



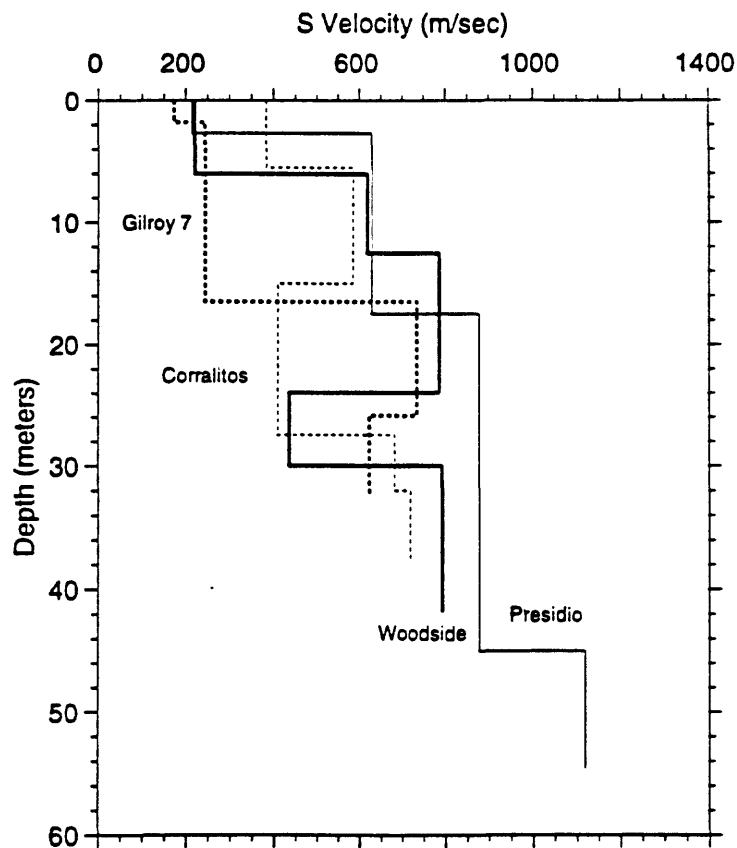
UNITED STATES
DEPARTMENT OF THE INTERIOR
U.S. GEOLOGICAL SURVEY



SEISMIC VELOCITIES AND GEOLOGIC LOGS
FROM BOREHOLE MEASUREMENTS AT EIGHT STRONG-MOTION STATIONS
THAT RECORDED THE 1989 LOMA PRIETA, CALIFORNIA, EARTHQUAKE

by

James F. Gibbs, Thomas E. Fumal, and Thomas J. Powers



U.S. Geological Survey *Open-File Report* 93-376

This report is preliminary and has not been reviewed for conformity with U.S. Geological Survey editorial standards or with the North American Stratigraphic Code. Any use of trade, or firm names is for descriptive purposes only and does not imply endorsement by the U.S. Government.

Menlo Park, California

1993

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INTRODUCTION

The Loma Prieta earthquake of October 17, 1989 (1704 PST) was recorded at 131 strong-motion stations located through-out the San Francisco Bay area (Maley et al., 1989, Shakal, et al., 1989). This data set has enormous value for engineering and seismological studies regarding earthquake ground motions. Using shaking-damage to man-made structures from the 1906 San Francisco earthquake, Lawson (1908) recognized that ground motion intensity could be correlated with differences in local site geology. In order to quantify the effect of local geology (e.g., Borchardt, 1970; Borchardt and Gibbs, 1976) on ground motions from the 1989 earthquake, detailed geologic and geophysical data are needed. To plan the acquisition of these data a meeting was held on July 6, 1990 at the USGS in Menlo Park, California. Eighteen scientist and engineers representing thirteen institutions attended the meeting to coordinate drilling and data aquisition plans at strong-motion stations.

This is the second of a planned series of four reports (Gibbs et al., 1992) detailing the results of borehole measurements at strong-motion stations recording significant ground motions during the 1989 Loma Prieta earthquake. This report contains the results of the field effort by the USGS for the following eight boreholes located near strong-motion stations operated by the California Division of Mines and Geology. (Figure 1).

1. APEEL #1
2. APEEL #2
3. Corralitos
4. Gilroy #7
5. Oakland 2-Story
6. Palo Alto 2-Story
7. Presidio
8. Woodside Fire Station

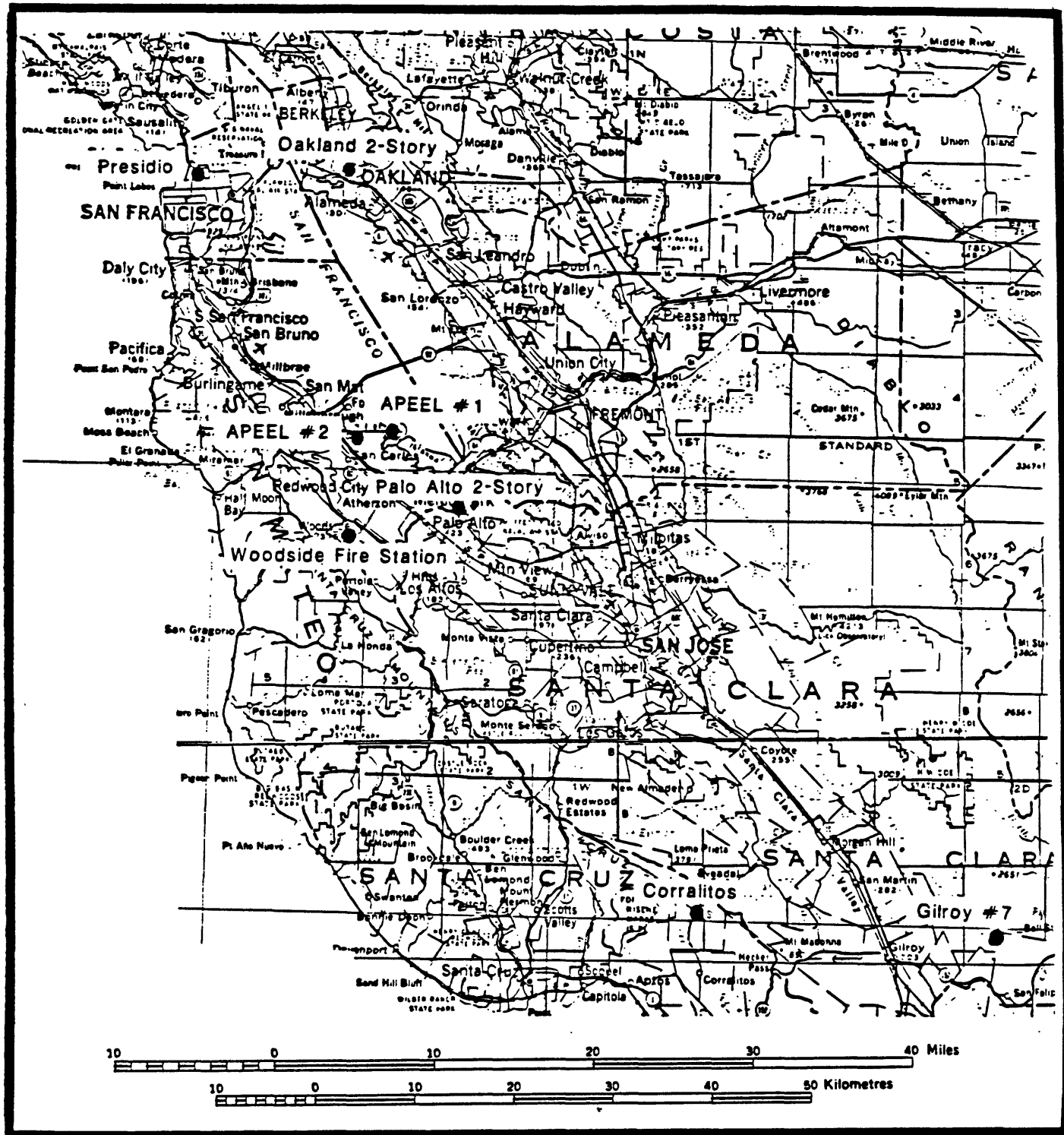


Figure 1. Regional map showing the locations of boreholes (solid circles) included in this report.

FIELD MEASUREMENTS

Drilling and Sampling Procedures

Boreholes were located as close as possible to the strong motion accelerographs usually within 10 meters. In the case of Oakland 2-Story office building site, the borehole was located in Snow Park about 150-200 meters from the instrument location. The Presidio borehole is located approximately 100 meters from the strong-motion instrument.

At each site a hole approximately 6 to 10 inches in diameter was drilled using rotary wash drilling with bentonite mud. For purposes of economy, samples were not taken in any of the boreholes except for Oakland 2-Story (Snow Park). At this site seven "Undisturbed" samples were taken inside Shelby tubes (3-inch outside diameter) using a Pitcher barrel. These samples were allowed to drain of free water and sealed with wax plugs and endcaps. These samples were sent to Jonathan Bray at Purdue University for testing. The borings at Woodsite Fire Station and Gilroy #7 were cased 3-inch inside diameter, class 200, polyvinyl-chloride pipe capped at the bottom. APEEL #1 and APEEL #2 were cased with 4-inch pipe and the other sites were cased with 5-inch inside diameter pipe.

The annular space around the casing was tremie grouted by pumping a water-cement-bentonite mixture through a 1-inch steel pipe installed next to the casing. This provides good coupling between the casing and the wall of the borehole, and provides a sanitary seal preventing contamination of ground water. Grouting was done in stages of about 50-60 meters to prevent collapse of the casing. The California Division of Mines and Geology plans to install a strong-motion instrument package at the bottom of each 5-inch hole to supplement surface recordings.

