0
0	1	0	0
0	0	0	0
-1	1	0	0
-1	1	0	0
0	1	0	0
0	0	0	0
0	0	0	0

## With the Parameter-Estimation Package

2	0	19	00
0	1	1	0
0	0	0	0
0	1	1	0
0	0	0	0
-1	1	1	0
0	1	1	0
0	0	0	0
-1	1	1	0
-1	1	1	0
0	1	1	0
0	0	0	0
-1	1	0	0
-1	1	0	0
0	1	0	0
0	0	0	0
-1	1	0	0
-1	1	0	0
0	1	0	0
0	0	0	0

.

## Block-Centered Flow Package Input Files

### Steady-State

```
1      0
0 0
0      1.
0     1000.
0     1000.
0     .02000
0    2.00E-08
18    .002200(18F3.0)
```

### Transient and with the Parameter-Estimation Package

```
0      0
0 0
0      1.
0     1000.
0     1000.
0     .00100
0     .02000
0    2.00E-08
0     .000100
18    .002200(18F3.0)
```

### File 18 used by the Block-Centered Flow Package

```
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
1 1 2 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
```

## Recharge Package Input File

### Steady-State

```
1      0
0      0
30     1.E-8(9F8.0)      0
```

	1	0	
	0	0	
	30	1.E-8(9F8.0)	0
-1			
-1			
-1			

	1	0	
	0	0	
	30	1.E-8(9F8.0)	0
-1			
-1			
-1			
-1			

[illegible]



Well Package Input File

Transient

2	0		
2			
1	9	10	-1.0
2	9	10	-1.0

-1  
-1  
-1

With the Parameter-Estimation Package

2	0		
2			
1	9	10	0.0
2	9	10	0.0
2			
1	9	10	-1.0
2	9	10	-1.0

-1  
-1  
-1

General-Head Boundary Package Input File

Steady-state

36	0			
36				
1	1	18	350.	1.0E-07
1	2	18	350.	1.0E-07
1	3	18	350.	1.0E-07
1	4	18	350.	1.0E-07
1	5	18	350.	1.0E-07
1	6	18	350.	1.0E-07
1	7	18	350.	1.0E-07
1	8	18	350.	1.0E-07
1	9	18	350.	1.0E-07
1	10	18	350.	1.0E-07
1	11	18	350.	1.0E-07
1	12	18	350.	1.0E-07
1	13	18	350.	1.0E-07
1	14	18	350.	1.0E-07
1	15	18	350.	1.0E-07
1	16	18	350.	1.0E-07
1	17	18	350.	1.0E-07
1	18	18	350.	1.0E-07
2	1	18	350.	1.0E-07
2	2	18	350.	1.0E-07
2	3	18	350.	1.0E-07
2	4	18	350.	1.0E-07
2	5	18	350.	1.0E-07
2	6	18	350.	1.0E-07

2	7	18	350.	1.0E-07
2	8	18	350.	1.0E-07
2	9	18	350.	1.0E-07
2	10	18	350.	1.0E-07
2	11	18	350.	1.0E-07
2	12	18	350.	1.0E-07
2	13	18	350.	1.0E-07
2	14	18	350.	1.0E-07
2	15	18	350.	1.0E-07
2	16	18	350.	1.0E-07
2	17	18	350.	1.0E-07
2	18	18	350.	1.0E-07

# Transient

36	0			
36				
1	1	18	350.	1.0E-07
1	2	18	350.	1.0E-07
1	3	18	350.	1.0E-07
1	4	18	350.	1.0E-07
1	5	18	350.	1.0E-07
1	6	18	350.	1.0E-07
1	7	18	350.	1.0E-07
1	8	18	350.	1.0E-07
1	9	18	350.	1.0E-07
1	10	18	350.	1.0E-07
1	11	18	350.	1.0E-07
1	12	18	350.	1.0E-07
1	13	18	350.	1.0E-07
1	14	18	350.	1.0E-07
1	15	18	350.	1.0E-07
1	16	18	350.	1.0E-07
1	17	18	350.	1.0E-07
1	18	18	350.	1.0E-07
2	1	18	350.	1.0E-07
2	2	18	350.	1.0E-07
2	3	18	350.	1.0E-07
2	4	18	350.	1.0E-07
2	5	18	350.	1.0E-07
2	6	18	350.	1.0E-07
2	7	18	350.	1.0E-07
2	8	18	350.	1.0E-07
2	9	18	350.	1.0E-07
2	10	18	350.	1.0E-07
2	11	18	350.	1.0E-07
2	12	18	350.	1.0E-07
2	13	18	350.	1.0E-07
2	14	18	350.	1.0E-07
2	15	18	350.	1.0E-07
2	16	18	350.	1.0E-07
2	17	18	350.	1.0E-07
2	18	18	350.	1.0E-07
-1				
-1				
-1				

# With the Parameter-Estimation Package

36	0			
36				
1	1	18	350.	1.0E-07
1	2	18	350.	1.0E-07
1	3	18	350.	1.0E-07
1	4	18	350.	1.0E-07
1	5	18	350.	1.0E-07
1	6	18	350.	1.0E-07
1	7	18	350.	1.0E-07
1	8	18	350.	1.0E-07
1	9	18	350.	1.0E-07
1	10	18	350.	1.0E-07
1	11	18	350.	1.0E-07
1	12	18	350.	1.0E-07
1	13	18	350.	1.0E-07
1	14	18	350.	1.0E-07
1	15	18	350.	1.0E-07
1	16	18	350.	1.0E-07
1	17	18	350.	1.0E-07
1	18	18	350.	1.0E-07
2	1	18	350.	1.0E-07
2	2	18	350.	1.0E-07
2	3	18	350.	1.0E-07
2	4	18	350.	1.0E-07
2	5	18	350.	1.0E-07
2	6	18	350.	1.0E-07
2	7	18	350.	1.0E-07
2	8	18	350.	1.0E-07
2	9	18	350.	1.0E-07
2	10	18	350.	1.0E-07
2	11	18	350.	1.0E-07
2	12	18	350.	1.0E-07
2	13	18	350.	1.0E-07
2	14	18	350.	1.0E-07
2	15	18	350.	1.0E-07
2	16	18	350.	1.0E-07
2	17	18	350.	1.0E-07
2	18	18	350.	1.0E-07
-1				
-1				
-1				
-1				

# Streamflow-Routing Package Input File

## Steady-state

	18		1		0	0	0	0.	0	0
	18		0		0					
1	1	1	1	1		10.0	100	1.00	90	95
1	2	1	1	2		0.0	100	1.00	90	95
1	3	1	1	3		0.0	100	1.00	90	95
1	4	1	1	4		0.0	100	1.00	90	95
1	5	1	1	5		0.0	100	1.00	90	95
1	6	1	1	6		0.0	100	1.00	90	95
1	7	1	1	7		0.0	100	1.00	90	95
1	8	1	1	8		0.0	100	1.00	90	95
1	9	1	1	9		0.0	100	1.00	90	95
1	10	1	1	10		0.0	100	1.00	90	95
1	11	1	1	11		0.0	100	1.00	90	95
1	12	1	1	12		0.0	100	1.00	90	95
1	13	1	1	13		0.0	100	1.00	90	95
1	14	1	1	14		0.0	100	1.00	90	95
1	15	1	1	15		0.0	100	1.00	90	95
1	16	1	1	16		0.0	100	1.00	90	95
1	17	1	1	17		0.0	100	1.00	90	95
1	18	1	1	18		0.0	100	1.00	90	95

## Transient

	18		1		0	0	0	0.	0	0
	18		0		0					
1	1	1	1	1		10.0	100	1.00	90	95
1	2	1	1	2		0.0	100	1.00	90	95
1	3	1	1	3		0.0	100	1.00	90	95
1	4	1	1	4		0.0	100	1.00	90	95
1	5	1	1	5		0.0	100	1.00	90	95
1	6	1	1	6		0.0	100	1.00	90	95
1	7	1	1	7		0.0	100	1.00	90	95
1	8	1	1	8		0.0	100	1.00	90	95
1	9	1	1	9		0.0	100	1.00	90	95
1	10	1	1	10		0.0	100	1.00	90	95
1	11	1	1	11		0.0	100	1.00	90	95
1	12	1	1	12		0.0	100	1.00	90	95
1	13	1	1	13		0.0	100	1.00	90	95
1	14	1	1	14		0.0	100	1.00	90	95
1	15	1	1	15		0.0	100	1.00	90	95
1	16	1	1	16		0.0	100	1.00	90	95
1	17	1	1	17		0.0	100	1.00	90	95
1	18	1	1	18		0.0	100	1.00	90	95
-1										
-1										
-1										

With the Parameter-Estimation Package

	18		1		0		0		0		0.		0		0		0		0
	18		0		0														
1	1	1	1	1			10.0		100		1.00		90		95				
1	2	1	1	2			0.0		100		1.00		90		95				
1	3	1	1	3			0.0		100		1.00		90		95				
1	4	1	1	4			0.0		100		1.00		90		95				
1	5	1	1	5			0.0		100		1.00		90		95				
1	6	1	1	6			0.0		100		1.00		90		95				
1	7	1	1	7			0.0		100		1.00		90		95				
1	8	1	1	8			0.0		100		1.00		90		95				
1	9	1	1	9			0.0		100		1.00		90		95				
1	10	1	1	10			0.0		100		1.00		90		95				
1	11	1	1	11			0.0		100		1.00		90		95				
1	12	1	1	12			0.0		100		1.00		90		95				
1	13	1	1	13			0.0		100		1.00		90		95				
1	14	1	1	14			0.0		100		1.00		90		95				
1	15	1	1	15			0.0		100		1.00		90		95				
1	16	1	1	16			0.0		100		1.00		90		95				
1	17	1	1	17			0.0		100		1.00		90		95				
1	18	1	1	18			0.0		100		1.00		90		95				
	-1																		
	-1																		
	-1																		
	-1																		

PCG2 Package Input File

(not changed when using the Parameter-Estimation Package)

1	50	1																	
.00001	.00001	1.	2	0	2														

### Output for test case 1

The output for test case 1 is shown in the following pages. The following points are noteworthy.

1. In the regression, observed hydraulic heads are used at steady state, and observed drawdowns are used at subsequent time steps. Larger values are used to weight the drawdowns because the subtraction eliminates the  $\epsilon_1$  errors, which are constant over time and larger than the  $\epsilon_3$  errors in this test case.
2. Interpretation of the coefficients of variation (see the "PARAMETER SUMMARY" on the output) can be confusing when there are log-transformed parameters. For example, in test case 1, a naive interpretation of the coefficients of variation would indicate that  $\ln K_z$  (parameter 5) is estimated more precisely than  $\ln K_1$  (parameter 3). However, 95-percent confidence intervals on  $\ln K_z$  and  $\ln K_1$  calculated using equation (36) and then converted into confidence intervals on  $K_{2M}$  and  $K_1$  (the modes of the lognormal distribution) by taking the exponential are  $1.70 \times 10^{-7} < K_{2M} < 2.71 \times 10^{-7}$ , and  $3.69 \times 10^{-4} < K_1 < 4.91 \times 10^{-4}$ . The uncertainty in  $K_{2M}$  and  $K_1$  can be compared by considering the difference between the upper and lower confidence limits divided by the exponential of the estimated values,  $\hat{K}_z = 2.15 \times 10^{-7}$  and  $\hat{K}_1 = 4.26 \times 10^{-4}$ . The resulting value for  $K_z$  is 0.47; the value for  $K_1$  is 0.29. Thus, the coefficients of variation for the log-transformed parameters indicate that  $\ln K_z$  is more precisely known, while the confidence limits indicate that  $K_1$  is known more precisely. In general, if the coefficient of variation is the same for two log-transformed parameters, the confidence interval on the exponential of the parameter will be relatively wider, using the criteria described above, for the log-transformed parameter with an estimated value farther from 1.0.
3. The values printed below each column of the scaled sensitivities equal the square root of the sum of the squared scaled sensitivities in each column, divided by the number of values in the column. These values can be used to compare overall sensitivity of all parameters to the dependent-variable observations. For parameters that are not log-transformed, large values generally correspond to small parameter coefficients of

variation (see the 'PARAMETER SUMMARY' on the output), and small values correspond to large parameter coefficients of variation. In test case 1, this generalization can be tested by listing the parameters as in table A4. The generalization is followed by parameters that are not log-transformed. For parameters that are log-transformed, the square root of the sum of squared, scaled sensitivities divided by ND still indicates overall sensitivity to the parameter, but the coefficients of variation may not (see item 2).

4. The calculated error variance (1.39) printed near the bottom of the output is close to the estimated common error variance (1.0) printed above the observed head data, and the final weighted residuals are nearly independently, normally distributed. The latter is indicated by the fact that the correlation coefficient printed at the bottom of the output equals 0.978, which exceeds the critical values of 0.943 and 0.952 of table 3, and the runs statistic printed after the final table of "Data at Head Locations" indicates neither too few nor too many runs. These characteristics indicate that the weights are assigned appropriately, and there is little bias in the model. A more thorough analysis of the residuals, as described in the text, needs to be pursued to verify this conclusion.

Table A4.--Parameters of test case 1 ranked in order of decreasing (sum of squared, scaled sensitivities)<sup>1/2</sup>/ND and increasing coefficients of variation

Ordered (sum of squared, scaled sensitivities) <sup>1/2</sup> /ND	Related parameter number and parameter identifier	Related parameter number and parameter identifier	Ordered coefficients of variation
260	3(T)*	7(T)*	0.0075
97	7(T)*	5(KV)*	0.0076
47	1(Q)	3(T)*	0.0092
29	2(S1)*	2(S1)*	0.013
12	5(KV)*	6(S1)*	0.068
3.0	6(S1)*	1(Q)	0.072
2.9	9(RCH)	4(KST)*	0.088
1.1	8(RCH)	9(RCH)	0.098
1.0	4(KST)*	8(RCH)	0.11

\*Log-transformed parameters.

# Output for Test Case 1

```

      U.S. GEOLOGICAL SURVEY MODULAR FINITE-DIFFERENCE GROUND-WATER MODEL - MODFLOWP VERSION
MODULAR MODEL - TWO-LAYER EXAMPLE PROBLEM
  2 LAYERS          18 ROWS          18 COLUMNS
  12 STRESS PERIOD(S) IN SIMULATION
MODEL TIME UNIT IS SECONDS
I/O UNITS:
ELEMENT OF IUNIT:  1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
I/O UNIT:  7  8  0  0  0  0 12 31  0  0  0 11  9  0 16  0  0 13  0  0  0  0  0
BAS1 -- BASIC MODEL PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 5
ARRAYS RHS AND BUFF WILL SHARE MEMORY.
START HEAD WILL BE SAVED
  6200 ELEMENTS IN X ARRAY ARE USED BY BAS
  6200 ELEMENTS OF X ARRAY USED OUT OF 900000
BCF1 -- BLOCK-CENTERED FLOW PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 7
TRANSIENT SIMULATION
  LAYER  AQUIFER TYPE
  -----
    1      0
    2      0
  650 ELEMENTS IN X ARRAY ARE USED BY BCF
  6850 ELEMENTS OF X ARRAY USED OUT OF 900000
WELL1 -- WELL PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM 8
MAXIMUM OF 2 WELLS
  8 ELEMENTS IN X ARRAY ARE USED FOR WELLS
  6858 ELEMENTS OF X ARRAY USED OUT OF 900000
RCH1 -- RECHARGE PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 31
OPTION 1 -- RECHARGE TO TOP LAYER
  324 ELEMENTS OF X ARRAY USED FOR RECHARGE
  7182 ELEMENTS OF X ARRAY USED OUT OF 900000
GHB1 -- GHB PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 12
MAXIMUM OF 36 HEAD-DEPENDENT BOUNDARY NODES
  180 ELEMENTS IN X ARRAY ARE USED FOR HEAD-DEPENDENT BOUNDARIES
  7362 ELEMENTS OF X ARRAY USED OUT OF 900000
STRM -- STREAM PACKAGE, VERSION 1, 10/23/87 INPUT READ FROM UNIT 13
MAXIMUM OF 18 STREAM NODES

NUMBER OF STREAM SEGMENTS IS      1
NUMBER OF STREAM TRIBUTARIES IS    0

  290 ELEMENTS IN X ARRAY ARE USED FOR STREAMS
  7652 ELEMENTS OF X ARRAY USED OUT OF 900000
PCG2 -- CONJUGATE GRADIENT SOLUTION PACKAGE, VERSION 2, 5/1/88
MAXIMUM OF 1 CALLS OF SOLUTION ROUTINE
MAXIMUM OF 50 INTERNAL ITERATIONS PER CALL TO SOLUTION ROUTINE
MATRIX PRECONDITIONING TYPE : 1
  2992 ELEMENTS IN X ARRAY ARE USED BY PCG
  10644 ELEMENTS OF X ARRAY USED OUT OF 900000
SEN1 -- SENSITIVITY PACKAGE, VERSION 1, 12/01/91 INPUT READ FROM UNIT 16
TWO-LAYER EXAMPLE - TRANSIENT

NUMBER OF PARAMETERS.....: 9
NUMBER NLL>0 IN ALL DATA SETS 2 FOR PID=T,KV,
  TKV, AND S1, +1 FOR NLL(1)>0 FOR PID=RCH OR ETM...: 5
SUM ALL {NLL(1)} FOR PID=Q,KRB,KDR,KST,GHB,AND CH...: 56
LARGEST NLL VECTOR IN ALL DATA SETS 2.....: 4
LARGEST LZ VECTOR IN ALL DATA SETS 2B.....: 2
NUMBER OF MULTIPLICATION MATRICES IN DATA SET 3....: 1
NUMBER OF ZONE MATRICES IN DATA SET 4.....: 1

PRINT MATRICES PRODUCED BY INIT. PARAM. EST. (>0)...: 2
CHECK CELL REPETITIONS FOR MATRIX PARAMETERS (>0)...: 1
  NUMBER OF CELL REPETITIONS ALLOWED.....: 1

NUMBER OF HEADS.....: 32
  NUMBER OF MULTILAYER HEADS.....: 0
  MAXIMUM NUMBER OF LAYERS FOR MULTILAYER HEADS....: 0
NUMBER OF FLUX CELL GROUPS.....: 1
  NUMBER OF CELLS IN FLUX CELL GROUPS.....: 18
  NUMBER OF FLUXES.....: 3
NUMBER OF PRIORS WITH MULTIPLE PARAMETERS.....: 0

```



HEADS (<0), HEADS AND SENS. (0), OR PAR. EST. (1)...: 1  
 ADJOINT (+) OR SEN. EQ. (-) CALCULATIONS.....: -1  
 (GRADIENT SEARCH (+) OR GAUSS-NEWTON (-) REGRESSION)  
 SCALE PRINTED SENSITIVITIES (>0).....: 1  
 ADJUST GAUSS-NEWTON MATRIX WITH NEWTON UPDATES.....: 0

OUTPUT/INPUT UNIT FOR HEADS OR SENSITIVITIES.....: 40  
 OUTPUT/INPUT UNIT NUMBER FOR INFO FROM ITERATIONS...: 33  
 INPUT UNIT FOR SS/TR IBOUND ARRAYS.....: 0  
 INPUT UNIT FOR KNOWN HEADS AT CONSTANT-HEAD BNDRYS.: 0

NUMBER OF INPUT UNITS IDENTIFIED IN RCH AND EVT....: 1  
 NUMBER OF TIME STEPS>0 AT WHICH HEAD=0.....: 0  
 NUMBER OF USUALLY POS. PARAMETERS THAT MAY BE NEG...: 0

4233 ELEMENTS IN X ARRAY ARE USED FOR SENSITIVITIES  
 14877 ELEMENTS OF X ARRAY USED OUT OF 900000  
 PAR1 -- PARAMETER ESTIMATION PACKAGE, VERSION 1, 12/01/91  
 369 ELEMENTS IN X ARRAY ARE USED FOR PARAMETER ESTIMATION  
 15246 ELEMENTS OF X ARRAY USED OUT OF 900000  
 MODULAR MODEL - TWO-LAYER EXAMPLE PROBLEM

BOUNDARY ARRAY = 1 FOR LAYER 1  
 BOUNDARY ARRAY = 1 FOR LAYER 2  
 AQUIFER HEAD WILL BE SET TO 0.00000 AT ALL NO-FLOW NODES (IBOUND=0).  
 INITIAL HEAD = 200.0000 FOR LAYER 1  
 INITIAL HEAD = 200.0000 FOR LAYER 2  
 HEAD PRINT FORMAT IS FORMAT NUMBER 2 DRAWDOWN PRINT FORMAT IS FORMAT NUMBER 0  
 HEADS WILL BE SAVED ON UNIT 19 DRAWDOWNS WILL BE SAVED ON UNIT 0  
 OUTPUT CONTROL IS SPECIFIED EVERY TIME STEP

COLUMN TO ROW ANISOTROPY = 1.000000  
 DELR = 1000.000  
 DELC = 1000.000  
 PRIMARY STORAGE COEF = 0.9999999E-03 FOR LAYER 1  
 TRANSMIS. ALONG ROWS = 0.2000000E-01 FOR LAYER 1  
 VERT HYD COND /THICKNESS = 0.2000000E-07 FOR LAYER 1  
 PRIMARY STORAGE COEF = 0.1000000E-03 FOR LAYER 2  
 TRANSMIS. ALONG ROWS = 0.2200000E-02 FOR LAYER 2

#### SOLUTION BY THE CONJUGATE-GRADIENT METHOD

MAXIMUM NUMBER OF CALLS TO PCG ROUTINE = 1  
 MAXIMUM ITERATIONS PER CALL TO PCG = 50  
 MATRIX PRECONDITIONING TYPE = 1  
 RELAXATION FACTOR (ONLY USED WITH PRECOND. TYPE 1) = 0.10000E+01  
 PARAMETER OF POLYNOMIAL PRECOND. = 2 (2) OR IS CALCULATED : 2  
 HEAD CHANGE CRITERION FOR CLOSURE = 0.10000E-04  
 RESIDUAL CHANGE CRITERION FOR CLOSURE = 0.10000E-04  
 PCG HEAD AND RESIDUAL CHANGE PRINTOUT INTERVAL = 999  
 PRINTING FROM SOLVER IS LIMITED(1) OR SUPPRESSED (>1) = 2

INPUT UNIT NUMBERS LISTED IN RCH AND EVT PACKAGE INPUT FILES : 30

#### DEFINITION OF TEMPORAL AND SPATIAL EXTENT OF PARAMETERS (PARAMETERIZATION)

PARAMETER NUMBER: 1, PARAMETER IDENTIFIER: Q

LN: 0, VECTOR NLL: -2 1 15 -1  

LAYER	ROW	COLUMN	FACTOR
1.	9.	10.	0.100E+01
2.	9.	10.	0.100E+01

PARAMETER NUMBER: 2, PARAMETER IDENTIFIER: S1

LN: 1, VECTOR NLL: -1 0 0 0

PARAMETER NUMBER: 3, PARAMETER IDENTIFIER: T

LN: 1, VECTOR NLL: 1 0 0 0  
 SFAC= 50.0, MULT. MATRIX 0, ZONE MATRIX 0  
 ZONES = 0 0

PARAMETER NUMBER: 4, PARAMETER IDENTIFIER: KST

LN: 1, VECTOR NLL: 18 0 15 -1  

SEGMENT	REACH	ZERO	FACTOR
1.	1.	0.	0.100E+04
1.	2.	0.	0.100E+04
1.	3.	0.	0.100E+04
1.	4.	0.	0.100E+04

1.	5.	0.	0.100E+04
1.	6.	0.	0.100E+04
1.	7.	0.	0.100E+04
1.	8.	0.	0.100E+04
1.	9.	0.	0.100E+04
1.	10.	0.	0.100E+04
1.	11.	0.	0.100E+04
1.	12.	0.	0.100E+04
1.	13.	0.	0.100E+04
1.	14.	0.	0.100E+04
1.	15.	0.	0.100E+04
1.	16.	0.	0.100E+04
1.	17.	0.	0.100E+04
1.	18.	0.	0.100E+04

PARAMETER NUMBER: 5, PARAMETER IDENTIFIER: KV  
 LN: 1, VECTOR NLL: 1 0 0 0  
 SFAC= 0.100 , MULT. MATRIX 0, ZONE MATRIX 0  
 ZONES = 0 0

PARAMETER NUMBER: 6, PARAMETER IDENTIFIER: S1  
 LN: 1, VECTOR NLL: -2 0 0 0

PARAMETER NUMBER: 7, PARAMETER IDENTIFIER: T  
 LN: 1, VECTOR NLL: 2 0 0 0  
 SFAC= 50.0 , MULT. MATRIX 1, ZONE MATRIX 0  
 ZONES = 0 0

PARAMETER NUMBER: 8, PARAMETER IDENTIFIER: RCH  
 LN: 0, VECTOR NLL: 1 0 15 -1  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 1 0

PARAMETER NUMBER: 9, PARAMETER IDENTIFIER: RCH  
 LN: 0, VECTOR NLL: 1 0 15 -1  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 2 0

MULTIPLICATION MATRIX WILL BE READ ON UNIT 16 USING FORMAT: (18F3.0)

	1	2	3	4	5	6	7	8	9	10
	11	12	13	14	15	16	17	18		
1	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
2	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
3	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
4	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
5	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
6	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
7	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
8	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
9	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
10	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
11	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
12	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
13	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
14	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
15	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
16	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		

17	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		
18	1.000	1.000	2.000	2.000	3.000	3.000	4.000	4.000	5.000	5.000
	6.000	6.000	7.000	7.000	8.000	8.000	9.000	9.000		

-----  
 ZONE MATRIX WILL BE READ ON UNIT 16 USING FORMAT: (918)  
 -----

	1	2	3	4	5	6	7	8	9	10
	11	12	13	14	15	16	17	18		
1	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
2	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
3	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
4	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
5	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
6	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
7	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
8	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
9	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
10	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
11	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
12	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
13	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
14	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
15	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
16	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
17	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	
18	1	1	1	1	1	1	1	1	1	2
	2	2	2	2	2	2	2	2	2	

NSN CAN BE REDUCED FROM 56 TO 20

INPUT ERROR VARIANCES FOR HEADS AND FLOWS: 1.000 1.000  
 INPUT UNIT NUMBERS FOR HEADS AND FLOWS : 0 0  
 ESTIMATED COMMON ERROR VARIANCE : 1.000

# OBSERVED HEAD DATA

OBS#	ID	LAYER	ROW	COLUMN	TIME STEP	ROW/COLUMN/TIME	OFFSETS	OBSERVATION	VARIANCE
TRANSIENT DATA AT THIS LOCATION, ITT = 2									
1	1.0	1	3	1	-3	0.00	0.00	0.00	0.00000
					0			0.00	101.80
1	1.0							0.00	1.0025
2	1.1				1			0.00	-0.29007E-01
3	1.12				12			0.00	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2									
4	2.0	1	4	4	-5	0.00	0.00	0.00	0.00000
					0			0.00	128.12
4	2.0							0.00	1.0025
5	2.1				1			0.00	-0.41016E-01
6	2.2				2			0.00	0.25000E-02
7	2.8				8			0.00	-0.55701
8	2.12				12			0.00	-11.531
TRANSIENT DATA AT THIS LOCATION, ITT = 2									
9	3.0	1	10	9	-3	0.00	0.00	0.00	0.00000
					0			0.00	156.68
9	3.0							0.00	1.0025
10	3.1				1			0.00	-4.3810
11	3.12				12			0.00	0.25000E-02
								0.00	-42.540

TRANSIENT DATA AT THIS LOCATION, ITT = 2										
12	4.0	1	13	4	-3	0.00	0.00	0.00	0.00000	0.00000
12	4.0				0			0.00	124.89	1.0025
13	4.1				1			0.00	-0.67001E-01	0.25000E-02
14	4.12				12			0.00	-14.304	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
15	5.0	1	14	6	-3	0.00	0.00	0.00	0.00000	0.00000
15	5.0				0			0.00	140.96	1.0025
16	5.1				1			0.00	-0.59998E-01	0.25000E-02
17	5.12				12			0.00	-21.676	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
18	6.0	2	4	4	-3	0.00	0.00	0.00	0.00000	0.00000
18	6.0				0			0.00	126.54	1.0025
19	6.1				1			0.00	0.50049E-02	0.25000E-02
20	6.12				12			0.00	-14.365	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
21	7.0	2	10	1	-3	0.00	0.00	0.00	0.00000	0.00000
21	7.0				0			0.00	101.11	1.0025
22	7.1				1			0.00	0.48004E-01	0.25000E-02
23	7.12				12			0.00	-0.56799	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
24	8.0	2	10	9	-3	0.00	0.00	0.00	0.00000	0.00000
24	8.0				0			0.00	158.14	1.0025
25	8.1				1			0.00	-5.5330	0.25000E-02
26	8.12				12			0.00	-43.217	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
27	9.0	2	10	18	-3	0.00	0.00	0.00	0.00000	0.00000
27	9.0				0			0.00	176.37	1.0025
28	9.1				1			0.00	-0.10071E-02	0.25000E-02
29	9.12				12			0.00	-38.242	0.25000E-02
TRANSIENT DATA AT THIS LOCATION, ITT = 2										
30	0.0	2	18	6	-3	0.00	0.00	0.00	0.00000	0.00000
30	0.0				0			0.00	142.02	1.0025
31	0.1				1			0.00	-0.13000E-01	0.25000E-02
32	0.12				12			0.00	-19.921	0.25000E-02

# HEAD-DEPENDENT FLOW DATA

GROUP# 1, BOUNDARY TYPE 3, # OF FLOWS 3, # OF CELLS IN GROUP -18  
OBSERVED STREAMFLOW

OBS#	ID	TIME STEP	AND OFFSET	GAIN(-) OR LOSS(+)	VARIANCE
33	SS	0	0.00	-4.40	0.160
34	TR3	3	0.00	-4.10	0.144
35	TR12	12	0.00	-2.20	0.441E-01

SEGMENT	REACH	FACTOR
1.	1.	1.00
1.	2.	1.00
1.	3.	1.00
1.	4.	1.00
1.	5.	1.00
1.	6.	1.00
1.	7.	1.00
1.	8.	1.00
1.	9.	1.00
1.	10.	1.00
1.	11.	1.00
1.	12.	1.00
1.	13.	1.00
1.	14.	1.00
1.	15.	1.00
1.	16.	1.00
1.	17.	1.00
1.	18.	1.00

## REGRESSION DATA:

MAX. PARAMETER CORRECTION (DMAX) = 2.0000  
 SEARCH DIR. ADJUSTMENT PAR. (CSA) = 0.8000E-01  
 CLOSURE CRITERION (TOL) ----- = 0.1000E-01  
 MAXIMUM NO. OF ITERATIONS (ITMAX) = 10  
 MODIFY CONV. CRITERIA (>0) (FCONV) = 0.00000  
 USE PRIOR PAR EST (>0) (IPRIOR) = 0  
 OUTPUT UNIT FOR RESAN (IOUT) ---- = 0  
 FORMAT CODE FOR COV AND COR (IPRC) = 12  
 PRINT SENS., ETC. (>0) (IPRINT) = 0  
 PRINT LAST HEADS (1) (KPRINT) --- = 0  
 PRINT EIGEN V&V OF COV(>0) (LPRINT) = 0  
 CALC. SEN. W/ LAST PAR (>0) (LASTX) = 0  
 NO. FLETCHER-REEVES ITES (NFIT) = 0  
 SUM OF SQUARES CLOSURE CRIT. (SSC) = 0.00000

## PARAMETER INFORMATION:

(CONVERGENCE CRITERIA LISTED HERE ARE USED TO SOLVE FOR SENSITIVITY-EQUATION SENSITIVITIES)

#	ID	INITIAL VALUE	LN	CONVERGENCE	CRITERIA	GROUP#	WEIGHT OF PRIOR EST.
1	Q	-1.100	0	0.909E-07	0.909E-07	2	
2	S1	0.1300E-02	1	0.769E-04	0.769E-04	3	
3	T	0.3000E-03	1	0.333E-03	0.333E-03	4	
4	KST	0.1200E-02	1	0.533E-04	0.833E-04	5	
5	KV	0.1000E-06	1	1.00	1.00	6	
6	S1	0.2000E-03	1	0.500E-03	0.500E-03	3	
7	T	0.4000E-04	1	0.250E-02	0.250E-02	4	
8	RCH	0.2000E-07	0	5.00	5.00	7	
9	RCH	0.1000E-07	0	10.0	10.0	7	

2 WELLS

LAYER	ROW	COL	STRESS RATE	WELL NO.
1	9	10	0.00000	1
2	9	10	0.00000	2

RECHARGE WILL BE READ ON UNIT 30 USING FORMAT: (9F8.0)

	1 11	2 12	3 13	4 14	5 15	6 16	7 17	8 18	9	10
1	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
2	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
3	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
4	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
5	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
6	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
7	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
8	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
9	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
10	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
11	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
12	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
13	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
14	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
15	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
16	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08
17	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.0000E-08	1.5000E-08
18	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08	1.5000E-08

## 36 HEAD-DEPENDENT BOUNDARY NODES

LAYER	ROW	COL	ELEVATION	CONDUCTANCE	BOUND NO.
1	1	18	350.0	0.1000E-06	1
1	2	18	350.0	0.1000E-06	2
1	3	18	350.0	0.1000E-06	3
1	4	18	350.0	0.1000E-06	4
1	5	18	350.0	0.1000E-06	5
1	6	18	350.0	0.1000E-06	6
1	7	18	350.0	0.1000E-06	7
1	8	18	350.0	0.1000E-06	8
1	9	18	350.0	0.1000E-06	9
1	10	18	350.0	0.1000E-06	10
1	11	18	350.0	0.1000E-06	11
1	12	18	350.0	0.1000E-06	12
1	13	18	350.0	0.1000E-06	13
1	14	18	350.0	0.1000E-06	14
1	15	18	350.0	0.1000E-06	15
1	16	18	350.0	0.1000E-06	16
1	17	18	350.0	0.1000E-06	17
1	18	18	350.0	0.1000E-06	18
2	1	18	350.0	0.1000E-06	19
2	2	18	350.0	0.1000E-06	20
2	3	18	350.0	0.1000E-06	21
2	4	18	350.0	0.1000E-06	22
2	5	18	350.0	0.1000E-06	23
2	6	18	350.0	0.1000E-06	24
2	7	18	350.0	0.1000E-06	25
2	8	18	350.0	0.1000E-06	26
2	9	18	350.0	0.1000E-06	27
2	10	18	350.0	0.1000E-06	28
2	11	18	350.0	0.1000E-06	29
2	12	18	350.0	0.1000E-06	30
2	13	18	350.0	0.1000E-06	31
2	14	18	350.0	0.1000E-06	32
2	15	18	350.0	0.1000E-06	33
2	16	18	350.0	0.1000E-06	34
2	17	18	350.0	0.1000E-06	35
2	18	18	350.0	0.1000E-06	36

## 18 STREAM NODES

LAYER	ROW	COL	SEGMENT NUMBER	REACH NUMBER	STREAMFLOW	STREAM STAGE	STREAMBED CONDUCTANCE	STREAMBED BOT ELEVATION	STREAMBED TOP ELEVATION
1	1	1	1	1	10.00	100.0	1.000	90.00	95.00
1	2	1	1	2	0.0000	100.0	1.000	90.00	95.00
1	3	1	1	3	0.0000	100.0	1.000	90.00	95.00
1	4	1	1	4	0.0000	100.0	1.000	90.00	95.00
1	5	1	1	5	0.0000	100.0	1.000	90.00	95.00
1	6	1	1	6	0.0000	100.0	1.000	90.00	95.00
1	7	1	1	7	0.0000	100.0	1.000	90.00	95.00
1	8	1	1	8	0.0000	100.0	1.000	90.00	95.00
1	9	1	1	9	0.0000	100.0	1.000	90.00	95.00
1	10	1	1	10	0.0000	100.0	1.000	90.00	95.00
1	11	1	1	11	0.0000	100.0	1.000	90.00	95.00
1	12	1	1	12	0.0000	100.0	1.000	90.00	95.00
1	13	1	1	13	0.0000	100.0	1.000	90.00	95.00
1	14	1	1	14	0.0000	100.0	1.000	90.00	95.00
1	15	1	1	15	0.0000	100.0	1.000	90.00	95.00
1	16	1	1	16	0.0000	100.0	1.000	90.00	95.00
1	17	1	1	17	0.0000	100.0	1.000	90.00	95.00
1	18	1	1	18	0.0000	100.0	1.000	90.00	95.00

MODEL INPUT MATRICES CALCULATED WITH INITIAL PARAMETER VALUES

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## 2 WELLS

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REUSING RECH FROM LAST STRESS PERIOD
REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD
REUSING STREAM NODES FROM LAST STRESS PERIOD
REUSING WELLS FROM LAST STRESS PERIOD
REUSING RECH FROM LAST STRESS PERIOD
REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD
REUSING STREAM NODES FROM LAST STRESS PERIOD
REUSING WELLS FROM LAST STRESS PERIOD
REUSING RECH FROM LAST STRESS PERIOD
REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD
REUSING STREAM NODES FROM LAST STRESS PERIOD
REUSING WELLS FROM LAST STRESS PERIOD
REUSING RECH FROM LAST STRESS PERIOD
REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD
REUSING STREAM NODES FROM LAST STRESS PERIOD
REUSING WELLS FROM LAST STRESS PERIOD

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REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD  
 REUSING WELLS FROM LAST STRESS PERIOD  
 REUSING RECH FROM LAST STRESS PERIOD  
 REUSING HEAD-DEPENDENT BOUNDS FROM LAST STRESS PERIOD  
 REUSING STREAM NODES FROM LAST STRESS PERIOD

# DATA AT HEAD LOCATIONS

OBS#	ID	LAYER,ROW,COL	TIME STEP	ROW/COL/TIME OFFSETS	MEAS. HEAD	CALC. HEAD	RESIDUAL	WEIGHT**,5	WEIGHTED RESIDUAL
1	1.0	1 3 1	0	0.00 0.00 0.00	101.804	100.225	1.58	0.999	1.58
2	1.1	1 3 1	1	0.00 0.00 0.00	-0.029	0.000	-0.290E-01	20.0	-0.580
3	1.12	1 3 1	12	0.00 0.00 0.00	-0.129	-0.091	-0.384E-01	20.0	-0.767
4	2.0	1 4 4	0	0.00 0.00 0.00	128.117	139.329	-11.2	0.999	-11.2
5	2.1	1 4 4	1	0.00 0.00 0.00	-0.041	-0.010	-0.315E-01	20.0	-0.630
6	2.2	1 4 4	2	0.00 0.00 0.00	-0.557	-0.276	-0.281	20.0	-5.62
7	2.8	1 4 4	8	0.00 0.00 0.00	-11.531	-12.963	1.43	20.0	28.6
8	2.12	1 4 4	12	0.00 0.00 0.00	-14.184	-18.771	4.59	20.0	91.7
9	3.0	1 10 9	0	0.00 0.00 0.00	156.678	174.360	-17.7	0.999	-17.7
10	3.1	1 10 9	1	0.00 0.00 0.00	-4.381	-3.666	-0.715	20.0	-14.3
11	3.12	1 10 9	12	0.00 0.00 0.00	-42.540	-56.237	13.7	20.0	274.
12	4.0	1 13 4	0	0.00 0.00 0.00	124.893	139.329	-14.4	0.999	-14.4
13	4.1	1 13 4	1	0.00 0.00 0.00	-0.067	-0.016	-0.507E-01	20.0	-1.01
14	4.12	1 13 4	12	0.00 0.00 0.00	-14.304	-18.848	4.54	20.0	90.9
15	5.0	1 14 6	0	0.00 0.00 0.00	140.961	157.130	-16.2	0.999	-16.1
16	5.1	1 14 6	1	0.00 0.00 0.00	-0.060	-0.037	-0.232E-01	20.0	-0.464
17	5.12	1 14 6	12	0.00 0.00 0.00	-21.676	-28.461	6.78	20.0	136.
18	6.0	2 4 4	0	0.00 0.00 0.00	126.537	139.629	-13.1	0.999	-13.1
19	6.1	2 4 4	1	0.00 0.00 0.00	0.005	-0.013	0.175E-01	20.0	0.350
20	6.12	2 4 4	12	0.00 0.00 0.00	-14.365	-19.183	4.82	20.0	96.4
21	7.0	2 10 1	0	0.00 0.00 0.00	101.112	102.851	-1.74	0.999	-1.74
22	7.1	2 10 1	1	0.00 0.00 0.00	0.048	-0.001	0.491E-01	20.0	0.982
23	7.12	2 10 1	12	0.00 0.00 0.00	-0.568	-1.372	0.804	20.0	16.1
24	8.0	2 10 9	0	0.00 0.00 0.00	158.135	173.954	-15.8	0.999	-15.8
25	8.1	2 10 9	1	0.00 0.00 0.00	-5.533	-5.807	0.274	20.0	5.47
26	8.12	2 10 9	12	0.00 0.00 0.00	-43.217	-57.252	14.0	20.0	281.
27	9.0	2 10 18	0	0.00 0.00 0.00	176.374	190.298	-13.9	0.999	-13.9
28	9.1	2 10 18	1	0.00 0.00 0.00	-0.001	-0.050	0.494E-01	20.0	0.989
29	9.12	2 10 18	12	0.00 0.00 0.00	-38.242	-49.510	11.3	20.0	225.
30	0.0	2 18 6	0	0.00 0.00 0.00	142.020	157.039	-15.0	0.999	-15.0
31	0.1	2 18 6	1	0.00 0.00 0.00	-0.013	-0.004	-0.873E-02	20.0	-0.175
32	0.12	2 18 6	12	0.00 0.00 0.00	-19.921	-26.127	6.21	20.0	124.

## STATISTICS FOR THESE RESIDUALS :

MAXIMUM WEIGHTED RESIDUAL : 0.281E+03 OBS# 26  
 MINIMUM WEIGHTED RESIDUAL : -0.177E+02 OBS# 9  
 AVERAGE WEIGHTED RESIDUAL : 0.385E+02  
 # RESIDUALS >= 0. : 15  
 # RESIDUALS < 0. : 17  
 NUMBER OF RUNS : 19 IN 32 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (HEADS) 0.26751E+06

DATA FOR FLOWS

OBS#	ID	TIME STEP	MEAS. FLOW	CALC. FLOW	RESIDUAL	WEIGHT**5	WEIGHTED RESIDUAL
33	SS	0	-4.40	-4.86	0.460	2.50	1.15
34	TR3	3	-4.10	-4.72	0.618	2.63	1.63
35	TR12	12	-2.20	-2.86	0.663	4.76	3.16

STATISTICS FOR THESE RESIDUALS :

MAXIMUM WEIGHTED RESIDUAL :-0.115E+01 OBS# 33  
 MINIMUM WEIGHTED RESIDUAL :-0.316E+01 OBS# 35  
 AVERAGE WEIGHTED RESIDUAL :-0.198E+01  
 # RESIDUALS >= 0. : 0  
 # RESIDUALS < 0. : 3  
 NUMBER OF RUNS : 19 IN 35 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 0.26752E+06

STATISTICS FOR ALL RESIDUALS :

AVERAGE WEIGHTED RESIDUAL :-0.353E+02

# RESIDUALS >= 0. : 17

# RESIDUALS < 0. : 18

NUMBER OF RUNS : 19 IN 35 OBSERVATIONS

RUNS STATISTIC (TOO FEW RUNS): 0.348

(IF #NEG>10 AND #POS>10, P(STAT < -1.28) = 0.10,  
 P(STAT < -1.645) = 0.05,  
 P(STAT < -1.96) = 0.025)

RUNS STATISTIC (TOO MANY RUNS): 0.491E-02

(IF #NEG>10 AND #POS>10, P(STAT > 1.28) = 0.10,  
 P(STAT > 1.645) = 0.05,  
 P(STAT > 1.96) = 0.025)

SCALED SENSITIVITIES (SCALED BY B\*(WT\*\*5))

PARAMETER # :	1	2	3	4	5	6	7	8	9
PARAMETER ID :	Q	S1	T	KST	KV	S1	T	RCH	RCH
OBS# & ID									
1 1.0	0.000	0.000	-0.902E-04	1.51	-0.712E-06	0.000	-0.392E-04	0.150	0.749E-01
2 1.1	-0.262E-03	-0.573E-02	0.608E-02	-0.204E-02	-0.903E-03	-0.198E-02	0.404E-02	0.000	0.000
3 1.12	-1.81	-2.22	2.30	-12.2	0.198E-01	-0.439	1.02	0.000	0.000
4 2.0	0.000	0.000	270.	1.51	4.58	0.000	55.4	24.0	15.3
5 2.1	-0.190	-3.31	2.15	-0.237E-03	0.489	-1.11	2.08	0.000	0.000
6 2.2	-5.52	-66.5	33.1	-0.275E-01	-2.57	-15.5	24.2	0.000	0.512E-04
7 2.8	-259.	-784.	-930.	-6.44	-8.78	-155.	-70.7	0.102E-03	0.512E-04
8 2.12	-375.	-447.	-0.210E+04	-11.4	-22.9	-88.2	-362.	0.102E-03	0.512E-04
9 3.0	0.000	0.000	470.	1.51	7.95	0.000	159.	38.3	35.9
10 3.1	-73.3	-394.	-14.9	0.401E-05	112.	-83.7	-94.5	0.102E-03	0.000
11 3.12	-0.112E+04	-975.	-0.569E+04	-10.1	70.7	-192.	-0.260E+04	0.307E-03	0.307E-03
12 4.0	0.000	0.000	270.	1.51	4.58	0.000	55.4	24.0	15.3
13 4.1	-0.325	-5.29	3.33	-0.329E-03	0.690	-1.74	3.11	0.000	0.000
14 4.12	-377.	-447.	-0.211E+04	-11.2	-21.3	-88.2	-370.	0.102E-03	0.512E-04
15 5.0	0.000	0.000	377.	1.51	6.35	0.000	101.	32.9	24.1
16 5.1	-0.736	-10.5	5.94	-0.321E-04	-1.24	-3.55	6.19	0.000	0.000
17 5.12	-569.	-690.	-0.302E+04	-10.6	-28.0	-136.	-745.	0.205E-03	0.205E-03
18 6.0	0.000	0.000	271.	1.51	10.2	0.000	54.2	24.0	15.6
19 6.1	-0.249	-3.60	2.14	-0.245E-03	-1.95	-1.84	3.71	0.000	0.000
20 6.12	-384.	-456.	-0.213E+04	-11.3	-165.	-90.6	-306.	0.205E-03	0.102E-03
21 7.0	0.000	0.000	18.9	1.51	38.4	0.000	-21.1	1.81	1.04
22 7.1	-0.227E-01	-0.345	0.229	-0.892E-02	0.368	-0.192	0.482	0.000	0.000
23 7.12	-27.4	-30.7	-148.	-13.2	-378.	-6.15	218.	0.640E-05	0.320E-05
24 8.0	0.000	0.000	467.	1.51	2.15	0.000	162.	37.8	36.1
25 8.1	-116.	-275.	-73.3	0.000	-456.	-238.	-94.9	0.102E-03	0.000
26 8.12	-0.115E+04	-975.	-0.544E+04	-10.1	-283.	-194.	-0.289E+04	0.307E-03	0.205E-03
27 9.0	0.000	0.000	540.	1.51	0.938	0.000	236.	38.1	52.1
28 9.1	-1.01	-9.93	3.70	0.120E-04	-11.8	-6.73	15.7	0.102E-03	0.000
29 9.12	-990.	-0.132E+04	-0.456E+04	-9.24	-76.5	-262.	-0.195E+04	0.410E-03	0.410E-03
30 0.0	0.000	0.000	375.	1.51	5.33	0.000	103.	32.6	24.4
31 0.1	-0.858E-01	-1.44	0.858	-0.160E-04	0.914	-0.763	1.74	0.000	0.000
32 0.12	-523.	-695.	-0.276E+04	-10.4	-128.	-138.	-528.	0.205E-03	0.102E-03
33 SS	0.000	0.000	0.488E-02	0.135E-04	0.417E-04	0.000	0.211E-02	-8.10	-4.05
34 TR3	0.375	3.25	-3.62	-0.161E-01	0.592E-02	0.709	-1.26	-8.53	-4.26
35 TR12	9.51	11.4	-12.1	-0.311E-01	0.180	2.26	-4.83	-15.4	-7.71

((SUM OF THE SQUARED VALUES)\*\*5)/ND

0.617E+02 0.703E+02 0.306E+03 0.102E+01 0.202E+02 0.154E+02 0.129E+03 0.265E+01 0.244E+01

UNSCALED RIGHT-HAND SIDE VECTOR (= -0.5\*GRADIENT)  
 0.10071E+07 0.17486E+06 0.68179E+06 2097.1 7937.7 27104. 0.22105E+06 -.19133E+12 -.33156E+12

ITERATION NO. = 1  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.60737E-09  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.85868  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 5

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0009	0.12205E-02	0.39340E-03	0.20973E-03	0.18587E-06	0.87396E-04	0.42774E-04	0.12443E-07	0.13861E-07

ITERATION NO. = 2  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.86775E-09  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 1.4328  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 4

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0594	0.11481E-02	0.42276E-03	0.51023E-03	0.21470E-06	0.54922E-04	0.47328E-04	0.11028E-07	0.15692E-07

ITERATION NO. = 3  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.11453E-08  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.88538  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 4

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0736	0.11373E-02	0.42541E-03	0.96197E-03	0.21483E-06	0.63302E-04	0.48216E-04	0.10828E-07	0.15995E-07

ITERATION NO. = 4  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.12056E-08  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.33946  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 4

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0742	0.11371E-02	0.42563E-03	0.12885E-02	0.21508E-06	0.63091E-04	0.48228E-04	0.10821E-07	0.16009E-07

ITERATION NO. = 5  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.12128E-08  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.54045E-01  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 4

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0742	0.11370E-02	0.42566E-03	0.13582E-02	0.21507E-06	0.63170E-04	0.48232E-04	0.10820E-07	0.16011E-07

ITERATION NO. = 6  
 VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :  
 DET OF SCALED LEAST-SQUARES MATRIX = 0.24034E-07  
 MARQUARDT PARAMETER (AMP)----- = 0.10000E-02  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.17538E-02  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 4

UPDATED ESTIMATES OF REGRESSION PARAMETERS :  

Q	S1	T	KST	KV	S1	T	RCH	RCH
-1.0742	0.11370E-02	0.42565E-03	0.13605E-02	0.21506E-06	0.63185E-04	0.48232E-04	0.10819E-07	0.16011E-07

PARAMETER ESTIMATION CONVERGED BY SATISFYING TOL CRITERIA

# DATA AT HEAD LOCATIONS

OBS#	ID	LAYER,ROW,COL	TIME STEP	ROW/COL/TIME OFFSETS	MEAS. HEAD	CALC. HEAD	RESIDUAL	WEIGHT**.5	WEIGHTED RESIDUAL
1	1.0	1 3 1	0	0.00 0.00 0.00	101.804	100.178	1.63	0.999	1.62
2	1.1	1 3 1	1	0.00 0.00 0.00	-0.029	0.000	-0.289E-01	20.0	-0.578
3	1.12	1 3 1	12	0.00 0.00 0.00	-0.129	-0.084	-0.450E-01	20.0	-0.900
4	2.0	1 4 4	0	0.00 0.00 0.00	128.117	126.993	1.12	0.999	1.12
5	2.1	1 4 4	1	0.00 0.00 0.00	-0.041	-0.034	-0.728E-02	20.0	-0.146
6	2.2	1 4 4	2	0.00 0.00 0.00	-0.557	-0.544	-0.131E-01	20.0	-0.261
7	2.8	1 4 4	8	0.00 0.00 0.00	-11.531	-11.554	0.233E-01	20.0	0.466
8	2.12	1 4 4	12	0.00 0.00 0.00	-14.184	-14.192	0.845E-02	20.0	0.169
9	3.0	1 10 9	0	0.00 0.00 0.00	156.678	157.131	-0.453	0.999	-0.452
10	3.1	1 10 9	1	0.00 0.00 0.00	-4.381	-4.319	-0.620E-01	20.0	-1.24
11	3.12	1 10 9	12	0.00 0.00 0.00	-42.540	-42.593	0.530E-01	20.0	1.06
12	4.0	1 13 4	0	0.00 0.00 0.00	124.893	126.993	-2.10	0.999	-2.10
13	4.1	1 13 4	1	0.00 0.00 0.00	-0.067	-0.051	-0.155E-01	20.0	-0.310
14	4.12	1 13 4	12	0.00 0.00 0.00	-14.304	-14.251	-0.530E-01	20.0	-1.06
15	5.0	1 14 6	0	0.00 0.00 0.00	140.961	140.914	0.471E-01	0.999	0.471E-01
16	5.1	1 14 6	1	0.00 0.00 0.00	-0.060	-0.099	0.387E-01	20.0	0.773
17	5.12	1 14 6	12	0.00 0.00 0.00	-21.676	-21.657	-0.185E-01	20.0	-0.370
18	6.0	2 4 4	0	0.00 0.00 0.00	126.537	127.204	-0.667	0.999	-0.666
19	6.1	2 4 4	1	0.00 0.00 0.00	0.005	-0.038	0.433E-01	20.0	0.867
20	6.12	2 4 4	12	0.00 0.00 0.00	-14.365	-14.367	0.233E-02	20.0	0.467E-01
21	7.0	2 10 1	0	0.00 0.00 0.00	101.112	101.200	-0.876E-01	0.999	-0.875E-01
22	7.1	2 10 1	1	0.00 0.00 0.00	0.048	-0.003	0.508E-01	20.0	1.02
23	7.12	2 10 1	12	0.00 0.00 0.00	-0.568	-0.648	0.799E-01	20.0	1.60
24	8.0	2 10 9	0	0.00 0.00 0.00	158.135	157.114	1.02	0.999	1.02
25	8.1	2 10 9	1	0.00 0.00 0.00	-5.533	-5.535	0.153E-02	20.0	0.305E-01
26	8.12	2 10 9	12	0.00 0.00 0.00	-43.217	-43.108	-0.109	20.0	-2.18
27	9.0	2 10 18	0	0.00 0.00 0.00	176.374	176.750	-0.376	0.999	-0.376
28	9.1	2 10 18	1	0.00 0.00 0.00	-0.001	-0.100	0.993E-01	20.0	1.99
29	9.12	2 10 18	12	0.00 0.00 0.00	-38.242	-38.355	0.113	20.0	2.25
30	0.0	2 18 6	0	0.00 0.00 0.00	142.020	141.022	0.998	0.999	0.997
31	0.1	2 18 6	1	0.00 0.00 0.00	-0.013	-0.017	0.378E-02	20.0	0.757E-01
32	0.12	2 18 6	12	0.00 0.00 0.00	-19.921	-19.876	-0.447E-01	20.0	-0.894

## STATISTICS FOR THESE RESIDUALS :

MAXIMUM WEIGHTED RESIDUAL : 0.225E+01 OBS# 29  
 MINIMUM WEIGHTED RESIDUAL :-0.218E+01 OBS# 26  
 AVERAGE WEIGHTED RESIDUAL : 0.110E+00  
 # RESIDUALS >= 0. : 17  
 # RESIDUALS < 0. : 15  
 NUMBER OF RUNS : 16 IN 32 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (HEADS) 36.127

## DATA FOR FLOWS

OBS#	ID	TIME STEP	MEAS. FLOW	CALC. FLOW	RESIDUAL	WEIGHT**.5	WEIGHTED RESIDUAL
33	SS	0	-4.40	-4.35	-0.528E-01	2.50	-0.132
34	TR3	3	-4.10	-4.06	-0.417E-01	2.63	-0.110
35	TR12	12	-2.20	-2.25	0.495E-01	4.76	0.236

## STATISTICS FOR THESE RESIDUALS :

MAXIMUM WEIGHTED RESIDUAL : 0.236E+00 OBS# 35  
 MINIMUM WEIGHTED RESIDUAL :-0.132E+00 OBS# 33  
 AVERAGE WEIGHTED RESIDUAL :-0.199E-02  
 # RESIDUALS >= 0. : 1  
 # RESIDUALS < 0. : 2  
 NUMBER OF RUNS : 17 IN 35 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 36.220

STATISTICS FOR ALL RESIDUALS :

AVERAGE WEIGHTED RESIDUAL :-0.100E+00

# RESIDUALS >= 0. : 17

# RESIDUALS < 0. : 18

NUMBER OF RUNS : 17 IN 35 OBSERVATIONS

RUNS STATISTIC (TOO FEW RUNS): -0.339

(IF #NEG>10 AND #POS>10, P(STAT < -1.28) = 0.10,

P(STAT < -1.645) = 0.05,

P(STAT < -1.96) = 0.025)

RUNS STATISTIC (TOO MANY RUNS): -0.682

(IF #NEG>10 AND #POS>10, P(STAT > 1.28) = 0.10,

P(STAT > 1.645) = 0.05,

P(STAT > 1.96) = 0.025)

SCALED SENSITIVITIES (SCALED BY B\*(WT\*\*.5))

PARAMETER # :	1	2	3	4	5	6	7	8	9
PARAMETER ID :	Q	S1	T	KST	KV	S1	T	RCH	RCH
OBS# & ID									
1 1.0	0.000	0.000	-0.652E-04	1.17	-0.186E-06	0.000	-0.289E-04	0.716E-01	0.106
2 1.1	-0.171E-02	-0.360E-01	0.334E-01	-0.119E-01	-0.340E-02	-0.386E-02	0.159E-01	-0.216E-06	-0.320E-06
3 1.12	-1.68	-0.812	0.718	-11.1	-0.167E-02	-0.643E-01	0.341	0.000	-0.320E-06
4 2.0	0.000	0.000	180.	1.17	1.34	0.000	34.5	9.34	17.6
5 2.1	-0.674	-11.5	6.12	-0.211E-02	-1.06	-1.21	4.32	0.277E-04	0.000
6 2.2	-10.9	-118.	39.5	-0.108	-2.88	-10.2	26.5	0.554E-04	0.820E-04
7 2.8	-231.	-520.	-0.105E+04	-7.79	-5.95	-41.3	-128.	0.554E-04	0.164E-03
8 2.12	-284.	-133.	-0.177E+04	-11.0	-10.5	-10.6	-322.	0.554E-04	0.820E-04
9 3.0	0.000	0.000	351.	1.17	2.47	0.000	115.	15.0	42.0
10 3.1	-86.4	-407.	-104.	-0.122E-03	58.5	-36.6	-129.	0.000	0.164E-03
11 3.12	-852.	-295.	-0.474E+04	-10.6	42.6	-23.3	-0.195E+04	0.111E-03	0.164E-03
12 4.0	0.000	0.000	180.	1.17	1.34	0.000	34.5	9.34	17.6
13 4.1	-1.03	-16.2	8.22	-0.271E-02	-1.42	-1.70	5.71	0.277E-04	0.000
14 4.12	-285.	-133.	-0.178E+04	-10.9	-9.85	-10.6	-327.	0.554E-04	0.820E-04
15 5.0	0.000	0.000	263.	1.17	1.76	0.000	66.2	12.9	28.0
16 5.1	-1.97	-27.8	12.5	-0.523E-03	-2.46	-2.94	9.74	0.000	0.000
17 5.12	-433.	-207.	-0.260E+04	-10.7	-13.1	-16.4	-625.	0.554E-04	0.000
18 6.0	0.000	0.000	181.	1.17	4.89	0.000	33.3	9.33	17.8
19 6.1	-0.767	-12.4	6.30	-0.223E-02	-2.89	-1.59	5.94	0.277E-04	0.000
20 6.12	-287.	-135.	-0.179E+04	-11.0	-67.8	-10.7	-298.	0.554E-04	0.000
21 7.0	0.000	0.000	7.13	1.17	14.8	0.000	-8.56	0.451	0.747
22 7.1	-0.545E-01	-0.861	0.496	-0.447E-01	-0.791	-0.122	0.790	0.000	-0.256E-05
23 7.12	-13.0	-5.73	-71.4	-12.1	-162.	-0.456	94.4	0.000	-0.256E-05
24 8.0	0.000	0.000	350.	1.17	2.01	0.000	116.	14.9	42.1
25 8.1	-111.	-356.	-141.	-0.142E-03	-329.	-66.9	-116.	0.000	0.000
26 8.12	-862.	-295.	-0.465E+04	-10.6	-158.	-23.4	-0.203E+04	0.111E-03	0.164E-03
27 9.0	0.000	0.000	441.	1.17	-0.968	0.000	196.	15.0	61.7
28 9.1	-2.01	-26.7	9.33	0.118E-04	-12.2	-3.87	19.2	0.000	0.164E-03
29 9.12	-767.	-404.	-0.417E+04	-10.3	-33.7	-32.0	-0.162E+04	0.111E-03	0.164E-03
30 0.0	0.000	0.000	263.	1.17	3.57	0.000	65.9	12.8	28.2
31 0.1	-0.334	-6.50	3.48	-0.244E-03	-1.64	-0.833	3.67	0.000	0.000
32 0.12	-398.	-208.	-0.241E+04	-10.5	-54.7	-16.5	-492.	0.554E-04	0.000
33 SS	0.000	0.000	0.399E-02	0.109E-04	0.122E-04	0.000	0.177E-02	-4.38	-6.48
34 TR3	0.759	5.70	-5.61	-0.279E-01	0.268E-01	0.473	-1.62	-4.61	-6.83
35 TR12	9.99	4.73	-4.40	-0.131E-01	-0.331E-01	0.374	-1.63	-8.35	-12.4

((SUM OF THE SQUARED VALUES)\*\*.5)/ND

0.471E+02 0.293E+02 0.264E+03 0.101E+01 0.119E+02 0.295E+01 0.974E+02 0.106E+01 0.287E+01

# PARAMETER VALUES AND STATISTICS FOR ALL ITERATIONS

PAR. ID.:												
ITER	Q	S1	T	KST	KV	S1	SUM OF SQUARED HEADS	WEIGHTED W/FLOWS	RESIDUALS W/PARAMS	DMX	PAR#	AMP OR AGMX
	T	RCH	RCH									
	-0.110E+01	0.130E-02	0.300E-03	0.120E-02	0.100E-06	0.200E-03						
	0.400E-04	0.200E-07	0.100E-07									
1	-0.100E+01	0.122E-02	0.393E-03	0.210E-03	0.186E-06	0.874E-04	0.268E+06	0.268E+06	0.268E+06	0.859	5	0.000
	0.428E-04	0.124E-07	0.139E-07									
2	-0.106E+01	0.115E-02	0.423E-03	0.510E-03	0.215E-06	0.549E-04	0.113E+04	0.113E+04	0.113E+04	1.43	4	0.000
	0.473E-04	0.110E-07	0.157E-07									
3	-0.107E+01	0.114E-02	0.425E-03	0.962E-03	0.215E-06	0.633E-04	62.7	62.8	62.8	0.885	4	0.000
	0.482E-04	0.108E-07	0.160E-07									
4	-0.107E+01	0.114E-02	0.426E-03	0.129E-02	0.215E-06	0.631E-04	40.3	40.4	40.4	0.339	4	0.000
	0.482E-04	0.108E-07	0.160E-07									
5	-0.107E+01	0.114E-02	0.426E-03	0.136E-02	0.215E-06	0.632E-04	36.2	36.3	36.3	0.540E-01	4	0.000
	0.482E-04	0.108E-07	0.160E-07									
6	-0.107E+01	0.114E-02	0.426E-03	0.136E-02	0.215E-06	0.632E-04	36.1	36.2	36.2	0.175E-02	4	0.100E-02
	0.482E-04	0.108E-07	0.160E-07									
7							36.1	36.2	36.2			

## COVARIANCE MAT.

	1	2	3	4	5	6	7	8	9
1	5.9319E-03	-5.5862E-03	-5.5080E-03	-5.3527E-03	-5.5753E-03	-4.8110E-03	-5.5623E-03	-1.3943E-11	-1.0984E-10
2	-5.5862E-03	7.4539E-03	5.1664E-03	-5.5827E-03	8.5119E-03	-2.5022E-02	5.2008E-03	1.2420E-11	1.0267E-10
3	-5.5080E-03	5.1664E-03	5.1564E-03	2.2975E-03	5.2591E-03	4.4799E-03	5.0570E-03	1.3355E-11	1.0182E-10
4	-5.3527E-03	-5.5827E-03	2.2975E-03	0.3361	-2.0936E-02	0.1599	1.1507E-02	7.6163E-12	1.0854E-10
5	-5.5753E-03	8.5119E-03	5.2591E-03	-2.0936E-02	1.3486E-02	-4.5061E-02	4.9276E-03	1.3502E-11	1.0156E-10
6	-4.8110E-03	-2.5022E-02	4.4799E-03	0.1599	-4.5061E-02	0.4300	5.4141E-03	1.7087E-11	9.9397E-11
7	-5.5623E-03	5.2008E-03	5.0570E-03	1.1507E-02	4.9276E-03	5.4141E-03	5.5212E-03	1.1806E-11	1.0366E-10
8	-1.3943E-11	1.2420E-11	1.3355E-11	7.6163E-12	1.3502E-11	1.7087E-11	1.1806E-11	1.4337E-18	-4.7146E-19
9	-1.0984E-10	1.0267E-10	1.0182E-10	1.0854E-10	1.0156E-10	9.9397E-11	1.0366E-10	-4.7146E-19	2.4504E-18

## PARAMETER SUMMARY

PARAMETER # :	1	2	3	4	5	6	7	8	9
PARAMETER ID :	Q	S1	T	KST	KV	S1	T	RCH	RCH
FINAL VALUES									
	-0.107E+01	-0.678E+01	-0.776E+01	-0.660E+01	-0.154E+02	-0.967E+01	-0.994E+01	0.108E-07	0.160E-07
EXPONENTIAL OF LN PARAMETERS									
(0.0 FOR UNTRANSFORMED PARAMETERS)									
	0.000E+00	0.114E-02	0.426E-03	0.136E-02	0.215E-06	0.632E-04	0.482E-04	0.000E+00	0.000E+00
STD. DEV.									
	0.770E-01	0.863E-01	0.718E-01	0.580E+00	0.116E+00	0.656E+00	0.743E-01	0.120E-08	0.157E-08
COEF. OF VAR.									
	0.717E-01	0.127E-01	0.925E-02	0.878E-01	0.756E-02	0.678E-01	0.748E-02	0.111E+00	0.978E-01
+ 2 STD. DEV.									
	-0.920E+00	-0.661E+01	-0.762E+01	-0.544E+01	-0.151E+02	-0.836E+01	-0.979E+01	0.132E-07	0.191E-07
EXPONENTIAL OF LN PARAMETERS									
(0.0 FOR UNTRANSFORMED PARAMETERS)									
	0.000E+00	0.135E-02	0.491E-03	0.434E-02	0.271E-06	0.235E-03	0.560E-04	0.000E+00	0.000E+00
- 2 STD. DEV.									
	-0.123E+01	-0.695E+01	-0.791E+01	-0.776E+01	-0.156E+02	-0.110E+02	-0.101E+02	0.842E-08	0.129E-07
EXPONENTIAL OF LN PARAMETERS									
(0.0 FOR UNTRANSFORMED PARAMETERS)									
	0.000E+00	0.957E-03	0.369E-03	0.427E-03	0.170E-06	0.170E-04	0.416E-04	0.000E+00	0.000E+00

CORRELATION MAT.

	1	2	3	4	5	6	7	8	9
1	1.000	-0.8401	-0.9959	-0.1199	-0.6233	-9.5264E-02	-0.9719	-0.1512	-0.9111
2	-0.8401	1.000	0.8333	-0.1115	0.8490	-0.4420	0.8107	0.1201	0.7597
3	-0.9959	0.8333	1.000	5.5186E-02	0.6307	9.5145E-02	0.9478	0.1553	0.9058
4	-0.1199	-0.1115	5.5186E-02	1.000	-0.3110	0.4207	0.2671	1.0972E-02	0.1196
5	-0.6233	0.8490	0.6307	-0.3110	1.000	-0.5918	0.5711	9.7099E-02	0.5587
6	-9.5264E-02	-0.4420	9.5145E-02	0.4207	-0.5918	1.000	0.1111	2.1763E-02	9.6838E-02
7	-0.9719	0.8107	0.9478	0.2671	0.5711	0.1111	1.000	0.1327	0.8912
8	-0.1512	0.1201	0.1553	1.0972E-02	9.7099E-02	2.1763E-02	0.1327	1.000	-0.2515
9	-0.9111	0.7597	0.9058	0.1196	0.5587	9.6838E-02	0.8912	-0.2515	1.000

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS >= .95

PARAMETER #	ID	#	ID	CORRELATION
1	Q	3	T	-1.00
1	Q	7	T	-0.97

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS BETWEEN .90 AND .95

PARAMETER #	ID	#	ID	CORRELATION
1	Q	9	RCH	-0.91
3	T	7	T	0.95
3	T	9	RCH	0.91

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS BETWEEN .85 AND .90

PARAMETER #	ID	#	ID	CORRELATION
7	T	9	RCH	0.89

RSQ (DEP.VAR. ONLY)----- = 36.220  
 RSQ (W/PARAMETERS)----- = 36.220  
 CALCULATED ERROR VARIANCE = 1.3931  
 CORRELATION COEFFICIENT-- = 0.99999  
 W/PARAMETERS----- = 0.99999  
 ITERATIONS----- = 6

MAX LIKE OBJ FUNC = -38.131  
 AIC STATISTIC---- = -20.131  
 BIC STATISTIC---- = -6.1326

ORDERED DEPENDENT-VARIABLE WEIGHTED RESIDUALS

NUMBER OF RESIDUALS INCLUDED: 35									
-2.25	-1.99	-1.62	-1.60	-1.12	-1.06	-1.02	-1.01		
-0.997	-0.867	-0.774	-0.463	-0.237	-0.166	-0.745E-01	-0.474E-01		
-0.430E-01	-0.323E-01	0.874E-01	0.109	0.132	0.146	0.262	0.312		
0.372	0.376	0.452	0.578	0.666	0.896	0.900	1.06		
1.24	2.10	2.18							

CORRELATION BETWEEN ORDERED WEIGHTED RESIDUALS AND  
 INDEPENDENT NORMAL DEVIATES = 0.978



## Test Case 2

The physical system for test case 2 is shown in figure A8. This test case represents the same ground-water system discussed by Cooley and Naff (1990, p. 79-81), and is repeated here partly for the benefit of users to whom it is familiar. The system is comprised of one confined aquifer that is divided into three zones. The system is bounded by no-flow, defined-flow ( $q_{b1}$  and  $q_{b2}$ , in units of L/T), and constant hydraulic-head ( $h_B$ ) boundaries, and is affected by a river with a riverbed hydraulic conductance equal to  $R_2$ . The aquifer properties shown in figure A8 are the transmissivity values in zones 1, 2, and 3 ( $T_1$ ,  $T_2$ , and  $T_3$ ). Stresses on the system include areal recharge in zones 1, 2, and 3 ( $W_1$ ,  $W_2$ , and  $W_3$ ), and pumpage from two wells ( $Q_1$  and  $Q_2$ ). The system is at steady state.

For the finite-difference method, most of the system is discretized into square 1,000-ft<sup>2</sup> cells, with the following exceptions: along the river, the cells are 200 ft wide across the river; along the defined-flux and constant-head boundaries, the cells are 50 ft wide across the boundary. The two wells are located at the center of cells at row 7, column 11, and at row 9, column 12. The following 14 model parameters are estimated:  $q_{B1}$ ,  $q_{B2}$ ,  $Q_1$ ,  $Q_2$ ,  $h_{B1}$ ,  $h_{B2}$ , and  $h_{B3}$  (located in fig. A8; the constant hydraulic head at intermediate points is calculated by linear interpolation),  $T_1$ ,  $W_1$ ,  $T_2$ ,  $W_2$ ,  $T_3$ ,  $W_3$ , and  $R_2$ ; the true values are shown in figure A8. The hydraulic-head data were produced by using the true parameter values, and then were corrupted by adding normally distributed noise with a standard deviation of 1.0 ft.

### INPUT FILE and Input Files from Other Packages for Test Case 2

The INPUT FILE used for test case 2 is shown on the following pages. Note that two repetitions of DATA SET 12 are used to represent two of the nine prior parameter estimates. Because each of these prior estimates are associated only with one parameter, they also could have been represented with DATA SET 10. Use of DATA SET 12, however, enables the user to change the initial parameter values, as might be required to produce convergence of parameter estimation, without changing the prior estimate of the parameter (see section "Restarting the Parameter-Estimation Routine" of Appendix B).

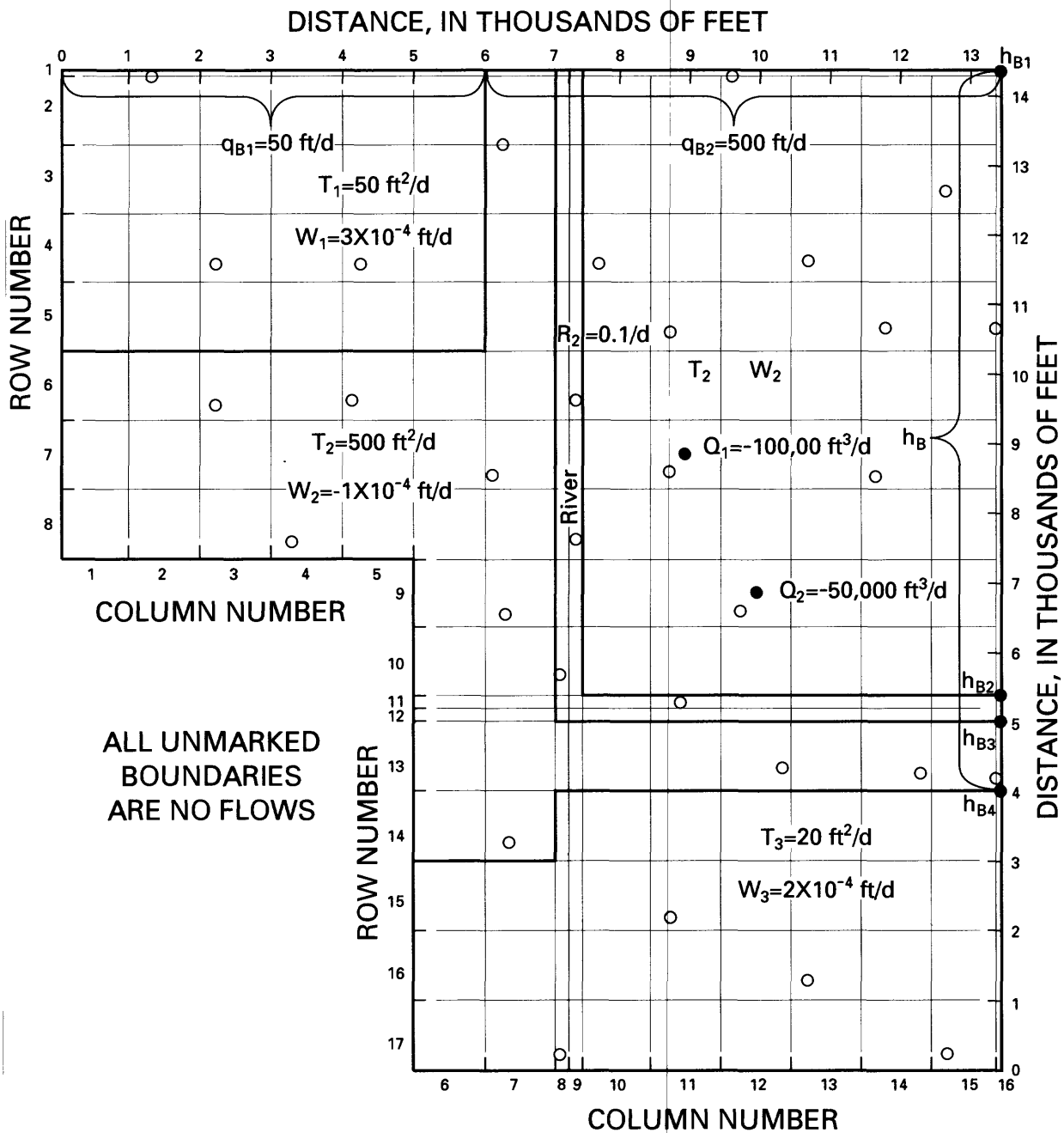


Figure A8.--Physical system for test case 2.

# INPUT FILE

## TEST CASE 2

	14	10	68	4	3	0	1
	2	1	1				
	32	0	0	0	0	0	2
	1	-1	0	0			
	36	13	0	0			
	0	0	0				
Q		6	0	0	-1		
		1		1		1	10.
		1		1		2	10.
		1		1		3	10.
		1		1		4	10.
		1		1		5	10.
		1		1		6	10.
Q		9	0	0	-1		
		1		1		7	.56
		1		1		8	.112
		1		1		9	.112
		1		1		10	.56
		1		1		11	.56
		1		1		12	.56
		1		1		13	.56
		1		1		14	.56
		1		1		15	.56
Q		1	0	0	-1		
		1		7		11	1.0
Q		1	0	0	-1		
		1		9		12	1.0
CH	13	3	0	1			
		1		1		16	2.
		1		2		16	0.
		1		3		16	0.
		1		4		16	0.
		1		5		16	0.
		1		6		16	0.
		1		7		16	0.
		1		8		16	0.
		1		9		16	0.
		1		10		16	0.
		1		11		16	3.
		1		12		16	3.
		1		13		16	4.

LINE 1  
 LINE 2  
 LINE 3  
 LINE 4  
 LINE 5  
 LINE 6  
 LINE 7  
 LINE 8  
 DATA SET 2  
 DATA SET 2A

DATA SET 2  
 DATA SET 2A

DATA SET 2  
 DATA SET 2A  
 DATA SET 2  
 DATA SET 2A  
 DATA SET 2  
 DATA SET 2A

1	1	8
1	2	8
1	3	8
1	4	8
1	5	8
1	6	8
1	7	8
1	8	8
1	9	8
1	10	8
1	11	8
1	12	8
1	12	9
1	12	10
1	12	11
1	12	12
1	12	13
1	12	14
1	12	15
1	12	16
1	1	9
1	2	9
1	3	9
1	4	9
1	5	9
1	6	9
1	7	9
1	8	9
1	9	9
1	10	9
1	11	9
1	11	10
1	11	11
1	11	12
1	11	13
1	11	14
1	11	15
1	11	16

[illegible]

16		1(8I8)						DATA SET 4			
4	4	4	4	4	4	5	5	5			
5	5	5	5	5	5	5	5	5			
1	1	1	1	1	1	2	2	5			
5	2	2	2	2	2	2	2	5			
1	1	1	1	1	1	2	2	5			
5	2	2	2	2	2	2	2	5			
1	1	1	1	1	1	2	2	5			
5	2	2	2	2	2	2	2	5			
1	1	1	1	1	1	2	2	5			
5	2	2	2	2	2	2	2	5			
2	2	2	2	2	2	2	2	5	5		
5	2	2	2	2	2	2	2	5			
2	2	2	2	2	2	2	2	5			
5	2	2	2	2	2	2	2	5			
2	2	2	2	2	2	2	2	5			
5	2	2	2	2	2	2	2	5			
0	0	0	0	0	0	2	2	5			
5	2	2	2	2	2	2	2	5			
0	0	0	0	0	0	2	2	5			
5	2	2	2	2	2	2	2	5			
0	0	0	0	0	0	2	2	5	10		
5	5	5	5	5	5	5	5	5			
0	0	0	0	0	0	2	2	5			
5	5	5	5	5	5	5	5	5			
0	0	0	0	0	0	2	2	2			
2	2	2	2	2	2	2	2	5			
0	0	0	0	0	0	2	2	3			
3	3	3	3	3	3	3	3	6			
0	0	0	0	0	0	3	3	3			
3	3	3	3	3	3	3	3	6			
0	0	0	0	0	0	3	3	3			
3	3	3	3	3	3	3	3	6			
0	0	0	0	0	0	3	3	3	30		
3	3	3	3	3	3	3	3	6			
1.0		0.0		0		1.0		DATA SET 5			
1	1	17	8	0	0.20	-0.30	0.00	69.22	1.00	0	DATA SET 6
2	1	17	15	0	0.20	-0.30	0.00	80.58	1.00	0	DATA SET 6
3	1	16	13	0	0.20	-0.30	0.00	72.66	1.00	0	DATA SET 6
4	1	15	11	0	0.20	-0.30	0.00	49.55	1.00	0	DATA SET 6
5	1	14	7	0	0.20	-0.20	0.00	10.04	1.00	0	DATA SET 6
6	1	13	12	0	0.20	0.40	0.00	7.66	1.00	0	DATA SET 6
7	1	13	14	0	0.30	0.40	0.00	11.44	1.00	0	DATA SET 6
8	1	13	16	0	0.40	0.30	0.00	13.50	1.00	0	DATA SET 6
9	1	11	11	0	0.20	-0.30	0.00	4.60	1.00	0	DATA SET 6
10	1	10	8	0	0.20	-0.30	0.00	5.30	1.00	0	DATA SET 6
11	1	9	12	0	0.20	-0.30	0.00	-38.73	1.00	0	DATA SET 6
12	1	10	16	0	0.20	-0.30	0.00	6.62	1.00	0	DATA SET 6
13	1	9	7	0	0.20	-0.30	0.00	6.54	1.00	0	DATA SET 6
14	1	8	4	0	0.20	-0.30	0.00	12.19	1.00	0	DATA SET 6
15	1	8	9	0	0.20	-0.30	0.00	4.40	1.00	0	DATA SET 6
16	1	7	11	0	0.20	-0.30	0.00	-61.07	1.00	0	DATA SET 6
17	1	7	7	0	0.20	-0.30	0.00	6.44	1.00	0	DATA SET 6

18	1	7	14	0	0.20	-0.30	0.00	-14.03	1.00	0	DATA SET 6
19	1	6	3	0	0.20	-0.30	0.00	15.73	1.00	0	DATA SET 6
20	1	6	5	0	0.20	-0.30	0.00	14.89	1.00	0	DATA SET 6
21	1	6	9	0	0.20	-0.30	0.00	4.30	1.00	0	DATA SET 6
22	1	5	11	0	0.20	-0.30	0.00	-16.15	1.00	0	DATA SET 6
23	1	5	14	0	0.20	-0.30	0.00	-5.37	1.00	0	DATA SET 6
24	1	5	16	0	0.20	-0.30	0.00	7.59	1.00	0	DATA SET 6
25	1	4	3	0	0.20	-0.30	0.00	42.42	1.00	0	DATA SET 6
26	1	4	5	0	0.20	-0.30	0.00	29.08	1.00	0	DATA SET 6
27	1	4	10	0	0.20	-0.30	0.00	1.47	1.00	0	DATA SET 6
28	1	4	13	0	0.20	-0.30	0.00	-7.42	1.00	0	DATA SET 6
29	1	3	7	0	-0.50	0.20	0.00	6.58	1.00	0	DATA SET 6
30	1	3	15	0	0.20	-0.30	0.00	4.02	1.00	0	DATA SET 6
31	1	1	2	0	0.20	-0.30	0.00	85.49	1.00	0	DATA SET 6
32	1	1	12	0	0.20	-0.30	0.00	0.98	1.00	0	DATA SET 6
45.		420.		-97000.		-51000.	10.4	4.8	5.1	70.	
.00040		420.		-.00020		15.	.00017	.080			DATA SET 8
1		1		2		2	3	3	3	4	
5		4		5		4	5	6			DATA SET 9
0.		0.		0.		0.	1.04	.48	.51	0.	
.00012		84.		0.		0.	.000051	.008			DATA SET 10
1											DATA SET 11
0.		0.		1.		0.	0.	0.	0.	0.	DATA
0.		0.		0.		0.	0.	0.	-97000.	1940.	SET 12
0.		0.		0.		1.	0.	0.	0.	0.	
0.		0.		0.		0.	0.	0.	-51000.	1020.	
2.0	.08	.001	100	0.	1	35	2	0	0	2	0
										0	.00
										.00	DATA SET 13

Input files from other packages used without and with the Parameter-Estimation Package are shown on the following pages. The true model input values are included in these files.

# Basic Package Input Files

## Without the Parameter-Estimation Package

### CLASS PROBLEM

		1				17			16			1			4
7	8	0	15	0	0	0	31	0	0	0	11	9	0	0	
		0				0									
		10				1(16I3)									-1
		99999.													
		12				1.(10F8.0)									-1
		86400.				1			1						

## With the Parameter-Estimation Package

### CLASS PROBLEM - PARAMETER ESTIMATION

		1				17			16			0			4
7	8	0	15	0	0	0	31	0	0	0	11	9	0	16	
		0				0									
		10				1(16I3)									-1
		99999.													
		12				1.(10F8.0)									-1
		86400.				1			1						

## File 10 used by the Basic Package

1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	-1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1
0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1

# File 12 used by the Basic Package

5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	10.0				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	9.71233				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	9.16438				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	8.61644				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	8.06849				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	7.52055				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	6.97260				
5.	5.	5.	5.	5.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	6.42466				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.87671				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.32877				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.0				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.0				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.5				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.				
0.	0.	0.	0.	0.	5.	5.	5.	5.	5.
5.	5.	5.	5.	5.	5.				

## Output Control Package Input File

(not changed when using the Parameter-Estimation Package)

2	2	33	0
0	1	1	0
1	0	1	0





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River Package Input File  
(not changed when using the Parameter-Estimation Package)

38	0				
38					
1	1	8	4.5	1000.	-4.5
1	2	8	4.5	20000.	-4.5
1	3	8	4.5	20000.	-4.5
1	4	8	4.5	20000.	-4.5
1	5	8	4.5	20000.	-4.5
1	6	8	4.5	20000.	-4.5
1	7	8	4.5	20000.	-4.5
1	8	8	4.5	20000.	-4.5
1	9	8	4.5	20000.	-4.5
1	10	8	4.5	20000.	-4.5
1	11	8	4.5	4000.	-4.5
1	12	8	4.5	4000.	-4.5
1	12	9	4.5	4000.	-4.5
1	12	10	4.5	20000.	-4.5
1	12	11	4.5	20000.	-4.5
1	12	12	4.5	20000.	-4.5
1	12	13	4.5	20000.	-4.5
1	12	14	4.5	20000.	-4.5
1	12	15	4.5	20000.	-4.5
1	12	16	4.5	1000.	-4.5
1	1	9	4.5	1000.	-4.5
1	2	9	4.5	20000.	-4.5
1	3	9	4.5	20000.	-4.5
1	4	9	4.5	20000.	-4.5
1	5	9	4.5	20000.	-4.5
1	6	9	4.5	20000.	-4.5
1	7	9	4.5	20000.	-4.5
1	8	9	4.5	20000.	-4.5
1	9	9	4.5	20000.	-4.5
1	10	9	4.5	20000.	-4.5
1	11	9	4.5	4000.	-4.5
1	11	10	4.5	20000.	-4.5
1	11	11	4.5	20000.	-4.5
1	11	12	4.5	20000.	-4.5
1	11	13	4.5	20000.	-4.5
1	11	14	4.5	20000.	-4.5
1	11	15	4.5	20000.	-4.5
1	11	16	4.5	1000.	-4.5

Recharge Package Input File  
(not changed when using the Parameter-Estimation Package)

1	0	NRCHOP	IRCHBD					
0	0							
31	1.E-4(8F8.0)				2			
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
3.0	3.0	3.0	3.0	3.0	3.0	-1.0	0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
3.0	3.0	3.0	3.0	3.0	3.0	-1.0	0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
3.0	3.0	3.0	3.0	3.0	3.0	-1.0	0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
3.0	3.0	3.0	3.0	3.0	3.0	-1.0	-0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-0.0	5
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	-0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	-0.0	
-0.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	-0.0	10
-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	-0.0	
-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	-1.0	
-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	-1.0	0.0	
0.	0.	0.	0.	0.	-1.0	-1.0	2.0	
2.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	
0.	0.	0.	0.	0.	2.0	2.0	2.0	
2.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	
0.	0.	0.	0.	0.	2.0	2.0	2.0	
2.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	
0.	0.	0.	0.	0.	2.0	2.0	2.0	16
2.0	2.0	2.0	2.0	2.0	2.0	2.0	0.0	

Well Package Input File

(not changed when using the Parameter-Estimation Package)

17	0		
17			
1	1	1	500.
1	1	2	500.
1	1	3	500.
1	1	4	500.
1	1	5	500.
1	1	6	500.
1	1	7	280.
1	1	8	56.
1	1	9	56.
1	1	10	280.
1	1	11	280.
1	1	12	280.
1	1	13	280.
1	1	14	280.
1	1	15	280.
1	7	11	-100000.
1	9	12	-50000.

PCG2 Package Input File

(not changed when using the Parameter-Estimation Package)

1	.40	1			
.00001	.00001	1.	2	1	3

## Output for Test Case 2

```

1          U.S. GEOLOGICAL SURVEY MODULAR FINITE-DIFFERENCE GROUND-WATER MODEL - MODFLOWP VERSION
OCLASS PROBLEM - PARAMETER ESTIMATION
  1 LAYERS      17 ROWS      16 COLUMNS
  0 STRESS PERIOD(S) IN SIMULATION
MODEL TIME UNIT IS DAYS
OI/O UNITS:
ELEMENT OF IUNIT:  1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
I/O UNIT:  7  8  0 15  0  0  0 31  0  0  0 11  9  0 16  0  0  0  0  0  0  0  0  0
OBAS1 -- BASIC MODEL PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 5
ARRAYS RHS AND BUFF WILL SHARE MEMORY.
START HEAD WILL NOT BE SAVED -- DRAWDOWN CANNOT BE CALCULATED
  2213 ELEMENTS IN X ARRAY ARE USED BY BAS
  2213 ELEMENTS OF X ARRAY USED OUT OF 900000
OBCF1 -- BLOCK-CENTERED FLOW PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 7
STEADY-STATE SIMULATION
  LAYER  AQUIFER TYPE
  -----
    1      0
    1 ELEMENTS IN X ARRAY ARE USED BY BCF
    2214 ELEMENTS OF X ARRAY USED OUT OF 900000
OWELL1 -- WELL PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM 8
MAXIMUM OF 17 WELLS
    68 ELEMENTS IN X ARRAY ARE USED FOR WELLS
    2282 ELEMENTS OF X ARRAY USED OUT OF 900000
ORCH1 -- RECHARGE PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 31
OPTION 1 -- RECHARGE TO TOP LAYER
    272 ELEMENTS OF X ARRAY USED FOR RECHARGE
    2554 ELEMENTS OF X ARRAY USED OUT OF 900000
ORIV1 -- RIVER PACKAGE, VERSION 1, 9/1/87 INPUT READ FROM UNIT 15
MAXIMUM OF 38 RIVER NODES
    228 ELEMENTS IN X ARRAY ARE USED FOR RIVERS
    2782 ELEMENTS OF X ARRAY USED OUT OF 900000
OPCG2 -- CONJUGATE GRADIENT SOLUTION PACKAGE, VERSION 2, 5/1/88
MAXIMUM OF 1 CALLS OF SOLUTION ROUTINE
MAXIMUM OF 40 INTERNAL ITERATIONS PER CALL TO SOLUTION ROUTINE
MATRIX PRECONDITIONING TYPE : 1
    1408 ELEMENTS IN X ARRAY ARE USED BY PCG
    4190 ELEMENTS OF X ARRAY USED OUT OF 900000
OSEN1 -- SENSITIVITY PACKAGE, VERSION 1, 12/01/91 INPUT READ FROM UNIT 16
OCLASS PROBLEM
0
NUMBER OF PARAMETERS..... 14
NUMBER NLL>0 IN ALL DATA SETS 2 FOR PID=T,KV,
TKV, AND S1, +1 FOR NLL(1)>0 FOR PID=RCH OR ETH... 10
SUM ALL !NLL(1)! FOR PID=Q,KRB,KDR,KST,GHB,AND CH... 68
LARGEST NLL VECTOR IN ALL DATA SETS 2..... 4
LARGEST LZ VECTOR IN ALL DATA SETS 2B..... 3
NUMBER OF MULTIPLICATION MATRICES IN DATA SET 3.... 0
NUMBER OF ZONE MATRICES IN DATA SET 4..... 1

PRINT MATRICES PRODUCED BY INIT. PARAM. EST. (>0)... 2
CHECK CELL REPETITIONS FOR MATRIX PARAMETERS (>0)... 0
NUMBER OF CELL REPETITIONS ALLOWED..... 0

NUMBER OF HEADS..... 32
NUMBER OF MULTILAYER HEADS..... 0
MAXIMUM NUMBER OF LAYERS FOR MULTILAYER HEADS.... 0
NUMBER OF FLUX CELL GROUPS..... 0
NUMBER OF CELLS IN FLUX CELL GROUPS..... 0
NUMBER OF FLUXES..... 0
NUMBER OF PRIORS WITH MULTIPLE PARAMETERS..... 2

HEADS (<0), HEADS AND SENS. (0), OR PAR. EST. (1)... 1
ADJOINT (+) OR SEN. EQ. (-) CALCULATIONS..... -1
(GRAIENT SEARCH (+) OR GAUSS-NEWTON (-) REGRESSION)
SCALE PRINTED SENSITIVITIES (>0)..... 0
ADJUST GAUSS-NEWTON MATRIX WITH NEWTON UPDATES..... 0

OUTPUT/INPUT UNIT FOR HEADS OR SENSITIVITIES..... 36
OUTPUT/INPUT UNIT NUMBER FOR INFO FROM ITERATIONS... 13
INPUT UNIT FOR SS/TR IBOUND ARRAYS..... 0
INPUT UNIT FOR KNOWN HEADS AT CONSTANT-HEAD BNDRTS.. 0

NUMBER OF INPUT UNITS IDENTIFIED IN RCH AND EVT.... 0
NUMBER OF TIME STEPS>0 AT WHICH HEAD=0..... 0
NUMBER OF USUALLY POS. PARAMETERS THAT MAY BE NEG.. 0

```

2718 ELEMENTS IN X ARRAY ARE USED FOR SENSITIVITIES  
 6908 ELEMENTS OF X ARRAY USED OUT OF 900000  
 PART -- PARAMETER ESTIMATION PACKAGE, VERSION 1, 12/01/91  
 816 ELEMENTS IN X ARRAY ARE USED FOR PARAMETER ESTIMATION  
 7724 ELEMENTS OF X ARRAY USED OUT OF 900000  
 CLASS PROBLEM - PARAMETER ESTIMATION

BOUNDARY ARRAY FOR LAYER 1 WILL BE READ ON UNIT 5 USING FORMAT: (16I3)

AQUIFER HEAD WILL BE SET TO 99999. AT ALL NO-FLOW NODES (IBOUND=0).

INITIAL HEAD FOR LAYER 1 WILL BE READ ON UNIT 5 USING FORMAT: (10F8.0)

HEAD PRINT FORMAT IS FORMAT NUMBER 2 DRAWDOWN PRINT FORMAT IS FORMAT NUMBER 2  
 HEADS WILL BE SAVED ON UNIT 33 DRAWDOWNS WILL BE SAVED ON UNIT 0  
 OUTPUT CONTROL IS SPECIFIED EVERY TIME STEP

COLUMN TO ROW ANISOTROPY = 1.000000

DELR WILL BE READ ON UNIT 7 USING FORMAT: (8F8.0)

1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	200.00	200.00	1000.0
1000.0	1000.0	1000.0	1000.0	1000.0	50.0000				

DELC WILL BE READ ON UNIT 7 USING FORMAT: (8F8.0)

50.0000	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0
200.00	200.00	1000.0	1000.0	1000.0	1000.0	1000.0			

TRANSMIS. ALONG ROWS FOR LAYER 1 WILL BE READ ON UNIT 7 USING FORMAT: (8F8.0)

	1 11	2 12	3 13	4 14	5 15	6 16	7	8	9	10
1	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
2	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
3	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
4	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
5	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
6	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
7	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
8	50.00	50.00	50.00	50.00	50.00	50.00	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
9	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
10	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
11	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
12	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
13	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	500.0	500.0	500.0
	500.0	500.0	500.0	500.0	500.0	500.0				
14	0.0000	0.0000	0.0000	0.0000	0.0000	500.0	500.0	20.00	20.00	20.00
	20.00	20.00	20.00	20.00	20.00	20.00				
15	0.0000	0.0000	0.0000	0.0000	0.0000	20.00	20.00	20.00	20.00	20.00
	20.00	20.00	20.00	20.00	20.00	20.00				

16	0.0000	0.0000	0.0000	0.0000	0.0000	20.00	20.00	20.00	20.00	20.00
	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00
17	0.0000	0.0000	0.0000	0.0000	0.0000	20.00	20.00	20.00	20.00	20.00
	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00

# SOLUTION BY THE CONJUGATE-GRADIENT METHOD

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MAXIMUM NUMBER OF CALLS TO PCG ROUTINE = 1
MAXIMUM ITERATIONS PER CALL TO PCG = 40
MATRIX PRECONDITIONING TYPE = 1
RELAXATION FACTOR (ONLY USED WITH PRECOND. TYPE 1) = 0.10000E+01
PARAMETER OF POLYNOMIAL PRECOND. = 2 (2) OR IS CALCULATED : 2
HEAD CHANGE CRITERION FOR CLOSURE = 0.10000E-04
RESIDUAL CHANGE CRITERION FOR CLOSURE = 0.10000E-04
PCG HEAD AND RESIDUAL CHANGE PRINTOUT INTERVAL = 1
PRINTING FROM SOLVER IS LIMITED(1) OR SUPPRESSED (>1) = 3

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## DEFINITION OF TEMPORAL AND SPATIAL EXTENT OF PARAMETERS (PARAMETERIZATION)

PARAMETER NUMBER: 1, PARAMETER IDENTIFIER: Q

LN: 0, VECTOR NLL: 6 0 0 -1

LAYER	ROW	COLUMN	FACTOR
1.	1.	1.	0.100E+02
1.	1.	2.	0.100E+02
1.	1.	3.	0.100E+02
1.	1.	4.	0.100E+02
1.	1.	5.	0.100E+02
1.	1.	6.	0.100E+02

PARAMETER NUMBER: 2, PARAMETER IDENTIFIER: Q

LN: 0, VECTOR NLL: 9 0 0 -1

LAYER	ROW	COLUMN	FACTOR
1.	1.	7.	0.560E+00
1.	1.	8.	0.112E+00
1.	1.	9.	0.112E+00
1.	1.	10.	0.560E+00
1.	1.	11.	0.560E+00
1.	1.	12.	0.560E+00
1.	1.	13.	0.560E+00
1.	1.	14.	0.560E+00
1.	1.	15.	0.560E+00

PARAMETER NUMBER: 3, PARAMETER IDENTIFIER: Q

LN: 0, VECTOR NLL: 1 0 0 -1

LAYER	ROW	COLUMN	FACTOR
1.	7.	11.	0.100E+01

PARAMETER NUMBER: 4, PARAMETER IDENTIFIER: Q

LN: 0, VECTOR NLL: 1 0 0 -1

LAYER	ROW	COLUMN	FACTOR
1.	9.	12.	0.100E+01

PARAMETER NUMBER: 5, PARAMETER IDENTIFIER: CH

LN: 0, VECTOR NLL: 13 3 0 1

LAYER	ROW	COLUMN	FACTOR
0.	1.	16.	0.200E+01
0.	2.	16.	0.000E+00
0.	3.	16.	0.000E+00
0.	4.	16.	0.000E+00
0.	5.	16.	0.000E+00
0.	6.	16.	0.000E+00
0.	7.	16.	0.000E+00
0.	8.	16.	0.000E+00
0.	9.	16.	0.000E+00
0.	10.	16.	0.000E+00
0.	11.	16.	0.300E+01
0.	12.	16.	0.300E+01
0.	13.	16.	0.400E+01

PARAMETER NUMBER: 8, PARAMETER IDENTIFIER: T

LN: 0, VECTOR NLL: 1 0 0 0

SFAC= 1.00, MULT. MATRIX 0, ZONE MATRIX 1

ZONES = 1 4 0

PARAMETER NUMBER: 9, PARAMETER IDENTIFIER: RCH  
 LN: 0, VECTOR NLL: 1 0 0 -1  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 1 0 0

PARAMETER NUMBER: 10, PARAMETER IDENTIFIER: T  
 LN: 0, VECTOR NLL: 1 0 0 0  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 2 5 0

PARAMETER NUMBER: 11, PARAMETER IDENTIFIER: RCH  
 LN: 0, VECTOR NLL: 2 0 0 -1  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 2 0 0

PARAMETER NUMBER: 12, PARAMETER IDENTIFIER: T  
 LN: 0, VECTOR NLL: 1 0 0 0  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 3 6 0

PARAMETER NUMBER: 13, PARAMETER IDENTIFIER: RCH  
 LN: 0, VECTOR NLL: 3 0 0 -1  
 SFAC= 1.00 , MULT. MATRIX 0, ZONE MATRIX 1  
 ZONES = 3 0 0

PARAMETER NUMBER: 14, PARAMETER IDENTIFIER: KRB  
 LN: 0, VECTOR NLL: 38 0 0 -1

LAYER	ROW	COLUMN	FACTOR
1.	1.	8.	0.100E+05
1.	2.	8.	0.200E+06
1.	3.	8.	0.200E+06
1.	4.	8.	0.200E+06
1.	5.	8.	0.200E+06
1.	6.	8.	0.200E+06
1.	7.	8.	0.200E+06
1.	8.	8.	0.200E+06
1.	9.	8.	0.200E+06
1.	10.	8.	0.200E+06
1.	11.	8.	0.400E+05
1.	12.	8.	0.400E+05
1.	12.	9.	0.400E+05
1.	12.	10.	0.200E+06
1.	12.	11.	0.200E+06
1.	12.	12.	0.200E+06
1.	12.	13.	0.200E+06
1.	12.	14.	0.200E+06
1.	12.	15.	0.200E+06
1.	12.	16.	0.100E+05
1.	1.	9.	0.100E+05
1.	2.	9.	0.200E+06
1.	3.	9.	0.200E+06
1.	4.	9.	0.200E+06
1.	5.	9.	0.200E+06
1.	6.	9.	0.200E+06
1.	7.	9.	0.200E+06
1.	8.	9.	0.200E+06
1.	9.	9.	0.200E+06
1.	10.	9.	0.200E+06
1.	11.	9.	0.400E+05
1.	11.	10.	0.200E+06
1.	11.	11.	0.200E+06
1.	11.	12.	0.200E+06
1.	11.	13.	0.200E+06
1.	11.	14.	0.200E+06
1.	11.	15.	0.200E+06
1.	11.	16.	0.100E+05



ZONE MATRIX WILL BE READ ON UNIT 16 USING FORMAT: (818)

	1	2	3	4	5	6	7	8	9	10
	11	12	13	14	15	16				
1	4	4	4	4	4	4	5	5	5	5
2	5	5	5	5	5	5	1	5	5	2
3	1	1	1	1	1	1	2	5	5	2
4	2	2	2	2	2	2	5	5	5	2
5	1	1	1	1	1	1	2	5	5	2
6	2	2	2	2	2	2	5	5	5	2
7	2	2	2	2	2	2	2	5	5	2
8	2	2	2	2	2	2	2	5	5	2
9	0	0	0	0	0	0	2	5	5	2
10	2	2	2	2	2	2	5	5	5	2
11	0	0	0	0	0	0	2	5	5	5
12	5	5	5	5	5	5	2	5	5	5
13	0	0	0	0	0	0	2	2	2	2
14	2	2	2	2	2	2	5	3	3	3
15	0	0	0	0	0	0	3	3	3	3
16	3	3	3	3	3	3	6	3	3	3
17	0	0	0	0	0	0	3	3	3	3
	3	3	3	3	3	3	6			

NSM CAN BE REDUCED FROM 10 TO 6

INPUT ERROR VARIANCES FOR HEADS AND FLOWS: 1.000 0.0000

INPUT UNIT NUMBERS FOR HEADS AND FLOWS : 0 0

ESTIMATED COMMON ERROR VARIANCE : 1.000

OBSERVED HEAD DATA

OBS#	ID	LAYER	ROW	COLUMN	TIME STEP	ROW/COLUMN/TIME OFFSETS	OBSERVATION	VARIANCE
1	1	1	17	8	0	0.20 -0.30 0.00	69.220	1.0000
2	2	1	17	15	0	0.20 -0.30 0.00	80.580	1.0000
3	3	1	16	13	0	0.20 -0.30 0.00	72.660	1.0000
4	4	1	15	11	0	0.20 -0.30 0.00	49.550	1.0000
5	5	1	14	7	0	0.20 -0.20 0.00	10.040	1.0000
6	6	1	13	12	0	0.20 0.40 0.00	7.6600	1.0000
7	7	1	13	14	0	0.30 0.40 0.00	11.440	1.0000
8	8	1	13	16	0	0.40 0.30 0.00	13.500	1.0000
9	9	1	11	11	0	0.20 -0.30 0.00	4.6000	1.0000
10	10	1	10	8	0	0.20 -0.30 0.00	5.3000	1.0000
11	11	1	9	12	0	0.20 -0.30 0.00	-38.730	1.0000
12	12	1	10	16	0	0.20 -0.30 0.00	6.6200	1.0000
13	13	1	9	7	0	0.20 -0.30 0.00	6.5400	1.0000
14	14	1	8	4	0	0.20 -0.30 0.00	12.190	1.0000
15	15	1	8	9	0	0.20 -0.30 0.00	4.4000	1.0000
16	16	1	7	11	0	0.20 -0.30 0.00	-61.070	1.0000
17	17	1	7	7	0	0.20 -0.30 0.00	6.4400	1.0000
18	18	1	7	14	0	0.20 -0.30 0.00	-14.030	1.0000
19	19	1	6	3	0	0.20 -0.30 0.00	15.730	1.0000
20	20	1	6	5	0	0.20 -0.30 0.00	14.890	1.0000
21	21	1	6	9	0	0.20 -0.30 0.00	4.3000	1.0000
22	22	1	5	11	0	0.20 -0.30 0.00	-16.150	1.0000
23	23	1	5	14	0	0.20 -0.30 0.00	-5.3700	1.0000
24	24	1	5	16	0	0.20 -0.30 0.00	7.5900	1.0000
25	25	1	4	3	0	0.20 -0.30 0.00	42.420	1.0000
26	26	1	4	5	0	0.20 -0.30 0.00	29.080	1.0000
27	27	1	4	10	0	0.20 -0.30 0.00	1.4700	1.0000
28	28	1	4	13	0	0.20 -0.30 0.00	-7.4200	1.0000
29	29	1	3	7	0	-0.50 0.20 0.00	6.5800	1.0000
30	30	1	3	15	0	0.20 -0.30 0.00	4.0200	1.0000
31	31	1	1	2	0	0.20 -0.30 0.00	85.490	1.0000
32	32	1	1	12	0	0.20 -0.30 0.00	0.98000	1.0000

## REGRESSION DATA:

MAX. PARAMETER CORRECTION (DMAX) = 2.0000  
 SEARCH DIR. ADJUSTMENT PAR. (CSA) = 0.80000E-01  
 CLOSURE CRITERION (TOL) ----- = 0.10000E-02  
 MAXIMUM NO. OF ITERATIONS (ITMXP) = 100  
 MODIFY CONV. CRITERIA (>0) (FCONV) = 0.00000  
 USE PRIOR PAR EST (>0) (IPRIOR) = 1  
 OUTPUT UNIT FOR RESAN (IOUR) ---- = 35  
 FORMAT CODE FOR COV AND COR (IPRC) = 2  
 PRINT SENS., ETC. (>0) (IPRINT) = 0  
 PRINT LAST HEADS (1) (KPRINT) --- = 0  
 PRINT EIGEN V&V OF COV(>0) (LPRINT) = 2  
 CALC. SEN. W/ LAST PAR (>0) (LASTX) = 0  
 NO. FLETCHER-REEVES ITES (NFIT) = 0  
 SUM OF SQUARES CLOSURE CRIT. (SOSC) = 0.00000

## PARAMETER INFORMATION:

(CONVERGENCE CRITERIA LISTED HERE ARE USED TO SOLVE FOR SENSITIVITY-EQUATION SENSITIVITIES)

#	ID	INITIAL VALUE	LN	CONVERGENCE CRITERIA		GROUP#	WEIGHT OF PRIOR EST.
1	Q	45.00	0	0.222E-08	0.222E-08	1	
2	Q	420.0	0	0.238E-09	0.238E-09	1	
3	Q	-0.9700E+05	0	0.103E-11	0.103E-11	2	
4	Q	-0.5100E+05	0	0.196E-11	0.196E-11	2	
5	CH	10.40	0	0.962E-08	0.962E-08	3	0.9246
6	CH	4.800	0	0.208E-07	0.208E-07	3	4.340
7	CH	5.100	0	0.196E-07	0.196E-07	3	3.845
8	T	70.00	0	0.143E-08	0.143E-08	4	
9	RCH	0.4000E-03	0	0.250E-03	0.250E-03	5	0.6944E+08
10	T	420.0	0	0.238E-09	0.238E-09	4	0.1417E-03
11	RCH	-0.2000E-03	0	0.500E-03	0.500E-03	5	
12	T	15.00	0	0.667E-08	0.667E-08	4	
13	RCH	0.1700E-03	0	0.588E-03	0.588E-03	5	0.3845E+09
14	KRB	0.8000E-01	0	0.125E-05	0.125E-05	6	0.1563E+05

## PRIOR ESTIMATES OF PARAMETER SUMS

EQ.# :	1	2
PAR#	PID	
1	Q	0.000 0.000
2	Q	0.000 0.000
3	Q	1.00 0.000
4	Q	0.000 1.00
5	CH	0.000 0.000
6	CH	0.000 0.000
7	CH	0.000 0.000
8	T	0.000 0.000
9	RCH	0.000 0.000
10	T	0.000 0.000
11	RCH	0.000 0.000
12	T	0.000 0.000
13	RCH	0.000 0.000
14	KRB	0.000 0.000
ESTIMATE		-0.970E+05-0.510E+05
WEIGHT**5		0.515E-03 0.980E-03

WARNING -- NP &gt; ND/3 : YOU MAY BE TRYING TO ESTIMATE TOO MANY PARAMETERS FOR THE DATA (PAR1RP)

## 17 WELLS

LAYER	ROW	COL	STRESS RATE	WELL NO.
1	1	1	500.00	1
1	1	2	500.00	2
1	1	3	500.00	3
1	1	4	500.00	4
1	1	5	500.00	5
1	1	6	500.00	6
1	1	7	280.00	7
1	1	8	56.000	8
1	1	9	56.000	9
1	1	10	280.00	10
1	1	11	280.00	11
1	1	12	280.00	12
1	1	13	280.00	13
1	1	14	280.00	14
1	1	15	280.00	15
1	7	11	-0.10000E+06	16
1	9	12	-50000.	17

RECHARGE WILL BE READ ON UNIT 31 USING FORMAT: (8F8.0)

	1 10	2 11	3 12	4 13	5 14	6 15	7 16	8	9
1	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	-1.000000E-04	0.000000	0.000000
4	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	0.000000	0.000000
5	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	-1.000000E-04	0.000000	0.000000
6	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	0.000000	0.000000
7	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	3.000000E-04	-1.000000E-04	0.000000	0.000000
8	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	0.000000	0.000000
9	0.000000	0.000000	0.000000	0.000000	0.000000	-1.000000E-04	-1.000000E-04	0.000000	0.000000
10	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	0.000000	0.000000
11	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
12	0.000000	0.000000	0.000000	0.000000	0.000000	-1.000000E-04	-1.000000E-04	0.000000	0.000000
13	0.000000	0.000000	0.000000	0.000000	0.000000	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04
14	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	-1.000000E-04	2.000000E-04	2.000000E-04
15	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	0.000000	2.000000E-04	2.000000E-04
16	0.000000	0.000000	0.000000	0.000000	0.000000	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04
17	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	2.000000E-04	0.000000	2.000000E-04	2.000000E-04

38 RIVER REACHES

LAYER	ROW	COL	STAGE	CONDUCTANCE	BOTTOM ELEVATION	RIVER REACH
1	1	8	4.500	1000.	-4.500	1
1	2	8	4.500	0.2000E+05	-4.500	2
1	3	8	4.500	0.2000E+05	-4.500	3
1	4	8	4.500	0.2000E+05	-4.500	4
1	5	8	4.500	0.2000E+05	-4.500	5
1	6	8	4.500	0.2000E+05	-4.500	6
1	7	8	4.500	0.2000E+05	-4.500	7
1	8	8	4.500	0.2000E+05	-4.500	8
1	9	8	4.500	0.2000E+05	-4.500	9
1	10	8	4.500	0.2000E+05	-4.500	10
1	11	8	4.500	4000.	-4.500	11
1	12	8	4.500	4000.	-4.500	12
1	12	9	4.500	4000.	-4.500	13
1	12	10	4.500	0.2000E+05	-4.500	14
1	12	11	4.500	0.2000E+05	-4.500	15
1	12	12	4.500	0.2000E+05	-4.500	16
1	12	13	4.500	0.2000E+05	-4.500	17
1	12	14	4.500	0.2000E+05	-4.500	18
1	12	15	4.500	0.2000E+05	-4.500	19
1	12	16	4.500	1000.	-4.500	20
1	1	9	4.500	1000.	-4.500	21
1	2	9	4.500	0.2000E+05	-4.500	22
1	3	9	4.500	0.2000E+05	-4.500	23
1	4	9	4.500	0.2000E+05	-4.500	24
1	5	9	4.500	0.2000E+05	-4.500	25
1	6	9	4.500	0.2000E+05	-4.500	26
1	7	9	4.500	0.2000E+05	-4.500	27
1	8	9	4.500	0.2000E+05	-4.500	28
1	9	9	4.500	0.2000E+05	-4.500	29
1	10	9	4.500	0.2000E+05	-4.500	30
1	11	9	4.500	4000.	-4.500	31



11	0.000000	0.000000	0.000000	0.000000	0.000000	-2.000000E-04	-2.000000E-04	0.000000	0.000000
	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
12	0.000000	0.000000	0.000000	0.000000	0.000000	-2.000000E-04	-2.000000E-04	0.000000	0.000000
	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
13	0.000000	0.000000	0.000000	0.000000	0.000000	-2.000000E-04	-2.000000E-04	-2.000000E-04	-2.000000E-04
	-2.000000E-04	-2.000000E-04	-2.000000E-04	-2.000000E-04	-2.000000E-04	-2.000000E-04	0.000000	0.000000	0.000000
14	0.000000	0.000000	0.000000	0.000000	0.000000	-2.000000E-04	-2.000000E-04	1.700000E-04	1.700000E-04
	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	0.000000	0.000000	0.000000
15	0.000000	0.000000	0.000000	0.000000	0.000000	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04
	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	0.000000	0.000000	0.000000
16	0.000000	0.000000	0.000000	0.000000	0.000000	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04
	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	0.000000	0.000000	0.000000
17	0.000000	0.000000	0.000000	0.000000	0.000000	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04
	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	1.700000E-04	0.000000	0.000000	0.000000

# DATA AT HEAD LOCATIONS

OBS#	ID	LAYER,ROW,COL	TIME STEP	ROW/COL/TIME OFFSETS	MEAS. HEAD	CALC. HEAD	RESIDUAL	WEIGHT**.5	WEIGHTED RESIDUAL
1	1	1 17 8	0	0.00-0.30 0.00	69.220	75.801	-6.58	1.00	-6.58
2	2	1 17 15	0	0.00-0.30 0.00	80.580	90.568	-9.99	1.00	-9.99
3	3	1 16 13	0	0.20-0.30 0.00	72.660	80.344	-7.68	1.00	-7.68
4	4	1 15 11	0	0.20-0.30 0.00	49.550	56.003	-6.45	1.00	-6.45
5	5	1 14 7	0	0.20-0.20 0.00	10.040	12.171	-2.13	1.00	-2.13
6	6	1 13 12	0	0.20 0.40 0.00	7.660	9.334	-1.67	1.00	-1.67
7	7	1 13 14	0	0.30 0.40 0.00	11.440	11.742	-0.302	1.00	-0.302
8	8	1 13 16	0	0.40 0.00 0.00	13.500	13.831	-0.331	1.00	-0.331
9	9	1 11 11	0	0.20-0.30 0.00	4.600	4.151	0.449	1.00	0.449
10	10	1 10 8	0	0.20-0.30 0.00	5.300	4.519	0.781	1.00	0.781
11	11	1 9 12	0	0.20-0.30 0.00	-38.730	-45.718	6.99	1.00	6.99
12	12	1 10 16	0	0.20-0.30 0.00	6.620	4.994	1.63	1.00	1.63
13	13	1 9 7	0	0.20-0.30 0.00	6.540	4.830	1.71	1.00	1.71
14	14	1 8 4	0	0.20-0.30 0.00	12.190	11.969	0.221	1.00	0.221
15	15	1 8 9	0	0.20-0.30 0.00	4.400	3.934	0.466	1.00	0.466
16	16	1 7 11	0	0.20-0.30 0.00	-61.070	-72.046	11.0	1.00	11.0
17	17	1 7 7	0	0.20-0.30 0.00	6.440	5.878	0.562	1.00	0.562
18	18	1 7 14	0	0.20-0.30 0.00	-14.030	-19.139	5.11	1.00	5.11
19	19	1 6 3	0	0.20-0.30 0.00	15.730	16.378	-0.648	1.00	-0.648
20	20	1 6 5	0	0.20-0.30 0.00	14.890	11.882	3.01	1.00	3.01
21	21	1 6 9	0	0.20-0.30 0.00	4.300	3.894	0.406	1.00	0.406
22	22	1 5 11	0	0.20-0.30 0.00	-16.150	-19.851	3.70	1.00	3.70
23	23	1 5 14	0	0.20-0.30 0.00	-5.370	-9.861	4.49	1.00	4.49
24	24	1 5 16	0	0.20-0.30 0.00	7.590	7.959	-0.369	1.00	-0.369
25	25	1 4 3	0	0.20-0.30 0.00	42.420	40.661	1.76	1.00	1.76
26	26	1 4 5	0	0.20-0.30 0.00	29.080	28.663	0.417	1.00	0.417
27	27	1 4 10	0	0.20-0.30 0.00	1.470	0.682	0.788	1.00	0.788
28	28	1 4 13	0	0.20-0.30 0.00	-7.420	-10.410	2.99	1.00	2.99
29	29	1 3 7	0	-0.50 0.20 0.00	6.580	6.021	0.559	1.00	0.559
30	30	1 3 15	0	0.20-0.30 0.00	4.020	3.962	0.582E-01	1.00	0.582E-01
31	31	1 1 2	0	0.20-0.30 0.00	85.490	72.029	13.5	1.00	13.5
32	32	1 1 12	0	0.20-0.30 0.00	0.980	-2.157	3.14	1.00	3.14

# STATISTICS FOR THESE RESIDUALS :

MAXIMUM WEIGHTED RESIDUAL : 0.135E+02 OBS# 31  
MINIMUM WEIGHTED RESIDUAL : -0.999E+01 OBS# 2  
AVERAGE WEIGHTED RESIDUAL : 0.859E+00  
# RESIDUALS >= 0. : 22  
# RESIDUALS < 0. : 10  
NUMBER OF RUNS : 6 IN 32 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (HEADS) 701.51

# PARAMETERS WITH PRIOR INFORMATION, BY GROUP

PARAMETER	VALUES	WEIGHT	WEIGHTED			
#	PID	MEAS.	CALC.	RESIDUAL	** .5	RESIDUAL
5	CH	0.104E+02	0.104E+02	0.000E+00	0.962	0.000
6	CH	0.480E+01	0.480E+01	0.000E+00	2.08	0.000
7	CH	0.510E+01	0.510E+01	0.000E+00	1.96	0.000
10	T	0.420E+03	0.420E+03	0.000E+00	0.119E-01	0.000
9	RCH	0.400E-03	0.400E-03	0.000E+00	0.833E+04	0.000
13	RCH	0.170E-03	0.170E-03	0.000E+00	0.196E+05	0.000
14	KRB	0.800E-01	0.800E-01	0.000E+00	125.	0.000

STATISTICS FOR THESE RESIDUALS :  
 MAXIMUM WEIGHTED RESIDUAL : 0.000E+00  
 MINIMUM WEIGHTED RESIDUAL : 0.000E+00  
 AVERAGE WEIGHTED RESIDUAL : 0.000E+00  
 # RESIDUALS >= 0. : 7  
 # RESIDUALS < 0. : 0  
 NUMBER OF RUNS : 6 IN 40 OBSERVATIONS

PARAMETER SUMS WITH PRIOR INFORMATION

EQ.#	MEAS.	VALUES	RESIDUAL	WEIGHT	WEIGHTED
		CALC.		** 5	RESIDUAL
1	-0.970E+05	-0.970E+05	0.000E+00	0.515E-03	0.000
2	-0.510E+05	-0.510E+05	0.000E+00	0.980E-03	0.000

STATISTICS FOR THESE RESIDUALS :  
 MAXIMUM WEIGHTED RESIDUAL : 0.000E+00  
 MINIMUM WEIGHTED RESIDUAL : 0.000E+00  
 AVERAGE WEIGHTED RESIDUAL : 0.000E+00  
 # RESIDUALS >= 0. : 2  
 # RESIDUALS < 0. : 0  
 NUMBER OF RUNS : 6 IN 42 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 701.51  
 SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 701.51

STATISTICS FOR ALL RESIDUALS :  
 AVERAGE WEIGHTED RESIDUAL : -0.671E+00  
 # RESIDUALS >= 0. : 19  
 # RESIDUALS < 0. : 22  
 NUMBER OF RUNS : 6 IN 42 OBSERVATIONS  
 RUNS STATISTIC (TOO FEW RUNS): -4.74  
 (IF #NEG>10 AND #POS>10, P(STAT < -1.28) = 0.10,  
 P(STAT < -1.645) = 0.05,  
 P(STAT < -1.96) = 0.025)  
 RUNS STATISTIC (TOO MANY RUNS): -5.05  
 (IF #NEG>10 AND #POS>10, P(STAT > 1.28) = 0.10,  
 P(STAT > 1.645) = 0.05,  
 P(STAT > 1.96) = 0.025)

SENSITIVITIES

PARAMETER # :	1	2	3	4	5	6	7	8	9	10
PARAMETER ID :	11	12	13	14	CH	CH	CH	T	RCH	T
	Q	Q	Q	Q						
	RCH	T	RCH	KRB						
OBS# & ID										
1 1	0.147E-02	0.818E-06	0.178E-06	0.361E-06	0.695E-04	0.436E-03	0.325E-01	-0.401E-03	711.	-0.587E-02
	0.761E+04	-4.59	0.426E+06	0.577						
2 2	0.380E-03	0.251E-06	0.140E-06	0.422E-06	0.121E-03	0.169E-02	0.154	-0.104E-03	184.	-0.368E-02
	0.285E+04	-5.63	0.509E+06	0.576						
3 3	0.527E-03	0.331E-06	0.159E-06	0.466E-06	0.111E-03	0.120E-02	0.102	-0.144E-03	255.	-0.399E-02
	0.354E+04	-4.94	0.449E+06	0.662						
4 4	0.893E-03	0.521E-06	0.179E-06	0.452E-06	0.818E-04	0.538E-03	0.396E-01	-0.244E-03	431.	-0.461E-02
	0.516E+04	-3.31	0.308E+06	0.683						
5 5	0.229E-02	0.124E-05	0.184E-06	0.248E-06	0.455E-04	0.101E-03	0.380E-02	-0.623E-03	0.110E+04	-0.647E-02
	0.112E+05	-0.329	0.553E+05	0.456						
6 6	0.652E-04	0.112E-06	0.204E-06	0.782E-06	0.134E-03	0.632E-03	0.314E-01	-0.178E-04	31.5	-0.189E-02
	0.170E+04	-0.274	0.306E+05	1.11						
7 7	0.313E-04	0.610E-07	0.912E-07	0.295E-06	0.155E-03	0.287E-02	0.256	-0.855E-05	15.1	-0.173E-02
	0.124E+04	-0.426	0.432E+05	0.335						
8 8	0.322E-04	0.306E-07	0.304E-07	0.960E-07	0.510E-04	0.125E-02	0.746	-0.878E-05	15.6	-0.116E-02
	512.	-0.560	0.529E+05	0.106						
9 9	0.249E-05	0.415E-06	0.152E-05	0.385E-05	0.437E-03	0.709E-03	0.419E-04	-0.669E-06	1.20	0.658E-04
	95.7	0.869E-05	60.7	4.05						
10 10	0.332E-03	0.199E-06	0.101E-06	0.170E-06	0.238E-04	0.348E-04	0.598E-04	-0.902E-04	160.	-0.801E-04
	765.	-0.168E-03	651.	0.302						
11 11	0.963E-05	0.490E-04	0.151E-03	0.684E-03	0.566E-01	0.934E-01	0.837E-04	-0.159E-05	4.50	0.119
	0.538E+04	0.723E-06	14.3	5.59						
12 12	0.102E-07	0.112E-06	0.179E-06	0.456E-06	0.438E-01	0.938	0.309E-04	-0.102E-08	0.459E-02	0.105E-03
	25.9	0.714E-08	0.262	0.232E-01						
13 13	0.583E-02	0.315E-05	0.398E-06	0.343E-06	0.803E-04	0.947E-04	0.230E-03	-0.158E-02	0.282E+04	-0.701E-03
	0.727E+04	-0.700E-03	0.263E+04	1.08						
14 14	0.631E-01	0.284E-04	0.649E-06	0.267E-06	0.162E-03	0.133E-03	0.839E-04	-0.182E-01	0.300E+05	-0.150E-01
	0.373E+05	-0.260E-03	975.	1.34						
15 15	0.103E-03	0.998E-06	0.429E-05	0.283E-05	0.705E-03	0.848E-03	0.166E-05	-0.274E-04	50.1	0.920E-04
	185.	-0.367E-05	14.0	6.67						
16 16	0.274E-04	0.115E-03	0.700E-03	0.156E-03	0.758E-01	0.786E-01	0.283E-04	-0.396E-05	12.9	0.182
	0.632E+04	-0.181E-06	5.25	7.30						

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17 17 0.143E-01 0.858E-05 0.818E-06 0.298E-06 0.154E-03 0.140E-03 0.549E-04-0.367E-02 0.697E+04-0.300E-02
0.104E+05-0.169E-03 635. 1.77
18 18 0.895E-05 0.147E-03 0.164E-03 0.154E-03 0.256 0.345 0.733E-04-0.382E-06 3.89 0.597E-01
0.774E+04 0.134E-06 4.53 2.44
19 19 0.862E-01 0.365E-04 0.639E-06 0.254E-06 0.170E-03 0.134E-03 0.745E-04-0.253E-01 0.407E+05-0.243E-01
0.418E+05-0.231E-03 865. 1.28
20 20 0.552E-01 0.281E-04 0.661E-06 0.254E-06 0.170E-03 0.136E-03 0.702E-04-0.153E-01 0.267E+05-0.153E-01
0.294E+05-0.218E-03 815. 1.33
21 21 0.146E-03 0.292E-05 0.559E-05 0.133E-05 0.125E-02 0.102E-02 0.609E-06-0.251E-04 72.3 0.111E-03
209. -0.106E-05 4.00 7.11
22 22 0.328E-04 0.325E-03 0.214E-03 0.582E-04 0.115 0.752E-01 0.136E-04 0.233E-05 14.3 0.588E-01
0.713E+04-0.101E-06 1.99 4.66
23 23 0.125E-04 0.412E-03 0.122E-03 0.663E-04 0.398 0.269 0.234E-04 0.569E-06 4.98 0.396E-01
0.877E+04 0.176E-07 1.88 1.81
24 24 0.102E-06 0.409E-05 0.983E-06 0.602E-06 0.590 0.407 0.262E-06 0.459E-08 0.401E-01 0.342E-03
102. 0.265E-09 0.177E-01 0.150E-01
25 25 0.205 0.755E-04 0.568E-06 0.220E-06 0.191E-03 0.134E-03 0.601E-04-0.371 0.838E+05-0.245E-01
0.333E+05-0.187E-03 698. 1.01
26 26 0.129 0.886E-04 0.509E-06 0.188E-06 0.211E-03 0.135E-03 0.443E-04-0.245 0.565E+05-0.168E-01
0.216E+05-0.137E-03 514. 0.794
27 27 0.411E-04 0.149E-03 0.325E-04 0.967E-05 0.318E-01 0.166E-01 0.239E-05 0.900E-05 17.2 0.894E-02
0.219E+04-0.762E-07 0.556 3.20
28 28 0.221E-04 0.832E-03 0.128E-03 0.550E-04 0.344 0.170 0.162E-04 0.186E-05 8.26 0.400E-01
0.107E+05-0.138E-07 1.59 2.24
29 29 0.114E-01 0.236E-03 0.159E-06 0.539E-07 0.297E-03 0.122E-03 0.166E-05 0.121E-02 0.316E+04-0.372E-02
0.170E+04-0.510E-05 19.1 -0.515
30 30 0.693E-05 0.613E-03 0.315E-04 0.146E-04 0.671 0.187 0.477E-05 0.621E-06 2.45 0.107E-01
0.509E+04-0.235E-08 0.430 0.581
31 31 0.547 0.106E-03 0.526E-06 0.202E-06 0.202E-03 0.133E-03 0.534E-04-0.827 0.122E+06-0.230E-01
0.301E+05-0.166E-03 620. 0.855
32 32 0.386E-04 0.292E-02 0.643E-04 0.249E-04 0.275 0.910E-01 0.709E-05 0.398E-05 12.0 0.194E-01
0.101E+05-0.277E-07 0.801 1.74

UNSCALED RIGHT-HAND SIDE VECTOR (= -0.5*GRADIENT)
7.9058 0.19006E-01 0.11534E-01 0.80376E-02 6.5618 6.9291 -3.1775 -11.922 0.18719E+07 3.4751
0.67349E+06 147.23 -.13510E+08 177.43

ITERATION NO. = 1
VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :
DET OF SCALED LEAST-SQUARES MATRIX = 0.31565E-07
MARQUARDT PARAMETER (AMP)----- = 0.00000
FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000
MAX. FRACTIONAL PAR. CHANGE (DMX) = 1.0844
MAX. FRAC. CHANGE OCCURRED FOR PAR.# 2

UPDATED ESTIMATES OF REGRESSION PARAMETERS :
Q Q Q Q CH CH CH T RCH T
RCH T RCH KRB
87.694 875.46 -96921. -51064. 10.161 5.1424 5.2235 67.610 0.29818E-03 478.66
-.14004E-03 13.310 0.13339E-03 0.80495E-01

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 31.053
SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 33.405

ITERATION NO. = 2
VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :
DET OF SCALED LEAST-SQUARES MATRIX = 0.15610E-07
MARQUARDT PARAMETER (AMP)----- = 0.00000
FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000
MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.90701E-01
MAX. FRAC. CHANGE OCCURRED FOR PAR.# 11

UPDATED ESTIMATES OF REGRESSION PARAMETERS :
Q Q Q Q CH CH CH T RCH T
RCH T RCH KRB
84.059 937.99 -96870. -51047. 10.155 5.1421 5.2228 66.264 0.29818E-03 487.46
-.12734E-03 12.854 0.13067E-03 0.80461E-01

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 24.131
SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 26.722

ITERATION NO. = 3
VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :
DET OF SCALED LEAST-SQUARES MATRIX = 0.87981E-07
MARQUARDT PARAMETER (AMP)----- = 0.10000E-02
FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000
MAX. FRACTIONAL PAR. CHANGE (DMX) = 0.35499E-02
MAX. FRAC. CHANGE OCCURRED FOR PAR.# 2

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UPDATED ESTIMATES OF REGRESSION PARAMETERS :

Q RCH	Q T	Q RCH	Q KRB	CH	CH	CH	T	RCH	T
84.288	941.32	-96866.	-51045.	10.157	5.1424	5.2227	66.382	0.29830E-03	487.63
-.12767E-03	12.870	0.13077E-03	0.80459E-01						

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 24.128  
 SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 26.717

ITERATION NO. = 4

VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :

DET OF SCALED LEAST-SQUARES MATRIX = 0.14678E-07  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = -.52083E-02  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 11

UPDATED ESTIMATES OF REGRESSION PARAMETERS :

Q RCH	Q T	Q RCH	Q KRB	CH	CH	CH	T	RCH	T
84.497	943.73	-96867.	-51045.	10.158	5.1426	5.2226	66.523	0.29873E-03	487.67
-.12833E-03	12.912	0.13119E-03	0.80459E-01						

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 24.145  
 SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 26.717

ITERATION NO. = 5

VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :

DET OF SCALED LEAST-SQUARES MATRIX = 0.14787E-07  
 MARQUARDT PARAMETER (AMP)----- = 0.00000  
 FACTOR FOR SCALING PAR. CHANGE (AP)= 1.0000  
 MAX. FRACTIONAL PAR. CHANGE (DMX) = -.51786E-04  
 MAX. FRAC. CHANGE OCCURRED FOR PAR.# 1

UPDATED ESTIMATES OF REGRESSION PARAMETERS :

Q RCH	Q T	Q RCH	Q KRB	CH	CH	CH	T	RCH	T
84.492	943.72	-96867.	-51045.	10.158	5.1426	5.2226	66.522	0.29873E-03	487.67
-.12833E-03	12.912	0.13119E-03	0.80459E-01						

PARAMETER ESTIMATION CONVERGED BY SATISFYING TOL CRITERIA

DATA AT HEAD LOCATIONS

OBS#	ID	LAYER,ROW,COL	TIME STEP	ROW/COL/TIME OFFSETS	MEAS. HEAD	CALC. HEAD	RESIDUAL	WEIGHT**5	WEIGHTED RESIDUAL
1	1	1 17 8	0	0.00-0.30 0.00	69.220	68.077	1.14	1.00	1.14
2	2	1 17 15	0	0.00-0.30 0.00	80.580	81.404	-0.824	1.00	-0.824
3	3	1 16 13	0	0.20-0.30 0.00	72.660	72.219	0.441	1.00	0.441
4	4	1 15 11	0	0.20-0.30 0.00	49.550	50.375	-0.825	1.00	-0.825
5	5	1 14 7	0	0.20-0.20 0.00	10.040	11.081	-1.04	1.00	-1.04
6	6	1 13 12	0	0.20 0.40 0.00	7.660	8.693	-1.03	1.00	-1.03
7	7	1 13 14	0	0.30 0.40 0.00	11.440	10.899	0.541	1.00	0.541
8	8	1 13 16	0	0.40 0.00 0.00	13.500	12.903	0.597	1.00	0.597
9	9	1 11 11	0	0.20-0.30 0.00	4.600	4.162	0.438	1.00	0.438
10	10	1 10 8	0	0.20-0.30 0.00	5.300	4.538	0.762	1.00	0.762
11	11	1 9 12	0	0.20-0.30 0.00	-38.730	-38.395	-0.335	1.00	-0.335
12	12	1 10 16	0	0.20-0.30 0.00	6.620	5.313	1.31	1.00	1.31
13	13	1 9 7	0	0.20-0.30 0.00	6.540	5.111	1.43	1.00	1.43
14	14	1 8 4	0	0.20-0.30 0.00	12.190	12.976	-0.786	1.00	-0.786
15	15	1 8 9	0	0.20-0.30 0.00	4.400	3.956	0.444	1.00	0.444
16	16	1 7 11	0	0.20-0.30 0.00	-61.070	-60.909	-0.161	1.00	-0.161
17	17	1 7 7	0	0.20-0.30 0.00	6.440	6.220	0.220	1.00	0.220
18	18	1 7 14	0	0.20-0.30 0.00	-14.030	-15.046	1.02	1.00	1.02
19	19	1 6 3	0	0.20-0.30 0.00	15.730	17.006	-1.28	1.00	-1.28
20	20	1 6 5	0	0.20-0.30 0.00	14.890	12.394	2.50	1.00	2.50
21	21	1 6 9	0	0.20-0.30 0.00	4.300	3.920	0.380	1.00	0.380
22	22	1 5 11	0	0.20-0.30 0.00	-16.150	-15.816	-0.334	1.00	-0.334
23	23	1 5 14	0	0.20-0.30 0.00	-5.370	-6.814	1.44	1.00	1.44
24	24	1 5 16	0	0.20-0.30 0.00	7.590	7.984	-0.394	1.00	-0.394
25	25	1 4 3	0	0.20-0.30 0.00	42.420	42.371	0.491E-01	1.00	0.491E-01
26	26	1 4 5	0	0.20-0.30 0.00	29.080	29.372	-0.292	1.00	-0.292
27	27	1 4 10	0	0.20-0.30 0.00	1.470	1.411	0.591E-01	1.00	0.591E-01
28	28	1 4 13	0	0.20-0.30 0.00	-7.420	-7.054	-0.366	1.00	-0.366
29	29	1 3 7	0	-0.50 0.20 0.00	6.580	6.126	0.454	1.00	0.454
30	30	1 3 15	0	0.20-0.30 0.00	4.020	5.084	-1.06	1.00	-1.06
31	31	1 1 2	0	0.20-0.30 0.00	85.490	85.431	0.585E-01	1.00	0.585E-01
32	32	1 1 12	0	0.20-0.30 0.00	0.980	0.896	0.844E-01	1.00	0.844E-01



STATISTICS FOR THESE RESIDUALS :  
 MAXIMUM WEIGHTED RESIDUAL : 0.128E+01 OBS# 19  
 MINIMUM WEIGHTED RESIDUAL : -0.250E+01 OBS# 20  
 AVERAGE WEIGHTED RESIDUAL : -0.145E+00  
 # RESIDUALS >= 0. : 13  
 # RESIDUALS < 0. : 19  
 NUMBER OF RUNS : 23 IN 32 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (HEADS) 24.146

PARAMETERS WITH PRIOR INFORMATION, BY GROUP

PARAMETER #	PID	MEAS.	CALC.	RESIDUAL	WEIGHT **5	WEIGHTED RESIDUAL
5	CH	0.104E+02	0.102E+02	0.242E+00	0.962	0.232
6	CH	0.480E+01	0.514E+01	-0.343E+00	2.08	-0.714
7	CH	0.510E+01	0.522E+01	-0.123E+00	1.96	-0.240
10	T	0.420E+03	0.488E+03	-0.677E+02	0.119E-01	-0.806
9	RCH	0.400E-03	0.299E-03	0.101E-03	0.833E+04	0.844
13	RCH	0.170E-03	0.131E-03	0.388E-04	0.196E+05	0.761
14	KRB	0.800E-01	0.805E-01	-0.459E-03	125.	-0.574E-01

STATISTICS FOR THESE RESIDUALS :  
 MAXIMUM WEIGHTED RESIDUAL : 0.844E+00  
 MINIMUM WEIGHTED RESIDUAL : -0.806E+00  
 AVERAGE WEIGHTED RESIDUAL : 0.286E-02  
 # RESIDUALS >= 0. : 3  
 # RESIDUALS < 0. : 4  
 NUMBER OF RUNS : 27 IN 40 OBSERVATIONS

PARAMETER SUMS WITH PRIOR INFORMATION

EQ.#	MEAS.	CALC.	RESIDUAL	WEIGHT **5	WEIGHTED RESIDUAL
1	-0.970E+05	-0.969E+05	-0.133E+03	0.515E-03	-0.683E-01
2	-0.510E+05	-0.510E+05	0.452E+02	0.980E-03	0.443E-01

STATISTICS FOR THESE RESIDUALS :  
 MAXIMUM WEIGHTED RESIDUAL : 0.443E-01  
 MINIMUM WEIGHTED RESIDUAL : -0.683E-01  
 AVERAGE WEIGHTED RESIDUAL : -0.120E-01  
 # RESIDUALS >= 0. : 1  
 # RESIDUALS < 0. : 1  
 NUMBER OF RUNS : 28 IN 42 OBSERVATIONS

SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) 24.146  
 SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) 26.717

STATISTICS FOR ALL RESIDUALS :  
 AVERAGE WEIGHTED RESIDUAL : -0.113E+00  
 # RESIDUALS >= 0. : 17  
 # RESIDUALS < 0. : 24  
 NUMBER OF RUNS : 28 IN 42 OBSERVATIONS  
 RUNS STATISTIC (TOO FEW RUNS): 2.48  
 (IF #NEG>10 AND #POS>10, P(STAT < -1.28) = 0.10,  
 P(STAT < -1.645) = 0.05,  
 P(STAT < -1.96) = 0.025)  
 RUNS STATISTIC (TOO MANY RUNS): 2.15  
 (IF #NEG>10 AND #POS>10, P(STAT > 1.28) = 0.10,  
 P(STAT > 1.645) = 0.05,  
 P(STAT > 1.96) = 0.025)

SENSITIVITIES

PARAMETER # :	1	2	3	4	5	6	7	8	9	10
PARAMETER ID :	11	12	13	14	CH	CH	CH	T	RCH	T
	Q	Q	Q	Q						
	RCH	T	RCH	KRB						
OBS# & ID										
1 1	0.132E-02	0.650E-06	0.200E-06	0.401E-06	0.895E-04	0.522E-03	0.323E-01	-0.390E-03	641.	-0.388E-02
	0.666E+04	-4.78	0.489E+06	0.611						
2 2	0.340E-03	0.211E-06	0.156E-06	0.468E-06	0.156E-03	0.201E-02	0.155	-0.100E-03	165.	-0.229E-02
	0.248E+04	-5.86	0.587E+06	0.630						
3 3	0.472E-03	0.275E-06	0.177E-06	0.518E-06	0.143E-03	0.143E-02	0.102	-0.139E-03	229.	-0.251E-02
	0.308E+04	-5.15	0.518E+06	0.726						
4 4	0.801E-03	0.421E-06	0.199E-06	0.502E-06	0.105E-03	0.648E-03	0.394E-01	-0.237E-03	388.	-0.298E-02
	0.451E+04	-3.44	0.353E+06	0.744						
5 5	0.206E-02	0.972E-06	0.207E-06	0.274E-06	0.583E-04	0.120E-03	0.338E-02	-0.607E-03	996.	-0.448E-02
	0.983E+04	-0.340	0.564E+05	0.455						

6	6	0.568E-04	0.112E-06	0.227E-06	0.869E-06	0.172E-03	0.779E-03	0.313E-01	-0.168E-04	27.5	-0.120E-02
		0.147E+04-0.285		0.336E+05	1.24						
7	7	0.272E-04	0.618E-07	0.101E-06	0.327E-06	0.200E-03	0.341E-02	0.257	-0.803E-05	13.2	-0.105E-02
		0.107E+04-0.443		0.485E+05	0.365						
8	8	0.284E-04	0.280E-07	0.336E-07	0.106E-06	0.656E-04	0.147E-02	0.747	-0.839E-05	13.8	-0.689E-03
		443.	-0.583	0.604E+05	0.112						
9	9	0.265E-05	0.410E-06	0.150E-05	0.378E-05	0.500E-03	0.812E-03	0.480E-04	-0.769E-06	1.28	0.609E-04
		95.2	0.735E-05	61.8	3.87						
10	10	0.306E-03	0.166E-06	0.114E-06	0.190E-06	0.310E-04	0.453E-04	0.515E-04	-0.900E-04	148.	-0.104E-03
		694.	-0.123E-03	590.	0.254						
11	11	0.109E-04	0.424E-04	0.130E-03	0.590E-03	0.567E-01	0.937E-01	0.108E-03	-0.197E-05	5.10	0.879E-01
		0.464E+04	0.731E-06	15.9	5.27						
12	12	0.115E-07	0.976E-07	0.156E-06	0.396E-06	0.438E-01	0.938	0.396E-04	-0.125E-08	0.517E-02	0.749E-04
		22.5	0.489E-08	0.289	0.189E-01						
13	13	0.517E-02	0.244E-05	0.444E-06	0.382E-06	0.103E-03	0.122E-03	0.189E-03	-0.152E-02	0.251E+04	-0.121E-02
		0.637E+04-0.498E-03		0.231E+04	1.07						
14	14	0.558E-01	0.214E-04	0.732E-06	0.302E-06	0.206E-03	0.172E-03	0.703E-04	-0.171E-01	0.266E+05	-0.153E-01
		0.329E+05-0.189E-03		871.	1.36						
15	15	0.107E-03	0.981E-06	0.423E-05	0.279E-05	0.808E-03	0.972E-03	0.182E-05	-0.307E-04	51.9	0.866E-04
		187.	-0.306E-05	14.3	6.33						
16	16	0.308E-04	0.997E-04	0.603E-03	0.135E-03	0.759E-01	0.788E-01	0.364E-04	-0.492E-05	14.5	0.134
		0.546E+04-0.152E-06		5.86	6.86						
17	17	0.126E-01	0.667E-05	0.911E-06	0.332E-06	0.197E-03	0.181E-03	0.455E-04	-0.356E-02	0.618E+04	-0.333E-02
		0.913E+04-0.122E-03		561.	1.78						
18	18	0.999E-05	0.127E-03	0.141E-03	0.133E-03	0.256	0.346	0.942E-04	-0.469E-06	4.35	0.431E-01
		0.668E+04	0.144E-06	5.03	2.28						
19	19	0.763E-01	0.275E-04	0.723E-06	0.289E-06	0.215E-03	0.173E-03	0.630E-04	-0.237E-01	0.361E+05	-0.226E-01
		0.371E+05-0.170E-03		781.	1.30						
20	20	0.488E-01	0.213E-04	0.745E-06	0.288E-06	0.216E-03	0.176E-03	0.591E-04	-0.146E-01	0.237E+05	-0.144E-01
		0.260E+05-0.159E-03		732.	1.35						
21	21	0.150E-03	0.288E-05	0.550E-05	0.131E-05	0.143E-02	0.117E-02	0.724E-06	-0.289E-04	74.2	0.104E-03
		210.	-0.889E-06	4.15	6.71						
22	22	0.362E-04	0.280E-03	0.185E-03	0.503E-04	0.115	0.754E-01	0.175E-04	0.298E-05	15.8	0.424E-01
		0.616E+04-0.856E-07		2.22	4.30						
23	23	0.139E-04	0.355E-03	0.105E-03	0.572E-04	0.398	0.269	0.301E-04	0.714E-06	5.50	0.279E-01
		0.756E+04	0.243E-07	2.09	1.67						
24	24	0.113E-06	0.352E-05	0.848E-06	0.519E-06	0.590	0.407	0.336E-06	0.573E-08	0.443E-01	0.237E-03
		88.2	0.321E-09	0.197E-01	0.138E-01						
25	25	0.202	0.622E-04	0.642E-06	0.250E-06	0.243E-03	0.173E-03	0.509E-04	-0.410	0.820E+05	-0.219E-01
		0.296E+05-0.137E-03		631.	1.00						
26	26	0.127	0.749E-04	0.572E-06	0.212E-06	0.269E-03	0.174E-03	0.373E-04	-0.266	0.553E+05	-0.148E-01
		0.191E+05-0.100E-03		462.	0.755						
27	27	0.447E-04	0.130E-03	0.283E-04	0.842E-05	0.321E-01	0.167E-01	0.310E-05	0.116E-04	18.7	0.626E-02
		0.191E+04-0.660E-07		0.613	2.85						
28	28	0.243E-04	0.717E-03	0.110E-03	0.475E-04	0.345	0.170	0.209E-04	0.233E-05	9.08	0.276E-01
		0.919E+04-0.580E-08		1.77	2.02						
29	29	0.981E-02	0.207E-03	0.175E-06	0.595E-07	0.384E-03	0.157E-03	0.122E-05	0.113E-02	0.267E+04	-0.336E-02
		0.140E+04-0.323E-05		14.9	-0.749						
30	30	0.764E-05	0.528E-03	0.271E-04	0.126E-04	0.671	0.187	0.614E-05	0.765E-06	2.68	0.675E-02
		0.438E+04-0.223E-09		0.478	0.519						
31	31	0.563	0.892E-04	0.593E-06	0.229E-06	0.258E-03	0.171E-03	0.452E-04	-1.07	0.123E+06	-0.206E-01
		0.267E+05-0.121E-03		559.	0.818						
32	32	0.425E-04	0.252E-02	0.556E-04	0.215E-04	0.275	0.911E-01	0.912E-05	0.480E-05	13.1	0.105E-01
		0.875E+04-0.210E-07		0.888	1.45						

PARAMETER VALUES AND STATISTICS FOR ALL ITERATIONS

PAR. ID.:		Q		Q		CH		CH			
		CH	T	RCH	T	RCH	T				
		RCH	KRB								
ITER										SUM OF SQUARED WEIGHTED RESIDUALS W/FLOWS W/PARAMS	DMX PAR# AMP OR AGMX
		0.450E+02	0.420E+03-0.970E+05-0.510E+05	0.104E+02	0.480E+01	0.510E+01	0.700E+02	0.400E-03	0.420E+03-0.200E-03	0.150E+02	
		0.170E-03	0.800E-01								
1		0.877E+02	0.875E+03-0.969E+05-0.511E+05	0.102E+02	0.514E+01	0.522E+01	0.676E+02	0.298E-03	0.479E+03-0.140E-03	0.133E+02	702. 702. 702. 1.08 2 0.000
		0.133E-03	0.805E-01								
2		0.841E+02	0.938E+03-0.969E+05-0.510E+05	0.102E+02	0.514E+01	0.522E+01	0.663E+02	0.298E-03	0.487E+03-0.127E-03	0.129E+02	31.1 31.1 33.4 0.907E-01 11 0.000
		0.131E-03	0.805E-01								
3		0.843E+02	0.941E+03-0.969E+05-0.510E+05	0.102E+02	0.514E+01	0.522E+01	0.664E+02	0.298E-03	0.488E+03-0.128E-03	0.129E+02	24.1 24.1 26.7 0.355E-02 2 0.100E-02
		0.131E-03	0.805E-01								
4											24.1 24.1 26.7 -0.521E-02 11 0.000

0.845E+02 0.944E+03-0.969E+05-0.510E+05 0.102E+02 0.514E+01  
0.522E+01 0.665E+02 0.299E-03 0.488E+03-0.128E-03 0.129E+02  
0.131E-03 0.805E-01

5 24.1 24.1 26.7 -0.518E-04 1 0.000  
0.845E+02 0.944E+03-0.969E+05-0.510E+05 0.102E+02 0.514E+01  
0.522E+01 0.665E+02 0.299E-03 0.488E+03-0.128E-03 0.129E+02  
0.131E-03 0.805E-01

6 24.1 24.1 26.7

# COVARIANCE MAT.

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	1 10	2 11	3 12	4 13	5 14	6	7	8	9
1	622.988 94.0038	5524.23 -1.528137E-03	-1340.21 35.7137	-105.164 3.649065E-04	3.90627 1.406541E-03	0.496596	-0.126735	381.153	8.333315E-04
2	5524.23 904.322	230069. -1.977631E-02	-28512.0 475.420	7780.00 4.853034E-03	-50.6715 6.535410E-03	4.50571	-1.72681	3897.63	1.283299E-02
3	-1340.21 -12143.8	-28512.0 -7.155699E-05	3.186814E+06 -121.348	261081. -1.266235E-03	3.75333 -7.862717E-03	5.06365	-0.646858	-1071.27	-5.194813E-03
4	-105.164 -3211.41	7780.00 -9.208089E-04	261081. -11.8393	887290. -1.284579E-04	6.01000 -9.760942E-03	-1.81634	-0.274024	-107.957	-8.064179E-04
5	3.90627 7.942402E-02	-50.6715 -1.411267E-05	3.75333 0.332923	6.01000 3.397347E-06	0.600486 2.011733E-05	-4.803833E-02	-1.251545E-03	2.75140	9.127029E-06
6	0.496596 -0.105960	4.50571 -1.845650E-06	5.06365 4.229291E-02	-1.81634 4.308881E-07	-4.803833E-02 2.635596E-06	0.183722	-2.487270E-04	0.348475	1.132305E-06
7	-0.126735 -2.139092E-02	-1.72681 4.717472E-07	-0.646858 -3.331387E-02	-0.274024 -3.848981E-07	-1.251545E-03 -2.301360E-06	-2.487270E-04	0.222355	-8.989228E-02	-3.041467E-07
8	381.153 67.2651	3897.63 -1.078880E-03	-1071.27 25.2922	-107.957 2.584176E-04	2.75140 9.509675E-04	0.348475	-8.989228E-02	250.937	6.786562E-04
9	8.333315E-04 2.356624E-04	1.283299E-02 -3.588451E-09	-5.194813E-03 8.515101E-05	-8.064179E-04 8.699049E-10	9.127029E-06 2.887065E-09	1.132305E-06	-3.041467E-07	6.786562E-04	2.821650E-09
10	94.0038 103.111	904.322 -2.995447E-04	-12143.8 8.09422	-3211.41 8.283317E-05	7.942402E-02 -2.982097E-03	-0.105960	-2.139092E-02	67.2651	2.356624E-04
11	-1.528137E-03 -2.995447E-04	-1.977631E-02 5.429574E-09	-7.155699E-05 -1.308984E-04	-9.208089E-04 -1.336331E-09	-1.411267E-05 -9.115427E-09	-1.845650E-06	4.717472E-07	-1.078880E-03	-3.588451E-09
12	35.7137 8.09422	475.420 -1.308984E-04	-121.348 13.2751	-11.8393 1.320840E-04	0.332923 6.746671E-05	4.229291E-02	-3.331387E-02	25.2922	8.515101E-05
13	3.649065E-04 8.283317E-05	4.853034E-03 -1.336331E-09	-1.266235E-03 1.320840E-04	-1.284579E-04 1.315503E-09	3.397347E-06 6.344654E-10	4.308881E-07	-3.848981E-07	2.584176E-04	8.699049E-10
14	1.406541E-03 -2.982097E-03	6.535410E-03 -9.115427E-09	-7.862717E-03 6.746671E-05	-9.760942E-03 6.344654E-10	2.011733E-05 6.287817E-05	2.635596E-06	-2.301360E-06	9.509675E-04	2.887065E-09

# SCALED W PARAM.

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	1 10	2 11	3 12	4 13	5 14	6	7	8	9
1	8.726616E-02 2.281394E-03	6.928034E-02 0.140934	1.637485E-04 3.273533E-02	2.438341E-05 3.292082E-02	4.551128E-03 2.069003E-04	1.142886E-03	-2.872042E-04	6.781410E-02	3.301548E-02
2	6.928034E-02 1.964946E-03	0.258327 0.163295	3.118931E-04 3.901500E-02	-1.615028E-04 3.919896E-02	-5.285584E-03 8.607042E-05	9.284002E-04	-3.503580E-04	6.208591E-02	4.551978E-02
3	1.637485E-04 2.570676E-04	3.118931E-04 -5.756337E-06	3.396261E-04 9.701839E-05	5.280108E-05 9.964198E-05	-3.814278E-06 1.008835E-06	-1.016488E-05	1.278625E-06	1.662492E-04	1.795183E-04
4	2.438341E-05 1.290069E-04	-1.615028E-04 -1.405681E-04	5.280108E-05 1.796263E-05	3.405307E-04 1.918279E-05	-1.159027E-05 2.376636E-06	6.919265E-06	1.027890E-06	3.179325E-05	5.288373E-05
5	4.551128E-03 1.603235E-05	-5.285584E-03 1.082566E-02	-3.814278E-06 2.538144E-03	-1.159027E-05 2.549289E-03	5.819019E-03 2.461328E-05	-9.195552E-04	-2.359024E-05	4.071598E-03	3.007597E-03
6	1.142886E-03 -4.225052E-05	9.284002E-04 2.796647E-03	-1.016488E-05 6.369171E-04	6.919265E-06 6.386850E-04	-9.195552E-04 6.369730E-06	6.946954E-03	-9.260868E-06	1.018651E-03	7.370496E-04
7	-2.872042E-04 -8.398732E-06	-3.503580E-04 -7.038719E-04	1.278625E-06 -4.940107E-04	1.027890E-06 -5.617770E-04	-2.359024E-05 -5.476746E-06	-9.260868E-06	8.152138E-03	-2.587449E-04	-1.949450E-04
8	6.781410E-02 2.073473E-03	6.208591E-02 0.126381	1.662492E-04 2.944575E-02	3.79325E-05 2.961181E-02	4.071598E-03 1.776758E-04	1.018651E-03	-2.587449E-04	5.670717E-02	3.415100E-02
9	3.301548E-02 1.617629E-03	4.551978E-02 9.360425E-02	1.795183E-04 2.207524E-02	5.288373E-05 2.219700E-02	3.007597E-03 1.201155E-04	7.370496E-04	-1.949450E-04	3.415100E-02	3.161815E-02
10	2.281394E-03 4.335577E-04	0.163295 4.786360E-03	-5.756337E-06 1.285423E-03	2.207524E-02 1.294738E-03	1.201155E-04 -7.600099E-05	-4.225052E-05	-8.398732E-06	2.073473E-03	1.617629E-03
11	0.140934 4.786360E-03	0.163295 0.329693	-5.756337E-06 7.899597E-02	-1.405681E-04 7.937643E-02	1.082566E-02 8.828246E-04	2.796647E-03	-7.038719E-04	0.126381	9.360425E-02
12	3.273533E-02 1.285423E-03	3.901500E-02 7.899597E-02	9.701839E-05 7.962216E-02	1.796263E-05 7.797490E-02	2.538144E-03 6.494026E-05	6.369171E-04	-4.940107E-04	2.944575E-02	2.207524E-02
13	3.292082E-02 1.294738E-03	3.19896E-02 7.937643E-02	9.964198E-05 7.797490E-02	1.918279E-05 7.643698E-02	2.549289E-03 6.010898E-05	6.386850E-04	-5.617770E-04	2.961181E-02	2.219700E-02
14	2.069003E-04 -7.600099E-05	8.607042E-05 8.828246E-04	1.008835E-06 6.494026E-05	2.376636E-06 6.010898E-05	2.461328E-05 9.712951E-03	6.369730E-06	-5.476746E-06	1.776758E-04	1.201155E-04

# EIGENVALUES

0.2993D-04	0.7148D-04	0.9311D-04	0.2980D-03	0.6162D-03	0.3569D-02	0.4472D-02	0.7345D-02
0.8149D-02	0.9715D-02	0.2928D-01	0.1054D+00	0.1538D+00	0.6286D+00		

# EIGENVECTORS

Q	0.2156D-02	0.2140D+00	0.4440D+00	0.1329D-01	-0.5931D-01	0.1954D-01	0.7809D-02	0.1124D-02
	-0.2747D-03	0.5430D-02	-0.7625D+00	0.2255D+00	0.1519D+00	-0.3123D+00		
Q	-0.2593D-04	-0.3277D-02	0.3392D-02	-0.8954D-03	-0.1619D-02	-0.2682D-01	0.5211D-01	0.2128D-01
	0.6188D-04	0.1480D-02	-0.3910D-01	-0.2254D+00	-0.8466D+00	-0.4765D+00		
Q	0.4347D-02	0.5516D+00	-0.3639D+00	0.4317D+00	-0.6093D+00	-0.7195D-01	-0.1933D-01	0.1893D-02
	0.2973D-03	-0.7654D-03	-0.4497D-02	-0.1055D-02	-0.9749D-03	-0.5070D-03		
Q	0.1360D-02	0.1873D+00	-0.1173D+00	-0.8936D+00	-0.3888D+00	-0.3578D-01	-0.1319D-01	-0.1804D-02
	0.1571D-03	-0.1950D-03	-0.2124D-02	-0.1510D-03	0.7826D-03	0.2212D-03		
CH	-0.2149D-03	-0.2487D-01	0.1534D-01	0.1031D-02	-0.2421D-01	-0.2861D+00	0.8761D+00	0.3761D+00
	0.7454D-03	-0.3828D-02	0.3640D-01	0.3541D-01	0.6978D-01	-0.1466D-01		
CH	-0.2389D-04	-0.1071D-01	0.6527D-02	0.3285D-02	-0.1202D-01	-0.1148D+00	0.3586D+00	-0.9262D+00
	-0.3585D-02	0.1925D-02	0.5385D-02	0.3751D-02	0.4348D-02	-0.5475D-02		
CH	0.6726D-02	-0.1058D-03	-0.2123D-05	-0.4178D-05	0.2643D-03	0.1099D-02	0.1090D-02	-0.3599D-02
	0.1000D+01	-0.3007D-02	-0.3393D-03	0.3847D-02	-0.1968D-02	0.1721D-02		
T	-0.2187D-02	-0.3108D+00	-0.6619D+00	-0.2512D-01	0.1557D+00	-0.4487D+00	-0.1469D+00	-0.3329D-02
	0.4864D-03	-0.1084D-01	-0.3090D+00	0.1757D+00	0.1253D+00	-0.2745D+00		
RCH	0.2708D-02	0.2043D+00	0.4011D+00	0.4817D-02	0.4004D-01	-0.7262D+00	-0.2627D+00	-0.7733D-02
	0.1256D-02	-0.2914D-01	0.3852D+00	0.8307D-01	0.7609D-01	-0.1931D+00		
T	-0.2249D-01	-0.6892D+00	0.2328D+00	0.1194D+00	-0.6678D+00	-0.7227D-01	-0.6754D-01	0.1599D-02
	0.3965D-03	-0.1035D-01	0.5790D-03	0.4956D-02	0.7267D-02	-0.1014D-01		
RCH	-0.6183D-02	-0.1785D-01	-0.5594D-01	0.9147D-03	-0.3554D-01	0.4030D+00	0.7278D-01	-0.1240D-01
	0.1430D-03	0.6614D-02	0.4100D+00	0.3210D+00	0.2767D+00	-0.6926D+00		
T	-0.6967D+00	0.1445D-01	-0.1681D-02	-0.1505D-02	0.1040D-01	-0.9941D-02	-0.1541D-02	0.4705D-04
	0.8000D-02	0.1620D-02	-0.4501D-01	-0.6249D+00	0.2832D+00	-0.2036D+00		
RCH	0.7170D+00	-0.1380D-01	0.2748D-02	0.1232D-02	-0.6219D-02	-0.6709D-02	-0.2053D-02	0.1106D-03
	-0.1602D-02	0.5999D-03	-0.4025D-01	-0.6048D+00	0.2774D+00	-0.2033D+00		
KRB	0.5731D-03	-0.5223D-02	0.4626D-02	0.1183D-02	-0.4126D-02	-0.3044D-01	-0.7900D-02	0.3014D-02
	0.3053D-02	0.9994D+00	0.9595D-02	0.2878D-02	0.1878D-02	-0.1315D-02		

# PARAMETER SUMMARY

PARAMETER # :	1	2	3	4	5	6	7	8	9	10
	11	12	13	14						
PARAMETER ID :	Q	Q	Q	Q	CH	CH	CH	T	RCH	T
	RCH	T	RCH	KRB						
FINAL VALUES	0.845E+02	0.944E+03	-0.969E+05	-0.510E+05	0.102E+02	0.514E+01	0.522E+01	0.665E+02	0.299E-03	0.488E+03
	-0.128E-03	0.129E+02	0.131E-03	0.805E-01						
STD. DEV.	0.250E+02	0.480E+03	0.179E+04	0.942E+03	0.775E+00	0.429E+00	0.472E+00	0.158E+02	0.531E-04	0.102E+02
	0.737E-04	0.364E+01	0.363E-04	0.793E-02						
COEF. OF VAR.	0.295E+00	0.508E+00	0.184E-01	0.185E-01	0.763E-01	0.833E-01	0.903E-01	0.238E+00	0.178E+00	0.208E-01
	0.574E+00	0.282E+00	0.276E+00	0.986E-01						
+ 2 STD. DEV.	0.134E+03	0.190E+04	-0.933E+05	-0.492E+05	0.117E+02	0.600E+01	0.617E+01	0.982E+02	0.405E-03	0.508E+03
	0.190E-04	0.202E+02	0.204E-03	0.963E-01						
- 2 STD. DEV.	0.346E+02	-0.156E+02	-0.100E+06	-0.529E+05	0.861E+01	0.429E+01	0.428E+01	0.348E+02	0.192E-03	0.467E+03
	-0.276E-03	0.563E+01	0.586E-04	0.646E-01						

# CORRELATION MAT.

	1	2	3	4	5	6	7	8	9
	10	11	12	13	14				
1	1.00000	0.461426	-3.007835E-02	-4.472944E-03	0.201963	4.641762E-02	-1.076793E-02	0.964002	0.628531
	0.370897	-0.830883	0.392714	0.403084	7.106612E-03				
2	0.461426	1.00000	-3.329819E-02	1.721937E-02	-0.136328	2.191560E-02	-7.634695E-03	0.512967	0.503671
	0.185670	-0.559543	0.272038	0.278958	1.718279E-03				
3	-3.007835E-02	-3.329819E-02	1.00000	0.155262	2.713232E-03	6.617659E-03	-7.684345E-04	-3.788263E-02	-5.478226E-02
	-0.669921	-5.439898E-04	-1.865678E-02	-1.955645E-02	-5.554490E-04				
4	-4.472944E-03	1.721937E-02	0.155262	1.00000	8.233614E-03	-4.498675E-03	-6.169253E-04	-7.234989E-03	-1.611669E-02
	-0.335747	-1.326642E-02	-3.449648E-03	-3.759949E-03	-1.306799E-03				
5	0.201963	-0.136328	2.713232E-03	8.233614E-03	1.00000	-0.144629	-3.425088E-03	0.224141	0.221731
	1.009366E-02	-0.247158	0.117916	0.120877	3.273927E-03				
6	4.641762E-02	2.191560E-02	6.617659E-03	-4.498675E-03	-0.144629	1.00000	-1.230605E-03	5.132265E-02	4.973147E-02
	-2.434509E-02	-5.843670E-02	2.708125E-02	2.771646E-02	7.754400E-04				
7	-1.076793E-02	-7.634695E-03	-7.684345E-04	-6.169253E-04	-3.425088E-03	-1.230605E-03	1.00000	-1.203419E-02	-1.214250E-02
	-4.467396E-03	1.357698E-02	-1.939026E-02	-2.250487E-02	-6.154762E-04				
8	0.964002	0.512967	-3.788263E-02	-7.234989E-03	0.224141	5.132265E-02	-1.203419E-02	1.00000	0.806522
	0.418173	-0.924290	0.438214	0.449774	7.570660E-03				
9	0.628531	0.503671	-5.478226E-02	-1.611669E-02	0.221731	4.973147E-02	-1.214250E-02	0.806522	1.00000
	0.436905	-0.916796	0.439967	0.451517	6.854173E-03				
10	0.370897	0.185670	-0.669921	-0.335747	1.009366E-02	-2.434509E-02	-4.467396E-03	0.418173	0.436905
	1.00000	-0.400338	0.218779	0.224909	-3.703567E-02				
11	-0.830883	-0.559543	-5.439898E-04	-1.326642E-02	-0.247158	-5.843670E-02	1.357698E-02	-0.924290	-0.916796
	-0.400338	1.00000	-0.487566	-0.500017	-1.560070E-02				
12	0.392714	0.272038	-1.865678E-02	-3.449648E-03	0.117916	2.708125E-02	-1.939026E-02	0.438214	0.439967
	0.218779	-0.487566	1.00000	0.999508	2.335186E-03				
13	0.403084	0.278958	-1.955645E-02	-3.759949E-03	0.120877	2.771646E-02	-2.250487E-02	0.449774	0.451517
	0.224909	-0.500017	0.999508	1.00000	2.206033E-03				
14	7.106612E-03	1.718279E-03	-5.554490E-04	-1.306799E-03	3.273927E-03	7.754400E-04	-6.154762E-04	7.570660E-03	6.854173E-03
	-3.703567E-02	-1.560070E-02	2.335186E-03	2.206033E-03	1.00000				

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS >= .95

PARAMETER #	ID	#	ID	CORRELATION
1	Q	8	T	0.96
12	T	13	RCH	1.00

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS BETWEEN .90 AND .95

PARAMETER #	ID	#	ID	CORRELATION
8	T	11	RCH	-0.92
9	RCH	11	RCH	-0.92

THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS BETWEEN .85 AND .90

PARAMETER #	ID	#	ID	CORRELATION
-------------	----	---	----	-------------

RSQ (DEP.VAR. ONLY)----- = 24.146  
 RSQ (W/PARAMETERS)----- = 26.717  
 CALCULATED ERROR VARIANCE = 0.98952  
 CORRELATION COEFFICIENT-- = 0.99961  
 W/PARAMETERS----- = 0.99966  
 ITERATIONS----- = 5

MAX LIKE OBJ FUNC = 89.711  
 AIC STATISTIC---- = 117.71  
 BIC STATISTIC---- = 141.70

ORDERED DEPENDENT-VARIABLE WEIGHTED RESIDUALS

NUMBER OF RESIDUALS INCLUDED: 32

-2.50	-1.44	-1.43	-1.31	-1.14	-1.02	-0.762	-0.597
-0.541	-0.454	-0.444	-0.441	-0.438	-0.380	-0.220	-0.844E-01
-0.591E-01	-0.585E-01	-0.491E-01	0.161	0.292	0.334	0.335	0.366
0.394	0.786	0.824	0.825	1.03	1.04	1.06	1.28

CORRELATION BETWEEN ORDERED WEIGHTED RESIDUALS AND INDEPENDENT NORMAL DEVIATES = 0.967

ORDERED WEIGHTED RESIDUALS

NUMBER OF RESIDUALS INCLUDED: 41

-2.50	-1.44	-1.43	-1.31	-1.14	-1.02	-0.806	-0.762
-0.714	-0.597	-0.541	-0.454	-0.444	-0.441	-0.438	-0.380
-0.240	-0.220	-0.844E-01	-0.683E-01	-0.591E-01	-0.585E-01	-0.574E-01	-0.491E-01
0.443E-01	0.161	0.232	0.292	0.334	0.335	0.366	0.394
0.761	0.786	0.824	0.825	0.844	1.03	1.04	1.06
1.28							

CORRELATION BETWEEN ORDERED WEIGHTED RESIDUALS AND INDEPENDENT NORMAL DEVIATES = 0.969

## APPENDIX B: GETTING STARTED AND RESOLVING PROBLEMS

### Compiling and Loading MODFLOWP

MAIN of MODFLOW (McDonald and Harbaugh, 1988, p. 3-32) was changed substantially for MODFLOWP; a description of the changes and the code are presented in Appendix C. The main of MODFLOWP presented in this report includes call statements for Prudic's (1989) Streamflow-Routing Package and Hill's (1990b) PCG2 Package. The user needs to include these packages when compiling the program, or eliminate the call statements of any missing package.

The following six primary modules and one submodule from MODFLOW were modified for MODFLOWP: BAS1OT, BCF1RP, BCF1FM, RIV1FM, EVT1FM, DRN1FM, and SBCF1H. In addition, STR1FM from the Streamflow-Routing Package was modified. Although in most instances the modifications are minor, problems and confusion probably best can be avoided by eliminating these subroutines from an existing version of MODFLOW and by adding the versions presented in Appendix C. Usually this procedure is unnecessary, however, because the unchanged primary modules and submodules are included in distributed versions of MODFLOWP.

The program presented in this report used the IUNIT positions used in McDonald and Harbaugh (1988) for their packages, IUNIT(18) is used for the Streamflow-Routing Package, IUNIT(13) is used for the PCG2 Package, and IUNIT(15) is used for the Parameter-Estimation Package. To modify these, change references to IUNIT in MAIN, SEN1RW, SEN1RR, and SSEN1G (see Appendix C).

After substituting the new versions of MAIN and the primary modules and submodule discussed above and in Appendix C, including the FORTRAN of the new modules and submodules presented in Appendix C, adjusting the IUNIT positions, and allocating sufficient space in the X, PID, and DID arrays (see next section), the model can be compiled and loaded as usual, with the following exception. New submodule SPAR1E includes calls to subroutine DE2CSF and function DEPISF from IMSL (1987). If this library is available, it needs to be included when loading the program. If this library is not available, the statements in SPAR1E which include DE2CSF and DEPISF need to be commented out or deleted, and LPRINT of DATA SET 13 of the INPUT FILE cannot equal 1.

### Space Requirements

In addition to the X-array, which includes space for all real and integer numbers used by MODFLOWP, the Parameter-Estimation Package uses two character arrays. These arrays are all dimensioned in the beginning of MAIN.

The X-array space needed by MODFLOWP without the Parameter-Estimation Package is the same as that needed by MODFLOW, as discussed by McDonald and Harbaugh (1988, Appendix B). To use the Parameter-Estimation Package, X-array storage needs to be increased as follows:

[NODES=NROW×NCOL×NLAY; see the data entry instructions for LINES 3, 5, and 6 of the the INPUT FILE or the listing of variables in Appendix C for the definitions of all other variable names]

A.  $2 \times \text{NODES} + 2 + (4 + \text{NLLI1}) \times \text{NP} + (\text{NMM} + \text{NZM}) \times \text{NROW} \times \text{NCOL} + 2 + 13 \times \text{NH} + \text{MAXM} \times \text{MOBS} + 4 \times \text{NQ} + \text{NQT} + 4 \times \text{NQC} + (\text{NP} + 4) \times (\text{NH} + \text{NQT}) + \text{NSM} \times (3 + \text{LZI1}) + 4 \times \text{NSN} + \text{NRWD} + \text{NZER} + \text{NPNG}.$

B. If  $\text{NPER} > 0$  (NPER is specified in the Basic Package input file), the following additional X-array storage is needed:

$$(2 \times \text{NPER}) - 1.$$

C. If  $\text{IPAR} > 0$  and  $\text{ISN} > 0$  (the gradient is calculated using adjoint states), the following additional X-array storage is needed:

$$3 \times (\text{NPER} + 1) + 2 \times \text{NP}.$$

If  $\text{IPAR} > 0$  and  $\text{ISN} < 0$  (sensitivity-equation sensitivities are calculated) and  $\text{NPER} > 0$ , the following additional X-array storage is needed:

NODES

D. If  $\text{IPAR} = 1$ , parameter estimation is performed and the following additional X-array storage is needed:

$$(5 + \text{MPR}) \times \text{NP} + (\text{NP} + 1) \times \text{MPR}.$$

If  $\text{ISN} < 0$  or  $\text{ISN} = 4$  (the variance-covariance matrix is calculated), the following additional X-array storage is needed:

$$2 \times \text{NP}^2 + 2 \times \text{NP}.$$

If  $\text{ISN} = 1$  (quasi-Newton conjugate-direction iterations are used), the following additional X-array storage is needed:

$$\text{NP}^2 + \text{NP} + 2.$$

If  $\text{ISN} > 0$  (a conjugate-direction optimization method is used), the following additional X-array storage is needed:

$$\text{NP} + 2 \times (\text{NH} + \text{NQT}) + 2 \times \text{NP}.$$

If the top model layer is a water-table layer and there is more than one layer in the model, the following additional X-array storage is needed:

NROW×NCOL.

The two character arrays are named PID and DID and are dimensioned in the beginning of MAIN. PID needs to be dimensioned to NP (LINE 3) or greater; DID needs to be dimensioned to NH+NQT (LINE 5) or greater. On some computers, failure to provide sufficient space in these arrays causes integer constants, such as IOUT or LCname (see "List of Variables" in Appendix C) to be changed to very large negative or positive values while executing the program.

#### Adapting the Residual Analysis Program for use with the Parameter-Estimation Package

To perform graphical analyses of weighted residuals (see section "Analysis of Results for Linear Problems"), realizations from the probability distribution function  $N(\underline{0}, (\underline{I} - \underline{X}(\underline{X}^T \underline{W} \underline{X})^{-1} \underline{X}^T \underline{W})\sigma^2)$  are needed. Such realizations can be produced by RESAN, a program presented by Cooley and Naff (1990, p. 176-183). The Parameter-Estimation Package can produce output that is compatible with a slightly modified version of RESAN, RESAN.MODP. In RESAN.MODP, the variance-covariance matrix on the parameters, the weights, and the sensitivities are read from a formatted instead of an unformatted file by making the following changes in the residual analysis program of Cooley and Naff (1990, p. 176-183).

- (1) Add after format statement 16:  
500 FORMAT (6F13.0)
- (2) Change: READ(ITB) (C(I,J),I=J,NVAR)  
To: READ(ITB,500) (C(I,J),I=J,NVAR)
- (3) Change: READ(ITB) (W(I),I=1,NOBS)  
To: READ(ITB,20) (W(I),I=1,NOBS)
- (4) Change: READ(ITB) (X(I,J),I=1,NVAR)  
To: READ(ITB,20) (X(I,J),I=1,NVAR)



In addition, the following changes can be made to avoid having to change dimensions of the program in multiple places when a larger or smaller problem is considered:

- (1) Add before the first DIMENSION statement:

PARAMETER (NP=20, ND=70)

- (2) Change first DIMENSION statement from:

DIMENSION X(20,20), COV(20,20), W(20), WP(20),  
IPR(20), R(90,90), D(90), G(90), F(90)

To:

DIMENSION X(NP,NP), COV(NP,NP), W(NP), WP(NP),  
IPR(NP), R(ND+NP, ND+NP), D(ND+NP), G(ND+NP), F(ND+NP)

- (3) Change: NVD=20

NTD=70

To: NVD=NP

NTD=ND

Then, to change the dimensions of RESAN.MODP, just change NP and ND in the PARAMENTER statement so that they are at least as large as NP and NH+NQT of LINES 3 and 5 of the INPUT FILE of the problem considered.

#### Common Problems

1. Problem: Overshoot of a parameter to a very small absolute value.

Discussion: In the iteration after the overshoot, the regression routine might try to increase the absolute value of the parameter, but the calculated fractional change is huge because the absolute value of the parameter is so small. To respect the DMAX (DATA SET 13) limit on the maximum fractional change for any iteration, all changes are scaled by a small number by making AP ( $\rho_r$  of eq. 50b) small, and little improvement occurs in the sum of squared residuals (RSQ). (The value of AP is printed for each parameter-estimation iteration; values of RSQ are printed in a table at the end of the simulation.)

Resolution: Make the initial parameter value of the overshoot parameter smaller in absolute value.

2. Problem: Lack of convergence of parameters that have relatively small scaled sensitivity-equation sensitivities (printed when  $ISN < 0$  and  $ISCALS \neq 0$ ; see LINE 6 of the INPUT FILE) or scaled gradient of the objective function (the gradient is printed; scale by multiplying by the parameter value).

Discussion: The parameter(s) that cause the lack of convergence of parameter estimation is(are) generally the parameter(s) for which the maximum fractional change (printed for each parameter-estimation iteration) is calculated in latter parameter-estimation iterations. Inspection indicates that these parameters are associated with relatively small scaled sensitivity-equation sensitivities or gradient of the objective function.

Resolution: Modified Gauss-Newton optimization with quasi-Newton updating, activated using NOPT of LINE 6 and NFIT of DATA SET 13, sometimes can solve these problems more effectively than the other methods. Alternatively, this situation was successfully resolved by R.M. Yager (U.S. Geological Survey, oral commun., 1990) by executing two runs of the parameter-estimation routine using modified Gauss-Newton optimization. In the first run, the relatively insensitive parameters were set to reasonable values, and only the relatively sensitive parameters were estimated. The resulting parameter estimates were used as initial estimates for the relatively sensitive parameters in the second run of the parameter-estimation program, in which all the parameters were estimated. This was accomplished conveniently by including the insensitive parameters in the last repetitions of DATA SET 2 and making IWPG of DATA SET 9 negative for these parameters for the first run. The IWPG values were changed to positive values for the second run. If these procedures are unsuccessful, consider reparameterizing to produce parameters that are more sensitive; see the section "Parameterization" in the main text of this report.

3. Problem: Parameter estimates are unreasonable (see item 1 in this section if the unreasonable parameter value is small in absolute value).

Discussion: Unrealistic parameter estimates can be produced if (a) there are inconsistencies between the dependent-variable data and the way the model is constructed or parameterized, or (b) the calculated values ( $\hat{y}$ ) related to the dependent-variable observations ( $y$ ) are insensitive to the estimated parameters.

Resolution: For (a), evaluate the calculated weighted and unweighted residuals and the scaled sensitivity-equation sensitivities (ISN>0; LINE 6 of the INPUT FILE). The dependent-variable observations that are most influential in producing unrealistic parameter estimates generally are associated with large weighted residuals and large scaled sensitivity-equation sensitivities for the parameter considered. Once these data are identified, evaluate the data, their weights, the model construction, and the parameterization for inconsistencies (see section "Adjustments Commonly Required During Parameter Estimation"). Make appropriate changes and try estimating the parameters again.

For (b), If the scaled sensitivity-equation sensitivities for a parameter are all small, reparameterize to produce parameters with larger sensitivities. This generally is accomplished by decreasing the number of parameters. Alternatively, prior information can be used to maintain parameters at reasonable values.

4. Problem: The solver does not function satisfactorily when calculating hydraulic heads, sensitivity-equation sensitivities, adjoint states, or the derivative of hydraulic head with respect to the iteration parameter of Newton's method. For iterative solvers, convergence is not reached in a reasonable number of iterations, execution is terminated, and an error message is printed, or there are unacceptably large errors (generally greater than 1 percent) in the volumetric budgets for the entire model. For direct solvers, excessive round-off errors produce an inaccurate solution, producing large errors in the volumetric budgets for the entire model.

Discussion: Parameter estimates in initial or subsequent parameter-estimation iterations can produce problems that are too difficult for most solvers. This difficulty happens most commonly when horizontal or vertical hydraulic-conductivity values in adjacent finite-difference cells are too different. For example, R.M. Yager (oral commun., 1990) had difficulty with Hill's (1990b) conjugate-gradient solver preconditioned with a modified incomplete Cholesky preconditioner when adjacent horizontal hydraulic-conductivity values differed by five orders of magnitude.

Resolution: Resolution depends on whether the problem occurs on the first or subsequent parameter-estimation iterations, and whether it occurs when calculating hydraulic heads or other quantities. The possibilities and suggested resolutions are as follows:

- (A) Solver problems occur for the first parameter-estimation iteration.

Resolution: Change the initial parameter estimates.

- (B) Solver problems occur for quantities other than hydraulic head for subsequent parameter-estimation iterations.

- (a) The parameter values are unreasonable.

Resolution: See item 3 of this section.

- (b) The parameter values are reasonable.

Resolution: Try changing how the solver is used. For example, consider changes in convergence criteria or other user-defined parameters. If problems persist, try improving the calibration by trial and error, using the Parameter-Estimation Package to easily change parameter values and provide information on the residuals. Attempt to use the Parameter-Estimation Package again after the model calibration has been improved.

- (C) Solver problems occur for hydraulic heads for subsequent parameter-estimation iterations.

- (a) The parameter values are unreasonable.

Resolution: See item 3 of this section.

- (b) The parameter values are reasonable. This can occur, for example, if a fracture is being represented by a few rows or columns of a finite-difference grid, and the estimated hydraulic conductivity along the fracture is so much greater than the surrounding material that solver performance is adversely affected.

Resolution: First, consider using another solver; PCG2 (Hill, 1990b) or another preconditioned conjugate-gradient solver probably are most effective. Increasing the convergence criteria might allow the solver to converge, but check the errors in the volumetric budgets of the entire model to ensure that the solution is sufficiently accurate.

If changes to the solver do not work, another model needs to be considered. In the situation described above, an analytical or numerical model designed to represent flow through fractures needs to be considered. Parameter estimation probably will need to be accomplished by trial and error.

5. Problem: Sum-of-squared weighted residuals increases from one parameter-estimation iteration to the next.

Discussion:

- (a) The sum-of-squared weighted residuals can increase when using the modified Gauss-Newton optimization because of overshoot. Overshoot occurs when the optimization procedure goes past the parameter values associated with the small value of the objective function for which it was aiming to parameter values associated with a large value of the objective function (fig. 17).
- (b) The sum-of-squared weighted residuals also can increase because of problems 1 and 3 discussed above, in which case the reader is referred to those discussions. Alternatively, the increase might indicate that observations that had been omitted are included (see section "Omitted Observations"). If the weighted residual of these observations is large, their alternating omission and inclusion can cause the sum of squared weighted residuals to fluctuate and to inhibit the convergence of parameter estimation.

Resolution: If the sum-of-squared weighted residuals increases for only a few iterations and the increase is small, no action is required. More persistent problems can be addressed by reducing the maximum fractional parameter change (DMAX of DATA SET 13). Note that  $DMAX \leq 1.0$  prohibits parameter values from changing sign.

Additional techniques for addressing 5.b were discussed in the section "Omitted Observations."

### Restarting the Parameter-Estimation Routine

The parameter-estimation routine is restarted when estimated parameter values from one run are used as the initial parameter values in a subsequent run. A user might wish to restart a run if, for example, a parameter value becomes physically unreasonable. If the value is first unreasonable in the fifth parameter-estimation iteration, parameter values from the fourth iteration can be used to restart the run. See the preceding section entitled "Common Problems" for suggestions on how the restarted run could differ from the original run so that physically reasonable values are maintained.

The parameter estimates from each iteration of the parameter-estimation routine are saved on the output unit specified as IOUB on LINE 7 of the INPUT FILE, as discussed in the section "Parameter Values for Restarting Parameter Estimation." These values are printed to be compatible with the input format required for initial parameter values, and can be used to produce DATA SET 8 of the INPUT FILE for the restarted run.

When prior estimates of the parameters are specified by using DATA SET 10 of the INPUT FILE, the initial values are used as the prior estimates. When the parameter-estimation routine is restarted, the new initial values rarely equal the original initial values. To preserve the original prior estimates, specify them using repetitions of DATA SET 12. For example, to represent prior on the  $I$ th parameter using DATA SET 12, set  $PRM(I)$  equal to 1.0,  $PRM(J)$ ,  $J \neq I$ , equal to 0.0, and  $PRM(NP+1)$  equal to the prior estimate of the parameter. WP of DATA SET 12 needs to equal the old value of WP(I) of DATA SET 10, and WP(I) of DATA SET 10 needs to be set to zero.

Parameters also can be added or eliminated when restarting the parameter-estimation routine. This addition or deletion is accomplished by (1) adding or deleting negative values in DATA SET 9, or by (2) adding or subtracting appropriate repetitions of DATA SETS 2 and 2A or 2B. If the first method is used, remember that negative group numbers must follow all positive group numbers, and that the repetitions of DATA SET 2 may need to be rearranged. If the second method is used, add or eliminate numbers in DATA SETS 9, 10, and 12, and change the values on LINE 3, as needed.

### Reducing Computer-Execution Time of Modified Gauss-Newton Optimization

Early iterations of modified Gauss-Newton optimization do not need hydraulic heads and sensitivities to be calculated accurately because inaccurate values still can produce substantial improvements in the estimated parameters. Accurate values, of course, are needed as the optimum parameter values are approached. When an iterative solver, such as PCG2 (Hill, 1990b) is used, larger solver convergence criteria can be used in the early parameter-estimation iterations to decrease the number of solver iterations and, thus, save computer time. Smaller convergence criteria needs to be used as the final parameter estimates are approached.

In this report, this change in solver convergence criteria is implemented with the user-specified variables FCONV and TOL (DATA SET 13), and the internally calculated variables AP and ADMX. FCONV is used to control the size of the solver convergence criteria for the first parameter-estimation iteration; TOL is the closure criteria for the parameter-estimation procedure; AP is equal to  $\rho_r$  of equation (50b), and ADMX is defined as discussed in the section "The Modified Gauss-Newton Method." AP times ADMX approaches TOL as the optimal parameter values are approached and, thus, can be used to indicate how close the parameter-estimation routing is to the final parameter estimates.

At the first parameter-estimation iteration, if FCONV is larger than zero, ADMX is set equal to  $10 \times \text{FCONV}$  for the purpose of this calculation, AP is set equal to 1.0, and all convergence criteria are increased as follows:

$$\text{CONV}' = \text{CONV} (\text{AP} \times \text{ADMX}) / \text{TOL}, \quad (\text{B1})$$

where CONV is the original convergence criteria (from the solver input file or as calculated as described in the section "Sensitivity-Equation Method of Calculating Sensitivities" and printed as noted in the section "Printing and Checking of the INPUT FILE"), and CONV' is the increased convergence criteria. If, for example, FCONV = 5.0 and TOL = 0.01, the convergence criteria would be increased by a factor of 5,000.

After the first parameter-estimation iteration, AP and ADMX are calculated by the modified Gauss-Newton routine (AP equals  $\rho_r$  of eq. 54 and ADMX is calculated as in eq. 52), and equation (B1) is used to increase the convergence criteria. If  $(AP \times ADMX)/TOL$  is less than 10, CONV' is set equal to CONV, the original convergence criteria; if  $(AP \times ADMX)/TOL$  is greater than 10,000, CONV' is set to  $CONV \times 10,000$ .

Numerical experiments based on test case 1 of Appendix A that use this procedure with modified Gauss-Newton optimization indicate that computer execution times can be reduced by as much as 50 percent. Although it seems likely that a similar procedure might reduce the computer execution time for conjugate-direction optimization, this option is not available in the Parameter-Estimation Package.



## APPENDIX C: PROGRAM DESCRIPTION AND FORTRAN LISTINGS

### Program Description

McDonald and Harbaugh (1988) use the terms "primary module," "submodule," and "utility module" when referring to subroutines in MODFLOW, and their terminology is followed in this report. Only modules that were modified from those presented in McDonald and Harbaugh (1988) and Prudic (1989) or which are new are discussed in this section. For modified modules, only the modifications are discussed.

The modules of the Parameter-Estimation Package are referred to as new in the following discussion and are named with the label SEN if they are used to calculate sensitivity-equation sensitivities or the gradient of the objective function, and with the label PAR if they are used for parameter estimation. Use of two labels made it easier to organize the large number of modules and, hopefully, will make it easier for those who wish to modify or add to the Parameter-Estimation Package. Also, the SEN modules can be used without the PAR modules, as might be required for some applications. The remaining characters of the module names were assigned according to the conventions used by McDonald and Harbaugh (1988) where possible. The names of new utility modules begin with "u," except for those modified from Press and others (1989).

This documentation describes the function of each new primary module, submodule, and utility module, and the changes made to MAIN, existing primary modules, and to one existing submodule. The discussion is organized by what is calculated: calculation of hydraulic heads is presented first, calculation of sensitivity-equation sensitivities or the gradient of the objective function follows, and parameter estimation is described last. Flowcharts and outlines illustrate the logic the program follows and how the new primary modules fit into this logic. It is anticipated that a more detailed understanding of the program will be pursued only by users who are considering making modifications to the Parameter-Estimation Package and know FORTRAN, and that these users will examine the program itself. The program is written to be as straightforward as possible, and numerous comments are used to explain the purpose of each part of the program. A list of variables is included to help those interested in examining the program at this detailed level.