Geologic Logs

Geologic logs are based on descriptions of drill cuttings, samples, reaction of the drill rig, and inspection of nearby outcrops. Sediment samples are described using the field techniques of the Soil Conservation Service (1951). Descriptions include sediment texture, color, and the amount and size of coarse fragments. Texture refers to the relative proportions of clay, silt, and sand particles less than 2 millimeters in diameter. This is determined visually and by feel without using laboratory tests. As such, this system is easier to use in the field than other classification systems. The dominant color of the

sediment and prominent mottles are determined from the Munsell soil color charts.

Descriptions of rock samples include rock name, weathering condition, color, grain size, hardness, and fracture spacing. Classifications of rock hardness and fracture spacing are those used by Ellen et al., (1972) in describing hillside materials in San Mateo County, California.

Most information needed for describing relatively well-sorted soils and such properties of rock as lithology, color, and hardness are readily obtained from cuttings. Inspection of samples and nearby outcrops is necessary for determining the nature of poorly-sorted materials and fracture spacing. Reaction of the drill rig is useful in determining approximate sediment texture and in determining degree of fracturing because the rate of penetration in rock is highest for very closely fractured and crushed materials and drilling roughness generally is at a maximum in closely to moderately fractured rock. In-situ consistency of soil is determined largely from standard penetration measurements and rate of drill penetration.

Site Geology

Four sites, APEEL #1, APEEL #2 (Portside Park), Oakland 2-Story (Snow Park) and Palo Alto 2-Story are located near the margin of San Francisco Bay on thick sections of Holocene and Pliestocene estuarine and alluvial sedimentary deposits. These deposits consist largely of fine-grained sediments with occasional thick layers of sand and/or gravelly sand. Two of the boreholes were drilled into the underlying bedrock. At APEEL #1, serpentinite was encountered at 188.5 meters (618 feet) and at APEEL #2, greywacke sandstone of the Franciscan assemblage was encountered at 84.7 meters (278 feet).

The geology at Gilroy #7 consists of 17.4 meters (57 feet) of poorly sorted gravelly clay and sandy clay alluvium overlying hard Tertiary shale and sandstone. Two sites are underlain by bedrock. The Presidio site is underlain by serpentinite. Woodside Fire Station is underlain by firm to hard sandstone and mudstone which may be a part of the Butano sandstone. The strong motion instrument at Corralitos sits on 32 meters (105 feet) landslide deposits consisting of very closely fractured black shale. Major slide planes apparently were encountered at 15 meters (50 feet) and 32 meters (105 feet). The landslide deposits are underlain by sandstone which is probably part of the Purisima formation.

Cracks in the road above the site suggest that the landslide may have moved slightly during the earthquake.

Travel-time Data

Shear waves* were generated at the ground surface by an air-powered horizontal hammer (Liu, et al., 1988) striking anvils attached to the ends of a 2.3-meter-long aluminum channel. The hammer can be driven in both horizontal directions to generate positive and negative shear pulses. The switch that determines zero time is a piezo-electric sensor attached to the shear source. The source is offset from the borehole to prevent the direct arrival from traveling down the grout next to the casing. The source offset is 2 to 5 meters depending on the depth of the borehole. Shallow holes (30 meters or less) are generally offset 2 meters, while boreholes deeper than approximately 100 meters are offset 5 meters. Travel times are corrected (for slant offset) to vertical by the cosine of the angle of ray incidence.

P-waves are made by striking a steel plate with a sledge hammer at the same intervals described above. The recorder is triggered by the sledge hammer making electrical contact with the steel plate.

Measurements are made by lowering a single three-component geophone into the borehole and clamping it to the casing-wall with an electrically actuated lever arm. A second three-component geophone is placed at the surface approximately 30 centimeters from the shear source and is used as a check of the switch triggering the recorder for zero time. Depending on geologic information, measurements are repeated at 2.5 or 5.0 meter intervals. The 2.5 meter spacing is used when the layering of the sediments is thin (under 10 meters) and generally from the surface to 30 meters depth.

The data are recorded on magnetic tape cassettes in digital form on a twelve channel recording system.

DATA INTERPRETATION and PROCESSING

The flow-chart, Figure 2, describes the processing and interpretation procedures. The magnetic tape cassette contains 18 recorded traces from each depth. These include data

* In this report shear-wave(s) and S-wave are used interchangeably as well as P-wave and compressional-wave.

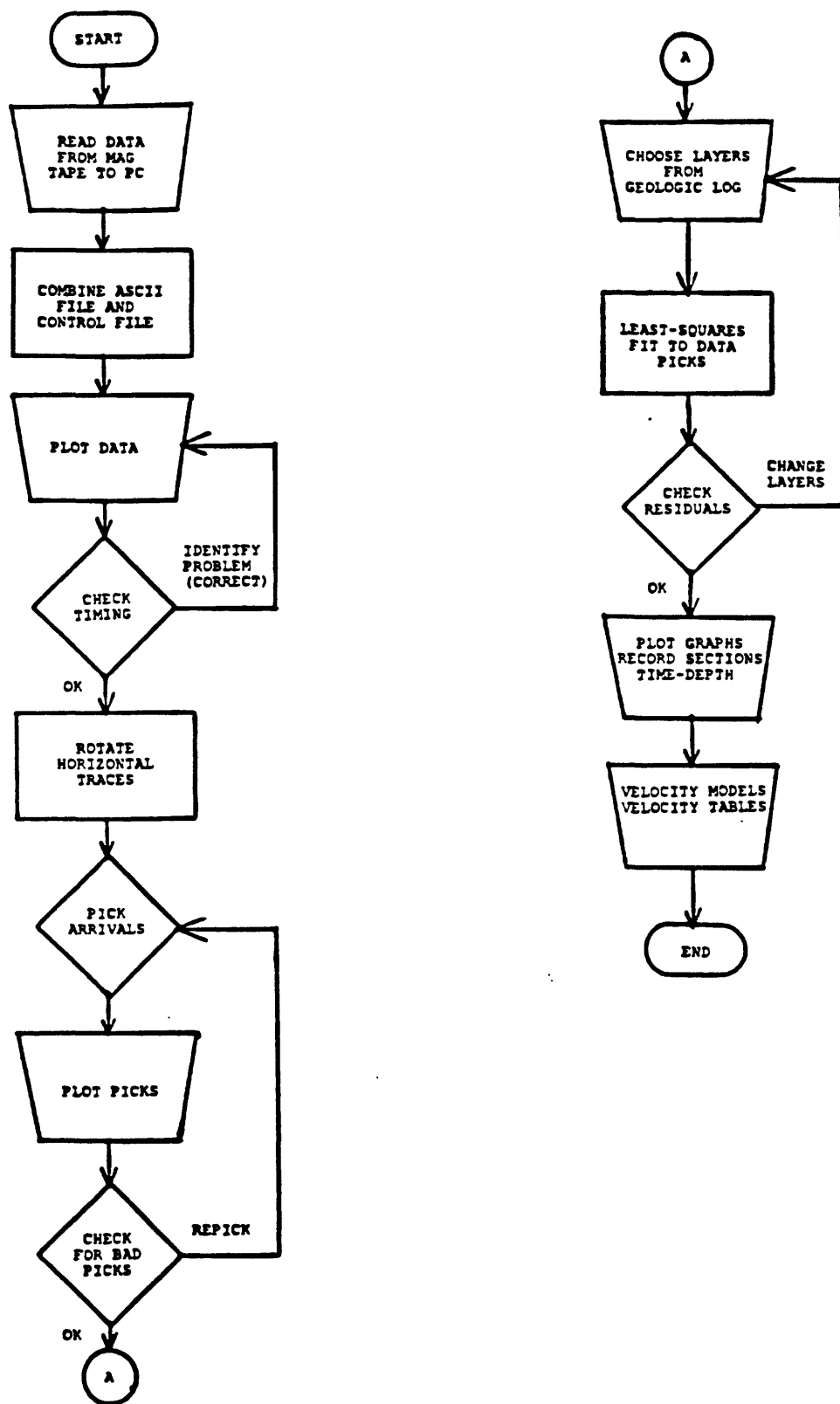


Figure 2. Flow-chart outlining the data processing and interpretation steps.

from the surface three component geophone and the downhole three-component geophone: A total of 6 traces for each source type (positive horizontal, negative horizontal, and vertical). As mentioned previously, the surface geophone is used only to check timing.

The orientation of the downhole geophone cannot be controlled when moving from one depth to the next, so that horizontal components are not generally oriented parallel and perpendicular to the source. This causes slight phase shifts, timing differences and amplitude variations. To minimize these effects, when timing shear-wave arrivals, the horizontal components are combined (rotated) to obtain a single component of motion. The direction of motion is determined by maximizing the integral square amplitude within a time interval containing the shear wave (Boatwright et al., 1986). Rotated traces are plotted on a 20-inch computer monitor and the first shear-wave arrival is timed for each of the horizontal rotated traces. Two arrival times are obtained from picks of positive and negative shear-wave arrivals. Timing of the arrivals is done to one millisecond precision. The two time-picks are not always identical, due to interfering waves obscuring the first shear-arrival, slight phase shifts, or amplitude differences. If the time difference is greater than about 5 milliseconds a mistake in phase correlation (perhaps due to a reversed trace, noise etc.) can be suspected and a repick may be necessary. The two picks are averaged for velocity determinations. On clear traces one-millisecond picking accuracy can be maintained; however, because of lower signal-to-noise ratios and interfering waves in the deeper sections of the boreholes, this accuracy cannot always be achieved. The arrivals are weighted by the inverse of an assigned normalized variance. A normalized standard deviation of 1 was assigned to the accurate picks and values ranging up to 5 were assigned to the others.

For determining the final velocity model there are a number of ways to proceed. In previous reports (e.g., Gibbs et al., 1975) we determined the initial layer boundaries from the travel time plots by eye and then added or subtracted layers based on geologic boundaries consistent with the data. We also required at least three data points in each layer. This requirement limited the velocity determination to layers greater than 7.5 meters in thickness. The problem with this procedure is that a mismatch (overlap or underlap) of the line segments sometimes occurred at the intersections of the layers, resulting in a

discontinuous travel time curve. To address this problem we are now using a least-squares program (Press et al., 1986) that fits the travel time data with line segments hinged at each selected layer boundary from the surface (forced through zero) to the bottom data point. Initial layer boundaries are chosen from the geologic log and are adjusted, if necessary, to reduce residuals and for consistency with the data. The S-wave travel time data are analyzed first; layer boundaries are initially the same for the P-wave model, and are then adjusted, if necessary, by adding a layer for the water table or reducing the number of layers. The velocity plots (e.g., Figure 13) show upper and lower bounds which approximate 68% confidence limits. These bounds are not symmetrical because they are based on the standard deviation of the slope of the least-squares line fit to the travel time plots (the inverse of the velocity).

SUMMARY OF RESULTS

S-wave velocities

Figure 3 summarizes S-wave velocities at four sites; Palo Alto 2-Story, Oakland 2-Story (Snow Park), APEEL #2 and at APEEL #1 to a depth of 120 meters. The S-wave velocities are similar in the upper 50 meters at Palo Alto 2-Story, APEEL #1, and APEEL #2. Oakland 2-Story has somewhat higher velocities due in part to the gravelly layers at 15 and 28 meters. Velocities shown on Figure 3 are similar to those reported earlier (Gibbs et al., 1992) for San Francisco Airport, Treasure Island, Alameda Naval Air Station, and Oakland Outer Harbor Wharf, typical of mixtures of young clay-loam-sand near the margins of San Francisco Bay. At APEEL #2 bedrock (Franciscan Graywacke) was penetrated in the borehole at 85 meters. Unfortunately, we were unable to interpret a bedrock velocity due to poor transmission of energy across the sedimentary-bedrock boundary.

Figure 4 summarizes S-wave velocities at Gilroy #7, Corralitos, Woodside Fire Station, and at the Presidio. The S-wave velocity below 6 meters are near 600 meters/second at Corralitos, Woodside Fire Station, Presidio and Gilroy #7 at a depth below 16 meters. Lower velocities occur at Corralitos and Woodside Fire Station at 15 and 24 meters respectively. The velocities shown on Figure 4 are generally higher than those of Figure 3 which are closer to the Bay margins.

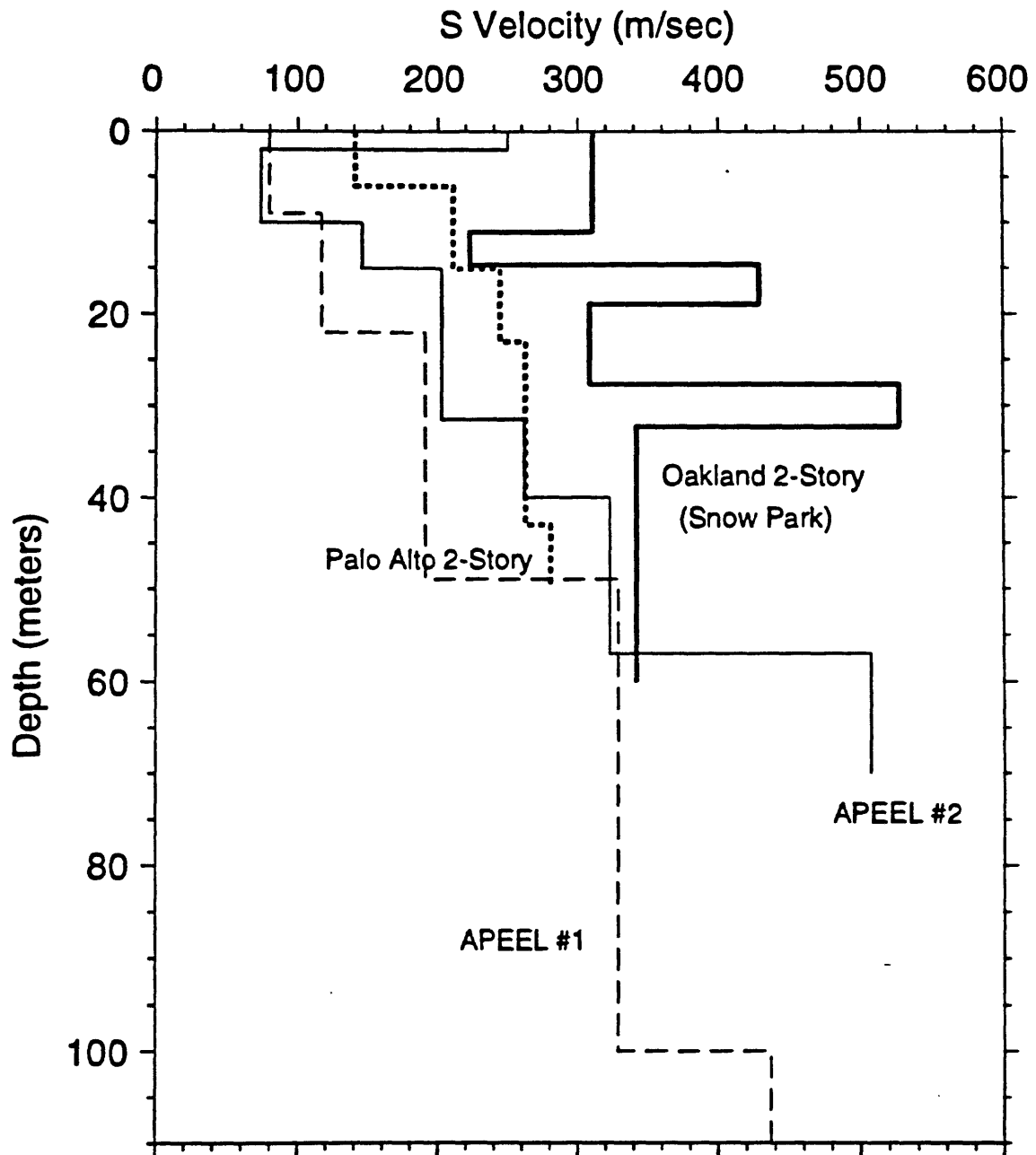


Figure 3. S-wave velocity models superimposed for comparison. The four sites shown are soft fine-grained deposits located close to the margin of San Francisco Bay. The velocities shown here are generally lower than those of Figure 4.

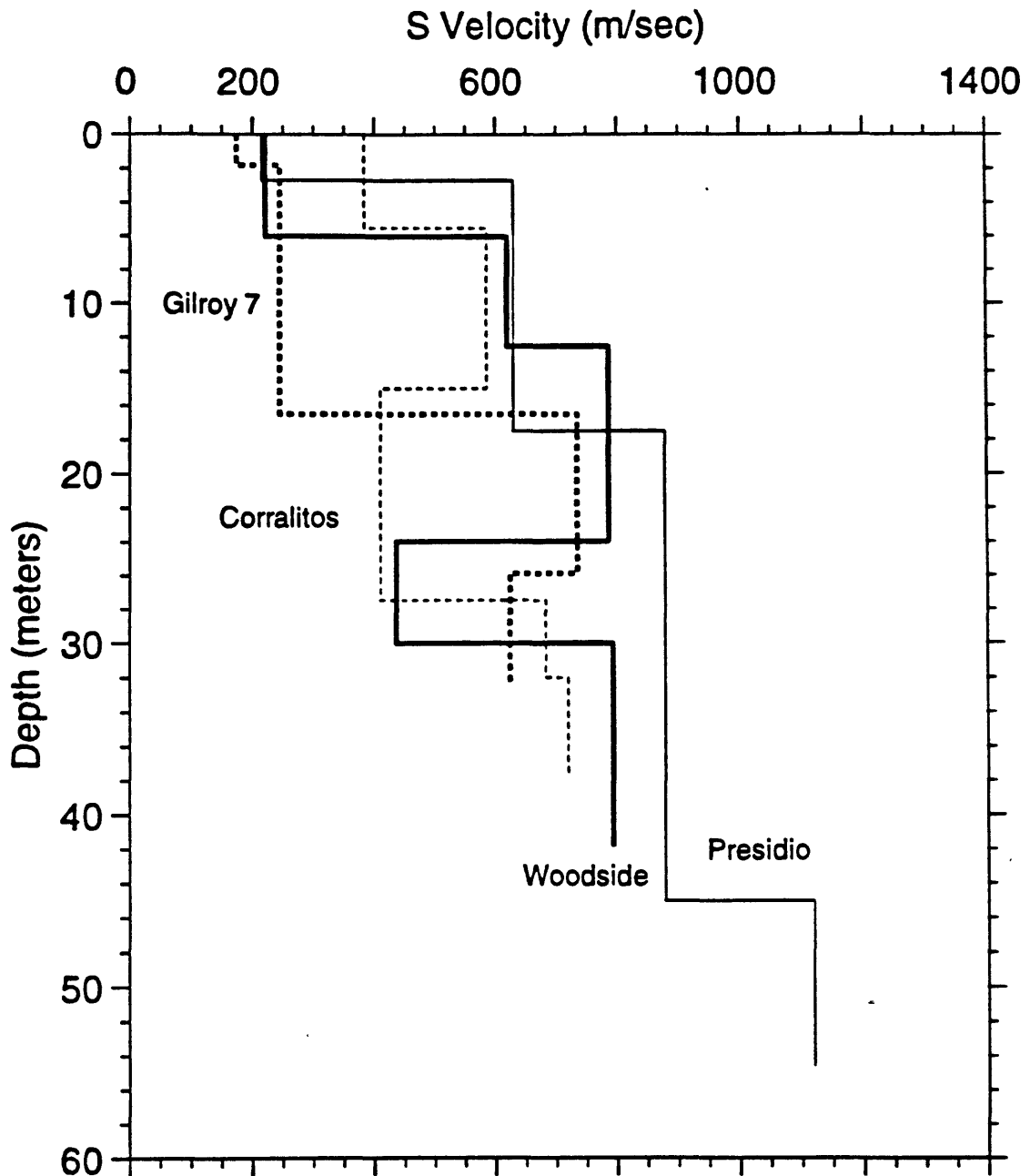


Figure 4. S-wave velocity models superimposed for comparison. The velocities shown here are somewhat higher than those of Figure 3. In general they have thinner sections of fine-grained deposits overlying denser sandstone, shales or Franciscan bedrock. Corralitos site is a detached landslide block that may have moved during the 1989 Loma Prieta earthquake.