## Hydraulic Heads

If the Parameter-Estimation Package is not used (IUNIT(15)=0), MODFLOWP functions like MODFLOW (McDonald and Harbaugh, 1988; and Prudic, 1989), except that if the solver does not converge, execution stops and no hydraulic heads, drawdowns, or budget terms are printed or saved. MODFLOW prints and saves the solution even if the solver does not converge. If the Parameter-Estimation Package is used (IUNIT(15)≠0), but only hydraulic heads are calculated (IPAR=-1 on LINE 6 of the INPUT FILE), the parameter values from DATA SET 8 and parameter definition from DATA SETS 2, 2A, and 2B of the INPUT FILE are used to replace the related model-input values read from the input files from other packages. This is accomplished by using new primary module SEN1FN, which is discussed in the next section. Calculation of hydraulic heads with the Parameter-Estimation Package is discussed in more detail in section "Calculating Hydraulic Heads and Flows" in Appendix A.

## Sensitivity-Equation Sensitivities or the Gradient of the Objective Function

To calculate sensitivity-equation sensitivities or the gradient of the objective function, MAIN, 8 primary modules, and 1 submodule were modified, and there are 14 new primary modules, 17 new submodules, and 5 new utility modules.

### Modified MAIN

Call statements for the new primary modules are added. Statements are added to coordinate the following: calculation of steady-state and transient hydraulic heads in a single model run; the calculation of sensitivity-equation sensitivities, or adjoint states and  $\partial h / \partial p_r$  (eq. 60).

### Modified primary modules--Listed in order of first appearance in MAIN.

- BAS10T Assigns KSTP as shown in table A3.
- BCF1RP Transmissivity and hydraulic conductivity are saved in array ST; if the top layer is unconfined, the vertical leakance beneath the top layer is saved in array SV.
- BCF1FM Two time-step lengths are used to formulate the matrix equations; they are unequal only when calculating adjoint states.

RIV1FM, EVT1FM, DRN1FM, STR1FM, GHBI1FM For these five modules, hydraulic heads are stored in array SHNW when calculating adjoint states,  $\partial h / \partial p_r$  (eq. 60), or sensitivity-equation sensitivities with ISN=-2. When calculating adjoint states, no contributions are added to RHS.

#### Modified submodule

SBCF1H Hydraulic heads are stored in array SHNW when calculating adjoint states,  $\partial h(n) / \partial p_r$  (eq. 60), or sensitivity-equation sensitivities with ISN=-2. If cells went dry in the previous parameter-estimation iteration, HOLD for those cells is set equal to BOT+10.0.

#### New primary modules--Listed in order of first appearance in MAIN.

SEN1AL Reads LINES 1 through 8 of the INPUT FILE and allocates space for calculating sensitivity-equation sensitivities and adjoint states.

SEN1RP Calls SSEN1G to read, check, print, and store the part of the INPUT FILE that defines the parameters (DATA SETS 2, 2A, 2B, 3, and 4); reads DATA SET 5; calls SSEN1H and SSEN1F to read, check, print, and store observations from the INPUT FILE (DATA SETS 6, 6A, 6B, 6C, 7, 7A, 7B); reads initial parameter estimates and group numbers (DATA SETS 8 and 9); and calculates convergence criteria for sensitivity-equation sensitivities.

SEN1ST Reads the stress period data from the Basic Package input file and calculates and stores the time-step lengths.

SEN1RW Rewinds input files that are to be read again.

SEN1FM Reads hydraulic heads or sensitivity-equation sensitivities from the files defined using IUHEAD (LINE 7) and stores them in the appropriate model arrays.

SEN1RR Reads input files from other packages of the MODFLOW without printing anything.

SEN1FN Resets parameter values that are negative but need to be positive to be physically reasonable, calls SSEN1J, SSEN1K, and SSEN1M to calculate model-input values from the parameter values and DATA SETS 2, 2A, and 2B, and puts the new model-input values in model arrays. Rereads IBOUND arrays, if required.

SEN1RH Modifies hydraulic heads at constant hydraulic-head boundaries (see section "IUNHEA" of Appendix A).

SEN1AR Calls submodules SSEN1U to calculate the objective-function derivative required to calculate adjoint states (eq. 73).

SEN1AP Calls submodules SSEN1C, SSEN1D, SSEN1P, SSEN1R, and SSEN1N to calculate the gradient of the objective function from the adjoint states (eq. 75) and to calculate the RHS array required to calculate sensitivity-equation sensitivities (eq. 69 or 71).

SEN1NZ Checks arrays HNEW and RHS for nonzero values. If none are located, the matrix equation is not solved.

SEN1HZ Sets all elements of array HNEW to zero at time steps listed in DATA SET 1B when calculating hydraulic heads.

SEN1FD Sets IFLD, which, when ISN<0 and IPAR=0, is used to limit the printing and saving of cell-by-cell sensitivity-equation sensitivity arrays to time steps at which there are observations.

SEN1OT When ISN≠-1, writes hydraulic heads on files defined using IUHEAD (LINE 7); when ISN>0, stores the hydraulic heads from the last time step in SHNW; calls SSEN1U and SSEN1V to calculate, print, and save hydraulic heads or head-dependent boundary flows and sensitivity-equation sensitivities related to the NH+NQT observations; and calls SSEN1O to print weighted residuals for dependent-variable observations and prior parameter estimates and related statistics.

New submodules--Divided by function and then listed in alphabetical order.

The following five new submodules are used to read and prepare data.

SSEN1A Called by SEN1RP when ICHECK>0 (LINE 4) to check on multiple use of grid cells for parameters used to calculate model-input arrays.

SSEN1B Called by SSEN1G when PID=CH to calculate coefficients for linear interpolation.

SSEN1F Called by SEN1RP to read and prepare data for head-dependent boundary flow observations (DATA SETS 7, 7A, and 7B).

SSEN1G Called by SEN1RP to read and prepare data that defines the parameters (DATA SETS 2, 2A, 2B, 3, and 4).

- SSEN1H    Called by SEN1RP to read and prepare data for hydraulic-head observations (DATA SETS 6, 6A, 6B, 6C).
- SSEN1I    Called by SSEN1H to calculate interpolation coefficients for hydraulic heads from ROFF and COFF (fig. 6). Also called by SEN1FN and SEN1OT if cells used in the interpolation have gone dry.

Three new submodules are called by SEN1FN to put parameter values in model arrays from other packages and to check the parameter definitions.

- SSEN1J    Called when PID=CH to put new constant hydraulic-head values in HNEW.
- SSEN1K    Called when PID=Q, KRB, KDR, KST, or GHB to put new parameter values in model arrays.
- SSEN1M    Called when PID=KV, TKV, S1, RCH, or ETM to put new parameter values in model arrays.

Eight new submodules are used to calculate sensitivity-equation sensitivities or the gradient of the objective function. For the adjoint-state method, four new submodules are called by SEN1AP to calculate the matrix and vector derivatives of equation (75), multiply them by hydraulic heads and adjoint states, as needed, and sum the results to get the gradient. For the sensitivity-equation method, the same four new submodules calculate the right-hand side of equation (69) or the identical terms on the right-hand side of equation (71). The four submodules are:

- SSEN1C    Called when PID=CH;
- SSEN1D    Called when PID=Q, KRB, KDR, KST, or GHB;
- SSEN1P    Called when PID=T, KV, TKV, ANI, or S1; and
- SSEN1R    Called when PID=RCH or ETM.

One new submodule is called by SEN1AP when there are water-table layers to calculate the term on the right-hand side of equation (71) that is calculated using equation (72).

- SSEN1N    Called for water-table layers.

The following three new submodules are called by SEN10T:

- SSEN10 Prints weighted residuals for dependent-variable observations and prior parameter estimates and selected statistics.
- SSEN1U Interpolates calculated hydraulic heads and associated sensitivity-equation sensitivities to locations not at cell centers, interpolates values temporally if needed, and calculates contributions to array RHS when calculating adjoint states. Recalculates interpolation coefficients if cells used in the interpolation have gone dry.
- SSEN1V Calculates flows at head-dependent boundaries and associated sensitivity-equation sensitivities.

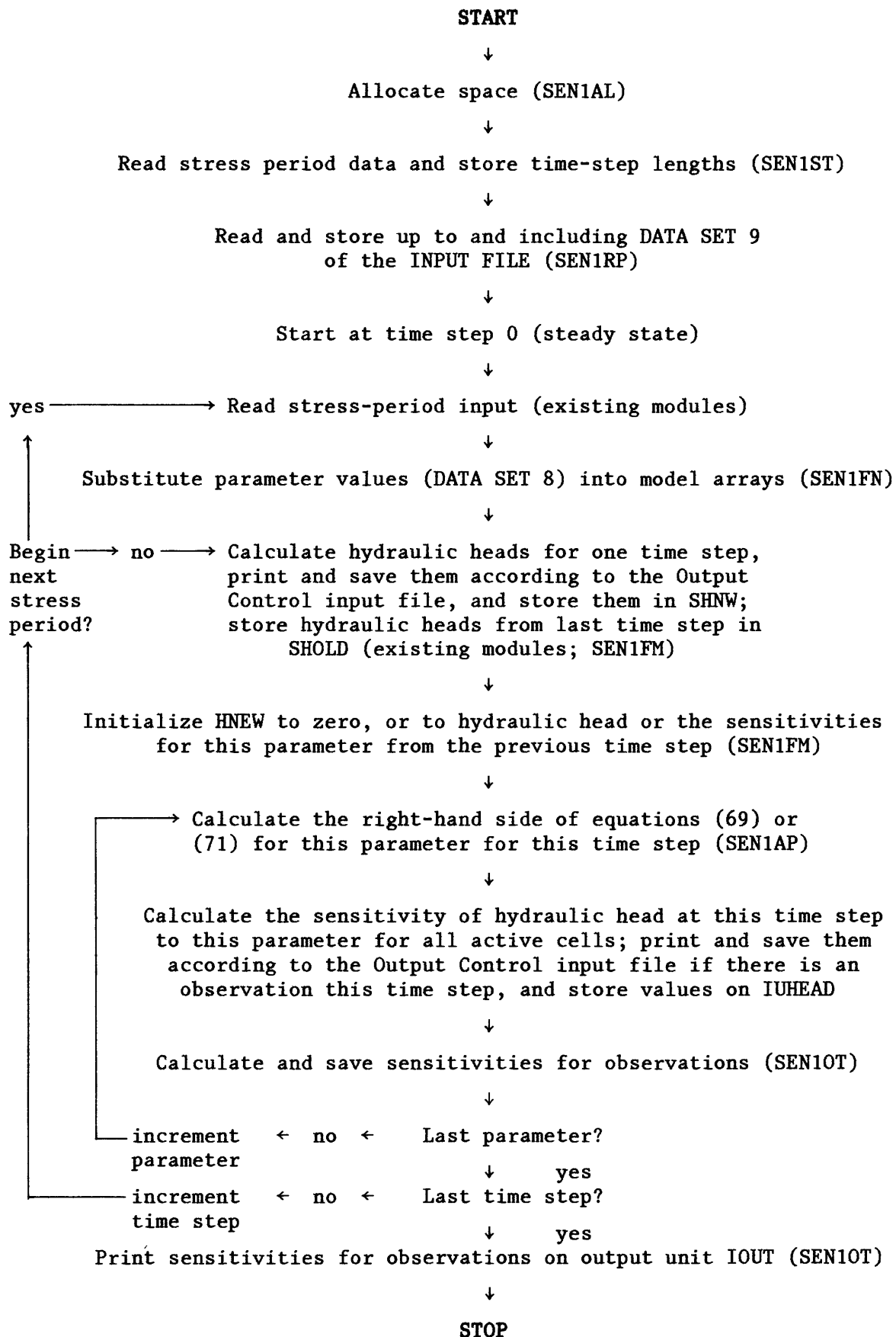
New utility modules - Listed in alphabetical order

- U2DINN Called by SEN1RR to read integer arrays without printing anything. Very similar to U2DINT (McDonald and Harbaugh, 1988, p. 14-30).
- U2DREN Called by SEN1RR to read real arrays without printing anything. Very similar to U2DREL (McDonald and Harbaugh, 1988, p. 14-26).
- UNORM Called by SSEN10 to find the random variable from a  $N(0,1)$  probability distribution given a cumulative probability.
- UREADF Reads a NROW×NCOL array from an unformatted file with multiple NROW×NCOL arrays.
- USAVEF Puts elements of one array, which can be single or double precision, into another array, which also can be single or double precision.

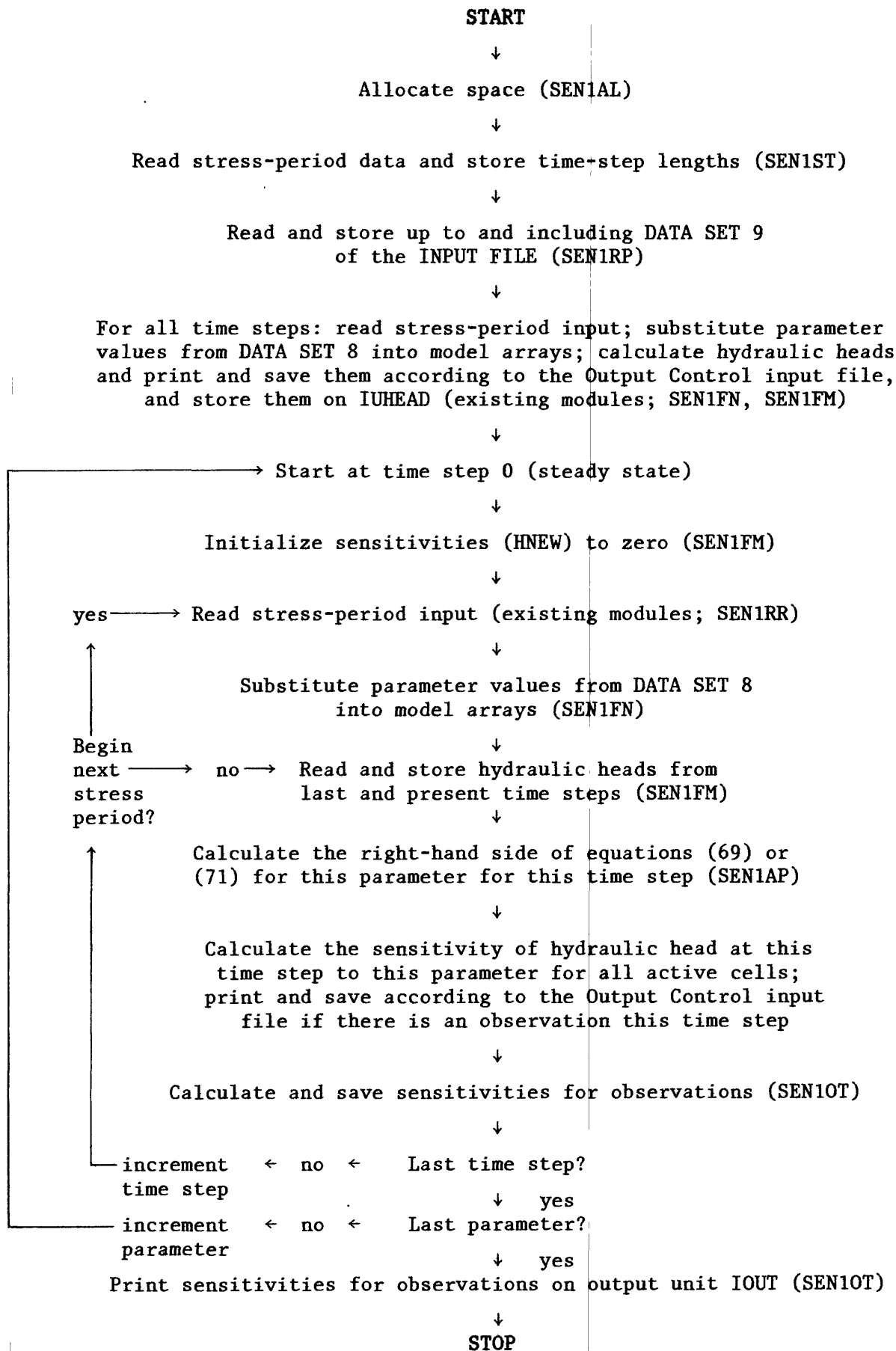
Flowcharts for calculating sensitivity-equation sensitivities and the gradient of the objective function

The following flowcharts display the logic followed by the program when calculating sensitivity-equation sensitivities or the gradient of the objective function using the adjoint-state method. Selected primary module names are included at steps for which the modules are used.

Flowchart for calculating sensitivity-equation sensitivities with ISN =-1

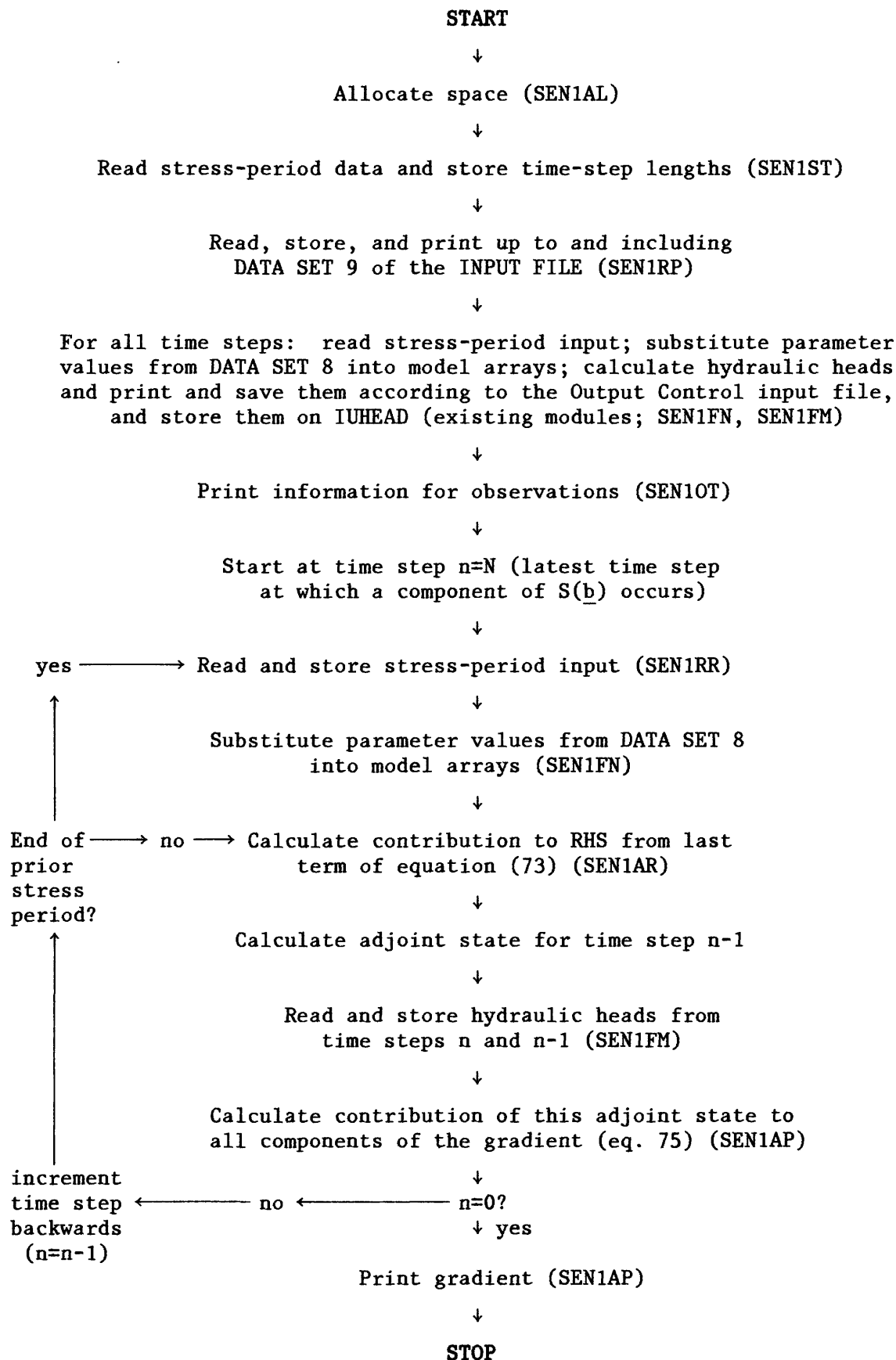


Flowchart for calculating sensitivity-equation sensitivities with ISN =-2





Flowchart for calculating the gradient of the objective function  
using the adjoint-state method (ISN>0)



## Parameter Estimation

To perform parameter estimation, MAIN was modified, and there are 7 new primary modules, 7 new submodules, and 3 new utility modules. PAR1AS, PAR1AQ, PAR1AP, and SPAR1P were developed from algorithms provided by Richard L. Cooley (U.S. Geological Survey, Lakewood, Colo., 1988); the 3 utility modules were developed from algorithms from Press and others (1989).

### Modified MAIN

Call statements for the new primary modules were added, and statements were added to execute multiple parameter-estimation iterations.

### New primary modules--Listed in order of appearance in MAIN

- PAR1AL Allocates space for the parameter-estimation calculations.
- PAR1RP Reads, checks, prints, and stores the part of the INPUT FILE used only for parameter estimation when IPAR>0 (DATA SETS 10 through 13 or 14).
- PAR1AS Calculates the search direction and prints data for each conjugate-direction nonlinear regression iteration. Checks for convergence and prints final statistics.
- PAR1AQ Calculates the iteration parameter, updates parameter estimates, and prints data for each conjugate-direction nonlinear regression iteration.
- PAR1AP Executes one iteration of nonlinear regression by using the modified Gauss-Newton method and prints data for the iteration.
- PAR1OT Final output for parameter estimation when the variance-covariance matrix for the parameter estimates (eq. 35) is printed.
- PAR1RE Calculates  $R_N^2$  (eq. 38) and prints the ordered weighted residuals and  $R_N^2$ .

### New submodules--Listed in alphabetical order

- SPAR1A Called by PAR1AS (ISN>0) or PAR1OT (ISN<0) to calculate R (eq. 37).
- SPAR1E Called by PAR1OT to calculate and print the eigenvalues and eigenvectors of the variance-covariance matrix on the parameters.

- SPAR1I Complete calculation of the inverse of the scaled modified Gauss-Newton coefficient matrix starting with the decomposed matrix from SPAR1R.
- SPAR1M Called by PAR1AS (ISN>0) or PAR1OT (ISN<0) to calculate statistics based on the maximum likelihood objective function (eq. 48, 64, and 65).
- SPAR1P Called by PAR1AS (ISN>0), PAR1OT (ISN<0), or MAIN (if convergence is not achieved when solving for hydraulic heads, sensitivity-equation sensitivities, adjoint states, or  $\partial h / \partial p_r$ ) to read parameter values and statistics for all iterations from file IOUB and to print them on the output file.
- SPAR1Q Called by PAR1AP to compute the component of the Hessian calculated with quasi-Newton updating and add it to the modified Gauss-Newton approximation of the Hessian.
- SPAR1R Called by PAR1AP to compute parameter step lengths for modified Gauss-Newton optimization by using the Marquardt procedure.

#### Utility modules--Modified from Press and others (1989).

- TRED2 Uses the Householder method to reduce a matrix to a tridiagonal form.
- TQLI Uses the QL method to calculate eigenvalues and eigenvectors of a matrix using the output from TRED2.
- ELGSRT Sorts the eigenvalues from smallest to largest and correspondingly rearranges the eigenvectors.

#### Outlines for Parameter-Estimation Calculations

The following outlines display the logic followed by the Parameter-Estimation Package when estimating parameters by modified Gauss-Newton or conjugate-direction optimization. Primary PAR module names are included at the step for which the modules are used.

#### Modified Gauss-Newton Optimization

1. Allocate space and read data required for parameter estimation (PAR1AL, PAR1RP).
2. Using the most recent parameter estimates, calculate hydraulic heads and sensitivity-equation sensitivities (see McDonald and Harbaugh, 1988, and previous section for documentation of the modules used).

3. Solve for scaled changes in parameters (eq. 50a).

4. Solve for new parameters (eq. 50b)

(PAR1AP)

5. Check for convergence.

6. If not converged and not yet reached the maximum number of parameter-estimation iterations, return to (2) after replacing the old parameter values with the new parameter values (PAR1FM). If converged, print final output (PAR1OT and PAR1RE). If not converged and reached the maximum number of iterations, print a message that indicates the lack of convergence and a table with parameter estimates and iteration information, and stop (PAR1OT).

### Conjugate-Direction Optimization

1. Allocate space and read data required for parameter estimation (PAR1AL, PAR1RP).

2. Using the most recent parameter estimates, calculate hydraulic heads and the gradient of the objective function (see McDonald and Harbaugh, 1988, and previous section for documentation of the modules used).

3. Calculate the sum of squared, weighted residuals. Check for convergence, and, if not converged and not yet reached the maximum number of iterations, calculate the direction vector (eq. 57 or 59) and proceed to step 4. If converged and the variance-covariance matrix on the parameter estimates is not to be calculated (DATA SET 13: LASTX=0), calculate and print the available statistics, print a table with parameter estimates and iteration information, and stop. (PAR1AS)

If convergence is reached and the variance-covariance matrix on the parameter estimates is to be calculated (LASTX>0), use the final parameter estimates to calculate hydraulic head and sensitivity-equation sensitivities (see McDonald and Harbaugh, 1988, and the previous section for documentation of the modules used), calculate and print the variance-covariance matrix and related statistics, print a table with parameter estimates and iteration information, and stop. (PAR1AP, PAR1OT, and PAR1RE)

If not converged and reached the maximum number of iterations, print a message that indicates the lack of convergence and a table with parameter estimates and iteration information, and stop (PAR1AS).

4. Calculate the  $\partial h / \partial p_r$  (eq. 60) (existing modules, SEN1FM, SEN1AP).

5. Calculate optimum step size and new model parameters (PAR1AQ).

6. Return to step 2.

### Program Portability

This program is written in FORTRAN 77 in a style similar to that of MODFLOW. The only difference between the programming in the codes is the extensive use of block IF statements in the Parameter-Estimation Package. McDonald and Harbaugh (1988, appendix A) discuss portability in detail.

International Mathematical and Statistical Library (IMSL) routines DE2CSF and DEPISF are used to calculate eigenvalues and eigenvectors of the variance-covariance matrix in SPAR1E. If IMSL is not available, comment out the lines where these routines are used, and set LPRINT#1 (see DATA SET 13 in the section "Instructions for the INPUT FILE").

As discussed by McDonald and Harbaugh (1988, p. A-2 to A-4), in some circumstances it might be necessary to convert the flow code to double precision. Although there is no advantage to converting all regression variables and arrays to double precision, the conversion of the flow code probably is accomplished most easily if all of MODFLOWP is converted to double precision, using the instructions from McDonald and Harbaugh (1988, p. A-3). In addition, the intrinsic function DBLE(.), which is used in some of the new and modified subroutines of MODFLOWP, needs to be omitted from the code.

### List of Variables

The following list includes most of the variables that occur in the FORTRAN program of the next sections; however, two types of variables are not included. These are: (1) variables that are used to store only the quantities that McDonald and Harbaugh (1988) and Prudic (1989) indicate they store, and (2) variables that are used briefly in a few calculations so their meaning can be clearly identified from a small part of the FORTRAN code. Note that HNEW and HOLD are included in the list below because they are used in the Parameter-Estimation Package to store other arrays besides the hydraulic head of the present and previous time step, as discussed in McDonald and Harbaugh (1988).

In the following list, the "Range" is listed as "SEN" and "PAR" for variables that are used only within SEN or PAR modules of the Parameter-Estimation Package, respectively. Variables used within both SEN and PAR modules are listed with a range of "Package". Variables used in any part of the Parameter-Estimation Package and in other parts of MODFLOWP are listed with a range of "Global". Variables that are used within a single module have that module listed under "Range".

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
ADMX	Global	Absolute value of DMX.
ALPH	PAR1AQ	Iteration parameter calculated by Newton's method.
ATS	SEN	DIMENSION (2×(NPER+1)), sequence of time-step lengths used to calculate adjoint states.
AVE	SSEN10	Arithmetic average of the weighted residuals of observed hydraulic heads and drawdowns, observed head-dependent boundary gains and losses, or prior parameter estimates.
AVET	SSEN10	Arithmetic average of the weighted residuals of all observations and prior parameter estimates.
B	Package	DIMENSION (NP), updated parameter estimates.
B1	Package	DIMENSION (NP), original parameter estimates.
BSTP	SEN	DIMENSION (NPER+1), last time step of each pumping period, starting with the last. Used only for calculating adjoint-state sensitivities.
BUFF	Global	DIMENSION (NCOL, NROW, NLAY), general-purpose storage space used as required in many modules and sub-modules. Generally uses same storage space as RHS (McDonald and Harbaugh, 1988, p. 4-11).
C	PAR	DIMENSION (NP,NP), double precision coefficient matrix of the Gauss-Newton method, matrix $\underline{H}$ of the quasi-Newton conjugate-direction method, or variance-covariance and correlation matrices of the parameters.
CELS	SEN	DIMENSION (4,NSN), cell information for parameters defined by lists of cells. Read from repetitions of DATA SET 2A.
COFF	SEN	DIMENSION (NH), column offsets which, with ROFF, define the locations of hydraulic-head observation points relative to cell centers. Read from repetitions of DATA SET 6.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
CONV	Global	DIMENSION (2,NP+1), solver convergence criteria for hydraulic head and sensitivity-equation sensitivities.
CSA	PAR	Search direction adjustment parameter used in Marquardt procedure (CSA=0.08 is suggested by Cooley and Naff, 1990, p. 71-72, 91).
DD	PAR	DIMENSION (NP), double-precision array of the calculated changes in parameters.
DELT1	Global	Time-step length used to calculate $\underline{B}(n+1)$ of equation (23).
DID	Global	DIMENSION (ND), character array used to store labels for each of the ND dependent-variable observations.
DMAX	PAR	Maximum allowed fractional change for parameter values in one iteration.
DMX	PAR	Maximum calculated fractional change for any parameter value in one parameter-estimation iteration.
EV	PAR	Estimated common error variance.
FCONV	Global	User-defined factor that produces coarser solver convergence criteria when calculating heads and sensitivity-equation sensitivities for the first parameter-estimation iterations.
G	PAR	DIMENSION (NP), double-precision array of the gradient of the objective function with respect to each of the NP parameters.
H	Package	DIMENSION (ND), calculated dependent-variable values.
HNEW	Global	DIMENSION (NODES), double precision array of hydraulic heads, sensitivity-equation sensitivities, adjoint states, or the derivative of hydraulic heads with respect to the iteration parameter from Newton's method. Always for the present time step.
HOBS	Package	DIMENSION (ND), observed dependent-variable values.
HOLD	Global	DIMENSION (NODES), hydraulic heads, sensitivity-equation sensitivities, adjoint states, or the derivative of hydraulic heads with respect to the iteration parameter from Newton's method. Always for the prior time step. When calculating adjoint-state sensitivities, HOLD in module SEN1AP contains the hydraulic heads from the previous time step.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>										
IBT	SEN	<p>DIMENSION (2,NQ), IBT(1,NQ) indicates the package used to simulate the head-dependent boundary for which a gain or loss is observed:</p> <table><tr><th><u>IBT(1,NQ)</u></th><th><u>Package</u></th></tr><tr><td>1</td><td>River</td></tr><tr><td>2</td><td>General-Head Boundary</td></tr><tr><td>3</td><td>Stream</td></tr><tr><td>4</td><td>Drain</td></tr></table> <p>IBT(2,NQ) equals zero unless one of the NP parameters is used to calculate the conductance of the head-dependent boundary, when IBT (2,NQ) equals the number of that parameter.</p>	<u>IBT(1,NQ)</u>	<u>Package</u>	1	River	2	General-Head Boundary	3	Stream	4	Drain
<u>IBT(1,NQ)</u>	<u>Package</u>											
1	River											
2	General-Head Boundary											
3	Stream											
4	Drain											
ICH	SEN	Counter for cells included in DATA SET 2A for PID=CH.										
ICHECK	SEN	If ICHECK >0, model inputs determined with PID=T, KV, TKV, S1, RCH, and ETM are checked to ensure that that cells do not occur more than NUMR times.										
IDIS	SEN	Number of head-dependent boundary gain or loss observations eliminated because the head-dependent boundary is no longer calculated by using the simulated hydraulic head in the aquifer.										
IDRY	SEN	Number of hydraulic-head observations eliminated because cells in water-table layers have gone dry.										
IFLCH	Global	Counter for parameters included for PID=CH.										
IFLCH1	MAIN	Saves previous value of IFLCH, as required when an iterative solver is used.										
IFO	Global	Flag that equals one when parameter estimation has converged.										
IHESS	SEN	When ISN>0, IHESS=0 when adjoint states are calculated, and IHESS=1 when the derivative of hydraulic heads with respect to the iteration parameter of Newton's method is calculated.										
IOFF	SEN	DIMENSION (NH), used to identify neighboring cells that are to be used to interpolate hydraulic heads of observation locations.										
IOUR	PAR	Output unit for unformatted data to be used by RESAN, a separate FORTRAN program used to analyze residuals										



<u>Variable</u>	<u>Range</u>	<u>Definition</u>								
IP	Global	IP=0 when hydraulic heads are calculated. Positive, nonzero values of IP equal the parameter numbers when ISN<0, and in SEN1RP, PAR1RP, SEN1AP, SEN1OT, and SSEN1C when ISN>0. In other modules and submodules used when ISN>0, IP=1 when adjoint states are calculated, and IP=2 when the derivative of hydraulic heads with respect to the iteration parameter of Newton's method is calculated.								
IPP	MAIN	Flag that equals one when a new pumping period has been reached.								
IPAR	Package	Flag that controls program execution: <table><tr><th><u>IPAR</u></th><th><u>Result</u></th></tr><tr><td>&lt;0</td><td>Hydraulic heads are calculated</td></tr><tr><td>0</td><td>Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated.</td></tr><tr><td>1</td><td>Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated and parameter-estimation is performed.</td></tr></table>	<u>IPAR</u>	<u>Result</u>	<0	Hydraulic heads are calculated	0	Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated.	1	Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated and parameter-estimation is performed.
<u>IPAR</u>	<u>Result</u>									
<0	Hydraulic heads are calculated									
0	Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated.									
1	Hydraulic heads and sensitivity-equation sensitivities or the gradient of the objective function are calculated and parameter-estimation is performed.									
		For more information, see the definition in the INPUT FILE instructions (LINE 6).								
IPRC	PAR	Format code with which the covariance and correlation matrices are printed when parameter estimation converges and the modified Gauss-Newton coefficient matrix is calculated.								
IPRINT	PAR	See definition in the input instructions for the last DATA SET 13 of the INPUT FILE.								
IPRIOR	PAR	All prior information on the parameters is disregarded if IPRIOR=0.								
IQOB	SEN	DIMENSION (NQT), time steps of observed fluxes at head-dependent boundaries.								
IRBOT	SSENIV	Flag that controls the printing preceding and following the list of cells or reaches affected by nonlinearities when calculating head-dependent boundary gains and losses along observed reaches.								
IRWD	SEN	DIMENSION (NRWD), FORTRAN input unit numbers that are identified from within the Recharge or Evapotranspiration Packages by LOCAT.								

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
ISCALS	SEN	If = 0, actual sensitivity-equation sensitivities are printed. If $\neq$ 0, printed sensitivities are scaled by multiplying by the parameter value and multiplying by the square root of the weight.
ISN	Package	Flag identifying which numerical and optimization methods are used. See the definition in the INPUT FILE instructions (LINE 6).
ISUM	Global	Index number of the lowest element in the X array that has not yet been allocated. When space is allocated for an array, the size of the array is added to ISUM.
ITMXP	PAR	Maximum number of parameter-estimation iterations.
ITT	SEN	Flag for transient observations:
	<u>ITT</u>	<u>Description</u>
	1	Observed hydraulic heads are used for parameter estimation.
	2	Initial observed hydraulic heads and subsequent changes in hydraulic head at each location are used for parameter estimation.
IUBD	SEN	If IUBD>0, IBOUND arrays are read from FORTRAN unit IUBD.
IUHEAD	SEN	Output/input unit for hydraulic heads or sensitivity-equation sensitivities stored in binary format.
IUNHEA	SEN	Flag indicating that known hydraulic heads at constant hydraulic-head boundaries change during the simulation.
IWP	PAR	Flag indicating how the weights are to be calculated from the user-provided data for prior information on the parameters. See discussion for DATA SETS 10, 11, and 12 of the INPUT FILE instructions.
IWPG	PAR	Dimension (NP), parameter group numbers read from DATA SET 9 of the INPUT FILE. Weighted residuals for prior estimates of single parameter values are printed out by groups. Negative values in the last entries of the IWPG array indicate that the related parameters are not estimated.
IWT	SEN	Flag indicating how the weights are to be calculated from the user-provided data for dependent-variable observations. See discussion for DATA SETS 6 and 7A of the INPUT FILE instructions.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
JDRY	Package	Number of hydraulic-head observations interpolations that have been changed because cells in water-table aquifers have gone dry.
JOFF	SEN	DIMENSION (NH), used to identify neighboring cells that are to be used to interpolate hydraulic heads of observation locations.
JRBOT	SSEIV	Flag that controls printing of explanation about the effect of nonlinearities in head-dependent boundary flows.
JT	Global	Latest time step required for calculating dependent-variable values related to observations.
KNST	Global	Used in SEN1FM when calculating adjoint states to indicate that all components of HNEW are to be set to zero (KNST=1), hydraulic heads from the previous time step are to be read and stored in HOLD (KNST=-1), or the hydraulic heads in HOLD are to be stored in SHNW (KNST=0).
KNT	Global	Number of times the change in parameters calculated by the conjugate-direction method has been diminished because the value of the objective function was not reduced.
KPER	Global	The time step plus one. At steady state, KPER=1, at time step 1, KPER=2, and so on.
KPRINT	PAR	Controls printing of final hydraulic-head array and sensitivity-equation sensitivity ratios (ISN<0 only) when parameter estimation converges.
KRBOT	SSEIV	The number of cells in a head-dependent boundary observation group at which flow is not calculated using calculated hydraulic head or any parameter. The head-dependent boundary observation is eliminated if KRBOT=NQCL.
KSTP	Global	Always equals 1 when using the Parameter-Estimation Package. See KPER for the time-step number.
LASTX	PAR	See definition in the input instructions for the last DATA CARD of the INPUT FILE.
LCname	Package	Location in the X array (McDonald and Harbaugh, 1988, p. 3-22) of the first element of array 'name'. If name is longer than four letters, only the first four letters are used.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
LM	SEN	DIMENSION (NSM), multiplication array numbers. Read from DATA SET 2B.
LN	Package	DIMENSION (NP), flag that indicates whether the log-transform of a parameter is to be considered. If LN(I)=0, no log-transform is applied to the Ith parameter.
LPRINT	PAR	Controls calculation and printing of eigenvectors and eigenvalues of the scaled variance-covariance matrix on the parameters.
LZ	SEN	DIMENSION (LZI1+1,NSM), LZ(1) is a zone array number; LZ(I,NM), I=2,LZI1 are zone numbers; NM is incremented from 1 to NSM. Read from DATA SET 2B. LZ(1) is called LZA in the INPUT FILE instructions.
LZI1	SEN	Used to dimension array LZ. Read on LINE 3 of the INPUT FILE; set to the value read plus 1 in MODFLOWP.
MATZ	SEN	DIMENSION (NCOL, NROW, NZM). Zone arrays used in parameterization.
MAXM	Package	Maximum number of layers used for any of the MOBS locations.
MLAY	Package	DIMENSION (MAXM,MOBS), layers of a multilayer observation well. Read from DATA SET 6A of the INPUT FILE.
MOBS	SEN	Number of the NH locations and times at which observed hydraulic head or changes in hydraulic head are multilayer.
MPR	Package	Number of equations of prior information on the parameters that include more than one parameter.
ND	Package	Total number of dependent-variable observations: ND=NH+NQT.
NDER	SEN	DIMENSION (5,NH), layer, row, column, and time step of hydraulic-head observations, and the number of the first observation, which is used to calculate changes in hydraulic head for ITT=2.
NFIT	PAR	Number of Fletcher-Reeves iterations used in combined Fletcher-Reeves/quasi-Newton optimization.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
NH	Package	Number of locations and times at which there are observed hydraulic heads or changes in hydraulic heads.
NLL	SEN	DIMENSION (NLLI1,NP), used to define the parameters to which sensitivities are to be calculated or which are to be estimated. Use depends on PID of parameter involved. See description of DATA SET 2 of the INPUT FILE.
NLLI1	SEN	Largest required first dimension for array NLL. Read on LINE 3 of the INPUT FILE.
NLLIT	SEN	Calculated as (NLLI1-1)/2, and used as described in the INPUT FILE instructions for DATA FILE 2.
NM	Global	Counter that is incremented from one to NSM.
NMM	SEN	Number of multiplication arrays in DATA SET 3 of the INPUT FILE.
NNEG	SSEN10	Number of negative weighted residuals for one type of observation.
NNEGT	SSEN10	Number of negative weighted residuals for all observations.
NODES	Global	Total number of nodes in the finite-difference grid. Equals the product of the number of rows, columns, and layers.
NP	Package	Read from LINE 3. Changed in MODFLOWP to the number of estimated parameters.
NP1	Package	Original value of NP read from LINE 3; includes estimated and unestimated parameters.
NPER	Global	Value read from the Basic Package input file needs to be equal to or greater than JT+1. In MAIN of the Parameter-Estimation Package, NPER is set equal to JT+1 after the INPUT FILE is read.
NPOS	SSEN10	Number of positive weighted residuals for one type of observation.
NPOST	SSEN10	Number of positive weighted residuals for all observations.
NPR	Package	Number of prior estimates of single parameters. Equals the number of nonzero values in DATA SET 10 of the INPUT FILE. In the text of this report, NPR is used to indicate the sum of NPR and MPR as they are defined in the appendices.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
NQ	SEN	Number of cell groups for which the sum of cell-by-cell, head-dependent flows are observed.
NQC	SEN	Total number of individual cells, or nodes, in the NQ cell groups.
NQCL	SEN	DIMENSION (NQ), number of cells included in each of the NQ cell groups.
NQOB	SEN	DIMENSION (NQ), number of head-dependent boundary flux observations for each of the NQ groups.
NQT	Package	Total number of head-dependent boundary flux observations.
NRP	Global	Number of pumping periods of data to be read to reach the pumping period in questions. Equals one except when calculating adjoint states.
NRWD	SEN	Number of FORTRAN input units identified from within the Recharge and Evapotranspiration Packages by LOCAT.
NS	Global	Counter that is incremented from one to NSN.
NSM	SEN	Number of NLL values larger than zero for the T, KV, TKV, S1, RCH, and ETM parameter identifiers in DATA SET 2 of the INPUT FILE.
NSN	SEN	Number of cell locations listed for parameter definition in the INPUT FILE (equals the sum of the absolute values of NLL(1) for all GHB, Q, KRB, and CH parameter identifiers in DATA SET 2).
NUMR	SEN	See explanation for ICHECK.
NZM	SEN	Number of zone arrays in DATA SET 4 of the INPUT FILE.
PID	Package	DIMENSION (NP), character variable used to identify parameter type (see table A1).
PR	SEN	DIMENSION (5,MOBS), proportion assigned to each layer of a multilayer observation well. Read from DATA SET 6A.
PRM	PAR	DIMENSION (NP+1), coefficients and prior estimate for prior information on the parameters that can include more than one parameter. Read from DATA SET 12.
PV	PAR1AQ	DIMENSION (ND), double-precision array of derivatives of observed dependent variables with respect to the iteration parameter of Newton's method.

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
QCLS	SEN	DIMENSION (4,NQC), layer, row, and column of cells in the head-dependent boundary groups. The fourth position is zero unless one of the NP parameters being estimated is used to calculate the conductance of this head-dependent boundary. Then, information required to calculate the derivative is stored in the fourth position.
RINT	SEN	DIMENSION (4,NH), values of interpolation basis functions for hydraulic-head observation locations.
ROFF	SEN	DIMENSION (NH), row offsets that, with COFF, define the locations of observation points relative to cell centers. Read from repetitions of DATA SET 6.
RSQ	Package	Sum of squared weighted residuals for dependent-variable observations.
RSQP	Package	Sum of squared weighted residuals for dependent-variable observations and prior parameter estimates.
SCL	PAR	DIMENSION (NP), user-defined parameter scaling factors used in conjugate-direction optimization methods.
SCLE	PAR	DIMENSION (NP), double precision array of the diagonal components of the unscaled coefficient matrix of the Gauss-Newton method.
SFAC	SEN	DIMENSION (NSM), multiplication factor used to define parameters.
SHOLD	SEN	DIMENSION (NODES), hydraulic-head array from previous time step. Used only when calculating sensitivity-equation sensitivities.
SHNW	SEN	DIMENSION (NODES), hydraulic-head array for current time step. Used only when calculating sensitivity-equation sensitivities, adjoint-state sensitivities, or the derivative of hydraulic head with respect to the iteration parameter from Newton's method.
SMAT	SEN	DIMENSION (NCOL, NROW, NMM), multiplication matrices used in parameterization. Read from DATA SET 3.
SSG	PAR1AS	Double-precision scalar variable of the sum of the squared components of the gradient; used in the Fletcher-Reeves method, equation (57).
SSG1	PAR1AS	Single precision scalar variable used to save the previous value of SSG, as required for equation (57).

<u>Variable</u>	<u>Range</u>	<u>Definition</u>
ST	SEN	DIMENSION (NODES), transmissivity or hydraulic-conductivity values for each cell.
STP	SEN	DIMENSION (NPER+1), first time step of each pumping period, starting with the first.
TOFF	SEN	DIMENSION (ND), time offsets that define the time of dependent-variable observations relative to the end of the preceding time step.
TMEAN	SEN10T	Sum of the absolute values of all scaled sensitivities divided by ND×NP.
TOL	PAR	Parameter-estimation closure criterion. Solution is reached when the convergence criteria described in the text for the optimization methods are less than or equal to TOL.
TS	SEN	DIMENSION (NPER), or DIMENSION (1) when NPER=0, time-step lengths.
VMAX	SSEN10	Maximum weighted residual for one type of observation.
VMIN	SSEN10	Minimum weighted residual for one type of observation.
WP	PAR	DIMENSION (NP+MPR), weights of prior information on the parameters.
WT	Package	DIMENSION (ND), weights of the observed hydraulic heads, changes in hydraulic heads, and head-dependent flows.
X	Package	DIMENSION (NP,ND) calculated sensitivity-equation sensitivities of observed dependent variables. Used only for modified Gauss-Newton regression (ISN<0 or LASTX>0).
XD	PAR1AS	Double-precision scalar variable equal to $(g_{r+1} - g_r) \frac{1}{d_r}$ (terms are defined after eq. 57).
XX	Package	DIMENSION (NP), double-precision array of the gradient of the objective function. Used only for conjugate-direction optimization (ISN>0).



# FORTRAN Listings

## Modified MAIN

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C *****MAI0001
C MAIN CODE FOR MODULAR MODEL -- 9/1/87 MAI0002
C BY MICHAEL G. MCDONALD AND ARLEN W. HARBAUGH MAI0003
C-----VERSION 1638 24JUL1987 MAIN1 MAI0004
C *****MAI0005
C MODIFIED FOR ADJOINT SENSITIVITY CALCULATIONS 9/1/87MAI0006
C BY MARY C. HILL AND RUSSELL NELSON, WRD, USGS, TRENTON NJ. MAI0007
C *****MAI0008
C MODIFIED FOR PARAMETER ESTIMATION BY MARY C. HILL 2/1/92MAI0009
C *****MAI0010
C MAI0011
C SPECIFICATIONS: MAI0012
C -----MAI0013
C CHARACTER*4 PID(30),DID(600) MAI0014
C COMMON X(900000) MAI0015
C DIMENSION HEADNG(32),VENM(4,20),VBVL(4,20),IUNIT(24) MAI0016
C DOUBLE PRECISION DUMMY MAI0017
C EQUIVALENCE (DUMMY,X(1)) MAI0018
C -----MAI0019
C MAI0020
C1-----SET SIZE OF X ARRAY. REMEMBER TO REDIMENSION X. MAI0021
C LENX=900000 MAI0022
C MAI0023
C2-----ASSIGN BASIC INPUT UNIT AND PRINTER UNIT. MAI0024
C INBAS=5 MAI0025
C IOUT=6 MAI0026
C MAI0027
C3-----DEFINE PROBLEM_ROWS,COLUMNS,LAYERS,STRESS PERIODS,PACKAGES MAI0028
C CALL BAS1DF(ISUM,HEADNG,NPER,ITMUNI,TOTIM,NCOL,NROW,NLAY, MAI0029
C 1 NODES,INBAS,IOUT,IUNIT) MAI0030
C-----INITIALIZE SCALARS USED TO ALLOCATE SPACE IN X ARRAY FOR ARRAYS MAI0031
C-----THAT MAY NOT BE USED, BUT ARE INCLUDED IN CALLS FOR THE MAI0032
C-----PARAMETER-ESTIMATION PACKAGE. MAI0033
C .LCWELL=1 MAI0034
C LCDRAI=1 MAI0035
C LCIRCH=1 MAI0036
C LCRECH=1 MAI0037
C LCIEVT=1 MAI0038
C LCEVTR=1 MAI0039
C LCXDP=1 MAI0040
C LCSURF=1 MAI0041
C LCRIVR=1 MAI0042
C LCSTRM=1 MAI0043
C ICSTRM=1 MAI0044
C LCTBAR=1 MAI0045
C LCIVAR=1 MAI0046
C LCBNDS=1 MAI0047
C LCST=1 MAI0048
C LCSV=1 MAI0049
C LCC=1 MAI0050
C LCSCLE=1 MAI0051
C LCG=1 MAI0052
C LCDD=1 MAI0053
C LCWP=1 MAI0054
C LCB1=1 MAI0055
C LCB=1 MAI0056
C LCPRM=1 MAI0057
C LCIWPG=1 MAI0058
C LCSC1=1 MAI0059
C LCSHNW=1 MAI0060
C-----SET VARIABLES TO ZERO MAI0061
C MXDRN=0 MAI0062
C MXSTRM=0 MAI0063
C MXBND=0 MAI0064
C MXRIVR=0 MAI0065
C KNT=0 MAI0066
C JDRY=0 MAI0067
C IDRY=0 MAI0068
C KPRINT=0 MAI0069
C LPRINT=0 MAI0070
C NPR=0 MAI0071
C MPR=0 MAI0072
C MAI0073
C4-----ALLOCATE SPACE IN "X" ARRAY. MAI0074
C CALL BAS1AL(ISUM,LENX,LCHNEW,LCHOLD,LCIBOU,LCCR,LCCC,LCCV, MAI0075
C 1 LCHCOF,LCRHS,LCDELRL,LCDELC,LCSTRT,LCTRT,LCTRT,LCTRT,LCTRT, MAI0076
C 2 INBAS,ISTRT,NCOL,NROW,NLAY,IOUT) MAI0077
C IF(IUNIT(1).GT.0) CALL BCF1AL(ISUM,LENX,LCSC1,LCHY, MAI0078
C 1 LCBOT,LCTOP,LCSC2,LCTRPY,IUNIT(1),ISS, MAI0079

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2      NCOL,NROW,NLAY,IOUT,IBCFCE)                                MAI0080
  IF(IUNIT(2).GT.0) CALL WELIAL(ISUM,LENX,LCWELL,MXWELL,NWELLS, MAI0081
1      IUNIT(2),IOUT,IWELCB)                                    MAI0082
  IF(IUNIT(3).GT.0) CALL DRNIAL(ISUM,LENX,LCDRAI,NDRAIN,MXDRN, MAI0083
1      IUNIT(3),IOUT,IDRNCB)                                    MAI0084
  IF(IUNIT(8).GT.0) CALL RCHIAL(ISUM,LENX,LCIRCH,LCRECH,NRCHOP, MAI0085
1      NCOL,NROW,IUNIT(8),IOUT,IRCHCB)                        MAI0086
  IF(IUNIT(5).GT.0) CALL EVTIAL(ISUM,LENX,LCIEVT,LCEVTR,LCEXDP, MAI0087
1      LCSURF,NCOL,NROW,NEVTOP,IUNIT(5),IOUT,IEVTCE)         MAI0088
  IF(IUNIT(4).GT.0) CALL RIVIAL(ISUM,LENX,LCRIVR,MXRIVR,NRIVER, MAI0089
1      IUNIT(4),IOUT,IRIVCB)                                    MAI0090
  IF(IUNIT(7).GT.0) CALL GHIAL(ISUM,LENX,LCBND,NBOUND,MXBND, MAI0091
1      IUNIT(7),IOUT,IGHBCB)                                    MAI0092
  IF(IUNIT(9).GT.0) CALL SIPIAL(ISUM,LENX,LCEL,LCFL,LCGL,LCV, MAI0093
1      LCHDCG,LCLRCH,LCW,MXITER,NPARM,NCOL,NROW,NLAY, MAI0094
2      IUNIT(9),IOUT)                                           MAI0095
  IF(IUNIT(11).GT.0) CALL SORIAL(ISUM,LENX,LCA,LCRES,LCHDCG,LCLRCH, MAI0096
1      LCIEQP,MXITER,NCOL,NLAY,NSLICE,NBW,IUNIT(11),IOUT)     MAI0097
  IF(IUNIT(18).GT.0) CALL STRIAL(ISUM,LENX,LCSTRM,ICSTRM,MXSTRM, MAI0098
1      NSTREM,IUNIT(18),IOUT,ISTCB1,ISTCB2,NSS,NTRIB, MAI0099
2      NDIV,ICALC,CONST,LCTBAR,LCTTRIB,LCIVAR)               MAI0100
  IF(IUNIT(13).GT.0) CALL PCG2AL(ISUM,LENX,LCV,LCSS,LCP,LCCD, MAI0101
1      LCHCHG,LCLHCH,LCRCHG,LCLRCH,MXITER,ITER1,NCOL,NROW,NLAY, MAI0102
2      IUNIT(13),IOUT,NPCOND)                                   MAI0103
  IF(IUNIT(15).NE.0) CALL SENIAL(ISUM,LENX,NCOL,NROW,NLAY,NPER,IOUT, MAI0104
1      LCSHNW,LCNLL,LCSMAT,LCCELS,IUHEAD,NP,NSM,NSN,ISN,LCTS, MAI0105
2      LCATS,LCST,NH,LCNDER,LCSHOL,LCSTP,NRWD,LCIRWD,IUNIT(15), MAI0106
3      LCBSTP,IPAR,LCB,LCH,LCX,LCRINT,LCJOFF,LCIOFF,LCCONV, MAI0107
4      LCCOFF,LCROFF,LCMLAY,LCPR,MOBS,LCLN,NQ,NQC,NQT,LCIBT, MAI0108
5      LCNQOB,LCNQCL,LCIQOB,LCQCLS,IUBD,ISCALS,LCTOFF,MPR, MAI0109
6      LCXX,MAXM,LCLZ,NLLI1,NLLIT,NMM,NZM,LZIL,LCSFAC,LCLM, MAI0110
7      LCMATZ,LCHOBS,LCWT,IUBD,LCSV,IPRNP,IUNHEA,NUMR,ICHECK, MAI0111
8      NPNG,LCIPNG,NZER,LCIZER,LCIWPNG,NQPT,LCXD)             MAI0112
  ND=NH+NQT                                                       MAI0113
  IF(IUNIT(15).GT.0.AND.(IPAR.GE.1.OR.ISN.GT.0)) CALL PARIAL(ISUM, MAI0114
1      LENX,IOUT,NP,NH,LCC,LCSCLE,LCG,LCDD,LCWP,LCB1,NQT,MPR, MAI0115
2      LCPRM,ISN,LCSCLE,LCPV,ND,LCR,LCU,LCGD,LCS)            MAI0116
C                                                                    MAI0117
C5-----IF THE "X" ARRAY IS NOT BIG ENOUGH THEN STOP.          MAI0118
  IF(ISUM-1.GT.LENX) STOP                                         MAI0119
C                                                                    MAI0120
C6-----READ AND PREPARE INFORMATION FOR ENTIRE SIMULATION.     MAI0121
  CALL BASIRP(X(LCIBOU),X(LCHNEW),X(LCSTRT),X(LCHOLD),          MAI0122
1      ISTRT,INBAS,HEADNG,NCOL,NROW,NLAY,NODES,VBVL,X(LCIOFL), MAI0123
2      IUNIT(12),IHEDFM,IDDNEF,IHEDUN,IDDNUN,IOUT)           MAI0124
  IF(IUNIT(1).GT.0) CALL BCFIRP(X(LCIBOU),X(LCHNEW),X(LCSC1), MAI0125
1      X(LCHY),X(LCCR),X(LCCC),X(LCCV),X(LCDELR), MAI0126
2      X(LCDELC),X(LCBOT),X(LCTOP),X(LCSC2),X(LCTRPY), MAI0127
3      IUNIT(1),ISS,NCOL,NROW,NLAY,NODES,IOUT, MAI0128
4      IUNIT(15),X(LCST),X(LCSV))                               MAI0129
  IF(IUNIT(9).GT.0) CALL SIPIRP(NPARM,MXITER,ACCL,HCLOSE,X(LCW), MAI0130
1      IUNIT(9),IPCALC,IPRSIP,IOUT)                             MAI0131
  IF(IUNIT(10).GT.0) LINO=LINEAR                                  MAI0132
  IF(IUNIT(11).GT.0) CALL SORIRP(MXITER,ACCL,HCLOSE,IUNIT(11), MAI0133
1      IPRSOR,IOUT)                                              MAI0134
  IF(IUNIT(13).GT.0) CALL PCG2RP(MXITER,ITER1,HCLOSE,RCLOSE,NPCOND, MAI0135
1      NEPOL,RELAX,IPRPGC,IUNIT(13),IOUT,MUTPCG,NITER)        MAI0136
  NPO=NP                                                           MAI0137
  IF(IUNIT(15).NE.0) CALL SENIRP(NCOL,NROW,NLAY,NSN,NSM,MXBND, MAI0138
1      MXWELL,MXRIVR,NPER,IUNIT(15),IOUT,NP,PID,DID,X(LCNLL), MAI0139
2      X(LCCELS),X(LCSMAT),NH,X(LCNDER),JT,NRWD,X(LCIRWD), MAI0140
3      X(LCIBOU),ISN,X(LCJOFF),X(LCIOFF),X(LCHOBS),X(LCWT), MAI0141
4      X(LCB),X(LCB1),IPAR,X(LCCONV),HCLOSE,RCLOSE,X(LCTOP), MAI0142
5      X(LCBOT),X(LCDELR),X(LCDELC),X(LCRINT),X(LCCOFF), MAI0143
6      X(LCROFF),X(LCMLAY),X(LCPR),MOBS,X(LCLN),NQ,NQC,NQT, MAI0144
7      X(LCIBT),X(LCNQOB),X(LCNQCL),X(LCIQOB),X(LCQCLS),IUBD, MAI0145
8      X(LCBUFF),X(LCTOFF),MXDRN,MXSTRM,MAXM,NMM,NZM,LZIL, MAI0146
9      X(LCSFAC),X(LCLZ),X(LCLM),X(LCMATZ),NLLI1,IUNIT,NLLIT, MAI0147
X      EV,NUMR,ICHECK,NPNG,X(LCIPNG),NZER,X(LCIZER), MAI0148
1      X(LCIWPNG),NPO)                                           MAI0149
  IF(IUNIT(15).NE.0) NPER=JT+1                                    MAI0150
  IF(IUNIT(15).NE.0.AND.ISS.NE.0.AND.NPER.GT.1) THEN           MAI0151
    WRITE(IOUT,540)                                               MAI0152
    FORMAT(' DEPENDENT-VARIABLE DATA HAS TIME STEPS >0, BUT ' MAI0153
1      'ISS OF THE BCF PACKAGE INDICATES STEADY-STATE --' MAI0154
2      ' STOP EXECUTION') MAI0155
    STOP                                                         MAI0156
  ENDIF                                                         MAI0157
  IF(IUNIT(15).NE.0.AND.IPAR.GE.1) CALL PARIRP(IUNIT(15),IOUT,NP, MAI0158
1      PID,X(LCWP),X(LCB),X(LCCONV),X(LCLN),LASTX,DMAX,CSA, MAI0159
1      TOL,ITMP,X(LCDD),IOUT,IPRC,IPRINT,FCONV,NPR,EV,NH, MAI0160
1      X(LCWT),NQT,KPRINT,MPR,X(LCPRM),X(LCIWPNG),X(LCSCL), MAI0161
1      ISN,NFIT,LPRINT,NPO,SOSC,NPER,SOSR) MAI0162

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C		MAI0163
C-----	INITIALIZE VALUES FOR PARAMETER ESTIMATION	MAI0164
	DMX=DMAX	MAI0165
	AP=1.	MAI0166
	IFO=0	MAI0167
	FAC=1.	MAI0168
	ADMX=10.*FCONV	MAI0169
	ISN1=ISN	MAI0170
	IF(ISN.EQ.10) ISN=-1	MAI0171
C-----	BEGIN ITERATION LOOP FOR PARAMETER ESTIMATION	MAI0172
	ITERP=0	MAI0173
	ITERPF=ITMXP	MAI0174
290	CONTINUE	MAI0175
	IF(ISN1.EQ.10.AND.MOD(ITERP-1,1+NFIT).EQ.0.AND.IFO.EQ.0) ISN=1	MAI0176
	IF(ISN1.EQ.10.AND.MOD(ITERP,1+NFIT).EQ.0.AND.IFO.EQ.0) ISN=-1	MAI0177
	ITERP=ITERP+1	MAI0178
	IF(IUNIT(15).GT.0.AND.ISN.GT.0.AND.ITERP.GT.1.AND.KNT.GT.0)	MAI0179
1	ITERP=ITERP-1	MAI0180
	IF(IUNIT(15).GT.0.AND.IFO.GT.0) THEN	MAI0181
	ITERPF=ITERP-1	MAI0182
	ITERP=ITMXP	MAI0183
	ENDIF	MAI0184
	IP=-1	MAI0185
	NS=0	MAI0186
	NM=0	MAI0187
	IFLCH=0	MAI0188
C-----	PREPARE FACTOR FOR CONVERGENCE CRITERIA FOR FCONV OPTION	MAI0189
	IF(IUNIT(15).GT.0.AND.IPAR.GT.0.AND.FCONV.GT.0.) THEN	MAI0190
	FAC=(AP*ADMX)/TOL	MAI0191
	IF(FAC.GT.1000.) FAC=1000.	MAI0192
	IF(FAC.LT.10.) FAC=1.	MAI0193
	WRITE(IOUT,550) FAC	MAI0194
	ENDIF	MAI0195
550	FORMAT(///' CONVERGENCE CRITERIA INCREASED BY FACTOR OF',G14.5,///)	MAI0196
C-----	BEGIN LOOP FOR CALCULATING HEADS, SENSITIVITY-EQUATION	MAI0197
C-----	SENSITIVITIES, ADJOINT STATES, AND DERIVATIVES OF HEAD WITH	MAI0198
C-----	RESPECT TO THE ITERATION PARAMETER	MAI0199
295	CONTINUE	MAI0200
	IP=IP+1	MAI0201
	IS=0	MAI0202
C-----	ASSIGN CONVERGENCE CRITERIA.	MAI0203
	IF(IUNIT(15).NE.0.AND.ISN.LT.0) THEN	MAI0204
	HCLOSE=X(LCCONV+IP)	MAI0205
	RCLOSE=X(LCCONV+NPO+1+IP)	MAI0206
	HCLOSE=FAC*HCLOSE	MAI0207
	RCLOSE=FAC*RCLOSE	MAI0208
	ENDIF	MAI0209
C		MAI0210
C7-----	SIMULATE EACH STRESS PERIOD.	MAI0211
	DO 300 KPER=1,NPER	MAI0212
	KKPER=KPER	MAI0213
C		MAI0214
C7A-----	READ STRESS PERIOD TIMING INFORMATION.	MAI0215
	IF(IUNIT(15).EQ.0) CALL BAS1ST(NSTP,DELT,TSMULT,PERTIM,KKPER,	MAI0216
	# INBAS,IOUT)	MAI0217
C		MAI0218
C-----	PREPARE TIME STEPS FOR ADJOINT STATES AND SENSITIVITIES.	MAI0219
	IF(IUNIT(15).NE.0) THEN	MAI0220
	IF(KPER.EQ.1.AND.IP.EQ.0.AND.ITERP.EQ.1) CALL SEN1ST(	MAI0221
	# JT,INBAS,PERLEN,NSTP,X(LCTS),X(LCATS),X(LCSTP),ISN,X(LCBSTP))	MAI0222
C		MAI0223
C-----	ASSIGN TIME STEPS TO VARIABLES.	MAI0224
	IF(IP.EQ.1.AND.ISN.GT.0) THEN	MAI0225
	DELT=X((2*KPER-1)+LCATS-1)	MAI0226
	DELT1=X((2*KPER)+LCATS-1)	MAI0227
	IF(NPER.EQ.1) DELT1=0.	MAI0228
	ELSE	MAI0229
	IF(KPER.EQ.1) DELT=1.E22	MAI0230
	IF(KPER.GT.1) DELT=X(KPER-1+LCTS-1)	MAI0231
	ENDIF	MAI0232
	IF(KPER.EQ.2) THEN	MAI0233
	PERTIM=0.	MAI0234
	TOTIM=0.	MAI0235
	ENDIF	MAI0236
C		MAI0237
C-----	IF THIS TIMESTEP IS THE FIRST IN A NEW PUMPING PERIOD,	MAI0238
C-----	SET IPP=1 AND IS=IS+1.	MAI0239
	IPP=0	MAI0240
	IF(KPER.EQ.1) THEN	MAI0241
	IPP=1	MAI0242
	ELSE	MAI0243
	IF((ISN.LT.0.OR.IP.EQ.0.OR.IP.EQ.2).AND.	MAI0244
1	KPER-1.EQ.INT(X(LCSTP+IS))) THEN	MAI0245

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        IS=IS+1
        IPP=1
    ENDIF
    IF((ISN.GT.0.AND.IP.EQ.1).AND.
1      NPER-KPER.EQ.INT(X(LCBSTP+1+IS))) THEN
        IS=IS+1
        IPP=1
        X(LCBSTP)=X(LCBSTP)-1
    ENDIF
    ENDIF
    ENDIF
C-----PREPARE HEADS, REWIND SOME FILES, REINITIALIZE HNEW
    IF(IUNIT(15).NE.0) THEN
C      REWIND SOME FILES
        IF((IP.GT.0.OR.ITERP.GT.1).AND.((ISN.EQ.-2.AND.KPER.EQ.1)
1          .OR.(ISN.EQ.-1.AND.KPER.EQ.1.AND.IP.EQ.0)
2          .OR.(ISN.GT.0.AND.(KPER.EQ.1.OR.IP.EQ.1))))
3          CALL SEN1RW(IUNIT,NRWD,X(LCIRWD))
        KNST=1
        IF(IPAR.GE.0.AND.ISN.NE.-1)
1          CALL SEN1FM(KNST,NCOL,NROW,NLAY,KPER,IUHEAD,NPER,X(LCSHNV),
2          X(LCSHOL),ISN,IP,X(LCHNEW),NODES,PID,NP,KSTP,PERTIM,TOTIM,
3          X(LCBUFF),X(LCHOLD),ITERP,ISN1,IOUT)
        ENDIF
C
C7B-----READ AND PREPARE INFORMATION FOR STRESS PERIOD.
C-----READ USING PACKAGE READ AND PREPARE MODULES.
        IF(IUNIT(15).EQ.0.OR.IPP.EQ.1) THEN
            IF(IUNIT(15).EQ.0.OR.(ITERP.EQ.1.AND.IP.EQ.0)) THEN
                IF(IUNIT(2).GT.0) CALL WEL1RP(X(LCWELL),NWELLS,MXWELL,IUNIT(2),
1                    IOUT)
                IF(IUNIT(3).GT.0) CALL DRN1RP(X(LCDRAI),NDRAIN,MXDRN,IUNIT(3),
1                    IOUT)
                IF(IUNIT(8).GT.0) CALL RCH1RP(NRCHOP,X(LCIRCH),X(LCRECH),
1                    X(LCDELRL),X(LCDELCL),NROW,NCOL,IUNIT(8),IOUT)
                IF(IUNIT(5).GT.0) CALL EVT1RP(NEVTOP,X(LCIEVT),X(LCEVTR),
1                    X(LCEXDP),X(LCSURF),X(LCDELRL),X(LCDELCL),NCOL,NROW,
1                    IUNIT(5),IOUT)
                IF(IUNIT(4).GT.0) CALL RIV1RP(X(LCRIVR),NRIVER,MXRIVR,IUNIT(4),
1                    IOUT)
                IF(IUNIT(7).GT.0) CALL GH1RP(X(LCBNDS),NBOUND,MXBND,IUNIT(7),
1                    IOUT)
                IF(IUNIT(18).GT.0) CALL STR1RP(X(LCSTRM),X(ICSTRM),NSTREM,
1                    MXSTRM,IUNIT(18),IOUT,X(LCTBAR),NDIV,NSS,
1                    NTRIB,X(LCIVAR),ICALC,IPTFLG)
            ELSE
C-----READ USING REPEATED READ MODULE FROM SEN PACKAGE -- NO PRINTING
                NRP=1
                IF(ISN.GT.0.AND.IP.EQ.1.AND.NPER.NE.1)
1                    NRP=X(LCBSTP)+1
C-----IUNIT POSITION FOR STR PACKAGE IS 18 IN SEN1RR
                IF(ISN.NE.-1.OR.IP.EQ.0)
1                    CALL SEN1RR(IUNIT,X(LCWELL),NWELLS,MXWELL,X(LCDRAI),NDRAIN,
1                    MXDRN,NRCHOP,X(LCIRCH),X(LCRECH),X(LCDELRL),X(LCDELCL),
1                    NROW,NCOL,NLAY,NEVTOP,X(LCIEVT),X(LCEVTR),X(LCEXDP),
1                    X(LCSURF),X(LCRIVR),NRIVER,MXRIVR,X(LCBNDS),NBOUND,
1                    MXBND,IOUT,IP,ITERP,X(LCSTRM),X(ICSTRM),NSTREM,
1                    MXSTRM,X(LCTBAR),NDIV,NSS,NTRIB,X(LCIVAR),ICALC,NRP)
                ENDIF
C-----PUT PARAMETERS IN MODEL ARRAYS.
                IF(IUNIT(15).NE.0.AND.(ISN.NE.-1.OR.IP.EQ.0))
1                    CALL SEN1FN(X(LCCC),X(LCCR),X(LCCV),X(LCCELS),X(LCSMAT),NSN,
2                    NSM,X(LCSC1),X(LCST),X(LCHNEW),X(LCBNDS),NBOUND,
3                    X(LCWELL),NWELLS,X(LCRIVR),NRIVER,X(LCRECH),X(LCDELRL),
4                    X(LCDELCL),NROW,NCOL,NLAY,NP,X(LCNLL),X(LCIBOU),IP,
5                    X(LCB),KPER,NPER,MXBND,MXRIVR,MXWELL,X(LCTRPY),PID,
6                    ISN,ITERP,X(LCB1),IOUT,X(LCLN),X(LCHY),X(LCEVTR),
7                    X(LCDRAI),NDRAIN,MXDRN,X(LCSTRM),MXSTRM,NSTREM,
8                    X(ICSTRM),IUBD,NMM,NZM,LZ11,X(LCSFAC),X(LCLZ),X(LCLM),
9                    X(LCMATZ),NLL11,NLL1T,X(LCSV),X(LCWT),ND,IPRNP,X(LCBUFF),
X                    X(LCIWPG),NPO,NPNG,X(LCIPNG),IOUB,X(LCNDER),X(LCCOFF),
1                    X(LCROFF),X(LCRINT),X(LCJOFF),X(LCIOFF),X(LCMLAY),NH,
2                    MAXM,MOBS,IDRY,JDRY)
                ENDIF
C
C7C-----SIMULATE EACH TIME STEP.
                DO 200 KSTP=1,NSTP
                    KKSTP=KSTP
C
C7C1-----CALCULATE TIME STEP LENGTH. SET HOLD=HNEW.
                    CALL BAS1AD(DELTA,TSMULT,TOTIM,PERTIM,X(LCHNEW),X(LCHOLD),KKSTP,
1                        NCOL,NROW,NLAY)
C-----MODIFY HEADS AT CONSTANT-HEAD BOUNDARIES

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 MAI0328

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      IF(IUNIT(15).GT.0.AND.IUNHEA.GT.0) CALL SEN1RH(IUNHEA,X(LCBUFF), MAI0329
1      X(LCHNEW),KPER,NROW,NCOL,NLAY,X(LCIBOU)) MAI0330
C MAI0331
C FOR CALCULATING ANYTHING BUT ADJOINT STATES: MAI0332
      IF(IUNIT(15).EQ.0.OR.ISN.LT.0.OR.IP.EQ.0.OR.IP.EQ.2) DELT1=DELT MAI0333
C MAI0334
C7C2-----ITERATIVELY FORMULATE AND SOLVE THE EQUATIONS. MAI0335
90 DO 100 KITER=1,MXITER MAI0336
      KKITER=KITER MAI0337
      IF(IUNIT(15).NE.0) THEN MAI0338
        IF((ISN.EQ.-2.AND.IP.GT.0) MAI0339
1        .AND.(KPER.NE.1.OR.KITER.NE.1)) THEN MAI0340
          NS=NS1 MAI0341
          NM=NM1 MAI0342
          IFLCH=IFLCH1 MAI0343
        ENDIF MAI0344
        IF(ISN.EQ.-1) THEN MAI0345
          IF(IP.EQ.1) THEN MAI0346
            NS=0 MAI0347
            NM=0 MAI0348
            IFLCH=0 MAI0349
          ENDIF MAI0350
          IF(KITER.GT.1) THEN MAI0351
            NS=NS1 MAI0352
            NM=NM1 MAI0353
            IFLCH=IFLCH1 MAI0354
          ENDIF MAI0355
          IF(IP.GT.0) GO TO 95 MAI0356
        ENDIF MAI0357
      ENDIF MAI0358
C MAI0359
C7C2A---FORMULATE THE FINITE DIFFERENCE EQUATIONS. MAI0360
      CALL BAS1FM(X(LCHCOF),X(LCRHS),NODES) MAI0361
      IF(IUNIT(1).GT.0) CALL BC1FM(X(LCHCOF),X(LCRHS),X(LCHOLD), MAI0362
1      X(LCSC1),X(LCHNEW),X(LCIBOU),X(LCCR),X(LCCC),X(LCCV), MAI0363
2      X(LCHY),X(LCTRPY),X(LCBOT),X(LCTOP),X(LCSC2), MAI0364
3      X(LCDELRL),X(LCDELRL),DELT,ISS,KKITER,KKSTP,KKPER,NCOL, MAI0365
4      NROW,NLAY,IOUT, MAI0366
5      DELT1,X(LCSHNR),IUNIT(15),IP,ISN,IPAR) MAI0367
      IF(IUNIT(2).GT.0.AND.(IUNIT(15).EQ.0.OR.IP.EQ.0)) MAI0368
1      CALL WELLFM(NWELLS,MXWELL,X(LCRHS),X(LCWELL), MAI0369
1      X(LCIBOU),NCOL,NROW,NLAY) MAI0370
      IF(IUNIT(3).GT.0) CALL DRN1FM(NDRAIN,MXDRN,X(LCDRAI),X(LCHNEW), MAI0371
1      X(LCHCOF),X(LCRHS),X(LCIBOU),NCOL,NROW,NLAY, MAI0372
2      X(LCSHNR),IUNIT(15),IP,ISN) MAI0373
      IF(IUNIT(8).GT.0.AND.(IUNIT(15).EQ.0.OR.IP.EQ.0)) MAI0374
1      CALL RCH1FM(NRCHOP,X(LCIRCH),X(LCRECH), MAI0375
1      X(LCRHS),X(LCIBOU),NCOL,NROW,NLAY) MAI0376
      IF(IUNIT(5).GT.0) CALL EVT1FM(NEVTOP,X(LCIEVT),X(LCEVTR), MAI0377
1      X(LCEXDP),X(LCSURF),X(LCRHS),X(LCHCOF),X(LCIBOU), MAI0378
1      X(LCHNEW),NCOL,NROW,NLAY, MAI0379
2      X(LCSHNR),IUNIT(15),IP,ISN) MAI0380
      IF(IUNIT(4).GT.0) CALL RIV1FM(NRIVER,MXRIVR,X(LCRIVR),X(LCHNEW), MAI0381
1      X(LCHCOF),X(LCRHS),X(LCIBOU),NCOL,NROW,NLAY, MAI0382
2      X(LCSHNR),IUNIT(15),IP,ISN) MAI0383
      IF(IUNIT(18).GT.0) CALL STR1FM(NSTREM,X(LCSTRM),X(ICSTRM), MAI0384
1      X(LCHNEW),X(LCHCOF),X(LCRHS), MAI0385
2      X(LCIBOU),MXSTRM,NCOL,NROW,NLAY,IOUT,NSS, MAI0386
3      X(LCTBAR),NTRIB,X(LCTTRIB),X(LCIVAR),ICALC,CONST, MAI0387
4      X(LCSHNR),IUNIT(15),IP,ISN) MAI0388
      IF(IUNIT(7).GT.0) CALL GH1FM(NBOUND,MXBND,X(LCBNDS),X(LCHCOF), MAI0389
1      X(LCRHS),X(LCIBOU),NCOL,NROW,NLAY, MAI0390
2      IUNIT(15),IP,ISN) MAI0391
C MAI0392
C-----PREPARE RHS TO CALCULATE . . . MAI0393
C----- . . . ADJOINT STATES MAI0394
      IF(IUNIT(15).NE.0.AND.ISN.GT.0.AND.IP.EQ.1) MAI0395
1      CALL SEN1AR(IOUT,NROW,NCOL,NLAY,NP,ISN,NH,X(LCNDER),X(LCHNEW), MAI0396
2      PID,DID,IP,KPER,BUFF,KSTP,PRTIM,TOTIM,X(LCX),X(LCDELRL), MAI0397
3      X(LCDELRL),X(LCIBOU),X(LCCOFF),X(LCROFF),X(LCH),X(LCWT), MAI0398
4      X(LCHOBS),IFO,ITERP,IPAR,X(LCRINT),X(LCJOFF),X(LCJOFF), MAI0399
5      X(LCMLAY),X(LCPR),MOBS,NPER,X(LCB),X(LCLN),NQ,NQC,NQT, MAI0400
6      NQOB,NQCL,X(LCIQOB),X(LCQCLS),X(LCIBT),MXBND,NBOUND, MAI0401
7      X(LCBNDS),MXRIVR,NRIVER,X(LCRIVR),X(LCSHNR),LASTX,ISCALS, MAI0402
8      X(LCTOFF),MXDRN,NDRAIN,X(LCDRAI),MXSTRM,NSTREM,X(LCSTRM), MAI0403
9      X(ICSTRM),X(LCRHS),MAXM) MAI0404
C----- . . . SENSITIVITY-EQUATION SENSITIVITIES OR ITERATION PARAM MAI0405
95 IF(IUNIT(15).NE.0.AND.((ISN.LT.0.AND.IP.GT.0).OR. MAI0406
1      (ISN.GT.0.AND.IP.EQ.2))) THEN MAI0407
      IF(ISN.LT.0) THEN MAI0408
        NM1=NM MAI0409
        NS1=NS MAI0410
        IFLCH1=IFLCH MAI0411

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ENDIF
CALL SENIAP(PID,KPER,NPER,DELT,IP,NP,NCOL,NROW,NLAY,
1      NODES,X(LCHOLD),X(LCSHNV),X(LCHNEW),X(LCXX),
2      X(LCSMAT),X(LCNLL),NM,NSM,X(LCDELR),X(LCDELC),
3      X(LCST),X(LCIBOU),X(LCTRPY),X(LCCELS),NS,NSN,
4      MXWELL,NWELLS,MXBND,NBOUND,MXRIVR,NRIVER,X(LCBNDS),
5      X(LCWELL),X(LCRIVR),NRCHOP,X(LCIRCH),ISN,X(LCRHS),
6      X(LCSHOL),X(LCSCL),X(LCCR),X(LCCC),X(LCCV),
7      IFLCH,IOUT,X(LCHY),X(LCBOT),X(LCSC2),
8      KITER,NDRAIN,MXDRN,X(LCDRAI),X(LCSURF),X(LCEXDP),
9      NEVTOP,MXSTRM,NSTREM,X(LCSTRM),X(ICSTRM),X(LCDD),
X      X(LCB),X(LCLN),X(LCBUFF),X(LCH),X(LCHOBS),X(LCRINT),
1      X(LCIOFF),X(LCJOFF),X(LCNDER),NH,X(LCTOFF),X(LCSCL),
2      NMM,NZM,LZIL,X(LCSFAC),X(LCLZ),X(LCLM),X(LCMATZ),
3      NLLIL,NLLIT)
ENDIF
C-----IF HNEW=HOLD=0 AND RHS=0, NO NEED TO SOLVE.
CALL SEN1NZ(X(LCRHS),X(LCHNEW),NODES,ISA)
IF(IUNIT(15).NE.0.AND.NZER.GT.0.AND.ISA.NE.0)
1      CALL SEN1HZ(X(LCHNEW),KPER,NODES,NZER,X(LCIZER),X(LCRHS),
2      ISA)
IF(ISA.EQ.0) THEN
ICNVG=1
GO TO 110
ENDIF
C
C7C2B---MAKE ONE CUT AT AN APPROXIMATE SOLUTION OR . . .
IF(IUNIT(9).GT.0) CALL SIPLAP(X(LCHNEW),X(LCIBOU),X(LCCR),X(LCCC),
1      X(LCCV),X(LCHCOF),X(LCRHS),X(LCEL),X(LCFL),X(LCGL),X(LCV),
2      X(LCW),X(LCHDCG),X(LCLRCH),NPARM,KKITER,HCLOSE,ACCL,ICNVG,
3      KKSTP,KKPER,IPCALC,IPRSIP,MXITER,NSTP,NCOL,NROW,NLAY,NODES,
4      IOUT)
IF(IUNIT(11).GT.0) CALL SORIAP(X(LCHNEW),X(LCIBOU),X(LCCR),
1      X(LCCC),X(LCCV),X(LCHCOF),X(LCRHS),X(LCA),X(LCRES),X(LCIEQP),
2      X(LCHDCG),X(LCLRCH),KKITER,HCLOSE,ACCL,ICNVG,KKSTP,KKPER,
3      IPRSOP,MXITER,NSTP,NCOL,NROW,NLAY,NSLICE,MBW,IOUT)
C . . . . . EXECUTE MULTIPLE INNER ITERATIONS OR . . .
KPER1=KPER
KSTP1=KSTP
MX1=MXITER
ITER11=ITER1
IF(IUNIT(15).NE.0) THEN
KPER1=IP
KSTP1=KPER-1
ENDIF
IF(IUNIT(13).GT.0) CALL PCG2AP(X(LCHNEW),X(LCIBOU),X(LCCR),
1      X(LCCC),X(LCCV),X(LCHCOF),X(LCRHS),X(LCV),X(LCSS),X(LCP),
2      X(LCCD),X(LCHCHG),X(LCLHCH),X(LCRCHG),X(LCLRCH),
3      KKITER,NITER,HCLOSE,RCLOSE,ICNVG,KSTP1,KPER1,IPRPGC,
4      MX1,ITER11,NPCOND,NBPOL,NSTP,NCOL,NROW,NLAY,NODES,
5      RELAX,IOUT,MUTPCG,IUNIT(15),IP,SN,SP,SR)
C
IF(ICNVG.EQ.1) GO TO 110
100 CONTINUE
105 CONTINUE
C
C7C2C---IF CONVERGENCE CRITERION HAS NOT BEEN MET STOP EXECUTION.
IF(ICNVG.EQ.0) THEN
IF(IUNIT(15).NE.0) THEN
WRITE(IOUT,502) IP,KSTP1,KSTP1
502      FORMAT(' *****WARNINGS ABOUT FOLLOWING TABLE : ',/,
1      ' IP=',I2,/,', '
2      ' IF ISN=-1 OR IP=0, DEPENDENT VARIABLES AT TIME STEPS',
3      ' AFTER',I5,' ARE CALCULATED WITH OLD PARAMETER VALUES.',
4      /,' IF IP=0, DEPENDENT VARIABLES',
5      ' CALCULATED AT TIME STEP',I5,' ARE IN ERROR BECAUSE THE',
6      ' SOLVER DID NOT CONVERGE (SEE BELOW)')
CALL SSEN10(NP,X(LCB),X(LCB1),X(LCIWPG),PID,X(LCWP),IOUT,NH,
1      X(LCH),X(LCHOBS),X(LCWT),DID,X(LCNDER),X(LCROFF),
2      X(LCCOFF),X(LCTOFF),NQT,X(LCIQOB),ND,IPAR,NPR,MPR,
3      X(LCPRM),RSQ,RSQP,1,X(LCLN),RSQH,NPO)
IF(IOUB.GT.0.AND.IPAR.GT.0) CALL SPARI(PID,X(LCBUFF),NP,
1      IOUB,IOUT,ISN)
ENDIF
WRITE(IOUT,500) KPER1,KSTP1
500      FORMAT(' ***** SOLUTION DID NOT CONVERGE FOR KPER=',I5,
1      ', KSTP=',I5,' *****')
IF(IUNIT(15).NE.0) WRITE(IOUT,505) IP
505      FORMAT(' PARAMETER NUMBER (0 FOR HEADS) =',I5)
STOP
ENDIF
110 CONTINUE
C

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C7C3-----DETERMINE WHICH OUTPUT IS NEEDED.
IF(IUNIT(15).EQ.0.OR. IPAR.LT.0.OR.
1  (IPAR.EQ.0.AND.(IP.EQ.0.OR.(ISN.NE.-1.AND.ISA.NE.0))) .OR.
2  (IPAR.GT.0.AND.IP.EQ.0.AND.
3  (IFO.GT.0.AND.(KPRINT.EQ.1.OR.KPRINT.EQ.3))))
4CALL BASLOC(NSTP,KKSTP,ICNVG,X(LCIOFL),NLAY,
5  IBUDFL,ICBCFL,IHDDFL,IUNIT(12),IOUT)
C
C7C4-----CALCULATE BUDGET TERMS. SAVE CELL-BY-CELL FLOW TERMS.
C-----SKIP WHEN CALCULATING ADJOINT STATES OR SENSITIVITIES.
IF(IUNIT(15).EQ.0.OR.(IP.EQ.0.AND.(IPAR.LE.0.OR.
1  (IFO.GT.0.AND.(KPRINT.EQ.1.OR.KPRINT.EQ.3)))) THEN
MSUM=1
IF(IUNIT(1).GT.0) CALL BCF1BD(VBNM,VBVL,MSUM,X(LCHNEW),
1  X(LCIBOU),X(LCHOLD),X(LCSCI),X(LCCR),X(LCCC),X(LCCV),
2  X(LCTOP),X(LCSC2),DELT,ISS,NCOL,NROW,NLAY,KKSTP,KKPER,
3  IBCFCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(2).GT.0) CALL WELL1BD(NWELLS,MXWELL,VBNM,VBVL,MSUM,
1  X(LCWELL),X(LCIBOU),DELT,NCOL,NROW,NLAY,KKSTP,KKPER,IWELCB,
2  ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(3).GT.0) CALL DRN1BD(NDRAIN,MXDRN,VBNM,VBVL,MSUM,
1  X(LCDRAI),DELT,X(LCHNEW),NCOL,NROW,NLAY,X(LCIBOU),KKSTP,
2  KKPER,IDRNCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(8).GT.0) CALL RCH1BD(NRCHOP,X(LCIRCH),X(LCRECH),
1  X(LCIBOU),NROW,NCOL,NLAY,DELT,VBVL,VBNM,MSUM,KKSTP,KKPER,
2  IRCHCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(5).GT.0) CALL EVT1BD(NEVTOP,X(LCIEVT),X(LCEVTR),
1  X(LCEXDP),X(LCSURF),X(LCIBOU),X(LCHNEW),NCOL,NROW,NLAY,
2  DELT,VBVL,VBNM,MSUM,KKSTP,KKPER,IEVTCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(4).GT.0) CALL RIV1BD(NRIVER,MXRIVR,X(LCRIVR),X(LCIBOU),
1  X(LCHNEW),NCOL,NROW,NLAY,DELT,VBVL,VBNM,MSUM,
2  KKSTP,KKPER,IRIVCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(7).GT.0) CALL GH1BD(NBOUND,MXBND,VBNM,VBVL,MSUM,
1  X(LCBNDS),DELT,X(LCHNEW),NCOL,NROW,NLAY,X(LCIBOU),KKSTP,
2  KKPER,IGHBCB,ICBCFL,X(LCBUFF),IOUT)
IF(IUNIT(18).GT.0) CALL STR1BD(NSTREM,X(LCSTRM),X(ICSTRM),
1  X(LCIBOU),MXSTRM,X(LCHNEW),NCOL,NROW,NLAY,DELT,VBVL,
2  VBNM,MSUM,KKSTP,KKPER,ISTCB1,ISTCB2,ICBCFL,X(LCBUFF),IOUT,
3  NTRIB,NSS,X(LCTRIB),X(LCTBAR),X(LCIVAR),ICALC,CONST,IPTFLG)
ENDIF
C-----SET FLAG WHICH INDICATES HETHER THERE IS AN OBS. THIS TIME STEP
IF(ISN.LT.0.AND.IPAREQ.0) CALL SEN1FD(IFLD,X(LCNDER),NH,KPER,
1  X(LCTOFF),NQ,X(LCNQOB),... (LCIQOB),NQT)
C
C7C5---PRINT AND/OR SAVE HEAD, DRAWDOWN OR SENSITIVITY MATRICES.
C-----PRINT OVERALL WATER BUDGET.
IF(IUNIT(15).EQ.0.OR.IPARELT.0.OR.
1  (IPAREEQ.0.AND.(ISNGT.0.OR.IFLDEQ.1)).OR.
2  (IPAREGT.0.AND.IPEQ.0.AND.(IFOGT.0.AND.
3  (KPRINT.EQ.1.OR.KPRINT.EQ.3)))) THEN
KSTP1=KSTP
KPER1=KPER
IF(IUNIT(15).NE.0.AND.IHDDFL.NE.0) THEN
IF(IP.NE.0) THEN
IF(ISN.LT.0) THEN
WRITE(IOUT,510) IP,PID(IP)
ELSE
IF(IP.EQ.1) WRITE(IOUT,515)
IF(IP.EQ.2) WRITE(IOUT,520)
ENDIF
ENDIF
510  FORMAT(/,' SENSITIVITY MATRIX FOR PARAMETER NO.',I5,
1  ', ID ',A4,', SCALED BY *B',/)
515  FORMAT(/,' ADJOINT STATES',/)
520  FORMAT(/,' DERIVATIVE OF HEAD WITH RESPECT TO ITERATION',
1  ' PARAMETER',/)
KPER1=0
KSTP1=KPER-1
IF(ISNGT.0.AND.IPEQ.1) KSTP1=NPER-KPER
ENDIF
IF(ISA.EQ.0) THEN
WRITE(IOUT,525) KSTP1
525  FORMAT(/,' FOR TIME STEP',I5,' ALL VALUES ARE 0.0',/)
ELSE
CALL BASIOT(X(LCHNEW),X(LCSTR),ISTR,X(LCBUFF),X(LCIOFL),
1  MSUM,X(LCIBOU),VBNM,VBVL,KSTP1,KPER1,DELT,
2  PERTIM,TOTIM,ITMUNI,NCOL,NROW,NLAY,ICNVG,
3  IHDDFL,IBUDFL,IHEDFM,IHEDUN,IDDNFM,IDDNUN,IOUT,
4  IUNIT(15),IP,ISN,X(LCB+IP-1))
IF(IUNIT(15).GT.0.AND.IPEGT.0.AND.
1  IUNIT(13).GT.0.AND.MXITER.GT.1) THEN
SE=100.*SR/((SP-SN)/2.)
WRITE(IOUT,530) SP,SN,SR,SE