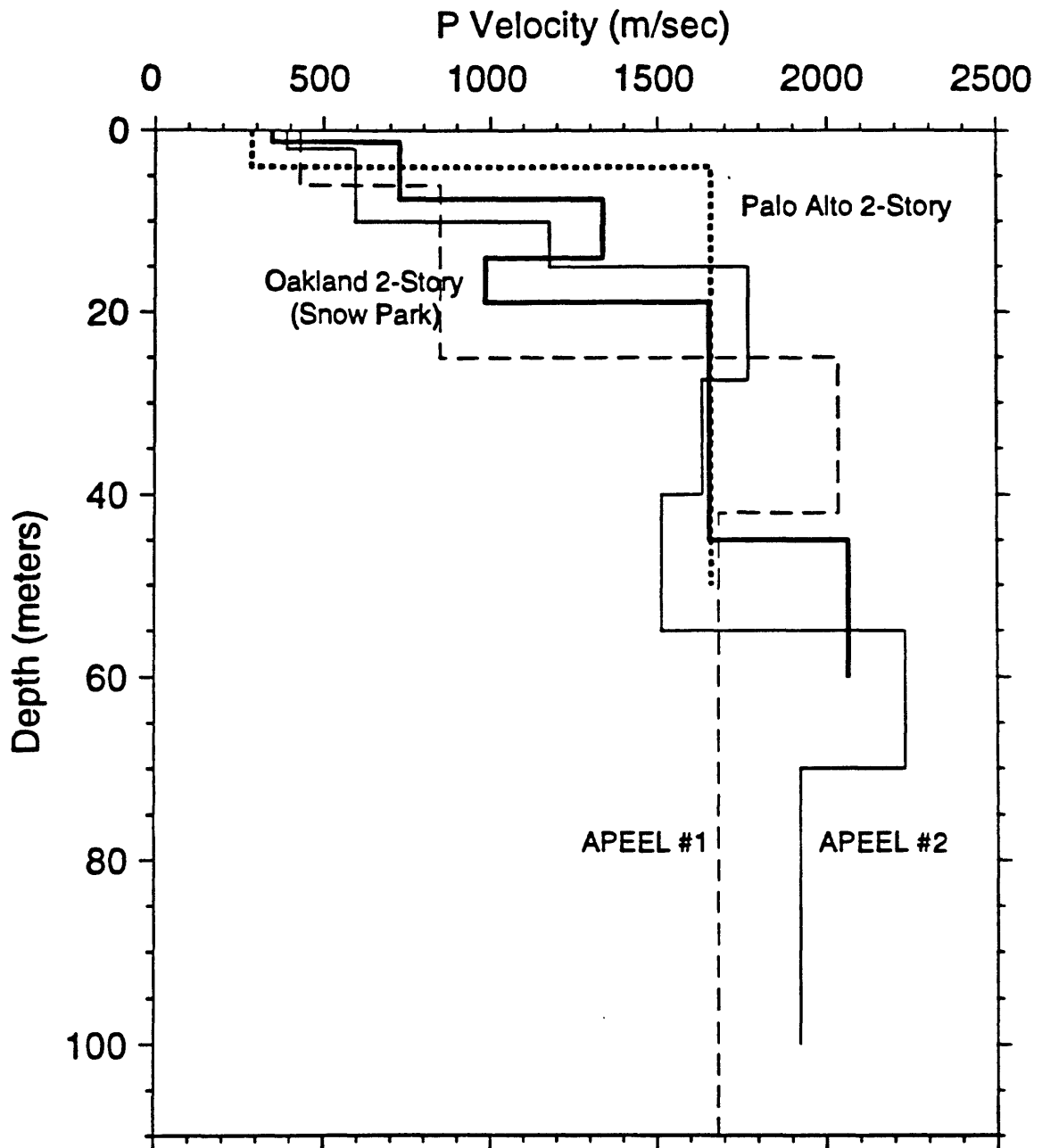


Figure 5. P-wave velocity models superimposed for comparison.

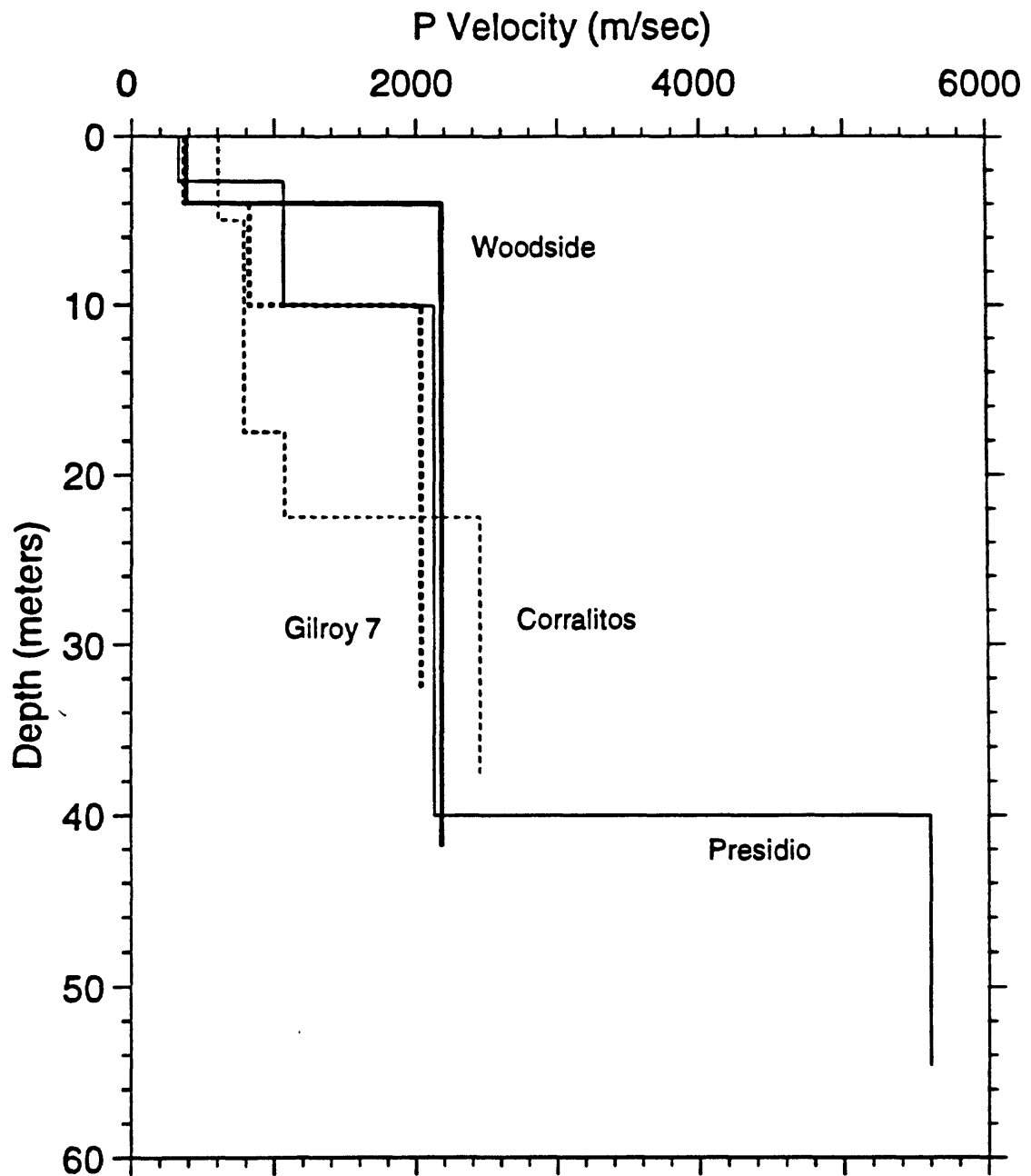


Figure 6. P -wave velocity models superimposed for comparison.

P-wave velocities

Figures 5 and 6 summarize the P-wave velocities at four sites near the margins of San Francisco Bay and at four sites further inland respectively. There is a poorer correlation between P-wave velocity and lithology than S-wave velocity and lithology because P-wave velocity is strongly affected by degree of saturation. Note that even though saturated, the P-wave velocities measured in the Holocene bay mud are less than the velocity of P-waves in water (≈ 1500 meters/second). The explanation for this may be that the presence of trapped gas (Brandt, 1960) has reduced the P-wave velocity (e.g. air, methane from decaying organic matter).

The appendix lists the detailed results, organized alphabetically by borehole. Figures and tables for each site are arranged in the following order:

1. location map
2. geologic log
3. record sections
4. time-depth graph
5. velocity profiles
6. velocity tables

ACKNOWLEDGMENTS

We wish to thank Mr. Robert Westerlund of the *USGS* for building the electrically actuated clamp for the borehole geophone and Dr. Hsi-Ping Liu of the *USGS* for designing the shear-wave generator. In addition, we were assisted in the field by Mr. Michael Carter, Mr. Cristofer Garvin, and Mr. Robert Westerlund of the *USGS*.

We acknowledge the cooperation of Dr. Robert Darragh and Dr. Anthony Shakal of *California Division of Mines and Geology* for providing information on the strong-motion stations.

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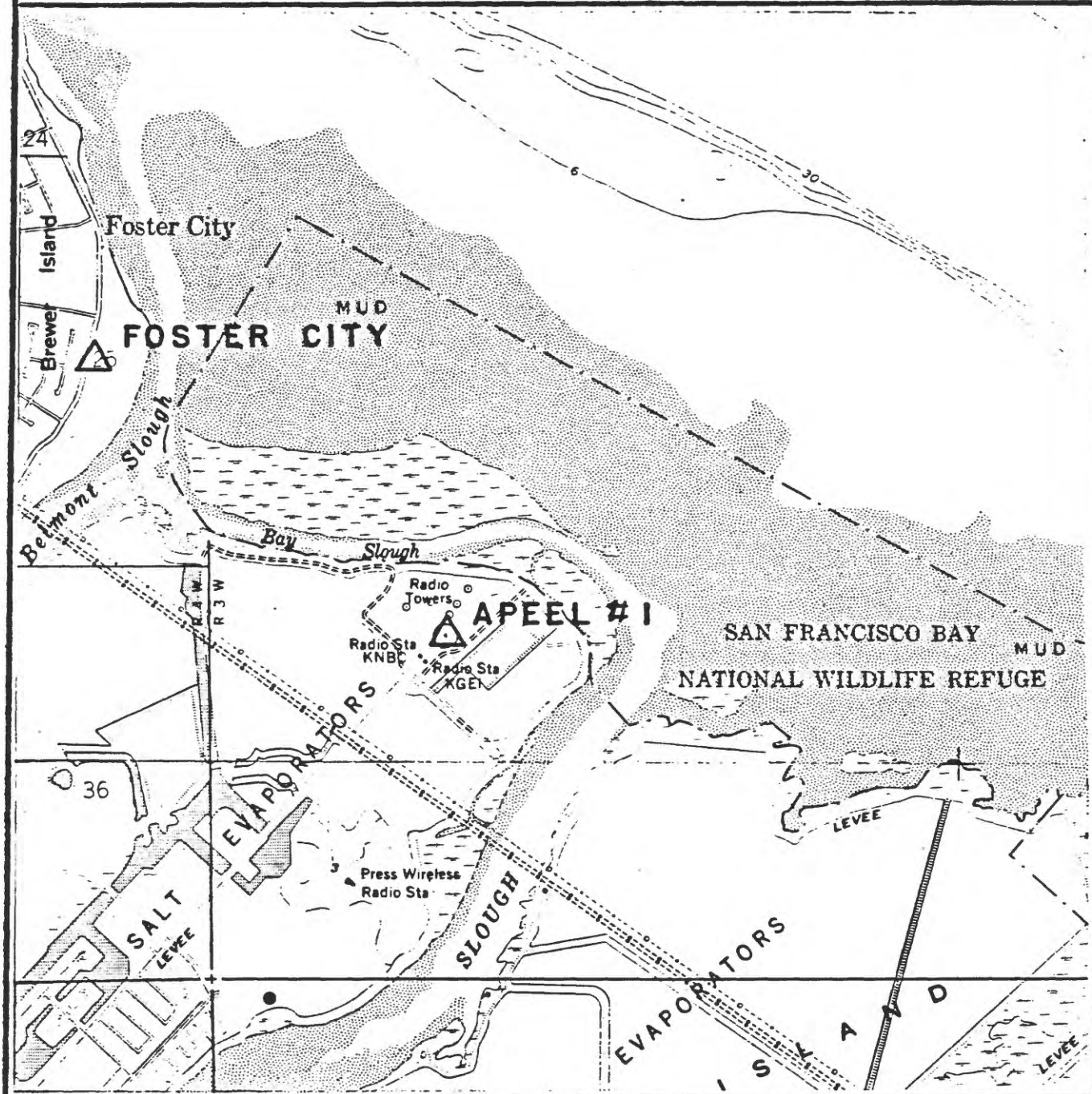


Figure 7. Site location map for the borehole at APEEL #1 and Foster City (not in this report). The borehole at APEEL #1 is located within 30 meters of the strong-motion recorder.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

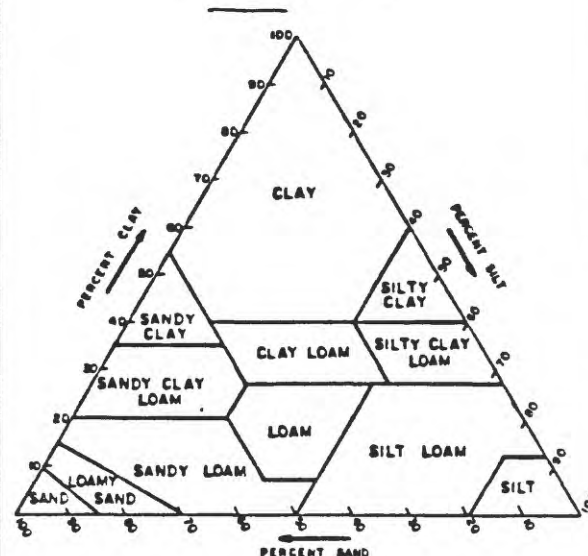
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 8. Explanation of geologic logs. 18

SITE: APEEL #1 (KGEI)

DATE: 5/1/91

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			0	SANDY CLAY LOAM, dk brown (10YR 3/3)
			1	LOAMY SAND, dk olive brown (2.5Y 3/4), moderately well sorted (some fine gravel), some shells
			2	
			3	CLAY (BAY MUD), dk grey (5Y 4/1), very soft
			4	dk grey
			5	very dk greenish grey (5G 3/1)
			6	
			7	
			8	
			9	
			10	
			11	
			12	
			13	
			14	
			15	
			16	
			17	
			18	
			19	
			20	
			21	
			22	very dk greenish grey (5GY 3/1), silty
			23	
			24	
			25	
			26	
			27	
			28	SANDY FINE GRAVEL, dk greenish grey
			29	CLAY (OLDER BAY MUD), dk greenish grey, very stiff
			30	mottled olive grey (5Y 5/2)
			31	
			32	dk greenish grey (5G 4/1)
			33	
			110	

Figure 9. Geologic log for APEEL #1 borehole. 19

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			110 34	
			35	
			36	
			120 37	
			38	
			39	
			130 40	very dk greenish grey (5G 3/1), silty, soft
			41	
			42	
			140 43	dk greenish grey (5G 4/1), very stiff
			44	
			150 45	very dk greenish grey (5G 3/1), soft
			46	
			47	
			48	
			160 49	FINE GRAVEL AND SHELLS
			50	CLAY, dk greenish grey, very stiff
			51	
			170 52	softer
			53	
			54	stiffer
			180 55	
			56	
			57	very stiff
			190 58	softer
			59	
			60	
			200 61	
			62	
			63	
			210 64	
			65	
			66	SAND, fine to coarse grained
			220 67	

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			220	
			68	
			69	
			230	
			70	
			71	
			72	
			240	
			73	
			74	
			75	GRAVELLY SAND
			250	
			76	SAND, fine to coarse grained (moderately well sorted)
			77	
			78	
			260	
			79	
			80	
			81	
			270	
			82	
			83	
			84	
			280	
			85	
			86	
			87	CLAY, dk greenish grey, stiff
			290	
			88	
			89	
			90	
			300	
			91	CLAY LOAM, olive (5Y 5/4)
			92	
			93	
			310	
			94	brownish yellow (10YR 6/6) to yellowish brown (10YR 5/4)
			95	
			96	
			320	
			97	
			98	
			99	
			100	
			330	

Figure 9. (Continued).

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			330 101	
			102	
			103	
			340 104	
			105	
			106	
			350 107	GRAVELLY SAND, dk greyish brown
			108	
			109	
			360 110	
			111	CLAY, dk greenish grey, very stiff
			112	
			370 113	
			114	
			115	
			380 116	
			117	
			118	GRAVELLY SAND
			390 119	CLAY, olive grey (5Y 4/2), very stiff
			120	
			121	
			400 122	
			123	
			124	
			410 125	
			126	
			127	
			420 128	olive (5Y 5/3)
			129	
			130	
			430 131	
			132	
			133	
			440 134	

Figure 9. (Continued).

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			440	
			135	SAND, some gravel, dense
			136	
			450	CLAY LOAM, lt olive brown (2.5Y 5/4), very stiff
			137	
			138	
			139	
			460	
			140	
			141	
			142	
			470	
			143	
			144	
			145	
			480	olive brown (2.5Y 4/4), sandy
			146	
			147	
			148	
			490	
			149	
			150	
			151	CLAY, very stiff
			500	SAND, yellowish brown (10YR 5/4), very dense
			152	
			153	
			510	GRAVELLY SAND, poorly sorted
			154	
			155	
			156	
			157	CLAY, very stiff
			158	
			520	SAND, some gravel, dense
			159	
			160	CLAY, very stiff
			161	
			530	dk greenish grey, firm
			162	
			163	
			164	
			540	
			165	
			166	
			550	GRAVELLY SAND, dk yellowish brown (10YR 5/4), poorly sorted
			167	

Figure 9. (Continued).