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530      FORMAT(//,'      SUM OF ALL POSITIVE RATES..... =',G20.5,MAI0578
1          //,'      SUM OF ALL NEGATIVE RATES..... =',G20.5,MAI0579
2          //,'      SUM OF ALL RATES (SUM OF RESIDUALS) =',G20.5,MAI0580
3          //,'      PERCENT DISCREPANCY..... =',F20.2)MAI0581
      ENDIF
      ENDIF
      ENDIF
C-----WRITE HEADS TO IUHEAD; INTERPOLATE, SAVE AND PRINT DATA AND
C-----SENSITIVITIES FOR OBSERVATIONS.
      IF(IUNIT(15).NE.0.AND.ICNVG.NE.0.AND.(ISN.LT.0.OR.IP.EQ.0))
1      CALL SENLOT(IUHEAD,IOUT,NROW,NCOL,NLAY,NP,ISN,NH,X(LCNDER),
2      X(LCHNEW),PID,DID,IP,KPER,X(LCBUFF),KSTP,PERTIM,TOTIM,
3      X(LCX),X(LCDELR),X(LCDELC),X(LCIBOU),X(LCCOFF),X(LCROFF),
4      X(LCH),X(LCWT),X(LCHOBS),IPRINT,IFO,ITERP,IPAR,X(LCRINT),
5      X(LCJOFF),X(LCIOFF),X(LCMLAY),X(LCPR),MOBS,NPER,X(LCB),
6      X(LCLN),NQ,NQC,NQT,X(LCNQOB),X(LCNQCL),X(LCIQOB),X(LCQCLS),
7      X(LCIBT),MXBND,NBOUND,X(LCBNDS),MXRIVR,NRIVER,X(LCRIVR),
8      X(LCSHNW),LASTX,ISCALS,X(LCTOFF),MXDRN,NDRAIN,X(LCDRAI),
9      MXSTRM,NSTREM,X(LCSTRM),X(ICSTRM),MAXM,KPRINT,JDRY,IDRY,NPR,
X      X(LCWP),MPR,X(LCPRM),X(LCIWPG),X(LCBL),IOUB,RSQ,RSQP,RSQO,
1     RSQOO,NPO,SOSC,SOSR)
C
C7C6-----IF ITERATION FAILED TO CONVERGE THEN STOP.
      IF(ICNVG.EQ.0) STOP
C-----IF CONVERGENCE ACHIEVED BY SUM OF SQUARES CRITERIA
      IF(IFO.EQ.2.AND.ISN.LT.0.AND.IP.EQ.NP) THEN
          ITERPF=ITERP
          ITERP=ITMXP
          GO TO 200
      ENDIF
C-----FOR ISN=-1 PUT CORRECT VALUES IN HNEW, SET CONVERGENCE CRITERIA,
C-----AND LOOP BACK TO APPROPRIATE PLACE
      IF(IUNIT(15).NE.0.AND.ISN.EQ.-1) THEN
          IF(IPAR.LT.0) GO TO 200
          IF(IFO.EQ.0.OR.LASTX.NE.0)
1          CALL SEN1FM(KNST,NCOL,NROW,NLAY,KPER,IUHEAD,NPER,X(LCSHNW),
2          X(LCSHOL),ISN,IP,X(LCHNEW),NODES,PID,NP,KSTP,PERTIM,TOTIM,
3          X(LCBUFF),X(LCHOLD),ITERP,ISN1,IOUT)
          IF(IP.EQ.NP) THEN
              IF(KPER.NE.NPER) IP=0
              HCLOSE=X(LCCONV)
              RCLOSE=X(LCCONV+NPO+1)
              HCLOSE=FAC*HCLOSE
              RCLOSE=FAC*RCLOSE
              GO TO 200
          ENDIF
          IF(IFO.EQ.1.AND.LASTX.EQ.0) THEN
              IF(KPER.EQ.1) IP=0
              GO TO 200
          ENDIF
          IP=IP+1
          HCLOSE=X(LCCONV+IP)
          RCLOSE=X(LCCONV+NPO+1+IP)
          HCLOSE=FAC*HCLOSE
          RCLOSE=FAC*RCLOSE
          GO TO 90
      ENDIF
C
C-----ADJOINT STATE AND CONJUGATE-DIRECTION CALCULATIONS
      IF(IUNIT(15).NE.0.AND.ISN.GT.0) THEN
C-----CALCULATE CONTRIBUTION TO THE GRADIENT FROM THE ADJOINT STATE
C-----FROM ONE TIME STEP
          IF(IP.EQ.1) THEN
C-----PRINT TIME STEP LENGTHS USED TO CALCULATE ADJOINT STATES.
              IF(IPAR.EQ.0) WRITE(IOUT,25) DELT,DELT1
25      FORMAT(//,' TIME STEP LENGTHS :',F15.5,', ',F15.5)
C-----PUT APPROPRIATE HEAD VECTORS IN SHNW AND HOLD
              KNST=-1
              CALL SEN1FM(KNST,NCOL,NROW,NLAY,KPER,IUHEAD,NPER,X(LCSHNW),
2              X(LCSHOL),ISN,IP,X(LCHNEW),NODES,PID,NP,KSTP,PERTIM,TOTIM,
3              X(LCBUFF),X(LCHOLD),ITERP,ISN1,IOUT)
C-----CALCULATE THE GRADIENT
              CALL SENLAP(PID,KPER,NPER,DELT,IP,NP,NCOL,NROW,NLAY,
1              NODES,X(LCHOLD),X(LCSHNW),X(LCHNEW),X(LCX),
2              X(LCSMAT),X(LCNLL),NM,NSM,X(LCDELR),X(LCDELC),
3              X(LCST),X(LCIBOU),X(LCTRPY),X(LCCELS),NS,NSN,
4              MXWELL,NWELLS,MXBND,NBOUND,MXRIVR,NRIVER,X(LCBNDS),
5              X(LCWELL),X(LCRIVR),NRCHOP,X(LCIRCH),ISN,X(LCRHS),
6              X(LCSHOL),X(LCSC1),X(LCCR),X(LCCC),X(LCCV),
7              IFLCH,IOUT,X(LCHY),X(LCBOT),X(LCSC2),
8              KITER,NDRAIN,MXDRN,X(LCDRAI),X(LCSURF),X(LCEXDP),
9              NEVTOP,MXSTRM,NSTREM,X(LCSTRM),X(ICSTRM),X(LCDD),
X              X(LCB),X(LCLN),X(LCBUFF),X(LCH),X(LCHOBS),X(LCRINT),MAI0660

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1          X(LCIOFF),X(LCJOFF),X(LCNDER),NH,X(LCTOFF),X(LCSCL),MAI0661
2          NMM,NZM,LZIL,X(LCSFAC),X(LCLZ),X(LCLM),X(LCMATZ),MAI0662
3          NLLIL,NLLIT)MAI0663
C-----SAVE HEAD VECTOR THAT WAS STORED IN HOLDMAI0664
          KNST=0MAI0665
          CALL SENIFM(KNST,NCOL,NROW,NLAY,KPER,IUHEAD,NPER,X(LCSHNW),MAI0666
2          X(LCSHOL),ISN,IP,X(LCHNEW),NODES,PID,NP,KSTP,PBRTIM,TOTIM,MAI0667
3          X(LCBUFF),X(LCHOLD),ITERP,ISN1,IOUT)MAI0668
          ENDIFMAI0669
C-----NONLINEAR REGRESSION BY GRADIENT SEARCHMAI0670
C-----CALCULATE SEARCH DIRECTIONMAI0671
          IF(IPAR.GT.0.AND.KPER.EQ.NPER.AND.IP.NE.2)MAI0672
X      CALL PARLAS(RSQP,KNT,AP,X(LCB),MAI0673
1          X(LCDD),ITERP,X(LCG),NP,IP,X(LCH),X(LCHOBS),X(LCSCL),MAI0674
2          X(LCWP),X(LCWT),ND,MPR,IOUT,SSX,NFIT,ITG,PID,MAI0675
3          X(LCBUFF),X(LCB1),X(LCC),X(LCXX),X(LCLN),IFO,LASTX,ADMX,MAI0676
4          X(LCPRM),IPAR,TOL,ITMXP,NPR,RSQ,AGMX,DID,X(LCNDER),MAI0677
5          X(LCROFF),X(LCCOFF),X(LCTOFF),NH,NQT,X(LCIQOB),IDRY,MAI0678
6          X(LCIWPG),IOUB,EV,ISN,ISN1,X(LCSCLE),X(LCC),NPO)MAI0679
C-----UPDATE PARAMETERSMAI0680
          IF(IP.EQ.2.AND.IFO.EQ.0) CALL PARIAQ(ND,X(LCHOBS),X(LCH),MAI0681
1          X(LCB1),X(LCB),X(LCDD),NP,X(LCWT),X(LCWP),PID,X(LCHNEW),MAI0682
2          NCOL,NROW,NLAY,ISN,IP,X(LCSCL),X(LCPV),NH,X(LCNDER),MAI0683
3          X(LCIOFF),X(LCJOFF),KPER,X(LCMLAY),X(LCIBOU),X(LCRINT),MAI0684
4          DID,X(LCCOFF),X(LCROFF),X(LCDELR),X(LCDELC),X(LCPR),MAI0685
5          MOBS,X(LCLN),NQT,X(LCTOFF),NQ,NQC,NQOB,NQCL,MAI0686
6          X(LCIQOB),X(LCQCLS),X(LCIBT),MXBND,NBOUND,X(LCBNDS),MAI0687
7          MXRIVR,NRIVER,X(LCRIVR),X(LCSHNW),NPER,MXDRN,NDRAIN,MAI0688
8          X(LCDRAI),MXSTRM,NSTREM,X(LCSTRM),X(ICSTRM),MAI0689
9          ADMX,X(LCPRM),MPR,IOUT,DMX,DMAX,AP,NPR,ITERP,AGMX,MAXM,MAI0690
X          JDRY,IPAR,IOUB,NPO)MAI0691
          ENDIFMAI0692
C-----END OF TIME STEP (KSTP) AND STRESS PERIOD (KPER) LOOPSMAI0693
200 CONTINUEMAI0694
300 CONTINUEMAI0695
C-----INCREMENT IP AND CONTINUE?MAI0696
          IF(IUNIT(15).NE.0.AND.
1          (ISN.EQ.-2.AND.((IPAR.EQ.0.AND.IP.NE.NP).OR.
1          (IPAR.GT.0.AND.IP.NE.NP.AND.(IFO.EQ.0.OR.
1          LASTX.NE.0))))MAI0697
1          .OR.
1          (ISN.GT.0.AND.((IP.EQ.0.AND.IPAR.GE.0.AND.KNT.EQ.0).OR.
1          (IP.EQ.1.AND.PAR.GT.0.AND.IFO.EQ.0)))) GO TO 295MAI0698
C-----ANOTHER GRADIENT-SEARCH REGRESSION ITERATION?MAI0699
          IF(IPAR.GT.0.AND.ISN.GT.0.AND.ITERP.LT.ITMXP.AND.IFO.EQ.0)MAI0700
1          GO TO 290MAI0701
C-----CALCULATE FINAL GAUSS-NEWTON STATISTICS FOR GRADIENT-SEARCHMAI0702
C-----REGRESSION?MAI0703
          IF(IPAR.GT.0.AND.ISN.GT.0.AND.IFO.NE.0.AND.LASTX.NE.0) THENMAI0704
            ISN=LASTXMAI0705
            GO TO 290MAI0706
          ENDIFMAI0707
C-----NONLINEAR REGRESSION BY MODIFIED GAUSS-NEWTONMAI0708
          IF(IUNIT(15).NE.0.AND.IPAR.GT.0.AND.ISN.LT.0) THENMAI0709
C-----EXECUTE ONE GAUSS-NEWTON ITERATIONMAI0710
          CALL PARIAQ(X(LCX),X(LCB),ND,NP,X(LCHOBS),X(LCWT),X(LCWP),MAI0711
1          X(LCC),X(LCSCLE),X(LCG),X(LCH),X(LCDD),DMAX,CSA,TOL,PID,MAI0712
1          IND,IFO,AMP,AP,DMX,IOUT,X(LCB1),ITERP,IPRINT,ADMX,X(LCLN),MAI0713
1          LASTX,MPR,X(LCPRM),NPR,IOUB,RSQ,JMAX,ITMXP,ISN1,NFIT,MAI0714
1          NPO,X(LCR),X(LCGD),X(LCU),NOPT,X(LCXD),NPER,X(LCS),SOSR)MAI0715
C-----DO CALCULATIONS REQUIRED TO DO ANOTHER GAUSS-NEWTON ITERATION?MAI0716
          IF(ITERP.LT.ITMXP.AND.IND.EQ.0) GO TO 290MAI0717
C-----FINAL OUTPUTMAI0718
          IF(IND.GT.0.OR.IFO.EQ.0) CALL SSENLO(NP,X(LCB),X(LCB1),MAI0719
1          X(LCIWPG),PID,X(LCWP),IOUT,NH,X(LCH),X(LCHOBS),X(LCWT),DID,MAI0720
2          X(LCNDER),X(LCROFF),X(LCCOFF),X(LCTOFF),NQT,X(LCIQOB),ND,MAI0721
3          IPAR,NPR,MPR,X(LCPRM),RSQ,RSQ,1,X(LCLN),RSQH,NPO)MAI0722
          IF(IOUB.GT.0) CALL SPARIP(PID,X(LCBUFF),NP,IOUB,IOUT,ISN)MAI0723
          CALL PARLOT(X(LCC),X(LCWT),NP,IOUR,RSQ,IOUT,X(LCBUFF),ND,IIRC,MAI0724
1          IFO,IND,PID,X(LCSCLE),X(LCB),X(LCHOBS),X(LCH),NPR,X(LCB1),MAI0725
2          X(LCWP),ITERPF,X(LCX),X(LCHNEW),X(LCLN),MPR,X(LCPRM),MAI0726
3          X(LCIWPG),NODES,LPRINT,IDRY,EV,RSQ,ISN,NPO)MAI0727
          ENDIFMAI0728
C-----RESIDUAL ANALYSISMAI0729
          IF(IUNIT(15).GT.0) CALL PARIRE(NP,X(LCB),X(LCB1),X(LCIWPG),MAI0730
1          X(LCWP),IOUT,NH,X(LCH),X(LCHOBS),X(LCWT),DID,NQT,ND,MAI0731
2          IPAR,NPR,MPR,X(LCPRM),NPO)MAI0732
C-----END PROGRAMMAI0733
STOPMAI0734
C-----STOPMAI0735
ENDMAI0736

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# Modified Primary Modules and Submodules

SUBROUTINE BASLOT(HNEW,STRT,ISTRT,BUFF,IOFLG,MSUM,IBOUND,VBNM,	SUB0001
1 VBV, KSTP, KPER, DELT, PERTIM, TOTIM, ITMUNI, NCOL, NROW, NLAY, ICNVG,	SUB0002
2 IHDDFL, IBUDFL, IHEDFM, IHEDUN, IDDNFM, IDDNUN, IOUT,	SUB0003
3 IU, IP, ISN, B)	SUB0004
C-----VERSION 1522 12MAY1987 BASLOT	SUB0005
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0006
C	SUB0007
C *****	SUB0008
C OUTPUT TIME, VOLUMETRIC BUDGET, HEAD, AND DRAWDOWN	SUB0009
C *****	SUB0010
C	SUB0011
C SPECIFICATIONS:	SUB0012
C -----	SUB0013
C CHARACTER*4 VBNM	SUB0014
C DOUBLE PRECISION HNEW,DB	SUB0015
C	SUB0016
C DIMENSION HNEW(NCOL,NROW,NLAY),STRT(NCOL,NROW,NLAY),	SUB0017
1 VBNM(4,20),VBV(4,20),IOFLG(NLAY,4),	SUB0018
2 IBOUND(NCOL,NROW,NLAY),BUFF(NCOL,NROW,NLAY)	SUB0019
C -----	SUB0020
C	SUB0021
C1-----CLEAR PRINTOUT FLAG (IPFLG)	SUB0022
C IPFLG=0	SUB0023
C	SUB0024
C2-----IF ITERATIVE PROCEDURE FAILED TO CONVERGE PRINT MESSAGE	SUB0025
IF(ICNVG.EQ.0) WRITE(IOUT,1) KSTP,KPER	SUB0026
1 FORMAT(1H0,10X,'****FAILED TO CONVERGE IN TIME STEP',I3,	SUB0027
1 ' OF STRESS PERIOD',I3,'****')	SUB0028
C	SUB0029
C3-----IF HEAD AND DRAWDOWN FLAG (IHDDFL) IS SET WRITE HEAD AND	SUB0030
C3-----DRAWDOWN IN ACCORDANCE WITH FLAGS IN IOFLG.	SUB0031
IF(IHDDFL.EQ.0) GO TO 100	SUB0032
C	SUB0033
C IDUM=KPER	SUB0034
IF(IU.GT.0.AND.IP.GT.0) THEN	SUB0035
IDUM=IP	SUB0036
IF(ISN.LT.0) THEN	SUB0037
DB=DBLE(B)	SUB0038
DO 50 K=1,NLAY	SUB0039
DO 50 I=1,NROW	SUB0040
DO 50 J=1,NCOL	SUB0041
50 HNEW(J,I,K)=HNEW(J,I,K)*DB	SUB0042
ENDIF	SUB0043
ENDIF	SUB0044
CALL SBASIH(HNEW,BUFF,IOFLG,KSTP,IDUM,NCOL,NROW,	SUB0045
1 NLAY,IOUT,IHEDFM,IHEDUN,IPFLG,PERTIM,TOTIM)	SUB0046
CALL SBASID(HNEW,BUFF,IOFLG,KSTP,KPER,NCOL,NROW,NLAY,IOUT,	SUB0047
1 IDDNFM,IDDNUN,STRT,ISTRT,IBOUND,IPFLG,PERTIM,TOTIM)	SUB0048
IF(IU.GT.0.AND.IP.GT.0.AND.ISN.LT.0) THEN	SUB0049
DO 70 K=1,NLAY	SUB0050
DO 70 I=1,NROW	SUB0051
DO 70 J=1,NCOL	SUB0052
70 HNEW(J,I,K)=HNEW(J,I,K)/DB	SUB0053
ENDIF	SUB0054
C	SUB0055
C4-----PRINT TOTAL BUDGET IF REQUESTED	SUB0056
C-----MODIFIED FOR CALCULATING SENSITIVITIES	SUB0057
100 IF(IBUDFL.EQ.0.OR.IP.NE.0) GO TO 120	SUB0058
CALL SBASIV(MSUM,VBNM,VBV,KSTP,KPER,IOUT)	SUB0059
IPFLG=1	SUB0060
C	SUB0061
C5-----END PRINTOUT WITH TIME SUMMARY AND FORM FEED IF ANY PRINTOUT	SUB0062
C5-----WILL BE PRODUCED.	SUB0063
120 IF(IPFLG.EQ.0) RETURN	SUB0064
CALL SBASIT(KSTP,KPER,DELT,PERTIM,TOTIM,ITMUNI,IOUT)	SUB0065
WRITE(IOUT,101)	SUB0066
101 FORMAT(1H1)	SUB0067
C	SUB0068
C6-----RETURN	SUB0069
RETURN	SUB0070
END	SUB0071

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SUBROUTINE BCF1RP( IBOUND, HNEW, SC1, HY, CR, CC, CV, DELR, DELC,
1 BOT, TOP, SC2, TRPY, IN, ISS, NCOL, NROW, NLAY, NODES, IOUT,
2 IU, ST, SV)
C
C-----VERSION 1636 15MAY1987 BCF1RP
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992
C
C *****
C READ AND INITIALIZE DATA FOR BLOCK-CENTERED FLOW PACKAGE
C *****
C SPECIFICATIONS:
C -----
C CHARACTER*4 ANAME
C DOUBLE PRECISION HNEW
C
C DIMENSION HNEW(NODES), SC1(NODES), HY(NODES), CR(NODES), CC(NODES),
1 CV(NODES), ANAME(6,10), DELR(NCOL), DELC(NROW), BOT(NODES),
1 TOP(NODES), SC2(NODES), TRPY(NLAY), IBOUND(NODES)
2 ST(NCOL, NROW, NLAY), SV(NCOL*NROW)
C
C COMMON /FLWCOM/LAYCON(80)
C
C DATA ANAME(1,1), ANAME(2,1), ANAME(3,1), ANAME(4,1), ANAME(5,1),
1 ANAME(6,1) / ' ', 'PRIM', 'ARY', 'STOR', 'AGE', 'COEF' /
C DATA ANAME(1,2), ANAME(2,2), ANAME(3,2), ANAME(4,2), ANAME(5,2),
1 ANAME(6,2) / ' ', 'TRAN', 'SMIS', 'AL', 'ONG', 'ROWS' /
C DATA ANAME(1,3), ANAME(2,3), ANAME(3,3), ANAME(4,3), ANAME(5,3),
1 ANAME(6,3) / 'H', 'YD', 'COND', 'AL', 'ONG', 'ROWS' /
C DATA ANAME(1,4), ANAME(2,4), ANAME(3,4), ANAME(4,4), ANAME(5,4),
1 ANAME(6,4) / 'VERT', 'HYD', 'CON', 'D/T', 'HICK', 'NESS' /
C DATA ANAME(1,5), ANAME(2,5), ANAME(3,5), ANAME(4,5), ANAME(5,5),
1 ANAME(6,5) / ' ', ' ', ' ', ' ', 'BO', 'TTOM' /
C DATA ANAME(1,6), ANAME(2,6), ANAME(3,6), ANAME(4,6), ANAME(5,6),
1 ANAME(6,6) / ' ', ' ', ' ', ' ', ' ', 'TOP' /
C DATA ANAME(1,7), ANAME(2,7), ANAME(3,7), ANAME(4,7), ANAME(5,7),
1 ANAME(6,7) / 'SE', 'COND', 'ARY', 'STOR', 'AGE', 'COEF' /
C DATA ANAME(1,8), ANAME(2,8), ANAME(3,8), ANAME(4,8), ANAME(5,8),
1 ANAME(6,8) / 'COLU', 'MN T', 'O RO', 'W AN', 'ISOT', 'ROPY' /
C DATA ANAME(1,9), ANAME(2,9), ANAME(3,9), ANAME(4,9), ANAME(5,9),
1 ANAME(6,9) / ' ', ' ', ' ', ' ', 'DELR' /
C DATA ANAME(1,10), ANAME(2,10), ANAME(3,10), ANAME(4,10), ANAME(5,10),
1 ANAME(6,10) / ' ', ' ', ' ', ' ', 'DELC' /
C
C1-----CALCULATE NUMBER OF NODES IN A LAYER AND READ TRPY, DELR, DELC
NIJ=NCOL*NROW
C
C CALL UIDREL(TRPY, ANAME(1,8), NLAY, IN, IOUT)
C CALL UIDREL(DELR, ANAME(1,9), NCOL, IN, IOUT)
C CALL UIDREL(DELC, ANAME(1,10), NROW, IN, IOUT)
C
C2-----READ ALL PARAMETERS FOR EACH LAYER
KT=0
KB=0
DO 200 K=1, NLAY
KK=K
C
C2A-----FIND ADDRESS OF EACH LAYER IN THREE DIMENSION ARRAYS.
IF(LAYCON(K).EQ.1 .OR. LAYCON(K).EQ.3) KB=KB+1
IF(LAYCON(K).EQ.2 .OR. LAYCON(K).EQ.3) KT=KT+1
LOC=1+(K-1)*NIJ
LOCB=1+(KB-1)*NIJ
LOCT=1+(KT-1)*NIJ
C
C2B-----READ PRIMARY STORAGE COEFFICIENT INTO ARRAY SC1 IF TRANSIENT
IF(ISS.EQ.0) CALL U2DREL(SC1(LOC), ANAME(1,1), NROW, NCOL, KK, IN, IOUT)
C
C2C-----READ TRANSMISSIVITY INTO ARRAY CC IF LAYER TYPE IS 0 OR 2
IF(LAYCON(K).EQ.3 .OR. LAYCON(K).EQ.1) GO TO 100
CALL U2DREL(CC(LOC), ANAME(1,2), NROW, NCOL, KK, IN, IOUT)
IF(IU.GT.0) THEN
DO 300 I=1, NROW
DO 300 J=1, NCOL
300 ST(J,I,K)=CC(LOC-1+(J+(I-1)*NCOL))
ENDIF
GO TO 110
C
C2D-----READ HYDRAULIC CONDUCTIVITY(HY) AND BOTTOM ELEVATION(BOT)
C2D-----IF LAYER TYPE IS 1 OR 3
100 CALL U2DREL(HY(LOCB), ANAME(1,3), NROW, NCOL, KK, IN, IOUT)
CALL U2DREL(BOT(LOCB), ANAME(1,5), NROW, NCOL, KK, IN, IOUT)

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C-----ADDED FOR PARAMETER ESTIMATION	SUB0155
IF(IU.GT.0) THEN	SUB0156
DO 310 I=1,NROW	SUB0157
DO 310 J=1,NCOL	SUB0158
310 ST(J,I,K)=HY(LOCB-1+(J+(I-1)*NCOL))	SUB0159
ENDIF	SUB0160
C	SUB0161
C2E-----READ VERTICAL HYCOND/THICK INTO ARRAY CV IF NOT BOTTOM LAYER	SUB0162
C2E----- READ AS HYCOND/THICKNESS -- CONVERTED TO CONDUCTANCE LATER	SUB0163
110 IF(K.EQ.NLAY) GO TO 120	SUB0164
CALL U2DREL(CV(LOC),ANAME(1,4),NROW,NCOL,KK,IN,IOUT)	SUB0165
C-----ADDED FOR PARAMETER ESTIMATION	SUB0166
IF(IU.GT.0.AND.LAYCON(K).EQ.1) THEN	SUB0167
DO 115 II=1,NIJ	SUB0168
115 SV(II)=CV(II)	SUB0169
ENDIF	SUB0170
C	SUB0171
C2F-----READ SECONDARY STORAGE COEFFICIENT INTO ARRAY SC2 IF TRANSIENT	SUB0172
C2F-----AND LAYER TYPE IS 2 OR 3	SUB0173
120 IF(LAYCON(K).NE.3 .AND. LAYCON(K).NE.2) GO TO 200	SUB0174
IF(ISS.EQ.0)CALL U2DREL(SC2(LOCT),ANAME(1,7),NROW,NCOL,KK,IN,IOUT)	SUB0175
C	SUB0176
C2G-----READ TOP ELEVATION(TOP) IF LAYER TYPE IS 2 OR 3	SUB0177
CALL U2DREL(TOP(LOCT),ANAME(1,6),NROW,NCOL,KK,IN,IOUT)	SUB0178
200 CONTINUE	SUB0179
C	SUB0180
C3-----PREPARE AND CHECK BCF DATA	SUB0181
CALL SBCFLN(HNEW,IBOUND,SC1,SC2,CR,CC,CV,HY,TRPY,DELR,DELC,ISS,	SUB0182
1 NCOL,NROW,NLAY,IOUT)	SUB0183
C	SUB0184
C4-----RETURN	SUB0185
RETURN	SUB0186
END	SUB0187
SUBROUTINE BCF1FM(HCOF,RHS,HOLD,SC1,HNEW,IBOUND,CR,CC,CV,HY,TRPY,	SUB0188
1 BOT,TOP,SC2,DELR,DELC,DELT,ISS,KITER,KSTP,KPER,	SUB0189
2 NCOL,NROW,NLAY,IOUT,	SUB0190
3 DELT1,SHNW,IU,IP,ISN,IPAR)	SUB0191
C-----VERSION 1640 15MAY1987 BCF1FM	SUB0192
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0193
C	SUB0194
C	SUB0195
C *****	SUB0196
C ADD LEAKAGE CORRECTION AND STORAGE TO HCOF AND RHS, AND CALCULATE	SUB0197
C CONDUCTANCE AS REQUIRED	SUB0198
C *****	SUB0199
C	SUB0200
C SPECIFICATIONS:	SUB0201
C -----	SUB0202
C DOUBLE PRECISION HNEW	SUB0203
C	SUB0204
C DIMENSION HCOF(NCOL,NROW,NLAY),RHS(NCOL,NROW,NLAY),	SUB0205
1 HOLD(NCOL,NROW,NLAY),SC1(NCOL,NROW,NLAY),HNEW(NCOL,NROW,NLAY),	SUB0206
2 IBOUND(NCOL,NROW,NLAY),CR(NCOL,NROW,NLAY),	SUB0207
3 CC(NCOL,NROW,NLAY),CV(NCOL,NROW,NLAY),HY(NCOL,NROW,NLAY),	SUB0208
4 TRPY(NLAY),BOT(NCOL,NROW,NLAY),TOP(NCOL,NROW,NLAY),DELR(NCOL),	SUB0209
5 DELC(NROW),SC2(NCOL,NROW,NLAY)	SUB0210
6 ,SHNW(NCOL,NROW,NLAY)	SUB0211
C	SUB0212
C COMMON /FLWCOM/LAYCON(80)	SUB0213
C -----	SUB0214
C KB=0	SUB0215
C KT=0	SUB0216
C	SUB0217
C1-----FOR EACH LAYER: IF T VARIES CALCULATE HORIZONTAL CONDUCTANCES	SUB0218
DO 100 K=1,NLAY	SUB0219
KK=K	SUB0220
IF(LAYCON(K).EQ.3 .OR. LAYCON(K).EQ.2) KT=KT+1	SUB0221
C	SUB0222
C1A-----IF LAYER TYPE IS NOT 1 OR 3 THEN SKIP THIS LAYER.	SUB0223
IF(LAYCON(K).NE.3 .AND. LAYCON(K).NE.1) GO TO 100	SUB0224
KB=KB+1	SUB0225
C	SUB0226
C1B-----FOR LAYER TYPES 1 & 3 CALL SBCFHL TO CALCULATE	SUB0227
C1B-----HORIZONTAL CONDUCTANCES.	SUB0228
C-----MODIFIED FOR PARAMETER ESTIMATION	SUB0229
CALL SBCFHL(HNEW,IBOUND,CR,CC,CV,HY,TRPY,DELR,DELC,BOT,TOP,	SUB0230
1 KK,KB,KT,KITER,KSTP,KPER,NCOL,NROW,NLAY,IOUT,	SUB0231
2 SHNW,IU,IP,ISN,IPAR)	SUB0232
100 CONTINUE	SUB0233
C	SUB0234
C2-----IF THE SIMULATION IS TRANSIENT ADD STORAGE TO HCOF AND RHS	SUB0235

IF(ISS.NE.0) GO TO 201	SUB0236
TLED=1./DELT	SUB0237
C-----TIME STEP FOR CALCULATION OF ADJOINT STATES	SUB0238
TLED1=1./DELT1	SUB0239
KT=0	SUB0240
DO 200 K=1,NLAY	SUB0241
C	SUB0242
C3-----SEE IF THIS LAYER IS CONVERTIBLE OR NON-CONVERTIBLE.	SUB0243
IF(LAYCON(K).EQ.3 .OR. LAYCON(K).EQ.2) GO TO 150	SUB0244
C4-----NON-CONVERTIBLE LAYER, SO USE PRIMARY STORAGE	SUB0245
DO 140 I=1,NROW	SUB0246
DO 140 J=1,NCOL	SUB0247
IF(IBOUND(J,I,K).LE.0) GO TO 140	SUB0248
RHO=SC1(J,I,K)*TLED	SUB0249
C-----FOR ADJOINT STATES	SUB0250
RHO1=SC1(J,I,K)*TLED1	SUB0251
HCOF(J,I,K)=HCOF(J,I,K)-RHO	SUB0252
C-----LINE MODIFIED TO CALCULATE ADJOINT STATES (RHO TO RHO1)	SUB0253
RHS(J,I,K)=RHS(J,I,K)-RHO1*HOLD(J,I,K)	SUB0254
140 CONTINUE	SUB0255
GO TO 200	SUB0256
C	SUB0257
C5-----A CONVERTIBLE LAYER, SO CHECK OLD AND NEW HEADS TO DETERMINE	SUB0258
C5-----WHEN TO USE PRIMARY AND SECONDARY STORAGE	SUB0259
150 KT=KT+1	SUB0260
DO 180 I=1,NROW	SUB0261
DO 180 J=1,NCOL	SUB0262
C	SUB0263
C5A-----IF THE CELL IS EXTERNAL THEN SKIP IT.	SUB0264
IF(IBOUND(J,I,K).LE.0) GO TO 180	SUB0265
TP=TOP(J,I,KT)	SUB0266
RHO2=SC2(J,I,KT)*TLED	SUB0267
RHO1=SC1(J,I,K)*TLED	SUB0268
C-----TO CALCULATE ADJOINT STATES	SUB0269
RHO21=SC2(J,I,KT)*TLED1	SUB0270
RHO11=SC1(J,I,K)*TLED1	SUB0271
C	SUB0272
C5B-----FIND STORAGE FACTOR AT START OF TIME STEP.	SUB0273
C-----MODIFIED FOR ADJOINT STATES (RHO2 TO RHO21, AND RHO1 TO RHO11)	SUB0274
SOLD=RHO21	SUB0275
IF(HOLD(J,I,K).GT.TP) SOLD=RHO11	SUB0276
C	SUB0277
C5C-----FIND STORAGE FACTOR AT END OF TIME STEP.	SUB0278
HTMP=HNEW(J,I,K)	SUB0279
SNEW=RHO2	SUB0280
IF(HTMP.GT.TP) SNEW=RHO1	SUB0281
C-----ADDED FOR ADJOINT STATES	SUB0282
SNEW1=RHO21	SUB0283
IF(HTMP.GT.TP) SNEW1=RHO11	SUB0284
C	SUB0285
C5D-----ADD STORAGE TERMS TO RHS AND HCOF.	SUB0286
HCOF(J,I,K)=HCOF(J,I,K)-SNEW	SUB0287
C-----MODIFIED FOR ADJOINT STATES (SNEW TO SNEW1)	SUB0288
RHS(J,I,K)=RHS(J,I,K) - SOLD*(HOLD(J,I,K)-TP) - SNEW1*TP	SUB0289
C	SUB0290
180 CONTINUE	SUB0291
C	SUB0292
200 CONTINUE	SUB0293
C	SUB0294
C6-----FOR EACH LAYER DETERMINE IF CORRECTION TERMS ARE NEEDED FOR	SUB0295
C6-----FLOW DOWN INTO PARTIALLY SATURATED LAYERS.	SUB0296
201 KT=0	SUB0297
DO 300 K=1,NLAY	SUB0298
C	SUB0299
C7-----SEE IF CORRECTION IS NEEDED FOR LEAKAGE FROM ABOVE.	SUB0300
IF(LAYCON(K).NE.3 .AND. LAYCON(K).NE.2) GO TO 250	SUB0301
KT=KT+1	SUB0302
IF(K.EQ.1) GO TO 250	SUB0303
C	SUB0304
C7A-----FOR EACH CELL MAKE THE CORRECTION IF NEEDED.	SUB0305
DO 220 I=1,NROW	SUB0306
DO 220 J=1,NCOL	SUB0307
C	SUB0308
C7B-----IF THE CELL IS EXTERNAL (IBOUND<=0) THEN SKIP IT.	SUB0309
IF(IBOUND(J,I,K).LE.0) GO TO 220	SUB0310
HTMP=HNEW(J,I,K)	SUB0311
C	SUB0312
C7C-----IF HEAD IS ABOVE TOP THEN CORRECTION NOT NEEDED	SUB0313
IF(HTMP.GE.TOP(J,I,KT)) GO TO 220	SUB0314
C	SUB0315
C7D-----WITH HEAD BELOW TOP ADD CORRECTION TERMS TO RHS AND HCOF.	SUB0316
RHS(J,I,K)=RHS(J,I,K) + CV(J,I,K-1)*TOP(J,I,KT)	SUB0317
HCOF(J,I,K)=HCOF(J,I,K) + CV(J,I,K-1)	SUB0318

220 CONTINUE	SUB0319
C	SUB0320
C8-----SEE IF THIS LAYER MAY NEED CORRECTION FOR LEAKAGE TO BELOW.	SUB0321
250 IF(K.EQ.NLAY) GO TO 300	SUB0322
IF(LAYCON(K+1).NE.3 .AND. LAYCON(K+1).NE.2) GO TO 300	SUB0323
KT=KT+1	SUB0324
C	SUB0325
C8A-----FOR EACH CELL MAKE THE CORRECTION IF NEEDED.	SUB0326
DO 280 I=1,NROW	SUB0327
DO 280 J=1,NCOL	SUB0328
C	SUB0329
C8B-----IF CELL IS EXTERNAL (IBOUND<=0) THEN SKIP IT.	SUB0330
IF(IBOUND(J,I,K).LE.0) GO TO 280	SUB0331
C	SUB0332
C8C-----IF HEAD IN THE LOWER CELL IS LESS THAN TOP ADD CORRECTION	SUB0333
C8C-----TERM TO RHS.	SUB0334
HTMP=HNEW(J,I,K+1)	SUB0335
IF(HTMP.LT.TOP(J,I,KT)) RHS(J,I,K)=RHS(J,I,K)	SUB0336
1 - CV(J,I,K)*(TOP(J,I,KT)-HTMP)	SUB0337
280 CONTINUE	SUB0338
300 CONTINUE	SUB0339
C	SUB0340
C9-----RETURN	SUB0341
RETURN	SUB0342
END	SUB0343
SUBROUTINE SBCFLH(HNEW,IBOUND,CR,CC,CV,HY,TRPY,DELR,DELC	SUB0344
1,BOT,TOP,K,KB,KT,KITER,KSTP,KPER,NCOL,NROW,NLAY,IOUT,	SUB0345
2SHNW,IU,IP,ISN,IPAR)	SUB0346
C	SUB0347
C-----VERSION 1442 31DEC1986 SBCFLH	SUB0348
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0349
C	SUB0350
C	SUB0351
C *****	SUB0352
C COMPUTE CONDUCTANCE FROM SATURATED THICKNESS AND HYDRAULIC	SUB0353
C CONDUCTIVITY	SUB0354
C *****	SUB0355
C	SUB0356
C SPECIFICATIONS:	SUB0357
C -----	SUB0358
C DOUBLE PRECISION HNEW,HD	SUB0359
C	SUB0360
C DIMENSION HNEW(NCOL,NROW,NLAY),IBOUND(NCOL,NROW,NLAY)	SUB0361
C 1, CR(NCOL,NROW,NLAY), CC(NCOL,NROW,NLAY), CV(NCOL,NROW,NLAY)	SUB0362
C 2,HY(NCOL,NROW,NLAY), TRPY(NLAY), DELR(NCOL), DELC(NROW)	SUB0363
C 3, BOT(NCOL,NROW,NLAY),TOP(NCOL,NROW,NLAY),	SUB0364
C 4 SHNW(NCOL,NROW,NLAY)	SUB0365
C	SUB0366
C COMMON /FLWCOM/LAYCON(80)	SUB0367
C -----	SUB0368
C	SUB0369
C1-----CALCULATE TRANSMISSIVITY AT EACH ACTIVE CELL. TRANSMISSIVITY	SUB0370
C1-----WILL BE STORED TEMPORARILY IN THE CC ARRAY.	SUB0371
DO 200 I=1,NROW	SUB0372
DO 200 J=1,NCOL	SUB0373
C	SUB0374
C2-----IF CELL IS INACTIVE THEN SET T=0 & MOVE ON TO NEXT CELL.	SUB0375
IF(IBOUND(J,I,K).NE.0) GO TO 10	SUB0376
CC(J,I,K)=0.	SUB0377
GO TO 200	SUB0378
C	SUB0379
C3-----CALCULATE SATURATED THICKNESS.	SUB0380
10 HD=HNEW(J,I,K)	SUB0381
C-----LINE ADDED FOR PARAMETER ESTIMATION PACKAGE	SUB0382
IF(IU.NE.0.AND.ISN.NE.-1.AND.IP.NE.0) HD=SHNW(J,I,K)	SUB0383
IF(LAYCON(K).EQ.1) GO TO 50	SUB0384
IF(HD.GT.TOP(J,I,KT)) HD=TOP(J,I,KT)	SUB0385
50 THCK=HD-BOT(J,I,KB)	SUB0386
C	SUB0387
C4-----CHECK TO SEE IF SATURATED THICKNESS IS GREATER THAN ZERO.	SUB0388
IF(THCK.LE.0.) GO TO 100	SUB0389
C	SUB0390
C5-----IF SATURATED THICKNESS>0 THEN T=K*THICKNESS.	SUB0391
CC(J,I,K)=THCK*HY(J,I,KB)	SUB0392
GO TO 200	SUB0393
C	SUB0394
C6-----WHEN SATURATED THICKNESS < 0, PRINT A MESSAGE AND SET	SUB0395
C6-----TRANSMISSIVITY, IBOUND, AND VERTICAL CONDUCTANCE =0	SUB0396
100 WRITE(IOUT,150) K,I,J,KITER,KSTP,KPER	SUB0397
150 FORMAT(1H0,10(' '), 'NODE',3I4, ' (LAYER,ROW,COL) WENT DRY'	SUB0398
1 , ' AT ITERATION =',I3, ' TIME STEP =',I3	SUB0399

2	, ' STRESS PERIOD =' , I3)	SUB0400
	HNEW(J,I,K)=1.D30	SUB0401
C-----	LINE ADDED FOR PARAMETER-ESTIMATION PACKAGE	SUB0402
	IF(IU.NE.0.AND.IPAR.GE.0) HNEW(J,I,K)=BOT(J,I,KB)+10.	SUB0403
	CC(J,I,K)=0.	SUB0404
	IBOUND(J,I,K)=0	SUB0405
	IF(K.LT.NLAY) CV(J,I,K)=0.	SUB0406
	IF(K.GT.1) CV(J,I,K-1)=0.	SUB0407
	GO TO 200	SUB0408
200	CONTINUE	SUB0409
C		SUB0410
C7-----	COMPUTE HORIZONTAL BRANCH CONDUCTANCES FROM TRANSMISSIVITY	SUB0411
	CALL SBCFLC(CR,CC,TRPY,DELR,DELC,K,NCOL,NROW,NLAY)	SUB0412
C		SUB0413
C8-----	RETURN	SUB0414
	RETURN	SUB0415
	END	SUB0416
	SUBROUTINE RIVLFM(NRIVER,MXRIVR,RIVR,HNEW,HCOF,RHS,IBOUND,	SUB0417
1	NCOL,NROW,NLAY,	SUB0418
2	SHNW,IU,IP,ISN)	SUB0419
C		SUB0420
C-----	VERSION 0915 27AUG1982 RIVLFM	SUB0421
C-----	VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0422
C		SUB0423
C	*****	SUB0424
C	ADD RIVER TERMS TO RHS AND HCOF	SUB0425
C	*****	SUB0426
C		SUB0427
C	SPECIFICATIONS:	SUB0428
C	-----	SUB0429
C		SUB0430
	DOUBLE PRECISION HNEW	SUB0431
	DIMENSION RIVR(6,MXRIVR),HNEW(NCOL,NROW,NLAY),	SUB0432
1	HCOF(NCOL,NROW,NLAY),RHS(NCOL,NROW,NLAY),	SUB0433
2	IBOUND(NCOL,NROW,NLAY)	SUB0434
3	,SHNW(NCOL,NROW,NLAY)	SUB0435
C	-----	SUB0436
C		SUB0437
C		SUB0438
C1-----	IF NRIVER<=0 THERE ARE NO RIVERS. RETURN.	SUB0439
	IF(NRIVER.LE.0)RETURN	SUB0440
C		SUB0441
C2-----	PROCESS EACH CELL IN THE RIVER LIST.	SUB0442
	DO 100 L=1,NRIVER	SUB0443
C		SUB0444
C3-----	GET COLUMN, ROW, AND LAYER OF CELL CONTAINING REACH	SUB0445
	IL=RIVR(1,L)	SUB0446
	IR=RIVR(2,L)	SUB0447
	IC=RIVR(3,L)	SUB0448
C		SUB0449
C4-----	IF THE CELL IS EXTERNAL SKIP IT.	SUB0450
	IF(IBOUND(IC,IR,IL).LE.0)GO TO 100	SUB0451
C		SUB0452
C5-----	SINCE THE CELL IS INTERNAL GET THE RIVER DATA.	SUB0453
	HRIV=RIVR(4,L)	SUB0454
	CRIV=RIVR(5,L)	SUB0455
	RBOT=RIVR(6,L)	SUB0456
	HHNEW=HNEW(IC,IR,IL)	SUB0457
C-----	ADDED FOR ADJOINT AND SENSITIVITY CALCULATIONS	SUB0458
	IF(IU.NE.0.AND.IP.GT.0) HHNEW=DBLE(SHNW(IC,IR,IL))	SUB0459
C		SUB0460
C6-----	COMPARE AQUIFER HEAD TO BOTTOM OF STREAM BED.	SUB0461
	IF(HHNEW.LE.RBOT)GO TO 96	SUB0462
C		SUB0463
C7-----	SINCE HEAD>BOTTOM ADD TERMS TO RHS AND HCOF.	SUB0464
C-----	FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO HCOF.	SUB0465
	IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0466
1	RHS(IC,IR,IL)=RHS(IC,IR,IL)-CRIV*HRIV	SUB0467
	HCOF(IC,IR,IL)=HCOF(IC,IR,IL)-CRIV	SUB0468
	GO TO 100	SUB0469
C		SUB0470
C8-----	SINCE HEAD<BOTTOM ADD TERM ONLY TO RHS.	SUB0471
96	IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0472
1	RHS(IC,IR,IL)=RHS(IC,IR,IL)-CRIV*(HRIV-RBOT)	SUB0473
100	CONTINUE	SUB0474
C		SUB0475
C9-----	RETURN	SUB0476
	RETURN	SUB0477
	END	SUB0478

SUBROUTINE DRN1FM(NDRAIN,MXDRN,DRAI,HNEW,HCOF,RHS,IBOUND,	SUB0479
1 NCOL,NROW,NLAY,	SUB0480
2 SHNW,IU,IP,ISN)	SUB0481
C	SUB0482
C-----VERSION 1030 10APR1985 DRN1FM	SUB0483
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0484
C	SUB0485
C	SUB0486
C *****	SUB0487
C ADD DRAIN FLOW TO SOURCE TERM	SUB0488
C *****	SUB0489
C	SUB0490
C SPECIFICATIONS:	SUB0491
C -----	SUB0492
C DOUBLE PRECISION HNEW	SUB0493
C	SUB0494
C DIMENSION DRAI(5,MXDRN),HNEW(NCOL,NROW,NLAY),	SUB0495
1 RHS(NCOL,NROW,NLAY),IBOUND(NCOL,NROW,NLAY),	SUB0496
1 HCOF(NCOL,NROW,NLAY),	SUB0497
1 SHNW(NCOL,NROW,NLAY)	SUB0498
C -----	SUB0499
C	SUB0500
C1-----IF NDRAIN<=0 THERE ARE NO DRAINS. RETURN	SUB0501
IF(NDRAIN.LE.0) RETURN	SUB0502
C	SUB0503
C2-----PROCESS EACH CELL IN THE DRAIN LIST	SUB0504
DO 100 L=1,NDRAIN	SUB0505
C	SUB0506
C3-----GET COLUMN, ROW AND LAYER OF CELL CONTAINING DRAIN.	SUB0507
IL=DRAI(1,L)	SUB0508
IR=DRAI(2,L)	SUB0509
IC=DRAI(3,L)	SUB0510
C	SUB0511
C4-----IF THE CELL IS EXTERNAL SKIP IT.	SUB0512
IF(IBOUND(IC,IR,IL).LE.0) GO TO 100	SUB0513
C	SUB0514
C5-----IF THE CELL IS INTERNAL GET THE DRAIN DATA.	SUB0515
EL=DRAI(4,L)	SUB0516
HHNEW=HNEW(IC,IR,IL)	SUB0517
C-----ADDED FOR ADJOINT AND SENSITIVITY CALCULATIONS	SUB0518
IF(IU.NE.0.AND.IP.GT.0) HHNEW=SHNW(IC,IR,IL)	SUB0519
C	SUB0520
C6-----IF HEAD IS LOWER THAN DRAIN THEN SKIP THIS CELL.	SUB0521
IF(HHNEW.LE.EL) GO TO 100	SUB0522
C	SUB0523
C7-----HEAD IS HIGHER THAN DRAIN. ADD TERMS TO RHS AND HCOF.	SUB0524
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO HCOF.	SUB0525
C=DRAI(5,L)	SUB0526
HCOF(IC,IR,IL)=HCOF(IC,IR,IL)-C	SUB0527
IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0528
1 RHS(IC,IR,IL)=RHS(IC,IR,IL)-C*EL	SUB0529
100 CONTINUE	SUB0530
C	SUB0531
C8-----RETURN	SUB0532
RETURN	SUB0533
END	SUB0534
 SUBROUTINE EVT1FM(NEVTOP,IEVT,EVTR,EXDP,SURF,RHS,HCOF,	SUB0535
1 IBOUND,HNEW,NCOL,NROW,NLAY,	SUB0536
2 SHNW,IU,IP,ISN)	SUB0537
C	SUB0538
C-----VERSION 1031 10APR1985 EVT1FM	SUB0539
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0540
C	SUB0541
C *****	SUB0542
C ADD EVAPOTRANSPIRATION TO RHS AND HCOF	SUB0543
C *****	SUB0544
C	SUB0545
C SPECIFICATIONS:	SUB0546
C -----	SUB0547
C DOUBLE PRECISION HNEW	SUB0548
C DIMENSION IEVT(NCOL,NROW),EVTR(NCOL,NROW),EXDP(NCOL,NROW),	SUB0549
1 SURF(NCOL,NROW),RHS(NCOL,NROW,NLAY),	SUB0550
2 HCOF(NCOL,NROW,NLAY),IBOUND(NCOL,NROW,NLAY),	SUB0551
3 HNEW(NCOL,NROW,NLAY),	SUB0552
4 SHNW(NCOL,NROW,NLAY)	SUB0553
C -----	SUB0554
C	SUB0555
C1-----PROCESS EACH HORIZONTAL CELL LOCATION	SUB0556
DO 10 IR=1,NROW	SUB0557
DO 10 IC=1,NCOL	SUB0558
C	SUB0559



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C2-----SET THE LAYER INDEX EQUAL TO 1
      IL=1
C
C3-----IF OPTION 2 IS SPECIFIED THEN GET LAYER INDEX FROM IEVT ARRAY
      IF(NEVTOP.EQ.2) IL=IEVT(IC,IR)
C
C4-----IF THE CELL IS EXTERNAL IGNORE IT.
      IF(IBOUND(IC,IR,IL).LE.0)GO TO 10
      C=EVTR(IC,IR)
      S=SURF(IC,IR)
      H=HNEW(IC,IR,IL)
C-----ADDED FOR ADJOINT AND SENSITIVITY CALCULATIONS
      IF(IU.NE.0.AND.IP.GT.0) H=SHNW(IC,IR,IL)
C
C5-----IF AQUIFER HEAD IS GREATER THAN OR EQUAL TO SURF, ET IS CONSTANT
      IF(H.LT.S) GO TO 5
C
C5A-----SUBTRACT -EVTR FROM RHS
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO HCOF
      IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)
        1 RHS(IC,IR,IL)=RHS(IC,IR,IL) + C
        GO TO 10
C
C6-----IF DEPTH TO WATER>=EXTINCTION DEPTH THEN ET IS 0
      5 D=S-H
      X=EXDP(IC,IR)
      IF(D.GE.X)GO TO 10
C
C7-----LINEAR RANGE. ADD ET TERMS TO BOTH RHS AND HCOF.
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO HCOF
      IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)
        1 RHS(IC,IR,IL)=RHS(IC,IR,IL)+C-C*S/X
        HCOF(IC,IR,IL)=HCOF(IC,IR,IL)-C/X
        10 CONTINUE
C
C8-----RETURN
      RETURN
      END

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SUB0560  
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 SUB0597

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      SUBROUTINE STR1FM(NSTREM,STRM,ISTRM,HNEW,HCOF,RHS,IBOUND,MXSTRM,
1          NCOL,NROW,NLAY,IOUT,NSS,ITRBAR,NTRIB,ARTRIB,
2          IDIVAR,ICALC,CONST,
3          SHNW,IU,IP,ISN)
C
C-----VERSION 1 23OCT1987 STR1FM
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992
C
C *****
C ADD STREAM TERMS TO RHS AND HCOF IF FLOW OCCURS IN MODEL CELL
C *****
C SPECIFICATIONS:
C -----
C DOUBLE PRECISION HNEW
C DIMENSION STRM(11,MXSTRM),ISTRM(5,MXSTRM),HNEW(NCOL,NROW,NLAY),
1          HCOF(NCOL,NROW,NLAY),RHS(NCOL,NROW,NLAY),
2          IBOUND(NCOL,NROW,NLAY),ITRBAR(NSS,NTRIB),ARTRIB(NSS),
3          IDIVAR(NSS),SHNW(NCOL,NROW,NLAY)
C -----
C1-----IF NSTREM<=0 THERE ARE NO STREAMS. RETURN.
      IF(NSTREM.LE.0)RETURN
C
C2-----PROCESS EACH CELL IN THE STREAM LIST.
C
C3-----DETERMINE LAYER, ROW, COLUMN OF EACH REACH.
      DO 500 L=1,NSTREM
        LL=L-1
        IL=ISTRM(1,L)
        IR=ISTRM(2,L)
        IC=ISTRM(3,L)
C
C4-----DETERMINE IF CELL IS OUTSIDE OF MODEL BOUNDARIES.
      IF(IBOUND(IC,IR,IL).LE.0)GO TO 500
C
C5-----DETERMINE STREAM SEGMENT AND REACH NUMBER.
      ISTSG=ISTRM(4,L)
      NREACH=ISTRM(5,L)
C
C6-----SET FLOWIN EQUAL TO STREAM SEGMENT INFLOW IF FIRST REACH.
      IF(NREACH.GT.1) GO TO 200

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 CSUB0639  
 SUB0640

FLOWIN=STRM(1,L)	SUB0641
C	CSUB0642
C7-----STORE OUTFLOW FROM PREVIOUS SEGMENT IN ARTRIB IF SEGMENT >1.	CSUB0643
IF(ISTSG.GT.1) IFLG = ISTRM(4,LL)	SUB0644
IF(ISTSG.GT.1) ARTRIB(IFLG)=STRM(9,LL)	SUB0645
C	CSUB0646
C8-----IF SEGMENT IS A DIVERSION, COMPUTE FLOW OUT OF UPSTREAM REACH.	CSUB0647
IF(IDIVAR(ISTSG).LE.0) GO TO 50	SUB0648
NDFLG=IDIVAR(ISTSG)	SUB0649
DUM=ARTRIB(NDFLG)-FLOWIN	SUB0650
IF(DUM.GE.0.0) ARTRIB(NDFLG)=DUM	SUB0651
IF(DUM.GE.0.0) GO TO 50	SUB0652
FLOWIN=0.	SUB0653
50 IF(FLOWIN.GE.0.0) GO TO 300	SUB0654
C	CSUB0655
C9-----SUM TRIBUTARY OUTFLOW AND USE AS INFLOW INTO DOWNSTREAM SEGMENT.	CSUB0656
FLOWIN =0.	SUB0657
DO 100 ITRIB=1,NTRIB	SUB0658
INODE=ITRIBAR(ISTSG,ITRIB)	SUB0659
IF(INODE.LE.0) GO TO 100	SUB0660
FLOWIN=FLOWIN+ARTRIB(INODE)	SUB0661
100 CONTINUE	SUB0662
C	CSUB0663
C10-----IF REACH >1, SET INFLOW EQUAL TO OUTFLOW FROM UPSTREAM REACH.	CSUB0664
200 IF(NREACH.GT.1) FLOWIN=STRM(9,LL)	SUB0665
C	CSUB0666
C11-----COMPUTE STREAM STAGE IN REACH IF ICALC IS GREATER THAN 1.	CSUB0667
300 IF(ICALC.LE.0) GO TO 310	SUB0668
XNUM=((FLOWIN+STRM(9,L))/2.0)*STRM(8,L)	SUB0669
DNOM=CONST*STRM(6,L)*(SQRT(STRM(7,L)))	SUB0670
DEPTH=(XNUM/DNOM)**0.6	SUB0671
IF(DEPTH.LE.0.) DEPTH=0.	SUB0672
STRM(2,L)=DEPTH+STRM(5,L)	SUB0673
310 HSTR=STRM(2,L)	SUB0674
C	CSUB0675
C12-----DETERMINE LEAKAGE THROUGH STREAMBED.	CSUB0676
IF(FLOWIN.LE.0.) HSTR=STRM(5,L)	SUB0677
CSTR=STRM(3,L)	SUB0678
SBOT=STRM(4,L)	SUB0679
H=HNEW(IC,IR,IL)	SUB0680
C-----ADDED FOR PARAMETER ESTIMATION	SUB0681
IF(IU.GT.0.AND.IP.NE.0) H=SHNW(IC,IR,IL)	SUB0682
T=HSTR-SBOT	SUB0683
C	CSUB0684
C13-----COMPUTE LEAKAGE AS A FUNCTION OF STREAM STAGE AND HEAD IN CELL.	CSUB0685
FLOBOT=CSTR*(HSTR-H)	SUB0686
C	CSUB0687
C14-----RECOMPUTE LEAKAGE IF HEAD IN CELL IS BELOW STREAMBED BOTTOM.	CSUB0688
IQFLG=0	SUB0689
IF(H.GT.SBOT) GO TO 312	SUB0690
IQFLG=1	SUB0691
FLOBOT=CSTR*T	SUB0692
C	CSUB0693
C15-----SET LEAKAGE EQUAL TO STREAM INFLOW IF LEAKAGE MORE THAN INFLOW.	CSUB0694
312 IF(FLOBOT.LE.FLOWIN) GO TO 320	SUB0695
IQFLG=1	SUB0696
FLOBOT=FLOWIN	SUB0697
C	CSUB0698
C16-----STREAMFLOW OUT EQUALS STREAMFLOW IN MINUS LEAKAGE.	CSUB0699
320 FLOWOT=FLOWIN-FLOBOT	SUB0700
IF((ISTSG.GT.1).AND.(NREACH.EQ.1)) STRM(9,LL)=ARTRIB(IFLG)	SUB0701
C	CSUB0702
C17-----STORE STREAM INFLOW, OUTFLOW AND LEAKAGE FOR EACH REACH.	CSUB0703
STRM(9,L)=FLOWOT	SUB0704
STRM(10,L)=FLOWIN	SUB0705
STRM(11,L)=FLOBOT	SUB0706
C	CSUB0707
C18-----RETURN TO STEP 3 IF STREAM INFLOW IS LESS THAN OR EQUAL TO ZERO	CSUB0708
AND LEAKAGE IS GREATER THAN OR EQUAL TO ZERO.	CSUB0709
IF((FLOWIN.LE.0.0).AND.(FLOBOT.GE.0.0)) GO TO 500	SUB0710
C	CSUB0711
C19-----IF HEAD > BOTTOM THEN ADD TERMS TO RHS AND HCOF.	CSUB0712
IF(IQFLG.GT.0) GO TO 400	SUB0713
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO HCOF	SUB0714
IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0715
1RHS(IC,IR,IL)=RHS(IC,IR,IL)-CSTR*HSTR	SUB0716
HCOF(IC,IR,IL)=HCOF(IC,IR,IL)-CSTR	SUB0717
GO TO 500	SUB0718
C	CSUB0719
C20-----IF HEAD < BOTTOM THEN ADD TERM ONLY TO RHS.	CSUB0720
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO RHS	SUB0721
400 IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0722
1RHS(IC,IR,IL)=RHS(IC,IR,IL)-FLOBOT	SUB0723

500 CONTINUE	SUB0724
C	CSUB0725
C22-----RETURN.	CSUB0726
RETURN	SUB0727
END	SUB0728
SUBROUTINE GHBI1FM(NBOUND,MXBND,BNDS,HCOF,RHS,IBOUND,	SUB0729
1                NCOL,NROW,NLAY,	SUB0730
2                IU,IP,ISN)	SUB0731
C	SUB0732
C-----VERSION 1037 10APR1985 GHBI1FM	SUB0733
C-----VERSION MODIFIED FOR MODFLOWP 1000 01FEB1992	SUB0734
C	SUB0735
C *****	SUB0736
C ADD GHBI TERMS TO RHS AND HCOF	SUB0737
C *****	SUB0738
C	SUB0739
C SPECIFICATIONS:	SUB0740
C -----	SUB0741
DIMENSION BNDS(5,MXBND),HCOF(NCOL,NROW,NLAY),	SUB0742
1                RHS(NCOL,NROW,NLAY),IBOUND(NCOL,NROW,NLAY)	SUB0743
C -----	SUB0744
C	SUB0745
C1-----IF NBOUND<=0 THEN THERE ARE NO GENERAL HEAD BOUNDS. RETURN.	SUB0746
IF(NBOUND.LE.0) RETURN	SUB0747
C	SUB0748
C2-----PROCESS EACH ENTRY IN THE GENERAL HEAD BOUND LIST (BNDS)	SUB0749
DO 100 L=1,NBOUND	SUB0750
C	SUB0751
C3-----GET COLUMN, ROW AND LAYER OF CELL CONTAINING BOUNDARY	SUB0752
IL=BNDS(1,L)	SUB0753
IR=BNDS(2,L)	SUB0754
IC=BNDS(3,L)	SUB0755
C	SUB0756
C4-----IF THE CELL IS EXTERNAL THEN SKIP IT.	SUB0757
IF(IBOUND(IC,IR,IL).LE.0) GO TO 100	SUB0758
C	SUB0759
C5-----SINCE THE CELL IS INTERNAL GET THE BOUNDARY DATA.	SUB0760
HB=BNDS(4,L)	SUB0761
C=BNDS(5,L)	SUB0762
C	SUB0763
C6-----ADD TERMS TO RHS AND HCOF	SUB0764
HCOF(IC,IR,IL)=HCOF(IC,IR,IL)-C	SUB0765
C-----FOR ADJOINT STATES, ONLY CALCULATE CONTRIBUTION TO RHS	SUB0766
IF(IU.EQ.0.OR.IP.EQ.0.OR.ISN.LT.0)	SUB0767
1 RHS(IC,IR,IL)=RHS(IC,IR,IL)-C*HB	SUB0768
100 CONTINUE	SUB0769
C	SUB0770
C7-----RETURN	SUB0771
RETURN	SUB0772
END	SUB0773

#### New SEN Primary Modules

Listed in order of first appearance in MAIN

C=====	SEN0001
SUBROUTINE SENIAL (ISUM,LENX,NCOL,NROW,NLAY,NPER,IOUT,LCSHNV,	SEN0002
1                LCNLL,LCSMAT,LCCELS,IUHEAD,NP,NSM,NSN,ISN,LCTS,LCATS,	SEN0003
2                LCST,NH,LCNDR,LCSHOL,LCSTP,NRWD,LCIRWD,IU,LCBSTP,IPAR,	SEN0004
3                LCB,LCH,LCX,LCRINT,LCJOFF,LCIOFF,LCCONV,LCCOFF,LCROFF,	SEN0005
4                LCMLAY,LCPR,MOBS,LCLN,NQ,NQC,NQT,LCIBT,LCNQOB,LCNQCL,	SEN0006
5                LCIQOB,LCQCLS,IUBD,ISCALS,LCTOFF,MPR,LCXX,MAXM,LCLZ,	SEN0007
6                NLLI1,NLLIT,NMM,NZM,LZII,LCSEFAC,LCLM,LCMATZ,LCHOBS,	SEN0008
7                LCWT,IUB,LCSV,IPRNP,IUNHEA,NUMR,ICHECK,NPNG,LCIPNG,	SEN0009
8                NZER,LCIZER,LCIWPNG,NOPT,LCKD)	SEN0010
C-----VERSION 1000 01FEB1992 SENIAL	SEN0011
C *****	SEN0012
C ALLOCATE ARRAY STORAGE FOR SENSITIVITIES	SEN0013
C *****	SEN0014
C SPECIFICATIONS:	SEN0015
C -----	SEN0016
CHARACTER*4 HEADNG(20)	SEN0017
COMMON /FLWCOM/LAYCON(80)	SEN0018
C -----	SEN0019
C	SEN0020
C1-----IDENTIFY PACKAGE AND PRINT HEADING	SEN0021
WRITE(IOUT,1) IU	SEN0022
1 FORMAT(1H0,'SEN1 -- SENSITIVITY PACKAGE, ,	SEN0023
1 'VERSION 1, 12/01/91 INPUT READ FROM UNIT',I3)	SEN0024
READ(IU,2) HEADNG	SEN0025

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2 FORMAT(20A4) SEN0026
WRITE(IOUT,3) HEADNG SEN0027
3 FORMAT(1H0,20A4) SEN0028
READ(IU,2) HEADNG SEN0029
WRITE(IOUT,3) HEADNG SEN0030
C SEN0031
C-----READ & PRINT LINES 3 THROUGH 8 OF THE INPUT FILE SEN0032
READ(IU,10) NP,NSM,NSN,NLL11,LZ11,NMM,NZM SEN0033
READ(IU,10) IPRNP,ICHECK,NUMR SEN0034
READ(IU,10) NH,MOBS,MAXM,NQ,NQT,MPR SEN0035
READ(IU,10) IPAR,ISN,ISCALS,NOPT SEN0036
READ(IU,10) IUHEAD,IOUB,IUBD,IUNHEA SEN0037
READ(IU,10) NRWD,NZER,NPNG SEN0038
10 FORMAT(15I5) SEN0039
WRITE(IOUT,20) NP,NSM,NSN,NLL11,LZ11,NMM,NZM SEN0040
20 FORMAT( SEN0041
1 ' NUMBER OF PARAMETERS.....',I5,, SEN0042
2 ' NUMBER NLL>0 IN ALL DATA SETS 2 FOR PID=T,KV,',/, SEN0043
3 ' TKV, AND S1, +1 FOR NLL(1)>0 FOR PID=RCH OR ETM....',I5,, SEN0044
4 ' SUM ALL |NLL(1)| FOR PID=Q,KRB,KDR,KST,GHB,AND CH...',I5,, SEN0045
5 ' LARGEST NLL VECTOR IN ALL DATA SETS 2.....',I5,, SEN0046
6 ' LARGEST LZ VECTOR IN ALL DATA SETS 2B.....',I5,, SEN0047
7 ' NUMBER OF MULTIPLICATION MATRICES IN DATA SET 3.....',I5,, SEN0048
8 ' NUMBER OF ZONE MATRICES IN DATA SET 4.....',I5,, SEN0049
WRITE(IOUT,30) IPRNP,ICHECK,NUMR SEN0050
30 FORMAT( SEN0051
3 ' PRINT MATRICES PRODUCED BY INIT. PARAM. EST. (>0)...',I5,, SEN0052
4 ' CHECK CELL REPETITIONS FOR MATRIX PARAMETERS (>0)...',I5,, SEN0053
5 ' NUMBER OF CELL REPETITIONS ALLOWED.....',I5,, SEN0054
WRITE(IOUT,40) NH,MOBS,MAXM,NQ,NQT,MPR SEN0055
40 FORMAT( SEN0056
1 ' NUMBER OF HEADS.....',I5,, SEN0057
2 ' NUMBER OF MULTILAYER HEADS.....',I5,, SEN0058
3 ' MAXIMUM NUMBER OF LAYERS FOR MULTILAYER HEADS.....',I5,, SEN0059
4 ' NUMBER OF FLUX CELL GROUPS.....',I5,, SEN0060
5 ' NUMBER OF CELLS IN FLUX CELL GROUPS.....',I5,, SEN0061
6 ' NUMBER OF FLUXES.....',I5,, SEN0062
7 ' NUMBER OF PRIORS WITH MULTIPLE PARAMETERS.....',I5,, SEN0063
WRITE(IOUT,50) IPAR,ISN,ISCALS,NOPT SEN0064
50 FORMAT( SEN0065
1 ' HEADS (<0), HEADS AND SENS. (0), OR PAR. EST. (1)...',I5,, SEN0066
2 ' ADJOINT (+) OR SEN. EQ. (-) CALCULATIONS.....',I5,, SEN0067
3 ' (GRADIENT SEARCH (+) OR GAUSS-NEWTON (-) REGRESSION)',/, SEN0068
4 ' SCALE PRINTED SENSITIVITIES (>0).....',I5,, SEN0069
5 ' ADJUST GAUSS-NEWTON MATRIX WITH NEWTON UPDATES.....',I5,, SEN0070
WRITE(IOUT,60) IUHEAD,IOUB,IUBD,IUNHEA SEN0071
60 FORMAT( SEN0072
1 ' OUTPUT/INPUT UNIT FOR HEADS OR SENSITIVITIES.....',I5,, SEN0073
2 ' OUTPUT/INPUT UNIT NUMBER FOR INFO FROM ITERATIONS...',I5,, SEN0074
3 ' INPUT UNIT FOR SS/TR IBOUND ARRAYS.....',I5,, SEN0075
4 ' INPUT UNIT FOR KNOWN HEADS AT CONSTANT-HEAD BNDRYS..',I5,, SEN0076
WRITE(IOUT,70) NRWD,NZER,NPNG SEN0077
70 FORMAT( SEN0078
1 ' NUMBER OF INPUT UNITS IDENTIFIED IN RCH AND EVT.....',I5,, SEN0079
2 ' NUMBER OF TIME STEPS>0 AT WHICH HEAD=0.....',I5,, SEN0080
3 ' NUMBER OF USUALLY POS. PARAMETERS THAT MAY BE NEG...',I5,, SEN0081
NLL11=(NLL11-1)/2 SEN0082
LZ11=LZ11+1 SEN0083
IF(IPAR.LT.1) MPR=0 SEN0084
IF(MAXM.EQ.1) THEN SEN0085
WRITE(IOUT,80) SEN0086
STOP SEN0087
ENDIF SEN0088
80 FORMAT(/,' MAXM CAN NOT EQUAL 1 -- STOP EXECUTION') SEN0089
C-----STORE, IN ISOLD, LOCATION OF FIRST UNALLOCATED SPACE IN X. SEN0090
ISOLD=ISUM SEN0091
C SEN0092
C2-----ALLOCATE SPACE FOR ARRAYS SEN0093
C-----TIME STEP ARRAYS SEN0094
NODES=NROW*NCOL*NLAY SEN0095
LCTS=ISUM SEN0096
IF(NPER.NE.0) ISUM=ISUM+NPER SEN0097
IF(NPER.EQ.0) ISUM=ISUM+1 SEN0098
LCATS=ISUM SEN0099
IF(ISN.GT.0) ISUM=ISUM+(2*(NPER+1)) SEN0100
LCSTP=ISUM SEN0101
ISUM=ISUM+NPER+1 SEN0102
LCBSTP=ISUM SEN0103
IF(ISN.GT.0) ISUM=ISUM+NPER+1 SEN0104
C-----FULL GRID ARRAYS SEN0105
LCSHNW=ISUM SEN0106
ISUM=ISUM+NODES SEN0107
LCST=ISUM SEN0108

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ISUM=ISUM+NODES	SEN0109
LCSV=ISUM	SEN0110
IF(LAYCON(1).EQ.1.AND.NLAY.GT.1.AND.IPAR.GT.0) ISUM=ISUM+NROW*NCOL	SEN0111
LCSHOL=ISUM	SEN0112
IF((ISN.LT.0.OR.ISN.EQ.10).AND.NPER.NE.0) ISUM=ISUM+NODES	SEN0113
C-----ARRAYS FOR PARAMETER DEFINITION	SEN0114
LCLN=ISUM	SEN0115
ISUM=ISUM+NP	SEN0116
LCNLL=ISUM	SEN0117
ISUM=ISUM+NP*NLLI1	SEN0118
LCSFAC=ISUM	SEN0119
ISUM=ISUM+NSM	SEN0120
LCLM=ISUM	SEN0121
ISUM=ISUM+NSM	SEN0122
LCLZ=ISUM	SEN0123
ISUM=ISUM+NSM*LZ11	SEN0124
LCSMAT=ISUM	SEN0125
ISUM=ISUM+NMM*NROW*NCOL	SEN0126
LCMATZ=ISUM	SEN0127
ISUM=ISUM+NZM*NROW*NCOL	SEN0128
LCCELS=ISUM	SEN0129
ISUM=ISUM+(NSN*4)	SEN0130
LCB=ISUM	SEN0131
ISUM=ISUM+NP	SEN0132
LCIWP=ISUM	SEN0133
ISUM=ISUM+NP	SEN0134
C-----HEAD DATA ARRAYS	SEN0135
LCNDR=ISUM	SEN0136
ISUM=ISUM+5*NH	SEN0137
LCCOFF=ISUM	SEN0138
ISUM=ISUM+NH	SEN0139
LCROFF=ISUM	SEN0140
ISUM=ISUM+NH	SEN0141
LCIOFF=ISUM	SEN0142
ISUM=ISUM+NH	SEN0143
LCJOFF=ISUM	SEN0144
ISUM=ISUM+NH	SEN0145
LCRINT=ISUM	SEN0146
ISUM=ISUM+4*NH	SEN0147
LCMLAY=ISUM	SEN0148
ISUM=ISUM+MAXM*MOBS	SEN0149
LCPR=ISUM	SEN0150
ISUM=ISUM+MAXM*MOBS	SEN0151
C-----FLOW DATA ARRAYS	SEN0152
LCIBT=ISUM	SEN0153
ISUM=ISUM+NQ*2	SEN0154
LCNQOB=ISUM	SEN0155
ISUM=ISUM+NQ	SEN0156
LCNQCL=ISUM	SEN0157
ISUM=ISUM+NQ	SEN0158
LCIQOB=ISUM	SEN0159
ISUM=ISUM+NQT	SEN0160
LCQCLS=ISUM	SEN0161
ISUM=ISUM+5*NQ	SEN0162
C-----ARRAYS USED FOR ALL DEPENDENT-VARIABLE DATA	SEN0163
LCTOFF=ISUM	SEN0164
ISUM=ISUM+NH+NQT	SEN0165
LCH=ISUM	SEN0166
ISUM=ISUM+NH+NQT	SEN0167
LCHOBS=ISUM	SEN0168
ISUM=ISUM+NH+NQT	SEN0169
LCWT=ISUM	SEN0170
ISUM=ISUM+NH+NQT	SEN0171
IF(MOD(ISUM,2).EQ.0) ISUM=ISUM+1	SEN0172
LCX=ISUM	SEN0173
ISUM=ISUM+NP*(NH+NQT)	SEN0174
LCXD=ISUM	SEN0175
IF(IPAR.GT.0.AND.NOPT.EQ.1) ISUM=ISUM+NP*(NH+NQT)	SEN0176
LCXX=ISUM	SEN0177
IF(ISN.GT.0) ISUM=ISUM+2*NP	SEN0178
C-----MISCELLANEOUS ARRAYS	SEN0179
LCIRWD=ISUM	SEN0180
ISUM=ISUM+NRWD	SEN0181
LCIPNG=ISUM	SEN0182
ISUM=ISUM+NPNG	SEN0183
LCIZER=ISUM	SEN0184
ISUM=ISUM+NZER	SEN0185
LCCONV=ISUM	SEN0186
IF(ISN.LT.0.OR.ISN.GE.4) ISUM=ISUM+2*NP+2	SEN0187
C	SEN0188
C8-----PRINT AMOUNT OF SPACE USED BY SENSITIVITY PACKAGE.	SEN0189
ISP=ISUM-ISOLD	SEN0190
WRITE (IOUT,4)ISP	SEN0191

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4 FORMAT(1X,I6,' ELEMENTS IN X ARRAY ARE USED FOR SENSITIVITIES') SEN0192
  ISUM1=ISUM-1 SEN0193
  WRITE(IOUT,5)ISUM1,LENX SEN0194
5 FORMAT(1X,I6,' ELEMENTS OF X ARRAY USED OUT OF',I7) SEN0195
  IF(ISUM1.GT.LENX) WRITE(IOUT,6) SEN0196
6 FORMAT(1X,' ***X ARRAY MUST BE DIMENSIONED LARGER***') SEN0197
C SEN0198
C9-----RETURN SEN0199
  RETURN SEN0200
  END SEN0201

C=====SEN0202
  SUBROUTINE SENLRP ( SEN0203
1 NCOL,NROW,NLAY,NSN,NSM,MXBND,MXWELL,MXRIVR,NPER,IU,IOUT,NP, SEN0204
2 PID,DID,NLL,CELS,SMAT,NH,NDER,JT,NRWD,IRWD,IBOUND,ISN,JOFF, SEN0205
3 IOFF,HOBBS,WT,B,B1,IPAR,CONV,HCLOSE,RCLOSE,TOP,BOT,DELR,DELC, SEN0206
4 RINT,COFF,ROFF,MLAY,PR,MOBS,LN,NQ,NQC,NQT,IBT,NQOB,NQCL, SEN0207
5 IQOB,QCLS,IUBD,BUFF,TOFF,MXDRN,MXSTRM,MAXM,NMM,NZM,LZ11, SEN0208
6 SFAC,LZ,LM,MATZ,NLL11,IUNIT,NLL1T,EV,NUMR,ICHECK,NPNG,IPNG, SEN0209
7 NZER,IZER,IWPG,NPO) SEN0210
C-----VERSION 1000 01FEB1992 SEN0211
C *****SEN0212
C READ, CHECK AND STORE DATA FOR SENSITIVITY CALCULATIONS AND SEN0213
C PARAMETER ESTIMATION, AND INITIALIZE SOME VARIABLES. SEN0214
C *****SEN0215
C SPECIFICATIONS: SEN0216
C -----SEN0217
  CHARACTER*4 PID(NPO),DID(NH+NQT),PIDTMP SEN0218
  INTEGER NLL(NLL11,NPO),IUNIT(24) SEN0219
  DIMENSION NDER(5,NH),CELS(4,NSN),SMAT(NCOL,NROW,NMM),IWPG(NPO), SEN0220
1 IRWD(NRWD),IBOUND(NCOL,NROW,NLAY),IOFF(NH),JOFF(NH), SEN0221
2 WT(NH+NQT),B(NPO),B1(NPO),CONV(2*NPO+2),TOP(NCOL,NROW,NLAY), SEN0222
3 BOT(NCOL,NROW,NLAY),DELR(NCOL),DELC(NROW),RINT(4,NH), SEN0223
4 COFF(NH),ROFF(NH),MLAY(MAXM,MOBS),PR(MAXM,MOBS),LN(NPO), SEN0224
5 NQOB(NQ),NQCL(NQ),IQOB(NQT),QCLS(4,NQC),HOBBS(NH+NQT), SEN0225
6 BUFF(NCOL,NROW,NLAY),TOFF(NH,NQT),IBT(2,NQ),LZ(LZ11,NSM), SEN0226
7 LM(NSM),SFAC(NSM),MATZ(NCOL,NROW,NZM),IPNG(NPNG),IZER(NZER) SEN0227
  COMMON /FLWCOM/LAYCON(80) SEN0228
C -----SEN0229
503 FORMAT(8F10.0) SEN0230
504 FORMAT(2F10.0,2I5,F10.0) SEN0231
505 FORMAT(16I5) SEN0232
510 FORMAT(8I10) SEN0233
530 FORMAT(//,' DEFINITION OF TEMPORAL AND SPATIAL EXTENT OF ', SEN0234
3 'PARAMETERS (PARAMETERIZATION)') SEN0235
531 FORMAT(//,' INPUT UNIT NUMBERS LISTED IN RCH AND EVT PACKAGE ' SEN0236
2 ',INPUT FILES :',9I5) SEN0237
535 FORMAT(//,' PARAMETER NUMBERS OF AQUIFER PROPERTIES DEFINED ', SEN0238
1 'WITH KRIGING OPTION 2 :',9I5) SEN0239
540 FORMAT(//,' TIME STEPS AT WHICH HEADS ARE SET TO ZERO :',9I5) SEN0240
550 FORMAT(//,' IPNG('',I3,'')='',I3,''; PID('',I3,'')='',A4,/, SEN0241
1 ' INCLUSION OF THIS PARAMETER IN IPNG IS WRONG OR UNNECESSARY', SEN0242
2 ' -- STOP EXECUTION (SENLRP)') SEN0243
575 FORMAT(//,' INPUT ERROR VARIANCES FOR HEADS AND FLOWS: ',2G15.4, SEN0244
1/,', INPUT UNIT NUMBERS FOR HEADS AND FLOWS :',2I5, SEN0245
2/,', ESTIMATED COMMON ERROR VARIANCE :',G15.4) SEN0246
580 FORMAT(//,' PARAMETER INFORMATION',/, SEN0247
1 ' (CONVERGENCE CRITERIA LISTED HERE ARE USED TO SOLVE FOR ', SEN0248
1 'SENSITIVITY-EQUATION SENSITIVITIES)',/,', # ID ', SEN0249
1 'INITIAL VALUE LN CONVERGENCE CRITERIA GROUP #') SEN0250
582 FORMAT(//,' PARAMETER INFORMATION',/,', # ID ', SEN0251
1 'INITIAL VALUE LN GROUP #') SEN0252
585 FORMAT(' ',I5,2X,A4,G14.4,I3,3X,2G13.3,I5) SEN0253
587 FORMAT(' ',I5,2X,A4,G14.4,I3,3X,I5) SEN0254
590 FORMAT(//,' LAYCON OF THE BLOCK-CENTERED FLOW PACKAGE MAY', SEN0255
1 ' ONLY EQUAL 0 OR 1 -- STOP EXECUTION (SENLRP)') SEN0256
595 FORMAT(//,' CONJUGATE-DIRECTION OPTIMIZATION NOT PROGRAMMED ', SEN0257
1 'FOR FLOW DATA -- STOP EXECUTION (SENLRP)') SEN0258
600 FORMAT(//,' EXECUTION TERMINATED DUE TO ERRORS IN', SEN0259
1 ' PARAMETER-ESTIMATION PACKAGE INPUT FILE',/, SEN0260
1 ' -- SEARCH ABOVE FOR STOP EXECUTION TO FIND', SEN0261
1 ' ERROR MESSAGES (SENLRP)') SEN0262
610 FORMAT(//,' CONJUGATE-DIRECTION OPTIMIZATION NOT PROGRAMMED ', SEN0263
1 'FOR NZER>0 -- STOP EXECUTION (SENLRP)') SEN0264
C SEN0265
  DO 10 I=1,NP SEN0266
  PID(I)=' ' SEN0267
10 CONTINUE SEN0268
C-----BEGIN READING INPUT FILE SEN0269
  IF(NRWD.GT.0) THEN SEN0270
  READ(IU,505) (IRWD(I),I=1,NRWD) SEN0271
  WRITE(IOUT,531) (IRWD(I),I=1,NRWD) SEN0272

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ENDIF	SEN0273
IF(NZER.GT.0) THEN	SEN0274
READ(IU,505) (IZER(I),I=1,NZER)	SEN0275
WRITE(IOUT,540) (IZER(I),I=1,NZER)	SEN0276
ENDIF	SEN0277
IF(NPNG.GT.0) THEN	SEN0278
READ(IU,505) (IPNG(I),I=1,NPNG)	SEN0279
WRITE(IOUT,535) (IPNG(I),I=1,NPNG)	SEN0280
ENDIF	SEN0281
WRITE(IOUT,530)	SEN0282
C-----READ PARAMETER DEFINITIONS	SEN0283
CALL SSEN1G(NCOL,NROW,NLAY,NSN,NSM,MXBND,MXWELL,MXRIVR,NPER,IU,	SEN0284
1 IOUT,NP,PID,NLL,CELS,SMAT,IBOUND,TOP,BOT,LN,IERR,IUBD,BUFF,	SEN0285
2 DELR,DELC,MXDRN,MXSTRM,NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,	SEN0286
3 NLL11,IUNIT)	SEN0287
C-----CHECK NPNG PARAMETER NUMBERS	SEN0288
IF(NPNG.GT.0) THEN	SEN0289
DO 50 I=1,NPNG	SEN0290
PIDTMP=PID(IPNG(I))	SEN0291
IF(PIDTMP.EQ.'ANI '.OR.PIDTMP.EQ.'ANIV'.OR.PIDTMP.EQ.'Q '	SEN0292
1 .OR.PIDTMP.EQ.'CH '.OR.PIDTMP.EQ.'RCH ') THEN	SEN0293
IERR=1	SEN0294
WRITE(IOUT,550) I,IPNG(I),IPNG(I),PIDTMP	SEN0295
ENDIF	SEN0296
50 CONTINUE	SEN0297
ENDIF	SEN0298
C-----NZER>0 OKAY ONLY FOR ISN<0	SEN0299
IF(NZER.GT.0.AND.ISN.GT.0) THEN	SEN0300
WRITE(IOUT,610)	SEN0301
IERR=1	SEN0302
ENDIF	SEN0303
C-----READ MULTIPLICATIVE FACTOR FOR VARIANCES OF HEADS AND FLOWS	SEN0304
READ(IU,504) EVH,EVF,IUH,IUF,EV	SEN0305
WRITE(IOUT,575) EVH,EVF,IUH,IUF,EV	SEN0306
C	SEN0307
C-----READ HEAD TIMES, LOCATIONS, OBSERVED VALUES, AND STATS FOR WTS	SEN0308
C    CALL TIMER(6)	SEN0309
IF(IUH.EQ.0) IUH=IU	SEN0310
IF(NH.GT.0)	SEN0311
1 CALL SSEN1H(NCOL,NROW,NLAY,NPER,IUH,IOUT,DID,NH,NDER,JT,IBOUND,	SEN0312
1 JOFF,IOFF,HOBS,WT,DELR,DELC,RINT,COFF,ROFF,MLAY,PR,	SEN0313
2 MOBS,IERR,TOFF,EVH,ISN,MAXM)	SEN0314
C	SEN0315
C-----READ HEAD-DEPENDENT BOUNDARY FLOW DATA	SEN0316
C    CALL TIMER(7)	SEN0317
IF(IUF.EQ.0) IUF=IU	SEN0318
IF(NQ.GT.0)	SEN0319
1 CALL SSEN1F(NCOL,NROW,NLAY,MXBND,MXRIVR,NPER,IUF,IOUT,	SEN0320
2 DID,NH,JT,IBOUND,NQ,NQC,NQT,IBT,NQOB,NQCL,IQOB,QCLS,IERR,	SEN0321
3 PID,NP,NLL,CELS,NSN,WT,HOBS,TOFF,EVF,MXDRN,MXSTRM,ISN,	SEN0322
4 NLL11,NLLIT)	SEN0323
C    CALL TIMER(8)	SEN0324
C-----MAKE SURE THERE ARE NO CONVERTIBLE LAYERS	SEN0325
DO 90 K=1,NLAY	SEN0326
IF(LAYCON(K).GT.1) THEN	SEN0327
WRITE(IOUT,590)	SEN0328
IERR=1	SEN0329
ENDIF	SEN0330
90 CONTINUE	SEN0331
C-----CONJUGATE-DIRECTION METHODS NOT PROGRAMMED FOR FLUX DATA	SEN0332
IF(ISN.GT.0.AND.NQT.GT.0) THEN	SEN0333
WRITE(IOUT,595)	SEN0334
IERR=1	SEN0335
ENDIF	SEN0336
C-----CHECK FOR MULTIPLE USE OF CELLS IN DEFINING MATRIX MODEL INPUTS	SEN0337
IF(ICHECK.NE.0) CALL SSEN1A(PID,LM,LZ,NLL,SMAT,MATZ,BUFF,NCOL,	SEN0338
1 NROW,NLAY,NSM,NP,NMM,NZM,LZ11,NLL11,NLLIT,JT+1,IOUT,IERR,NUMR)	SEN0339
C-----STOP IF THERE ARE ERRORS IN THE DATA SET	SEN0340
IF(IERR.GT.0) THEN	SEN0341
WRITE(IOUT,600)	SEN0342
STOP	SEN0343
ENDIF	SEN0344
C-----CROP TIME STEPS IN NLL FOR PARAMETERS USED TO CALCULATE	SEN0345
C-----ADJOINT STATES.	SEN0346
IF(ISN.GT.0) THEN	SEN0347
DO 126 IP=1,NP	SEN0348
PIDTMP=PID(IP)	SEN0349
IF(PIDTMP.EQ.'KRB '.OR.PIDTMP.EQ.'GHB '.OR.	SEN0350
1 PIDTMP.EQ.'KDR '.OR.PIDTMP.EQ.'KST ') THEN	SEN0351
DO 128 NT=1,NLLIT	SEN0352
IF(NLL(2*NT,IP).LE.JT.AND.NLL(2*NT+1,IP).GT.JT)	SEN0353
1 NLL(2*NT+1,IP)=JT	SEN0354
128 CONTINUE	SEN0355

ENDIF	SEN0356
126 CONTINUE	SEN0357
ENDIF	SEN0358
C-----READ INITIAL PARAMETER VALUES.	SEN0359
READ(IU,503)(B(I),I=1,NP)	SEN0360
C-----PARAMETER GROUP NUMBERS	SEN0361
READ(IU,510)(IWP( IP),IP=1,NP)	SEN0362
C-----SAVE CONVERGENCE CRITERIA FOR HEAD.	SEN0363
CONV(1)=HCLOSE	SEN0364
CONV(NP+2)=RCLOSE	SEN0365
C-----CALCULATE CONVERGENCE CRITERIA FOR SENSITIVITY-EQ. SENSITIVITIES	SEN0366
IF (ISN.LT.0.OR.ISN.GE.4) THEN	SEN0367
DO 130 IP=1,NP	SEN0368
CONV(1+IP)=0.	SEN0369
CONV(NP+2+IP)=0.	SEN0370
IF (IWP( IP).GT.0) THEN	SEN0371
BB=ABS(B(IP))	SEN0372
IF (BB.LT.1.E-15) BB=1.0	SEN0373
CONV(1+IP)=HCLOSE/(BB*100.)	SEN0374
CONV(NP+2+IP)=RCLOSE/(BB*100.)	SEN0375
ENDIF	SEN0376
130 CONTINUE	SEN0377
ENDIF	SEN0378
C-----CONVERT HEAD AND FLOW OBSERVATION VARIANCES TO WEIGHTS.	SEN0379
ND=NH+NQT	SEN0380
DO 135 N=1,ND	SEN0381
135 WT(N)=EV/WT(N)	SEN0382
C-----IF THERE IS NO REGRESSION, PRINT PARAMETER INFORMATION	SEN0383
IF (IPAR.LE.0) THEN	SEN0384
IF (ISN.LT.0.OR.ISN.GE.4) WRITE(IOUT,580)	SEN0385
IF (ISN.GT.0.AND.ISN.LT.4) WRITE(IOUT,582)	SEN0386
DO 140 IP=1,NP	SEN0387
IF (ISN.LT.0.OR.ISN.GE.4) WRITE(IOUT,585) IP,PID(IP),B(IP),	SEN0388
1 LN(IP),CONV(1+IP),CONV(NP+2+IP),IWP( IP)	SEN0389
IF (ISN.GT.0.AND.ISN.LT.4) WRITE(IOUT,587) IP,PID(IP),B(IP),	SEN0390
1 LN(IP)	SEN0391
140 CONTINUE	SEN0392
ENDIF	SEN0393
C-----OMIT PARAMETERS WITH NEGATIVE GROUP NUMBERS	SEN0394
DO 150 IIP=1,NPO	SEN0395
IF (IWP(IIP).LT.0) THEN	SEN0396
NP=IIP-1	SEN0397
GO TO 155	SEN0398
ENDIF	SEN0399
150 CONTINUE	SEN0400
155 CONTINUE	SEN0401
C-----IF THERE IS REGRESSION, SAVE INITIAL PARAMETER VALUES AND	SEN0402
C-----CONVERT INDICATED PARAMETERS TO NATURAL LOGS	SEN0403
IF (IPAR.GT.0) THEN	SEN0404
DO 160 IP=1,NP	SEN0405
B1(IP)=B(IP)	SEN0406
160 IF (LN(IP).GT.0) B1(IP)=ALOG(B(IP))	SEN0407
ENDIF	SEN0408
RETURN	SEN0409
END	SEN0410
C=====SEN0411	
SUBROUTINE SEN1ST(JT,INBAS,PERLEN,NSTP,TS,ATS,STP,ISN,BSTP)	SEN0412
C-----VERSION 1000 01FEB1992	SEN0413
C *****	SEN0414
C PRODUCE TIME STEP FILES REQUIRED TO CALCULATE ADJOINT	SEN0415
C STATES AND SENSITIVITIES	SEN0416
C *****	SEN0417
C SPECIFICATIONS:	SEN0418
C -----	SEN0419
DIMENSION TS(JT),ATS((2*JT)+2),STP(JT+1),BSTP(JT+1)	SEN0420
C -----	SEN0421
C	SEN0422
1 FORMAT(F10.0,I10,F10.0)	SEN0423
DUM=1.E22	SEN0424
STP(1)=1.	SEN0425
C	SEN0426
C FOR JT=0 (SENSITIVITIES CALCULATED AT STEADY STATE ONLY)	SEN0427
C	SEN0428
IF (JT.EQ.0) THEN	SEN0429
READ(INBAS,1,END=100) PERLEN,NSTP,TSMULT	SEN0430
IF (TSMULT.NE.1.)	SEN0431
# TS(1)=PERLEN*(1.-TSMULT)/(1.-(TSMULT**NSTP))	SEN0432
IF (TSMULT.EQ.1.) TS(1)=TS(1)/NSTP	SEN0433
NSTP=1	SEN0434
PERLEN=0.0	SEN0435
IF (ISN.GT.0) THEN	SEN0436



ATS(1)=DUM	SEN0437
ATS(2)=TS(1)	SEN0438
ENDIF	SEN0439
RETURN	SEN0440
ENDIF	SEN0441
C	SEN0442
C	SEN0443
C	SEN0444
JJ=0	SEN0445
DO 80 K=1,1000	SEN0446
JJ=JJ+1	SEN0447
READ(INBAS,1,END=100) PERLEN,NSTP,TSMULT	SEN0448
STP(1+K)=STP(K)+NSTP	SEN0449
IF(PERLEN.EQ.0.0) GO TO 100	SEN0450
IF(TSMULT.NE.1.)	SEN0451
# TS(JJ)=PERLEN*(1.-TSMULT)/(1.-(TSMULT**NSTP))	SEN0452
IF(TSMULT.EQ.1.) TS(JJ)=PERLEN/NSTP	SEN0453
IF(JJ.EQ.JT) GO TO 110	SEN0454
DO 90 I=2,NSTP	SEN0455
JJ=JJ+1	SEN0456
TS(JJ)=TSMULT*TS(JJ-1)	SEN0457
IF(JJ.EQ.JT) GO TO 110	SEN0458
90 CONTINUE	SEN0459
80 CONTINUE	SEN0460
100 STOP 'TIME STEP EXCEEDS STRESS PERIOD DATA - FROM SEN1ST'	SEN0461
110 CONTINUE	SEN0462
C	SEN0463
NSTP=1	SEN0464
PERLEN=0.0	SEN0465
IF(ISN.GT.0) THEN	SEN0466
DO 121 I=1,JT	SEN0467
ATS((I*2)-1) = TS(JT-I+1)	SEN0468
121 ATS((I*2)+2)=TS(JT-I+1)	SEN0469
ATS(2)=DUM	SEN0470
ATS((JT*2)+1)=DUM	SEN0471
C	SEN0472
C	SEN0473
C	SEN0474
FOR ADJOINT STATES, SAVE THE LAST PUMPING PERIOD AND THE LAST	SEN0475
TIME STEP IN PRIOR PUMPING PERIODS	SEN0476
BSTP(1)=K	SEN0477
DO 130 I=1,K	SEN0478
130 BSTP(I+1)=STP(K-I+1)-1	SEN0479
ENDIF	SEN0480
RETURN	
END	
C=====	SEN0481
SUBROUTINE SENLRW(IUNIT,NRWD,IRWD)	SEN0482
C-----VERSION 1000 01FEB1992	SEN0483
C *****	SEN0484
C REWIND DATA FILES WHICH ARE TO BE REREAD	SEN0485
C *****	SEN0486
C SPECIFICATIONS:	SEN0487
C DIMENSION IUNIT(24),IRWD(NRWD)	SEN0488
C -----	SEN0489
5 FORMAT(I10)	SEN0490
IF(IUNIT(2).GT.0) THEN	SEN0491
REWIND(IUNIT(2))	SEN0492
READ(IUNIT(2),5)	SEN0493
ENDIF	SEN0494
IF(IUNIT(3).GT.0) THEN	SEN0495
REWIND(IUNIT(3))	SEN0496
READ(IUNIT(3),5)	SEN0497
ENDIF	SEN0498
IF(IUNIT(8).GT.0) THEN	SEN0499
REWIND(IUNIT(8))	SEN0500
READ(IUNIT(8),5)	SEN0501
ENDIF	SEN0502
IF(IUNIT(5).GT.0) THEN	SEN0503
REWIND(IUNIT(5))	SEN0504
READ(IUNIT(5),5)	SEN0505
ENDIF	SEN0506
IF(IUNIT(4).GT.0) THEN	SEN0507
REWIND(IUNIT(4))	SEN0508
READ(IUNIT(4),5)	SEN0509
ENDIF	SEN0510
IF(IUNIT(7).GT.0) THEN	SEN0511
REWIND(IUNIT(7))	SEN0512
READ(IUNIT(7),5)	SEN0513
ENDIF	SEN0514
IF(IUNIT(18).GT.0) THEN	SEN0515
REWIND(IUNIT(18))	SEN0516
READ(IUNIT(18),5)	SEN0517

ENDIF	SEN0518
IF(NRWD.GT.0) THEN	SEN0519
DO 180 N=1,NRWD	SEN0520
180 REWIND(IRWD(N))	SEN0521
ENDIF	SEN0522
REWIND(IUNIT(12))	SEN0523
READ(IUNIT(12),5)	SEN0524
RETURN	SEN0525
END	SEN0526
C=====	
SUBROUTINE SEN1FM(	SEN0527
1 KNST,NCOL,NROW,NLAY,KPER,IUHEAD,NPER,SHNW,SHOLD,ISN,IP,HNEW,	SEN0528
2 NODES,PID,NP,KSTP,PERTIM,TOTIM,BUFF,HOLD,ITERP,ISN1,IOUT)	SEN0529
C-----VERSION 1000 01FEB1992	SEN0530
C *****	SEN0531
C PREPARE HEAD ARRAYS REQUIRED TO CALCULATE SENSITIVITIES,	SEN0532
C INITIALIZE HNEW FOR SENSITIVITIES.	SEN0533
C *****	SEN0534
C SPECIFICATIONS:	SEN0535
C -----	SEN0536
CHARACTER*4 PID(NP),TEXT	SEN0537
INTEGER*4 IUNIT4	SEN0538
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)	SEN0539
DIMENSION SHNW(NCOL,NROW,NLAY),SHOLD(NCOL,NROW,NLAY),	SEN0540
1 BUFF(NCOL,NROW,NLAY),HOLD(NCOL,NROW,NLAY),TEXT(4,2)	SEN0541
COMMON /FLWCOM/LAYCON(80)	SEN0542
DATA TEXT(1,1),TEXT(2,1),TEXT(3,1),TEXT(4,1)	SEN0543
# /' ',' ',' ','HEAD'/	SEN0544
DATA TEXT(1,2),TEXT(2,2),TEXT(3,2),TEXT(4,2)	SEN0545
# /' ','SEN','SITI','VITY'/	SEN0546
C -----	SEN0547
C	SEN0548
C	SEN0549
C-----OPEN FILES	SEN0550
IF(IP.EQ.0.AND.ITERP.EQ.1.AND.KPER.EQ.1) THEN	SEN0551
NFILES=NPER	SEN0552
IF(ISN1.EQ.-1) NFILES=NP+1	SEN0553
IF(ISN1.EQ.10.AND.NP+1.GT.NPER) NFILES=NP+1	SEN0554
DO 20 I=1,NFILES	SEN0555
IUNIT4=IUHEAD-1+I	SEN0556
OPEN(UNIT=IUNIT4,STATUS='SCRATCH',FORM='UNFORMATTED',ERR=30)	SEN0557
20 CONTINUE	SEN0558
GO TO 40	SEN0559
30 WRITE(IOUT,600) NFILES,IUHEAD	SEN0560
600 FORMAT(' ERROR IN OPENING SCRATCH FILES. MAKE SURE',I5,	SEN0561
1 ' FORTRAN UNIT NUMBERS INCLUDING AND AFTER IUHEAD,',	SEN0562
1 ' WHICH EQUALS',I3,' (LINE 7)',	SEN0563
2 ' ARE UNSPECIFIED. (SEN1FM)')	SEN0564
STOP	SEN0565
40 CONTINUE	SEN0566
ENDIF	SEN0567
C-----ONLY NEED TO UPDATE HEAD VECTORS ONCE IF NPER=1	SEN0568
IF(NPER.EQ.1.AND.IP.GT.1) GO TO 70	SEN0569
C-----USE SS HEADS FROM LAST PAR. EST. ITERATION AS NEXT INITIAL HEADS	SEN0570
C-----READ PREVIOUS STEADY-STATE HEADS	SEN0571
IF(IP.EQ.0.AND.KPER.EQ.1.AND.	SEN0572
1 ((ITERP.GT.1.AND.ISN1.NE.10).OR.ITERP.GT.2).AND.ISN.NE.-1) THEN	SEN0573
REWIND(IUHEAD)	SEN0574
CALL UREADF(BUFF,NCOL,NROW,NLAY,IUHEAD)	SEN0575
CALL USAVEF(BUFF,DUM,DUM,HNEW,NODES,2)	SEN0576
ENDIF	SEN0577
C-----CALCULATING ADJOINT STATES	SEN0578
IF(ISN.GT.0.AND.IP.EQ.1) THEN	SEN0579
C-----HEADS FROM FINAL TIME STEP WERE PUT IN SHNW IN SENLOT	SEN0580
IF(KNST.EQ.1.AND.KPER.EQ.1) GO TO 70	SEN0581
C-----READ HEADS	SEN0582
IF(KNST.EQ.-1.AND.KPER.NE.NPER) THEN	SEN0583
IUNIT=IUHEAD+NPER-KPER	SEN0584
REWIND(IUNIT)	SEN0585
CALL UREADF(HOLD,NCOL,NROW,NLAY,IUNIT)	SEN0586
ENDIF	SEN0587
C-----SAVE HEADS FROM HOLD IN SHNW	SEN0588
IF(KNST.EQ.0.AND.NPER.GT.1)	SEN0589
1 CALL USAVEF(HOLD,SHNW,DUM,DUM,NODES,1)	SEN0590
ENDIF	SEN0591
C-----CALCULATING ITERATION-PARAMETER VECTOR	SEN0592
IF(ISN.GT.0.AND.IP.EQ.2) THEN	SEN0593
C-----READ HEADS	SEN0594
IUNIT=IUHEAD+KPER-1	SEN0595
REWIND(IUNIT)	SEN0596
CALL UREADF(SHNW,NCOL,NROW,NLAY,IUNIT)	SEN0597
ENDIF	SEN0598

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C-----CALCULATING SENSITIVITY-EQUATION SENSITIVITIES FOR ALL          SEN0599
C-----TIME STEPS BEFORE PROCEEDING TO THE NEXT PARAMETER              SEN0600
      IF (ISN.EQ.-2.AND.IP.GT.0) THEN                                     SEN0601
C-----SAVE HEADS FROM SHNW IN SHOLD                                     SEN0602
      IF (KPER.GT.1) CALL USAVEF(SHNW,SHOLD,DUM,DUM,NODES,1)           SEN0603
C-----READ HEADS                                                       SEN0604
      IUNIT=IUHEAD+KPER-1                                              SEN0605
      REWIND(IUNIT)                                                    SEN0606
      CALL UREADF(SHNW,NCOL,NROW,NLAY,IUNIT)                           SEN0607
      ENDIF                                                            SEN0608
C-----INITIALIZE HNEW FOR SENSITIVITY-EQUATION SENSITIVITIES (ISN=-2), SEN0609
C-----ADJOINT STATES, AND ITERATION-PARAMETER VECTOR (ISN>0)          SEN0610
      70 CONTINUE                                                       SEN0611
      IF (ISN.NE.-1.AND.KNST.EQ.1.AND.KPER.EQ.1.AND.IP.GT.0) THEN     SEN0612
        DO 105 IL=1,NLAY                                                SEN0613
        DO 105 IR=1,NROW                                                SEN0614
        DO 105 IC=1,NCOL                                                SEN0615
105      HNEW(IC,IR,IL)=0.D0                                           SEN0616
        ENDIF                                                            SEN0617
C-----CALCULATING SENSITIVITY-EQUATION SENSITIVITIES FOR ALL          SEN0618
C-----PARAMETERS BEFORE PROCEEDING TO NEXT TIME STEP                  SEN0619
      IF (ISN.EQ.-1) THEN                                              SEN0620
C-----HEADS                                                            SEN0621
      IF (IP.EQ.0) THEN                                                 SEN0622
        IF (KPER.GT.1) CALL USAVEF(SHNW,SHOLD,DUM,DUM,NODES,1)         SEN0623
        CALL USAVEF(DUM,SHNW,HNEW,DUM,NODES,3)                         SEN0624
        IF (KPER.EQ.1) THEN                                             SEN0625
          DO 220 K=1,NLAY                                               SEN0626
          CALL ULASAV(SHNW(1,1,K),TEXT(1,1),KSTP,KPER,PERTIM,         SEN0627
            TOTIM,NCOL,NROW,K,IUHEAD)                                   SEN0628
220      CONTINUE                                                       SEN0629
          REWIND(IUHEAD)                                                SEN0630
          ENDIF                                                          SEN0631
        ENDIF                                                            SEN0632
C-----SENSITIVITIES                                                    SEN0633
      IF ((KPER.EQ.1.OR.IFLAG.EQ.1).AND.IP.LT.NP) THEN                 SEN0634
        DO 230 IL=1,NLAY                                                SEN0635
        DO 230 IR=1,NROW                                                SEN0636
        DO 230 IC=1,NCOL                                                SEN0637
230      HOLD(IC,IR,IL)=0.                                             SEN0638
        ENDIF                                                            SEN0639
        IUNIT=IUHEAD+IP                                                SEN0640
        IF (IP.GE.1.AND.NPER.NE.1) THEN                                SEN0641
          CALL USAVEF(DUM,BUFF,HNEW,DUM,NODES,3)                       SEN0642
          DO 250 K=1,NLAY                                               SEN0643
          CALL ULASAV(BUFF(1,1,K),TEXT(1,2),KSTP,KPER,PERTIM,         SEN0644
            TOTIM,NCOL,NROW,K,IUNIT)                                   SEN0645
250      CONTINUE                                                       SEN0646
          REWIND(IUNIT)                                                SEN0647
          ENDIF                                                          SEN0648
        IF (KPER.GT.1.AND.IP.LT.NP) THEN                                SEN0649
          CALL UREADF(HOLD,NCOL,NROW,NLAY,IUNIT+1)                     SEN0650
          REWIND(IUNIT+1)                                              SEN0651
          ENDIF                                                          SEN0652
        IF (IP.NE.NP) CALL USAVEF(HOLD,DUM,DUM,HNEW,NODES,2)           SEN0653
C-----HEADS                                                            SEN0654
      IF (IP.EQ.NP) THEN                                                SEN0655
        IF (KPER.EQ.NPER) THEN                                         SEN0656
          CALL UREADF(SHNW,NCOL,NROW,NLAY,IUHEAD)                     SEN0657
          REWIND(IUHEAD)                                              SEN0658
          ENDIF                                                          SEN0659
        CALL USAVEF(SHNW,DUM,DUM,HNEW,NODES,2)                         SEN0660
        ENDIF                                                            SEN0661
      ENDIF                                                            SEN0662
C                                                                    SEN0663
      RETURN                                                            SEN0664
      END                                                                SEN0665

C=====SEN0666
      SUBROUTINE SENLRR (                                               SEN0667
1      IUNIT,WELL,NWELLS,MXWELL,DRAI,NDRAIN,MXDRN,NRCHOP,IRCH,        SEN0668
2      RECH,DELR,DELC,NROW,NCOL,NLAY,NEVTOP,IEVT,EVTR,EXDP,SURF,     SEN0669
3      RIVR,NRIVER,MXRIVR,BNDS,NBOUND,MXBND,IOUT,IP,ITERP,STRM,      SEN0670
4      ISTRM,NSTREM,MXSTRM,ITRBAR,NDIV,NSS,NTRIB,IDIVAR,ICALC,NRP) SEN0671
C-----VERSION 1000 01FEB1992 SENLRR                                  SEN0672
C      *****SEN0673
C      READ THE INPUT FILES AFTER THE FIRST READING, WHICH IS DONE BY THESEN0674
C      ORIGINAL MODULE SUBROUTINES                                    SEN0675
C      *****SEN0676
C      SPECIFICATIONS:                                                SEN0677
C      -----SEN0678
      DIMENSION IUNIT(24),WELL(4,MXWELL),DRAI(5,MXDRN),IEVT(NCOL,NROW), SEN0679

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1	EVTR(NCOL,NROW),EXDP(NCOL,NROW),SURF(NCOL,NROW),	SEN0680
1	DELR(NCOL),DELC(NROW),BND(5,MXBND),RIVR(6,MXRIVR),	SEN0681
1	IRCH(NCOL,NROW),RECH(NCOL,NROW),STRM(11,MXSTRM),	SEN0682
1	ISTRM(5,MXSTRM),ITRBAR(NSS,NTRIB),IDIVAR(NSS)	SEN0683
C	-----	SEN0684
C		SEN0685
	501 FORMAT(3I10,3F10.0)	SEN0686
	510 FORMAT(8I10)	SEN0687
	520 FORMAT(5I5,F15.0,4F10.0)	SEN0688
	530 FORMAT(3F10.0)	SEN0689
	540 FORMAT(10I5)	SEN0690
	C-----REPEAT READ NRP TIMES (FOR ADJOINT STATES NEED RECORDS FOR	SEN0691
	C-----LATTER TIME STEPS FIRST)	SEN0692
	DO 400 N=1,NRP	SEN0693
	C-----WEL	SEN0694
	IF(IUNIT(2).GT.0) THEN	SEN0695
	IN=IUNIT(2)	SEN0696
	READ(IN,501) ITMP	SEN0697
	IF(ITMP.GE.0) NWELLS=ITMP	SEN0698
	IF(ITMP.GT.0) THEN	SEN0699
	DO 100 II=1,NWELLS	SEN0700
	READ(IN,501) K,I,J,WELL(4,II)	SEN0701
	WELL(1,II)=K	SEN0702
	WELL(2,II)=I	SEN0703
	WELL(3,II)=J	SEN0704
100	CONTINUE	SEN0705
	ENDIF	SEN0706
	ENDIF	SEN0707
	C-----DRN	SEN0708
	IF(IUNIT(3).GT.0) THEN	SEN0709
	IN=IUNIT(3)	SEN0710
	READ(IN,501) ITMP	SEN0711
	IF(ITMP.GE.0) NDRAIN=ITMP	SEN0712
	IF(ITMP.GT.0) THEN	SEN0713
	DO 110 II=1,NDRAIN	SEN0714
	READ(IN,501) K,I,J,DRAI(4,II),DRAI(5,II)	SEN0715
	DRAI(1,II)=K	SEN0716
	DRAI(2,II)=I	SEN0717
	DRAI(3,II)=J	SEN0718
110	CONTINUE	SEN0719
	ENDIF	SEN0720
	ENDIF	SEN0721
	C-----RCH	SEN0722
	IF(IUNIT(8).GT.0) THEN	SEN0723
	IN=IUNIT(8)	SEN0724
	READ(IN,501) INRECH,INIRCH	SEN0725
	IF(INRECH.GE.0) THEN	SEN0726
	CALL U2DREN(RECH,NROW,NCOL,IN,IOUT)	SEN0727
	DO 125 IR=1,NROW	SEN0728
	DO 125 IC=1,NCOL	SEN0729
	RECH(IC,IR)=RECH(IC,IR)*DELR(IC)*DELC(IR)	SEN0730
125	CONTINUE	SEN0731
	ENDIF	SEN0732
	IF(NRCHOP.EQ.2.AND.INIRCH.GE.0)CALL U2DINN(IRCH,NROW,NCOL,IN)	SEN0733
	ENDIF	SEN0734
	C-----EVT	SEN0735
	IF(IUNIT(5).GT.0) THEN	SEN0736
	IN=IUNIT(5)	SEN0737
	READ(IN,510) INSURF,INEVTR,INEXDP,INIEVT	SEN0738
	IF(INSURF.GE.0) CALL U2DREN(SURF,NROW,NCOL,IN,IOUT)	SEN0739
	IF(INEVTR.GE.0) THEN	SEN0740
	CALL U2DREN(EVTR,NROW,NCOL,IN,IOUT)	SEN0741
	DO 135 IR=1,NROW	SEN0742
	DO 135 IC=1,NCOL	SEN0743
	EVTR(IC,IR)=EVTR(IC,IR)*DELR(IC)*DELC(IR)	SEN0744
135	CONTINUE	SEN0745
	ENDIF	SEN0746
	IF(INEXDP.GE.0) CALL U2DREN(EXDP,NROW,NCOL,IN,IOUT)	SEN0747
	IF(NEVTOP.EQ.2.AND.INIEVT.GE.0)CALL U2DINN(IEVT,NROW,NCOL,IN)	SEN0748
	ENDIF	SEN0749
	C-----RIV	SEN0750
	IF(IUNIT(4).GT.0) THEN	SEN0751
	IN=IUNIT(4)	SEN0752
	READ(IN,501) ITMP	SEN0753
	IF(ITMP.GE.0) NRIVER=ITMP	SEN0754
	IF(ITMP.GT.0) THEN	SEN0755
	DO 150 II=1,NRIVER	SEN0756
	READ(IN,501) K,I,J,(RIVR(JJ,II),JJ=4,6)	SEN0757
	RIVR(1,II)=K	SEN0758
	RIVR(2,II)=I	SEN0759
150	RIVR(3,II)=J	SEN0760
	ENDIF	SEN0761
	ENDIF	SEN0762

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C-----GHB
      IF(IUNIT(7).GT.0) THEN
      IN=IUNIT(7)
      READ(IN,501) ITMP
      IF(ITMP.GE.0) NBOUND=ITMP
      IF(ITMP.GT.0) THEN
      DO 170 II=1,NBOUND
      READ(IN,501) K,I,J,(BNDS(JJ,II),JJ=4,5)
      BNDS(1,II)=K
      BNDS(2,II)=I
170    BNDS(3,II)=J
      ENDIF
    ENDIF
C-----STR
      IF(IUNIT(18).NE.0) THEN
      IN=IUNIT(18)
      READ(IN,501) ITMP
      IF(ITMP.GE.0) NSTREM=ITMP
      IF(ITMP.GT.0) THEN
      DO 190 II=1,NSTREM
190    READ(IN,520) (ISTRM(JJ,II),JJ=1,5),(STRM(JJ,II),JJ=1,5)
      IF(ICALC.GT.0) THEN
      DO 200 II=1,NSTREM
200    READ(IN,530) (STRM(JJ,II),JJ=6,8)
      ENDIF
      DO 210 IK=1,NSS
      IDIVAR(IK)=0
      DO 210 JK=1,NTRIB
210    ITRBAR(IK,JK)=0
      IF(NTRIB.GT.0) THEN
      DO 220 IK=1,NSS
220    READ(IN,540) (ITRBAR(IK,JK),JK=1,NTRIB)
      ENDIF
      IF(NDIV.GT.0) THEN
      DO 230 IK=1,NSS
230    READ(IN,540) IDIVAR(IK)
      ENDIF
      DO 240 II=1,NSTREM
      DO 240 JJ=9,11
240    STRM(JJ,II)=0.
      ENDIF
    ENDIF
C
400 CONTINUE
RETURN
END
SEN0763
SEN0764
SEN0765
SEN0766
SEN0767
SEN0768
SEN0769
SEN0770
SEN0771
SEN0772
SEN0773
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SEN0800
SEN0801
SEN0802
SEN0803
SEN0804
SEN0805
SEN0806
SEN0807
SEN0808

C=====SEN0809
      SUBROUTINE SEN1FN(
1      CC,CR,CV,CELS,SMAT,NSN,NSM,SC1,ST,HNEW,BNDS,NBOUND,WELL,
2      NWELLS,RIVR,NRIVER,RECH,DELR,DELC,NROW,NCOL,NLAY,NP,NLL,
3      IBOUND,IP,B,KPER,NPER,MXBND,MXRIVR,MXWELL,TRPY,PID,ISN,
4      ITRP,B1,IOUT,LN,HY,EVTR,DRAI,NDRAIN,MXDRN,STRM,MXSTRM,
5      NSTREM,ISTRM,IUBD,NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,NLL11,
6      NLLIT,SV,WT,ND,IPRNP,BUFF,IWPG,NP1,NPNG,IPNG,IOUB,NDER,
7      COFF,ROFF,RINT,JOFF,IOFF,MLAY,NH,MAXM,MOBS,IDRY,JDRY)
C-----VERSION 1000 01FEB1992
C *****
C PUT NEW PARAMETERS IN MODEL ARRAYS.
C *****
C SPECIFICATIONS:
C -----
C CHARACTER*4 PID(NP1),PIDTMP,ANAME(6,6),PID1
C DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)
C DIMENSION SMAT(NCOL,NROW,NMM),NLL(NLL11,NP1),DELR(NCOL),DELC(NROW)
1      ,IBOUND(NCOL,NROW,NLAY),TRPY(NLAY),RECH(NCOL,NROW),
2      BNDS(5,MXBND),WELL(4,MXWELL),RIVR(6,MXRIVR),LM(NSM),
3      CELS(4,NSN),SC1(NCOL,NROW,NLAY),MATZ(NCOL,NROW,NZM),
4      CC(NCOL,NROW,NLAY),CR(NCOL,NROW,NLAY),LN(NP1),SFAC(NSM)
5      ,CV(NCOL,NROW,NLAY),ST(NCOL,NROW,NLAY),B(NP1),B1(NP1),
6      HY(NCOL,NROW,NLAY),EVTR(NCOL,NROW),DRAI(5,MXDRN),
7      STRM(11,MXSTRM),ISTRM(5,MXSTRM),LZ(LZ11,NSM),WT(ND),
8      SV(NCOL,NROW),BUFF(NCOL,NROW),IWPG(NP1),IPNG(NPNG),
9      COFF(NH),ROFF(NH),RINT(4,NH),JOFF(NH),IOFF(NH),
X      MLAY(MAXM,MOBS),NDER(5,NH)
C COMMON /FLWCOM/LAYCON(80)
C
C DATA ANAME(1,1),ANAME(2,1),ANAME(3,1),ANAME(4,1),ANAME(5,1),
1 ANAME(6,1) / 'H','YD','COND','AL','ONG','ROWS'/
C DATA ANAME(1,2),ANAME(2,2),ANAME(3,2),ANAME(4,2),ANAME(5,2),
1 ANAME(6,2) / '','TRAN','SMIS','AL','ONG','ROWS'/
C DATA ANAME(1,3),ANAME(2,3),ANAME(3,3),ANAME(4,3),ANAME(5,3),
SEN0810
SEN0811
SEN0812
SEN0813
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SEN0835
SEN0836
SEN0837
SEN0838
SEN0839
SEN0840
SEN0841
SEN0842
SEN0843

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1  ANAME(6,3) /' EVA','POTR','ANSP','IRAT','ION ','RATE'/          SEN0844
DATA ANAME(1,4),ANAME(2,4),ANAME(3,4),ANAME(4,4),ANAME(5,4),        SEN0845
1  ANAME(6,4) /'      ','V','ERTI','CAL ','LEAK','ANCE'/          SEN0846
DATA ANAME(1,5),ANAME(2,5),ANAME(3,5),ANAME(4,5),ANAME(5,5),        SEN0847
1  ANAME(6,5) /'      ','PRIM','ARY ','STOR','AGE ','COEF'/        SEN0848
DATA ANAME(1,6),ANAME(2,6),ANAME(3,6),ANAME(4,6),ANAME(5,6),        SEN0849
1  ANAME(6,6) /'      ','      ','      ','      ','RECH','ARGE'/  SEN0850
C-----SEN0851
500 FORMAT(/,' PARAMETER #',I3,', ID ',A4,' < 0 : NOT ',          SEN0852
1  'PHYSICALLY REASONABLE. CHANGED TO ',G13.6,' (SEN1FN)')        SEN0853
510 FORMAT(/,' LN PARAMETER #',I3,', ID ',A4,' <= 0 : NOT ',        SEN0854
1  'PHYSICALLY OR MATHEMATICALLY REASONABLE. CHANGED TO ',G13.6,SEN0855
2  '(SEN1FN)')              SEN0856
515 FORMAT(/,' MODEL-INPUT ARRAYS CALCULATED WITH INITIAL ',      SEN0857
1  'PARAMETER VALUES (DATA SET 8)')          SEN0858
520 FORMAT(1H0,/30X,6A4,' LAYER',I3,/,30X,73('-'))              SEN0859
530 FORMAT(/,10X,6A4,' FOR TIME STEP',I5,/,10X,43('-'))          SEN0860
540 FORMAT(8G10.3)                                                SEN0861
C-----SEN0862
C-----CHECK FOR PARAMETER VALUES <=0 THAT SHOULD BE >0      SEN0863
IF(IP.EQ.0.AND.KPER.EQ.1.AND.ITERP.GT.1) THEN                      SEN0864
DO 20 IIP=1,NP                                                    SEN0865
PIDTMP=PID(IIP)                                                  SEN0866
IF(B(IIP).LT.0..AND.LN(IIP).EQ.0.AND.                            SEN0867
1  (PIDTMP.EQ.'T ' .OR.PIDTMP.EQ.'S1 ' .OR.                      SEN0868
2  PIDTMP.EQ.'KV ' .OR.PIDTMP.EQ.'TKV ' .OR.                      SEN0869
3  PIDTMP.EQ.'GHB ' .OR.PIDTMP.EQ.'KRB ' .OR.                      SEN0870
4  PIDTMP.EQ.'KST ' .OR.PIDTMP.EQ.'KDR ' .OR.                      SEN0871
5  PIDTMP.EQ.'ANI ' .OR.PIDTMP.EQ.'ANIV ' .OR.                     SEN0872
6  PIDTMP.EQ.'ETM ')) THEN                                         SEN0873
IF(NPNG.GT.0) THEN                                                SEN0874
DO 10 I=1,NPNG                                                    SEN0875
10  IF(IIP.EQ.IPNG(I)) GO TO 20                                     SEN0876
ENDIF                                                             SEN0877
B(IIP)=B1(IIP)/100.                                               SEN0878
WRITE(IOUT,500) IIP,PIDTMP,B(IIP)                                SEN0879
ENDIF                                                             SEN0880
IF(B(IIP).LT.1.E-14.AND.LN(IIP).GT.0) THEN                       SEN0881
B(IIP)=1.E-14                                                     SEN0882
WRITE(IOUT,510) IIP,PIDTMP,B(IIP)                                SEN0883
ENDIF                                                             SEN0884
20  CONTINUE                                                       SEN0885
C-----WRITE PARAMETER VALUES TO IOUB                            SEN0886
WRITE(IOUB,540) (B(IIP),IIP=1,NP)                                SEN0887
ENDIF                                                             SEN0888
C-----SET FLAG TO INDICATE UNCONFINED LAYERS                    SEN0889
KK=0                                                              SEN0890
DO 30 K=1,NLAY                                                    SEN0891
30  KK=KK+LAYCON(K)                                                SEN0892
C-----READ IBOUND ARRAYS                                         SEN0893
IF(IUBD.GT.0.AND.(IP.EQ.0.OR.ISN.NE.-1).AND.                      SEN0894
1  (KPER.EQ.1.OR.(KPER.EQ.2.AND.KK.EQ.0))) THEN                  SEN0895
IF(KPER.EQ.1) REWIND(IUBD)                                         SEN0896
DO 40 K=1,NLAY                                                    SEN0897
40  CALL U2DINN(IBOUND(1,1,K),NROW,NCOL,IUBD)                     SEN0898
ENDIF                                                             SEN0899
C-----RECALCULATE INTERPOLATION COEFFICIENTS, IF NEEDED        SEN0900
IF(IP.EQ.0.AND.ISN.EQ.-1.AND.KPER.EQ.1.AND.ITERP.GT.1) THEN      SEN0901
C-----SKIP IF ALL LAYERS ARE CONFINED                            SEN0902
IF(KK.EQ.0) GO TO 60                                              SEN0903
C-----HAVE ANY DRY CELLS AFFECTED THE INTERPOLATION?          SEN0904
IF(IDRY+JDRY.GT.0) THEN                                           SEN0905
ML=0                                                              SEN0906
DO 50 N=1,NH                                                      SEN0907
IF(NDER(1,N).LT.0) ML=ML+1                                         SEN0908
IF(COFF(N).GT..5.OR.WT(N).LT.0) THEN                               SEN0909
IF(COFF(N).GT..5) COFF(N)=COFF(N)-5.                             SEN0910
IF(WT(N).LT.0) WT(N)=ABS(WT(N))                                  SEN0911
CALL SSEN1I (NDER(1,N),COFF(N),ROFF(N),DELR,DELC,IBOUND,          SEN0912
1  NCOL,NROW,NLAY,RINT(1,N),JOFF(N),IOFF(N),MLAY(1,ML))          SEN0913
ENDIF                                                             SEN0914
50  CONTINUE                                                       SEN0915
ENDIF                                                             SEN0916
ENDIF                                                             SEN0917
60  CONTINUE                                                       SEN0918
C-----INITIALIZE MODEL INPUTS TO ZERO                            SEN0919
IF(IP.EQ.0.AND.KPER.EQ.1) THEN                                     SEN0920
DO 80 IIP=1,NP1                                                  SEN0921
IF(PID(IIP).EQ.'T ' .OR.PID(IIP).EQ.'TKV ') THEN                 SEN0922
DO 70 K=1,NLAY                                                    SEN0923
DO 70 I=1,NROW                                                    SEN0924
DO 70 J=1,NCOL                                                    SEN0925
SEN0926

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70	ST(J,I,K)=0.	SEN0927
	GO TO 90	SEN0928
	ENDIF	SEN0929
80	CONTINUE	SEN0930
90	DO 110 IIP=1,NP1	SEN0931
	IF(PID(IIP).EQ.'KV '.OR.PID(IIP).EQ.'TKV ') THEN	SEN0932
	DO 100 K=1,NLAY-1	SEN0933
	DO 100 I=1,NROW	SEN0934
	DO 100 J=1,NCOL	SEN0935
100	CV(J,I,K)=0.	SEN0936
	GO TO 130	SEN0937
	ENDIF	SEN0938
110	CONTINUE	SEN0939
C-----	IF NO PID=KV OR TKV, REINITIALIZE CV BENEATH A WATER TABLE LAYER	SEN0940
	IF(ITERP.GT.1.AND.KPER.EQ.1.AND.NLAY.GT.1.AND.	SEN0941
1	LAYCON(1).EQ.1) THEN	SEN0942
	DO 120 I=1,NROW	SEN0943
	DO 120 J=1,NCOL	SEN0944
	CV(J,I,1)=SV(J,I)	SEN0945
	IF(BOUND(J,I,1).EQ.0) CV(J,I,1)=0.	SEN0946
120	CONTINUE	SEN0947
	ENDIF	SEN0948
130	DO 150 IIP=1,NP1	SEN0949
	IF(PID(IIP).EQ.'S1 ') THEN	SEN0950
	DO 140 K=1,NLAY	SEN0951
	DO 140 I=1,NROW	SEN0952
	DO 140 J=1,NCOL	SEN0953
140	SCL(J,I,K)=0.	SEN0954
	GO TO 160	SEN0955
	ENDIF	SEN0956
150	CONTINUE	SEN0957
	ENDIF	SEN0958
160	DO 180 IIP=1,NP1	SEN0959
	IF(PID(IIP).EQ.'RCH ') THEN	SEN0960
	DO 170 I=1,NROW	SEN0961
	DO 170 J=1,NCOL	SEN0962
170	RECH(J,I)=0.	SEN0963
	GO TO 190	SEN0964
	ENDIF	SEN0965
180	CONTINUE	SEN0966
190	DO 210 IIP=1,NP1	SEN0967
	IF(PID(IIP).EQ.'ETM ') THEN	SEN0968
	DO 200 I=1,NROW	SEN0969
	DO 200 J=1,NCOL	SEN0970
200	EVTR(J,I)=0.	SEN0971
	GO TO 220	SEN0972
	ENDIF	SEN0973
210	CONTINUE	SEN0974
220	CONTINUE	SEN0975
C-----	PUT NEW PARAMETERS IN MODEL ARRAYS.	SEN0976
C-----	SET COUNTERS	SEN0977
	NS=0	SEN0978
	NM=0	SEN0979
	ICH=0	SEN0980
C-----	LOOP THROUGH PARAMETERS	SEN0981
	DO 350 IIP=1,NP1	SEN0982
	PIDTMP=PID(IIP)	SEN0983
	BB=B(IIP)	SEN0984
C-----	PARAMETERS DEFINED BY MATRICES	SEN0985
	IF(PIDTMP.EQ.'T '.OR.PIDTMP.EQ.'TKV ') THEN	SEN0986
	IF(PIDTMP.EQ.'TKV '.AND.KPER.GT.1) GO TO 320	SEN0987
	NM1=NK	SEN0988
	DO 310 LL=1,NLL1	SEN0989
	NLO=NLL(LL,IIP)	SEN0990
	IF(NLO.EQ.0) THEN	SEN0991
	IF(PIDTMP.EQ.'TKV ') GO TO 310	SEN0992
	GO TO 320	SEN0993
	ENDIF	SEN0994
	IF(NLO.GT.0) NM=NM+1	SEN0995
	IF(IP.EQ.0.AND.KPER.EQ.1) THEN	SEN0996
	IF(PIDTMP.EQ.'TKV '.AND.MOD(LL+1,3).NE.0) GO TO 310	SEN0997
	NL=IABS(NLO)	SEN0998
	IF(NLO.GT.0) THEN	SEN0999
	SF=SFAC(NM)*BB	SEN1000
	M=IM(NM)	SEN1001
	LZ1=LZ(1,NM)	SEN1002
	IF(M.EQ.0.AND.LZ1.EQ.0) THEN	SEN1003
	DO 240 I=1,NROW	SEN1004
	DO 240 J=1,NCOL	SEN1005
240	ST(J,I,NL)=ST(J,I,NL)+SF	SEN1006
	ENDIF	SEN1007
	IF (M.NE.0.AND.LZ1.EQ.0) THEN	SEN1008
	DO 250 I=1,NROW	SEN1009

	DO 250 J=1,NCOL	SEN1010
250	IF(SMAT(J,I,M).NE.0.) ST(J,I,NL)=ST(J,I,NL)+	SEN1011
1	SF*SMAT(J,I,M)	SEN1012
	ENDIF	SEN1013
	IF (M.EQ.0.AND.LZ1.NE.0) THEN	SEN1014
	DO 260 IZ=2,LZ1	SEN1015
	NZ=LZ(IZ,NM)	SEN1016
	IF(NZ.EQ.0) GO TO 270	SEN1017
	DO 260 I=1,NROW	SEN1018
	DO 260 J=1,NCOL	SEN1019
260	IF(MATZ(J,I,LZ1).EQ.NZ) ST(J,I,NL)=ST(J,I,NL)+SF	SEN1020
270	CONTINUE	SEN1021
	ENDIF	SEN1022
	IF (M.NE.0.AND.LZ1.NE.0) THEN	SEN1023
	DO 280 IZ=2,LZ1	SEN1024
	NZ=LZ(IZ,NM)	SEN1025
	IF(NZ.EQ.0) GO TO 290	SEN1026
	DO 280 I=1,NROW	SEN1027
	DO 280 J=1,NCOL	SEN1028
280	IF(MATZ(J,I,LZ1).EQ.NZ.AND.SMAT(J,I,M).NE.0.)	SEN1029
1	ST(J,I,NL)=ST(J,I,NL)+SF*SMAT(J,I,M)	SEN1030
290	CONTINUE	SEN1031
	ENDIF	SEN1032
	ELSEIF(NLO.LT.0) THEN	SEN1033
	DO 300 I=1,NROW	SEN1034
	DO 300 J=1,NCOL	SEN1035
300	ST(J,I,NL)=ST(J,I,NL)+BB	SEN1036
	ENDIF	SEN1037
	ENDIF	SEN1038
310	CONTINUE	SEN1039
	IF(PIDTMP.EQ.'TKV ') NM=NM1	SEN1040
320	CONTINUE	SEN1041
	ENDIF	SEN1042
	IF(PIDTMP.EQ.'KV ' .OR.PIDTMP.EQ.'TKV ')	SEN1043
1	CALL SSEN1M(PIDTMP,CV,SMAT,NCOL,NROW,NLAY,NSM,NM,	SEN1044
2	NLL(1,IIP),BB,KPER,IP,DELR,DELC,IBOUND,ISN,	SEN1045
3	NMM,NZM,LZ1,SFAC,LZ,LM,MATZ,NLL11,NLLIT)	SEN1046
	IF(PIDTMP.EQ.'S1 ')	SEN1047
1	CALL SSEN1M(PIDTMP,SCI,SMAT,NCOL,NROW,NLAY,NSM,NM,	SEN1048
2	NLL(1,IIP),BB,KPER,IP,DELR,DELC,IBOUND,ISN,	SEN1049
3	NMM,NZM,LZ1,SFAC,LZ,LM,MATZ,NLL11,NLLIT)	SEN1050
	IF(PIDTMP.EQ.'RCH ')	SEN1051
1	CALL SSEN1M(PIDTMP,RECH,SMAT,NCOL,NROW,NLAY,NSM,NM,	SEN1052
2	NLL(1,IIP),BB,KPER,IP,DELR,DELC,IBOUND,ISN,	SEN1053
3	NMM,NZM,LZ1,SFAC,LZ,LM,MATZ,NLL11,NLLIT)	SEN1054
	IF(PIDTMP.EQ.'ETM ')	SEN1055
1	CALL SSEN1M(PIDTMP,EVTR,SMAT,NCOL,NROW,NLAY,NSM,NM,	SEN1056
2	NLL(1,IIP),BB,KPER,IP,DELR,DELC,IBOUND,ISN,	SEN1057
3	NMM,NZM,LZ1,SFAC,LZ,LM,MATZ,NLL11,NLLIT)	SEN1058
C-----	ANI PARAMETERS	SEN1059
	IF(PIDTMP.EQ.'ANI '.AND.KPER.EQ.1) THEN	SEN1060
	DO 330 LL=1,NLL11	SEN1061
330	IF(NLL(LL,IIP).GT.0) TRPY(NLL(LL,IIP))=BB	SEN1062
	ENDIF	SEN1063
C-----	PARAMETERS DEFINED BY LISTS OF CELLS	SEN1064
	IF(PIDTMP.EQ.'CH ')	SEN1065
1	CALL SSEN1J(IIP,B,NLL(1,IIP),CELS,NS,NSN,HNEW,NCOL,NROW,NLAY,	SEN1066
1	NPI,IP,KPER,ICH,NLL11)	SEN1067
	IF(PIDTMP.EQ.'GHB ')	SEN1068
1	CALL SSEN1K(PIDTMP,IIP,NLL(1,IIP),NBOUND,MXBND,BNDS,CELS,	SEN1069
1	NSN,NS,NCOL,NROW,NLAY,5,IBOUND,NPER,KPER,BB,IP,ISN,	SEN1070
1	ISTRM,NLL11,NLLIT)	SEN1071
	IF(PIDTMP.EQ.'Q ')	SEN1072
1	CALL SSEN1K(PIDTMP,IIP,NLL(1,IIP),NWELLS,MXWELL,WELL,CELS,	SEN1073
1	NSN,NS,NCOL,NROW,NLAY,4,IBOUND,NPER,KPER,BB,IP,ISN,	SEN1074
1	ISTRM,NLL11,NLLIT)	SEN1075
	IF(PIDTMP.EQ.'KRB ')	SEN1076
1	CALL SSEN1K(PIDTMP,IIP,NLL(1,IIP),NRIVER,MXRIVR,RIVR,CELS,	SEN1077
1	NSN,NS,NCOL,NROW,NLAY,6,IBOUND,NPER,KPER,BB,IP,ISN,	SEN1078
1	ISTRM,NLL11,NLLIT)	SEN1079
	IF(PIDTMP.EQ.'KDR ')	SEN1080
1	CALL SSEN1K(PIDTMP,IIP,NLL(1,IIP),NDRAIN,MXDRN,DRAI,CELS,	SEN1081
1	NSN,NS,NCOL,NROW,NLAY,5,IBOUND,NPER,KPER,BB,IP,ISN,	SEN1082
1	ISTRM,NLL11,NLLIT)	SEN1083
	IF(PIDTMP.EQ.'KST ')	SEN1084
1	CALL SSEN1K(PIDTMP,IIP,NLL(1,IIP),NSTREM,MXSTRM,STRM,CELS,	SEN1085
1	NSN,NS,NCOL,NROW,NLAY,11,IBOUND,NPER,KPER,BB,IP,ISN,	SEN1086
1	ISTRM,NLL11,NLLIT)	SEN1087
350	CONTINUE	SEN1088
C-----	ANIV PARAMETERS	SEN1089
	IF(KPER.EQ.1.AND.IP.EQ.0) THEN	SEN1090
	DO 380 IIP=1,NP	SEN1091
	IF(PID(IIP).EQ.'ANIV') THEN	SEN1092



BB=B(IIP)	SEN1093
DO 370 LL=1,NLLI1	SEN1094
IF(NLL(LL,IIP).GT.0) THEN	SEN1095
NL=NLL(LL,IIP)	SEN1096
DO 360 I=1,NROW	SEN1097
DO 360 J=1,NCOL	SEN1098
360 CV(J,I,NL)=BB*CV(J,I,NL)	SEN1099
ENDIF	SEN1100
370 CONTINUE	SEN1101
ENDIF	SEN1102
380 CONTINUE	SEN1103
ENDIF	SEN1104
C-----SET CV TO ZERO WHERE NOT USED	SEN1105
DO 400 IIP=1,NP1	SEN1106
PIDTMP=PID(IIP)	SEN1107
IF(PIDTMP.EQ.'KV'.OR.PIDTMP.EQ.'TKV') THEN	SEN1108
DO 390 NL=1,NLAY-1	SEN1109
DO 390 I=1,NROW	SEN1110
DO 390 J=1,NCOL	SEN1111
IF(IBOUND(J,I,NL).EQ.0.OR.IBOUND(J,I,NL+1).EQ.0)	SEN1112
1 CV(J,I,NL)=0.	SEN1113
390 CONTINUE	SEN1114
GO TO 410	SEN1115
ENDIF	SEN1116
400 CONTINUE	SEN1117
410 CONTINUE	SEN1118
C-----PRINT MODEL INPUT ARRAYS WHICH ARE NROW X NCOL	SEN1119
IF(ITERP.EQ.1.AND.IPRNP.GT.0.AND.(ISN.NE.-2.OR.IP.EQ.0)) THEN	SEN1120
ITS=KPER-1	SEN1121
IFLAG=1	SEN1122
IF(ITS.EQ.0) IFLAG=0	SEN1123
IF(ISN.GT.0.AND.IP.EQ.1) ITS=NPER-KPER	SEN1124
IF(KPER.EQ.1) THEN	SEN1125
DO 470 JJ=1,3	SEN1126
IF(JJ.EQ.1) THEN	SEN1127
PIDTMP='S1'	SEN1128
INAME=5	SEN1129
ELSEIF(JJ.EQ.3) THEN	SEN1130
PIDTMP='KV'	SEN1131
INAME=4	SEN1132
ENDIF	SEN1133
IF(JJ.EQ.2) PIDTMP='T'	SEN1134
DO 460 NL=1,NLAY	SEN1135
DO 450 IIP=1,NP1	SEN1136
PID1=PID(IIP)	SEN1137
DO 440 L=1,NLLI1	SEN1138
ICOR=0	SEN1139
IF(PID1.EQ.'TKV'.AND.MOD(L+2,3).EQ.0) ICOR=1	SEN1140
IF((PID1.EQ.PIDTMP.OR.(PID1.EQ.'TKV'.AND.	SEN1141
1 ((JJ.EQ.2.AND.MOD(L+1,3).EQ.0).OR.	SEN1142
1 (JJ.EQ.3.AND.MOD(L+1,3).NE.0)))	SEN1143
1 .AND.NLL(L,IIP)-ICOR.EQ.NL) THEN	SEN1144
IF(JJ.EQ.2) THEN	SEN1145
INAME=2	SEN1146
IF(NL.EQ.1.AND.LAYCON(NL).EQ.1) INAME=1	SEN1147
ENDIF	SEN1148
IF(IFLAG.EQ.0) WRITE(IOUT,515)	SEN1149
IFLAG=1	SEN1150
WRITE(IOUT,520) (ANAME(I,INAME),I=1,6),NL-ICOR	SEN1151
IF(JJ.EQ.2) THEN	SEN1152
1 CALL ULAPRW(ST(1,1,NL),ANAME(1,INAME),0,	SEN1153
1 0,NCOL,NROW,0,IPRNP,IOUT)	SEN1154
GO TO 460	SEN1155
ELSEIF(JJ.EQ.1) THEN	SEN1156
DO 420 I=1,NROW	SEN1157
DO 420 J=1,NCOL	SEN1158
420 BUFF(J,I)=SC1(J,I,NL)/(DELR(J)*DELC(I))	SEN1159
ELSEIF(JJ.EQ.3) THEN	SEN1160
DO 430 I=1,NROW	SEN1161
DO 430 J=1,NCOL	SEN1162
430 BUFF(J,I)=CV(J,I,NL-ICOR)/(DELR(J)*DELC(I))	SEN1163
ENDIF	SEN1164
CALL ULAPRW(BUFF,ANAME(1,INAME),0,0,	SEN1165
1 NCOL,NROW,0,IPRNP,IOUT)	SEN1166
GO TO 460	SEN1167
ENDIF	SEN1168
440 CONTINUE	SEN1169
450 CONTINUE	SEN1170
460 CONTINUE	SEN1171
470 CONTINUE	SEN1172
ENDIF	SEN1173
C-----RCH AND ETM	SEN1174
DO 720 JJ=1,2	SEN1175

PIDTMP='ETM '	SEN1176
IF(JJ.EQ.1) PIDTMP='RCH '	SEN1177
DO 710 IIP=1,NP1	SEN1178
IF(PID(IIP).EQ.PIDTMP) THEN	SEN1179
DO 700 LL=1,NLLIT	SEN1180
1 IF((ISN.LT.0.OR.IP.NE.1).AND.NLL(2*LL,IIP).EQ.ITS	SEN1181
.AND.NLL(1,IIP).GT.0) THEN	SEN1182
INAME=3	SEN1183
IF(JJ.EQ.1) INAME=6	SEN1184
WRITE(IOUT,530) (ANAME(I,INAME),I=1,6),NLL(2*LL,IIP)	SEN1185
IF(JJ.EQ.1) THEN	SEN1186
DO 480 I=1,NROW	SEN1187
DO 480 J=1,NCOL	SEN1188
480 BUFF(J,I)=RECH(J,I)/(DELR(J)*DELC(I))	SEN1189
ELSE	SEN1190
DO 490 I=1,NROW	SEN1191
DO 490 J=1,NCOL	SEN1192
490 BUFF(J,I)=EVTR(J,I)/(DELR(J)*DELC(I))	SEN1193
ENDIF	SEN1194
CALL ULAPRW(BUFF,ANAME(1,INAME),0,0,	SEN1195
1 NCOL,NROW,0,IPRNP,IOUT)	SEN1196
GO TO 720	SEN1197
ENDIF	SEN1198
700 CONTINUE	SEN1199
ENDIF	SEN1200
710 CONTINUE	SEN1201
720 CONTINUE	SEN1202
ENDIF	SEN1203
C UPDATE CC AND CR	SEN1204
IF(IP.EQ.0.AND.KPER.EQ.1) THEN	SEN1205
KB=0	SEN1206
DO 750 K=1,NLAY	SEN1207
IF(LAYCON(K).EQ.0) THEN	SEN1208
YX=TRPY(K)*2.	SEN1209
DO 730 I=1,NROW	SEN1210
DO 730 J=1,NCOL	SEN1211
T1=ST(J,I,K)	SEN1212
CR(J,I,K)=0.	SEN1213
CC(J,I,K)=0.	SEN1214
IF(IBOUND(J,I,K).NE.0.AND.T1.NE.0.) THEN	SEN1215
IF(J.NE.NCOL.AND.IBOUND(J+1,I,K).NE.0) THEN	SEN1216
T2=ST(J+1,I,K)	SEN1217
IF(T2.NE.0.)	SEN1218
1 CR(J,I,K)=2.*T2*T1*DELC(I)/(T1*DELR(J+1)+T2*DELR(J))	SEN1219
ENDIF	SEN1220
IF(I.NE.NROW.AND.IBOUND(J,I+1,K).NE.0) THEN	SEN1221
T2=ST(J,I+1,K)	SEN1222
IF(T2.NE.0.)	SEN1223
1 CC(J,I,K)=YX*T2*T1*DELR(J)/(T1*DELC(I+1)+T2*DELC(I))	SEN1224
ENDIF	SEN1225
ENDIF	SEN1226
730 CONTINUE	SEN1227
ELSEIF (LAYCON(K).EQ.1) THEN	SEN1228
KB=KB+1	SEN1229
DO 740 I=1,NROW	SEN1230
DO 740 J=1,NCOL	SEN1231
740 HY(J,I,KB)=ST(J,I,K)	SEN1232
ENDIF	SEN1233
750 CONTINUE	SEN1234
ENDIF	SEN1235
C RETURN	SEN1236
END	SEN1237
	SEN1238
C=====	SEN1239
SUBROUTINE SENLRH(IUNHEA,BUFF,HNEW,KPER,NROW,NCOL,NLAY,IBOUND)	SEN1240
C-----VERSION 1000 01FEB1992	SEN1241
C *****	SEN1242
C CHANGE HEADS AT CONSTANT-HEAD BOUNDARIES	SEN1243
C *****	SEN1244
C SPECIFICATIONS:	SEN1245
C -----	SEN1246
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)	SEN1247
DIMENSION BUFF(NCOL,NROW,NLAY),IBOUND(NCOL,NROW,NLAY)	SEN1248
C -----	SEN1249
500 FORMAT(10F5.0)	SEN1250
C-----REWIND INPUT FILE	SEN1251
REWIND(IUNHEA)	SEN1252
C-----READ TIME STEPS AT WHICH HYDRAULIC HEADS AT CONSTANT-HEAD	SEN1253
C-----BOUNDARIES CHANGE	SEN1254
READ(IUNHEA,500) (BUFF(IN,1,1),IN=1,16)	SEN1255
C-----ARE THERE CHANGES FOR THE PRESENT TIME STEP?	SEN1256

```

DO 100 IN=1,16
  IF(BUFF(IN,1,1).EQ.0.) RETURN
  IF(INT(BUFF(IN,1,1)).EQ.KPER) GO TO 105
100 CONTINUE
  RETURN
C-----READ ASSOCIATED HYDRAULIC HEADS FROM IUNHEA
105 DO 120 IM=1,IN
  DO 110 K=1,NLAY
110   CALL U2DREN(BUFF(1,1,K),NCOL,NROW,IUNHEA)
120 CONTINUE
C-----REPLACE HYDRAULIC HEADS ALONG CONSTANT-HEAD BOUNDARIES
DO 140 K=1,NLAY
DO 140 I=1,NROW
DO 140 J=1,NCOL
140   IF(BOUND(J,I,K).LT.0) HNEW(J,I,K)=BUFF(J,I,K)
  RETURN
END

```

SEN1257  
SEN1258  
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SEN1260  
SEN1261  
SEN1262  
SEN1263  
SEN1264  
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SEN1267  
SEN1268  
SEN1269  
SEN1270  
SEN1271  
SEN1272  
SEN1273

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C-----
SUBROUTINE SENLAR(
1   IOUT,NROW,NCOL,NLAY,NP,ISN,NH,NDER,HNEW,PID,
2   DID,IP,KPER,BUFF,KSTP,PERTIM,TOTIM,X,DELR,DELC,
3   IBOUND,COFF,ROFF,H,WT,HOBS,IPO,ITERP,IPAR,
4   RINT,JOFF,IOFF,MLAY,PR,MOBS,NPER,B,LN,NQ,NQC,
5   NQT,NQOB,NQCL,IQOB,QCLS,IBT,MXBND,NBOUND,BNDS,
6   MXRIVR,NRIVER,RIVR,SHNW,LASTX,ISCALS,TOFF,
7   MXDRN,NDRAIN,DRAI,MXSTRM,NSTREM,STRM,ISTRM,RHS,
8   MAXM)
C-----VERSION 1000 01FEB1992
C *****
C COMPUTE OBJ. FUNC. DERIVATIVE AND ADD TO RHS TO CALCULATE ADJOINT
C STATES
C *****
C SPECIFICATIONS:
C -----
CHARACTER*4 PID(NP),DID(NH+NQT)
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)
DIMENSION NDER(5,NH),BUFF(NCOL*NROW*NLAY),X(NP,1),
1   DELR(NCOL),DELC(NROW),IBOUND(NCOL,NROW,NLAY),COFF(NH),
1   ROFF(NH),H(NH+NQT),WT(NH+NQT),HOBS(NH+NQT),RINT(4,NH),
1   JOFF(NH),IOFF(NH),MLAY(MAXM,MOBS),PR(MAXM,MOBS),B(NP),LN(NP),
1   RIVR(6,MXRIVR),BNDS(5,MXBND),IBT(2,NQ),NQOB(NQ),NQCL(NQ),
1   IQOB(NQT),QCLS(4,NQC),TOFF(NH+NQT),DRAI(5,MXDRN),
1   RHS(NCOL,NROW,NLAY),STRM(11,MXSTRM),ISTRM(5,MXSTRM)
COMMON /FLWCOM/LAYCON(80)
C -----
C -----HEADS
C IF(NH.GT.0) CALL SSENLU(NH,NDER,IOFF,JOFF,KPER,MLAY,IBOUND,RINT,
1   DID,COFF,ROFF,DELR,DELC,NCOL,NROW,NLAY,PR,H,HOBS,WT,HNEW,X,IP,
1   IDRY,NP,MOBS,B,LN,ISN,NQT,TOFF,NPER,RHS,PV,MAXM,
3   ITERP,JDRY,IPAR,IOUT)
  RETURN
END

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SEN1274  
SEN1275  
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SEN1308

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C-----
SUBROUTINE SENLAP(
1   PID,KPER,NPER,DELT,IP,NP,NCOL,NROW,NLAY,NODES,
2   HOLD,SHNW,HNEW,XX,SMAT,NLL,NM,NSM,DELR,DELC,ST,
3   IBOUND,TRPY,CELS,NS,NSN,MXWELL,NWELLS,MXBND,
4   NBOUND,MXRIVR,NRIVER,BNDS,WELL,RIVR,NRCHOP,IRCH,
5   ISN,RHS,SHOLD,SC1,CR,CC,CV,IFLCH,IOUT,HY,BOT,
6   SC2,KITER,NDRAIN,MXDRN,DRAI,SURF,EXDP,
7   NEVTOP,MXSTRM,NSTREM,STRM,ISTRM,DD,B,LN,BUFF,
8   H,HOBS,RINT,IOFF,JOFF,NDER,NH,TOFF,SCL,MM,NZM,
9   LZ11,SFAC,LZ,LM,MATZ,NLL11,NLL1T)
C-----VERSION 1000 01FEB1992
C *****
C COMPUTE CONTRIBUTIONS TO THE ADJOINT SENSITIVITIES, OR COMPUTE
C RHS FOR SENSITIVITY-EQUATION SENSITIVITIES OR THE DERIVATIVE
C OF HYDRAULIC HEAD WITH RESPECT TO NEWTON'S STEP SIZE.
C *****
C SPECIFICATIONS:
C -----
CHARACTER*4 PID(NP),PIDTMP
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY),DD(NP),XX(NP)
DIMENSION HOLD(NCOL,NROW,NLAY),SHNW(NCOL,NROW,NLAY),LM(NSM),
1   SMAT(NCOL,NROW,NSM),NLL(NLL11,NP),DELR(NCOL),DELC(NROW),
2   IBOUND(NCOL,NROW,NLAY),TRPY(NLAY),DRAI(5,MXDRN),
3   BNDS(5,MXBND),WELL(4,MXWELL),RIVR(6,MXRIVR),SFAC(NSM),
4   CELS(4,NSN),IRCH(NCOL,NROW),RHS(NCOL,NROW,NLAY),
5   SHOLD(NCOL,NROW,NLAY),SC1(NCOL,NROW,NLAY),LZ(LZ11,NSM),

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SEN1309  
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SEN1335

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6          CC(NCOL,NROW,NLAY),CR(NCOL,NROW,NLAY),ST(NODES),          SEN1336
7          CV(NCOL,NROW,NLAY),HY(NCOL,NROW,NLAY),B(NP),SCL(NP),      SEN1337
8          BOT(NCOL,NROW,NLAY),LN(NP),MATZ(NCOL,NROW,NZM),          SEN1338
9          SC2(NCOL,NROW,NLAY),SURF(NCOL,NROW),EXDP(NCOL,NROW),      SEN1339
X          STRM(11,MXSTRM),ISTRM(5,MXSTRM),BUFF(NCOL,NROW,NLAY),    SEN1340
1         H(NH),HOBS(NH),RINT(4,NH),IOFF(NH),JOFF(NH),NDER(5,NH)    SEN1341
COMMON /FLWCOM/LAYCON(80)                                           SEN1342
C-----
C-----
C-----INITIALIZE RHS FOR SENSITIVITY-EQUATION SENSITIVITIES OR    SEN1343
C-----ITERATION-PARAMETER VECTOR                                  SEN1344
          IF(ISN.LT.0.OR.IP.EQ.2) THEN                               SEN1345
              DO 100 K=1,NLAY                                         SEN1346
              DO 100 I=1,NROW                                         SEN1347
              DO 100 J=1,NCOL                                         SEN1348
100         RHS(J,I,K) =0.                                           SEN1349
          ENDIF                                                       SEN1350
C-----INITIALIZE XX FOR ADJOINT-STATE SENSITIVITIES              SEN1351
          IF(ISN.GT.0.AND.IP.EQ.1.AND.KPER.EQ.1) THEN               SEN1352
              DO 105 IIP=1,NP                                         SEN1353
105         XX(IIP)=0.D0                                             SEN1354
          ENDIF                                                       SEN1355
C-----SET FLAG WHICH DISTINGUISHES BETWEEN CALCULATING ADJOINT-STATE SEN1356
C-----SENSITIVITIES AND THE ITERATION-PARAMETER VECTOR          SEN1357
          IHESS=0                                                     SEN1358
          IF(ISN.GT.0.AND.IP.EQ.2) IHESS=1                             SEN1359
C-----IF CALCULATING ADJOINT-STATE SENSITIVITIES OR ITERATION PARAMETER SEN1360
C-----VECTOR, ARRANGE TO LOOP THROUGH THE PARAMETERS            SEN1361
          IIP=IP                                                       SEN1362
          NNP=1                                                         SEN1363
          IF(ISN.GT.0) THEN                                             SEN1364
              NNP=NP                                                   SEN1365
              NS=0                                                     SEN1366
              NM=0                                                     SEN1367
              IFLCH=0                                                  SEN1368
          ENDIF                                                       SEN1369
          DO 110 IPP=1,NNP                                             SEN1370
              IP=IPP                                                   SEN1371
              IF(ISN.LT.0)IP=IIP                                       SEN1372
              PIDTMP=PID(IP)                                           SEN1373
              IF(PIDTMP.EQ.'GHB ') CALL SSEN1D(PIDTMP,NLL(1,IP),NBOUND,MXBND, SEN1374
1              BND,CELS,NSN,NS,SHNW,HNEW,NCOL,NROW,NLAY,IOUT,5,IBOUND, SEN1375
2              NPER,KPER,XX(IP),ISN,RHS,ISTRM,DD(IP),IHESS,B(IP),LN(IP), SEN1376
3              SCL(IP),NLL11,NLLIT)                                     SEN1377
              IF(PIDTMP.EQ.'KDR ') CALL SSEN1D(PIDTMP,NLL(1,IP),NBOUND,MXDRN, SEN1378
1              DRAI,CELS,NSN,NS,SHNW,HNEW,NCOL,NROW,NLAY,IOUT,5,IBOUND, SEN1379
2              NPER,KPER,XX(IP),ISN,RHS,ISTRM,DD(IP),IHESS,B(IP),LN(IP), SEN1380
3              SCL(IP),NLL11,NLLIT)                                     SEN1381
              IF(PIDTMP.EQ.'KRB ') CALL SSEN1D(PIDTMP,NLL(1,IP),NRIVER,MXRIVR, SEN1382
1              RIVR,CELS,NSN,NS,SHNW,HNEW,NCOL,NROW,NLAY,IOUT,6,IBOUND, SEN1383
2              NPER,KPER,XX(IP),ISN,RHS,ISTRM,DD(IP),IHESS,B(IP),LN(IP), SEN1384
3              SCL(IP),NLL11,NLLIT)                                     SEN1385
              IF(PIDTMP.EQ.'KST ') CALL SSEN1D(PIDTMP,NLL(1,IP),NSTREM,MXSTRM, SEN1386
1              STRM,CELS,NSN,NS,SHNW,HNEW,NCOL,NROW,NLAY,IOUT,11,IBOUND, SEN1387
2              NPER,KPER,XX(IP),ISN,RHS,ISTRM,DD(IP),IHESS,B(IP),LN(IP), SEN1388
3              SCL(IP),NLL11,NLLIT)                                     SEN1389
              IF(PIDTMP.EQ.'Q ') CALL SSEN1D(PIDTMP,NLL(1,IP),NWELLS,MXWELL, SEN1390
1              WELL,CELS,NSN,NS,SHNW,HNEW,NCOL,NROW,NLAY,IOUT,4,IBOUND, SEN1391
2              NPER,KPER,XX(IP),ISN,RHS,ISTRM,DD(IP),IHESS,B(IP),LN(IP), SEN1392
3              SCL(IP),NLL11,NLLIT)                                     SEN1393
              IF(PIDTMP.EQ.'T ' .OR. PIDTMP.EQ.'KV ' .OR. PIDTMP.EQ.'ANI ' SEN1394
1              .OR. PIDTMP.EQ.'ANIV' .OR. PIDTMP.EQ.'TKV '           SEN1395
2              .OR. (KPER.GT.1.AND.PIDTMP.EQ.'S1 '))                 SEN1396
              CALL SSEN1P(SMAT,NLL(1,IP),NSM,NM,SHNW,HOLD,HNEW,NCOL, SEN1397
3              NROW,NLAY,KPER,NPER,PIDTMP,ST,DELR,DELC,IBOUND,TRPY, SEN1398
4              DELT,XX(IP),ISN,RHS,SHOLD,BOT,DD(IP),IHESS,B(IP), SEN1399
5              LN(IP),SCL(IP),NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,NLL11,CV) SEN1400
              IF(PIDTMP.EQ.'RCH ') CALL SSEN1R(NLL(1,IP),KPER,NPER,NCOL, SEN1401
1              NROW,NLAY,DELR,DELC,SMAT,NSM,NM,IOUT,XX(IP),NRCHOP,IRCH, SEN1402
2              HNEW,IBOUND,ISN,RHS,SURF,EXDP,PIDTMP,SHNW,DD(IP),IHESS, SEN1403
3              SCL(IP),NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,NLL11,NLLIT)     SEN1404
              IF(PIDTMP.EQ.'ETM ') CALL SSEN1R(NLL(1,IP),KPER,NPER,NCOL, SEN1405
1              NROW,NLAY,DELR,DELC,SMAT,NSM,NM,IOUT,XX(IP),NEVTOP,IEVT, SEN1406
2              HNEW,IBOUND,ISN,RHS,SURF,EXDP,PIDTMP,SHNW,DD(IP),IHESS, SEN1407
3              SCL(IP),NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,NLL11,NLLIT)     SEN1408
              IF(PIDTMP.EQ.'CH ') CALL SSEN1C(IP,NLL(1,IP),NCOL,NROW,NLAY, SEN1409
1              CR,CC,CV,IBOUND,XX,NP,CELS,NS,NSN,ISN,HNEW,IFLCH,DD, SEN1410
2              IHESS,RHS,H,HOBS,RINT,IOFF,JOFF,NDER,NH,KPER,NPER,TOFF, SEN1411
3              SCL(IP),NLL11)                                         SEN1412
          110 CONTINUE                                                SEN1413
          IP=IIP                                                       SEN1414
C-----TERMS FOR UNCONFINED AQUIFERS                               SEN1415
          IF(KITER.GT.1) THEN                                          SEN1416
              SEN1417
              SEN1418

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        KB=0
        KT=0
        DO 120 K=1,NLAY
            IF(LAYCON(K).EQ.1) THEN
                KB=KB+1
                CALL SSEN1N(SHNW,HOLD,HNEW,NCOL,NROW,NLAY,ST,DELR,DELC,
1                IBOUND,TRPY,RHS,SHOLD,BOT,CR,CC,K,ISN,KB,XX,NP)
            ENDIF
        120 CONTINUE
    ENDIF
C-----B MATRIX TIMES SOLUTION FROM LAST TIME STEP FOR SENSITIVITY-
C-----EQUATION SENSITIVITIES AND ITERATION-PARAMETER VECTOR
    IF(ISN.LT.0.OR.IHESS.GT.0) THEN
        IF(KPER.GT.1) THEN
            DO 140 K=1,NLAY
                DO 140 I=1,NROW
                    DO 140 J=1,NCOL
140                RHS(J,I,K)=RHS(J,I,K)-HOLD(J,I,K)*SC1(J,I,K)/DELT
            ENDIF
        ENDIF
        RETURN
    END
END

C=====SEN1441
SUBROUTINE SEN1NZ(RHS,HNEW,NODES,ISA)
C-----VERSION 1000 01FEB1992
C *****
C CHECK FOR NONZERO VALUES IN HNEW OR RHS
C *****
C SPECIFICATIONS:
C -----
C DOUBLE PRECISION HNEW(NODES)
C DIMENSION RHS(NODES)
C -----
C
C ISA=0
C DO 100 I=1,NODES
C     IF(RHS(I).NE.0..OR.HNEW(I).NE.0.D0) THEN
C         ISA=1
C         RETURN
C     ENDIF
100 CONTINUE
RETURN
END
SEN1442
SEN1443
SEN1444
SEN1445
SEN1446
SEN1447
SEN1448
SEN1449
SEN1450
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SEN1459
SEN1460
SEN1461

C=====SEN1462
SUBROUTINE SEN1HZ(HNEW,KPER,NODES,NZER,IZER,RHS,ISA)
C-----VERSION 1000 01FEB1992
C *****
C SET ALL COMPONENTS OF HNEW AND RHS TO ZERO
C *****
C SPECIFICATIONS:
C -----
C DOUBLE PRECISION HNEW(NODES)
C DIMENSION IZER(NZER),RHS(NODES)
C -----
C
C ITS=KPER-1
C DO 50 I=1,NZER
C     IF(IZER(I).EQ.ITS) THEN
C         DO 70 J=1,NODES
C             RHS(J)=0.
70         HNEW(J)=0.D0
C         ISA=0
C         RETURN
C     ENDIF
50 CONTINUE
RETURN
END
SEN1463
SEN1464
SEN1465
SEN1466
SEN1467
SEN1468
SEN1469
SEN1470
SEN1471
SEN1472
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SEN1483
SEN1484

C=====SEN1485
SUBROUTINE SEN1FD(IFLD,NDER,NH,KPER,TOFF,NQ,NQOB,IQOB,NQT)
C-----VERSION 1000 01FEB1992
C *****
C ARE THERE ANY OBSERVATIONS AT THIS TIME STEP?
C *****
C SPECIFICATIONS:
C -----
C DIMENSION TOFF(NH+NQT),NDER(5,NH),NQOB(NQ),IQOB(NQT)
C -----
C
C
C
SEN1486
SEN1487
SEN1488
SEN1489
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SEN1493
SEN1494
SEN1495

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IFLD=0
ITS=KPER-1
DO 100 N=1,NH
  NTS=NDER(4,N)
  IF(NTS.EQ.ITS.OR.(NTS.EQ.ITS-1.AND.TOFF(N).GT.0.)) THEN
    IFLD=1
    RETURN
  ENDIF
100 CONTINUE
  NT1=1
  DO 200 IQ=1,NQ
    NT2=NT1+NQOB(IQ)-1
    DO 150 NT=NT1,NT2
      NTS=IQOB(NT)
      IF(NTS.EQ.ITS.OR.(NTS.EQ.ITS-1.AND.TOFF(NH+NT).GT.0.)) THEN
        IFLD=1
        RETURN
      ENDIF
150 CONTINUE
      NT1=NT2+1
200 CONTINUE
    RETURN
  END
END

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SEN1496  
SEN1497  
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SEN1500  
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C-----
SUBROUTINE SENLOT(
1  IUHEAD,IOUT,NROW,NCOL,NLAY,NP,ISN,NH,NDER,HNEW,PID,
2  DID,IP,KPER,BUFF,KSTP,PRTIM,TOTIM,X,DELR,DELC,
3  IBOUND,COFF,ROFF,H,WT,HOBS,IPRINT,IFO,ITERP,IPAR,
4  RINT,JOFF,IOFF,MLAY,PR,MOBS,NPER,B,LN,NQ,NQC,NQT,
5  NQOB,NQCL,IQOB,QCLS,IBT,MXBND,NBOUND,BNDS,MXRIVR,
6  NRIVER,RIVR,SHNW,LASTX,ISCALS,TOFF,MXDRN,NDRAIN,
7  DRAI,MXSTRM,NSTREM,STRM,ISTRM,MAXM,KPRINT,JDRI,IDRY,
8  NPR,WP,MPR,PRM,IWPG,B1,IOUB,RSQ,RSQP,RSQO,RSQOO,NPO,
9  SOSR,SOSR)
C-----VERSION 1000 01FEB1992
C *****
C WRITE HEADS ON FILE IUHEAD.
C INTERPOLATE AND SAVE HEADS AND SENSITIVITIES FOR OBSERVATIONS.
C PRINT DATA FOR OBSERVED HEAD POINTS AND FOR OBSERVED FLOWS.
C *****
C SPECIFICATIONS:
C -----
CHARACTER*4 PID(NP),DID(NH+NQT),TEXT
CHARACTER*8 MEAN,CVAR,CORR
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)
DIMENSION NDER(5,NH),BUFF(NCOL*NROW*NLAY),TEXT(4),X(NP,NH+NQT),
1  DELR(NCOL),DELC(NROW),IBOUND(NCOL,NROW,NLAY),COFF(NH),
1  ROFF(NH),H(NH+NQT),WT(NH+NQT),HOBS(NH+NQT),RINT(4,NH),
1  JOFF(NH),IOFF(NH),MLAY(MAXM,MOBS),PR(MAXM,MOBS),B(NPO),
1  RIVR(6,MXRIVR),BNDS(5,MXBND),IBT(2,NQ),NQOB(NQ),NQCL(NQ),
1  IQOB(NQT),QCLS(4,NQC),TOFF(NH+NQT),DRAI(5,MXDRN),
1  STRM(11,MXSTRM),ISTRM(5,MXSTRM),LN(NP),WP(NPO+MPR),
1  PRM(NPO+1,MPR),IWPG(NP),SHNW(NCOL,NROW,NLAY),B1(NPO)
COMMON /FLWCOM/LAYCON(80)
C
C DATA TEXT(1),TEXT(2),TEXT(3),TEXT(4) /' ',' ',' ',' '
1  'HEAD'/
C DATA MEAN,CVAR,CORR/' MEAN','COEF.VAR','CORRELAT'/
C -----
C
C
530 FORMAT(8G10.3)
539 FORMAT(' ')
542 FORMAT(4X,'MULTIPLE LAYERS AND PROPORTIONS :',5(I5,',',F5.2,3X))
545 FORMAT(' SENSITIVITIES',/,/, ' PARAMETER # :',3X,I6,9I10,/,
1  ,12(14X,3X,I6,9I10,/))
546 FORMAT(' SCALED SENSITIVITIES (SCALED BY B*(WT*.5))',
1  /,/, ' PARAMETER # :',3X,I6,9I10,/,12(14X,3X,I6,9I10,/))
547 FORMAT(' PARAMETER ID :',7X,A4,6X,A4,6X,A4,6X,A4,6X,A4,
1  6X,A4,6X,A4,6X,A4,6X,A4,/,12(15X,7X,A4,6X,A4,6X,A4,6X,A4,
1  6X,A4,6X,A4,6X,A4,6X,A4,6X,A4,6X,A4,/)
548 FORMAT(' OBS# & ID')
550 FORMAT(I5,2X,A4,6X,10G10.3,12(/,17X,10G10.3))
590 FORMAT(/,7X,'((SUM OF THE SQUARED VALUES)**.5)/ND'
1  ,13(/,17X,10E10.3))
605 FORMAT(/, ' PARAMETER ESTIMATION CONVERGED BECAUSE SUM OF',
1  ' SQUARED, WEIGHTED RESIDUALS HAS NOT CHANGED',F7.4,
1  ' PERCENT IN 2 ITERATIONS',/)
610 FORMAT(/, ' ADD R MATRIX OF EQUATION (51) TO EQUATION',
1  ' (50) OF TEXT FOR ALL SUBSEQUENT ITERATIONS BECAUSE THE ',/,
2  'SUM OF SQUARED, WEIGHTED RESIDUALS HAS NOT CHANGED MORE THAN',
3  F7.4,' PERCENT IN 2 ITERATIONS')

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SEN1576

C		SEN1577
C-----	WRITE HEADS ON SCRATCH FILE OPENED IN SEN1FM	SEN1578
	IF (IP.EQ.0.AND.(ISN.EQ.-2.OR.ISN.GT.0)) THEN	SEN1579
	IUNIT=IUHEAD+KPER-1	SEN1580
	NRC=NROW*NCOL	SEN1581
	DO 10 K=1,NLAY	SEN1582
	CALL USAVEF(DUM,BUFF,HNEW(1,1,K),DUM,NROW*NCOL,3)	SEN1583
	CALL ULASAV(BUFF,TEXT,KSTP,KPER,PERTIM,TOTIM,NCOL,NROW,K,	SEN1584
1	IUNIT)	SEN1585
10	CONTINUE	SEN1586
	REWIND(IUNIT)	SEN1587
C-----	PUT HEADS FROM FINAL TIME STEP IN SHNW	SEN1588
	IF (ISN.GT.0.AND.KPER.EQ.NPER)	SEN1589
1	CALL USAVEF(DUM,SHNW,HNEW,DUM,NROW*NCOL*NLAY,3)	SEN1590
	ENDIF	SEN1591
C-----	WRITE INITIAL PARAMETER VALUES ON FILE IOUB	SEN1592
	IF (ITERP.EQ.1.AND.IP.EQ.0.AND.KPER.EQ.1.AND.IOUB.GT.0)	SEN1593
1	WRITE(IOUB,530) (B(I),I=1,NP)	SEN1594
C-----	INTERPOLATE TO HEAD LOCATIONS	SEN1595
	IF (NH.GT.0) CALL SSENLU(NH,NDER,IOFF,JOFF,KPER,MLAY,IBOUND,RINT,	SEN1596
1	DID,COFF,ROFF,DELR,DELC,NCOL,NROW,NLAY,PR,H,HOBS,WT,HNEW,	SEN1597
1	X,IP,IDRY,NP,MOBS,B,LN,ISN,NQT,TOFF,NPER,RHS,PV,	SEN1598
1	MAXM,ITERP,JDRY,IPAR,IOUT)	SEN1599
C		SEN1600
	IF (NQ.GT.0) THEN	SEN1601
C-----	INITIALIZE CALCULATED FLOW AND SENSITIVITY ARRAYS.	SEN1602
	ITS=KPER-1	SEN1603
	IF (IP.EQ.0.AND.ITS.EQ.0) THEN	SEN1604
	DO 30 NT=1,NQT	SEN1605
30	H(NH+NT)=0.	SEN1606
	ENDIF	SEN1607
	IF (IP.EQ.1.AND.ITS.EQ.0) THEN	SEN1608
	DO 40 NT=1,NQT	SEN1609
	DO 40 IIP=1,NP	SEN1610
40	X(IIP,NH+NT)=0.	SEN1611
	ENDIF	SEN1612
C-----	CALCULATE FLOWS AND SENSITIVITIES FOR FLOW BOUNDARIES	SEN1613
	CALL SSEN1V(NQ,NQC,NQT,NQOB,NQCL,IQOB,QCLS,IBT,MXBND,	SEN1614
1	NBOUND,BNDS,MXRIVR,NRIVER,RIVR,SHNW,IP,HNEW,NCOL,	SEN1615
1	NROW,NLAY,IOUT,IBOUND,NPER,KPER,NH,X,DID,NP,H,	SEN1616
1	B,LN,TOFF,MXDRN,NDRAIN,DRAI,MXSTRM,NSTREM,STRM,ISTRM,ISN,	SEN1617
1	RHS,WT,HOBS)	SEN1618
	ENDIF	SEN1619
C		SEN1620
C-----	CALCULATE THE SUM OF SQUARED RESIDUALS AND PRINT RESIDUALS FOR	SEN1621
C-----	OBSERVATIONS AND PRIOR INFORMATION	SEN1622
C-----	SET FLAG WHICH CONTROLS PRINTING OF RESIDUALS	SEN1623
	IO=0	SEN1624
	IF (KPER.EQ.NPER.AND.(IPAR.LT.0.OR.	SEN1625
1	(IP.EQ.0.AND.(IPRINT.NE.0.OR.ITERP.EQ.1.OR.IFO.NE.0)))	SEN1626
1	IO=1	SEN1627
	IF (KPER.EQ.NPER.AND.IP.EQ.0) THEN	SEN1628
	CALL SSEN1O(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBS,WT,DID,NDER,	SEN1629
2	ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,	SEN1630
3	RSQ,RSQP,IO,LN,RSQH,NPO)	SEN1631
	IF (IOUB.GT.0) WRITE(IOUB,530) RSQH,RSQ,RSQP	SEN1632
	ENDIF	SEN1633
C-----	TEST FOR REDUCTION IN SUM OF SQUARED, WEIGHTED RESIDUALS	SEN1634
	IF (IPAR.GT.0.AND.IP.EQ.NP.AND.KPER.EQ.NPER.AND.ISN.LT.0.AND.	SEN1635
1	(SOSC.GT.0..OR.SOSR.GT.0.)) THEN	SEN1636
	IF (ITERP.GT.2) THEN	SEN1637
	TEMP=(ABS(RSQP-RSQO)/RSQP)+(ABS(RSQO-RSQOO)/RSQO)	SEN1638
	IF (IFO.EQ.0.AND.TEMP.LT.SOSC) THEN	SEN1639
	IFO=2	SEN1640
	WRITE(IOUT,605) SOSC*100.	SEN1641
	IF (IO.EQ.0) CALL SSEN1O(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBS,	SEN1642
1	WT,DID,NDER,ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,	SEN1643
3	PRM,RSQ,RSQP,1,LN,RSQH,NPO)	SEN1644
	ENDIF	SEN1645
	IF (IFO.EQ.0.AND.TEMP.LT.SOSR) THEN	SEN1646
	WRITE(IOUT,610) SOSR*100.	SEN1647
	SOSR=-SOSR	SEN1648
	ENDIF	SEN1649
	ENDIF	SEN1650
	IF (ITERP.GE.2) RSQOO=RSQO	SEN1651
	IF (ITERP.GE.1) RSQO=RSQP	SEN1652
	ENDIF	SEN1653
C-----	IF REQUESTED, PRINT UNSCALED OR SCALED SENSITIVITIES	SEN1654
	ND=NH+NQT	SEN1655
	IF (KPER.EQ.NPER.AND.	SEN1656
1	((IP.EQ.NP.AND.(IPRINT.NE.0.OR.ITERP.EQ.1.OR.IFO.NE.0)).OR.	SEN1657
1	(IP.EQ.0.AND.IFO.NE.0.AND.LASTX.EQ.0))) THEN	SEN1658
	WRITE(IOUT,539)	SEN1659

IF(ISCALS.EQ.0.AND.KPRINT.LE.1)WRITE(IOUT,545)(IIP,IIP=1,NP)	SEN1660
IF(ISCALS.GT.0.OR.KPRINT.GT.1)WRITE(IOUT,546)(IIP,IIP=1,NP)	SEN1661
WRITE(IOUT,547) (PID(IIP),IIP=1,NP)	SEN1662
WRITE(IOUT,548)	SEN1663
IF(ISCALS.EQ.0.AND.KPRINT.LE.1) THEN	SEN1664
DO 95 N=1,ND	SEN1665
WRITE(IOUT,550) N,DID(N),(X(IIP,N),IIP=1,NP)	SEN1666
95 CONTINUE	SEN1667
ELSE	SEN1668
DO 98 IIP=1,NP	SEN1669
98 BUFF(NP+IIP)=0.	SEN1670
DO 110 N=1,ND	SEN1671
DO 100 IIP=1,NP	SEN1672
IF(WT(N).LT.0.) THEN	SEN1673
BUFF(IIP)=0.	SEN1674
GO TO 100	SEN1675
ENDIF	SEN1676
BB=B(IIP)	SEN1677
IF(LN(IIP).GT.0) BB=ALOG(BB)	SEN1678
IF(ABS(BB).LT.1.E-25) BB=1.0	SEN1679
BUFF(IIP)=BB*X(IIP,N)*(WT(N)**.5)	SEN1680
BUFF(NP+IIP)=BUFF(NP+IIP)+(BUFF(IIP)*BUFF(IIP))	SEN1681
100 CONTINUE	SEN1682
WRITE(IOUT,550) N,DID(N),(BUFF(IIP),IIP=1,NP)	SEN1683
110 CONTINUE	SEN1684
DO 112 IIP=1,NP	SEN1685
112 BUFF(NP+IIP)=(BUFF(NP+IIP)**.5)/ND	SEN1686
WRITE(IOUT,590) (BUFF(NP+IIP),IIP=1,NP)	SEN1687
ENDIF	SEN1688
ENDIF	SEN1689
C RETURN	SEN1690
END	SEN1691
	SEN1692

#### New SEN Submodules

Listed in alphabetical order

SUBROUTINE SSENIA(	SSA0001
1 PID,LM,LZ,NLL,SMAT,MATZ,BUFF,NCOL,NROW,NLAY,	SSA0002
2 NSM,NP,NMM,NZM,LZ11,NLL11,NLL1T,NPER,IOUT,IERR,NUMR)	SSA0003
C-----VERSION 1000 01FEB1992	SSA0004
C *****	SSA0005
C CHECK FOR MULTIPLE USE OF A SINGLE CELL IN PARAMETER DEFINITIONS.	SSA0006
C *****	SSA0007
C SPECIFICATIONS:	SSA0008
C -----	SSA0009
CHARACTER*4 PID(NP),PID1,PID2,PIDTMP,TEXT(4)	SSA0010
DIMENSION BUFF(NCOL,NROW,NLAY),LM(NSM),LZ(LZ11,NSM),	SSA0011
1 SMAT(NCOL,NROW,NMM),MATZ(NCOL,NROW,NZM),NLL(NLL11,NP)	SSA0012
C -----	SSA0013
500 FORMAT(' AT LEAST ONE GRID CELL IS USED MORE THAN NUMR TIMES IN',	SSA0014
1 ' DEFINING THE FOLLOWING MODEL INPUTS -- STOP EXECUTION',/,	SSA0015
2 ' THE NUMBERS EQUAL THE NUMBER OF TIMES THE CELL IS REPEATED')	SSA0016
C	SSA0017
C-----INITIALIZE VARIABLES	SSA0018
TEXT(1)=' INP'	SSA0019
TEXT(2)='UT T'	SSA0020
TEXT(3)='YPE '	SSA0021
ITS=KPER-1	SSA0022
C-----MODEL INPUT TYPE LOOP	SSA0023
DO 350 II=1,5	SSA0024
KP2=1	SSA0025
IF(II.GE.4) KP2=NPER	SSA0026
DO 300 KPER=1,KP2	SSA0027
IFLAG=0	SSA0028
DO 5 NL=1,NLAY	SSA0029
DO 5 I=1,NROW	SSA0030
DO 5 J=1,NCOL	SSA0031
5 BUFF(J,I,NL)=0.	SSA0032
IF(II.EQ.1) THEN	SSA0033
PID1='T'	SSA0034
PID2='TKV'	SSA0035
GO TO 50	SSA0036
ELSEIF(II.EQ.2) THEN	SSA0037
PID1='KV'	SSA0038
PID2='TKV'	SSA0039
GO TO 50	SSA0040
ELSEIF(II.EQ.3) THEN	SSA0041
PID1='S1'	SSA0042
PID2=PID1	SSA0043



	GO TO 50	SSA0044
	ELSEIF(II.EQ.4) THEN	SSA0045
	PID1='RCH '	SSA0046
	PID2=PID1	SSA0047
	GO TO 50	SSA0048
	ELSEIF(II.EQ.5) THEN	SSA0049
	PID1='ETM '	SSA0050
	PID2=PID1	SSA0051
	GO TO 50	SSA0052
	ENDIF	SSA0053
C-----	LOOP THROUGH PARAMETERS	SSA0054
50	NM=0	SSA0055
	DO 200 IP=1,NP	SSA0056
	PIDTMP=PID(IP)	SSA0057
	IF(PIDTMP.NE.'T ' .AND.PIDTMP.NE.'TKV ' .AND.PIDTMP.NE.	SSA0058
1	'KV ' .AND.PIDTMP.NE.'S1 ' .AND.PIDTMP.NE.'RCH ' .AND.	SSA0059
2	PIDTMP.NE.'ETM ') GO TO 200	SSA0060
	NL2=NLLI1	SSA0061
	NT=1	SSA0062
	IF(PIDTMP.EQ.'RCH ' .OR.PIDTMP.EQ.'ETM ') THEN	SSA0063
	NL2=1	SSA0064
	NT=NLLIT	SSA0065
	ENDIF	SSA0066
C-----	LOOP THROUGH LAYER NUMBERS	SSA0067
	DO 90 LL=1,NL2	SSA0068
	NLO=NLL(LL,IP)	SSA0069
	IF(NLO.GT.0) NM=NM+1	SSA0070
C-----	MATCH?	SSA0071
	IF(PIDTMP.NE.PID1.AND.PIDTMP.NE.PID2) GO TO 90	SSA0072
C-----	IN SOME CASES JUST KEEP TRACK OF NM	SSA0073
	IF(PIDTMP.EQ.'TKV ' .AND.((II.EQ.1.AND.MOD(LL+1,3).NE.0)	SSA0074
1	.OR.(II.EQ.2.AND.MOD(LL+1,3).EQ.0))) GO TO 90	SSA0075
	IF(PIDTMP.NE.'RCH ' .AND.PIDTMP.NE.'ETM ') THEN	SSA0076
	IF(KPER.GT.1) GO TO 90	SSA0077
	IF(NLO.EQ.0.AND.PIDTMP.EQ.'TKV ') GO TO 90	SSA0078
	IF(NLO.EQ.0) GO TO 200	SSA0079
	ENDIF	SSA0080
	IFLAG=1	SSA0081
C-----	INITIALIZE NL	SSA0082
	NL=IABS(NLO)	SSA0083
	IF(PIDTMP.EQ.'RCH ' .OR.PIDTMP.EQ.'ETM ') NL=1	SSA0084
C-----	LOOP THROUGH TIMES FOR RCH AND ETM; NT=1 FOR OTHER PID'S	SSA0085
	DO 85 K=1,NT	SSA0086
	IF((PIDTMP.EQ.'RCH ' .OR.PIDTMP.EQ.'ETM ').AND.	SSA0087
1	(ITS.LT.NLL(2*K,IP).OR.ITS.GT.NLL(2*K+1,IP))) GO TO 85	SSA0088
	IF(NLO.LT.0)GO TO 20	SSA0089
	M=LM(NM)	SSA0090
	LZ1=LZ(1,NM)	SSA0091
	LZN=2	SSA0092
	IF(LZ1.NE.0) LZN=LZI1	SSA0093
	DO 15 IZ=2,LZN	SSA0094
	IF(LZ1.NE.0)THEN	SSA0095
	NZ=LZ(IZ,NM)	SSA0096
	IF(NZ.EQ.0) GO TO 20	SSA0097
	ENDIF	SSA0098
	DO 10 I=1,NROW	SSA0099
	DO 10 J=1,NCOL	SSA0100
	ICO=0	SSA0101
	IF(LZ1.EQ.0) THEN	SSA0102
	IF(M.EQ.0) ICO=1	SSA0103
	IF(M.NE.0.AND.SMAT(J,I,M).NE.0.)	SSA0104
1	ICO=1	SSA0105
	ELSE	SSA0106
	IF(MATZ(J,I,LZ1).EQ.NZ) THEN	SSA0107
	IF(M.EQ.0) ICO=1	SSA0108
	IF(M.NE.0.AND.SMAT(J,I,M).NE.0.)	SSA0109
1	ICO=1	SSA0110
	ENDIF	SSA0111
	ENDIF	SSA0112
	IF(ICO.NE.0) THEN	SSA0113
	KK=NL	SSA0114
	IF(PIDTMP.EQ.'TKV ' .AND.MOD(LL+2,3).EQ.0) KK=NL-1	SSA0115
	BUFF(J,I,KK)=BUFF(J,I,KK)+1.	SSA0116
	ENDIF	SSA0117
10	CONTINUE	SSA0118
15	CONTINUE	SSA0119
20	CONTINUE	SSA0120
	IF(NLO.LT.0) THEN	SSA0121
	DO 80 I=1,NROW	SSA0122
	DO 80 J=1,NCOL	SSA0123
	KK=NL	SSA0124
	IF(PIDTMP.EQ.'TKV ' .AND.MOD(LL+2,3).EQ.0) KK=NL-1	SSA0125
	BUFF(J,I,KK)=BUFF(J,I,KK)+1	SSA0126

80	CONTINUE	SSA0127
	ENDIF	SSA0128
85	CONTINUE	SSA0129
90	CONTINUE	SSA0130
200	CONTINUE	SSA0131
	IF(IFLAG.EQ.0) GO TO 350	SSA0132
	NL2=NLAY	SSA0133
	IF(II.EQ.2) NL2=NLAY-1	SSA0134
	IF(II.EQ.4.OR.II.EQ.5) NL2=1	SSA0135
	DO 260 NL=1,NL2	SSA0136
	DO 240 I=1,NROW	SSA0137
	DO 240 J=1,NCOL	SSA0138
240	IF(BUFF(J,I,NL).GT.REAL(NUMR)) GO TO 250	SSA0139
	GO TO 260	SSA0140
250	TEXT(4)=PID1	SSA0141
	IERR=1	SSA0142
	WRITE(IOUT,500)	SSA0143
	CALL ULAPRS(BUFF(1,1,NL),TEXT,ITS,0,NCOL,NROW,NL,8,IOUT)	SSA0144
260	CONTINUE	SSA0145
300	CONTINUE	SSA0146
350	CONTINUE	SSA0147
	RETURN	SSA0148
	END	SSA0149
C=====SSA0150		
	SUBROUTINE SSEN1B(	SSA0151
1	NLL,NCOL,NROW,CELS,NS,NSN,DELR,DELC,IOUT,IERR,NLLI1)	SSA0152
C----	VERSION 1000 01FEB1992	SSA0153
C	*****	SSA0154
C	CALCULATE COEFFICIENTS FOR CONSTANT-HEAD BOUNDARIES.	SSA0155
C	ONLY INTERPOLATE BACKWARDS FROM EACH ENDPOINT.	SSA0156
C	*****	SSA0157
C	SPECIFICATIONS:	SSA0158
C	-----	SSA0159
	DIMENSION CELS(4,NSN),NLL(NLLI1),DELR(NCOL),DELC(NROW)	SSA0160
C	-----	SSA0161
580	FORMAT(/,' LINEAR INTERPOLATION FOR CONSTANT HEADS REQUESTED '	SSA0162
1	'ALONG A DIAGONAL OR AROUND A CORNER -- STOP EXECUTION ',	SSA0163
2	'(SSEN1B)',/)	SSA0164
C		SSA0165
	NLI=NLL(1)	SSA0166
	IICH=0	SSA0167
	N1=NS-NLI+1	SSA0168
	DO 10 I=N1,NS	SSA0169
10	CELS(4,I)=0.	SSA0170
C-----	FIND THE NEXT PARAMETER OR KNOWN HEAD LOCATION.	SSA0171
22	NN2=NLI-IICH	SSA0172
	DO 25 NN=1,NN2	SSA0173
	N=N1-1+IICH+NN	SSA0174
	CE=CELS(3,N)	SSA0175
	IF(CE.NE.0.) THEN	SSA0176
	CELS(4,N)=CE	SSA0177
	IICH=IICH+NN	SSA0178
	GO TO 26	SSA0179
	ENDIF	SSA0180
25	CONTINUE	SSA0181
26	CONTINUE	SSA0182
C-----	COUNT HOW FAR BACK TO INTERPOLATE	SSA0183
	N0=0	SSA0184
	IF(IICH.GT.2.AND.CELS(3,N1-1+IICH-1).EQ.0.) THEN	SSA0185
	I1=IICH-1	SSA0186
	DO 40 I=I1,1,-1	SSA0187
	IF(CELS(3,N1-1+I).NE.0.) GO TO 41	SSA0188
40	CONTINUE	SSA0189
41	CONTINUE	SSA0190
	N0=IABS(I-IICH)-1	SSA0191
	IF(N0.EQ.1) GO TO 60	SSA0192
C-----	CALCULATE TOTAL INTERPOLATION DISTANCE	SSA0193
	TX=0.	SSA0194
	TY=0.	SSA0195
	DO 45 NN=1,N0+2	SSA0196
	N=N1-1+IICH-(NN-1)	SSA0197
	FAC=1.0	SSA0198
	IF(NN.EQ.1.OR.NN.EQ.N0+2) FAC=0.5	SSA0199
	IC=INT(CELS(1,N))	SSA0200
	JC=INT(CELS(2,N))	SSA0201
C-----	ALONG A ROW	SSA0202
	IF(N.LT.NS.AND.IC.EQ.INT(CELS(1,N+1)))	SSA0203
1	TX=TX+FAC*DELR(JC)	SSA0204
	IF(N.EQ.NS.AND.INT(CELS(1,N-1)).EQ.IC)	SSA0205
1	TX=TX+FAC*DELR(JC)	SSA0206
C-----	ALONG A COLUMN	SSA0207

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1          IF(N.LT.NS.AND.JC.EQ.INT(CELS(2,N+1)))          SSA0208
1          TY=TY+FAC*DELC(IC)                                SSA0209
1          IF(N.EQ.NS.AND.INT(CELS(2,N-1)).EQ.JC)          SSA0210
45         TY=TY+FAC*DELC(IC)                                SSA0211
1          CONTINUE                                          SSA0212
1          IF(TX.GT.0..AND.TY.GT.0.) THEN                    SSA0213
45         WRITE(IOUT,580)                                    SSA0214
1          IERR=1                                             SSA0215
1          ENDIF                                             SSA0216
C-----CALCULATE PARTIAL DISTANCES AND COEFFICIENTS        SSA0217
1          DX=0.                                              SSA0218
1          DY=0.                                              SSA0219
1          DO 50 NN=1,N0                                     SSA0220
1          N=NL-1+IICH-NN                                     SSA0221
C-----ALONG ROWS                                           SSA0222
1          IF(TX.GT.0.) THEN                                  SSA0223
1          DX = DX + 0.5*(DELR(INT(CELS(2,N+1)))             SSA0224
1          +DELR(INT(CELS(2,N))))                             SSA0225
1          CELS(4,N)=1.-DX/TX                                 SSA0226
1          ENDIF                                             SSA0227
C-----ALONG COLUMNS                                       SSA0228
1          IF(TY.GT.0) THEN                                    SSA0229
1          DY = DY + .5*(DELC(INT(CELS(1,N+1)))              SSA0230
1          +DELC(INT(CELS(1,N))))                             SSA0231
1          CELS(4,N)=1.-DY/TY                                 SSA0232
1          ENDIF                                             SSA0233
50         CONTINUE                                          SSA0234
1          ENDIF                                             SSA0235
C-----IS THE NEXT PARAMETER THE SAME?                      SSA0236
60        NNN2=NL1-IICH                                     SSA0237
1          DO 72 NNN=1,NNN2                                   SSA0238
1          N=NL-1+IICH+NNN                                   SSA0239
1          CE=CELS(3,N)                                       SSA0240
1          CEN=CELS(3,N1-1+IICH)                             SSA0241
1          IF(CE.GT.1..AND.CEN.GT.1.) THEN                   SSA0242
1          IF(CE.EQ.CEN) THEN                                  SSA0243
1          DO 70 NNNN=1,NNN                                   SSA0244
1          CELS(4,N1-1+IICH+NNNN)=1.                         SSA0245
1          IICH=IICH+NNN                                       SSA0246
1          ENDIF                                             SSA0247
1          ENDIF                                             SSA0248
72        CONTINUE                                          SSA0249
1          IF(IICH.LT.NL1) GO TO 22                           SSA0250
1          RETURN                                             SSA0251
1          END                                                SSA0252