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
		<p>The graphic log shows a soil profile with blow counts and depth markers. The depth scale on the right ranges from 550 to 660 feet. The blow count scale on the left ranges from 168 to 201. The soil is divided into three main sections: a top section of yellowish brown soil (550-580 ft), a middle section of sandy loam (580-620 ft), and a bottom section of serpentinite (620-660 ft). The serpentinite section is characterized by a pattern of 'S' shapes and is described as 'sheared, hard' and 'harder'.</p>	<p>550 168</p> <p>169</p> <p>170</p> <p>560 171</p> <p>172</p> <p>173</p> <p>570 174</p> <p>175</p> <p>176</p> <p>580 177</p> <p>178</p> <p>179</p> <p>590 180</p> <p>181</p> <p>182</p> <p>600 183</p> <p>184</p> <p>185</p> <p>610 186</p> <p>187</p> <p>188</p> <p>620 189</p> <p>190</p> <p>191</p> <p>630 192</p> <p>193</p> <p>194</p> <p>640 195</p> <p>196</p> <p>197</p> <p>650 198</p> <p>199</p> <p>200</p> <p>660 201</p>	<p>stiffer</p> <p>yellowish brown</p> <p>SAND, poorly sorted</p> <p>SANDY LOAM, lt olive brown (2.5Y 5/6), some dk brown fine gravel</p> <p>SERPENTINITE (FRANCISCAN FORMATION), pale green (5G 6/2) to greyish green (5G 5/2)</p> <p>sheared, hard</p> <p>harder</p>

Figure 9. (Continued).

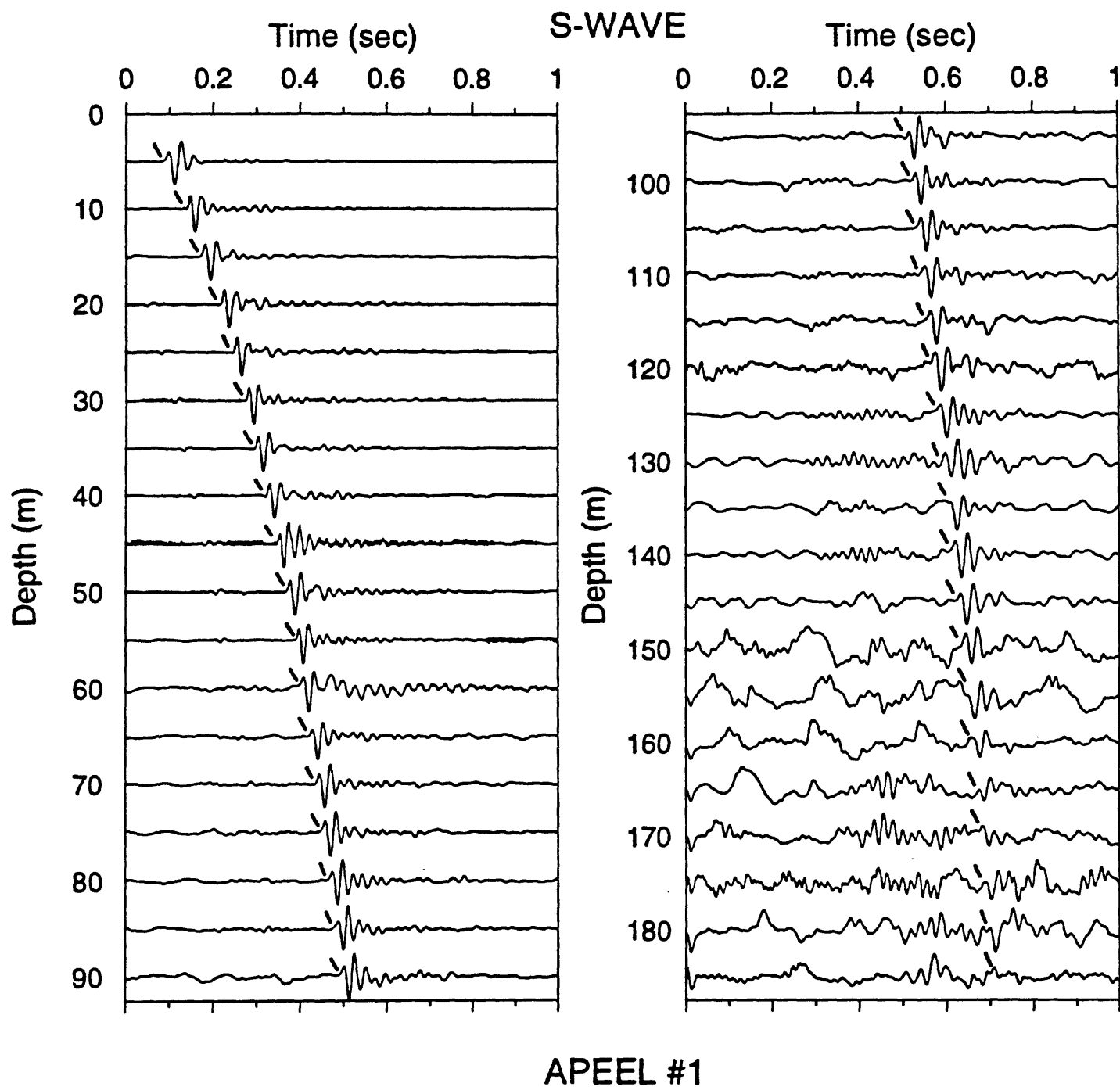


Figure 10. Record section showing the “Away” horizontal components. Records have been 50 Hz low-pass filtered. Because of better signal-to-noise ratios, the shear arrivals (shown by the accent marks) were picked from these components only. The “Toward” records are shown on the next figure.

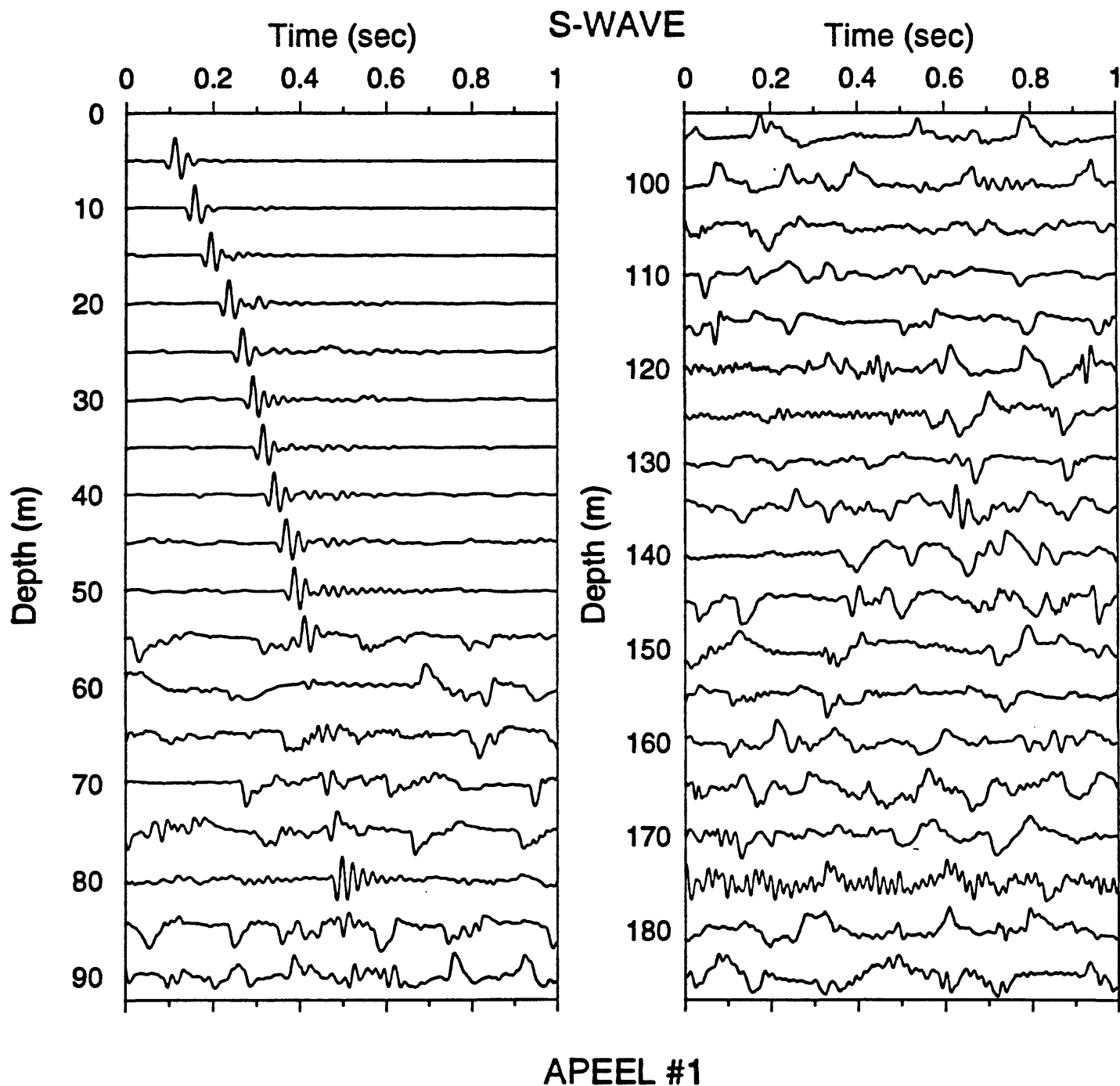


Figure 10. (Continued). Record section showing the "Toward" components. The noise level is higher on these records compared to the "Away" components. Because of the noise the shear arrivals were not pickable from the deeper traces and velocities were determined using the "Away" components only.