C=====SSA0253
SUBROUTINE SSenic(                                          SSA0254
1          IP,NLL,NCOL,NROW,NLAY,CR,CC,CV,IBOUND,XX,NP,      SSA0255
2          CELS,NS,NSN,ISN,HNEW,IFLCH,DD,IHESS,RHS,H,HOBS,   SSA0256
3          RINT,IOFF,JOFF,NDER,NH,KPER,NPER,TOFF,SCL,NLL1)   SSA0257
C-----VERSION 1000 01FEB1992                               SSA0258
C          *****SSA0259
C          FOR CONSTANT HEAD NODES - CALCULATE ADJOINT SENSITIVITY, OR SET
C          VALUES IN HNEW FOR THE SENSITIVITY EQUATIONS OR ITERATION SSA0261
C          PARAMETER VECTOR                                  SSA0262
C          *****SSA0263
C          SPECIFICATIONS:                                    SSA0264
C          -----SSA0265
C          DOUBLE PRECISION HNEW(NCOL,NROW,NLAY),DD(NP),XX(NP) SSA0266
C          DIMENSION CR(NCOL*NROW*NLAY),CC(NCOL*NROW*NLAY),CELS(4,NSN), SSA0267
1          CV(NCOL*NROW*NLAY),IBOUND(NCOL,NROW,NLAY),NLL(NLL1), SSA0268
2          RHS(NCOL,NROW,NLAY),H(NH),HOBS(NH),RINT(4,NH),IOFF(NH), SSA0269
3          JOFF(NH),NDER(5,NH),TOFF(NH)                     SSA0270
C          -----SSA0271
C          ITS=KPER-1                                         SSA0272
C          IF(ISN.GT.0.AND.IHESS.EQ.0) ITS=NPER-KPER         SSA0273
C          NL1=NLL(1)                                         SSA0274
C          NL2=NLL(2)                                         SSA0275
C          NL3=NLL(3)                                         SSA0276
C          IF(IFLCH.EQ.0) NS=NS+NL1                           SSA0277
C          IFLCH=IFLCH+1                                       SSA0278
C          IF((NL3.EQ.0.AND.ITS.NE.0).OR.(NL3.EQ.1.AND.ITS.EQ.0)) GO TO 150 SSA0280
C          NL=NS-NL1+1                                         SSA0281
C-----FIND PARAMETER AND THE PRECEDING SECTION OF THE BOUNDARY. SSA0282
C          II=0                                                SSA0283
C          I=0                                                 SSA0284
C          DO 30 INCH=NL,NS                                    SSA0285
C          CE=CELS(4,INCH)                                     SSA0286
C          IF(II.EQ.IFLCH-1.AND.INCH.GT.NL) THEN              SSA0287
C          CEM1=CELS(4,INCH-1)                                SSA0288

```

IF((CE.GT.0..AND.CE.LT.1.).AND.	SSA0289
1 (CEM1.LT.0..OR.CEM1.GE.1.)) I=INCH	SSA0290
IF(CE.GT.1.) GO TO 32	SSA0291
ENDIF	SSA0292
IF(CE.GT.1.) II=II+1	SSA0293
IF(INCH.EQ.N1.AND.II.EQ.IPLCH) GO TO 32	SSA0294
30 CONTINUE	SSA0295
32 CONTINUE	SSA0296
IF(I.EQ.0) I=INCH	SSA0297
IEND=INCH	SSA0298
C-----DOES THE PARAMETER EQUAL THE HEAD AT SUBSEQUENT CELLS OR IS THIS	SSA0299
C-----PARAMETER USED TO INTERPOLATE FURTHER?	SSA0300
IF=0	SSA0301
IF(IEND.LT.NS) THEN	SSA0302
II=IEND+1	SSA0303
DO 40 INCH=II,NS	SSA0304
CE=CELS(4,INCH)	SSA0305
IF(CE.GT.1..OR.CE.LT.0.) THEN	SSA0306
IEND=INCH-1	SSA0307
GO TO 42	SSA0308
ENDIF	SSA0309
IF(CE.NE.1..AND.IF.EQ.0) IF=INCH	SSA0310
40 CONTINUE	SSA0311
42 CONTINUE	SSA0312
ENDIF	SSA0313
IF(IF.EQ.0) IF=NS+1	SSA0314
C-----LOOP THROUGH THIS SECTION OF BOUNDARY	SSA0315
DO 100 INCH=I,IEND	SSA0316
FAC=CELS(4,INCH)	SSA0317
IF(FAC.GT.1) FAC=1.	SSA0318
IF(INCH.GE.IF) FAC=1.-FAC	SSA0319
II=CELS(1,INCH)	SSA0320
JJ=CELS(2,INCH)	SSA0321
C-----LOOP THROUGH LAYERS	SSA0322
DO 50 NL=4,NLL11	SSA0323
KK=NLL(NL)	SSA0324
IF(KK.EQ.0) GO TO 100	SSA0325
IND=JJ+NCOL*(II-1)+NRC*(KK-1)	SSA0326
C-----ADJOINT-STATE SENSITIVITIES	SSA0327
IF(ISN.GT.0.AND.IHESS.EQ.0) THEN	SSA0328
C-----CV	SSA0329
IF(KK.GT.1.AND.IBOUND(JJ,II,KK-1).GT.0)	SSA0330
# XX(IP)=XX(IP)+FAC*CV(IND-NRC)*HNEW(JJ,II,KK-1)	SSA0331
IF(KK.LT.NLAY.AND.IBOUND(JJ,II,KK+1).GT.0)	SSA0332
# XX(IP)=XX(IP)+FAC*CV(IND)*HNEW(JJ,II,KK+1)	SSA0333
C-----CC	SSA0334
IF(II.GT.1.AND.IBOUND(JJ,II-1,KK).GT.0)	SSA0335
# XX(IP)=XX(IP)+FAC*CC(IND-NCOL)*HNEW(JJ,II-1,KK)	SSA0336
IF(II.LT.NROW.AND.IBOUND(JJ,II+1,KK).GT.0)	SSA0337
# XX(IP)=XX(IP)+FAC*CC(IND)*HNEW(JJ,II+1,KK)	SSA0338
C-----CR	SSA0339
IF(JJ.GT.1.AND.IBOUND(JJ-1,II,KK).GT.0)	SSA0340
# XX(IP)=XX(IP)+FAC*CR(IND-1)*HNEW(JJ-1,II,KK)	SSA0341
IF(JJ.LT.NCOL.AND.IBOUND(JJ+1,II,KK).GT.0)	SSA0342
# XX(IP)=XX(IP)+FAC*CR(IND)*HNEW(JJ+1,II,KK)	SSA0343
C-----DOES THIS CH DIRECTLY AFFECT A HEAD OBSERVATION?	SSA0344
DO 46 N=1,NH	SSA0345
IF(KK.EQ.NDER(1,N).AND.(NDER(4,N).EQ.ITS.OR.	SSA0346
1 (NDER(4,N)-1.EQ.ITS.AND.TOFF(N).GT.0.0))) THEN	SSA0347
FACT=1.0	SSA0348
IF(TOFF(N).GT.0.0) THEN	SSA0349
IF(NDER(4,N).EQ.ITS) FACT=TOFF(N)	SSA0350
IF(NDER(4,N)-1.EQ.ITS) FACT=1.-TOFF(N)	SSA0351
ENDIF	SSA0352
IH=NDER(2,N)	SSA0353
JH=NDER(3,N)	SSA0354
IO=IOFF(N)	SSA0355
JO=JOFF(N)	SSA0356
FACH=0.	SSA0357
IF(II.EQ.IH.AND.JJ.EQ.JH) FACH=RINT(1,N)	SSA0358
IF(II.EQ.IH.AND.JJ.EQ.JH+JO) FACH=FACH+RINT(2,N)	SSA0359
IF(II.EQ.IH+IO.AND.JJ.EQ.JH) FACH=FACH+RINT(3,N)	SSA0360
IF(II.EQ.IH+IO.AND.JJ.EQ.JH+JO) FACH=FACH+RINT(4,N)	SSA0361
IF(FACH.EQ.0.) GO TO 46	SSA0362
XX(IP)=XX(IP)+2.*(H(N)-HOBS(N))*FAC*FACH*FACT	SSA0363
ENDIF	SSA0364
46 CONTINUE	SSA0365
ENDIF	SSA0366
C	SSA0367
C-----FOR SENSITIVITY-EQUATION SENSITIVITIES	SSA0368
IF(ISN.LT.0) HNEW(JJ,II,KK)=FAC	SSA0369
C-----FOR ITERATION PARAMETER VECTOR	SSA0370
IF(ISN.GT.0.AND.IHESS.NE.0) THEN	SSA0371

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        IF(IFLCH.EQ.1) HNEW(JJ,II,KK)=0.
        HNEW(JJ,II,KK)=HNEW(JJ,II,KK)+FAC*DD(IP)*SCL
    ENDIF
50    CONTINUE
100   CONTINUE
C
C-----IS THIS THE LAST PARAMETER OF THIS CH IDENTIFIER?
150   IF(IFLCH.EQ.NL2) IFLCH=0
    RETURN
    END
SSA0372
SSA0373
SSA0374
SSA0375
SSA0376
SSA0377
SSA0378
SSA0379
SSA0380
SSA0381

C=====SSA0382
SUBROUTINE SSENID(
1     PID,NLL,NNB,MXBN,BN,CELS,NSN,NS,SHNW,HNEW,NCOL,
2     NROW,NLAY,IOUT,ILBN,IBOUND,NPER,KPER,XX,ISN,
3     RHS,ISTRM,DD,IHESS,B,LN,SCL,NLLI1,NLLIT)
C-----VERSION 1000 01FEB1992
C *****SSA0388
C FOR PUMPING AND HEAD-DEPENDANT BOUNDARIES : CALCULATE MATRIX AND
C VECTOR DERIVATIVES, MULTIPLY BY HEADS AND ADJOINTS, AND ADD
C COMPONENTS TO THE SENSITIVITY OR RHS.
C *****SSA0392
C SPECIFICATIONS:
C -----SSA0394
CHARACTER*4 PID
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY),DD,XX,DF
DIMENSION BN(ILBN,MXBN),CELS(4,NSN),SHNW(NCOL,NROW,NLAY),
1     IBOUND(NCOL,NROW,NLAY),NLL(NLLI1),
1     RHS(NCOL,NROW,NLAY),ISTRM(5,MXBN)
C -----SSA0400
C
C-----CALCULATE TIME STEP
ITS=NPER-KPER
IF(ISN.LT.0.OR.IHESS.GT.0) ITS=KPER-1
NSI=NS
C-----LOOP THROUGH PARAMETER TIME DEFINITION
DO 250 KT=1,NLLIT
    IF(NLL(2*KT).LT.0) GO TO 255
    IF( ITS.GE.NLL(2*KT) .AND. ITS.LE.NLL(2*KT+1) ) THEN
        NLI=NLL(1)
        NLI1=IABS(NLI)
C-----LOOP THROUGH PARAMETER CELLS
DO 200 II=1,NLI1
    DF=0.
    NS=NS+1
    K=CELS(1,NS)
    I=CELS(2,NS)
    J=CELS(3,NS)
    IF(PID.NE.'KST '.AND.IBOUND(J,I,K).LE.0) GO TO 200
C-----LOOP THROUGH TO SEE IF THIS CELL IS BEING USED.
C-----IF SO, CALCULATE CONTRIBUTION TO SENSITIVITY.
DO 100 JJ=1,NNB
    IF(PID.NE.'KST ') THEN
        KB=BN(1,JJ)
        IB=BN(2,JJ)
        JB=BN(3,JJ)
    ELSE
        IS=ISTRM(4,JJ)
        IR=ISTRM(5,JJ)
    ENDIF
    IF((PID.NE.'KST '.AND.KB.EQ.K .AND. IB.EQ.I .AND. JB.EQ.J)
1     .OR.(PID.EQ.'KST '.AND.IS.EQ.K.AND.IR.EQ.I)) THEN
        IF(PID.EQ.'KST ') THEN
            IF(BN(10,JJ).LE.0.O.AND.BN(11,JJ).GE.0.0) GO TO 200
            K=ISTRM(1,JJ)
            I=ISTRM(2,JJ)
            J=ISTRM(3,JJ)
            IF(IBOUND(J,I,K).LE.0) GO TO 200
        ENDIF
        FACTOR=1.
        IF(NLI.GT.0) FACTOR=CELS(4,NS)
        IF(PID.EQ.'GHB ') DF=FACTOR*(BN(4,JJ)-SHNW(J,I,K))
        IF(PID.EQ.'Q ') DF=FACTOR
        IF(PID.EQ.'KRB '.OR.PID.EQ.'KST '.OR.PID.EQ.'KDR ')
1     THEN
            IN=4
            IF(PID.EQ.'KRB ') IN=6
            IF(SHNW(J,I,K).GT.BN(IN,JJ)) THEN
                IM=4
                IF(PID.EQ.'KST ') IM=2
                DF=FACTOR*(BN(IM,JJ)-SHNW(J,I,K))
            ELSE
SSA0383
SSA0384
SSA0385
SSA0386
SSA0387
SSA0388
SSA0389
SSA0390
SSA0391
SSA0392
SSA0393
SSA0394
SSA0395
SSA0396
SSA0397
SSA0398
SSA0399
SSA0400
SSA0401
SSA0402
SSA0403
SSA0404
SSA0405
SSA0406
SSA0407
SSA0408
SSA0409
SSA0410
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SSA0434
SSA0435
SSA0436
SSA0437
SSA0438
SSA0439
SSA0440
SSA0441
SSA0442
SSA0443
SSA0444
SSA0445
SSA0446
SSA0447
SSA0448
SSA0449
SSA0450
SSA0451
SSA0452

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          IF(PID.EQ.'KRB ') DF=FACTOR*(BN(4,JJ)-BN(6,JJ))
          IF(PID.EQ.'KST ') THEN
              IM=2
              IF(BN(10,JJ).LE.0.) IM=5
              DF=FACTOR*(BN(IM,JJ)-BN(4,JJ))
          ENDIF
        ENDIF
      ENDIF
C-----FOR ADJOINT SENSITIVITIES
      IF(ISN.GT.0.AND.IHESS.EQ.0)
        1      XX = XX + HNEW(J,I,K) * DF
C-----FOR ITERATION-PARAMETER VECTOR FOR CONJUGATE-DIRECTION OPT.
      IF(ISN.GT.0.AND.IHESS.GT.0) THEN
          BB=1.
          IF(LN.GT.0) BB=B/SCL
          RHS(J,I,K)=RHS(J,I,K)-DF*DD*BB*SCL
        ENDIF
C-----FOR SENSITIVITY-EQUATION SENSITIVITIES
      IF(ISN.LT.0) RHS(J,I,K) = RHS(J,I,K) - DF
      GO TO 200
    ENDIF
100    CONTINUE
200    CONTINUE
      ENDIF
250    CONTINUE
255    CONTINUE
C
      IF(NS.EQ.NS1) NS=NS+IABS(NLL(1))
      RETURN
      END
SSA0453
SSA0454
SSA0455
SSA0456
SSA0457
SSA0458
SSA0459
SSA0460
SSA0461
SSA0462
SSA0463
SSA0464
SSA0465
SSA0466
SSA0467
SSA0468
SSA0469
SSA0470
SSA0471
SSA0472
SSA0473
SSA0474
SSA0475
SSA0476
SSA0477
SSA0478
SSA0479
SSA0480
SSA0481
SSA0482

C=====SSA0483
      SUBROUTINE SSENIF (
        1      NCOL,NROW,NLAY,MXBND,MXRIVR,NPER,IU,IOUT,DID,NH,JT,
        2      IBOUND,NQ,NQC,NQT,IBT,NQOB,NQCL,IQOB,QCLS,IERR,PID,NP,NLL,
        3      CELS,NSN,WT,HOBS,TOFF,EVF,MXDRN,MXSTRM,ISN,NLLI1,NLLIT)
C-----VERSION 1000 01FEB1992
C *****
C READ, CHECK AND STORE DATA FOR HEAD-DEPENDENT FLOW BOUNDARIES.
C *****
C SPECIFICATIONS:
C -----
      CHARACTER*4  DID(NH+NQT),PID(NP),PIDTMP
      DIMENSION IBOUND(NCOL,NROW,NLAY),IBT(2,NQ),NQOB(NQ),NQCL(NQ),
        1      IQOB(NQT),QCLS(5,NQC),NLL(NLLI1,NP),CELS(4,NSN),WT(NH+NQT),
        1      HOBS(NH+NQT),TOFF(NH+NQT)
C -----
501    FORMAT(15X,2F5.0,F10.0)
503    FORMAT(8F10.0)
510    FORMAT(A4,1X,I5,F8.0,2F10.0,I5)
515    FORMAT(3I5)
517    FORMAT(/,' HEAD-DEPENDENT FLOW DATA')
518    FORMAT(/,' GROUP#',I3,' BOUNDARY TYPE',I3,
        1      ', # OF FLOWS',I5,', # OF CELLS IN GROUP',I5,/,
        1      40X,'OBSERVED STREAMFLOW',/,
        1      6X,'OBS# ID TIME STEP AND OFFSET',
        1      ' GAIN(-) OR LOSS(+) VARIANCE')
520    FORMAT(4X,I5,1X,A4,2X,I5,F10.2,12X,G10.3,3X,G14.3)
522    FORMAT(/,' LAYER ROW COLUMN FACTOR')
523    FORMAT(/,' SEGMENT REACH FACTOR')
525    FORMAT(4X,F8.0,F6.0,F7.0,F9.2)
530    FORMAT(4X,F8.0,F6.0,F9.2)
540    FORMAT(/,' STATISTIC RELATED TO WEIGHT < 0 -- STOP EXECUTION',
        1      '(SSENIF)',/)
560    FORMAT(/,' PACKAGE RELATED TO HEAD-DEPENDENT BOUNDARY DATA',
        1      ' IS NOT OPEN -- STOP EXECUTION (SSENIF)')
570    FORMAT(/,' TIME STEP ('I5,') LARGER THAN NPER ('I5,
        1      ') OF BASIC PACKAGE INPUT FILE -- STOP EXECUTION (SSENIF)',/)
575    FORMAT(/,' IBT MUST BE 1, 2, 3 OR 4 -- STOP EXECUTION',
        1      '(SSENIF)',/)
580    FORMAT(/,' NQC CAN BE REDUCED FROM',I5,' TO',I5)
585    FORMAT(/,' NQT CAN BE REDUCED FROM',I5,' TO',I5)
587    FORMAT(/,' ROW OR COLUMN NUMBER INVALID -- STOP EXECUTION',
        1      '(SSENIF)',/)
588    FORMAT(/,' NUMBER OF NODES IN THE NQ CELL GROUPS, ',
        1      'I5,' > NQC ('I5,') OR NUMBER FLOW OBSERVATIONS',I5,
        1      ' > NQT ('I5,') -- STOP EXECUTION (SSENIF)',/)
590    FORMAT(/,' LAYER INVALID OR CELL DESIGNATED AS INACTIVE IN '
        1      'IBOUND ARRAY OF BASIC PACKAGE INPUT -- STOP EXECUTION '
        2      '(SSENIF)',/)
C
C-----INITIALIZE VARIABLES
SSA0484
SSA0485
SSA0486
SSA0487
SSA0488
SSA0489
SSA0490
SSA0491
SSA0492
SSA0493
SSA0494
SSA0495
SSA0496
SSA0497
SSA0498
SSA0499
SSA0500
SSA0501
SSA0502
SSA0503
SSA0504
SSA0505
SSA0506
SSA0507
SSA0508
SSA0509
SSA0510
SSA0511
SSA0512
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SSA0516
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SSA0518
SSA0519
SSA0520
SSA0521
SSA0522
SSA0523
SSA0524
SSA0525
SSA0526
SSA0527
SSA0528
SSA0529
SSA0530
SSA0531
SSA0532
SSA0533

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DO 10 I=1,NQC	SSA0534
QCLS(5,I)=0.	SSA0535
10 CONTINUE	SSA0536
DO 20 IQ=1,NQ	SSA0537
20 IBT(2,IQ)=0	SSA0538
NC=0	SSA0539
NT=0	SSA0540
C-----WRITE TITLE AND LOOP THROUGH REACHES	SSA0541
WRITE(IOUT,517)	SSA0542
DO 200 IQ=1,NQ	SSA0543
READ(IU,515) IBT(1,IQ),NQOB(IQ),NQCL(IQ)	SSA0544
WRITE(IOUT,518) IQ,IBT(1,IQ),NQOB(IQ),NQCL(IQ)	SSA0545
C-----SET FLAG FOR SETTING ALL FACTORS TO 1	SSA0546
I4=0	SSA0547
IF(NQCL(IQ).LT.0) THEN	SSA0548
I4=1	SSA0549
NQCL(IQ)=-NQCL(IQ)	SSA0550
ENDIF	SSA0551
C-----READ TIME STEPS, MEASURED FLOWS, AND WEIGHTS.	SSA0552
NT1=NT+1	SSA0553
NT2=NT+NQOB(IQ)	SSA0554
DO 115 J=NT1,NT2	SSA0555
N=NH+J	SSA0556
1 READ(IU,510) DID(N),IQOB(J),TOFF(N),HOBS(N),	SSA0557
WT(N),IWT	SSA0558
IF(IWT.EQ.2) WT(N)=WT(N)*HOBS(N)	SSA0559
IF(IWT.GT.0) WT(N)=WT(N)*WT(N)	SSA0560
WT(N)=WT(N)*EVF	SSA0561
WRITE(IOUT,520) N,DID(N),IQOB(J),TOFF(N),HOBS(N),WT(N)	SSA0562
IF(WT(N).LT.0.) THEN	SSA0563
WRITE(IOUT,540)	SSA0564
IERR=1	SSA0565
ENDIF	SSA0566
C-----ERROR CHECKING	SSA0567
IF(IQOB(J).GT.JT) JT=IQOB(J)	SSA0568
IF(IQOB(J).GT.NPER) THEN	SSA0569
WRITE(IOUT,570) IQOB(J),NPER	SSA0570
IERR=1	SSA0571
ENDIF	SSA0572
IBT1=IBT(1,IQ)	SSA0573
IF(IBT1.LT.1.OR.IBT1.GT.4) THEN	SSA0574
WRITE(IOUT,575)	SSA0575
IERR=1	SSA0576
ELSEIF(IBT1.EQ.1.AND.MXRIVR.EQ.0.OR.	SSA0577
1 IBT1.EQ.2.AND.MXBND.EQ.0.OR.	SSA0578
2 IBT1.EQ.3.AND.MXSTRM.EQ.0.OR.	SSA0579
3 IBT1.EQ.4.AND.MXDRN.EQ.0) THEN	SSA0580
WRITE(IOUT,560)	SSA0581
IERR=1	SSA0582
ENDIF	SSA0583
115 CONTINUE	SSA0584
C-----READ LAYER, ROW AND COLUMN, OR SEGMENT AND REACH.	SSA0585
IBT1=IBT(1,IQ)	SSA0586
NC1=NC+1	SSA0587
NC2=NC+NQCL(IQ)	SSA0588
IF(IBT1.NE.3) WRITE(IOUT,522)	SSA0589
IF(IBT1.EQ.3) WRITE(IOUT,523)	SSA0590
NNUM=3	SSA0591
IF(IBT1.EQ.3) NNUM=2	SSA0592
DO 118 L=NC1,NC2	SSA0593
IF(IBT1.NE.3) THEN	SSA0594
READ(IU,503) (QCLS(I,L),I=1,4)	SSA0595
IF(QCLS(4,L).EQ.0..OR.I4.EQ.1) QCLS(4,L)=1.	SSA0596
WRITE(IOUT,525) (QCLS(I,L),I=1,4)	SSA0597
ELSE	SSA0598
READ(IU,501) (QCLS(I,L),I=1,2),QCLS(4,L)	SSA0599
IF(QCLS(4,L).EQ.0..OR.I4.EQ.1) QCLS(4,L)=1.	SSA0600
WRITE(IOUT,530) (QCLS(I,L),I=1,2),QCLS(4,L)	SSA0601
QCLS(3,L)=0.	SSA0602
GO TO 118	SSA0603
ENDIF	SSA0604
K=QCLS(1,L)	SSA0605
I=QCLS(2,L)	SSA0606
J=QCLS(3,L)	SSA0607
IF(J.LE.0.OR.J.GT.NCOL.OR.I.LE.0.OR.I.GT.NROW) THEN	SSA0608
WRITE(IOUT,587)	SSA0609
IERR=1	SSA0610
ENDIF	SSA0611
IF(K.LE.0.OR.K.GT.NLAY.OR.IBOUND(J,I,K).EQ.0) THEN	SSA0612
WRITE(IOUT,590)	SSA0613
IERR=1	SSA0614
ENDIF	SSA0615
118 CONTINUE	SSA0616

C-----ARE ANY PARAMETERS INVOLVED IN THIS BOUNDARY?	SSA0617
NS=0	SSA0618
IFLAG=0	SSA0619
IFL=0	SSA0620
ICH=0	SSA0621
DO 180 IP=1,NP	SSA0622
PIDTMP=PID(IP)	SSA0623
INS=NS	SSA0624
IF((IBT(1,IQ).EQ.1.AND.PIDTMP.EQ.'KRB ').OR.	SSA0625
(IBT(1,IQ).EQ.2.AND.PIDTMP.EQ.'GHB ').OR.	SSA0626
(IBT(1,IQ).EQ.3.AND.PIDTMP.EQ.'KST ').OR.	SSA0627
(IBT(1,IQ).EQ.4.AND.PIDTMP.EQ.'KDR ')) THEN	SSA0628
DO 170 IT=1,NLLIT	SSA0629
IF(NLL(2*IT,IP).LT.0) GO TO 175	SSA0630
DO 165 N=NT1,NT2	SSA0631
IF(IQOB(N).GE.NLL(2*IT,IP).AND.	SSA0632
IQOB(N).LE.NLL(2*IT+1,IP)) THEN	SSA0633
NLI=NLL(1,IP)	SSA0634
NLI1=IABS(NLI)	SSA0635
C-----LOOP THROUGH PARAMETER CELLS	SSA0636
DO 160 II=1,NLI1	SSA0637
INS=INS+1	SSA0638
K=CELS(1,INS)	SSA0639
I=CELS(2,INS)	SSA0640
J=CELS(3,INS)	SSA0641
IF(BOUND(J,I,K).LE.0) GO TO 160	SSA0642
C-----LOOP THROUGH TO SEE IF THIS CELL IS ON THE BOUNDARY	SSA0643
DO 150 JJ=NCL,NC2	SSA0644
K1=QCLS(1,JJ)	SSA0645
I1=QCLS(2,JJ)	SSA0646
J1=QCLS(3,JJ)	SSA0647
C-----IF SO, PUT PARAMETER FACTOR IN QCLS(5)	SSA0648
IF(QCLS(1,JJ).EQ.K .AND. QCLS(2,JJ).EQ.I .AND.	SSA0649
QCLS(3,JJ).EQ.J) THEN	SSA0650
IBT(2,IQ)=IP	SSA0651
IFLAG=1	SSA0652
QCLS(5,JJ)=1.	SSA0653
IF(NLI.GT.0) QCLS(5,JJ)=CELS(4,INS)	SSA0654
ENDIF	SSA0655
150 CONTINUE	SSA0656
160 CONTINUE	SSA0657
GO TO 175	SSA0658
ENDIF	SSA0659
165 CONTINUE	SSA0660
170 CONTINUE	SSA0661
ENDIF	SSA0662
175 CONTINUE	SSA0663
IF(IFLAG.EQ.1) GO TO 185	SSA0664
IF(PIDTMP.EQ.'CH ' .AND. ICH.EQ.0) THEN	SSA0665
ICH=ICH+1	SSA0666
IF(ICH.EQ.NLL(2,IP)) ICH=0	SSA0667
GO TO 180	SSA0668
ENDIF	SSA0669
IF(PIDTMP.EQ.'KRB ' .OR. PIDTMP.EQ.'GHB ' .OR.	SSA0670
PIDTMP.EQ.'Q ' .OR. PIDTMP.EQ.'CH ' .OR.	SSA0671
PIDTMP.EQ.'KDR ' .OR. PIDTMP.EQ.'KST ')	SSA0672
NS=NS+IABS(NLL(1,IP))	SSA0673
180 CONTINUE	SSA0674
IF(IFLAG.EQ.0) IBT(2,IQ)=0	SSA0675
185 CONTINUE	SSA0676
C-----UPDATE COUNTERS	SSA0677
NC=NC2	SSA0678
NT=NT2	SSA0679
200 CONTINUE	SSA0680
C-----EXCEEDED STORAGE RESERVED FOR FLOW DATA?	SSA0681
IF(NC.GT.NQC.OR.NT.GT.NQT) THEN	SSA0682
WRITE(IOUT,588) NC,NQC,NT,NQT	SSA0683
IERR=1	SSA0684
ENDIF	SSA0685
C-----ALLOCATED TOO MUCH STORAGE?	SSA0686
IF(NQC.GT.NC) THEN	SSA0687
WRITE(IOUT,580) NQC,NC	SSA0688
NQC=NC	SSA0689
ENDIF	SSA0690
IF(NQT.GT.NT) THEN	SSA0691
WRITE(IOUT,585) NQT,NT	SSA0692
NQT=NT	SSA0693
ENDIF	SSA0694
RETURN	SSA0695
END	SSA0696



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C=====SSA0697
      SUBROUTINE SSENIG (SSA0698
1        NCOL,NROW,NLAY,NSN,NSM,MXBND,MXWELL,MXRIVR,NPER,IU,IOUT,NP,SSA0699
2        PID,NLL,CELS,SMAT,IBOUND,TOP,BOT,LN,IERR,IUBD,BUFF,DELR,SSA0700
3        DELC,MXDRN,MXSTRM,NMM,NZM,LZ11,SFAC,LZ,LM,MATZ,NLL11,IUNIT)SSA0701
C-----VERSION 1000 01FEB1992SSA0702
C      *****SSA0703
C      READ, CHECK AND STORE DATA FOR PARAMETER DEFINITION.SSA0704
C      *****SSA0705
C      SPECIFICATIONS:SSA0706
C      -----SSA0707
C      CHARACTER*4    PID(NP),PIDTMP,ANAMESSA0708
C      INTEGER        NLL(NLL11,NP)SSA0709
C      DIMENSION CELS(4,NSN),SMAT(NCOL,NROW,NMM),ANAME(6,2),SFAC(NSM),SSA0710
1      IBOUND(NCOL,NROW,NLAY),TOP(NCOL,NROW,NLAY),LZ(LZ11,NSM),SSA0711
2      BOT(NCOL,NROW,NLAY),LN(NP),LM(NSM),MATZ(NCOL,NROW,NZM),SSA0712
3      BUFF(NCOL,NROW,NLAY),DELR(NCOL),DELC(NROW),IUNIT(24)SSA0713
C      DATA ANAME(1,1),ANAME(2,1),ANAME(3,1),ANAME(4,1),ANAME(5,1),SSA0714
C      # ANAME(6,1) /' M','ULTI','PLIC','ATIO','N MA','TRIX'/SSA0715
C      DATA ANAME(1,2),ANAME(2,2),ANAME(3,2),ANAME(4,2),ANAME(5,2),SSA0716
C      # ANAME(6,2) /' ',' ',' ',' ',' 'ZON','E MA','TRIX'/SSA0717
C      -----SSA0718
501  FORMAT(15X,2F5.0,25X,F10.0)SSA0719
503  FORMAT(8F10.0)SSA0720
504  FORMAT(3F10.0,10X,F10.0)SSA0721
506  FORMAT(24F3.0)SSA0722
508  FORMAT(F9.0,F11.0,F9.0,3X,E10.3)SSA0723
510  FORMAT(F10.0,15I5)SSA0724
520  FORMAT(16I5)SSA0725
525  FORMAT(A4,I1,11I5)SSA0726
527  FORMAT(/,' # FACTORS >1. (' ,I4,') DOES NOT EQUAL NLL(2) (' ,I4,')')SSA0727
528  FORMAT(/,' LN>0 IS NOT VALID FOR THIS PID -- STOP EXECUTION ',SSA0728
1  '(SSENIG)')SSA0729
530  FORMAT(' SFAC=',G11.3,', MULT. MATRIX',I5,SSA0730
1  ', ZONE MATRIX',I5)SSA0731
531  FORMAT(' ZONES =',20I5,/,20(8X,20I5,/))SSA0732
532  FORMAT(/,' PARAMETER NUMBER:',I5,', PARAMETER IDENTIFIER: ',1X,A4,SSA0733
C      # /,' LN:',I3,', VECTOR NLL:',11I5,/,20(11I5))SSA0734
533  FORMAT(/,' NLL VALUE',I5,', NOT VALID -- STOP EXECUTION (SSENIG)',/)SSA0735
534  FORMAT(/,' LH ,A5,' FOR PARAMETER NUMBER',I5,' IS NOT A VALID 'SSA0736
C      # 'PARAMETER IDENTIFIER -- STOP EXECUTION (SSENIG)')SSA0737
536  FORMAT(/,' NLL(1)',I5,', =0 OR >'SSA0738
C      # ' MAXIMUM SPECIFIED BY MXWELL, MXRIVR, MXBND, MXSTRM, OR MXDRN'SSA0739
C      # ' -- STOP EXECUTION (SSENIG)',/)SSA0740
538  FORMAT(/,' MODULAR MODEL PACKAGE RELATED TO THIS PARAMETER IS ',SSA0741
1  'NOT OPEN -- STOP EXECUTION (SSENIG)')SSA0742
539  FORMAT(/,' NEED NLL11>=3 FOR TIMING INFORMATION -- STOP ',SSA0743
1  'EXECUTION')SSA0744
540  FORMAT(/,' FOR CH, FACTOR MUST BE =0., <0., OR >1. -- 'SSA0745
1  'STOP EXECUTION',/)SSA0746
550  FORMAT(/,' NUMBER OF NODES USED FOR PARAMETER DEFINITION, ',SSA0747
1  'I5,' >NSN (' ,I5,') OR NUMBER OF MATRICES',I5,' >NSM ('SSA0748
1  ',I5,') -- STOP EXECUTION (SSENIG)',/)SSA0749
560  FORMAT(4X,'SEGMENT',5X,'REACH ZERO FACTOR')SSA0750
565  FORMAT(5X,'LAYER',7X,'ROW COLUMN FACTOR')SSA0751
570  FORMAT(/,' CELL NOT DESIGNATED AS CONSTANT HEAD IN IBOUND 'SSA0752
1  'ARRAY OF BASIC PACKAGE UNIT -- STOP EXECUTION (SSENIG)',/)SSA0753
575  FORMAT(/,' ENDS OF CONSTANT HEAD BOUNDARIES MUST HAVE 'SSA0754
1  'NONZERO VALUES -- STOP EXECUTION (SSENIG)',/)SSA0755
580  FORMAT(/,' NSN CAN BE REDUCED FROM',I5,' TO',I5)SSA0756
585  FORMAT(/,' NSM CAN BE REDUCED FROM',I5,' TO',I5)SSA0757
590  FORMAT(/,' ERROR IN CH DATA : FOURTH COLUMN ALL 0 OR FIRST OR',SSA0758
1  ' LAST VALUE IS 0 -- STOP EXECUTION (SSENIG)',/)SSA0759
600  FORMAT(/,' SPECIFIED ZONATION INCONSISTENT WITH LZ11 AND/OR NZM',SSA0760
1  ' (LINE 4) -- STOP EXECUTION')SSA0761
610  FORMAT(/,' ERROR IN ANIV DATA : LAYER NUMBER LISTED HERE',SSA0762
1  ' APPEARS FOR KV PARAMETER #',I5,' -- STOP EXECUTION')SSA0763
620  FORMAT(/,' ERROR IN ANIV DATA : ALL LAYERS MUST APPEAR ',SSA0764
1  ' IN A PREVIOUS TKV PARAMETER -- STOP EXECUTION')SSA0765
630  FORMAT(/,' MULTIPLICATION MATRIX NUMBER INCONSISTENT WITH NMM',SSA0766
1  ' (LINE 4) -- STOP EXECUTION')SSA0767
C      -----SSA0768
C      -----SET COUNTERSSSA0769
C      NS=0SSA0770
C      NM=0SSA0771
C      ICH=0SSA0772
C      IFL=0SSA0773
C      -----SET ERROR INDICATORSSA0774
C      IERR=0SSA0775
C      -----READ PARAMETER IDENTIFICATION DATASSA0776
C      DO 100 IP=1,NPSSA0777
C      -----ACCOUNT FOR MULTIPLE CONSTANT-HEAD PARAMETERS UNDER ONE PIDSSA0778

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        IF(IP.GT.1.AND.PID(IP-1).EQ.'CH ') THEN
            IF(ICH.EQ.NLL(2,IP-1)) THEN
                ICH=0
                GO TO 20
            ENDIF
            PID(IP)='CH '
            DO 15 NL=1,NLL11
                15  NLL(NL,IP)=NLL(NL,IP-1)
                LN(IP)=LN(IP-1)
                ICH=ICH+1
                GO TO 100
            ENDIF
C-----FIRST CARD FOR EACH PARAMETER
        20  IF(NLL11.LE.11) THEN
            READ(IU,525) PID(IP),LN(IP),(NLL(LL,IP),LL=1,NLL11)
        ELSE
            READ(IU,525) PID(IP),LN(IP),(NLL(LL,IP),LL=1,11)
            READ(IU,520) (NLL(LL,IP),LL=12,NLL11)
        ENDIF
        PIDTMP=PID(IP)
        WRITE(IOUT,532) IP,PIDTMP,LN(IP),(NLL(LL,IP),LL=1,NLL11)
C-----CHECK PARAMETER IDENTIFIER
        INAME=0
        IF(PIDTMP.EQ.'T ' .OR. PIDTMP.EQ.'S1 ' .OR.
        1  PIDTMP.EQ.'RCH ' .OR. PIDTMP.EQ.'ETM ' .OR. PIDTMP.EQ.'GHB '
        2  .OR. PIDTMP.EQ.'Q ' .OR. PIDTMP.EQ.'KV ' .OR.
        3  PIDTMP.EQ.'ANI ' .OR. PIDTMP.EQ.'CH ' .OR. PIDTMP.EQ.'KDR '
        4  .OR. PIDTMP.EQ.'KRB ' .OR. PIDTMP.EQ.'KST ' .OR.
        5  PIDTMP.EQ.'TKV ' .OR. PIDTMP.EQ.'ANIV') INAME=1
        IF(INAME.EQ.0) THEN
            WRITE(IOUT,534) PIDTMP,IP
            STOP
        ENDIF
C-----CHECK USE OF NATURAL LOG OF PARAMETER
        IF(LN(IP).NE.0.AND.(PIDTMP.EQ.'RCH ' .OR. PIDTMP.EQ.'Q
        1  .OR. PIDTMP.EQ.'CH ' .OR. PIDTMP.EQ.'ETM ')) THEN
            WRITE(IOUT,528)
            IERR=1
        ENDIF
C-----READ AND CHECK FOR PARAMETERS DEFINED BY LISTS OF CELLS
        IF(PIDTMP.EQ.'Q ' .OR. PIDTMP.EQ.'GHB ' .OR. PIDTMP.EQ.'KRB ' .OR.
        1  PIDTMP.EQ.'KDR ' .OR. PIDTMP.EQ.'KST ') THEN
            NLL=NLL(1,IP)
            NLLA=IABS(NLL)
            IF((NLLA.EQ.0).OR.
            1  (PIDTMP.EQ.'Q ' .AND. NLLA.GT.MXWELL).OR.
            2  (PIDTMP.EQ.'GHB ' .AND. NLLA.GT.MXBND).OR.
            3  (PIDTMP.EQ.'KDR ' .AND. NLLA.GT.MXDRN).OR.
            4  (PIDTMP.EQ.'KRB ' .AND. NLLA.GT.MXRIVR).OR.
            5  (PIDTMP.EQ.'KST ' .AND. NLLA.GT.MXSTRM)) THEN
                WRITE(IOUT,536) NLL
                IERR=1
            ENDIF
            IF(NLL11.LT.3) THEN
                WRITE(IOUT,539)
                IERR=1
            ENDIF
            IF(PIDTMP.EQ.'Q ' .AND. IUNIT(2).EQ.0.OR.
            1  PIDTMP.EQ.'GHB ' .AND. IUNIT(7).EQ.0.OR.
            1  PIDTMP.EQ.'KDR ' .AND. IUNIT(3).EQ.0.OR.
            1  PIDTMP.EQ.'KRB ' .AND. IUNIT(4).EQ.0) THEN
                WRITE(IOUT,538)
                IERR=1
            ENDIF
            IF(PIDTMP.NE.'KST ') WRITE(IOUT,565)
            IF(PIDTMP.EQ.'KST ') WRITE(IOUT,560)
            FAC=1.
            DO 30 J=1,NLLA
                NS=NS+1
                IF(PIDTMP.NE.'Q ' .AND. PIDTMP.NE.'KST ')
                1  READ(IU,504) (CELS(I,NS),I=1,4)
                IF(PIDTMP.EQ.'KST ') THEN
                    READ(IU,501) (CELS(I,NS),I=1,2),CELS(4,NS)
                    CELS(3,NS)=0.
                ENDIF
                IF(PIDTMP.EQ.'Q ') READ(IU,503) (CELS(I,NS),I=1,4)
                IF(NLL.GT.0) WRITE(IOUT,508)(CELS(I,NS),I=1,4)
                IF(NLL.LT.0) WRITE(IOUT,508)(CELS(I,NS),I=1,3),FAC
            30  CONTINUE
        ENDIF
C-----CH
        IF(PIDTMP.EQ.'CH ') THEN
            NLL=NLL(1,IP)

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SSA0780  
 SSA0781  
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 SSA0860  
 SSA0861  
 SSA0862

	IF(NL1.LE.0) THEN	SSA0863
	WRITE(IOUT,536) NL1	SSA0864
	STOP	SSA0865
	ENDIF	SSA0866
	ICH=1	SSA0867
C-----	READ IBOUND ARRAY(S)	SSA0868
33	IF(IUBD.NE.0.AND.IFL.EQ.0) THEN	SSA0869
	REWIND(IUBD)	SSA0870
	IFL=1	SSA0871
	DO 35 K=1,NLAY	SSA0872
35	CALL U2DINN(IBOUND(1,1,K),NROW,NCOL,IUBD)	SSA0873
	IF(NPER.GT.1) THEN	SSA0874
	DO 40 K=1,NLAY	SSA0875
	DO 38 I=1,NROW	SSA0876
	DO 38 J=1,NCOL	SSA0877
38	BUFF(J,I,K)=IBOUND(J,I,K)	SSA0878
40	CALL U2DINN(IBOUND(1,1,K),NROW,NCOL,IUBD)	SSA0879
	ENDIF	SSA0880
	ENDIF	SSA0881
	WRITE(IOUT,565)	SSA0882
	NPCH=0	SSA0883
	RPCH=0.	SSA0884
	NL3=NLL(3,IP)	SSA0885
	DO 50 ICH=1,NL1	SSA0886
	NS=NS+1	SSA0887
	READ(IU,503) DUM,(CELS(I,NS),I=1,3)	SSA0888
	DUM=0.	SSA0889
	WRITE(IOUT,508) DUM,(CELS(I,NS),I=1,3)	SSA0890
	CE3=CELS(3,NS)	SSA0891
	IF(CE3.GT.1..AND.CE3.NE.RPCH) THEN	SSA0892
	NPCH=NPCH+1	SSA0893
	RPCH=CE3	SSA0894
	ENDIF	SSA0895
	IF(CE3.GT.0..AND.CE3.LE.1.) THEN	SSA0896
	WRITE(IOUT,540)	SSA0897
	IERR=1	SSA0898
	ENDIF	SSA0899
	DO 45 NL=4,NLL1	SSA0900
	K=NLL(NL,IP)	SSA0901
	IF(K.EQ.0) GO TO 50	SSA0902
	IF((IUBD.EQ.0.OR.NL3.NE.0.OR.NPER.EQ.1).AND.	SSA0903
1	IBOUND( INT(CELS(2,NS)),INT(CELS(1,NS)),K).GT.0) THEN	SSA0904
	WRITE(IOUT,570)	SSA0905
	IERR=1	SSA0906
	ENDIF	SSA0907
	IF(IUBD.NE.0.AND.NL3.NE.1.AND.NPER.GT.1.AND.	SSA0908
1	INT(BUFF( INT(CELS(2,NS)),INT(CELS(1,NS)),K)).GE.0)	SSA0909
2	THEN	SSA0910
	WRITE(IOUT,570)	SSA0911
	IERR=1	SSA0912
	ENDIF	SSA0913
45	CONTINUE	SSA0914
50	CONTINUE	SSA0915
	IF(NPCH.NE.NLL(2,IP)) THEN	SSA0916
	WRITE(IOUT,527) NPCH,NLL(2,IP)	SSA0917
	IERR=1	SSA0918
	ENDIF	SSA0919
	IF(IUBD.NE.0) REWIND(IUBD)	SSA0920
C-----	CHECK TO BE SURE THAT THE FIRST AND LAST FACTORS ARE NOT ZERO.	SSA0921
	IF(CELS(3,(NS-NLL+1)).EQ.0..OR.CE3.EQ.0.) THEN	SSA0922
	WRITE(IOUT,590)	SSA0923
	IERR=1	SSA0924
	ENDIF	SSA0925
C-----	CALCULATE COEFFICIENTS FOR CONSTANT-HEAD BOUNDARIES	SSA0926
	CALL SSEN1B(NLL(1,IP),NCOL,NROW,CELS,NS,NSN,DELR,	SSA0927
1	DELC,IOUT,IERR,NLL1)	SSA0928
	ENDIF	SSA0929
C-----	READ AND CHECK FOR PARAMETERS DEFINED BY ONE NCOL X NROW ARR	SSA0930
	IF(PIDTMP.EQ.'RCH '.OR.PIDTMP.EQ.'ETM ')THEN	SSA0931
	NL1=NLL(1,IP)	SSA0932
	IF(NLL1.LT.3) THEN	SSA0933
	WRITE(IOUT,539)	SSA0934
	IERR=1	SSA0935
	ENDIF	SSA0936
	IF(NL1.EQ.0) THEN	SSA0937
	IERR=1	SSA0938
	WRITE(IOUT,536) NL1	SSA0939
	ELSEIF (NL1.GT.0) THEN	SSA0940
	NM=NM+1	SSA0941
	IF(LZ11.LE.14) THEN	SSA0942
	READ(IU,510) SFAC(NM),LM(NM),(LZ(IZ,NM),IZ=1,LZ11)	SSA0943
	ELSE	SSA0944
	READ(IU,510) SFAC(NM),LM(NM),(LZ(IZ,NM),IZ=1,14)	SSA0945

	READ(IU,520) (LZ(IZ,NM),IZ=15,LZ11)	SSA0946
	ENDIF	SSA0947
	WRITE(IOUT,530) SFAC(NM),LM(NM),LZ(1,NM)	SSA0948
	WRITE(IOUT,531) (LZ(IZ,NM),IZ=2,LZ11)	SSA0949
	IF(LZ(1,NM).NE.0.AND.(LZ11.LE.1.OR.NZM.LT.LZ(1,NM))) THEN	SSA0950
	WRITE(IOUT,600)	SSA0951
	IERR=1	SSA0952
	ENDIF	SSA0953
	IF(NMM.LT.LM(NM)) THEN	SSA0954
	WRITE(IOUT,630)	SSA0955
	IERR=1	SSA0956
	ENDIF	SSA0957
	ENDIF	SSA0958
	IF(PIDTMP.EQ.'RCH '.AND.IUNIT(8).EQ.0.OR.	SSA0959
1	PIDTMP.EQ.'ETM '.AND.IUNIT(5).EQ.0) THEN	SSA0960
	WRITE(IOUT,538)	SSA0961
	IERR=1	SSA0962
	ENDIF	SSA0963
	ENDIF	SSA0964
C-----	READ AND CHECK FOR PARAMETERS WHICH MAY APPLY TO MANY LAYERS	SSA0965
	IF(PIDTMP.EQ.'S1 '.OR.PIDTMP.EQ.'T '.OR.PIDTMP.EQ.'KV '	SSA0966
1	.OR.PIDTMP.EQ.'TKV ') THEN	SSA0967
	DO 70 LL=1,NLL11	SSA0968
	NL=NLL(LL,IP)	SSA0969
	NLLA=IABS(NL)	SSA0970
	IF(NL.EQ.0) GO TO 70	SSA0971
	IF(NLLA.GT.NLAY. OR .	SSA0972
1	(PIDTMP.EQ.'KV '.AND.NLAY.EQ.1).OR.	SSA0973
1	(PIDTMP.EQ.'TKV '.AND.MOD(LL+1,3).NE.0.AND.	SSA0974
1	(NLAY.EQ.1.OR.(MOD(LL+2,3).EQ.0.AND.NLLA.EQ.1))) THEN	SSA0975
	WRITE(IOUT,533) NL	SSA0976
	IERR=1	SSA0977
	ENDIF	SSA0978
	IF(PIDTMP.EQ.'TKV '.AND.MOD(LL+2,3).EQ.0) NLLA=NLLA-1	SSA0979
	IF(NL.GT.0) THEN	SSA0980
	NM=NM+1	SSA0981
	IF(LZ11.LE.14) THEN	SSA0982
	READ(IU,510) SFAC(NM),LM(NM),(LZ(IZ,NM),IZ=1,LZ11)	SSA0983
	ELSE	SSA0984
	READ(IU,510) SFAC(NM),LM(NM),(LZ(IZ,NM),IZ=1,14)	SSA0985
	READ(IU,520) (LZ(IZ,NM),IZ=15,LZ11)	SSA0986
	ENDIF	SSA0987
	WRITE(IOUT,530) SFAC(NM),LM(NM),LZ(1,NM)	SSA0988
	WRITE(IOUT,531) (LZ(IZ,NM),IZ=2,LZ11)	SSA0989
	IF(LZ(1,NM).NE.0.AND.(LZ11.LE.1.OR.NZM.LT.LZ(1,NM))) THEN	SSA0990
	WRITE(IOUT,600)	SSA0991
	IERR=1	SSA0992
	ENDIF	SSA0993
	IF(NMM.LT.LM(NM)) THEN	SSA0994
	WRITE(IOUT,630)	SSA0995
	IERR=1	SSA0996
	ENDIF	SSA0997
	ENDIF	SSA0998
70	CONTINUE	SSA0999
	ENDIF	SSA1000
C-----	READ AND CHECK FOR PARAMETER WITH NO ADDITIONAL DATA	SSA1001
	IF(PIDTMP.EQ.'ANI '.OR.PIDTMP.EQ.'ANIV') THEN	SSA1002
	DO 75 LL=1,NLL11	SSA1003
	IF(NLL(LL,IP).EQ.0) GO TO 77	SSA1004
	IF(NLL(LL,IP).GT.NLAY.OR.NLL(LL,IP).LT.0) THEN	SSA1005
	WRITE(IOUT,533) NLL(LL,IP)	SSA1006
	IERR=1	SSA1007
	ENDIF	SSA1008
	CONTINUE	SSA1009
75	CONTINUE	SSA1010
77	CONTINUE	SSA1011
	ENDIF	SSA1012
	IF(PIDTMP.EQ.'ANIV') THEN	SSA1013
	I1=0	SSA1014
	I2=0	SSA1015
	DO 90 LL=1,NLL11	SSA1016
	NLP=NLL(LL,IP)	SSA1017
	IF(NLP.EQ.0) GO TO 95	SSA1018
	IF(NLP.GT.0) THEN	SSA1019
	I1=I1+1	SSA1020
	DO 85 IIP=1,IP-1	SSA1021
	IF(PID(IIP).EQ.'TKV ') THEN	SSA1022
	DO 80 LV=1,NLL11	SSA1023
	IF(MOD(LV,2).NE.0.AND.	SSA1024
1	NLP.EQ.ABS(NLL(LV,IIP))) I2=I2+1	SSA1025
80	CONTINUE	SSA1026
	ENDIF	SSA1027
	IF(PID(IIP).EQ.'KV ') THEN	SSA1028

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DO 82 LV=1,NLLI1
  IF (ABS(NLL(LV,IIP)).EQ.NLP) THEN
    WRITE(IOUT,610) IIP
    IERR=1
  ENDIF
82  CONTINUE
  ENDIF
85  CONTINUE
  ENDIF
90  CONTINUE
  IF (I1.NE.I2) THEN
    WRITE(IOUT,620)
    IERR=1
  ENDIF
95  CONTINUE
  ENDIF
100 CONTINUE
C-----READ MULTIPLICATION AND ZONE MATRICES
  IF (NMM.GT.0) THEN
    DO 110 M=1,NMM
110  CALL U2DREL(SMAT(1,1,M),ANAME(1,1),NROW,NCOL,-M,IU,IOUT)
    ENDIF
    IF (NZM.GT.0) THEN
      DO 120 MZ=1,NZM
120  CALL U2DINT(MATZ(1,1,MZ),ANAME(1,2),NROW,NCOL,-MZ,IU,IOUT)
      ENDIF
C-----CHECK WHETHER ITEMS STORED EXCEED RESERVED STORAGE SPACE
    IF (NS.GT.NSN.OR.NM.GT.NSM) THEN
      WRITE(IOUT,550) NS,NSN,NM,NSM
      IERR=1
    ELSE
      IF (NSN.GT.NS) THEN
        WRITE(IOUT,580) NSN,NS
        NSN=NS
      ENDIF
      IF (NSM.GT.NM) THEN
        WRITE(IOUT,585) NSM,NM
        NSM=NM
      ENDIF
    ENDIF
  ENDIF
  RETURN
  END

C=====SSA1071
SUBROUTINE SSEN1H (
1  NCOL,NROW,NLAY,NPER,IU,IOUT,DID,NH,NDER,JT,IBOUND,JOFF,IOFF,
2  HOBS,WT,DELR,DELC,RINT,COFF,ROFF,MLAY,PR,MOBS,IERR,
3  TOFF,EVH,ISN,MAXM)
C-----VERSION 1000 01FEB1992
C *****SSA1077
C READ, CHECK AND STORE DATA FOR HYDRAULIC HEAD LOCATIONS.
C *****SSA1079
C SPECIFICATIONS:
C -----SSA1081
  CHARACTER*4 DID(NH)
  DIMENSION NDER(5,NH),IBOUND(NCOL,NROW,NLAY),IOFF(NH),JOFF(NH),
2  HOBS(NH),WT(NH),DELR(NCOL),DELC(NROW),RINT(4,NH),
4  COFF(NH),ROFF(NH),MLAY(MAXM,MOBS),PR(MAXM,MOBS),TOFF(NH)
C -----SSA1086
506 FORMAT(A4,1X,I5,3F8.0,F10.0,F8.0,I5)
509 FORMAT(8(I5,F5.0))
515 FORMAT(A4,1X,I5,F8.0,3F10.0,I5)
520 FORMAT(2X,'TRANSIENT DATA AT THIS LOCATION, ITT =',I4)
525 FORMAT(1X,I5,2X,A4,21X,I5,19X,F8.2,4X,2G12.5)
540 FORMAT(/,' STATISTIC RELATED TO WEIGHT < 0 -- STOP EXECUTION',
1  '(SSEN1H)',/)
555 FORMAT(/,' OBSERVED HEAD DATA',/,3X,'OBS# ID LAYER ROW',
P ' COLUMN TIME STEP ROW/COLUMN/TIME OFFSETS OBSERVATION ',
P ' VARIANCE')
560 FORMAT(1X,I5,2X,A4,I5,1X,2I5,5X,I5,3X,3F8.2,4X,2G12.5)
562 FORMAT(5X,'MULTIPLE LAYERS AND PROPORTIONS :',5(I5,',',F5.2,3X))
570 FORMAT(' TIME STEP (' ,I5,') LARGER THAN NPER (' ,I5,
1  ') OF BASIC PACKAGE INPUT FILE -- STOP EXECUTION (SSEN1H)',/)
587 FORMAT(' ROW OR COLUMN NUMBER INVALID -- STOP EXECUTION',
1  '(SSEN1H)',/)
590 FORMAT(' LAYER INVALID OR CELL DESIGNATED AS INACTIVE IN '
1  ',IBOUND ARRAY OF BASIC PACKAGE INPUT -- STOP EXECUTION',
2  '(SSEN1H)',/)
592 FORMAT(/,' MULTILAYER PROPORTIONS DO NOT SUM ',
1  'TO 1.0 -- STOP EXECUTION (SSEN1H)',/)
593 FORMAT(/,' NUMBER OF MULTILAYER OBSERVATIONS EXCEEDS MOBS -- '
1  ',STOP EXECUTION (SSEN1H)',/)

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600	FORMAT(' ')	SSA1110
610	FORMAT(' ITT MUST = 1 OR 2 -- STOP EXECUTION (SSEN1H)',/)	SSA1111
C		SSA1112
C-----	WRITE INTRODUCTORY LINES	SSA1113
	WRITE(IOUT,555)	SSA1114
C-----	INITIALIZE VARIABLES	SSA1115
	JT=0	SSA1116
	IDRY=-1	SSA1117
	ML=0	SSA1118
	NT=0	SSA1119
	NTC=0	SSA1120
	IF(MAXM.EQ.0) THEN	SSA1121
	DO 20 MM=1,MOBS	SSA1122
	DO 20 M=1,MAXM	SSA1123
	MLAY(M,MM)=0	SSA1124
	PR(M,MM)=0.	SSA1125
20	CONTINUE	SSA1126
	ENDIF	SSA1127
	DO 50 N=1,NH	SSA1128
50	NDER(5,N)=0	SSA1129
C-----	LOOP THROUGH HEAD OBSERVATIONS	SSA1130
	DO 110 N=1,NH	SSA1131
C-----	READ FIRST TRANSIENT OBSERVATIONS AT ONE LOCATION	SSA1132
	IF(N.GT.1.AND.(NDER(4,N-1).LT.0.OR.NTC.LT.NT)) THEN	SSA1133
	IF(NDER(4,N-1).LT.0) THEN	SSA1134
	N1=N-1	SSA1135
	NT=-NDER(4,N1)	SSA1136
	NTC=1	SSA1137
	READ(IU,515) DID(N1),NDER(4,N1),TOFF(N1),HOBS(N1),WT(N1),	SSA1138
	DUM,IWT	SSA1139
1	IF(IWT.EQ.2) WT(N1)=WT(N1)*HOBS(N1)	SSA1140
	IF(IWT.GT.0) WT(N1)=WT(N1)*WT(N1)	SSA1141
	WT(N1)=WT(N1)*EVH	SSA1142
	WRITE(IOUT,525) N1,DID(N1),NDER(4,N1),TOFF(N1),	SSA1143
	HOBS(N1),WT(N1)	SSA1144
1	IF(WT(N1).LT.0.) THEN	SSA1145
	WRITE(IOUT,540)	SSA1146
	IERR=1	SSA1147
	ENDIF	SSA1148
	ENDIF	SSA1149
C-----	SUBSEQUENT OBSERVATIONS AT ONE LOCATION	SSA1150
	NTC=NTC+1	SSA1151
C-----	ASSIGN INFORMATION WHICH STAYS THE SAME	SSA1152
	DO 80 I=1,3	SSA1153
80	NDER(I,N)=NDER(I,N1)	SSA1154
	ROFF(N)=ROFF(N1)	SSA1155
	COFF(N)=COFF(N1)	SSA1156
	IOFF(N)=IOFF(N1)	SSA1157
	JOFF(N)=JOFF(N1)	SSA1158
	DO 90 I=1,4	SSA1159
90	RINT(I,N)=RINT(I,N1)	SSA1160
	IF(NDER(1,N1).LT.0) THEN	SSA1161
	ML1=ML-1	SSA1162
	ML=ML+1	SSA1163
	DO 95 M=1,MAXM	SSA1164
	PR(M,ML)=PR(N,ML1)	SSA1165
95	MLAY(M,ML)=MLAY(M,ML1)	SSA1166
	ENDIF	SSA1167
C-----	READ INFORMATION UNIQUE TO THIS OBSERVATION	SSA1168
	READ(IU,515) DID(N),NDER(4,N),TOFF(N),HOBS(N),WT1,WT2,IWT	SSA1169
	IF(ITT.EQ.1) WT(N)=WT1	SSA1170
	IF(ITT.EQ.2) THEN	SSA1171
	WT(N)=WT2	SSA1172
	HOBS(N)=HOBS(N)-HOBS(N1)	SSA1173
	NDER(5,N)=N1	SSA1174
	ENDIF	SSA1175
	IF(IWT.EQ.2) WT(N)=WT(N)*HOBS(N)	SSA1176
	IF(IWT.GT.0) WT(N)=WT(N)*WT(N)	SSA1177
	WT(N)=WT(N)*EVH	SSA1178
	WRITE(IOUT,525) N,DID(N),NDER(4,N),TOFF(N),HOBS(N),WT(N)	SSA1179
	IF(WT(N).LT.0.) THEN	SSA1180
	WRITE(IOUT,540)	SSA1181
	IERR=1	SSA1182
	ENDIF	SSA1183
	IF(NTC.EQ.NT) WRITE(IOUT,600)	SSA1184
	GO TO 107	SSA1185
	ENDIF	SSA1186
C-----	READ A DATA SET 6	SSA1187
	READ(IU,506) DID(N),(NDER(I,N),I=1,4),	SSA1188
1	ROFF(N),COFF(N),TOFF(N),HOBS(N),WT(N),IWT	SSA1189
	IF(IWT.EQ.2) WT(N)=WT(N)*HOBS(N)	SSA1190
	IF(IWT.GT.0) WT(N)=WT(N)*WT(N)	SSA1191
	WT(N)=WT(N)*EVH	SSA1192

IF(NDER(4,N).LT.0) THEN	SSA1193
READ(IU,509) ITT	SSA1194
WRITE(IOUT,520) ITT	SSA1195
IF(ITT.NE.1.AND.ITT.NE.2) THEN	SSA1196
WRITE(IOUT,610)	SSA1197
STOP	SSA1198
ENDIF	SSA1199
ENDIF	SSA1200
WRITE(IOUT,560) N,DID(N),(NDER(I,N),I=1,4),	SSA1201
P      ROFF(N),COFF(N),TOFF(N),HOBS(N),WT(N)	SSA1202
IF(WT(N).LT.0.) THEN	SSA1203
WRITE(IOUT,540)	SSA1204
IERR=1	SSA1205
ENDIF	SSA1206
C-----ERROR CHECKING	SSA1207
K=NDER(1,N)	SSA1208
I=NDER(2,N)	SSA1209
J=NDER(3,N)	SSA1210
IF(J.LE.0.OR.J.GT.NCOL.OR.I.LE.0.OR.I.GT.NROW)THEN	SSA1211
WRITE(IOUT,587)	SSA1212
IERR=1	SSA1213
ENDIF	SSA1214
C-----INITIALIZE SOME VARIABLES	SSA1215
MM=1	SSA1216
TPR=1.	SSA1217
C-----READ INFORMATION FOR MULTILAYER OBSERVATIONS (DATA SET 6A)	SSA1218
IF(K.LT.0) THEN	SSA1219
ML=ML+1	SSA1220
READ(IU,509)(MLAY(M,ML),PR(M,ML),M=1,-K)	SSA1221
WRITE(IOUT,562)(MLAY(M,ML),PR(M,ML),M=1,-K)	SSA1222
MM=-K	SSA1223
TPR=0.	SSA1224
ENDIF	SSA1225
C-----ERROR CHECKING	SSA1226
DO 105 M=1,MM	SSA1227
KK=K	SSA1228
C-----ASSIGN LAYER NUMBERS AND ADD PROPORTIONS FOR MULTILAYER	SSA1229
C-----OBSERVATION WELLS	SSA1230
IF(K.LT.0) THEN	SSA1231
KK=MLAY(M,ML)	SSA1232
IF(KK.EQ.0) GO TO 105	SSA1233
TPR=TPR+PR(M,ML)	SSA1234
ENDIF	SSA1235
C-----CHECK LAYER NUMBER AND WHETHER THE CELL IS ACTIVE	SSA1236
IF(KK.LE.0.OR.KK.GT.NLAY.OR.IBOUND(J,I,KK).EQ.0)THEN	SSA1237
WRITE(IOUT,590)	SSA1238
IERR=1	SSA1239
ENDIF	SSA1240
105 CONTINUE	SSA1241
C-----CHECK SUM OF PROPORTIONS FOR MULTILAYER OBS WELLS	SSA1242
IF(K.LT.0.AND.(TPR.LT..98.OR.TPR.GT.1.02)) THEN	SSA1243
WRITE(IOUT,592)	SSA1244
IERR=1	SSA1245
ENDIF	SSA1246
C-----CALCULATE INTERPOLATION COEFFICIENTS	SSA1247
CALL SSEN1I(NDER(1,N),COFF(N),ROFF(N),DELR,DELC,IBOUND,NCOL,	SSA1248
1      NROW,NLAY,RINT(1,N),JOFF(N),IOFF(N),MLAY(1,ML))	SSA1249
C-----KEEP TRACK OF LATEST MEASUREMENT	SSA1250
107 IF(NDER(4,N).GT.JT) THEN	SSA1251
JT=NDER(4,N)	SSA1252
IF(TOFF(N).GT.0.) JT=JT+1	SSA1253
ENDIF	SSA1254
C-----ERROR CHECKING - MAKE SURE LAST MEASUREMENT IS NOT TOO LATE	SSA1255
IF(JT.GT.NPER) THEN	SSA1256
WRITE(IOUT,570) JT,NPER	SSA1257
IERR=1	SSA1258
JT=NPER	SSA1259
ENDIF	SSA1260
110 CONTINUE	SSA1261
C-----ERROR CHECKING -	SSA1262
C-----EXCEEDED STORAGE RESERVED FOR MULTILAYER OBSERVATIONS?	SSA1263
IF(ML.GT.MOBS) THEN	SSA1264
WRITE(IOUT,593)	SSA1265
IERR=1	SSA1266
ENDIF	SSA1267
RETURN	SSA1268
END	SSA1269

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C=====SSA1270
      SUBROUTINE SSEN1(
1          NDER,COFF,ROFF,DELR,DELC,IBOUND,
2          NCOL,NROW,NLAY,RINT,JOFF,IOFF,MLAY)
C-----SSA1271
C      VERSION 1000 01FEB1992SSA1272
C      *****SSA1273
C      CALCULATE INTERPOLATION COEFFICIENTS FOR LOCATING OBSERVED HEADS.SSA1274
C      *****SSA1275
C      SPECIFICATIONS:SSA1276
C      -----SSA1277
C      DIMENSION NDER(5),DELR(NCOL),DELC(NROW),IBOUND(NCOL,NROW,NLAY),
1          RINT(4)SSA1278
C      -----SSA1279
C      K=NDER(1)SSA1280
C      IF(K.LT.0) K=MLAYSSA1281
C      I=NDER(2)SSA1282
C      J=NDER(3)SSA1283
C      I1=I+1SSA1284
C      J1=J+1SSA1285
C      IOFF=1SSA1286
C      JOFF=1SSA1287
C      IF(ROFF.LT.0.) THENSSA1288
C          I1=I-1SSA1289
C          IOFF=-1SSA1290
C      ENDIFSSA1291
C      IF(COFF.LT.0.) THENSSA1292
C          J1=J-1SSA1293
C          JOFF=-1SSA1294
C      ENDIFSSA1295
C      IF(I1.LT.1.OR.I1.GT.NROW) ROFF=0.SSA1296
C      IF(J1.LT.1.OR.J1.GT.NCOL) COFF=0.SSA1297
C      IF((ABS(ROFF).LT..001.AND.ABS(COFF).LT..001).OR.
1          (ABS(ROFF).LT..001.AND.IBOUND(J1,I,K).EQ.0).OR.
1          (ABS(COFF).LT..001.AND.IBOUND(J,I1,K).EQ.0).OR.
1          (IBOUND(J,I1,K).EQ.0.AND.IBOUND(J1,I,K).EQ.0)) THENSSA1298
C          IOFF=0SSA1299
C          JOFF=0SSA1300
C          DO 100 IR=1,4SSA1301
100              RINT(IR)=.25SSA1302
C          RETURNSSA1303
C      ENDIFSSA1304
C      C-----CALCULATE CONSTANTSSSA1305
C      IF(ABS(ROFF).GT..001) THENSSA1306
C          DC=(DELC(I)+DELC(I1))/2.SSA1307
C          DCF=ABS(ROFF)*DELC(I)SSA1308
C      ENDIFSSA1309
C      IF(ABS(COFF).GT..001) THENSSA1310
C          DR=(DELR(J)+DELR(J1))/2.SSA1311
C          DRF=ABS(COFF)*DELR(J)SSA1312
C      ENDIFSSA1313
C      IF(ABS(ROFF).GT..001.AND.ABS(COFF).GT..001) A=1/(DC*DR)SSA1314
C      C-----LINEAR INTERPOLATIONSSA1315
C      IF(ABS(ROFF).LT..001.OR.
1          (IBOUND(J,I1,K).EQ.0.AND.IBOUND(J1,I1,K).EQ.0)) THENSSA1316
C          IOFF=0SSA1317
C          RINT(1)=0.5*(1.-DRF/DR)SSA1318
C          RINT(2)=0.5*DRF/DRSSA1319
C          RINT(3)=RINT(1)SSA1320
C          RINT(4)=RINT(2)SSA1321
C          RETURNSSA1322
C      ENDIFSSA1323
C      IF(ABS(COFF).LT..001.OR.
1          (IBOUND(J1,I,K).EQ.0.AND.IBOUND(J,I1,K).EQ.0)) THENSSA1324
C          JOFF=0SSA1325
C          RINT(1)=0.5*(1.-DCF/DC)SSA1326
C          RINT(2)=RINT(1)SSA1327
C          RINT(3)=0.5*DCF/DCSSA1328
C          RINT(4)=RINT(3)SSA1329
C          RETURNSSA1330
C      ENDIFSSA1331
C      C-----CALCULATE BASIS FUNCTIONS FOR INTERPOLATION ON A RECTANGLESSA1332
C      IF(IBOUND(J1,I,K).NE.0.AND.IBOUND(J,I1,K).NE.0.AND.
1          IBOUND(J1,I1,K).NE.0) THENSSA1333
C          RINT(3)=A*(DR-DRF)*DCFSSA1334
C          RINT(4)=A*DRF*DCFSSA1335
C          RINT(2)=A*DRF*(DC-DCF)SSA1336
C          RINT(1)=A*(DR-DRF)*(DC-DCF)SSA1337
C      ENDIFSSA1338
C      SSAL339
C      SSAL340
C      SSAL341
C      SSAL342
C      SSAL343
C      SSAL344
C      SSAL345
C      SSAL346
C      SSAL347
C      SSAL348
C      SSAL349
C      SSAL350
C      SSAL351
C      SSAL352

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RETURN	SSA1353
ENDIF	SSA1354
C	SSA1355
C---CALCULATE BASIS FUNCTIONS FOR INTERPOLATION ON A TRIANGLE	SSA1356
IF(IBOUND(J1,I,K).EQ.0) THEN	SSA1357
RINT(1)=A*(DR*DC - DR*DCF)	SSA1358
RINT(2)=0.	SSA1359
RINT(3)=A*(DR*DCF - DC*DRF)	SSA1360
RINT(4)=A*(DC*DRF)	SSA1361
RETURN	SSA1362
ENDIF	SSA1363
C	SSA1364
IF(IBOUND(J,I1,K).EQ.0) THEN	SSA1365
RINT(1)=A*(DR*DC - DC*DRF)	SSA1366
RINT(4)=A*(DR*DCF)	SSA1367
RINT(2)=A*(DC*DRF - DR*DCF)	SSA1368
RINT(3)=0.	SSA1369
RETURN	SSA1370
ENDIF	SSA1371
C	SSA1372
IF(IBOUND(J1,I1,K).EQ.0) THEN	SSA1373
RINT(1)=A*(DR*DC - DC*DRF - DR*DCF)	SSA1374
RINT(3)=A*(DR*DCF)	SSA1375
RINT(2)=A*(DC*DRF)	SSA1376
RINT(4)=0.	SSA1377
RETURN	SSA1378
ENDIF	SSA1379
END	SSA1380
C=====	SSJ0001
SUBROUTINE SSEN1J(	SSJ0002
1 IIP,B,NLL,CELS,NS,NSN,HNEW,NCOL,NROW,NLAY,	SSJ0003
2 NP,IP,KPER,ICH,NLL11)	SSJ0004
C---VERSION 1000 01FEB1992	SSJ0005
C *****	SSJ0006
C FOR PID=CH : PUT NEW CONSTANT HEAD VALUES IN HEAD ARRAY	SSJ0007
C *****	SSJ0008
C SPECIFICATIONS:	SSJ0009
C -----	SSJ0010
DOUBLE PRECISION HNEW(NCOL,NROW,NLAY)	SSJ0011
DIMENSION B(NP),CELS(4,NSN),NLL(NLL11)	SSJ0012
C -----	SSJ0013
C	SSJ0014
NL1=NLL(1)	SSJ0015
NL2=NLL(2)	SSJ0016
C-----DO NOT DO CALCULATIONS IF THIS ISN'T THE FIRST CALL FOR THIS	SSJ0017
C-----CONSTANT-HEAD SEQUENCE.	SSJ0018
IF(ICH.NE.0.OR.IP.GT.0) THEN	SSJ0019
IF(IP.GT.0.AND.ICH.EQ.0) NS=NS+NL1	SSJ0020
ICH=ICH+1	SSJ0021
IF(ICH.EQ.NL2) ICH=0	SSJ0022
RETURN	SSJ0023
ENDIF	SSJ0024
C-----CHECK TIMING	SSJ0025
IT=1	SSJ0026
NL3=NLL(3)	SSJ0027
IF((NL3.EQ.1.AND.KPER.NE.2).OR.	SSJ0028
1 ((NL3.EQ.0.OR.NL3.EQ.2).AND.KPER.NE.1)) THEN	SSJ0029
IF(ICH.EQ.0) NS=NS+NL1	SSJ0030
ICH=ICH+1	SSJ0031
IF(ICH.EQ.NL2) ICH=0	SSJ0032
RETURN	SSJ0033
ENDIF	SSJ0034
C-----INITIALIZE VARIABLES	SSJ0035
II=0	SSJ0036
N1=NS+1	SSJ0037
NS=NS+NL1	SSJ0038
IICH=0	SSJ0039
C-----GET LIMIT OF BACKWARD INTERP. (I) AND NEXT END-POINT	SSJ0040
C-----LOCATION (INCH)	SSJ0041
I1=N1	SSJ0042
15 I=0	SSJ0043
DO 20 INCH=I1,NS	SSJ0044
CE=CELS(4,INCH)	SSJ0045
IF(INCH.GT.N1) THEN	SSJ0046
CEM1=CELS(4,INCH-1)	SSJ0047
IF((CE.GT.0..AND.CE.LE.1.).AND.(CEM1.LT.0..OR.CEM1.GE.1.))	SSJ0048
1 I=INCH	SSJ0049
ENDIF	SSJ0050
IF(CE.GT.1..OR.CE.LT.0.) GO TO 21	SSJ0051
20 CONTINUE	SSJ0052
21 CONTINUE	SSJ0053

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C-----SAVE ROW AND COLUMN OF END POINT
      JC1=INT(CELS(2,INCH))
      IC1=INT(CELS(1,INCH))
C-----PUT PARAMETER VALUE IN HNEW
      IF(CE.GT.1.) THEN
        II=II+1
        DO 25 NL=4,NLLI1
          K=NLL(NL)
          IF(K.EQ.0) GO TO 26
          HNEW(JC1,IC1,K)=B(IIP-1+II)
25      CONTINUE
26      CONTINUE
      ENDIF
C-----INTERPOLATE BACKWARDS IF THERE ARE NONZERO COEFFICIENTS
      IF(I.NE.0.AND.I.LT.INCH) THEN
        JC2=INT(CELS(2,I-1))
        IC2=INT(CELS(1,I-1))
        DO 30 N=I,INCH-1
          P=CELS(4,N)
          JC=INT(CELS(2,N))
          IC=INT(CELS(1,N))
          DO 29 NL=4,NLLI1
            K=NLL(NL)
            IF(K.EQ.0) GO TO 30
            HNEW(JC,IC,K)=P*HNEW(JC1,IC1,K)+(1.-P)*HNEW(JC2,IC2,K)
29      CONTINUE
30      CONTINUE
      ENDIF
C-----DOES THE HEAD APPLY DIRECTLY TO A SERIES OF CELLS?
      IF(INCH.EQ.NS) GO TO 80
      I1=INCH+1
      DO 50 INCH=I1,NS
        IF(CELS(4,INCH).NE.1.) GO TO 51
        JC=INT(CELS(2,INCH))
        IC=INT(CELS(1,INCH))
        DO 35 NL=4,NLLI1
          K=NLL(NL)
          IF(K.EQ.0) GO TO 50
          HNEW(JC,IC,K)=HNEW(JC1,IC1,K)
35      CONTINUE
50      CONTINUE
C-----CHECK FOR LAST CH PARAMETER OF THIS GROUP
51 IF(INCH.EQ.NS.AND.II.EQ.NLL(2)) GO TO 80
      I1=INCH
      IICH=INCH-(NS-NLL)
      GO TO 15
80 ICH=1
      IF(NLL(2).EQ.1) ICH=0
      RETURN
      END

C=====SSJ0104
      SUBROUTINE SSENK(
1        PID,IIP,NLL,NNB,MXBN,BN,CELS,NSN,NS,NCOL,NROW,NLAY,I1BN,
2        IBOUND,NPER,KPER,B,IP,ISN,ISTRM,NLLI1,NLLIT)
C-----VERSION 1000 01FEB1992
C *****
C FOR PUMPING AND HEAD-DEPENDANT BOUNDARIES : PUT NEW PARAMETER
C VALUES IN MODEL ARRAYS
C *****
C SPECIFICATIONS:
C -----
C CHARACTER*4 PID
C DIMENSION BN(I1BN,MXBN),CELS(4,NSN),ISTRM(5,MXBN),
1 IBOUND(NCOL,NROW,NLAY),NLL(NLLI1)
C -----
C NL1=NLL(1)
C NL1A=IABS(NL1)
C NS1=NS+1
C NS=NS+NL1A
C ITS=KPER-1
C IF(ISN.GT.0.AND.IP.EQ.1) ITS=NPER-KPER
C-----LOOP THROUGH TIMES.
      DO 300 KT=1,NLLIT
C-----ONLY DO CALCULATIONS IF THE VALUE HAS CHANGED.
      IF((ISN.LT.0.OR.IP.NE.1).AND.NLL(2*KT).NE.ITS) GO TO 300
      IF((ISN.GT.0.AND.IP.EQ.1).AND.NLL(2*KT+1).NE.ITS) GO TO 300
      DO 200 II=NS1,NS
        K=CELS(1,II)
        I=CELS(2,II)
        J=CELS(3,II)

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IF(PID.NE.'KST '.AND.IBOUND(J,I,K).LE.0) GO TO 200          SSJ0135
DO 100 JJ=1,NNB                                              SSJ0136
  K1=BN(1,JJ)                                              SSJ0137
  I1=BN(2,JJ)                                              SSJ0138
  J1=BN(3,JJ)                                              SSJ0139
  IF((PID.NE.'KST '.AND.
1      K1.EQ.K .AND. I1.EQ.I .AND. J1.EQ.J)                SSJ0140
2      .OR.(PID.EQ.'KST '.AND.                             SSJ0141
3      ISTRM(4,JJ).EQ.K .AND. ISTRM(5,JJ).EQ.I))THEN      SSJ0142
    FACTOR=1.                                              SSJ0143
    IF(NL1.GT.0) FACTOR=CELS(4,I1)                        SSJ0144
    IF(PID.NE.'Q ' .AND.PID.NE.'KST ') BN(5,JJ)=FACTOR*B  SSJ0145
    IF(PID.EQ.'KST ') BN(3,JJ)=FACTOR*B                    SSJ0146
    IF(PID.EQ.'Q ' .AND.IP.EQ.0) BN(4,JJ)=FACTOR*B        SSJ0147
    ENDIF                                                  SSJ0148
100  CONTINUE                                              SSJ0149
200  CONTINUE                                              SSJ0150
300  CONTINUE                                              SSJ0151
    RETURN                                              SSJ0152
    END                                                  SSJ0153
    END                                                  SSJ0154

C=====SSJ0155
SUBROUTINE SSEN1M(                                          SSJ0156
1  PID,C,SMAT,NCOL,NROW,NLAY,NSM,NM,NLL,B,KPER,IP,DELR,DELC, SSJ0157
2  IBOUND,ISN,NMM,NZM,LZ1L,SFAC,LZ,LM,MATZ,NLL1L,NLLIT)    SSJ0158
C-----VERSION 1000 01FEB1992                             SSJ0159
C *****SSJ0160
C FOR PID=KV,S1,RCH,ETM,TKV : PUT NEW PARAMETER VALUES IN MODEL SSJ0161
C          ARRAYS                                           SSJ0162
C *****SSJ0163
C SPECIFICATIONS:                                          SSJ0164
C -----SSJ0165
CHARACTER*4 PID                                           SSJ0166
DIMENSION C(NCOL,NROW,NLAY),SMAT(NCOL,NROW,NMM),NLL(NLL1L), SSJ0167
1  DELR(NCOL),DELC(NROW),IBOUND(NCOL,NROW,NLAY),LM(NSM),    SSJ0168
2  MATZ(NCOL,NROW,NZM),SFAC(NSM),LZ(LZ1L,NSM)              SSJ0169
C -----SSJ0170
C NL2=NLL1L                                              SSJ0171
NT=1                                                       SSJ0172
IF(PID.EQ.'RCH '.OR.PID.EQ.'ETM ') THEN                  SSJ0173
  NL2=1                                                    SSJ0174
  NT=NLLIT                                                 SSJ0175
  ITS=KPER-1                                                SSJ0176
  IF(ISN.GT.0.AND.IP.EQ.1) ITS=NPER-KPER                  SSJ0177
ENDIF                                                       SSJ0178
C-----LOOP THROUGH LAYERS                               SSJ0179
DO 90 LL=1,NL2                                           SSJ0180
  NLO=NLL(LL)                                              SSJ0181
  IF(NLO.GT.0) NM=NM+1                                     SSJ0182
  IF(PID.EQ.'TKV '.AND.MOD(LL+1,3).EQ.0) GO TO 90         SSJ0183
C-----TIME INVARIANT PARAMETERS: FOR KPER>1, JUST KEEP TRACK OF NM.SSJ0184
  IF(PID.EQ.'KV '.OR.PID.EQ.'TKV '.OR.PID.EQ.'S1 ') THEN SSJ0185
    IF(KPER.GT.1.OR.IP.GT.0) GO TO 90                      SSJ0186
    IF(NLO.EQ.0.AND.PID.EQ.'TKV ') GO TO 90                SSJ0187
    IF(NLO.EQ.0) GO TO 95                                  SSJ0188
  ENDIF                                                    SSJ0189
  NL=IABS(NLO)                                             SSJ0190
  IF(PID.EQ.'RCH '.OR.PID.EQ.'ETM ') NL=1                SSJ0191
C-----LOOP THROUGH TIMES FOR RCH AND ETM; NT=1 FOR OTHER PID'S SSJ0192
DO 85 K=1,NT                                              SSJ0193
C-----APPLICABLE THIS TIME STEP?                        SSJ0194
  IF((PID.EQ.'RCH '.OR.PID.EQ.'ETM ').AND.                SSJ0195
1  (ITS.GT.NLL(2*K+1).OR.ITS.LT.NLL(2*K))) GO TO 85      SSJ0196
  IF(NLO.GT.0) THEN                                        SSJ0197
    SF=SFAC(NM)*B                                          SSJ0198
    M=LM(NM)                                               SSJ0199
    LZ1=LZ(1,NM)                                           SSJ0200
    LZN=2                                                    SSJ0201
    IF(LZ1.NE.0) LZN=LZ1L                                  SSJ0202
    DO 15 IZ=2,LZN                                         SSJ0203
      IF(LZ1.NE.0)THEN                                     SSJ0204
        NZ=LZ(IZ,NM)                                       SSJ0205
        IF(NZ.EQ.0) GO TO 20                               SSJ0206
      ENDIF                                                 SSJ0207
      DO 10 I=1,NROW                                       SSJ0208
        DO 10 J=1,NCOL                                     SSJ0209
          CO=0.0                                           SSJ0210
          IF(LZ1.EQ.0) THEN                                  SSJ0211
            IF(M.EQ.0) CO=SF*DELR(J)*DELC(I)              SSJ0212
            IF(M.NE.0.AND.SMAT(J,I,M).NE.0.)              SSJ0213
1          CO=SF*SMAT(J,I,M)*DELR(J)*DELC(I)              SSJ0214
          ELSE                                              SSJ0215

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      IF(MATZ(J,I,LZ1).EQ.NZ) THEN
      IF(M.EQ.0) CO=SF*DELR(J)*DELC(I)
      IF(M.NE.0.AND.SMAT(J,I,M).NE.0.)
1      CO=SF*SMAT(J,I,M)*DELR(J)*DELC(I)
      ENDIF
      ENDIF
      IF(CO.NE.0..AND.(PID.EQ.'KV '.OR.
1      (PID.EQ.'TKV '.AND.MOD(LL+1,3).NE.0))) THEN
      IF(PID.EQ.'KV '.OR.MOD(LL,3).EQ.0) THEN
      CNL=C(J,I,NL)
      IF(CNL.EQ.0.) C(J,I,NL)=CO
      IF(CNL.NE.0.) C(J,I,NL)=1./((1./CNL) + 1./CO)
      ELSEIF (MOD(LL+2,3).EQ.0) THEN
      CNLM=C(J,I,NL-1)
      IF(CNLM.EQ.0.) C(J,I,NL-1)=CO
      IF(CNLM.NE.0.) C(J,I,NL-1)=1./((1./CNLM) + 1./CO)
      ENDIF
      ELSEIF (CO.NE.0.) THEN
      C(J,I,NL)=C(J,I,NL)+CO
      ENDIF
10      CONTINUE
15      CONTINUE
20      CONTINUE
      ENDIF
      IF(NLO.LT.0) THEN
      DO 80 I=1,NROW
      DO 80 J=1,NCOL
      IF(IBOUND(J,I,NL).GT.0.OR.PID.EQ.'RCH '.OR.PID.EQ.'ETM ')
1      THEN
      IF((PID.EQ.'KV '.OR.PID.EQ.'TKV ').AND.
1      CO.NE.0..AND.(C(J,I,NL).NE.0..OR.
1      (PID.EQ.'TKV '.AND.MOD(LL+2,3).EQ.0.AND.
1      C(J,I,NL-1).NE.0.)) THEN
      IF(PID.EQ.'TKV '.AND.MOD(LL+2,3).EQ.0) THEN
      C(J,I,NL-1)=1./
1      ((1./C(J,I,NL-1)) + 1./(B*DELR(J)*DELC(I)))
      ELSE
      C(J,I,NL)=1./
1      ((1./C(J,I,NL)) + 1./(B*DELR(J)*DELC(I)))
      ENDIF
      ELSE
      C(J,I,NL)=C(J,I,NL)+(B*DELR(J)*DELC(I))
      ENDIF
      ENDIF
80      CONTINUE
      ENDIF
85      CONTINUE
90      CONTINUE
95      CONTINUE
      RETURN
      END
C=====
      SUBROUTINE SSEN1N(
1      H,HOLD,A,NC,NR,NL,ST,DELR,DELC,IBOUND,TRPY,
2      RHS,SHOLD,BOT,CR,CC,K,ISN,KB,X,NP)
C-----VERSION 1000 01FEB1992
C      *****
C      ADD NONLINEAR TERMS FOR SENSITIVITY EQUATION CALCULATIONS
C      *****
C      SPECIFICATIONS:
C      -----
      DOUBLE PRECISION A(NC*NR*NL),AO,AP
      DIMENSION H(NC*NR*NL),CR(NC,NR,NL),CC(NC,NR,NL),ST(NC,NR,NL),
1      DELR(NC),DELC(NR),RHS(NC,NR,NL),IBOUND(NC,NR,NL),TRPY(NL),
2      HOLD(NC*NR*NL),SHOLD(NC*NR*NL),BOT(NC,NR,NL),X(NP,1)
      COMMON /FLWCOM/LAYCON(80)
C      -----
C      NRC = NR*NC
      NRCL = NR*NC*NL
      NR1=NR-1
      NC1=NC-1
C      YX=TRPY(K)*2.
      LT=LAYCON(K)
C      CR
C      IF(NC.GT.1) THEN
      DO 300 I=1,NR
      DO 300 J=1,NC1
      IF( IBOUND(J,I,K).EQ.0.OR.IBOUND(J+1,I,K).EQ.0) GO TO 300
      IND=J+NC*(I-1)+NRC*(K-1)

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        IF( IBOUND(J,I,K).EQ.0.OR.IBOUND(J+1,I,K).EQ.0) GO TO 300      SSJ0297
        IND=J+NC*(I-1)+NRC*(K-1)                                       SSJ0298
        AO=A(IND)                                                         SSJ0299
        AP=A(IND+1)                                                       SSJ0300
        HO=H(IND)                                                         SSJ0301
        HP=H(IND+1)                                                       SSJ0302
        BO=BOT(J,I,KB)                                                   SSJ0303
        BP=BOT(J+1,I,KB)                                                 SSJ0304
        TH1=HO-BO                                                         SSJ0305
        TH2=HP-BP                                                         SSJ0306
C-----MATRIX DERIVATIVES                                              SSJ0307
        D1CR=(CR(J,I,K)**2)*DEL(R(J)/                                  SSJ0308
1          (2.*DEL(C(I)*ST(J,I,K)*(TH1**2))                             SSJ0309
        D2CR=(CR(J,I,K)**2)*DEL(R(J+1)/                                SSJ0310
1          (2.*DEL(C(I)*ST(J+1,I,K)*(TH2**2))                             SSJ0311
C-----MULTIPLY BY SENSITIVITIES FROM LAST ITERATION                  SSJ0312
        CO=0.                                                             SSJ0313
        CO=D1CR*AO+D2CR*AP                                              SSJ0314
C-----MULTIPLY BY HEAD VECTOR AND ADD TO RHS                         SSJ0315
        RHS(J,I,K)=RHS(J,I,K)-CO*(HP-HO)                               SSJ0316
        RHS(J+1,I,K)=RHS(J+1,I,K)-CO*(HO-HP)                           SSJ0317
300    CONTINUE                                                         SSJ0318
        ENDIF                                                            SSJ0319
C                                                                           SSJ0320
C    CC                                                                  SSJ0321
C                                                                           SSJ0322
        IF(NR.GT.1) THEN                                                SSJ0323
            DO 330 J=1,NC                                                SSJ0324
            DO 330 I=1,NR1                                              SSJ0325
                IF( IBOUND(J,I,K).EQ.0.OR.IBOUND(J,I+1,K).EQ.0) GO TO 330 SSJ0326
                IND=J+NC*(I-1)+NRC*(K-1)                               SSJ0327
                HO=H(IND)                                               SSJ0328
                HP=H(IND+NC)                                           SSJ0329
                AO=A(IND)                                               SSJ0330
                AP=A(IND+NC)                                           SSJ0331
                BO=BOT(J,I,KB)                                         SSJ0332
                BP=BOT(J,I+1,KB)                                       SSJ0333
                TH1=HO-BO                                              SSJ0334
                TH2=HP-BP                                              SSJ0335
C-----MATRIX DERIVATIVES                                              SSJ0336
                D1CC=(CC(J,I,K)**2)*DEL(C(I)/                          SSJ0337
1                  (2.*DEL(R(J)*ST(J,I,K)*(TH1**2))                     SSJ0338
                D2CC=(CC(J,I,K)**2)*DEL(C(I+1)/                        SSJ0339
1                  (2.*DEL(R(J)*ST(J,I+1,K)*(TH2**2))                     SSJ0340
C-----MULTIPLY BY DERIVATIVES FROM LAST ITERATION                  SSJ0341
                CO=0.                                                  SSJ0342
                CO=D1CC*AO+D2CC*AP                                      SSJ0343
C-----MULTIPLY BY HEAD VECTOR AND ADD TO RHS                         SSJ0344
                RHS(J,I,K)=RHS(J,I,K)-CO*(HP-HO)                     SSJ0345
                RHS(J,I+1,K)=RHS(J,I+1,K)-CO*(HO-HP)                 SSJ0346
330    CONTINUE                                                         SSJ0347
        ENDIF                                                            SSJ0348
        RETURN                                                           SSJ0349
        END                                                              SSJ0350

C=====SSJ0351
        SUBROUTINE SSEN10(                                             SSJ0352
1          NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBS,WT,DID,NDER,ROFF,COFF,   SSJ0353
2          TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,RSQ,RSQP,IO,LN,RSQH,NPO) SSJ0354
C-----VERSION 1000 01FEB1992                                         SSJ0355
C *****SSJ0356
C    CALCULATE AND PRINT WEIGHTED RESIDUALS FOR DEPENDENT-VARIABLE     SSJ0357
C    OBSERVATIONS, PRIOR PARAMETER ESTIMATES BY PARAMETER GROUPS,     SSJ0358
C    AND PRIOR ESTIMATES OF PARAMETER SUMS.                             SSJ0359
C *****SSJ0360
C    SPECIFICATIONS:                                                    SSJ0361
C -----SSJ0362
        CHARACTER*4 PID(NP),DID(ND)                                     SSJ0363
        DIMENSION B(NPO),IWPG(NP),B1(NPO),WP(NPO+MPR),H(ND),HOBS(ND), SSJ0364
1          WT(ND),NDER(5,ND),ROFF(NH),COFF(NH),TOFF(NH),IQOB(NQT),   SSJ0365
2          PRM(NPO+1,MPR),LN(NP)                                       SSJ0366
C -----SSJ0367
C                                                                           SSJ0368
580 FORMAT(/,' PARAMETERS WITH PRIOR INFORMATION, BY GROUP',//,      SSJ0369
1          ' PARAMETER          VALUES          ',9X,'WEIGHT ',    SSJ0370
1          ' WEIGHTED'                                                SSJ0371
1          ' ,/,', # PID MEAS. CALC. RESIDUAL **5 ',              SSJ0372
1          ' RESIDUAL')                                              SSJ0373
585 FORMAT(I4,3X,A4,E10.3,1X,E10.3,1X,E10.3,1X,G10.3,1X,G10.3)      SSJ0374
620 FORMAT(/,' DATA FOR FLOWS',//,7X,                               SSJ0375
1          ' TIME MEAS. CALC.',28X,'WEIGHTED',/,                    SSJ0376
1          ' OBS# ID STEP FLOW ',/,                                  SSJ0377

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1 'FLOW',6X,'RESIDUAL',3X,'WEIGHT**5',2X,'RESIDUAL',/) SSJ0378
625 FORMAT(1X,I5,3X,A4,I4,4X,G11.3) SSJ0379
630 FORMAT(1X,I5,3X,A4,I4,4X,G11.3,' DISCONNECTED') SSJ0380
635 FORMAT(/,' DATA AT HEAD LOCATIONS',/) SSJ0381
637 FORMAT(28X,'TIME ROW/COL/TIME MEAS.',6X, SSJ0382
1 'CALC.',24X,'WEIGHTED',/, SSJ0383
1 'OBS# ID LAYER,ROW,COL STEP OFFSETS',10X,'HEAD',7X, SSJ0384
1 'HEAD',2X,'RESIDUAL',2X,'WEIGHT**5',3X,'RESIDUAL',/) SSJ0385
640 FORMAT(I5,1X,A4,3X,3I4,I6,3X,3F5.2,F11.3,F11.3,3G11.3) SSJ0386
645 FORMAT(I5,1X,A4,3X,3I4,I6,3X,3F5.2,F11.3,' DRY') SSJ0387
650 FORMAT(/,' PARAMETER SUMS WITH PRIOR INFORMATION',/, SSJ0388
1 19X,'VALUES',24X,'WEIGHT WEIGHTED',/, SSJ0389
1 4X,'EQ.#',7X,'MEAS.',4X,'CALC.',5X,'RESIDUAL',8X,'**5',3X, SSJ0390
1 'RESIDUAL') SSJ0391
660 FORMAT(I7,4X,E10.3,1X,E10.3,1X,E10.3,1X,G10.3,1X,G10.3) SSJ0392
665 FORMAT(/,' SUM OF SQUARED WEIGHTED RESIDUALS (HEADS) ', SSJ0393
1 G11.5) SSJ0394
670 FORMAT(/,' SUM OF SQUARED WEIGHTED RESIDUALS (ALL DEP. VAR.) ', SSJ0395
1 G11.5) SSJ0396
675 FORMAT(' SUM OF SQUARED WEIGHTED RESIDUALS (WITH PARAMETERS) ', SSJ0397
1 G11.5) SSJ0398
680 FORMAT(' STATISTICS FOR THESE RESIDUALS :',/, SSJ0399
2 ' MAXIMUM WEIGHTED RESIDUAL :',E10.3,' OBS#',I7,/, SSJ0400
3 ' MINIMUM WEIGHTED RESIDUAL :',E10.3,' OBS#',I7,/, SSJ0401
4 ' AVERAGE WEIGHTED RESIDUAL :',E10.3,/, SSJ0402
X ' # RESIDUALS >= 0. :',I7,/, ' # RESIDUALS < 0. :',I7,/, SSJ0403
5 ' NUMBER OF RUNS :',I5,' IN',I5,' OBSERVATIONS') SSJ0404
685 FORMAT(' STATISTICS FOR ALL RESIDUALS :',/, SSJ0405
1 ' AVERAGE WEIGHTED RESIDUAL :',E10.3,/, SSJ0406
2 ' # RESIDUALS >= 0. :',I7,/, ' # RESIDUALS < 0. :',I7,/, SSJ0407
3 ' NUMBER OF RUNS :',I5,' IN',I5,' OBSERVATIONS') SSJ0408
690 FORMAT(' RUNS STATISTIC (TOO FEW RUNS):',G13.3,/, SSJ0409
1 ' (IF #NEG>10 AND #POS>10, P(STAT < -1.28) = 0.10,',/, SSJ0410
2 ' P(STAT < -1.645) = 0.05,',/, SSJ0411
3 ' P(STAT < -1.96) = 0.025)',/, SSJ0412
4 ' RUNS STATISTIC (TOO MANY RUNS):',G13.3,/, SSJ0413
5 ' (IF #NEG>10 AND #POS>10, P(STAT > 1.28) = 0.10,',/, SSJ0414
6 ' P(STAT > 1.645) = 0.05,',/, SSJ0415
7 ' P(STAT > 1.96) = 0.025)') SSJ0416
695 FORMAT(' STATISTICS FOR THESE RESIDUALS :',/, SSJ0417
1 ' MAXIMUM WEIGHTED RESIDUAL :',E10.3,/, SSJ0418
2 ' MINIMUM WEIGHTED RESIDUAL :',E10.3,/, SSJ0419
3 ' AVERAGE WEIGHTED RESIDUAL :',E10.3,/, SSJ0420
4 ' # RESIDUALS >= 0. :',I7,/, ' # RESIDUALS < 0. :',I7,/, SSJ0421
5 ' NUMBER OF RUNS :',I5,' IN',I5,' OBSERVATIONS') SSJ0422
C SSJ0423
RSQ=0. SSJ0424
RSQP=0. SSJ0425
NNEG=0 SSJ0426
NPOST=0 SSJ0427
AVET=0. SSJ0428
JDRY=0 SSJ0429
IDIS=0 SSJ0430
NRUNS=1 SSJ0431
C-----HEADS SSJ0432
IF(NH.GT.0) THEN SSJ0433
IF(IO.EQ.1) WRITE(IOUT,635) SSJ0434
NNEG=0 SSJ0435
NPOS=0 SSJ0436
VMAX=-1.E20 SSJ0437
VMIN=1.E20 SSJ0438
AVE=0. SSJ0439
IF(IO.EQ.1) WRITE(IOUT,637) SSJ0440
DO 160 N=1,NH SSJ0441
RES=HOBS(N)-H(N) SSJ0442
W=WT(N) SSJ0443
IF(W.LT.0.) THEN SSJ0444
WRITE(IOUT,645) N,DID(N),(NDER(J,N),J=1,4), SSJ0445
ROFF(N),COFF(N),TOFF(N) SSJ0446
1 JDRY=JDRY+1 SSJ0447
GO TO 160 SSJ0448
ENDIF SSJ0449
WT2=SQRT(W) SSJ0450
WTR=RES*WT2 SSJ0451
IF(IO.EQ.1) WRITE(IOUT,640) N,DID(N),(NDER(J,N),J=1,4), SSJ0452
ROFF(N),COFF(N),TOFF(N),HOBS(N),H(N),RES,WT2,WTR SSJ0453
1 RSQ=RSQ+(WTR**2) SSJ0454
IF(WTR.GT.VMAX) THEN SSJ0455
VMAX=WTR SSJ0456
NMAX=N SSJ0457
ENDIF SSJ0458
IF(WTR.LT.VMIN) THEN SSJ0459
VMIN=WTR SSJ0460

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        NMIN=N
        ENDIF
        IF(WTR.GE.0.) NPOS=NPOS+1
        IF(WTR.LT.0.) NNEG=NNEG+1
        IF(N.GT.1.AND.(WTRL*WTR).LT.0.) NRUNS=NRUNS+1
        WTRL=WTR
        AVE=AVE+WTR
160  CONTINUE
        IF(JDRY.NE.NH) THEN
            AVET=AVET+AVE
            NPOST=NPOST+NPOS
            NNEG=NNEG+NNEG
            AVE=AVE/REAL(NH-JDRY)
            IF(IO.EQ.1) WRITE(IOUT,680) VMAX,NMAX,VMIN,NMIN,AVE,
1          NPOS,NNEG,NRUNS,NH
            IF(IO.EQ.1) WRITE(IOUT,665) RSQ
        ENDIF
        ENDIF
        RSQH=RSQ
C-----HEAD-DEPENDENT FLOWS
        IF(NQT.GT.0) THEN
            IF(IO.EQ.1) WRITE(IOUT,620)
            NNEG=0
            NPOS=0
            VMAX=-1.E20
            VMIN=1.E20
            AVE=0.
            NH1=NH+1
            NH2=NH+NQT
            DO 170 N=NH1,NH2
                RES=HOBS(N)-H(N)
                W=WT(N)
                IF(W.LT.0.) THEN
                    WRITE(IOUT,630) N,DID(N),IQOB(N-NH),HOBS(N)
                    IDIS=IDIS+1
                    GO TO 170
                ENDIF
                WT2=SQRT(W)
                WTR=RES*WT2
                IF(IO.EQ.1) WRITE(IOUT,625) N,DID(N),IQOB(N-NH),HOBS(N),
1              H(N),RES,WT2,WTR
                RSQ=RSQ+(WTR**2)
                IF(WTR.GT.VMAX) THEN
                    VMAX=WTR
                    NMAX=N
                ENDIF
                IF(WTR.LT.VMIN) THEN
                    VMIN=WTR
                    NMIN=N
                ENDIF
                IF(WTR.GE.0.) NPOS=NPOS+1
                IF(WTR.LT.0.) NNEG=NNEG+1
                IF(N.GT.1.AND.(WTRL*WTR).LT.0.) NRUNS=NRUNS+1
                WTRL=WTR
                AVE=AVE+WTR
170  CONTINUE
                N=N-1
                IF(NQT.NE.IDIS) THEN
                    AVET=AVET+AVE
                    NPOST=NPOST+NPOS
                    NNEG=NNEG+NNEG
                    AVE=AVE/REAL(NQT-IDIS)
                    IF(IO.EQ.1) WRITE(IOUT,680) VMAX,NMAX,VMIN,NMIN,AVE,
1              NPOS,NNEG,NRUNS,N
                    IF(IO.EQ.1) WRITE(IOUT,670) RSQ
                ENDIF
            ENDIF
C-----PRINT WEIGHTED RESIDUALS FOR PRIOR INFORMATION ON INDIVIDUAL
C-----PARAMETERS BY PARAMETER GROUP
            RSQP=RSQ
            IF(IPAR.GT.0.AND.NPR.GT.0) THEN
                IF(IO.EQ.1) WRITE(IOUT,580)
                NNEG=0
                NPOS=0
                VMAX=-1.E20
                VMIN=1.E20
                AVE=0.
                DO 327 IG=1,NP
                    II=0
                    DO 326 IP=1,NP
                        IF(IWPG(IP).EQ.IG.AND.WP(IP).GT.0.) THEN
                            II=1
                            WPSR=WP(IP)**.5
SSJ0461
SSJ0462
SSJ0463
SSJ0464
SSJ0465
SSJ0466
SSJ0467
SSJ0468
SSJ0469
SSJ0470
SSJ0471
SSJ0472
SSJ0473
SSJ0474
SSJ0475
SSJ0476
SSJ0477
SSJ0478
SSJ0479
SSJ0480
SSJ0481
SSJ0482
SSJ0483
SSJ0484
SSJ0485
SSJ0486
SSJ0487
SSJ0488
SSJ0489
SSJ0490
SSJ0491
SSJ0492
SSJ0493
SSJ0494
SSJ0495
SSJ0496
SSJ0497
SSJ0498
SSJ0499
SSJ0500
SSJ0501
SSJ0502
SSJ0503
SSJ0504
SSJ0505
SSJ0506
SSJ0507
SSJ0508
SSJ0509
SSJ0510
SSJ0511
SSJ0512
SSJ0513
SSJ0514
SSJ0515
SSJ0516
SSJ0517
SSJ0518
SSJ0519
SSJ0520
SSJ0521
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SSJ0537
SSJ0538
SSJ0539
SSJ0540
SSJ0541
SSJ0542
SSJ0543

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BB=B(IP)
BB1=B1(IP)
IF(LN(IP).NE.0) THEN
  BB=ALOG(B(IP))
  BB1=EXP(B1(IP))
ENDIF
BDIF=B1(IP)-BB
BWP=BDIF*WPSR
IF(IO.EQ.1) WRITE(IOUT,585) IP,PID(IP),BB1,B(IP),BDIF,
1 WPSR,BWP
RSQP=RSQP+(BWP**2)
IF(BWP.GT.VMAX) VMAX=BWP
IF(BWP.LT.VMIN) VMIN=BWP
IF(BWP.GE.0.) NPOS=NPOS+1
IF(BWP.LT.0.) NNEG=NNEG+1
N=N+1
IF(N.GT.1.AND.(WTRL*BWP).LT.0.) NRUNS=NRUNS+1
WTRL=BWP
AVE=AVE+BWP
ENDIF
326 CONTINUE
327 CONTINUE
AVET=AVET+AVE
NPOST=NPOST+NPOS
NNEGT=NNEGT+NNEG
AVE=AVE/REAL(NPR)
IF(IO.EQ.1) WRITE(IOUT,695) VMAX,VMIN,AVE,NPOS,NNEG,NRUNS,N
ENDIF
C-----PRINT WEIGHTED RESIDUALS FOR PRIOR INFORMATION ON PARAMETER SUMS
IF(IPAR.GT.0.AND.MPR.GT.0) THEN
  IF(IO.EQ.1) WRITE(IOUT,650)
  NNEG=0
  NPOS=0
  VMAX=-1.E20
  VMIN=1.E20
  AVE=0.
  DO 350 IMP=1,MPR
    TEMP=0.
    LFLAG=0
    DO 340 IIP=1,NPO
      IF(PRM(IIP,IMP).NE.0.AND.LN(IIP).GT.0) LFLAG=1
      TEMP=TEMP+PRM(IIP,IMP)*B(IIP)
340 CONTINUE
      WPSR=WP(NPO+IMP)**.5
      TEMPl=PRM(NPO+1,IMP)
      TEMPlE=TEMPl
      TEMPl=TEMP
      IF(LFLAG.NE.0) THEN
        TEMPlE=ALOG(TEMP)
        TEMPlE=EXP(TEMPlE)
      ENDIF
      BDIF=TEMPl-TEMPlE
      BWP=BDIF*WPSR
      IF(IO.EQ.1) WRITE(IOUT,660) IMP,TEMPlE,TEMP,BDIF,WPSR,BWP
      RSQP=RSQP+(BWP**2)
      IF(BWP.GT.VMAX) VMAX=BWP
      IF(BWP.LT.VMIN) VMIN=BWP
      IF(BWP.GE.0.) NPOS=NPOS+1
      IF(BWP.LT.0.) NNEG=NNEG+1
      N=N+1
      IF(N.GT.1.AND.(WTRL*BWP).LT.0.) NRUNS=NRUNS+1
      WTRL=BWP
      AVE=AVE+BWP
350 CONTINUE
      AVET=AVET+AVE
      NPOST=NPOST+NPOS
      NNEGT=NNEGT+NNEG
      AVE=AVE/REAL(MPR)
      IF(IO.EQ.1) WRITE(IOUT,695) VMAX,VMIN,AVE,NPOS,NNEG,NRUNS,N
    ENDIF
  C-----FINAL PRINTOUT
  WRITE(IOUT,670) RSQ
  IF(IPAR.GT.0.AND.NPR+MPR.GT.0) WRITE(IOUT,675) RSQP
  IF(IO.EQ.1) THEN
    AVET=AVET/REAL(NH+NQT+NPR+MPR-JDRY-IDIS)
    RP=REAL(NPOST)
    RN=REAL(NNEGT)
    RNP=2.*RP*RN
    RNS=RP+RN
    RNR=REAL(NRUNS)
    IF(RNP.GT.0.) THEN
      ERUNS=(RNP/RNS)+1.0
      SDRUNS=((RNP*(RNP-RNS))/((RNS**2.)*(RNS-1.))**.5

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SSJ0626



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STRUNS=(RNR-ERUNS+.5)/SDRUNS                      SSJ0627
ST2RUNS=(RNR-ERUNS-.5)/SDRUNS                      SSJ0628
WRITE(IOUT,685) AVET,NPOST,NNEGT,NRUNS,N           SSJ0629
WRITE(IOUT,690) STRUNS,ST2RUNS                     SSJ0630
ELSE                                                 SSJ0631
WRITE(IOUT,685) AVET,NPOST,NNEGT,NRUNS,N           SSJ0632
ENDIF                                                SSJ0633
ENDIF                                                SSJ0634
RETURN                                              SSJ0635
END                                                  SSJ0636

C=====SSJ0637
SUBROUTINE SSEN1P(                                SSJ0638
1  SMAT,NLL,NSM,NM,H,HOLD,A,NC,NR,NL,KPER,NPER,PID,ST,DELR, SSJ0639
2  DELC,IBOUND,TRPY,DELT,XX,ISN,RHS,SHOLD,BOT,DD,IHES,B,LN, SSJ0640
3  SCL,NMM,NZM,LZ1L,SFAC,LZ,LM,MATZ,NLL1L,CV) SSJ0641
C-----VERSION 1000 01FEB1992                      SSJ0642
C *****SSJ0643
C CALCULATE MATRIX DERIVATIVES AND MULTIPLY BY HEADS AND ADJOINTS SSJ0644
C STATES, AS NEEDED. ADD RESULTING CONTRIBUTION TO THE ADJOINT- SSJ0645
C STATE SENSITIVITIES OR, FOR THE SENSITIVITY-EQUATION METHOD, TO SSJ0646
C RHS. SSJ0647
C *****SSJ0648
C SPECIFICATIONS: SSJ0649
C -----SSJ0650
CHARACTER*4 PID,PID1 SSJ0651
DOUBLE PRECISION A(NC*NR*NL),DD,XX SSJ0652
DIMENSION SMAT(NC,NR,NMM),NLL(NLL1L),H(NC*NR*NL),ST(NC,NR,NL), SSJ0653
1  DELR(NC),DELC(NR),RHS(NC,NR,NL),IBOUND(NC,NR,NL),TRPY(NL), SSJ0654
2  HOLD(NC*NR*NL),SHOLD(NC*NR*NL),BOT(NC,NR,NL),CV(NC,NR,NL), SSJ0655
3  MATZ(NC,NR,NZM),LZ(LZ1L,NSM),SFAC(NSM),LM(NSM) SSJ0656
COMMON /FLWCOM/LAYCON(80) SSJ0657
C -----SSJ0658
C NRC=NR*NC SSJ0659
C NR1=NR-1 SSJ0660
C NC1=NC-1 SSJ0661
C SSJ0662
C SSJ0663
DO 390 LL=1,NLL1L SSJ0664
  IL=NLL(LL) SSJ0665
  IF(IL.EQ.0) THEN SSJ0666
    IF(PID.EQ.'TKV ') GO TO 390 SSJ0667
    GO TO 400 SSJ0668
  ENDIF SSJ0669
  IF(IL.GT.0.AND.PID.NE.'ANI '.AND.PID.NE.'ANIV') THEN SSJ0670
    NM=NM+1 SSJ0671
    SF=SFAC(NM) SSJ0672
    LZ1=LZ(1,NM) SSJ0673
    M=LM(NM) SSJ0674
  ENDIF SSJ0675
  K=IABS(IL) SSJ0676
  IF(PID.EQ.'TKV '.AND.MOD(LL+2,3).EQ.0) K=K-1 SSJ0677
  LT=LAYCON(K) SSJ0678
  IF(LT.EQ.1) THEN SSJ0679
    KB=0 SSJ0680
    DO 210 KK=1,K SSJ0681
      IF(LAYCON(KK).EQ.1) KB=KB+1 SSJ0682
    CONTINUE SSJ0683
  ENDIF SSJ0684
  PID1=PID SSJ0685
  IF(PID.EQ.'TKV ') THEN SSJ0686
    IF(MOD(LL+1,3).EQ.0) THEN SSJ0687
      PID='T' SSJ0688
    ELSE SSJ0689
      PID='KV' SSJ0690
    ENDIF SSJ0691
  ENDIF SSJ0692
C-----HORIZONTAL CONDUCTANCES SSJ0693
IF(PID.EQ.'T '.OR.PID.EQ.'ANI ') THEN SSJ0694
  YX=TRPY(K)*2. SSJ0695
  DO 330 I=1,NR SSJ0696
    DO 330 J=1,NC SSJ0697
      IF(IBOUND(J,I,K).EQ.0) GO TO 330 SSJ0698
      IND=J+NC*(I-1)+NRC*(K-1) SSJ0699
      HO=H(IND) SSJ0700
      DR=DELR(J) SSJ0701
      DC=DELC(I) SSJ0702
      R0=0.0 SSJ0703
      SMAT0=1. SSJ0704
      IF(IL.GT.0.AND.PID.NE.'ANI ') THEN SSJ0705
        IF(M.EQ.0) SMAT0=SF SSJ0706
        IF(M.GT.0) SMAT0=SF*SMAT(J,I,M) SSJ0707
      ENDIF
    END DO
  END DO

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	IF(SMAT0.NE.0..AND.LZ1.GT.0) THEN	SSJ0708
	IFLAG0=0	SSJ0709
	DO 250 IZ=2,LZ11	SSJ0710
	NZ=LZ(IZ,NM)	SSJ0711
	IF(NZ.EQ.0.OR.IFLAG0.EQ.1) GO TO 255	SSJ0712
	IF(MATZ(J,I,LZ1).EQ.NZ) IFLAG0=1	SSJ0713
250	CONTINUE	SSJ0714
255	IF(IFLAG0.EQ.0) SMAT0=0.	SSJ0715
	ENDIF	SSJ0716
	ENDIF	SSJ0717
	IF(LT.EQ.1) TH1=HO-BOT(J,I,KB)	SSJ0718
C-----CR		SSJ0719
	IF(IBOUND(J+1,I,K).EQ.0.OR.PID.EQ.'ANI '.OR.J.EQ.NC)	SSJ0720
1	GO TO 300	SSJ0721
	SMAT1=1.	SSJ0722
	IF(IL.GT.0) THEN	SSJ0723
	IF(M.EQ.0) SMAT1=SF	SSJ0724
	IF(M.GT.0) SMAT1=SF*SMAT(J+1,I,M)	SSJ0725
	IF(SMAT1.NE.0..AND.LZ1.GT.0) THEN	SSJ0726
	IFLAG1=0	SSJ0727
	DO 270 IZ=2,LZ11	SSJ0728
	NZ=LZ(IZ,NM)	SSJ0729
	IF(NZ.EQ.0.OR.IFLAG1.EQ.1) GO TO 275	SSJ0730
	IF(MATZ(J+1,I,LZ1).EQ.NZ) IFLAG1=1	SSJ0731
270	CONTINUE	SSJ0732
275	IF(IFLAG1.EQ.0) SMAT1=0.	SSJ0733
	ENDIF	SSJ0734
	ENDIF	SSJ0735
	IF((IL.GT.0).AND.(SMAT0.EQ.0..AND.SMAT1.EQ.0.))	SSJ0736
1	GO TO 300	SSJ0737
	HP=H(IND+1)	SSJ0738
	DR1=DELR(J+1)	SSJ0739
	IF(LT.EQ.1) TH2=HP-BOT(J+1,I,KB)	SSJ0740
	IF(IL.LT.0.OR.(SMAT0.GT.0..AND.SMAT1.GT.0.))	SSJ0741
1	THEN	SSJ0742
	IF(LT.EQ.0) THEN	SSJ0743
	IF(IL.GT.0) THEN	SSJ0744
	T1=SMAT0	SSJ0745
	T2=SMAT1	SSJ0746
	ELSE	SSJ0747
	T1=1.	SSJ0748
	T2=1.	SSJ0749
	ENDIF	SSJ0750
	ELSE	SSJ0751
	T1=TH1	SSJ0752
	T2=TH2	SSJ0753
	ENDIF	SSJ0754
	CO=2.*T2*T1*DC/(T1*DR1+T2*DR)	SSJ0755
	ELSE	SSJ0756
	T1=ST(J,I,K)	SSJ0757
	T2=ST(J+1,I,K)	SSJ0758
	SM1=SMAT0	SSJ0759
	SM2=SMAT1	SSJ0760
	IF(LT.EQ.1) THEN	SSJ0761
	T1=T1*TH1	SSJ0762
	T2=T2*TH2	SSJ0763
	IF(SM1.NE.0.) SM1=TH1*SM1	SSJ0764
	IF(SM2.NE.0.) SM2=TH2*SM2	SSJ0765
	ENDIF	SSJ0766
	IF(SM1.EQ.0.)	SSJ0767
1	CO=2.*DC*(T1**2)*DR1*SM2/((T1*DR1+T2*DR)**2)	SSJ0768
	IF(SM2.EQ.0.)	SSJ0769
1	CO=2.*DC*(T2**2)*DR*SM1/((T1*DR1+T2*DR)**2)	SSJ0770
	ENDIF	SSJ0771
	HH=HO-HP	SSJ0772
	IF(ISN.GT.0) THEN	SSJ0773
	IF(IHESS.EQ.0) XX=XX - CO*(HO-HP)*A(IND)	SSJ0774
1	+ CO*(HO-HP)*A(IND+1)	SSJ0775
	IF(IHESS.GT.0) THEN	SSJ0776
	BB=1.	SSJ0777
	IF(LN.GT.0) BB=B/SCL	SSJ0778
	RHS(J,I,K)=RHS(J,I,K)+CO*(HO-HP)*DD*BB*SCL	SSJ0779
	RHS(J+1,I,K)=RHS(J+1,I,K)-CO*(HO-HP)*DD*BB*SCL	SSJ0780
	ENDIF	SSJ0781
	ELSE	SSJ0782
	R0=R0+CO*HH	SSJ0783
	RHS(J+1,I,K)=RHS(J+1,I,K)-CO*HH	SSJ0784
	ENDIF	SSJ0785
300	CONTINUE	SSJ0786
C-----CC		SSJ0787
	IF(IBOUND(J,I+1,K).EQ.0.OR.I.EQ.NR) GO TO 325	SSJ0788
	SMAT1=1.	SSJ0789
	IF(IL.GT.0.AND.PID.NE.'ANI ') THEN	SSJ0790

	IF(M.EQ.0) SMAT1=SF	SSJ0791
	IF(M.GT.0) SMAT1=SF*SMAT(J,I+1,M)	SSJ0792
	IF(SMAT1.NE.0..AND.LZ1.GT.0) THEN	SSJ0793
	IFLAG1=0	SSJ0794
	DO 310 IZ=2,LZI1	SSJ0795
	NZ=LZ(IZ,NM)	SSJ0796
	IF(NZ.EQ.0.OR.IFLAG1.EQ.1) GO TO 315	SSJ0797
	IF(MATZ(J,I+1,LZ1).EQ.NZ) IFLAG1=1	SSJ0798
310	CONTINUE	SSJ0799
315	IF(IFLAG1.EQ.0) SMAT1=0.	SSJ0800
	ENDIF	SSJ0801
	ENDIF	SSJ0802
	IF(PID.EQ.'T' .AND.IL.GT.0.AND.	SSJ0803
1	(SMAT0.EQ.0..AND.SMAT1.EQ.0.)) GO TO 325	SSJ0804
	HP=H(IND+NC)	SSJ0805
	DC1=DELC(I+1)	SSJ0806
	IF(LT.EQ.1) TH2=HP-BOT(J,I+1,KB)	SSJ0807
	IF(PID.EQ.'T' ) THEN	SSJ0808
	IF(IL.LT.0.OR.	SSJ0809
1	(SMAT0.GT.0..AND.SMAT1.GT.0.))THEN	SSJ0810
	IF(LT.EQ.0) THEN	SSJ0811
	IF(IL.GT.0) THEN	SSJ0812
	T1=SMAT0	SSJ0813
	T2=SMAT1	SSJ0814
	ELSE	SSJ0815
	T1=1.	SSJ0816
	T2=1.	SSJ0817
	ENDIF	SSJ0818
	ELSE	SSJ0819
	T1=TH1	SSJ0820
	T2=TH2	SSJ0821
	ENDIF	SSJ0822
	CO=YX*T2*T1*DR/(T1*DC1+T2*DC)	SSJ0823
	ELSE	SSJ0824
	T1=ST(J,I,K)	SSJ0825
	T2=ST(J,I+1,K)	SSJ0826
	SM1=SMAT0	SSJ0827
	SM2=SMAT1	SSJ0828
	IF(LT.EQ.1) THEN	SSJ0829
	T1=T1*TH1	SSJ0830
	T2=T2*TH2	SSJ0831
	IF(SM1.NE.0.) SM1=TH1*SM1	SSJ0832
	IF(SM2.NE.0.) SM2=TH2*SM2	SSJ0833
	ENDIF	SSJ0834
	IF(SM1.EQ.0.)	SSJ0835
1	CO=YX*DR*(T1**2)*DC1*SM2/((T1*DC1+T2*DC)**2)	SSJ0836
	IF(SM2.EQ.0.)	SSJ0837
1	CO=YX*DR*(T2**2)*DC*SM1/((T1*DC1+T2*DC)**2)	SSJ0838
	ENDIF	SSJ0839
	ENDIF	SSJ0840
	IF(PID.EQ.'ANI' ) THEN	SSJ0841
	T1=ST(J,I,K)	SSJ0842
	T2=ST(J,I+1,K)	SSJ0843
	IF(LT.EQ.1) THEN	SSJ0844
	T1=T1*TH1	SSJ0845
	T2=T2*TH2	SSJ0846
	ENDIF	SSJ0847
	IF(T2.EQ.0.0.OR.T1.EQ.0.0) GO TO 330	SSJ0848
	CO=2.*T2*T1*DR/(T1*DC1+T2*DC)	SSJ0849
	ENDIF	SSJ0850
	HH=HO-HP	SSJ0851
	IF(ISN.GT.0) THEN	SSJ0852
	IF(IHESS.EQ.0) XX=XX - CO*(HO-HP)*A(IND)	SSJ0853
1	+ CO*(HO-HP)*A(IND+NC)	SSJ0854
	IF(IHESS.GT.0) THEN	SSJ0855
	BB=1.	SSJ0856
	IF(LN.GT.0) BB=B/SCL	SSJ0857
	RHS(J,I,K)=RHS(J,I,K)+CO*(HO-HP)*DD*BB*SCL	SSJ0858
	RHS(J,I+1,K)=RHS(J,I+1,K)-CO*(HO-HP)*DD*BB*SCL	SSJ0859
	ENDIF	SSJ0860
	ELSE	SSJ0861
	R0=R0+CO*HH	SSJ0862
	RHS(J,I+1,K)=RHS(J,I+1,K)-CO*HH	SSJ0863
	ENDIF	SSJ0864
325	RHS(J,I,K)=RHS(J,I,K)+R0	SSJ0865
330	CONTINUE	SSJ0866
	ENDIF	SSJ0867
	C-----CV	SSJ0868
	IF(PID.EQ.'KV' .OR.PID.EQ.'ANIV') THEN	SSJ0869
	DO 360 I=1,NR	SSJ0870
	DO 360 J=1,NC	SSJ0871
	IF(BOUND(J,I,K).EQ.0.OR.BOUND(J,I,K+1).EQ.0) GO TO 360	SSJ0872
	IF(IL.LT.0) CO=DELR(J)*DELC(I)	SSJ0873

	IF(IL.GT.0.AND.PID.EQ.'KV ') THEN	SSJ0874
	SM=SF	SSJ0875
	IF(M.NE.0) THEN	SSJ0876
	SM=0.	SSJ0877
	IF(SMAT(J,I,M).NE.0.) SM=SF*SMAT(J,I,M)	SSJ0878
	ENDIF	SSJ0879
	IF(SM.NE.0..AND.LZ1.GT.0) THEN	SSJ0880
	IFLAG1=0	SSJ0881
	DO 340 IZ=2,LZ11	SSJ0882
	NZ=LZ(IZ,NM)	SSJ0883
	IF(NZ.EQ.0.OR.IFLAG1.EQ.1) GO TO 345	SSJ0884
	IF(MATZ(J,I,LZ1).EQ.NZ) IFLAG1=1	SSJ0885
340	CONTINUE	SSJ0886
345	IF(IFLAG1.EQ.0) SM=0.	SSJ0887
	ENDIF	SSJ0888
	IF(SM.EQ.0.) GO TO 360	SSJ0889
	CO=(CV(J,I,K)**2)/(SM*B*B*DELR(J)*DELC(I))	SSJ0890
	ENDIF	SSJ0891
	IF(PID.EQ.'ANIV') CO=CV(J,I,K)/B	SSJ0892
	IND=J+NC*(I-1)+NRC*(K-1)	SSJ0893
	HH=H(IND)-H(IND+NRC)	SSJ0894
	IF(ISN.GT.0) THEN	SSJ0895
	IF(IHESS.EQ.0) XX=XX - CO*HH*A(IND) + CO*HH*A(IND+NRC)	SSJ0896
	IF(IHESS.GT.0) THEN	SSJ0897
	BB=1.	SSJ0898
	IF(LN.GT.0) BB=B/SCL	SSJ0899
	RHS(J,I,K)=RHS(J,I,K)+CO*HH*DD*BB*SCL	SSJ0900
	RHS(J,I,K+1)=RHS(J,I,K+1)-CO*HH*DD*BB*SCL	SSJ0901
	ENDIF	SSJ0902
	ELSE	SSJ0903
	RHS(J,I,K)=RHS(J,I,K)+CO*HH	SSJ0904
	RHS(J,I,K+1)=RHS(J,I,K+1)-CO*HH	SSJ0905
	ENDIF	SSJ0906
360	CONTINUE	SSJ0907
	ENDIF	SSJ0908
C-----S		SSJ0909
	IF(PID.EQ.'S1 ') THEN	SSJ0910
	IF((ISN.GT.0.AND.IHESS.EQ.0.AND.KPER.EQ.NPER).OR.	SSJ0911
1	((ISN.LT.0.OR.IHESS.GT.0).AND.KPER.EQ.1)) GO TO 390	SSJ0912
	DO 370 I=1,NR	SSJ0913
	DO 370 J=1,NC	SSJ0914
	IF(BOUND(J,I,K).LE.0) GO TO 370	SSJ0915
	IND=J+NC*(I-1)+NRC*(K-1)	SSJ0916
	IF(IL.LT.0) CO=DELR(J)*DELC(I)/DELT	SSJ0917
	IF(IL.GT.0) THEN	SSJ0918
	SM=SF	SSJ0919
	IF(M.NE.0) SM=SF*SMAT(J,I,NM)	SSJ0920
	IF(SM.NE.0..AND.LZ1.GT.0) THEN	SSJ0921
	IFLAG1=0	SSJ0922
	DO 365 IZ=2,LZ11	SSJ0923
	NZ=LZ(IZ,NM)	SSJ0924
	IF(NZ.EQ.0.OR.IFLAG1.EQ.1) GO TO 367	SSJ0925
	IF(MATZ(J,I,LZ1).EQ.NZ) IFLAG1=1	SSJ0926
365	CONTINUE	SSJ0927
367	IF(IFLAG1.EQ.0) SM=0.	SSJ0928
	ENDIF	SSJ0929
	IF(SM.EQ.0.) GO TO 370	SSJ0930
	IF(LT.EQ.1) SM=1.	SSJ0931
	CO=SM*DELR(J)*DELC(I)/DELT	SSJ0932
	ENDIF	SSJ0933
C	DAH AND DBH	SSJ0934
	AO=A(IND)	SSJ0935
	HO=H(IND)	SSJ0936
	IF(ISN.GT.0) THEN	SSJ0937
	IF(IHESS.EQ.0) XX = XX - CO*(HO-HOLD(IND))*AO	SSJ0938
	IF(IHESS.GT.0) THEN	SSJ0939
	BB=1.	SSJ0940
	IF(LN.GT.0) BB=B/SCL	SSJ0941
	RHS(J,I,K)=RHS(J,I,K)-CO*(SHOLD(IND)-HO)*DD*BB*SCL	SSJ0942
	ENDIF	SSJ0943
	ELSE	SSJ0944
	RHS(J,I,K)=RHS(J,I,K)-CO*(SHOLD(IND)-HO)	SSJ0945
	ENDIF	SSJ0946
370	CONTINUE	SSJ0947
	ENDIF	SSJ0948
	PID=PID1	SSJ0949
390	CONTINUE	SSJ0950
400	RETURN	SSJ0951
	END	SSJ0952

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C=====SSJ0953
      SUBROUTINE SSENLR(                      SSJ0954
1      NLL,KPER,NPER,NCOL,NROW,NLAY,DELR,DELC,SMAT,NSM,NM,IOUT,XX,SSJ0955
2      IFLAG,ILAY,A,IBOUND,ISN,RHS,SURF,EXDP,PID,SHNW,DD,IHESS,  SSJ0956
3      SCL,NMM,NZM,LZ1,SFAC,LZ,LM,MATZ,NLL11,NLLIT)          SSJ0957
C-----VERSION 1000 01FEB1992                      SSJ0958
C      *****SSJ0959
C      CALCULATE FORCING FUNCTION DERIVATIVE FOR RCH OR ETM. MULTIPLY BY SSJ0960
C      THE ADJOINT STATE AND ADD TO THE DERIVATIVE, OR ADD TO RHS, AS SSJ0961
C      NEEDED.                      SSJ0962
C      *****SSJ0963
C      SPECIFICATIONS:                      SSJ0964
C      -----SSJ0965
C      CHARACTER*4 PID                      SSJ0966
C      DOUBLE PRECISION A(NCOL,NROW,NLAY),RO,DD,XX          SSJ0967
C      DIMENSION DELR(NCOL),DELC(NROW),NLL(NLL11),ILAY(NCOL,NROW), SSJ0968
1      SMAT(NCOL,NROW,NMM),IBOUND(NCOL,NROW,NLAY),SFAC(NSM),  SSJ0969
1      RHS(NCOL,NROW,NLAY),SURF(NCOL,NROW),EXDP(NCOL,NROW),LM(NSM), SSJ0970
3      SHNW(NCOL,NROW,NLAY),LZ(LZ1,NSM),MATZ(NCOL,NROW,NZM)  SSJ0971
C      -----SSJ0972
C      NLL1=NLL(1)                      SSJ0973
C      ITS=NPER-KPER                      SSJ0974
C      IF(ISN.LT.0.OR.IHESS.GT.0) ITS=KPER-1                SSJ0975
C-----LOOP THROUGH TIMES                      SSJ0976
      DO 450 K=1,NLLIT                      SSJ0977
1      IF(NLL(2*K).GE.0.AND.(ITS.GE.NLL(2*K).AND.ITS.LE.NLL(2*K+1))) SSJ0978
1      THEN                      SSJ0979
          SM=1.                      SSJ0980
          IF(NLL1.GT.0) THEN          SSJ0981
              NM=NM+1                SSJ0982
              M=LM(NM)                SSJ0983
              SF=SFAC(NM)              SSJ0984
              LZ1=LZ(1,NM)              SSJ0985
          ENDIF                      SSJ0986
C-----LOOP THROUGH CELLS                      SSJ0987
          DO 400 IR=1,NROW              SSJ0988
          DO 300 IC=1,NCOL              SSJ0989
              SM=1.                      SSJ0990
              IF(NLL1.GT.0) THEN          SSJ0991
                  SM=SF                SSJ0992
                  IF(M.GT.0) SM=SF*SMAT(IC,IR,M)          SSJ0993
                  IF(LZ1.GT.0) THEN          SSJ0994
                      IFL=0              SSJ0995
                      DO 230 IZ=2,LZ1      SSJ0996
                          NZ=LZ(IZ,NM)      SSJ0997
                          IF(NZ.EQ.0.OR.IFL.EQ.1) GO TO 235  SSJ0998
230                     IF(NZ.EQ.MATZ(IC,IR,LZ1)) IFL=1      SSJ0999
235                     IF(IFL.EQ.0) SM=0.      SSJ1000
                      ENDIF              SSJ1001
                  ENDIF              SSJ1002
                  IF(SM.EQ.0.) GO TO 300      SSJ1003
C-----IFLAG=1                      SSJ1004
                  IF(IFLAG.EQ.1.AND.IBOUND(IC,IR,1).GT.0) THEN SSJ1005
                      RO=SM*DELR(IC)*DELC(IR)          SSJ1006
                      KK=1                SSJ1007
                  ENDIF              SSJ1008
C-----IFLAG=2                      SSJ1009
                  IF(IFLAG.EQ.2.AND.IBOUND(IC,IR,(ILAY(IC,IR))).GT.0)THEN SSJ1010
                      RO=SM*DELR(IC)*DELC(IR)          SSJ1011
                      KK=ILAY(IC,IR)      SSJ1012
                  ENDIF              SSJ1013
C-----IFLAG=3                      SSJ1014
                  IF(IFLAG.EQ.3) THEN          SSJ1015
                      DO 250 KK=1,NLAY      SSJ1016
                          IF(IBOUND(IC,IR,KK).GT.0) GO TO 255  SSJ1017
250                     CONTINUE          SSJ1018
                          GO TO 300          SSJ1019
255                     RO=SM*DELR(IC)*DELC(IR)          SSJ1020
                  ENDIF              SSJ1021
C-----ADJUST FOR ETM                      SSJ1022
                  IF(PID.EQ.'ETM ') THEN          SSJ1023
                      RO=-RO              SSJ1024
                      S=SURF(IC,IR)          SSJ1025
                      H=SHNW(IC,IR,KK)          SSJ1026
                      IF(H.GE.S) GO TO 270          SSJ1027
                      DDD=S-H              SSJ1028
                      XXX=EXDP(IC,IR)          SSJ1029
                      IF(DDD.GE.XXX) GO TO 300          SSJ1030
                      RO=RO*(1.-(DDD/XXX))          SSJ1031
270                     CONTINUE          SSJ1032
                  ENDIF              SSJ1033
C-----CONTRIBUTIONS TO SENSITIVITIES OR RHS.          SSJ1034
                  IF(ISN.GT.0.AND.IHESS.EQ.0) XX=XX+A(IC,IR,KK)*RO SSJ1035

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      IF(ISN.GT.0.AND.IHESS.GT.0) SSJ1036
1      RHS(IC,IR,KK)=RHS(IC,IR,KK)-RO*DD*SCL SSJ1037
      IF(ISN.LT.0) RHS(IC,IR,KK)=RHS(IC,IR,KK)-RO SSJ1038
300      CONTINUE SSJ1039
400      CONTINUE SSJ1040
      ENDIF SSJ1041
450 CONTINUE SSJ1042
      IF(NLL(1).GT.0.AND.IR.EQ.0) NM=NM+1 SSJ1043
C RETURN SSJ1044
END SSJ1045
SSJ1046

C=====SSJ1047
      SUBROUTINE SSENLU( SSJ1048
1      NH,NDER,IOFF,JOFF,KPER,MLAY,IBOUND,RINT,DID,COFF,ROFF,DELR, SSJ1049
2      DELC,NCOL,NROW,NLAY,PR,H,HOBS,WT,HNEW,X,IP,IDRY,NP,MOBS,B, SSJ1050
3      LN,ISN,NQT,TOFF,NPER,RHS,PV,MAXM,ITERP,JDRY,IPAR,IOUT) SSJ1051
C-----VERSION 1000 01FEB1992 SSJ1052
C ***** SSJ1053
C INTERPOLATE HEADS; ACCOUNT FOR DRY CELLS, IF NEEDED SSJ1054
C ***** SSJ1055
C SPECIFICATIONS: SSJ1056
C ----- SSJ1057
      CHARACTER*4 DID(NH+NQT) SSJ1058
      DOUBLE PRECISION HNEW(NCOL,NROW,NLAY),V,PV SSJ1059
      DIMENSION IBOUND(NCOL,NROW,NLAY),X(NP,NH+NQT),DELR(NCOL), SSJ1060
1      DELC(NROW),COFF(NH),ROFF(NH),H(NH+NQT),WT(NH+NQT), SSJ1061
1      HOBS(NH+NQT),RINT(4,NH),JOFF(NH),IOFF(NH), SSJ1062
1      MLAY(MAXM,MOBS),PR(MAXM,MOBS),NDER(5,NH),B(NP),LN(NP), SSJ1063
1      TOFF(NH),RHS(NCOL,NROW,NLAY),PV(NH) SSJ1064
      COMMON /FLWCOM/LAYCON(80) SSJ1065
C ----- SSJ1066
555 FORMAT(/,' HEAD OBS#',I5,', ID ',A4,' IS DRY -- OMIT (SSENLU)') SSJ1067
560 FORMAT(/,' INTERPOLATION FOR HEAD OBS#',I5,', ID ',A4,' CHANGED', SSJ1068
1 ' BECAUSE AT LEAST ONE NEIGHBORING CELL IS DRY (SSENLU)') SSJ1069
565 FORMAT(/,' ',I5,' OF',I5,' OBSERVATIONS OMITTED. EXECUTION ', SSJ1070
1 ' STOPS IF # OF REMAINING OBS <= # OF PARAMETERS') SSJ1071
C SSJ1072
C-----CALCULATE TIME STEP SSJ1073
      ITS=KPER-1 SSJ1074
      IF(ISN.GT.0.AND.IP.EQ.1) ITS=NPER-KPER SSJ1075
C-----CHECK FOR NODES USED TO INTERPOLATE HEADS THAT HAVE GONE DRY. SSJ1076
C-----ELIMINATE OBSERVATIONS OR RECALC. INTERPOLATION COEFFICIENTS. SSJ1077
      IF(IP.EQ.0.AND.ISN.EQ.-1) THEN SSJ1078
C-----SKIP IF ALL LAYERS ARE CONFINED SSJ1079
      KK=0 SSJ1080
      DO 20 K=1,NLAY SSJ1081
20      KK=KK+LAYCON(K) SSJ1082
      IF(KK.EQ.0) GO TO 75 SSJ1083
C-----CHECK FOR OBSERVATIONS THAT NEED TO BE OMITTED OR NEED TO HAVE SSJ1084
C-----THE INTERPOLATION RECALCULATED SSJ1085
      IF(KPER.EQ.1) THEN SSJ1086
      IDRY=0 SSJ1087
      JDRY=0 SSJ1088
      ENDIF SSJ1089
      ML=0 SSJ1090
      DO 70 N=1,NH SSJ1091
      K=NDER(1,N) SSJ1092
      II=NDER(2,N) SSJ1093
      JJ=NDER(3,N) SSJ1094
      IO=IOFF(N) SSJ1095
      JO=JOFF(N) SSJ1096
      MM=1 SSJ1097
      IF(K.LT.0) THEN SSJ1098
      ML=ML+1 SSJ1099
      MM=MAXM SSJ1100
      ENDIF SSJ1101
      IF(NDER(4,N).EQ.ITS.OR.(TOFF(N).GT.0..AND.NDER(4,N).EQ.ITS-1)) SSJ1102
1      THEN SSJ1103
      DO 65 M=1,MM SSJ1104
      KK=K SSJ1105
      IF(K.LT.0) KK=MLAY(M,ML) SSJ1106
      IF(KK.EQ.0) GO TO 70 SSJ1107
      IF(LAYCON(KK).EQ.1) THEN SSJ1108
      IF(IBOUND(JJ,II,KK).EQ.0) THEN SSJ1109
      IDRY=IDRY+1 SSJ1110
      IF(IPAR.GE.1) WT(N)=-ABS(WT(N)) SSJ1111
      WRITE(IOUT,555) N,DID(N) SSJ1112
      GO TO 70 SSJ1113
      ELSE SSJ1114
      IF((RINT(2,N).NE.0..AND.IBOUND(JJ,JO,II,KK).EQ.0).OR. SSJ1115
1      (RINT(3,N).NE.0..AND.IBOUND(JJ,II+IO,KK).EQ.0).OR. SSJ1116

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1          (RINT(4,N).NE.0..AND.IBOUND(JJ+JO,II+IO,KK).EQ.0))THENSSJ1117
          IF(MM.GT.1) THEN
          IDRY=IDRY+1
          IF(IPAR.GE.1) WT(N)=-ABS(WT(N))
          WRITE(IOUT,555) N,DID(N)
          GO TO 70
          ENDIF
          WRITE(IOUT,560) N,DID(N)
          CALL SSEN1I (NDER(1,N),COFF(N),ROFF(N),DELR,DELC,
1          IBOUND,NCOL,NROW,NLAY,RINT(1,N),JOFF(N),IOFF(N),
2          MLAY(1,ML))
          COFF(N)=COFF(N)+5.
          JDRY=JDRY+1
          ENDIF
          ENDIF
          ENDIF
65      CONTINUE
          ENDIF
70      CONTINUE
          IF(IDRY.GT.0) WRITE(IOUT,565) IDRY,NH
          IF((NH-IDRY).LE.NP) STOP
          ENDIF
C-----INTERPOLATION
75      ML=0
          DO 80 N=1,NH
          IF(IPAR.GE.1.AND.WT(N).LT.0.) GO TO 80
          IF(NDER(4,N).EQ.ITS-1.AND.TOFF(N).GT.0.) GO TO 77
          IF(NDER(4,N).NE.ITS) GO TO 80
77      CONTINUE
          K=NDER(1,N)
          II=NDER(2,N)
          JJ=NDER(3,N)
          IO=IOFF(N)
          JO=JOFF(N)
          V=0.
          MM=1
          IF(K.LT.0) THEN
          ML=ML+1
          MM=-K
          ENDIF
          DO 78 M=1,MM
          KK=K
          PROP=1.
          IF(K.LT.0) THEN
          KK=MLAY(M,ML)
          PROP=PR(M,ML)
          ENDIF
          IF(KK.EQ.0) GO TO 79
C-----ADD CONTRIBUTION FROM THIS LAYER TO ....
C-----SENSITIVITY-EQUATION SENSITIVITIES
          IF(ISN.LT.0.OR.(ISN.GT.0.AND.IP.NE.1))
1          V = V + PROP * ( RINT(1,N)*HNEW(JJ,II,KK) +
1          RINT(2,N)*HNEW(JJ+JO,II,KK) + RINT(3,N)*HNEW(JJ,II+IO,KK)
1          + RINT(4,N)*HNEW(JJ+JO,II+IO,KK) )
C-----RHS FOR ADJOINT STATES
          IF(IP.EQ.1.AND.ISN.GT.0) THEN
          FACT=1.0
          IF(TOFF(N).GT.0.) THEN
          FACT=TOFF(N)
          IF(NDER(4,N).EQ.ITS-1) FACT=1.-FACT
          ENDIF
          HD=HOBS(N)-H(N)
          W=WT(N)
          RHS(JJ,II,KK)=RHS(JJ,II,KK)+2.*PROP*FACT*RINT(1,N)*W*HD
          RHS(JJ+JO,II,KK)=RHS(JJ+JO,II,KK)+
1          2.*PROP*FACT*RINT(2,N)*W*HD
          RHS(JJ,II+IO,KK)=RHS(JJ,II+IO,KK)+
1          2.*PROP*FACT*RINT(3,N)*W*HD
          RHS(JJ+JO,II+IO,KK)=RHS(JJ+JO,II+IO,KK)+
1          2.*PROP*FACT*RINT(4,N)*W*HD
          GO TO 80
          ENDIF
78      CONTINUE
C-----INDICE WHICH, IF NOT ZERO, IDENTIFIES THE HEAD USED TO
C-----CALCULATED DRAWDOWN
79      N1=NDER(5,N)
C-----HEADS OR DRAWDOWNS
          IF(IP.EQ.0) THEN
          IF(NDER(4,N).EQ.ITS) H(N)=V
          IF(NDER(4,N).EQ.ITS-1.AND.TOFF(N).GT.0.)
1          H(N)=H(N)+TOFF(N)*(V-H(N))
          IF(N1.GT.0) H(N)=H(N)-H(N1)
          ENDIF

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C-----ITERATION PARAMETER VECTOR FOR CONJUGATE-DIRECTION REGRESSION SSJ1200
      IF (ISN.GT.0.AND.IP.EQ.2) THEN SSJ1201
        IF (NDER(4,N).EQ.ITS) PV(N)=V SSJ1202
        IF (NDER(4,N).EQ.ITS-1.AND.TOFF(N).GT.0.) SSJ1203
          1 PV(N)=PV(N)+TOFF(N)*(V-PV(N)) SSJ1204
          IF (N1.GT.0) PV(N)=PV(N)-PV(N1) SSJ1205
        ENDIF SSJ1206
C-----SENSITIVITY-EQUATION SENSITIVITIES SSJ1207
      IF (ISN.LT.0.AND.IP.GT.0) THEN SSJ1208
        IF (NDER(4,N).EQ.ITS) THEN SSJ1209
          IF (LN(IP).NE.0) X(IP,N)=B(IP)*V SSJ1210
          IF (LN(IP).EQ.0) X(IP,N)=V SSJ1211
        ENDIF SSJ1212
        IF (NDER(4,N).EQ.ITS-1.AND.TOFF(N).GT.0.) THEN SSJ1213
          IF (LN(IP).NE.0) X(IP,N)=X(IP,N)+TOFF(N)*((B(IP)*V)-X(IP,N)) SSJ1214
          IF (LN(IP).EQ.0) X(IP,N)=X(IP,N)+TOFF(N)*(V-X(IP,N)) SSJ1215
        ENDIF SSJ1216
        IF (N1.GT.0) X(IP,N)=X(IP,N)-X(IP,N1) SSJ1217
      ENDIF SSJ1218
      80 CONTINUE SSJ1219
      RETURN SSJ1220
      END SSJ1221

C=====SSJ1222
      SUBROUTINE SSENIV( SSJ1223
        1 NQ,NQC,NQT,NQOB,NQCL,IQOB,QCLS,IBT,MXBND,NBOUND,BNDS, SSJ1224
        2 MXRIVR,NRIVER,RIVR,SHNW,IP,HNEW,NCOL,NROW,NLAY,IOUT, SSJ1225
        3 IBOUND,NPER,KPER,NH,X,DID,NP,H,B,LN,TOFF,MXDRN,NDRAIN,DRAI, SSJ1226
        4 MXSTRM,NSTREM,STRM,ISTRM,ISN,RHS,WT,HOBS) SSJ1227
C-----VERSION 1000 01FEB1992 SSJ1228
C ***** SSJ1229
C SAVE SIMULATED FLOWS AND CALCULATE SENSITIVITIES SSJ1230
C ***** SSJ1231
C SPECIFICATIONS: SSJ1232
C ----- SSJ1233
      CHARACTER*4 DID(NH+NQT) SSJ1234
      DOUBLE PRECISION HNEW(NCOL,NROW,NLAY) SSJ1235
      DIMENSION SHNW(NCOL,NROW,NLAY),RIVR(6,MXRIVR),BNDS(5,MXBND), SSJ1236
      1 IBOUND(NCOL,NROW,NLAY),X(NP,NH+NQT),IBT(2,NQ),B(NP),LN(NP), SSJ1237
      2 NQOB(NQ),NQCL(NQ),IQOB(NQT),QCLS(5,NQC),H(NH+NQT),TOFF(NH+NQT), SSJ1238
      3 STRM(11,MXSTRM),ISTRM(5,MXSTRM),RHS(NCOL,NROW,NLAY),WT(NH+NQT), SSJ1239
      4 HOBS(NH+NQT),DRAI(5,MXDRN) SSJ1240
C ----- SSJ1241
      505 FORMAT(/,' HEADS AT STREAM, RIVER, OR DRAIN CELLS ARE BELOW THE ', SSJ1242
      1 'BOTTOM OF THE STREAMBED, RIVER BED, OR DRAIN AT THE REACHES OR', SSJ1243
      2 /,' CELLS LISTED BELOW,', SSJ1244
      3 ' OR, FOR STREAMS, THE LOSS EXCEEDS THE FLOW IN THE STREAM (*).', SSJ1245
      4 /,' THESE CONDITIONS DIMINISH THE IMPACT', SSJ1246
      2 ' OF THE OBSERVATION ON ALL PARAMETERS EXCEPT, IN SOME CASES, ', SSJ1247
      3 /,' THE HYDRAULIC CONDUCTIVITY OF THE STREAMBED, RIVER BED, OR ', SSJ1248
      7 'DRAIN (SEE TEXT FOR MORE INFORMATION).') SSJ1249
      510 FORMAT(/,' OBS#',I5,', ID ',A4,', TIME STEP ',I5) SSJ1250
      515 FORMAT(' LAYER ROW COLUMN') SSJ1251
      520 FORMAT(' SEGMENT REACH') SSJ1252
      525 FORMAT(3I7) SSJ1253
      527 FORMAT(' *',I5,I7) SSJ1254
      530 FORMAT(I7,' OF THE',I7,' REACHES OR CELLS USED TO SIMULATE THE', SSJ1255
      1 ' GAIN OR LOSS ARE AFFECTED.') SSJ1256
      540 FORMAT(' THIS OBSERVATION NO LONGER IMPACTS PARAMETER ', SSJ1257
      1 ' ESTIMATION AND WILL BE ELIMINATED FROM THIS PARAMETER ',/, SSJ1258
      2 ' ESTIMATION ITERATION') SSJ1259
      550 FORMAT(' CELL OR REACH #',I5,' OF HEAD-DEP. BOUNDARY GAIN OR', SSJ1260
      1 ' LOSS OBS#',I5,' ID=',A4,' NOT FOUND IN CELLS LISTED FOR',/, SSJ1261
      2 ' PACKAGE',I5,' (1 RIVER; 2 GHB; 3 STREAM; 4 DRAIN) --', SSJ1262
      3 ' STOP EXECUTION') SSJ1263
C SSJ1264
C-----INITIALIZE VARIABLES SSJ1265
      ITS=KPER-1 SSJ1266
      IF (ISN.GT.0.AND.IP.EQ.1) ITS=NPER-KPER SSJ1267
      NC=0 SSJ1268
      NT1=1 SSJ1269
      JRBOT=0 SSJ1270
C-----LOOP THROUGH BOUNDARY FLOWS SSJ1271
      DO 200 IQ=1,NQ SSJ1272
        IBT1=IBT(1,IQ) SSJ1273
        NT2=NT1+NQOB(IQ)-1 SSJ1274
C-----WAS THERE A MEASUREMENT AT THIS BOUNDARY THIS TIME STEP? SSJ1275
      DO 100 NT=NT1,NT2 SSJ1276
        100 IF (IQOB(NT).EQ.ITS.OR.(IQOB(NT).EQ.ITS-1.AND. SSJ1277
          1 TOFF(NH+NT).GT.0.)) GO TO 110 SSJ1278
        GO TO 190 SSJ1279
C-----ASSIGN VARIABLES ACCORDING TO BOUNDARY TYPE SSJ1280

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110	CONTINUE	SSJ1281
	IRBOT=0	SSJ1282
	KRBOT=0	SSJ1283
	IF (IBT1.EQ.1) NBN=NRIVER	SSJ1284
	IF (IBT1.EQ.2) NBN=NBOUND	SSJ1285
	IF (IBT1.EQ.3) NBN=NSTREM	SSJ1286
	IF (IBT1.EQ.4) NBN=NDRAIN	SSJ1287
C-----	LOOP THROUGH CELLS.	SSJ1288
	NC1=NC+1	SSJ1289
	NC2=NC+NQCL(IQ)	SSJ1290
	DO 130 N=NC1,NC2	SSJ1291
	K=QCLS(1,N)	SSJ1292
	I=QCLS(2,N)	SSJ1293
	J=QCLS(3,N)	SSJ1294
	IF (IBT1.NE.3.AND.IBOUND(J,I,K).LE.0) GO TO 130	SSJ1295
C-----	LOOP THROUGH DATA FILE TO FIND A MATCH.	SSJ1296
	IFLAG=0	SSJ1297
	DO 120 NB=1,NBN	SSJ1298
	IF (IBT1.EQ.1) THEN	SSJ1299
	KK=RIVR(1,NB)	SSJ1300
	II=RIVR(2,NB)	SSJ1301
	JJ=RIVR(3,NB)	SSJ1302
	ENDIF	SSJ1303
	IF (IBT1.EQ.2) THEN	SSJ1304
	KK=BND(1,NB)	SSJ1305
	II=BND(2,NB)	SSJ1306
	JJ=BND(3,NB)	SSJ1307
	ENDIF	SSJ1308
	IF (IBT1.EQ.3) THEN	SSJ1309
	IS=ISTRM(4,NB)	SSJ1310
	IR=ISTRM(5,NB)	SSJ1311
	ENDIF	SSJ1312
	IF (IBT1.EQ.4) THEN	SSJ1313
	KK=DRAI(1,NB)	SSJ1314
	II=DRAI(2,NB)	SSJ1315
	JJ=DRAI(3,NB)	SSJ1316
	ENDIF	SSJ1317
C-----	DO CALCULATIONS IF THIS IS A MATCH	SSJ1318
	IF ((IBT1.NE.3.AND.I.EQ.II.AND.J.EQ.JJ.AND.K.EQ.KK).OR.	SSJ1319
1	(IBT1.EQ.3.AND.K.EQ.IS.AND.I.EQ.IR)) THEN	SSJ1320
	IFLAG=1	SSJ1321
C-----	ASSIGN VARIABLE VALUES	SSJ1322
	IF (IBT1.EQ.3) THEN	SSJ1323
	K=ISTRM(1,NB)	SSJ1324
	I=ISTRM(2,NB)	SSJ1325
	J=ISTRM(3,NB)	SSJ1326
	ENDIF	SSJ1327
	IF (IP.EQ.0) HHNEW=HNEW(J,I,K)	SSJ1328
	IF (IP.GT.0) HHNEW=SHNW(J,I,K)	SSJ1329
	IF (IBT1.EQ.1) THEN	SSJ1330
	HB=RIVR(4,NB)	SSJ1331
	C=RIVR(5,NB)	SSJ1332
	RBOT=RIVR(6,NB)	SSJ1333
	ENDIF	SSJ1334
	IF (IBT1.EQ.2) THEN	SSJ1335
	HB=BND(4,NB)	SSJ1336
	C=BND(5,NB)	SSJ1337
	ENDIF	SSJ1338
	IF (IBT1.EQ.3) THEN	SSJ1339
	HB=STRM(2,NB)	SSJ1340
	IF (STRM(10,NB).LE.0.) HB=STRM(5,NB)	SSJ1341
	C=STRM(3,NB)	SSJ1342
	RBOT=STRM(4,NB)	SSJ1343
	ENDIF	SSJ1344
	IF (IBT1.EQ.4) THEN	SSJ1345
	HB=DRAI(4,NB)	SSJ1346
	C=DRAI(5,NB)	SSJ1347
	RBOT=HB	SSJ1348
	ENDIF	SSJ1349
C-----	CALCULATE FLOWS	SSJ1350
	IF (IP.EQ.0) THEN	SSJ1351
	HH=C*(HB-HHNEW)	SSJ1352
	ISTRF=0	SSJ1353
	IF (IBT1.EQ.3.AND.STRM(10,NB)-STRM(11,NB).LE.0.) ISTRF=1	SSJ1354
	IF (((IBT1.NE.2).AND.HHNEW.LE.RBOT).OR.ISTRF.EQ.1) THEN	SSJ1355
	HH=C*(HB-RBOT)	SSJ1356
	IF (ISTRF.EQ.1) HH=STRM(10,NB)	SSJ1357
	IF (JRBOT.EQ.0) WRITE(IOUT,505)	SSJ1358
	JRBOT=1	SSJ1359
	IF (IRBOT.EQ.0) THEN	SSJ1360
	WRITE(IOUT,510)NH+NT,DID(NH+NT),ITS	SSJ1361
	IF (IBT1.NE.3) WRITE(IOUT,515)	SSJ1362
	IF (IBT1.EQ.3) WRITE(IOUT,520)	SSJ1363

	ENDIF	SSJ1364
	IRBOT=IRBOT+1	SSJ1365
	IF (IBT(2,IQ).EQ.0.OR.ISTRF.EQ.1) KRBOT=KRBOT+1	SSJ1366
	IF (IBT1.NE.3) WRITE(IOUT,525) K,I,J	SSJ1367
	IF (IBT1.EQ.3) THEN	SSJ1368
	IF (ISTRF.EQ.1) THEN	SSJ1369
	WRITE(IOUT,527) IS,IR	SSJ1370
	ELSE	SSJ1371
	WRITE(IOUT,525) IS,IR	SSJ1372
	ENDIF	SSJ1373
	ENDIF	SSJ1374
	ENDIF	SSJ1375
C-----	ENDIF	SSJ1376
	CALCULATE SENSITIVITIES	SSJ1377
	IF (IP.GT.0) THEN	SSJ1378
	XX=0.	SSJ1379
	IF ((IBT1.EQ.3.AND.STRM(10,NB).LE.0..AND.	SSJ1380
1	STRM(11,NB).GE.0.).OR.	SSJ1381
1	(IBT1.EQ.4.AND.HHNEW.LE.HB)) GO TO 120	SSJ1382
	IF (IBT1.EQ.2.OR.HHNEW.GT.RBOT) XX = -C*HHNEW(J,I,K)	SSJ1383
	IF (IP.EQ.IBT(2,IQ).AND.(IBT1.EQ.2.OR.HHNEW.GT.RBOT))	SSJ1384
1	XX = XX + QCLS(5,N)*(HB-HHNEW)	SSJ1385
	IF (IP.EQ.IBT(2,IQ).AND.(IBT1.EQ.1.OR.IBT1.EQ.3)	SSJ1386
1	.AND.HHNEW.LE.RBOT)	SSJ1387
1	XX = QCLS(5,N)*(HB-RBOT)	SSJ1388
	ENDIF	SSJ1389
	GO TO 125	SSJ1390
	ENDIF	SSJ1391
120	CONTINUE	SSJ1392
	IF (IFLAG.EQ.0) THEN	SSJ1393
	WRITE(IOUT,550) N,NH+NT,DID(NH+NT),IBT1	SSJ1394
	STOP	SSJ1395
	ENDIF	SSJ1396
C-----	SUM VALUES FROM INDIVIDUAL CELLS.	SSJ1397
125	CONTINUE	SSJ1398
C-----	CALCULATE FACTOR FOR TEMPORAL INTERPOLATION	SSJ1399
	FACT=1.0	SSJ1400
	IF (TOFF(NH+NT).GT.0.) THEN	SSJ1401
	IF (IQOB(NT).EQ.ITS) FACT=1.-TOFF(NH+NT)	SSJ1402
	IF (IQOB(NT).EQ.ITS-1) FACT=TOFF(NH+NT)	SSJ1403
	ENDIF	SSJ1404
C-----	FLows	SSJ1405
	IF (IP.EQ.0) H(NH+NT)=H(NH+NT)+HH*FACT*QCLS(4,N)	SSJ1406
C-----	SENSITIVITY-EQUATION SENSITIVITIES	SSJ1407
	IF (IP.GT.0.AND.(ISN.LT.0.OR.IP.EQ.2)) THEN	SSJ1408
	IF (LN(IP).GT.0) XX=XX*B(IP)	SSJ1409
	X(IP,NH+NT)=X(IP,NH+NT)+XX*FACT*QCLS(4,N)	SSJ1410
	ENDIF	SSJ1411
130	CONTINUE	SSJ1412
C-----	PRINT NUMBER OF CELLS AT WHICH HEAD IS BELOW THE BOTTOM OF THE	SSJ1413
C-----	STREAM OR RIVER BED; CHECK FOR DISCONNECTED OBSERVATIONS.	SSJ1414
	IF (IP.EQ.0.AND.IRBOT.GT.0) WRITE(IOUT,530) IRBOT,NQCL(IQ)	SSJ1415
	IF (IP.EQ.0.AND.KRBOT.EQ.NQCL(IQ)) THEN	SSJ1416
	WT(NH+NT)=-WT(NH+NT)	SSJ1417
	WRITE(IOUT,540)	SSJ1418
	ENDIF	SSJ1419
C-----	UPDATE COUNTERS	SSJ1420
190	NC=NC+NQCL(IQ)	SSJ1421
	NT1=NT2+1	SSJ1422
C		SSJ1423
200	CONTINUE	SSJ1424
	RETURN	SSJ1425
	END	SSJ1426

# New PAR Primary Modules

Listed in order of first appearance in MAIN

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C=====PAR0001
  SUBROUTINE PARIAL (
1      ISUM,LENX,IOUT,NP,NH,LCC,LCSCLE,LCG,LCDD,LCWP,
2      LCB1,NQT,MPR,LCPRM,ISN,LCSCLE,LCPV,ND,
3      LCR,LCU,LCGD,LCS)
C-----PAR0006
  VERSION 1000 01FEB1992 PARIAL
C *****PAR0007
C   ALLOCATE ARRAY STORAGE FOR PARAMETER ESTIMATION
C *****PAR0009
C   SPECIFICATIONS:
C   -----PAR0010
C   -----PAR0011
C   -----PAR0012
C   -----PAR0013
C1-----IDENTIFY PACKAGE
  WRITE(IOUT,1)
  1 FORMAT(1H0,'PAR1 -- PARAMETER ESTIMATION PACKAGE, ',
  1 'VERSION 1, 12/01/91')
C-----STORE, IN ISOLD, LOCATION OF FIRST UNALLOCATED SPACE IN X.
  ISOLD=ISUM
C-----ARRAYS USED ONLY FOR PARAMETER ESTIMATION
  LCSCLE=ISUM
  IF(ISN.GT.0) ISUM=ISUM+NP
  LCWP=ISUM
  ISUM=ISUM+NP+MPR
  LCB1=ISUM
  ISUM=ISUM+NP
  LCPRM=ISUM
  ISUM=ISUM+(NP+1)*MPR
  IF(MOD(ISUM,2).EQ.0) ISUM=ISUM+1
  LCG=ISUM
  IF(ISN.LT.0) ISUM=ISUM+NP*2
  IF(ISN.GT.0) THEN
    IF(MOD(ISUM,2).EQ.0) ISUM=ISUM+1
    ISUM=ISUM+NP*2
  ENDIF
  LCC=ISUM
  IF(ISN.LT.0.OR.ISN.GE.4) ISUM=ISUM+2*NP*NP
  IF(ISN.EQ.1) ISUM=ISUM+2*(NP*NP/2+NP/2+1)
  LCSCLE=ISUM
  IF(ISN.LT.0.OR.ISN.GE.4) ISUM=ISUM+2*NP
  LCPV=ISUM
  IF(ISN.GT.0) ISUM=ISUM+ND*2
  LCDD=ISUM
  ISUM=ISUM+2*NP
C-----FOR QUASI-NEWTON ADDITION TO THE GAUSS-NEWTON MATRIX
  IF(ISN.LT.0) THEN
    LCR=ISUM
    ISUM=ISUM+2*(NP*NP/2+NP)
    LCU=ISUM
    ISUM=ISUM+NP*2
    LCS=ISUM
    LCS=ISUM+NP*2
    LCGD=ISUM
    ISUM=ISUM+NP*2
  ENDIF
C
C8-----PRINT AMOUNT OF SPACE USED BY PARAMETER-ESTIMATION PACKAGE.
  ISP=ISUM-ISOLD
  WRITE(IOUT,4)ISP
  4 FORMAT(1X,I6,' ELEMENTS IN X ARRAY ARE USED FOR PARAMETER',
  1 ' ESTIMATION')
  ISUM1=ISUM-1
  WRITE(IOUT,5)ISUM1,LENX
  5 FORMAT(1X,I6,' ELEMENTS OF X ARRAY USED OUT OF',I7)
  IF(ISUM1.GT.LENX) WRITE(IOUT,6)
  6 FORMAT(1X,' ***X ARRAY MUST BE DIMENSIONED LARGER***')
C
C9-----RETURN
  RETURN
  END
C=====PAR0071
  SUBROUTINE PARIRP (
1      IU,IOUT,NP,PID,WP,B,CONV,LN,LASTX,DMAX,CSA,TOL,ITMXP,
2      DD,IOUR,IPRC,IPRINT,FCONV,NPR,EV,NH,WT,NQT,KPRINT,
3      MPR,PRM,IWPG,SCL,ISN,NFIT,LPRINT,NPO,SOSC,NPER,SOSR)
C-----PAR0076
  VERSION 1000 01FEB1992
C *****PAR0077

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C      READ, CHECK AND STORE DATA FOR PARAMETER ESTIMATION, AND          PAR0078
C      INITIALIZE SOME VARIABLES.                                         PAR0079
C      *****                                                             PAR0080
C      SPECIFICATIONS:                                                    PAR0081
C      -----                                                             PAR0082
C      CHARACTER*4  PID(NPO)                                              PAR0083
C      CHARACTER*10 EST,CVAR                                              PAR0084
C      DOUBLE PRECISION DD(NPO)                                           PAR0085
C      DIMENSION WP(NPO+MPR),B(NPO),CONV(2*NPO+2),LN(NPO),WT(NH+NQT),    PAR0086
C      1 PRM(NPO+1,MPR),IWP(NPO),SCL(NPO)                                PAR0087
C      DATA EST/'ESTIMATE '/,CVAR/'WEIGHT*.5'/                          PAR0088
C      -----                                                             PAR0089
503     FORMAT(8F10.0)                                                    PAR0090
505     FORMAT(8I10)                                                       PAR0091
507     FORMAT(3F5.0,I5,F5.0,8I5,2F5.0)                                  PAR0092
550     FORMAT(/,'PRIOR ESTIMATES OF PARAMETER SUMS EQUATION',I3,        PAR0093
1       ' INCLUDES MULTIPLE PARAMETERS AND PARAMETER(S) WITH LN > 0 ---',PAR0094
1       /,' STOP EXECUTION (PARLRP)',/)                                  PAR0095
560     FORMAT(/,' PRIOR ESTIMATES OF PARAMETER SUMS',/,' EQ.# : ',4X,    PAR0096
1       18I10,/,5(12X,8I10,/))                                           PAR0097
565     FORMAT(' PAR#  PID')                                              PAR0098
570     FORMAT(I5,4X,A4,4X,8G10.3,/,5(17X,8G10.3,/))                    PAR0099
575     FORMAT(2X,A10,5X,8G10.3,/,5(17X,8G10.3,/))                      PAR0100
580     FORMAT(/,' PARAMETER INFORMATION:',/,                             PAR0101
1       ' (CONVERGENCE CRITERIA LISTED HERE ARE USED TO SOLVE FOR ',    PAR0102
1       ' SENSITIVITY-EQUATION SENSITIVITIES)',/,' # ID ',             PAR0103
1       ' INITIAL VALUE LN  CONVERGENCE CRITERIA  GROUP# ',            PAR0104
1       ' WEIGHT OF PRIOR EST. ')                                         PAR0105
582     FORMAT(/,' PARAMETER INFORMATION',/,                             PAR0106
1       ' (CONVERGENCE CRITERIA LISTED HERE ARE USED TO SOLVE FOR ',    PAR0107
1       ' SENSITIVITY-EQUATION SENSITIVITIES)',/,' # ID ',             PAR0108
1       ' INITIAL VALUE LN  CONVERGENCE CRITERIA  GROUP# ',            PAR0109
1       ' SCALING FACTOR  ', ' WT OF PRIOR EST. ',/)                   PAR0110
584     FORMAT(/,' PARAMETER INFORMATION',/,' # ID ',                   PAR0111
1       ' INITIAL VALUE LN  GROUP# ',                                     PAR0112
1       ' SCALING FACTOR  ', ' WT OF PRIOR EST. ',/)                   PAR0113
585     FORMAT(' ',I5,2X,A4,G14.4,I3,1X,2G13.3,1X,I4,3X,2G14.4)         PAR0114
590     FORMAT(' ',I5,2X,A4,G14.4,I3,I4,3X,2G14.4)                      PAR0115
595     FORMAT(/,' REGRESSION DATA:',                                     PAR0116
$ /1H ,36HMAX. PARAMETER CORRECTION (DMAX) = ,G11.5                    PAR0117
$ /1H ,36HSEARCH DIR. ADJUSTMENT PAR. (CSA) = ,G11.5                  PAR0118
$ /1H ,36HCLOSURE CRITERION (TOL) ----- = ,G11.5                  PAR0119
$ /1H ,36HMAXIMUM NO. OF ITERATIONS (ITMXP) = ,I7,                    PAR0120
$ /1H ,36HMODIFY CONV. CRITERIA (>0) (FCONV) = ,G11.5,              PAR0121
$ /1H ,36HUSE PRIOR PAR EST (>0) (IPRIOR) = ,I7,                    PAR0122
$ /1H ,36HOUTPUT UNIT FOR RESAN (IOUR) ---- = ,I7,                  PAR0123
$ /1H ,36HFORMAT CODE FOR COV AND COR (IPRC) = ,I7,                  PAR0124
$ /1H ,36HPRINT SENS., ETC. (>0) (IPRINT) = ,I7,                    PAR0125
$ /1H ,36HPRINT LAST HEADS (1) (KPRINT) --- = ,I7,                  PAR0126
$ /1H ,36HPRINT EIGEN V&V OF COV(>0) (LPRINT) = ,I7,                PAR0127
$ /1H ,36HCALC. SEN. W/ LAST PAR (>0) (LASTX) = ,I7,                PAR0128
$ /1H ,36HNO. FLETCHER-REEVES ITERS (NFIT) = ,I7,                   PAR0129
$ /1H ,36HSUM OF SQUARES CLOSURE CRIT. (SOSC) = ,G11.5,             PAR0130
$ /1H ,36HCRITERIA FOR ADDING MATRIX R (SOSR) = ,G11.5)             PAR0131
600     FORMAT(/,' ESTIMATED ERROR VARIANCE <= 0 -- ',                 PAR0132
1       ' STOP EXECUTION (PARLRP)',/)                                  PAR0133
610     FORMAT(/,' WARNING -- NP > ND/3 : YOU MAY BE TRYING TO ESTIMATE'  PAR0134
1       ' , TOO MANY PARAMETERS FOR THE DATA (PARLRP)',/)           PAR0135
620     FORMAT(/,' ND MUST BE GREATER THAN NP -- STOP EXECUTION (PARLRP)')PAR0136
630     FORMAT(/,' ERROR IN SCL FOR PARAMETER SUMS EQ#',I5,            PAR0137
1       ' : MULTIPLE PARAMETERS REQUIRE SCL=1.0 -- STOP EXECUTION',    PAR0138
2       ' (PARLRP)')                                                    PAR0139
635     FORMAT(/,' ISN=2, BUT NFIT<ITMXP -- STOP EXECUTION (PARLRP)')    PAR0140
640     FORMAT(/,' FOR ISN>0, LASTX MUST EQUAL 0, 1 OR 2, AND IF LASTX>0,'PAR0141
1       ' ISN MUST EQUAL 4 -- STOP EXECUTION (PARLRP)')                PAR0142
C-----SET ERROR FLAG                                                  PAR0143
1ERR=0                                                                    PAR0144
C-----STATS FOR PRIOR USING INITIAL PARAMETER VALUES (DATA SET 10)    PAR0145
1READ(IU,503)(WP(IP),IP=1,NPO)                                           PAR0146
C-----SPECIFY STATISTIC TYPE (DATA SET 11)                             PAR0147
1READ(IU,505)IWP                                                         PAR0148
C-----READ PRIOR INFORMATION ON SUMS OF PARAMETERS (DATA SET 12)      PAR0149
1IF(MPR.GT.0) THEN                                                       PAR0150
2DO 60 IPM=1,MPR                                                         PAR0151
3READ(IU,503)(PRM(IP,IPM),IP=1,NPO+1),WP(NPO+IPM)                    PAR0152
60 CONTINUE                                                             PAR0153
2ENDIF                                                                    PAR0154
C-----DATA SET 13                                                       PAR0155
1READ(IU,507) DMAX,CSA,TOL,ITMXP,FCONV,IPRIOR,IOUR,IPRC,IPRINT,        PAR0156
2KPRINT,LPRINT,LASTX,NFIT,SOSC,SOSR                                     PAR0157
3WRITE(IOUT,595) DMAX,CSA,TOL,ITMXP,FCONV,IPRIOR,IOUR,IPRC,           PAR0158
4IPRINT,KPRINT,LPRINT,LASTX,NFIT,SOSC,SOSR                             PAR0159
C-----SCALING FACTORS FOR GRADIENT-SEARCH NONLINEAR REGRESSION         PAR0160

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IF(ISN.GT.0.AND.ISN.NE.10) READ(IU,503) (SCL(IP),IP=1,NPO)	PAR0161
C-----ERROR CHECKING	PAR0162
IF(ISN.EQ.2.AND.NFIT.LT.ITMXP) THEN	PAR0163
WRITE(IOUT,635)	PAR0164
IERR=1	PAR0165
ENDIF	PAR0166
IF(ISN.GT.0.AND.(LASTX.GT.2.OR.(LASTX.NE.0.AND.ISN.NE.4))) THEN	PAR0167
WRITE(IOUT,640)	PAR0168
IERR=1	PAR0169
ENDIF	PAR0170
IF(EV.LE.0.) THEN	PAR0171
WRITE(IOUT,600)	PAR0172
IERR=1	PAR0173
ENDIF	PAR0174
C-----OPTION TO IGNORE PRIOR INFORMATION	PAR0175
IF(IPRIOR.EQ.0) THEN	PAR0176
DO 150 IP=1,NPO	PAR0177
150 WP(IP)=0.	PAR0178
MPR=0	PAR0179
ENDIF	PAR0180
C-----CONVERT SCALING FACTORS FOR LOG-TRANSFORMED PARAMETERS	PAR0181
IF(ISN.GT.0) THEN	PAR0182
DO 155 IP=1,NPO	PAR0183
155 IF(LN(IP).GT.0) SCL(IP)=ALOG(SCL(IP))	PAR0184
ENDIF	PAR0185
C-----WRITE HEADER	PAR0186
IF(ISN.LT.0) WRITE(IOUT,580)	PAR0187
IF(ISN.EQ.4) WRITE(IOUT,582)	PAR0188
IF(ISN.GT.0.AND.ISN.LT.4) WRITE(IOUT,584)	PAR0189
C-----LOOP THROUGH PARAMETERS	PAR0190
NPR=0	PAR0191
DO 160 IP=1,NPO	PAR0192
C-----CONVERT STATS OF PRIOR SINGLE-PARAMETER ESTIMATES TO WEIGHTS	PAR0193
IF(WP(IP).NE.0..AND.IP.LE.NP) THEN	PAR0194
BB=B(IP)	PAR0195
IF(LN(IP).GT.0) BB=ALOG(BB)	PAR0196
WPP=WP(IP)	PAR0197
IF(IWP.EQ.2) WPP=WPP*BB	PAR0198
IF(IWP.GT.0) WPP=WPP*WPP	PAR0199
WP(IP)=EV/WPP	PAR0200
NPR=NPR+1	PAR0201
ENDIF	PAR0202
C-----IF GROUP# < 0, SET LN, WP, AND SCL TO ZERO	PAR0203
IF(IP.GT.NP) THEN	PAR0204
LN(IP)=0	PAR0205
WP(IP)=0.	PAR0206
IF(ISN.GT.0) SCL(IP)=0.	PAR0207
ENDIF	PAR0208
C-----PRINT INITIAL PARAMETER VALUES, CONV. CRIT., PARAMETER,	PAR0209
C-----GROUP #, WEIGHT OF PRIOR PARAMETER EST., AND SCALING FACTORS	PAR0210
IF(ISN.LT.0.OR.ISN.EQ.10) THEN	PAR0211
IF(WP(IP).LE.0) WRITE(IOUT,585) IP,PID(IP),B(IP),LN(IP),	PAR0212
CONV(1+IP),CONV(NPO+2+IP),IWPG(IP)	PAR0213
IF(WP(IP).GT.0) WRITE(IOUT,585) IP,PID(IP),B(IP),LN(IP),	PAR0214
CONV(1+IP),CONV(NPO+2+IP),IWPG(IP),WP(IP)	PAR0215
ELSEIF (ISN.EQ.4) THEN	PAR0216
IF(WP(IP).LE.0) WRITE(IOUT,585) IP,PID(IP),B(IP),LN(IP),	PAR0217
CONV(1+IP),CONV(NPO+2+IP),IWPG(IP),SCL(IP)	PAR0218
IF(WP(IP).GT.0) WRITE(IOUT,585) IP,PID(IP),B(IP),LN(IP),	PAR0219
CONV(1+IP),CONV(NPO+2+IP),IWPG(IP),SCL(IP),WP(IP)	PAR0220
ELSEIF (ISN.GT.0.AND.ISN.LT.4) THEN	PAR0221
IF(WP(IP).LE.0) WRITE(IOUT,590) IP,PID(IP),B(IP),LN(IP),	PAR0222
IWPG(IP),SCL(IP)	PAR0223
IF(WP(IP).GT.0) WRITE(IOUT,590) IP,PID(IP),B(IP),LN(IP),	PAR0224
IWPG(IP),SCL(IP),WP(IP)	PAR0225
ENDIF	PAR0226
160 CONTINUE	PAR0227
C-----PRIOR ESTIMATES OF PARAMETER SUMS	PAR0228
IF(MPR.NE.0) THEN	PAR0229
C-----CONVERT STATISTICS TO WEIGHTS; CALCULATE WP**.5 FOR PRINTING	PAR0230
DO 165 IPM=1,MPR	PAR0231
WPP=WP(NPO+IPM)	PAR0232
BB=PRM(NPO+1,IPM)	PAR0233
DO 163 IP=1,NPO	PAR0234
163 IF(PRM(IP,IPM).NE.0..AND.LN(IP).NE.0) BB=ALOG(BB)	PAR0235
PRM(NPO+1,IPM)=BB	PAR0236
IF(IWP.EQ.2) WPP=WPP*BB	PAR0237
IF(IWP.GT.0) WPP=WPP**2.	PAR0238
WP(NPO+IPM)=(EV/WPP)**.5	PAR0239
165 CONTINUE	PAR0240
C-----PRINT	PAR0241
WRITE(IOUT,560) (IPM,IPM=1,MPR)	PAR0242
WRITE(IOUT,565)	PAR0243

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DO 170 IP=1,NPO
170 WRITE(IOUT,570) IP,PID(IP),(PRM(IP,IPM),IPM=1,MPR)
WRITE(IOUT,575) EST,(PRM(NPO+1,IPM),IPM=1,MPR)
WRITE(IOUT,575) CVAR,(WP(NPO+IPM),IPM=1,MPR)
C-----CONVERT FROM WP**.5 TO WP FOR USE IN REGRESSION
DO 171 IPM=1,MPR
171 WP(NPO+IPM)=WP(NPO+IPM)**2.
C-----ERROR CHECKING
DO 174 IPM=1,MPR
ICOUNT=0
IFL=0
IFL2=0
DO 173 IP=1,NPO
IF(PRM(IP,IPM).NE.0) THEN
ICOUNT=ICOUNT+1
IF(ISN.GT.0.AND.SCL(IP).NE.1.) IFL=1
IF(LN(IP).NE.0) IFL2=1
ENDIF
173 CONTINUE
IF(ICOUNT.GT.1.AND.IFL.EQ.1) THEN
WRITE(IOUT,630) IPM
IERR=1
ENDIF
IF(ICOUNT.GT.1.AND.IFL2.EQ.1) THEN
WRITE(IOUT,550) IPM
IERR=1
ENDIF
174 CONTINUE
ENDIF
C-----CHECK NP VERSUS ND
ND=NH+NQT
IF(NP.GT.(ND/3).AND.NP.LT.ND) WRITE(IOUT,610)
IF(NP.GE.ND) THEN
WRITE(IOUT,620)
IERR=1
ENDIF
C-----STOP IF THERE ARE ERRORS IN THE DATA
IF(IERR.NE.0) STOP
C-----INITIALIZE DD
DO 190 IP=1,NPO
190 DD(IP)=0.D00
RETURN
END

C=====PAR0287
SUBROUTINE PARLAS(
1 RSQP,KNT,AP,B,DD,ITERP,G,NP,IP,H,HOBS,SCL,WP,WT,ND,MPR,
2 IOUT,SSX,NFIT,ITG,PID,BUFF,B1,C,XX,LN,IFO,LASTX,ADMX,PRM,
3 IPAR,TOL,ITMKP,NPR,RSQO,AGMX,DID,NDER,ROFF,COFF,TOFF,NH,
4 NQT,IQOB,IDRY,IWPG,IQUB,EV,ISN,ISN1,SCLE,CC,NPO)
C-----VERSION 1000 01FEB1992 PARLAS
C *****
C FOR GRADIENT-SEARCH NONLINEAR OPTIMIZATION
C IP=0: CALCULATE THE SUM OF SQUARED ERRORS
C IP=1: CALCULATE SEARCH DIRECTION
C *****
C SPECIFICATIONS:
C -----
C CHARACTER*4 PID(NP),DID(ND)
C DOUBLE PRECISION C((NP*NP/2)+NP),DD(NP),SSG,BDP,SCLDP,XX(NP),
1 G(NP),TEMP,XD,XHX,SUM,GAM,BUFF(NP),CC(NP,NP),SCLE(NP)
C DIMENSION B(NPO),SCL(NP),H(ND),HOBS(ND),WP(NP+MPR),WT(ND),
1 B1(NPO),LN(NP),PRM(NPO+1,MPR),NDER(4,ND),ROFF(ND),COFF(ND),
1 TOFF(ND),IQOB(NQT),IWPG(NP)
C -----
C 514 FORMAT (/, ' ITERATION NO. = ',I5)
521 FORMAT (//, ' RSQ(W/PARAMETERS) = ',G11.5/,
1 ' ERROR VARIANCE--- = ',G11.5/,
1 ' CORRELATION COEF. = ',G11.5/,
1 ' W/PARAMETERS = ',G11.5/,
1 ' ITERATIONS----- = ',I5)
525 FORMAT(//, ' CONVERGENCE ACHIEVED',/, ' CONVERGENCE CRITERIA :',/,
$ 2X, ' MAX. FRACTIONAL PAR. CHANGE (ADMX) = ',G11.5/,
1 2X, ' MAX. NORM OF GRADIENT (AGMX) = ',G11.5)
530 FORMAT(//, ' RSQ NOT REDUCED, BACK UP 50 PERCENT ALONG DIRECTION',
1 ' VECTOR')
540 FORMAT(//, ' RSQ NOT REDUCED IN THIS DIRECTION -- STOP EXECUTION',
1 ' (PARLAS)')
545 FORMAT(//, ' QUASI-NEWTON METHOD',/)
550 FORMAT(//, ' FLETCHER-REEVES METHOD',/)
555 FORMAT(//, ' FLETCHER-REEVES ITERATION PARAMETER :',/

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      $,2X,' SUM OF SQUARED COMPONENTS OF GRADIENT = ',G11.5,/
      $,2X,' PREVIOUS SUM OF SQUARED COMP. OF GRAD = ',G11.5,/
      $,2X,' ITERATION PARAMETER = RATIO OF SUMS = ',G11.5,/
560 FORMAT(2X,' DIRECTION = -GRADIENT')
562 FORMAT(13(5X,A4,9X,A4,9X,A4,9X,A4,9X,A4,9X,A4,
1    9X,A4,9X,A4,9X,A4,9X,A4,))