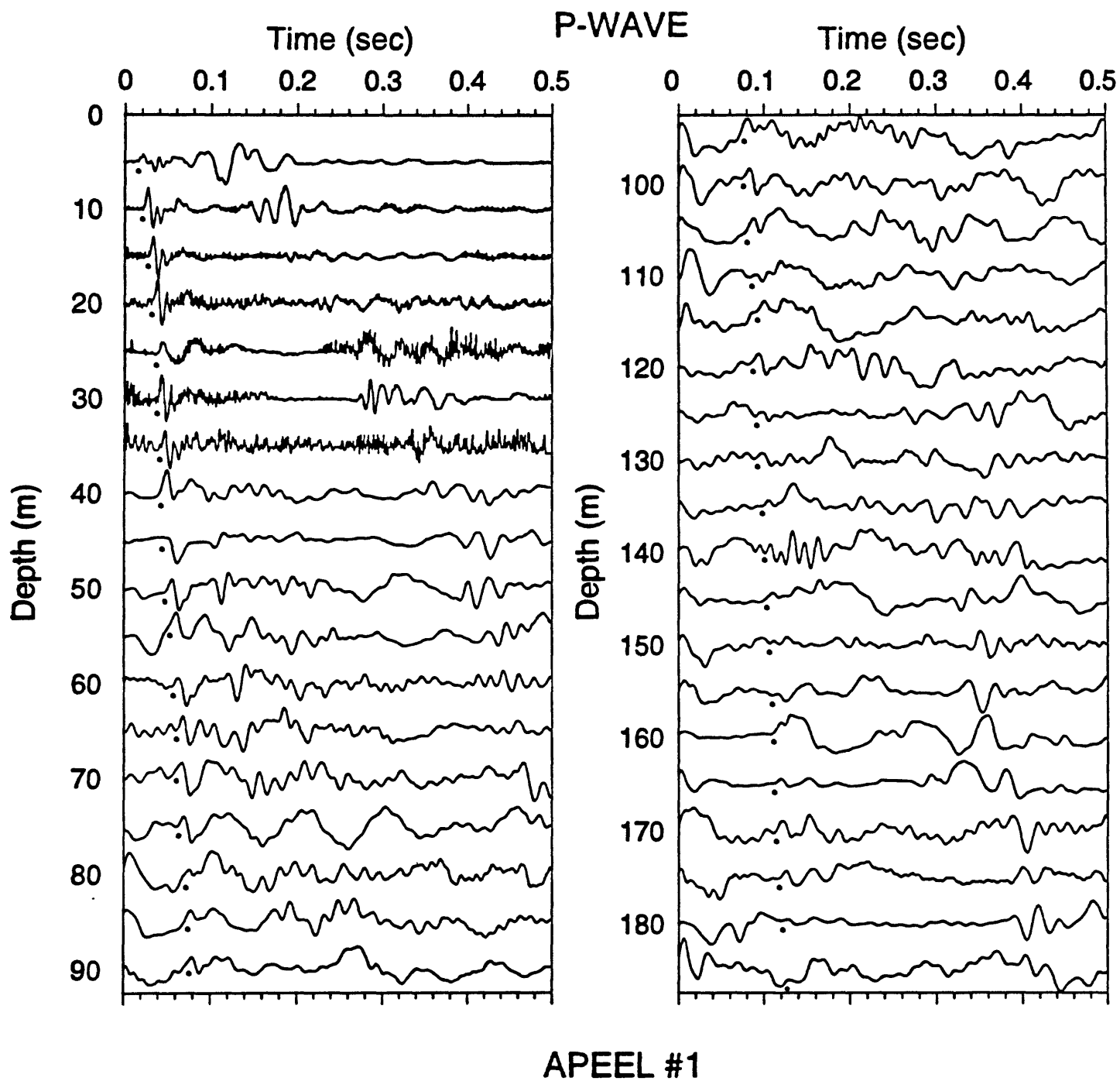


Figure 11. Vertical component record section. P-wave arrivals are shown by the solid circles.