570 FORMAT(/' SCALED SEARCH DIRECTION :',/ )
575 FORMAT(1H0,10(1H ,G11.5,1X))
585 FORMAT(/,' FINAL APPROXIMATE QUASI-NEWTON INVERSE HESSIAN MATRIX')
587 FORMAT(12(/,1X,10G13.6))
590 FORMAT(/,' CHANGE IN GRADIENT VECTOR * DIRECTION VECTOR',
1    ' LESS THAN OR EQUAL TO -0.0001 ON ITERATION NO. ',I5,
1    ' ; VALUE = ',G11.5,' (PARIAS)')
595 FORMAT(/,' PARAMETER ESTIMATION DID NOT CONVERGE -- STOP ',
1    ' EXECUTION (PARIAS)')
600 FORMAT(F10.0,I5,/,F10.0)
605 FORMAT(/,' SCALING FROM MODIFIED GAUSS-NEWTON:')
610 FORMAT(/,' UNSCALED GRADIENT OF THE OBJECTIVE FUNCTION WITHOUT',
1    ' CONTRIBUTION FROM PRIOR:')
615 FORMAT(/,' SCALED GRADIENT OF THE OBJECTIVE FUNCTION WITH PRIOR:')
620 FORMAT(' INITIAL QUASI-NEWTON MATRIX FROM MODIFIED ',
1    ' GAUSS-NEWTON')
C
      IF(ISN1.EQ.10) ITERP=ITERP-1
C-----DO THE FOLLOWING WHEN IP=0
      IF(IP.EQ.0) THEN
C-----INITIALIZE ITG (COUNTER FOR QN)
      IF(ITERP.EQ.1) ITG=1
C-----CHECK FOR REDUCTION IN SUM OF SQUARED ERRORS
      IF(ITERP.GT.1) THEN
        IF(RSQO-RSQP.GT.-0.0001) GO TO 70
        KNT=KNT+1
        IF(ITERP.EQ.ITMXP) THEN
          WRITE(IOUT,595)
          CALL SSEN10(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBBS,WT,DID,NDER,
2             ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,
3             RSQ,RSQP,1,LN,RSQH,NPO)
          IF(IOUB.GT.0) CALL SPAR1P(PID,BUFF,NP,IOUB,IOUT,ISN)
          STOP
        ENDIF
        IF(KNT.GT.5) THEN
          WRITE(IOUT,540)
          CALL SSEN10(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBBS,WT,DID,NDER,
2             ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,
3             RSQ,RSQP,1,LN,RSQH,NPO)
          IF(IOUB.GT.0) CALL SPAR1P(PID,BUFF,NP,IOUB,IOUT,ISN)
          STOP
        ENDIF
        WRITE(IOUT,530)
        DO 10 IIP=1,NP
10      IF(LN(IIP).NE.0) B(IIP)=ALOG(B(IIP))
          AP=.5*AP
          DO 60 IIP=1,NP
60      B(IIP)=B(IIP)-AP*DD(IIP)
          DO 90 IIP=1,NP
90      IF(LN(IIP).GT.0) B(IIP)=EXP(B(IIP))
          IF(IOUB.GT.0) THEN
            ZERO=0.
            IZERO=0
            WRITE(IOUT,600) ZERO,IZERO,ZERO
          ENDIF
          GO TO 80
70      KNT=0
        ENDIF
C-----SAVE SUM OF SQUARED ERRORS
        RSQO=RSQP
80      IF(ISN1.EQ.10) ITERP=ITERP+1
        RETURN
      ENDIF
C
C-----DO THE FOLLOWING WHEN THE GRADIENT IS AVAILABLE (IP=1)
C-----DEFINE FLAG WHEN ISN=10
      IITERP=ITERP
      IF(ISN1.EQ.10.AND.(ITERP.EQ.1.OR.MOD(ITERP-1,NFIT+1).EQ.0))
1    IITERP=1
C-----ASSIGN SCALE IF ISN=10
      IF(ISN1.EQ.10.AND.IITERP.EQ.1) THEN
        DO 91 IIP=1,NP
91      SCL(IIP)=1./SCLE(IIP)
        WRITE(IOUT,605)
        WRITE(IOUT,562) (PID(IIP),IIP=1,NP)
        WRITE(IOUT,575) (SCL(IIP),IIP=1,NP)
      ENDIF

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C-----NATURAL LOG CONVERSIONS	PAR0408
DO 92 IIP=1,NP	PAR0409
IF(LN(IIP).NE.0) THEN	PAR0410
XX(IIP)=B(IIP)*XX(IIP)	PAR0411
B(IIP)=ALOG(B(IIP))	PAR0412
ENDIF	PAR0413
92 CONTINUE	PAR0414
C-----PRINT UNSCALED GRADIENT WITHOUT PRIOR INFORMATION	PAR0415
IF(ITERP.EQ.1) THEN	PAR0416
WRITE(IOUT,610)	PAR0417
WRITE(IOUT,562) (PID(IIP),IIP=1,NP)	PAR0418
WRITE(IOUT,575) (XX(IIP),IIP=1,NP)	PAR0419
ENDIF	PAR0420
C-----SCALING	PAR0421
DO 95 IIP=1,NP	PAR0422
XX(IIP)=XX(IIP)*SCL(IIP)	PAR0423
95 CONTINUE	PAR0424
C-----ADD PRIOR COMPONENTS TO GRADIENT	PAR0425
C-----PRIOR ESTIMATES OF SINGLE PARAMETERS	PAR0426
IF(IPAR.GT.0) THEN	PAR0427
IF(NPR.GT.0) THEN	PAR0428
DO 100 IIP=1,NP	PAR0429
100 IF(WP(IIP).GT.0) XX(IIP)=XX(IIP)-2.*(WP(IIP))*	PAR0430
1 (B1(IIP)-B(IIP))*SCL(IIP)	PAR0431
ENDIF	PAR0432
C-----PRIOR ESTIMATES OF PARAMETER SUMS	PAR0433
IF(MPR.GT.0) THEN	PAR0434
DO 130 IMP=1,MPR	PAR0435
TEMP=0.	PAR0436
DO 110 IIP=1,NPO	PAR0437
110 TEMP=TEMP+PRM(IIP,IMP)*B(IIP)	PAR0438
DO 120 IIP=1,NP	PAR0439
120 XX(IIP)=XX(IIP)-2.*PRM(IIP,IMP)*WP(NPO+IMP)*	PAR0440
1 (PRM(NPO+1,IMP)-TEMP)*SCL(IIP)	PAR0441
130 CONTINUE	PAR0442
ENDIF	PAR0443
ENDIF	PAR0444
C-----PRINT GRADIENT	PAR0445
WRITE(IOUT,615)	PAR0446
WRITE(IOUT,562) (PID(IIP),IIP=1,NP)	PAR0447
WRITE(IOUT,575) (XX(IIP),IIP=1,NP)	PAR0448
C-----IF IPAR=0, RETURN	PAR0449
IF(IPAR.EQ.0) GO TO 340	PAR0450
C-----SAVE GRADIENT FOR THE FIRST ITERATION	PAR0451
IF(IITERP.EQ.1) THEN	PAR0452
DO 140 IIP=1,NP	PAR0453
140 G(IIP)=XX(IIP)	PAR0454
ENDIF	PAR0455
C-----INITIALIZE	PAR0456
AGMX=0.	PAR0457
C-----THE FOLLOWING IS DONE ONLY IF IITERP>1.	PAR0458
IF(IITERP.GT.1) THEN	PAR0459
XD=0.	PAR0460
C-----COMPUTE MAXIMUM NORM OF GRADIENT (AGMX), GRADIENT DIFFERENCE	PAR0461
C-----STORE IN XX, AND XX*DD (XD). STORE MOST RECENT GRADIENT IN G.	PAR0462
DO 150 IIP=1,NP	PAR0463
TEMP=XX(IIP)	PAR0464
TMP=ABS(TEMP)	PAR0465
IF(TMP.GT.AGMX) AGMX=TMP	PAR0466
XX(IIP)=TEMP-G(IIP)	PAR0467
XD=XD+XX(IIP)*DD(IIP)	PAR0468
150 G(IIP)=TEMP	PAR0469
C-----CHECK FOR CONVERGENCE	PAR0470
IF(ADMX.LE.TOL.AND.AGMX.LE.TOL) THEN	PAR0471
IFO=1	PAR0472
WRITE(IOUT,525) ADMX,AGMX	PAR0473
IF(ISN1.EQ.10) LASTX=1	PAR0474
C-----IF GAUSS-NEWTON STATISTICS ARE NOT CALCULATED . . .	PAR0475
C-----CALCULATE AND PRINT STATISTICS AND RESIDUALS	PAR0476
IF(LASTX.EQ.0) THEN	PAR0477
CALL SPAR1A(ND,WT,HOBS,H,R,R1,NPR,MPR,B1,NP,WP,B,PRM,NPO)	PAR0478
DO 160 IIP=1,NP	PAR0479
160 IF(LN(IIP).NE.0) B(IIP)=EXP(B(IIP))	PAR0480
CALL SSEN10(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBS,WT,DID,NDER,	PAR0481
2 ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,	PAR0482
3 RSQ,RSQP,1,LN,RSQH,NPO)	PAR0483
IF(IOUB.GT.0) CALL SPAR1P(PID,BUFF,NP,IOUB,IOUT,ISN)	PAR0484
VAR=RSQP/(ND-IDRY+NPR+MPR-NP)	PAR0485
WRITE(IOUT,521) RSQP,VAR,R,R1,ITERP	PAR0486
CALL SPAR1M(RSQP,WT,NP,ND,WP,MPR,IOUT,EV,NPR)	PAR0487
C-----PRINT QUASI-NEWTON MATRIX, IF USED ON LAST ITERATION	PAR0488
IF(ITERP.GT.NFIT) THEN	PAR0489
WRITE(IOUT,585)	PAR0490



	IP1=1	PAR0491
	IP2=0	PAR0492
	DO 180 IIP=1,NP	PAR0493
	IF(IIP.GT.1) IP1=IP1+(NP-(IIP-1)+1)	PAR0494
	IP2=IP2+(NP-IIP+1)	PAR0495
180	WRITE(IOUT,587) (C(IIP),IIP=IP1,IP2)	PAR0496
	ENDIF	PAR0497
	RETURN	PAR0498
	ENDIF	PAR0499
	GO TO 340	PAR0500
	ENDIF	PAR0501
	C-----EXCEEDED MAXIMUM PARAMETER-ESTIMATION ITERATIONS?	PAR0502
	IF(ITERP.EQ.ITMXP.OR.(ISN1.EQ.10.AND.ITERP.EQ.ITMXP-1)) THEN	PAR0503
	WRITE(IOUT,595)	PAR0504
	DO 185 IIP=1,NP	PAR0505
185	IF(LN(IIP).NE.0) B(IIP)=EXP(B(IIP))	PAR0506
	CALL SSEN10(NP,B,B1,IWPG,PID,WP,IOUT,NH,H,HOBS,WT,DID,NDER,	PAR0507
2	ROFF,COFF,TOFF,NQT,IQOB,ND,IPAR,NPR,MPR,PRM,	PAR0508
3	RSQ,RSQP,1,LN,RSQH,NPO)	PAR0509
	IF(IOUB.GT.0) CALL SPAR1P(PID,BUFF,NP,IOUB,IOUT,ISN)	PAR0510
	STOP	PAR0511
	ENDIF	PAR0512
	C-----IF XD IS ZERO OR NEGATIVE, DON'T CALCULATE A NEW HESSIAN MATRIX	PAR0513
	C-----USE SAME HESSIAN AND THE NEW GRADIENT TO CALCULATE DISPLACEMENT	PAR0514
	IF(XD.LE.0.) WRITE(IOUT,590) ITERP+1,XD	PAR0515
	ENDIF	PAR0516
	C	PAR0517
	C-----COMPUTE DISPLACEMENT VECTOR	PAR0518
	C-----FLETCHER-REEVES METHOD	PAR0519
	IF(ITERP.LE.NFIT.AND.ISN1.NE.10) THEN	PAR0520
	IF(ITERP.EQ.1) WRITE(IOUT,550)	PAR0521
	SSG=0.	PAR0522
	DO 190 IIP=1,NP	PAR0523
190	SSG=SSG+G(IIP)*G(IIP)	PAR0524
	IF(ITERP.EQ.1.OR.MOD(ITERP-1,NP).EQ.0) THEN	PAR0525
	DO 200 IIP=1,NP	PAR0526
200	DD(IIP)=-G(IIP)	PAR0527
	WRITE(IOUT,560)	PAR0528
	ELSE	PAR0529
	BETA=SSG/SSX	PAR0530
	DO 210 IIP=1,NP	PAR0531
210	DD(IIP)=-G(IIP)+BETA*DD(IIP)	PAR0532
	WRITE(IOUT,555) SSX,SSG,BETA	PAR0533
	ENDIF	PAR0534
	SSX=SSG	PAR0535
	GO TO 330	PAR0536
	ENDIF	PAR0537
	C-----QUASI-NEWTON METHOD	PAR0538
	C-----INITIAL APPROXIMATE INVERSE HESSIAN MATRIX	PAR0539
	IF(IITERP.EQ.NFIT+1.OR.(ISN1.EQ.10.AND.IITERP.EQ.1)) THEN	PAR0540
	WRITE(IOUT,545)	PAR0541
	K=0	PAR0542
	IF(ISN1.EQ.10) THEN	PAR0543
	WRITE(IOUT,620)	PAR0544
	CALL SPAR1I(NP,CC)	PAR0545
	DO 215 IIP=1,NP	PAR0546
	DO 215 I=IIP,NP	PAR0547
	K=K+1	PAR0548
215	C(K)=-2.*CC(I,IIP)	PAR0549
	GO TO 295	PAR0550
	ENDIF	PAR0551
	DO 230 IIP=1,NP	PAR0552
	KT=K+1	PAR0553
	DO 220 I=IIP,NP	PAR0554
	K=K+1	PAR0555
220	C(K)=0.	PAR0556
	BDP=B(IIP)	PAR0557
	SCLDP=SCL(IIP)	PAR0558
	LNN=LN(IIP)	PAR0559
	IF(LNN.EQ.0) BDP=BDP/SCLDP	PAR0560
	IF(LNN.NE.0) BDP=BDP-ALOG(SCL(IIP))	PAR0561
230	C(KT)=(BDP)**2	PAR0562
	ENDIF	PAR0563
	C-----SUBSEQUENT APPROXIMATE INVERSE HESSIAN MATRIX	PAR0564
	IF(IITERP.GT.NFIT+1.OR.(ISN1.EQ.10.AND.IITERP.NE.1)) THEN	PAR0565
	K=0	PAR0566
	XHX=0.	PAR0567
	DO 270 IIP=1,NP	PAR0568
	SUM=0.	PAR0569
	M=NP-IIP+1	PAR0570
	L=K+1	PAR0571
	DO 240 I=1,M	PAR0572
	K=K+1	PAR0573

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240      SUM=SUM+C(K)*XX(I+IIP-1)
          N=IIP-1
          IF(N.LT.1) GO TO 260
          DO 250 I=1,N
              L=L-M
              SUM=SUM+C(L)*XX(N-I+1)
250      M=M+1
260      BUFF(IIP)=SUM
270      XHX=XHX+XX(IIP)*SUM
          GAM=1.
          IF(ITG.LT.2) GAM=AP*XD/XHX
          TEMP=(AP+GAM*XHX/XD)/XD
          K=0
          DO 290 IIP=1,NP
              DO 280 I=IIP,NP
                  K=K+1
280          C(K)=(C(K)-(BUFF(I)*DD(IIP)+DD(I)*BUFF(IIP))/XD)*GAM+
1          TEMP*DD(I)*DD(IIP)
290      CONTINUE
          ITG=2
          ENDIF
C-----DISPLACEMENT VECTOR
295      K=0
          DO 320 IIP=1,NP
              SUM=0.
              M=NP-IIP+1
              L=K+1
              DO 300 I=1,M
                  K=K+1
300          SUM=SUM+C(K)*G(I+IIP-1)
              N=IIP-1
              IF(N.LT.1) GO TO 320
              DO 310 I=1,N
                  L=L-M
                  SUM=SUM+C(L)*G(N-I+1)
310          M=M+1
320      DD(IIP)=-SUM
330      CONTINUE
C-----PRINT RESULTS
          WRITE(IOUT,570)
          WRITE(IOUT,575) (DD(IIP),IIP=1,NP)
340      IF(IFO.GT.0.AND.IOUB.GT.0) THEN
          ZERO=0.
          IZERO=0
          WRITE(IOUB,600) ZERO,IZERO,ZERO
          ENDIF
C-----CONVERT TO PHYSICAL PARAMETERS FROM NATURAL LOGS
          DO 350 IIP=1,NP
350      IF(LN(IIP).NE.0) B(IIP)=EXP(B(IIP))
          IF(ISN1.EQ.10) ITERP=ITERP+1
          RETURN
          END

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PAR0625

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C=====
      SUBROUTINE PARLAQ(
1      ND,HOBS,H,BL,B,DD,NP,WT,WP,PID,HNEW,NCOL,NROW,NLAY,ISN,IP,SCL,
2      PV,NH,NDER,IOFF,JOFF,KPER,MLAY,IBOUND,RINT,DID,COFF,ROFF,DELR,
3      DELC,PR,MOBS,LN,NQT,TOFF,NQ,NQC,NQOB,NQCL,IQOB,QCLS,IBT,
4      MXBND,NBOUND,BNDS,MXRIVR,NRIVER,RIVR,SHNW,NPER,MXDRN,NDRAIN,
5      DRAI,MXSTRM,NSTREM,STRM,ISTRM,ADMX,PRM,MPR,IOUT,DMX,DMAX,AP,
6      NPR,ITERP,AGMX,MAXM,JDRY,IPAR,IOUB,NPO)
C-----VERSION 1000 01FEB1992 PARLAQ
C *****
C      NONLINEAR REGRESSION BY CONJUGATE-DIRECTION METHODS:
C      CALCULATE FINAL ITERATION PARAMETER AND UPDATE PARAMETERS
C *****
C      SPECIFICATIONS:
C -----
C      CHARACTER*4 PID(NP),DID(NH+NQT)
C      DOUBLE PRECISION HNEW(NCOL,NROW,NLAY),DD(NP),SWS,SWY,DDSCL,
1      TMP,F,PV,SCLDP
C      DIMENSION B(NPO),BL(NPO),HOBS(ND),H(ND),WT(ND),WP(NPO+MPR),
1      SCL(NPO),NDER(5,NH),DELR(NCOL),DELC(NROW),
1      IBOUND(NCOL,NROW,NLAY),COFF(NH),ROFF(NH),RINT(4,NH),JOFF(NH),
1      IOFF(NH),MLAY(MAXM,MOBS),PR(MAXM,MOBS),LN(NP),RIVR(6,MXRIVR),
1      BNDS(5,MXBND),IBT(2,NQ),NQOB(NQ),IQOB(NQT),QCLS(4,NQC),
1      TOFF(NH+NQT),DRAI(5,MXDRN),PV(ND),STRM(11,MXSTRM),
1      ISTRM(5,MXSTRM),PRM(NPO+1,MPR),NQCL(NQ)
C -----
C      514 FORMAT (/
          $' VALUES FROM CONJUGATE-DIRECTION REGRESSION PROCEDURE, ',

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PAR0652  
PAR0653  
PAR0654

\$'ITERATION',I3,' :',/	PAR0655
\$ 2X,' ITERATION PARAMETER (ALPH) = ',G11.5,/,	PAR0656
\$ 2X,' FACTOR FOR SCALING PAR. CHANGE (AP)= ',G11.5,/,	PAR0657
\$ 2X,' MAX. FRACTIONAL PAR. CHANGE (DMX) = ',G11.5,/,	PAR0658
\$ 2X,' MAX. FRAC. CHANGE OCCURRED FOR PAR.# ',I6,/,	PAR0659
1 2X,' MAX. NORM OF GRADIENT (AGMX) = ',G11.6,/,	PAR0660
1 /' UPDATED ESTIMATES OF REGRESSION PARAMETERS :',/	PAR0661
1,13(5X,A4,9X,A4,9X,A4,9X,A4,9X,A4,9X,A4,	PAR0662
1 9X,A4,9X,A4,9X,A4,9X,A4,/,)	PAR0663
530 FORMAT(E10.3,I5,/,E10.3)	PAR0664
540 FORMAT(8G10.3)	PAR0665
570 FORMAT(/	PAR0666
\$,2X,' ITERATION PARAMETER = ',G11.5,/,	PAR0667
\$,2X,' NUMERATOR OF ITERATION PARAMETER = ',G11.5,/,	PAR0668
\$,2X,' DENOMINATOR OF ITERATION PARAMETER = ',G11.5,/,)	PAR0669
575 FORMAT (1H0,10(1H ,G11.5,1X))	PAR0670
C-----INTERPOLATE ITERATION PARAMETER VECTOR TO HEAD LOCATIONS	PAR0671
IF(NH.GT.0) THEN	PAR0672
IF(KPER.EQ.1) THEN	PAR0673
DO 10 N=1,NH	PAR0674
10 PV(N)=0.DO	PAR0675
ENDIF	PAR0676
CALL SSEN1U(NH,NDER,IOFF,JOFF,KPER,MLAY,IBOUND,RINT,	PAR0677
1 DID,COFF,ROFF,DELR,DELC,NCOL,NROW,NLAY,PR,H,HOBS,WT,HNEW,	PAR0678
2 X,IP,IDRY,NP,MOBS,B,LN,ISN,NQT,TOFF,NPER,RHS,PV,	PAR0679
3 MAXM,ITERP,JDRY,IPAR,IOUT)	PAR0680
ENDIF	PAR0681
C-----CALCULATE ITERATION PARAMETER VECTOR VALUES FOR HEAD-DEPENDENT	PAR0682
C-----FLOW BOUNDARY DATA	PAR0683
IF(NQ.GT.0) THEN	PAR0684
ITS=KPER-1	PAR0685
C-----INITIALIZE COMPONENTS OF PV	PAR0686
IF(ITS.EQ.0) THEN	PAR0687
DO 30 NT=1,NQT	PAR0688
30 PV(NH+NT)=0.	PAR0689
ENDIF	PAR0690
CALL SSEN1V(NQ,NQC,NQT,NQOB,NQCL,IQOB,QCLS,IBT,MXBND,NBOUND,	PAR0691
1 BNDS,MXRIVR,NRIVER,RIVR,SHNW,IP,HNEW,NCOL,NROW,NLAY,	PAR0692
1 IOUT,IBOUND,NPER,KPER,NH,PV,DID,NP,FLAGD,H,B,LN,TOFF,	PAR0693
1 MXDRN,NDRAIN,DRAI,MXSTRM,NSTREM,STRM,ISTRM,ISN,RHS,WT,HOBS)	PAR0694
ENDIF	PAR0695
IF(KPER.NE.NPER) RETURN	PAR0696
C-----PARAMETER CONVERSIONS FOR NATURAL LOG OPTIONS	PAR0697
DO 50 IIP=1,NP	PAR0698
50 IF(LN(IIP).NE.0) B(IIP)=ALOG(B(IIP))	PAR0699
C-----CALCULATE ITERATION PARAMETER	PAR0700
C-----INITIALIZE VARIABLES	PAR0701
SWS=0.DO	PAR0702
SWY=0.DO	PAR0703
C-----DEPENDENT VARIABLES	PAR0704
DO 220 N=1,ND	PAR0705
F=PV(N)	PAR0706
W=WT(N)	PAR0707
IF(W.LT.0.) W=1.E-20	PAR0708
TMP=F*W	PAR0709
TMPA=HOBS(N)-H(N)	PAR0710
SWS=SWS+TMP*F	PAR0711
220 SWY=SWY+TMP*TMPA	PAR0712
C-----PRIOR ESTIMATES OF SINGLE PARAMETERS	PAR0713
IF(NPR.GT.0) THEN	PAR0714
DO 230 IIP=1,NP	PAR0715
IF(WP(IIP).GT.0.) THEN	PAR0716
LNN=LN(IIP)	PAR0717
SCLL=SCL(IIP)	PAR0718
DDSCL=DD(IIP)*SCLL	PAR0719
TMPA=B1(IIP)-B(IIP)	PAR0720
TMP=DDSCL*WP(IIP)	PAR0721
SWS=SWS+TMP*DDSCL	PAR0722
SWY=SWY+TMP*TMPA	PAR0723
ENDIF	PAR0724
230 CONTINUE	PAR0725
ENDIF	PAR0726
C-----PRIOR ESTIMATES OF PARAMETER SUMS	PAR0727
IF(MPR.GT.0) THEN	PAR0728
TMPA=0.	PAR0729
SCLDP=1.DO	PAR0730
DO 300 IPM=1,MPR	PAR0731
DO 298 IIP=1,NPO	PAR0732
IF(PRM(IIP,IPM).EQ.0.) GO TO 298	PAR0733
IF(SCL(IIP).NE.1.) SCLDP=SCL(IIP)	PAR0734
TMPA=TMPA+PRM(IIP,IPM)*B(IIP)	PAR0735
298 CONTINUE	PAR0736
TMPA=PRM(NPO+1,IPM)-TMPA	PAR0737

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DO 299 IIP=1,NPO
  IF(PRM(IIP,IPM).EQ.0.) GO TO 299
  SCLDP=SCL(IIP)
  DDSCL=DD(IIP)*PRM(IIP,IPM)*SCLDP
  IF(LN(IIP).NE.0) DDSCL=DD(IIP)+ALOG(SCL(IIP))
  TMP=DDSCL*WP(NPO+IPM)
  SWS=SWS+TMP*DDSCL
  SWY=SWY+TMP*TMPA
299  CONTINUE
300  CONTINUE
ENDIF
C-----ITERATION PARAMETER
  ALPH=SWY/SWS
C-----UPDATE PARAMETERS
  ADMX=0.
  DO 255 IIP=1,NP
    LNN=LN(IIP)
    SCLL=SCL(IIP)
    BB=B(IIP)
    TMPA=1.
    IF(BB.NE.0.) TMPA=BB
    IF(LNN.NE.0.AND.ABS(TMPA).LT..00001) TMPA=1.
    TMPA=TMPA/SCLL
    TMPA=(ALPH*DD(IIP)/TMPA)
    IF(LNN.GT.0) TMPA=EXP(ALPH*DD(IIP))-1.
    TMP=ABS(TMPA)
    IF((LNN.EQ.0.AND.TMP.LE.ADMX).OR.
1    (LNN.NE.0.AND.TMPA.LE.ADMX)) GO TO 255
    ADMX=TMP
    JJ=IIP
    DMX=TMPA
    LNMX=0
    IF(LNN.NE.0) LNMX=1
255  CONTINUE
    AP=1.
    IF(LNMX.EQ.0.AND.ADMX.GT.DMX) AP=DMX/ADMX
    IF(LNMX.NE.0.AND.ALPHA*DD(JJ).GT.ALOG(DMX+1.))
1    AP=ALOG(DMX+1.)/(ALPHA*DD(JJ))
C-----COMPUTE NEW PARAMETER VECTOR
  DO 260 IIP=1,NP
    LNN=LN(IIP)
    SCLL=SCL(IIP)
    IF(LNN.EQ.0) DDSCL=DD(IIP)*SCLL
    IF(LNN.NE.0) DDSCL=DD(IIP)
260  B(IIP)=B(IIP)+AP*ALPH*DDSCL
C-----PARAMETER CONVERSIONS FOR NATURAL LOG OPTIONS
  DO 270 IIP=1,NP
270  IF(LN(IIP).NE.0) B(IIP)=EXP(B(IIP))
C-----PRINT RESULTS
  WRITE(IOUT,514) ITERP,ALPH,AP,DMX,JJ,AGMX,(PID(IIP),IIP=1,NP)
  WRITE(IOUT,575) (B(IIP),IIP=1,NP)
  IF(IOUB.GT.0) THEN
    WRITE(IOUB,530) DMX,JJ,AGMX
    WRITE(IOUB,540) (B(IIP),IIP=1,NP)
  ENDIF
  AP=ALPH*AP
  RETURN
END

C=====
SUBROUTINE PARLAP(
1  X,B,ND,NP,HOBS,WT,WP,C,SCLE,G,H,DD,DMAX,CSA,TOL,PID,IND,IFO,
2  AMP,AP,DMX,IOUT,B1,ITERP,IPRINT,ADMX,LN,LASTX,MPR,PRM,NPR,
3  IOUB,RSQP,JMAX,ITMXP,ISN1,NFIT,NPO,R,GD,U,NOPT,XD,NPER,
4  S,SOSR)
C-----VERSION 1000 01FEB1992
C *****
C REGRESSION BY THE MODIFIED GAUSS-NEWTON METHOD
C *****
C SPECIFICATIONS:
C -----
C CHARACTER*4 PID(NP)
C DOUBLE PRECISION C(NP,NP),SCLE(NP),DD(NP),DTMPA,R(NP*NP/2+NP),
1  S(NP),U(NP),G,GD,DTMP
C DIMENSION X(NP,ND),B(NPO),HOBS(ND),WT(ND),WP(NPO+MPR),H(ND),
1  B1(NPO),G(NP),LN(NP),PRM(NPO+1,MPR),GD(NP),XD(NP,ND)
C -----
500 FORMAT(/,' SCALED LEAST-SQUARES MATRIX :')
508 FORMAT(/,' UNSCALED RIGHT-HAND SIDE VECTOR (= -0.5*GRADIENT)')
510 FORMAT(/,' SCALED GRADIENT VECTOR :')
514 FORMAT(/,' ITERATION NO. = ',I5,/,
$' VALUES FROM LEAST-SQUARES REGRESSION PROCEDURE :',/

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$ 2X, ' DET OF SCALED LEAST-SQUARES MATRIX = ',G11.5,/,
$ 2X, ' MARQUARDT PARAMETER (AMP)----- = ',G11.5,/,
$ 2X, ' FACTOR FOR SCALING PAR. CHANGE (AP) = ',G11.5,/,
$ 2X, ' MAX. FRACTIONAL PAR. CHANGE (DMX) = ',G11.5,/,
$ 2X, ' MAX. FRAC. CHANGE OCCURRED FOR PAR.# ',I6,/,
$/ ' UPDATED ESTIMATES OF REGRESSION PARAMETERS : ',/
1,13(5X,A4,9X,A4,9X,A4,9X,A4,9X,A4,9X,A4,9X,A4,
1 9X,A4,9X,A4,9X,A4,9X,A4,/)
516 FORMAT (1H0,10(1H ,G11.5,1X))
530 FORMAT(E10.3,I5)
600 FORMAT(/, ' PARAMETER ESTIMATION CONVERGED BY SATISFYING TOL',
1 ' CRITERIA',/)
C
C-----INITIALIZE SOME VARIABLES.
NP1=NP-1
AMP=0.
IND=0
C-----ASSEMBLE LEAST-SQUARES MATRIX (C) AND GRADIENT VECTOR (G)
C-----INITIALIZE C AND CONVERT LN PARAMETERS
DO 60 IP=1,NP
DO 50 I=1,NP
50 C(I,IP)=0.D00
IF(LN(IP).NE.0) B(IP)=ALOG(B(IP))
60 G(IP)=0.
C-----CALCULATE SENSITIVITY CONTRIBUTIONS TO C AND G.
C-----CALCULATE SUM OF SQUARED RESIDUALS.
DO 90 N=1,ND
TMPA=HOBS(N)-H(N)
W=WT(N)
IF(W.LT.0.) THEN
W=1.E-20
WT(N)=-WT(N)
ENDIF
DO 80 IP=1,NP
DTMPA=DBLE(W)*DBLE(X(IP,N))
DO 70 I=IP,NP
70 C(I,IP)=DBLE(X(I,N))*DTMPA+C(I,IP)
80 G(IP)=DTMPA*TMPA+G(IP)
90 CONTINUE
C-----FOR FIRST ITERATION, PRINT UNSCALED GRADIENT WITHOUT PRIOR
IF(ITERP.EQ.1) THEN
WRITE(IOUT,508)
WRITE(IOUT,516) (G(IP),IP=1,NP)
ENDIF
C-----ACCOUNT FOR PRIOR INFORMATION
C-----SINGLE PARAMETER ESTIMATES
IF(NPR.GT.0) THEN
DO 93 IP=1,NP
IF(WP(IP).GT.0.) THEN
C(IP,IP)=C(IP,IP)+WP(IP)
G(IP)=G(IP)+WP(IP)*(B1(IP)-B(IP))
ENDIF
93 CONTINUE
ENDIF
C-----ESTIMATES OF PARAMETER SUMS
IF(MPR.GT.0) THEN
DO 97 IPM=1,MPR
TMPA=0.
DO 94 IP=1,NPO
94 IF(PRM(IP,IPM).GT.0.) TMPA=TMPA+PRM(IP,IPM)*B(IP)
TMPA=PRM(NPO+1,IPM)-TMPA
DO 96 IP=1,NPO
IF(PRM(IP,IPM).EQ.0.) GO TO 96
DTMPA=DBLE(WP(NPO+IPM))*DBLE(PRM(IP,IPM))
DO 95 I=IP,NPO
95 C(I,IP)=DBLE(PRM(I,IPM))*DTMPA+C(I,IP)
G(IP)=DTMPA*TMPA+G(IP)
96 CONTINUE
97 CONTINUE
ENDIF
C-----QUASI-NEWTON ADDITION TO COEFFICIENT MATRIX
IF((NFIT.GT.0.OR.SOSR.GT.0.).AND.NOPT.EQ.1.AND.IFO.EQ.0)
1 CALL SPARIQ(C,DD,G,NP,R,GD,U,ITERP,1,X,ND,HOBS,H,WT,
2 S,NFIT,B1,B,WP,NPR,MPR,PRM,NPO,XD,NPER,SOSR)
C-----FOR ONE PARAMETER CASE
IF(NP.LT.2) GO TO 140
C-----SCALE COEFFICIENT MATRIX AND GRADIENT VECTOR
DO 100 IP=1,NP
SCLE(IP)=1.D00
100 IF(C(IP,IP).GT.1.D-30) SCLE(IP)=DSQRT(C(IP,IP))
DO 120 IP=1,NP1
DTMPA=SCLE(IP)
IP1=IP+1

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PAR0893  
PAR0894  
PAR0895  
PAR0896  
PAR0897  
PAR0898  
PAR0899  
PAR0900  
PAR0901

DO 110 I=IP1,NP	PAR0902
C(I,IP)=C(I,IP)/(SCLE(I)*DTMPA)	PAR0903
110 C(IP,I)=C(I,IP)	PAR0904
G(IP)=G(IP)/DTMPA	PAR0905
120 C(IP,IP)=1.D00+AMP	PAR0906
G(NP)=G(NP)/SCLE(NP)	PAR0907
C(NP,NP)=1.D00+AMP	PAR0908
C-----PRINT AS INDICATED BY IPRINT	PAR0909
IF(IPRINT.NE.0) THEN	PAR0910
WRITE(IOUT,500)	PAR0911
DO 125 J=1,NP	PAR0912
125 WRITE(IOUT,516)(C(I,J),I=1,NP)	PAR0913
WRITE(IOUT,510)	PAR0914
WRITE(IOUT,516)(G(I),I=1,NP)	PAR0915
ENDIF	PAR0916
C-----COMPUTE PARAMETER STEP LENGTHS	PAR0917
CALL SPAR1R(C,DD,G,NP,CSA,IND,IFO,AMP,DET)	PAR0918
C-----IF MATRIX EQUATION IS SINGULAR, OR CONVERGENCE HAS BEEN REACHED:	PAR0919
IF(IND.GT.0.OR.IFO.GT.0) THEN	PAR0920
C-----CONVERT NATURAL LOGS OF PARAMETER VALUES AND RETURN	PAR0921
126 DO 127 IP=1,NP	PAR0922
127 IF(LN(IP).NE.0) B(IP)=EXP(B(IP))	PAR0923
RETURN	PAR0924
ENDIF	PAR0925
C-----UNSCALE PARAMETER CHANGE VECTOR	PAR0926
DO 130 IP=1,NP	PAR0927
130 DD(IP)=DD(IP)/SCLE(IP)	PAR0928
GO TO 150	PAR0929
C-----CALCULATE STEP LENGTH FOR SINGLE-PARAMETER CASE	PAR0930
140 DET=C(1,1)	PAR0931
SCLE(1)=1.D00	PAR0932
IF(IFO.GT.0) THEN	PAR0933
IF(LN(1).GT.0) B(1)=EXP(B(1))	PAR0934
RETURN	PAR0935
ENDIF	PAR0936
DD(1)=G(1)/DET	PAR0937
C-----COMPUTE DAMPING PARAMETER AND NEW ESTIMATES OF REGRESSION	PAR0938
C-----PARAMETERS	PAR0939
150 ADMX=0.	PAR0940
ADMX1=0.	PAR0941
DMXO=DMX	PAR0942
JJ=0	PAR0943
DO 160 IP=1,NP	PAR0944
TMPA=0.	PAR0945
TMPB=0.	PAR0946
LNN=LN(IP)	PAR0947
IF(LNN.EQ.0) THEN	PAR0948
TMPA=B(IP)	PAR0949
IF(ABS(B(IP)).LT.ABS(B1(IP))*1.E-3) TMPA=B1(IP)	PAR0950
TMPA=DD(IP)/ABS(TMPA)	PAR0951
TMPB=ABS(TMPA)	PAR0952
ENDIF	PAR0953
IF(LNN.GT.0) THEN	PAR0954
IF(DD(IP).GE.0.) THEN	PAR0955
TMPA=1.E+10	PAR0956
IF(DD(IP).LT.23.) TMPA=DEXP(DD(IP))-1.	PAR0957
ELSEIF(DD(IP).LT.0.) THEN	PAR0958
TMPA=-1.	PAR0959
IF(DD(IP).GT.-23.) TMPA=DEXP(DD(IP))-1.	PAR0960
ENDIF	PAR0961
TMPB=ABS(TMPA)	PAR0962
ENDIF	PAR0963
IF(NP.GT.1.AND.TMPB.LE.ADMX) GO TO 160	PAR0964
IF(LN(IP).GT.0.AND.DD(IP).LT.0..AND.DMAX.GE.1..AND.	PAR0965
1 TMPB.GT.ADMX1) THEN	PAR0966
JJ1=IP	PAR0967
DMX1=TMPA	PAR0968
ADMX1=TMPB	PAR0969
GO TO 160	PAR0970
ENDIF	PAR0971
JJ=IP	PAR0972
DMX=TMPA	PAR0973
ADMX=TMPB	PAR0974
LNMX=0	PAR0975
IF(LNN.NE.0) LNMX=1	PAR0976
160 CONTINUE	PAR0977
IF(ADMX1.GT.ADMX) THEN	PAR0978
DMX=DMX1	PAR0979
JJ=JJ1	PAR0980
ADMX=ADMX1	PAR0981
LNMX=1	PAR0982
ENDIF	PAR0983
IF(ITERP.LE.1.OR.JJ.NE.JMAX.OR.	PAR0984

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1 (ISN1.EQ.10.AND.ITERP.EQ.NFIT+2)) GO TO 166 PAR0985
  SPR=DMX/(AP*DMXO) PAR0986
  IF (SPR.LT.-1.) GO TO 164 PAR0987
  AP=(3.+SPR)/(3.+ABS(SPR)) PAR0988
  GO TO 166 PAR0989
164 AP=.5/ABS(SPR) PAR0990
166 CONTINUE PAR0991
  JMAX=JJ PAR0992
  IF (ITERP.EQ.1.OR.JJ.EQ.0.OR.JJ.NE.JMAX.OR. PAR0993
1 (ISN1.EQ.10.AND.ITERP.EQ.NFIT+2)) AP=1. PAR0994
  IF (LNMX.EQ.0.AND.AP*ADMX.GT.DMAX) AP=DMAX/ADMX PAR0995
  IF (LNMX.NE.0) THEN PAR0996
    DTMP=DD(JJ) PAR0997
    IF (AP*DTMP.GT.ALOG(DMAX+1.)) AP=ALOG(DMAX+1.)/DTMP PAR0998
    IF (DMAX.LT.1..AND.AP*DTMP.LT.ALOG(1.-DMAX)) AP=ALOG(1.-DMAX)/DTMP PAR0999
  ENDIF PAR1000
  DO 170 IP=1,NP PAR1001
    DDC=AP*DD(IP) PAR1002
    B(IP)=B(IP)+DDC PAR1003
    DD(IP)=DDC PAR1004
    IF (LN(IP).NE.0) B(IP)=EXP(B(IP)) PAR1005
170 CONTINUE PAR1006
C-----PRINT DATA FROM CURRENT ITERATION PAR1007
  WRITE(IOUT,514) ITERP,DET,AMP,AP,DMX,JJ,(PID(IP),IP=1,NP) PAR1008
  WRITE(IOUT,516) (B(IP),IP=1,NP) PAR1009
  IF (IOUB.GT.0) WRITE(IOUB,530) DMX,JJ,AMP PAR1010
  AMP=0. PAR1011
C-----CHECK FOR CONVERGENCE PAR1012
  IF (ADMX.LE.TOL) THEN PAR1013
    IFO=1 PAR1014
    WRITE(IOUT,600) PAR1015
  ENDIF PAR1016
  RETURN PAR1017
  END PAR1018

C=====PAR1019
SUBROUTINE PARLOT( PAR1020
1 C,WT,NP,IOUR,RSQ,IOUT,BUFF,ND,IPRC,IFO,IND,PID, PAR1021
2 SCLE,B,HOBS,H,NPR,B1,WP,ITERPF,X,HNEW,LN,MPR, PAR1022
3 PRM,IWPG,NODES,LPRINT,IDRY,EV,RSQP,ISN,NPO) PAR1023
C-----VERSION 1000 01FEB1992 PAR1024
C ***** PAR1025
C FINAL GAUSS-NEWTON OUTPUT FOR PARAMETER ESTIMATION PAR1026
C ***** PAR1027
C SPECIFICATIONS: PAR1028
C ----- PAR1029
CHARACTER*4 PID(NP),ANAME PAR1030
DOUBLE PRECISION C(NP,NP),SCLE(NP),HNEW(NODES),DSUM,TMP PAR1031
DIMENSION BUFF(NP,NP+2),ANAME(4,2),WT(ND),B(NPO),HOBS(ND),H(ND), PAR1032
1 WP(NPO+MPR),B1(NPO),X(NP,ND),LN(NP),PRM(NPO+1,MPR),IWPG(NP) PAR1033
DATA ANAME(1,1),ANAME(2,1),ANAME(3,1),ANAME(4,1) PAR1034
1 /'COVA','RIAN','CE M','AT. ' / PAR1035
DATA ANAME(1,2),ANAME(2,2),ANAME(3,2),ANAME(4,2) PAR1036
1 /'CORR','ELAT','ION ','MAT.' / PAR1037
C ----- PAR1038
C PAR1039
520 FORMAT(//,' LEAST SQUARES COEFFICIENT MATRIX SINGULAR -- ' PAR1040
1 'STOP EXECUTION (PARLOT)') PAR1041
521 FORMAT(//,' RSQ (DEP.VAR. ONLY)----- = ',G11.5,/ PAR1042
1 ', RSQ (W/PARAMETERS)----- = ',G11.5,/ PAR1043
1 ', CALCULATED ERROR VARIANCE = ',G11.5,/ PAR1044
1 ', CORRELATION COEFFICIENT-- = ',G11.5,/ PAR1045
1 ', W/PARAMETERS----- = ',G11.5,/ PAR1046
1 ', ITERATIONS----- = ',I7) PAR1047
525 FORMAT(' ',I5,' CELLS WERE DRY IN FINAL PARAMETER-ESTIMATION ', PAR1048
1 'ITERATION') PAR1049
530 FORMAT(//,' MAXIMUM NUMBER OF PARAMETER ESTIMATION ITERATIONS', PAR1050
1 ' EXCEEDED -- STOP EXECUTION (PARLOT)') PAR1051
535 FORMAT('/' THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS >= ', PAR1052
1 '.95',/,5X,'PARAMETER # ID # ID CORRELATION') PAR1053
540 FORMAT(13X,I5,2X,A4,I5,2X,A4,F8.2) PAR1054
545 FORMAT('/' THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS ', PAR1055
1 'BETWEEN .90 AND .95',/,5X,'PARAMETER # ID # ID', PAR1056
1 'CORRELATION') PAR1057
550 FORMAT('/' THE CORRELATION OF THE FOLLOWING PARAMETER PAIRS IS ', PAR1058
1 'BETWEEN .85 AND .90',/,5X,'PARAMETER # ID # ID', PAR1059
1 'CORRELATION') PAR1060
555 FORMAT(//,' PARAMETER SUMMARY',/ PAR1061
1 ',//,' PARAMETER # :',3X,I6,9I10,/ PAR1062
1 ',12(14X,3X,I6,9I10,/)) PAR1063
557 FORMAT(' PARAMETER ID :',7X,A4,6X,A4,6X,A4,6X,A4,6X,A4, PAR1064
1 6X,A4,6X,A4,6X,A4,6X,A4,/,12(15X,7X,A4,6X,A4,6X,A4,6X,A4, PAR1065

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337	IF(LN(IP).GT.0) BUFF(IP,1)=EXP(B(IP))	PAR1149
	WRITE(IOUT,565)(BUFF(IP,1),IP=1,NP)	PAR1150
	ENDIF	PAR1151
C-----	PUT STANDARD DEVIATIONS IN SINGLE-PRECISION ARRAY AND PRINT	PAR1152
	DO 340 IP=1,NP	PAR1153
340	BUFF(IP,1)=SNGL(SCLE(IP))	PAR1154
	WRITE(IOUT,560)	PAR1155
	WRITE(IOUT,565)(BUFF(IP,1),IP=1,NP)	PAR1156
C-----	COMPUTE COEFFICIENTS OF VARIATION AND PRINT	PAR1157
	DO 345 IP=1,NP	PAR1158
345	BUFF(IP,1)=BUFF(IP,1)/ABS(B(IP))	PAR1159
	WRITE(IOUT,562)	PAR1160
	WRITE(IOUT,565)(BUFF(IP,1),IP=1,NP)	PAR1161
C-----	COMPUTE +- 2 STANDARD DEVIATIONS AND PRINT	PAR1162
	DO 346 IP=1,NP	PAR1163
346	BUFF(IP,1)=B(IP)+2.*SNGL(SCLE(IP))	PAR1164
	WRITE(IOUT,600)	PAR1165
	WRITE(IOUT,565) (BUFF(IP,1),IP=1,NP)	PAR1166
	IF(LNFLAG.NE.0) THEN	PAR1167
	WRITE(IOUT,559)	PAR1168
	DO 347 IP=1,NP	PAR1169
	IF(LN(IP).EQ.0) THEN	PAR1170
	BUFF(IP,1)=0.	PAR1171
	ELSE	PAR1172
	BT=BUFF(IP,1)	PAR1173
	IF(BT.LT.53.0) BUFF(IP,1)=EXP(BT)	PAR1174
	IF(BUFF(IP,1).LT.0.) BUFF(IP,1)=1.E-23	PAR1175
	IF(BT.GE.53.0) BUFF(IP,1)=1.E+23	PAR1176
	ENDIF	PAR1177
347	CONTINUE	PAR1178
	WRITE(IOUT,565)(BUFF(IP,1),IP=1,NP)	PAR1179
	ENDIF	PAR1180
	DO 348 IP=1,NP	PAR1181
348	BUFF(IP,1)=B(IP)-2.*SNGL(SCLE(IP))	PAR1182
	WRITE(IOUT,610)	PAR1183
	WRITE(IOUT,565) (BUFF(IP,1),IP=1,NP)	PAR1184
	IF(LNFLAG.NE.0) THEN	PAR1185
	WRITE(IOUT,559)	PAR1186
	DO 349 IP=1,NP	PAR1187
	IF(LN(IP).EQ.0) BUFF(IP,1)=0.	PAR1188
349	IF(LN(IP).GT.0) BUFF(IP,1)=EXP(BUFF(IP,1))	PAR1189
	WRITE(IOUT,565)(BUFF(IP,1),IP=1,NP)	PAR1190
	ENDIF	PAR1191
	WRITE(IOUT,590)	PAR1192
C-----	COMPUTE AND PRINT CORRELATION MATRIX FOR PARAMETERS	PAR1193
	IF(NP.GT.1) THEN	PAR1194
	DO 360 IP=1,NP	PAR1195
	DTMPA=SCLE(IP)	PAR1196
	DO 350 I=IP,NP	PAR1197
	C(I,IP)=C(I,IP)/(SCLE(I)*DTMPA)	PAR1198
350	C(IP,I)=C(I,IP)	PAR1199
360	CONTINUE	PAR1200
	DO 370 IP=1,NP	PAR1201
	DO 370 I=1,NP	PAR1202
370	BUFF(I,IP)=C(I,IP)	PAR1203
	WRITE(IOUT,570) (ANAME(I,2),I=1,4)	PAR1204
	CALL ULAPRW(BUFF,ANAME(1,2),IDUM,IDUM,NP,NP,-IDUM,IPRC,IOUT)	PAR1205
C-----	CHECK FOR HIGHLY CORRELATED PARAMETER PAIRS	PAR1206
	WRITE(IOUT,535)	PAR1207
	DO 380 IP=1,NP	PAR1208
	I1=IP+1	PAR1209
	DO 380 I=I1,NP	PAR1210
380	IF(DABS(C(IP,I)).GE..95) WRITE(IOUT,540) IP,PID(IP),I,PID(I),	PAR1211
1	SNGL(C(IP,I))	PAR1212
	WRITE(IOUT,545)	PAR1213
	DO 390 IP=1,NP	PAR1214
	I1=IP+1	PAR1215
	DO 390 I=I1,NP	PAR1216
	TMP=DABS(C(IP,I))	PAR1217
390	IF(TMP.GE..90.AND.TMP.LT..95)	PAR1218
1	WRITE(IOUT,540) IP,PID(IP),I,PID(I),SNGL(C(IP,I))	PAR1219
	WRITE(IOUT,550)	PAR1220
	DO 400 IP=1,NP	PAR1221
	I1=IP+1	PAR1222
	DO 400 I=I1,NP	PAR1223
	TMP=DABS(C(IP,I))	PAR1224
400	IF(TMP.GE..85.AND.TMP.LT..90)	PAR1225
1	WRITE(IOUT,540) IP,PID(IP),I,PID(I),SNGL(C(IP,I))	PAR1226
	ENDIF	PAR1227
C-----	CALCULATE CORRELATION COEFFICIENT	PAR1228
	CALL SPARLA(ND,WT,HOBBS,H,R,R1,NPR,MPR,B1,NP,WP,B,PRM,NPO)	PAR1229
C-----	PRINT FINAL RSQ'S, ERROR VARIANCE, CORRELATION, ITERATIONS	PAR1230
	WRITE(IOUT,521) RSQ,RSQP,VAR,R,R1,ITERPF	PAR1231

C-----CALC AND PRINT STATISTICS BASED ON MAX LIKELIHOOD OBJ FUNCTION	PAR1232
CALL SPAR1M(RSQP,WT,NP,ND,WP,MPR,IOUT,EV,NPR)	PAR1233
RETURN	PAR1234
END	PAR1235
C=====	PAR1236
SUBROUTINE PAR1RE(	PAR1237
1                    NP,B,B1,IWPG,WP,IOUT,NH,H,HOBS,WT,DID,	PAR1238
2                    NQT,ND,IPAR,NPR,MPR,PRM,NPO	PAR1239
1                    )	PAR1240
C-----VERSION 1000 01FEB1992	PAR1241
C*****	PAR1242
C    ANALYSIS OF RESIDUALS	PAR1243
C*****	PAR1244
C    SPECIFICATIONS:	PAR1245
C-----	PAR1246
DIMENSION B(NPO),IWPG(NP),B1(NPO),WP(NPO+MPR),H(ND+NPR+MPR),	PAR1247
1            HOBS(ND),WT(ND),PRM(NPO+1,NP)	PAR1248
C-----	PAR1249
C	PAR1250
AVET=0.	PAR1251
NND=0	PAR1252
C-----HEADS	PAR1253
IF(NH.GT.0) THEN	PAR1254
DO 160 N=1,NH	PAR1255
RES=H(N)-HOBS(N)	PAR1256
W=WT(N)	PAR1257
IF(W.LT.0.) GO TO 160	PAR1258
WT2=SQRT(W)	PAR1259
WTR=RES*WT2	PAR1260
NND=NND+1	PAR1261
H(NND)=WTR	PAR1262
AVET=AVET+WTR	PAR1263
160    CONTINUE	PAR1264
ENDIF	PAR1265
C-----HEAD-DEPENDENT FLOWS	PAR1266
IF(NQT.GT.0) THEN	PAR1267
NH1=NH+1	PAR1268
NH2=NH+NQT	PAR1269
DO 170 N=NH1,NH2	PAR1270
RES=H(N)-HOBS(N)	PAR1271
W=WT(N)	PAR1272
IF(W.LT.0.) GO TO 170	PAR1273
WT2=SQRT(W)	PAR1274
WTR=RES*WT2	PAR1275
NND=NND+1	PAR1276
H(NND)=WTR	PAR1277
AVET=AVET+WTR	PAR1278
170    CONTINUE	PAR1279
ENDIF	PAR1280
C-----TEST FOR NORMALITY OF THE DEPENDENT-VARIABLE WEIGHTED RESIDUALS	PAR1281
C-----CALCULATE THE MEAN	PAR1282
AVE=AVET/REAL(NND)	PAR1283
C-----ORDER THE RESIDUALS	PAR1284
DO 240 NN=1,NND-1	PAR1285
NMIN=NN	PAR1286
RMIN=H(NN)	PAR1287
DO 200 N=NN+1,NND	PAR1288
IF(H(N).LE.RMIN) THEN	PAR1289
RMIN=H(N)	PAR1290
NMIN=N	PAR1291
ENDIF	PAR1292
200    CONTINUE	PAR1293
IF(NMIN.NE.NN) THEN	PAR1294
H(NMIN)=H(NN)	PAR1295
H(NN)=RMIN	PAR1296
ENDIF	PAR1297
240    CONTINUE	PAR1298
WRITE(IOUT,515) NND	PAR1299
515    FORMAT(/,' ORDERED DEPENDENT-VARIABLE WEIGHTED RESIDUALS',	PAR1300
1/,' NUMBER OF RESIDUALS INCLUDED:',I10)	PAR1301
WRITE(IOUT,530) (H(N),N=1,NND)	PAR1302
C-----CALCULATE THE STATISTIC	PAR1303
RNUM=0.	PAR1304
DEN1=0.	PAR1305
DEN2=0.	PAR1306
DO 250 N=1,NND	PAR1307
RNORM=(REAL(N)-.5)/REAL(NND)	PAR1308
CALL UNORM(U,RNORM,-1)	PAR1309
DIF=H(N)-AVE	PAR1310
RNUM=RNUM+DIF*U	PAR1311
DEN1=DEN1+DIF**2	PAR1312

DEN2=DEN2+U**2	PAR1313
250 CONTINUE	PAR1314
STAT=RNUM**2/(DEN1*DEN2)	PAR1315
WRITE(IOUT,520) STAT	PAR1316
IF((NPR+MPR).EQ.0) RETURN	PAR1317
C-----PRIOR INFORMATION ON INDIVIDUAL PARAMETERS BY PARAMETER GROUP	PAR1318
IF(IPAR.GT.0.AND.NPR.GT.0) THEN	PAR1319
DO 327 IG=1,NP	PAR1320
DO 326 IP=1,NP	PAR1321
IF(IWPG(IP).EQ.IG.AND.WP(IP).GT.0.) THEN	PAR1322
WPSR=WP(IP)**.5	PAR1323
BDIF=B1(IP)-B(IP)	PAR1324
BWP=BDIF*WPSR	PAR1325
NND=NND+1	PAR1326
H(NND)=BWP	PAR1327
AVET=AVET+BWP	PAR1328
ENDIF	PAR1329
326 CONTINUE	PAR1330
327 CONTINUE	PAR1331
ENDIF	PAR1332
C-----PRIOR INFORMATION ON PARAMETER SUMS	PAR1333
IF(IPAR.GT.0.AND.MPR.GT.0) THEN	PAR1334
DO 350 IMP=1,MPR	PAR1335
TEMP=0.	PAR1336
DO 340 IIP=1,NPO	PAR1337
340 TEMP=TEMP+PRM(IIP,IMP)*B(IIP)	PAR1338
WPSR=WP(NPO+IMP)**.5	PAR1339
TEMP1=PRM(NPO+1,IMP)	PAR1340
BDIF=TEMP1-TEMP	PAR1341
BWP=BDIF*WPSR	PAR1342
NND=NND+1	PAR1343
H(NND)=BWP	PAR1344
AVET=AVET+BWP	PAR1345
350 CONTINUE	PAR1346
ENDIF	PAR1347
C-----CALCULATE THE MEAN	PAR1348
AVET=AVET/REAL(NND)	PAR1349
C-----ORDER THE RESIDUALS	PAR1350
DO 390 NN=1,NND-1	PAR1351
RMIN=H(NN)	PAR1352
NMIN=NN	PAR1353
DO 370 N=NN,NND	PAR1354
IF(H(N).LE.RMIN) THEN	PAR1355
RMIN=H(N)	PAR1356
NMIN=N	PAR1357
ENDIF	PAR1358
370 CONTINUE	PAR1359
IF(NMIN.NE.NN) THEN	PAR1360
H(NMIN)=H(NN)	PAR1361
H(NN)=RMIN	PAR1362
ENDIF	PAR1363
390 CONTINUE	PAR1364
WRITE(IOUT,510) NND	PAR1365
510 FORMAT(/,' ORDERED WEIGHTED RESIDUALS',	PAR1366
1/,' NUMBER OF RESIDUALS INCLUDED:',I10)	PAR1367
WRITE(IOUT,530) (H(N),N=1,NND)	PAR1368
530 FORMAT (8G10.3)	PAR1369
C-----CALCULATE THE STATISTIC	PAR1370
RNUM=0.	PAR1371
DEN1=0.	PAR1372
DEN2=0.	PAR1373
DO 420 N=1,NND	PAR1374
RNORM=(REAL(N)-.5)/REAL(NND)	PAR1375
CALL UNORM(U,RNORM,-1)	PAR1376
DIF=H(N)-AVET	PAR1377
RNUM=RNUM+DIF*U	PAR1378
DEN1=DEN1+DIF**2	PAR1379
DEN2=DEN2+U**2	PAR1380
420 CONTINUE	PAR1381
STAT=RNUM**2/(DEN1*DEN2)	PAR1382
WRITE(IOUT,520) STAT	PAR1383
520 FORMAT(' CORRELATION BETWEEN ORDERED WEIGHTED RESIDUALS AND',/,	PAR1384
1 ' INDEPENDENT NORMAL DEVIATES =',G13.3)	PAR1385
RETURN	PAR1386
END	PAR1387

# New PAR Submodules

Listed in alphabetical order

C=====		SPA0001
	SUBROUTINE SPARLA(	SPA0002
1	ND,WT,HOBS,H,R,R1,NPR,MPR,B1,NP,WP,B,PRM,NPO	SPA0003
1	)	SPA0004
C-----	VERSION 1000 01FEB1992	SPA0005
C		SPA0006
C	*****	SPA0007
C	CALCULATE CORRELATION COEFFICIENT	SPA0008
C	*****	SPA0009
C	SPECIFICATIONS:	SPA0010
C	-----	SPA0011
	DOUBLE PRECISION SUMA,SUMB,SUMC,SUMD,SUM,TMP,TEMP,TMPP	SPA0012
	DIMENSION WT(ND),HOBS(ND),H(ND),B1(NPO),B(NPO),PRM(NPO+1,MPR),	SPA0013
1	WP(NPO+MPR)	SPA0014
C	-----	SPA0015
C		SPA0016
	OBS=ND	SPA0017
	SUMA=0.	SPA0018
	SUMB=0.	SPA0019
	SUMC=0.	SPA0020
	SUMD=0.	SPA0021
	SUM=0.	SPA0022
	DO 460 N=1,ND	SPA0023
	IF(WT(N).LT.0.) THEN	SPA0024
	OBS=OBS-1.	SPA0025
	GO TO 460	SPA0026
	ENDIF	SPA0027
	TMP=WT(N)**.5	SPA0028
	TEMP=TMP*HOBS(N)	SPA0029
	TMP=TMP*H(N)	SPA0030
	SUMA=SUMA+TEMP	SPA0031
	SUMB=SUMB+TMP	SPA0032
	SUMC=SUMC+TEMP*TEMP	SPA0033
	SUMD=SUMD+TMP*TMP	SPA0034
	SUM=SUM+TEMP*TMP	SPA0035
460	CONTINUE	SPA0036
	R=(OBS*SUM-SUMA*SUMB)/((OBS*SUMC-SUMA*SUMA)*(OBS*SUMD-SUMB*SUMB))	SPA0037
1	** .5	SPA0038
	R1=R	SPA0039
C-----	PRIOR PARAMETER ESTIMATES	SPA0040
	IF(NPR+MPR.GT.0) THEN	SPA0041
	OBS=OBS+NPR+MPR	SPA0042
	DO 540 I=1,NPO+MPR	SPA0043
	IF(WP(I).GT.0..AND.(I.LE.NP.OR.I.GT.NPO)) THEN	SPA0044
	TMP=WP(I)**.5	SPA0045
	IF(I.LE.NP) THEN	SPA0046
	TEMP=TMP*B1(I)	SPA0047
	TMP=TMP*B(I)	SPA0048
	ELSE	SPA0049
	TEMP=TMP*PRM(NPO+1,I-NP)	SPA0050
	TMPP=0.	SPA0051
	DO 520 II=1,NPO	SPA0052
520	TMPP=TMPP+PRM(II,I-NPO)*B(II)	SPA0053
	TMP=TMPP*TMP	SPA0054
	ENDIF	SPA0055
	SUMA=SUMA+TEMP	SPA0056
	SUMB=SUMB+TMP	SPA0057
	SUMC=SUMC+TEMP*TEMP	SPA0058
	SUMD=SUMD+TMP*TMP	SPA0059
	SUM=SUM+TEMP*TMP	SPA0060
	ENDIF	SPA0061
540	CONTINUE	SPA0062
	R1=(OBS*SUM-SUMA*SUMB)/	SPA0063
1	((OBS*SUMC-SUMA*SUMA)*(OBS*SUMD-SUMB*SUMB))**.5	SPA0064
	ENDIF	SPA0065
	RETURN	SPA0066
	END	SPA0067
C=====		SPA0068
	SUBROUTINE SPARLE(	SPA0069
1	C,BUFF1,BUFF2,NP,BUFF3,IOUT,B,B1,ITERPF,BUFF,	SPA0070
1	PID,IPRC,IE	SPA0071
1	)	SPA0072
C-----	VERSION 1000 01FEB1992	SPA0073
C		SPA0074
C	*****	SPA0075
C	CALCULATE EIGENVALUES AND EIGENVECTORS OF COVARIANCE MATRIX ON THE	SPA0076
C	PARAMETERS.	SPA0077

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C *****SPA0078
C SPECIFICATIONS: SPA0079
C -----SPA0080
CHARACTER*4 PID(NP), ANAME SPA0081
DOUBLE PRECISION C(NP,NP), BUFF3(NP), BUFF1(NP,NP), BUFF2(NP) SPA0082
DIMENSION B(NP), B1(NP), ANAME(4), BUFF(NP,NP) SPA0083
DATA ANAME(1), ANAME(2), ANAME(3), ANAME(4) SPA0084
# /'SCAL', 'ED W', ' PAR', 'AM. '/ SPA0085
C -----SPA0086
500 FORMAT(/, A4, 8D13.4, /, 10(4X, 8D13.4)) SPA0087
510 FORMAT(/, 4X, 8D13.4, /, 10(4X, 8D13.4)) SPA0088
520 FORMAT(/, ' EIGENVALUES') SPA0089
530 FORMAT(/, ' EIGENVECTORS') SPA0090
540 FORMAT(/, ' EIGENVALUE AND EIGENVECTOR CALCULATION PERFORMANCE', SPA0091
1' INDEX = ', E13.4, ' (<1 EXCELLENT, 1 TO 100 GOOD, >100 POOR)') SPA0092
550 FORMAT(/, ' NUMBER OF JACOBI ROTATIONS:', I7) SPA0093
570 FORMAT(/, 10X, 4A4/10X, 16(' -')) SPA0094
C SPA0095
C-----SCALE VARIANCE-COVARIANCE MATRIX WITH PARAMETER VALUES SPA0096
DO 20 IP=1,NP SPA0097
DO 10 IIP=1,NP SPA0098
10 BUFF1(IP, IIP)=0. SPA0099
BUFF2(IP)=0. SPA0100
20 BUFF3(IP)=0. SPA0101
IF(ITERPF.GT.1) THEN SPA0102
DO 30 IP=1,NP SPA0103
DO 30 IIP=1,NP SPA0104
30 C(IP, IIP)=C(IP, IIP)/(B(IP)*B(IIP)) SPA0105
ELSE SPA0106
DO 40 IP=1,NP SPA0107
DO 40 IIP=1,NP SPA0108
40 C(IP, IIP)=C(IP, IIP)/(B1(IP)*B1(IIP)) SPA0109
ENDIF SPA0110
DUM=0. SPA0111
CALL USAVEF(DUM, BUFF, C, DUM, NP*NP, 3) SPA0112
DO 50 IP=1,NP SPA0113
DO 50 I=1,NP SPA0114
50 BUFF(I, IP)=C(I, IP) SPA0115
IDUM=1 SPA0116
WRITE(IOUT, 570) (ANAME(I), I=1, 4) SPA0117
CALL ULAPRW(BUFF, ANAME(1), IDUM, IDUM, NP, NP, -IDUM, IPRC, IOUT) SPA0118
C-----CALCULATE EIGENVALUES AND EIGENVECTORS SPA0119
IF(IE.EQ.1) THEN SPA0120
C CALL DE2CSF(NP, C, NP, BUFF3, BUFF1, NP, BUFF2) SPA0121
C-----CALCULATE PERFORMANCE INDEX SPA0122
PI = DEPISEF(NP, NP, C, NP, BUFF3, BUFF1, NP) SPA0123
ELSEIF(IE.GT.1) THEN SPA0124
DO 60 IP=1,NP SPA0125
DO 60 I=1,NP SPA0126
60 BUFF1(I, IP)=C(I, IP) SPA0127
CALL TRED2(BUFF1, NP, NP, BUFF3, BUFF2) SPA0128
CALL TQLI(BUFF3, BUFF2, NP, NP, BUFF1) SPA0129
CALL EIGSRT(BUFF3, BUFF1, NP, NP) SPA0130
ENDIF SPA0131
C-----SCALE EIGENVECTORS TO FORM UNIT VECTORS SPA0132
DO 80 I=1,NP SPA0133
TEMP=0. SPA0134
DO 70 J=1,NP SPA0135
70 TEMP=TEMP+BUFF1(J, I)**2 SPA0136
TEMP=TEMP**.5 SPA0137
DO 75 J=1,NP SPA0138
75 BUFF1(J, I)=BUFF1(J, I)/TEMP SPA0139
80 CONTINUE SPA0140
C-----PRINT EIGENVALUES SPA0141
WRITE(IOUT, 520) SPA0142
WRITE(IOUT, 510) (BUFF3(J), J=1, NP) SPA0143
C-----PRINT EIGENVECTORS SPA0144
WRITE(IOUT, 530) SPA0145
DO 90 J=1,NP SPA0146
90 WRITE(IOUT, 500) PID(J), (BUFF1(J, I), I=1, NP) SPA0147
IF(IE.EQ.1) WRITE(IOUT, 540) PI SPA0148
C-----EIGENVECTOR TEST (FROM PRESS AND OTHERS, 1989) SPA0149
IF(IE.EQ.3) THEN SPA0150
WRITE(IOUT, '(/1X, A)') 'EIGENVECTOR TEST' SPA0151
DO 130 J=1,NP SPA0152
DO 110 L=1,NP SPA0153
BUFF2(L)=0.0 SPA0154
DO 100 K=1,NP SPA0155
IF (K.GT.L) THEN SPA0156
KK=L SPA0157
LL=K SPA0158
ELSE SPA0159
KK=K SPA0160

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	LL=L	SPA0161
	ENDIF	SPA0162
	BUFF2(L)=BUFF2(L)+C(LL, KK)*BUFF1(K, J)	SPA0163
100	CONTINUE	SPA0164
110	CONTINUE	SPA0165
	WRITE(IOUT, '( /1X, A, I3 )' ) 'VECTOR NUMBER', J	SPA0166
	WRITE(IOUT, '( /1X, T7, A, T18, A, T31, A )' )	SPA0167
*	'VECTOR', 'MTRX*VEC', 'RATIO'	SPA0168
	DO 120 L=1, NP	SPA0169
	RATIO=BUFF2(L)/BUFF1(L, J)	SPA0170
	WRITE(IOUT, '(1X, 3G12.5)' ) BUFF1(L, J), BUFF2(L), RATIO	SPA0171
120	CONTINUE	SPA0172
130	CONTINUE	SPA0173
	ENDIF	SPA0174
C-----	UNSCALE VARIANCE-COVARIANCE MATRIX	SPA0175
	IF(ITERPF.GT.1) THEN	SPA0176
	DO 140 IP=1, NP	SPA0177
	DO 140 IIP=1, NP	SPA0178
140	C(IP, IIP)=C(IP, IIP)*(B(IP)*B(IIP))	SPA0179
	ELSE	SPA0180
	DO 150 IP=1, NP	SPA0181
	DO 150 IIP=1, NP	SPA0182
150	C(IP, IIP)=C(IP, IIP)*(B1(IP)*B1(IIP))	SPA0183
	ENDIF	SPA0184
	RETURN	SPA0185
	END	SPA0186
C=====		SPA0187
	SUBROUTINE SPARI(NP, C)	SPA0188
C----	VERSION 1000 01FEB1992	SPA0189
C		SPA0190
C	*****	SPA0191
C	COMPLETE CALCULATION OF THE INVERSE OF SCALED	SPA0192
C	COEFFICIENT MATRIX C STARTING FROM DECOMPOSED MATRIX	SPA0193
C	FROM SPAR1R, FOR NP>1	SPA0194
C	*****	SPA0195
C	SPECIFICATIONS:	SPA0196
C	-----	SPA0197
C	DOUBLE PRECISION C(NP, NP), DSUM	SPA0198
C	-----	SPA0199
	NP1=NP-1	SPA0200
	C(NP, NP)=1.D00/C(NP, NP)	SPA0201
	DO 260 K=1, NP1	SPA0202
	KP1=K+1	SPA0203
	DO 230 I=KP1, NP	SPA0204
	DSUM=0.	SPA0205
	IM1=I-1	SPA0206
	DO 220 J=K, IM1	SPA0207
220	DSUM=DSUM+C(I, J)*C(J, K)	SPA0208
	C(K, I)=-DSUM	SPA0209
230	C(I, K)=-DSUM*C(I, I)	SPA0210
	DO 250 I=1, K	SPA0211
	DSUM=C(K, I)	SPA0212
	DO 240 J=KP1, NP	SPA0213
240	DSUM=DSUM+C(J, K)*C(I, J)	SPA0214
	C(K, I)=DSUM	SPA0215
250	C(I, K)=C(K, I)	SPA0216
260	CONTINUE	SPA0217
	RETURN	SPA0218
	END	SPA0219
C=====		SPA0220
	SUBROUTINE SPAR1M(	SPA0221
1	RSQP, WT, NP, ND, WP, MPR, IOUT, EV, NPR	SPA0222
1	)	SPA0223
C----	VERSION 1000 01FEB1992	SPA0224
C		SPA0225
C	*****	SPA0226
C	CALCULATE STATISTICS BASED ON THE MAXIMUM LIKELIHOOD OBJECTIVE	SPA0227
C	FUNCTION	SPA0228
C	*****	SPA0229
C	SPECIFICATIONS:	SPA0230
C	-----	SPA0231
C	DIMENSION WT(ND), WP(NP+MPR)	SPA0232
C	-----	SPA0233
520	FORMAT(/, ' MAX LIKE OBJ FUNC = ', G11.5, /,	SPA0234
1	' AIC STATISTIC---- = ', G11.5, /,	SPA0235
2	' BIC STATISTIC---- = ', G11.5)	SPA0236
C		SPA0237
	AEV=ALOG(EV)	SPA0238
	RND=REAL(ND)	SPA0239

RP=REAL(NPR+MPR)	SPA0240
C-----DEPENDENT-VARIABLE PART OF WEIGHT MATRIX	SPA0241
PROD=0.	SPA0242
DO 100 N=1,ND	SPA0243
100 PROD=PROD+ALOG(WT(N))	SPA0244
PROD=PROD-RND*AEV	SPA0245
C-----PRIOR PART OF WEIGHT MATRIX	SPA0246
PRODP=0.	SPA0247
DO 120 IP=1,NP+MPR	SPA0248
120 IF(WP(IP).NE.0.) PRODP=PRODP+ALOG(WP(IP))	SPA0249
PRODP=PRODP-RP*AEV	SPA0250
C-----LOG-LIKELIHOOD FUNCTION	SPA0251
OF=(RSQP/EV)-PROD-PRODP+(RND+RP)*ALOG(2.*3.14159265)	SPA0252
C-----AIC AND BIC	SPA0253
AIC=OF+2.*REAL(NP)	SPA0254
BIC=OF+NP*ALOG(RND+RP)	SPA0255
WRITE(IOUT,520) OF,AIC,BIC	SPA0256
RETURN	SPA0257
END	SPA0258
C=====	SPA0259
SUBROUTINE SPARIP(	SPA0260
1 PID,B,NP,IOUB,IOUT,ISN	SPA0261
1 )	SPA0262
C-----VERSION 1000 01FEB1992	SPA0263
C	SPA0264
C *****	SPA0265
C READ AND PRINT PARAMETER VALUES AND STATISTICS FOR ALL	SPA0266
C ITERATIONS	SPA0267
C *****	SPA0268
C SPECIFICATIONS:	SPA0269
C -----	SPA0270
CHARACTER*4 PID(NP)	SPA0271
DIMENSION B(NP)	SPA0272
C -----	SPA0273
510 FORMAT(8F10.0)	SPA0274
520 FORMAT(6X,6E10.3,/,50(6X,6E10.3,/))	SPA0275
530 FORMAT(/,' PARAMETER VALUES AND STATISTICS FOR ALL ITERATIONS',	SPA0276
1 /,10X,' PAR. ID.:',/,	SPA0277
1 9X,A4,6X,A4,6X,A4,6X,A4,6X,A4,6X,A4,/,	SPA0278
1 50(9X,A4,6X,A4,6X,A4,6X,A4,6X,A4,6X,A4,/,))	SPA0279
550 FORMAT(70X,'SUM OF SQUARED WEIGHTED RESIDUALS',22X,'AMP OR',/,	SPA0280
1 ' ITER',66X,'HEADS W/FLOWS W/PARAMS',	SPA0281
2 DMX PAR# AGMX')	SPA0282
580 FORMAT(F10.0,I5)	SPA0283
590 FORMAT(I4,65X,G10.3,2X,G10.3,2X,G10.3,2X,G10.3,I5,2X,G10.3)	SPA0284
C	SPA0285
REWIND(IOUB)	SPA0286
WRITE(IOUT,530) (PID(IP),IP=1,NP)	SPA0287
WRITE(IOUT,550)	SPA0288
ITER=0	SPA0289
110 ITER=ITER+1	SPA0290
READ(IOUB,510,END=140) (B(IP),IP=1,NP)	SPA0291
WRITE(IOUT,520) (B(IP),IP=1,NP)	SPA0292
READ(IOUB,510,END=140) RSQH,RSQ,RSQP	SPA0293
C-----FOR ISN>0, AMP IS AGMX	SPA0294
READ(IOUB,580,END=120) DMX,NPAR,AMP	SPA0295
WRITE(IOUT,590) ITER,RSQH,RSQ,RSQP,DMX,NPAR,AMP	SPA0296
GO TO 110	SPA0297
120 WRITE(IOUT,590) ITER,RSQH,RSQ,RSQP	SPA0298
140 CONTINUE	SPA0299
RETURN	SPA0300
END	SPA0301
C=====	SPA0302
SUBROUTINE SPARIQ(C,DD,G,NP,R,GD,U,ITERP,IP,X,ND,HOBS,H,WT,S,NFIT,	SPA0303
1 B1,B,WP,NPR,MPR,PRM,NPO,XD,NPER,SOSR)	SPA0304
C-----VERSION 1000 01FEB1992	SPA0305
C	SPA0306
C *****	SPA0307
C COMPUTE QUASI-NEWTON COMPONENT OF C MATRIX AND ADD TO C	SPA0308
C *****	SPA0309
C SPECIFICATIONS:	SPA0310
C -----	SPA0311
DOUBLE PRECISION C(NP,NP),DD(NP),SUM,TMPA,DS,DGD,DU,CF,QD,TMP,T,	SPA0312
1 R(NP*NP/2+NP),DPGD,DPU,DTMPA,U(NP),S(NP),G,GD,DPGI,W1	SPA0313
DIMENSION G(NP),GD(NP),X(NP,ND),HOBS(ND),H(ND),WT(ND),	SPA0314
1 WP(NPO+MPR),PRM(NPO+1,MPR),B1(IP),B(IP),XD(NP,ND)	SPA0315
C -----	SPA0316
C-----FOR FIRST PARAMETER-ESTIMATION ITERATIONS, INITIALIZE UPDATING	SPA0317
C-----MATRIX R AND SAVE G AND X	SPA0318

IF(ITERP.EQ.1) THEN	SPA0319
I=0	SPA0320
DO 50 IIP=1,NP	SPA0321
DO 55 IPP=IIP,NP	SPA0322
I=I+1	SPA0323
R(I)=0.	SPA0324
55  CONTINUE	SPA0325
50  GD(IIP)=G(IIP)	SPA0326
DO 53 N=1,ND	SPA0327
DO 53 IIP=1,NP	SPA0328
53  XD(IIP,N)=X(IIP,N)	SPA0329
RETURN	SPA0330
ENDIF	SPA0331
C-----CALCULATE MATRIX R	SPA0332
DO 30 IIP=1,NP	SPA0333
30  S(IIP)=0.	SPA0334
DO 40 N=1,ND	SPA0335
IF(WT(N).LT.0.) GO TO 40	SPA0336
W1=(HOBS(N)-H(N))*WT(N)	SPA0337
DO 35 IIP=1,NP	SPA0338
35  S(IIP)=S(IIP)+W1*(XD(IIP,N)-X(IIP,N))	SPA0339
40  CONTINUE	SPA0340
C	SPA0341
DO 80 J=1,NP	SPA0342
80  GD(J)=GD(J)-G(J)	SPA0343
C	SPA0344
K=0	SPA0345
QD=0.	SPA0346
DS=0.	SPA0347
DO 340 J=1,NP	SPA0348
M=NP-J+1	SPA0349
K=K+1	SPA0350
L=K	SPA0351
SUM=0.	SPA0352
IF(J.EQ.NP) GO TO 325	SPA0353
JPL=J+1	SPA0354
DO 320 I=JPL,NP	SPA0355
K=K+1	SPA0356
320  SUM=SUM+DD(I)*R(K)	SPA0357
325  TMPA=DD(J)*R(L)	SPA0358
QD=QD+(SUM+SUM+TMPA)*DD(J)	SPA0359
SUM=SUM+TMPA	SPA0360
IF(J.EQ.1) GO TO 335	SPA0361
JML=J-1	SPA0362
DO 330 I=1,JML	SPA0363
L=L-M	SPA0364
SUM=SUM+R(L)*DD(J-I)	SPA0365
330  M=M+1	SPA0366
335  U(J)=SUM	SPA0367
340  DS=DS+DD(J)*S(J)	SPA0368
C	SPA0369
TMP=1.	SPA0370
IF(QD.NE.0.) TMP=DABS(DS/QD)	SPA0371
T=1.	SPA0372
IF(TMP.LT.1.) T=TMP	SPA0373
DGD=0.	SPA0374
DU=0.	SPA0375
DO 345 J=1,NP	SPA0376
DGD=DGD+DD(J)*GD(J)	SPA0377
U(J)=S(J)-T*U(J)	SPA0378
345  DU=DU+DD(J)*U(J)	SPA0379
C	SPA0380
CF=DU/(DGD*DGD)	SPA0381
K=0	SPA0382
DO 355 J=1,NP	SPA0383
DO 350 I=J,NP	SPA0384
K=K+1	SPA0385
DPGD=GD(J)	SPA0386
DPU=U(J)	SPA0387
DPGI=GD(I)	SPA0388
350  R(K)=T*R(K)+(U(I)*DPGD+DPGI*DPU)/DGD-CF*DPGI*DPGD	SPA0389
355  CONTINUE	SPA0390
C-----SAVE GRADIENT	SPA0391
DO 360 IIP=1,NP	SPA0392
360  GD(IIP)=G(IIP)	SPA0393
C-----SAVE SENSITIVITIES	SPA0394
DO 365 N=1,ND	SPA0395
DO 365 IIP=1,NP	SPA0396
365  XD(IIP,N)=X(IIP,N)	SPA0397
C-----ADD QN APPROXIMATION TO COEFFICIENT MATRIX	SPA0398
IF((NFIT.GT.0.AND.ITERP.GT.NFIT).OR.SOSR.LT.0.) THEN	SPA0399
I=0	SPA0400
DO 370 IIP=1,NP	SPA0401



DO 370 IPP=IIP,NP	SPA0402
I=I+1	SPA0403
C(IPP,IIP)=C(IPP,IIP)+R(I)	SPA0404
370 CONTINUE	SPA0405
ENDIF	SPA0406
RETURN	SPA0407
END	SPA0408
C=====	SPA0409
SUBROUTINE SPAR1R(C,DD,G,NP,CSA,IND,IFO,AMP,DET)	SPA0410
C-----VERSION 1000 01FEB1992	SPA0411
C	SPA0412
C *****	SPA0413
C COMPUTE PARAMETER STEP LENGTHS USING THE MARQUARDT PROCEDURE	SPA0414
C *****	SPA0415
C SPECIFICATIONS:	SPA0416
C -----	SPA0417
DOUBLE PRECISION C(NP,NP),DD(NP),DPIV,DTMPA,DSUM,G	SPA0418
DIMENSION G(NP)	SPA0419
C -----	SPA0420
C	SPA0421
C COMPUTE TRIAL PARAMETER STEP LENGTHS USING LDU FACTORIZATION:	SPA0422
C DECOMPOSE MATRIX	SPA0423
NM1=NP-1	SPA0424
20 IND=0	SPA0425
DET=1.	SPA0426
DO 60 K=1,NM1	SPA0427
DPIV=C(K,K)	SPA0428
DET=DET*DPIV	SPA0429
IF(DPIV.GT.1.D-13) GO TO 30	SPA0430
IND=1	SPA0431
GO TO 115	SPA0432
30 DPIV=1.D00/DPIV	SPA0433
KP1=K+1	SPA0434
DO 50 J=KP1,NP	SPA0435
DTMPA=C(J,K)*DPIV	SPA0436
DO 40 I=J,NP	SPA0437
40 C(I,J)=C(I,J)-DTMPA*C(I,K)	SPA0438
50 CONTINUE	SPA0439
C(K,K)=DPIV	SPA0440
60 CONTINUE	SPA0441
DET=DET*C(NP,NP)	SPA0442
IF(C(NP,NP).GT.1.D-13) GO TO 65	SPA0443
IND=1	SPA0444
IF(IFO.EQ.0) GO TO 115	SPA0445
65 IF(IFO.GT.0) RETURN	SPA0446
DO 67 K=1,NP	SPA0447
67 DD(K)=G(K)	SPA0448
C FORWARD SUBSTITUTE	SPA0449
DO 80 K=1,NM1	SPA0450
DTMPA=DD(K)*C(K,K)	SPA0451
KP1=K+1	SPA0452
DO 70 J=KP1,NP	SPA0453
70 DD(J)=DD(J)-C(J,K)*DTMPA	SPA0454
80 CONTINUE	SPA0455
C BACK SUBSTITUTE	SPA0456
DD(NP)=DD(NP)/C(NP,NP)	SPA0457
I=NP	SPA0458
85 I=I-1	SPA0459
IF(I.LT.1) GO TO 100	SPA0460
IP1=I+1	SPA0461
DSUM=0.	SPA0462
DO 90 J=IP1,NP	SPA0463
90 DSUM=DSUM+C(J,I)*DD(J)	SPA0464
DD(I)=(DD(I)-DSUM)*C(I,I)	SPA0465
GO TO 85	SPA0466
C CHECK SOLUTION AND ADD MARQUARDT PARAMETER IF NEEDED	SPA0467
100 SUM=0.	SPA0468
SUMA=0.	SPA0469
SUMB=0.	SPA0470
DO 110 I=1,NP	SPA0471
SUM=SUM+DD(I)*G(I)	SPA0472
SUMA=SUMA+DD(I)*DD(I)	SPA0473
110 SUMB=SUMB+G(I)*G(I)	SPA0474
IF(SUM.GT.CSA*SQR(SUMA*SUMB)) RETURN	SPA0475
115 AMP=1.5*AMP+.001	SPA0476
IF(AMP.GT.1.) RETURN	SPA0477
DO 130 I=1,NP	SPA0478
C(I,I)=1.D00+AMP	SPA0479
DO 120 J=I,NP	SPA0480
120 C(J,I)=C(I,J)	SPA0481
130 CONTINUE	SPA0482

SPA0483  
SPA0484

C	-----SUBROUTINE TRED2(A,N,NP,D,E)	UT10001
C	-----VERSION 1000 01FEB1992	UT10002
C		UT10003
C	*****	UT10004
C	*****	UT10005
C	FROM PRESS AND OTHERS (1989); MODIFIED FOR DOUBLE PRECISION	UT10006
C	*****	UT10007
C	SPECIFICATIONS:	UT10008
C	-----	UT10009
	IMPLICIT DOUBLE PRECISION (A-H,P-Z)	UT10010
	DIMENSION A(NP,NP),D(NP),E(NP)	UT10011
C	-----	UT10012
	IF(N.GT.1)THEN	UT10013
	DO 18 I=N,2,-1	UT10014
	L=I-1	UT10015
	H=0.	UT10016
	SCALE=0.	UT10017
	IF(L.GT.1)THEN	UT10018
	DO 11 K=1,L	UT10019
	SCALE=SCALE+DABS(A(I,K))	UT10020
11	CONTINUE	UT10021
	IF(SCALE.EQ.0.)THEN	UT10022
	E(I)=A(I,L)	UT10023
	ELSE	UT10024
	DO 12 K=1,L	UT10025
	A(I,K)=A(I,K)/SCALE	UT10026
12	H=H+A(I,K)**2	UT10027
	CONTINUE	UT10028
	F=A(I,L)	UT10029
	G=-SIGN(DSQRT(H),F)	UT10030
	E(I)=SCALE*G	UT10031
	H=H-F*G	UT10032
	A(I,L)=F-G	UT10033
	F=0.	UT10034
	DO 15 J=1,L	UT10035
	A(J,I)=A(I,J)/H	UT10036
	G=0.	UT10037
	DO 13 K=1,J	UT10038
	G=G+A(J,K)*A(I,K)	UT10039
13	CONTINUE	UT10040
	IF(L.GT.J)THEN	UT10041
	DO 14 K=J+1,L	UT10042
	G=G+A(K,J)*A(I,K)	UT10043
14	CONTINUE	UT10044
	ENDIF	UT10045
	E(J)=G/H	UT10046
	F=F+E(J)*A(I,J)	UT10047
15	CONTINUE	UT10048
	HH=F/(H+H)	UT10049
	DO 17 J=1,L	UT10050
	F=A(I,J)	UT10051
	G=E(J)-HH*F	UT10052
	E(J)=G	UT10053
	DO 16 K=1,J	UT10054
	A(J,K)=A(J,K)-F*E(K)-G*A(I,K)	UT10055
16	CONTINUE	UT10056
17	CONTINUE	UT10057
	ENDIF	UT10058
	ELSE	UT10059
	E(I)=A(I,L)	UT10060
	ENDIF	UT10061
	D(I)=H	UT10062
18	CONTINUE	UT10063
	ENDIF	UT10064
	D(1)=0.	UT10065
	E(1)=0.	UT10066
	DO 23 I=1,N	UT10067
	L=I-1	UT10068
	IF(D(I).NE.0.)THEN	UT10069
	DO 21 J=1,L	UT10070
	G=0.	UT10071
	DO 19 K=1,L	UT10072
	G=G+A(I,K)*A(K,J)	UT10073
19	CONTINUE	UT10074
	DO 20 K=1,L	UT10075
	A(K,J)=A(K,J)-G*A(K,I)	UT10076
20	CONTINUE	UT10077

21	CONTINUE	UT10078
	ENDIF	UT10079
	D(I)=A(I,I)	UT10080
	A(I,I)=1.	UT10081
	IF(L.GE.1)THEN	UT10082
	DO 22 J=1,L	UT10083
	A(I,J)=0.	UT10084
	A(J,I)=0.	UT10085
22	CONTINUE	UT10086
	ENDIF	UT10087
23	CONTINUE	UT10088
	RETURN	UT10089
	END	UT10090
C=====	SUBROUTINE TQLI(D,E,N,NP,Z)	UT10091
C-----	VERSION 1000 01FEB1992	UT10092
C		UT10093
C		UT10094
C	*****	UT10095
C	FROM PRESS AND OTHERS (1989); MODIFIED FOR DOUBLE PRECISION	UT10096
C	*****	UT10097
C	SPECIFICATIONS:	UT10098
C	-----	UT10099
	IMPLICIT DOUBLE PRECISION (A-H,P-Z)	UT10100
	DIMENSION D(NP),E(NP),Z(NP,NP)	UT10101
C	-----	UT10102
	IF (N.GT.1) THEN	UT10103
	DO 11 I=2,N	UT10104
	E(I-1)=E(I)	UT10105
11	CONTINUE	UT10106
	E(N)=0.	UT10107
	DO 15 L=1,N	UT10108
	ITER=0	UT10109
1	DO 12 M=L,N-1	UT10110
	DD=DABS(D(M))+DABS(D(M+1))	UT10111
	IF (DABS(E(M))+DD.EQ.DD) GO TO 2	UT10112
12	CONTINUE	UT10113
	M=N	UT10114
2	IF(M.NE.L)THEN	UT10115
	IF(ITER.EQ.30)PAUSE 'too many iterations'	UT10116
	ITER=ITER+1	UT10117
	G=(D(L+1)-D(L))/(2.*E(L))	UT10118
	R=DSQRT(G**2+1.)	UT10119
	G=D(M)-D(L)+E(L)/(G+SIGN(R,G))	UT10120
	S=1.	UT10121
	C=1.	UT10122
	P=0.	UT10123
	DO 14 I=M-1,L,-1	UT10124
	F=S*E(I)	UT10125
	B=C*E(I)	UT10126
	IF(DABS(F).GE.DABS(G))THEN	UT10127
	C=G/F	UT10128
	R=DSQRT(C**2+1.)	UT10129
	E(I+1)=F*R	UT10130
	S=1./R	UT10131
	C=C*S	UT10132
	ELSE	UT10133
	S=F/G	UT10134
	R=DSQRT(S**2+1.)	UT10135
	E(I+1)=G*R	UT10136
	C=1./R	UT10137
	S=S*C	UT10138
	ENDIF	UT10139
	G=D(I+1)-P	UT10140
	R=(D(I)-G)*S+2.*C*B	UT10141
	P=S*R	UT10142
	D(I+1)=G+P	UT10143
	G=C*R-B	UT10144
	DO 13 K=1,N	UT10145
	F=Z(K,I+1)	UT10146
	Z(K,I+1)=S*Z(K,I)+C*F	UT10147
	Z(K,I)=C*Z(K,I)-S*F	UT10148
13	CONTINUE	UT10149
14	CONTINUE	UT10150
	D(L)=D(L)-P	UT10151
	E(L)=G	UT10152
	E(M)=0.	UT10153
	GO TO 1	UT10154
	ENDIF	UT10155
15	CONTINUE	UT10156
	ENDIF	UT10157
	RETURN	UT10158

END

UT10159

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C=====UT10160
SUBROUTINE EIGSRT(D,V,N,NP)UT10161
C-----VERSION 1000 01FEB1992UT10162
CUT10163
C*****UT10164
C FROM PRESS AND OTHERS (1989); MODIFIED FOR DOUBLE PRECISION AND TOUT10165
C ORDER THE EIGENVALUES FROM SMALLEST TO LARGESTUT10166
C*****UT10167
C SPECIFICATIONS:UT10168
C-----UT10169
IMPLICIT DOUBLE PRECISION (A-H,P-Z)UT10170
DIMENSION D(NP),V(NP,NP)UT10171
C-----UT10172
DO 13 I=1,N-1UT10173
K=IUT10174
P=D(I)UT10175
DO 11 J=I+1,NUT10176
IF(D(J).LE.P)THENUT10177
K=JUT10178
P=D(J)UT10179
ENDIFUT10180
11 CONTINUEUT10181
IF(K.NE.I)THENUT10182
D(K)=D(I)UT10183
D(I)=PUT10184
DO 12 J=1,NUT10185
P=V(J,I)UT10186
V(J,I)=V(J,K)UT10187
V(J,K)=PUT10188
12 CONTINUEUT10189
ENDIFUT10190
13 CONTINUEUT10191
RETURNUT10192
ENDUT10193

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C=====UT10194
SUBROUTINE U2DINN (IA,II,JJ,IN)UT10195
C-----VERSION 1000 01FEB1992 U2DINNUT10196
C*****UT10197
C READ INTEGER MATRICES WITHOUT PRINTING ANYTHINGUT10198
C*****UT10199
C SPECIFICATIONS:UT10200
C-----UT10201
CHARACTER*20 FMTINUT10202
DIMENSION IA(JJ,II)UT10203
C-----UT10204
CUT10205
C READ(IN,1) LOCAT,ICONST,FMTIN,IPRNUT10206
1 FORMAT(I10,I10,A20,I10)UT10207
CUT10208
IF(LOCAT) 200,50,90UT10209
C LOCAT=0UT10210
50 DO 80 I=1,IIUT10211
DO 80 J=1,JJUT10212
80 IA(I,J)=ICONSTUT10213
RETURNUT10214
C LOCAT>0UT10215
90 DO 100 I=1,IIUT10216
100 READ(LOCAT,FMTIN)(IA(J,I),J=1,JJ)UT10217
GO TO 300UT10218
C LOCAT<0UT10219
200 LOCAT=-LOCATUT10220
READ(LOCAT)UT10221
READ(LOCAT) IAUT10222
C MULTIPLY BY A CONSTANTUT10223
300 IF(ICONST.EQ.0.) RETURNUT10224
DO 310 I=1,IIUT10225
DO 310 J=1,JJUT10226
310 IA(J,I)=IA(J,I)*ICONSTUT10227
RETURNUT10228
ENDUT10229

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C=====UT10230
SUBROUTINE U2DREN (A,II,JJ,IN)UT10231
C-----VERSION 1000 01FEB1992 U2DRENUT10232
C*****UT10233
C READ REAL MATRICES WITHOUT PRINTING ANYTHINGUT10234
C*****UT10235

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C      SPECIFICATIONS:
C      -----
C      CHARACTER*20 FMTIN
C      DIMENSION A(JJ,II)
C      -----
C      READ(IN,1) LOCAT,CNSTNT,FMTIN,IPRN
C      1 FORMAT(I10,F10.0,A20,I10)
C      IF(LOCAT) 200,50,90
C      LOCAT=0
C      50 DO 80 I=1,II
C      DO 80 J=1,JJ
C      80 A(I,J)=CNSTNT
C      RETURN
C      LOCAT>0
C      90 DO 100 I=1,II
C      100 READ(LOCAT,FMTIN)(A(J,I),J=1,JJ)
C      GO TO 300
C      LOCAT<0
C      200 LOCAT=-LOCAT
C      READ(LOCAT)
C      READ(LOCAT) A
C      MULTIPLY BY A CONSTANT
C      300 IF(CNSTNT.EQ.0.) RETURN
C      DO 310 I=1,II
C      DO 310 J=1,JJ
C      310 A(J,I)=A(J,I)*CNSTNT
C      RETURN
C      END
C      -----
C      SUBROUTINE UNORM(U,RNORM,IP)
C      -----
C      VERSION 1000 01FEB1992
C      *****
C      FIND THE PROBABILITY RELATED TO A U (IP=1), OR A U RELATED TO A
C      PROBABILITY (IP=-1) FOR A STANDARD GAUSSIAN DISTRIBUTION
C      *****
C      SPECIFICATIONS:
C      -----
C      DIMENSION PNORM(2,41)
C      DATA (PNORM(1,I),I=1,41)/0.0,.15,.20,.25,.30,.35,
C      1 .40,.45,.50,.55,.60,.65,.70,.75,.80,
C      2 .85,.90,.95,1.00,1.05,1.10,1.15,1.20,1.25,
C      3 1.30,1.35,1.40,1.45,1.50,1.55,1.60,1.65,
C      4 1.70,1.75,1.80,1.85,1.90,1.95,2.20,
C      5 4.00,5.5/
C      DATA (PNORM(2,I),I=1,41)/.5,.5596,.5793,.5987,.6179,.6368,
C      1 .6554,.6736,.6915,.7088,.7257,.7422,.7580,.7734,.7881,
C      2 .8023,.8159,.8289,.8413,.8531,.8643,.8749,.8849,.8944,
C      3 .90320,.91149,.91924,.92647,.93319,.93943,.94520,.95053,
C      4 .95543,.95994,.96407,.96784,.97128,.97441,.98610,
C      5 .9999683,1.0/
C      -----
C      GIVEN U, GET THE CUMULATIVE PROBABILITY
C      IF(IP.EQ.1) THEN
C      -----
C      FIND THE VALUES ABOVE AND BELOW U
C      AU=ABS(U)
C      IF(AU.GE.5.5) THEN
C      RNORM=1.0
C      IF(U.LT.0.0) RNORM=0.0
C      RETURN
C      ENDIF
C      DO 100 I=1,40
C      100 IF(AU.GE.PNORM(1,I).AND.AU.LT.PNORM(1,I+1)) GO TO 150
C      STOP 'ERROR IN UNORM -- U NOT FOUND'
C      -----
C      INTERPOLATE
C      150 FACTOR=(AU-PNORM(1,I))/(PNORM(1,I+1)-PNORM(1,I))
C      RNORM=PNORM(2,I)+FACTOR*(PNORM(2,I+1)-PNORM(2,I))
C      IF(U.LT.0) RNORM=1.0-RNORM
C      RETURN
C      ENDIF
C      -----
C      GIVEN THE CUMULATIVE PROBABILITY, GET U
C      IF(IP.EQ.-1) THEN
C      -----
C      FIND THE VALUES ABOVE AND BELOW RNORM
C      ARNORM=RNORM
C      IF(RNORM.LT..50) ARNORM=1.-RNORM
C      IF(ARNORM.EQ.1.0) THEN
C      U=5.5
C      IF(RNORM.LT..5) U=-5.5
C      RETURN

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ENDIF	UTIO317
DO 170 I=1,40	UTIO318
170 IF(ARNORM.GE.PNORM(2,I).AND.ARNORM.LT.PNORM(2,I+1))	UTIO319
1 GO TO 190	UTIO320
STOP 'ERROR IN UNORM -- RNORM NOT FOUND'	UTIO321
C-----INTERPOLATE	UTIO322
190 FACTOR=(ARNORM-PNORM(2,I))/(PNORM(2,I+1)-PNORM(2,I))	UTIO323
U=PNORM(1,I)+FACTOR*(PNORM(1,I+1)-PNORM(1,I))	UTIO324
IF(RNORM.LT..50) U=-U	UTIO325
RETURN	UTIO326
ENDIF	UTIO327
END	UTIO328
C=====	UTIO329
SUBROUTINE UREADF(C1,NCOL,NROW,NLAY,IU)	UTIO330
C-----VERSION 1000 01FEB1992	UTIO331
C *****	UTIO332
C READ NODAL ARRAY FROM UNFORMATTED FILE	UTIO333
C *****	UTIO334
C SPECIFICATIONS:	UTIO335
DIMENSION C1(NCOL,NROW,NLAY)	UTIO336
C-----	UTIO337
DO 110 IL=1,NLAY	UTIO338
READ(IU)	UTIO339
110 READ(IU) ((C1(IC,IR,IL),IC=1,NCOL),IR=1,NROW)	UTIO340
RETURN	UTIO341
END	UTIO342
C=====	UTIO343
SUBROUTINE USAVEF(C1,C2,D1,D2,NODES,IFLAG)	UTIO344
C-----VERSION 1000 01FEB1992	UTIO345
C *****	UTIO346
C PUT ELEMENTS OF ONE ARRAY INTO ANOTHER ARRAY	UTIO347
C *****	UTIO348
C SPECIFICATIONS:	UTIO349
DOUBLE PRECISION D1(NODES),D2(NODES)	UTIO350
DIMENSION C1(NODES),C2(NODES)	UTIO351
C-----	UTIO352
IF(IFLAG.EQ.1) THEN	UTIO353
DO 100 I=1,NODES	UTIO354
100 C2(I)=C1(I)	UTIO355
ENDIF	UTIO356
IF(IFLAG.EQ.2) THEN	UTIO357
DO 110 I=1,NODES	UTIO358
110 D2(I)=C1(I)	UTIO359
ENDIF	UTIO360
IF(IFLAG.EQ.3) THEN	UTIO361
DO 120 I=1,NODES	UTIO362
120 C2(I)=D1(I)	UTIO363
ENDIF	UTIO364
RETURN	UTIO365
END	UTIO366