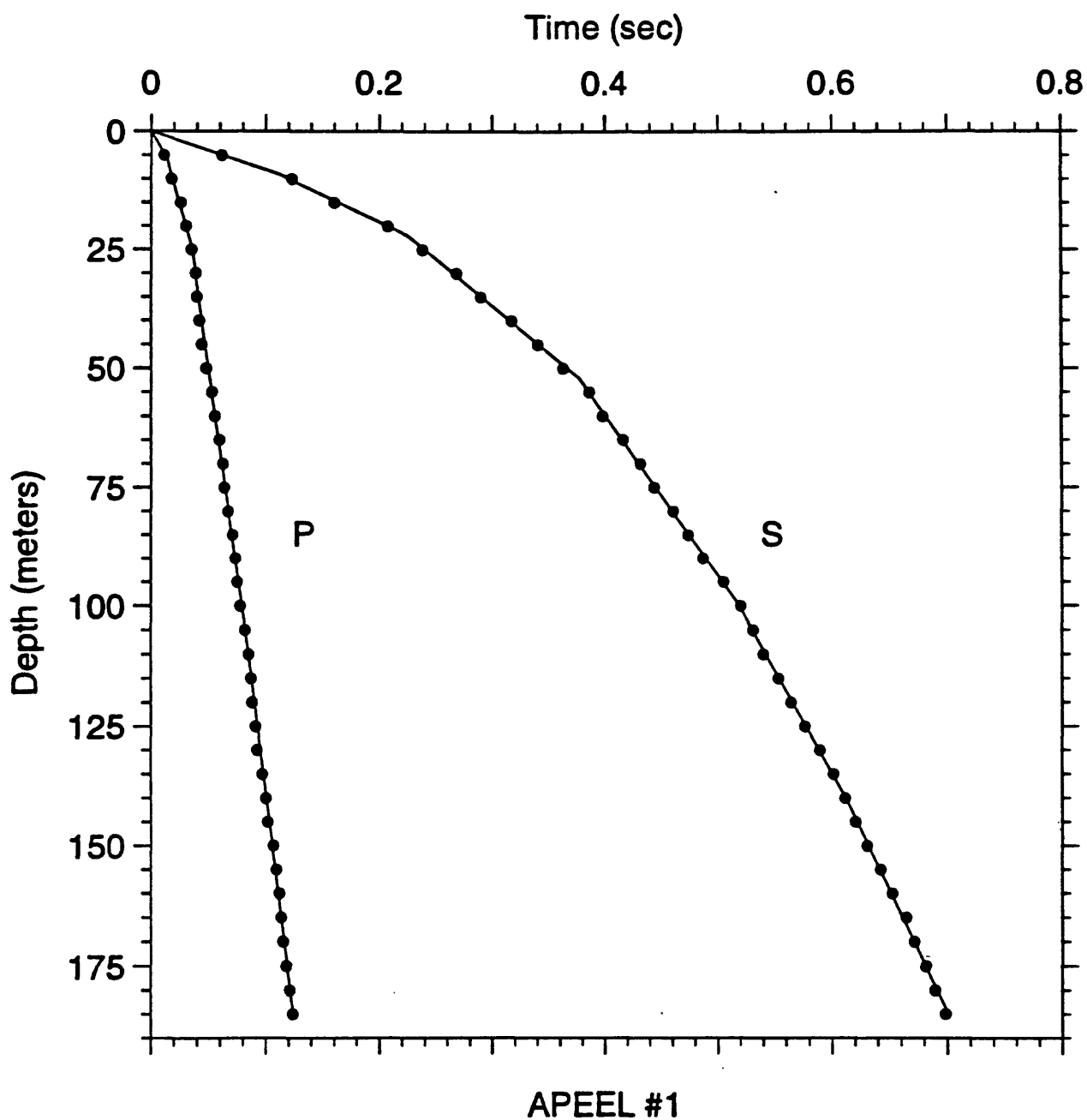


Figure 12. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

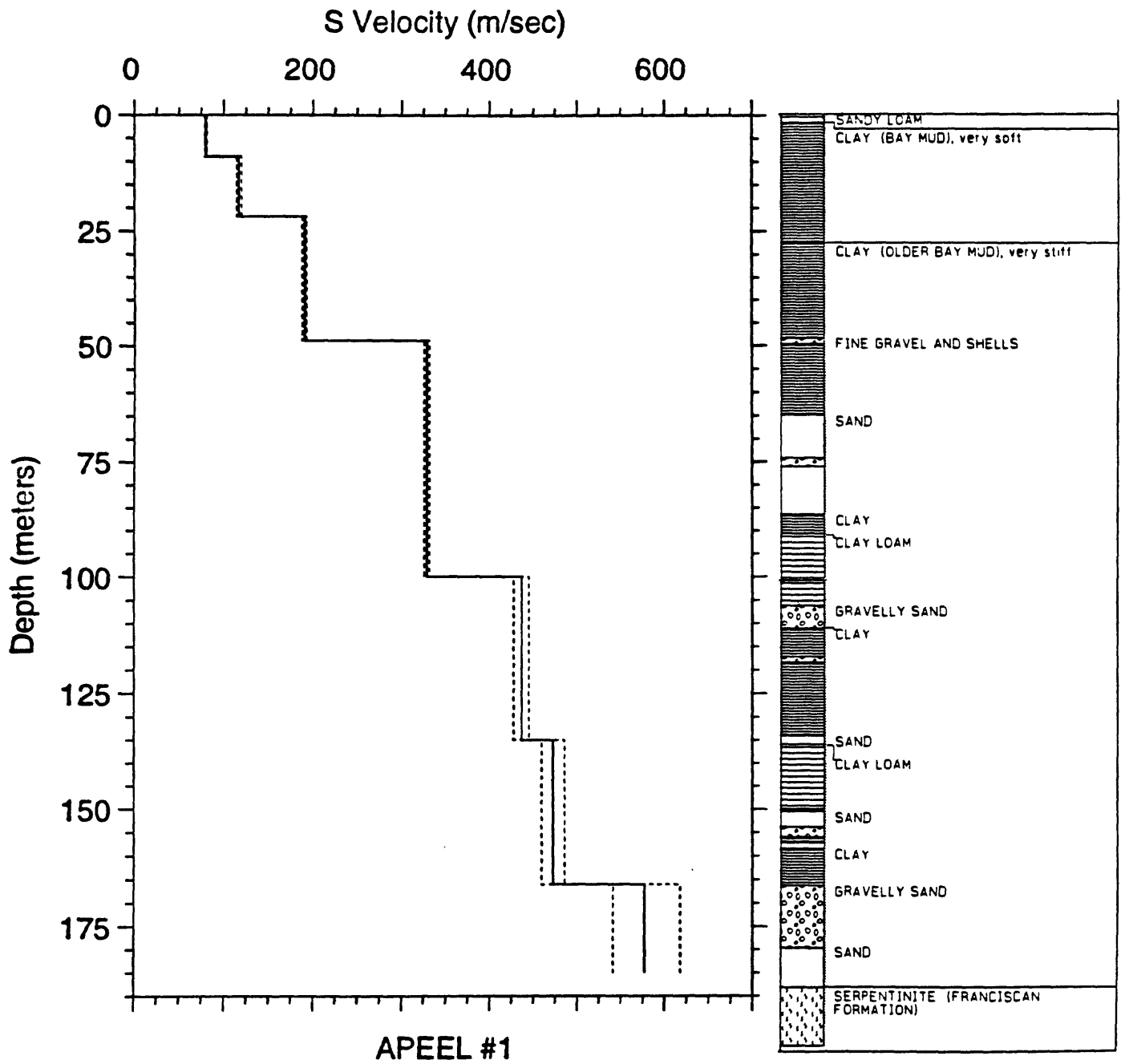


Figure 13. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

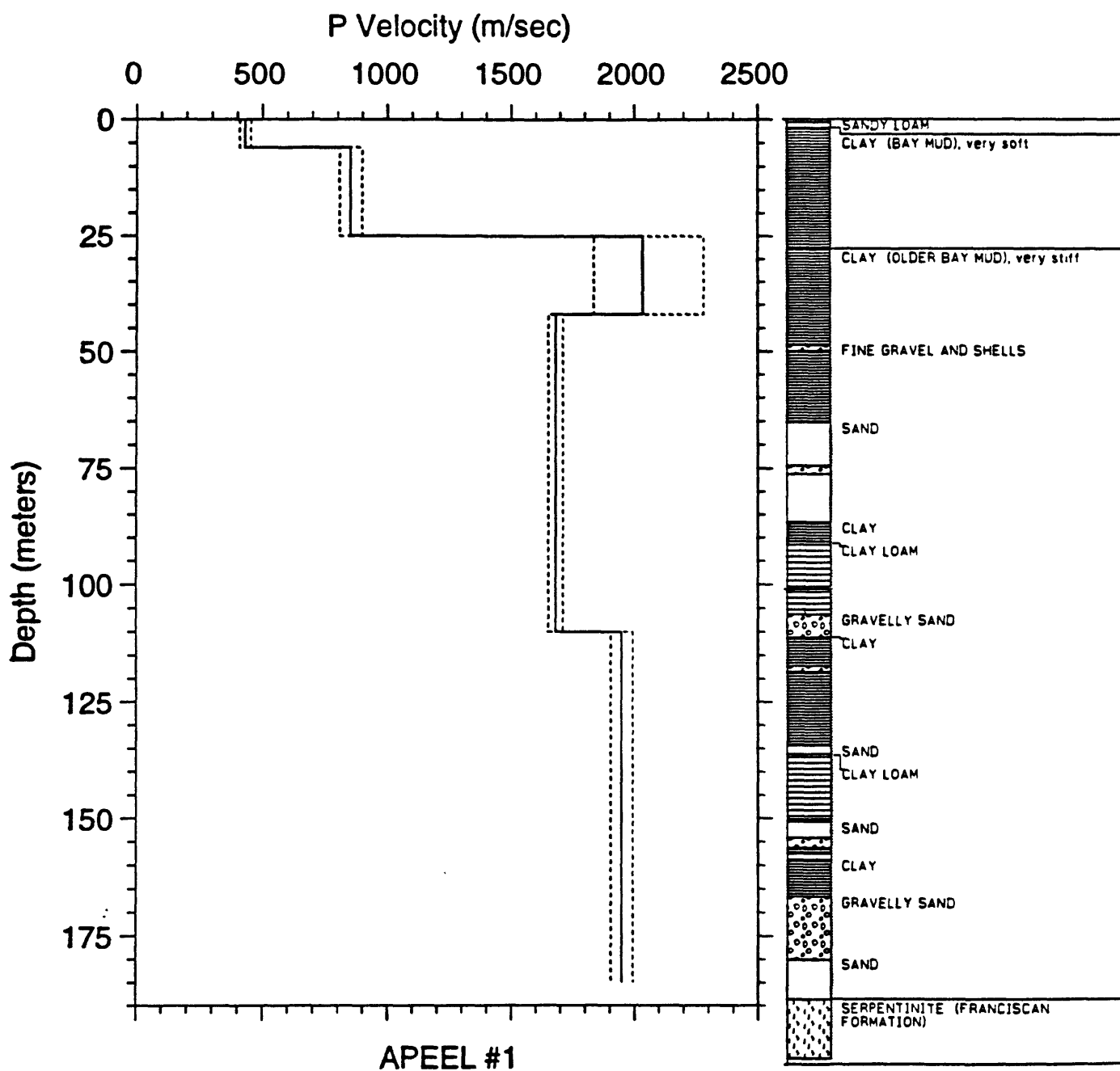


Figure 14. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 1. S-wave arrival times and velocity summaries for APEEL #1.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tbt(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
5.0	16.4	.0615	1	-1.0	.0	.0	.000	80	79	81	262	258	266
10.0	32.8	.1234	1	2.3	9.0	29.5	.113	80	79	81	262	258	266
15.0	49.2	.1603	1	-3.4	22.0	72.2	.223	117	115	120	385	377	394
20.0	65.6	.2076	1	1.4	49.0	160.8	.365	191	188	193	625	617	633
25.0	82.0	.2383	1	-7	100.0	328.1	.520	329	326	332	1080	1069	1091
30.0	98.4	.2683	1	3.0	135.0	442.9	.600	437	428	445	1433	1406	1460
35.0	114.8	.2901	1	-1.4	166.0	544.6	.666	473	460	486	1551	1511	1594
40.0	131.2	.3175	1	-2	185.0	607.0	.699	577	541	618	1893	1775	2027
45.0	147.6	.3409	1	-3.1									
50.0	164.0	.3632	1	-4.8									
55.0	180.4	.3864	1	3.2									
60.0	196.9	.3986	1	-2									
65.0	213.3	.4188	1	3.2									
70.0	229.7	.4319	1	3.1									
75.0	246.1	.4440	1	-0									
80.0	262.5	.4611	1	1.9									
85.0	278.9	.4742	1	-1									
90.0	295.3	.4872	1	-2.3									
95.0	311.7	.5053	1	.6									
100.0	328.1	.5203	1	.4									
105.0	344.5	.5314	1	.0									
110.0	360.9	.5404	1	-2.4									
115.0	377.3	.5535	1	-8									
120.0	393.7	.5645	1	-1.2									
125.0	410.1	.5765	1	-7									
130.0	426.5	.5896	1	1.0									
135.0	442.9	.6016	1	1.5									
140.0	459.3	.6116	1	.9									
145.0	475.7	.6206	1	-6									
150.0	492.1	.6306	1	-1.2									
155.0	508.5	.6427	1	.3									
160.0	524.9	.6527	1	-3									
165.0	541.3	.6647	1	1.2									
170.0	557.7	.6717	1	-9									
175.0	574.1	.6817	1	.5									
180.0	590.6	.6897	1	-2									
185.0	607.0	.6987	1	.1									

Explanation:

- d(m) = depth in meters
- d(ft) = depth in feet
- t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
- sig = sigma, standard deviation normalized to the standard deviation of best picks
- rsdl/sig = least-squares residual divided by sigma
- dtb(m) = depth to bottom of layer in meters
- dtb(ft) = depth to bottom of layer in feet
- tbt(s) = arrival time in seconds to bottom of layer
- v(m/s) = velocity in meters per second
- vl(m/s) = lower limit of velocity in meters per second *
- vu(m/s) = upper limit of velocity in meters per second
- v(ft/s) = velocity in feet per second
- vl(ft/s) = lower limit of velocity in feet per second
- vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

TABLE 2. P-wave arrival times and velocity summaries for APEEL #1.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tth(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
5.0	16.4	.0113	1	-.3	.0	19.7	.000	430	409	453	1411	1343	1486
10.0	32.8	.0179	1	-.8	6.0	82.0	.014	430	409	453	1411	1343	1486
15.0	49.2	.0261	1	1.6	25.0	137.8	.036	850	808	897	2789	2652	2942
20.0	65.6	.0306	1	.2	42.0	110.0	.045	2034	1835	2281	6672	6019	7484
25.0	82.0	.0353	2	-.5	110.0	607.0	.085	1681	1652	1710	5514	5419	5611
30.0	98.4	.0390	1	-.2	185.0		.124	1947	1904	1993	6389	6247	6538
35.0	114.8	.0401	1	-1.1									
40.0	131.2	.0422	1	-1.5									
45.0	147.6	.0442	4	-.6									
50.0	164.0	.0483	1	-1.1									
55.0	180.4	.0533	1	.9									
60.0	196.9	.0558	1	.4									
65.0	213.3	.0598	1	1.5									
70.0	229.7	.0628	1	1.5									
75.0	246.1	.0639	1	-.4									
80.0	262.5	.0674	1	-.1									
85.0	278.9	.0714	1	1.2									
90.0	295.3	.0739	1	.7									
95.0	311.7	.0754	1	-.8									
100.0	328.1	.0779	1	-1.3									
105.0	344.5	.0824	1	.3									
110.0	360.9	.0854	1	.3									
115.0	377.3	.0874	4	-.1									
120.0	393.7	.0884	2	-.9									
125.0	410.1	.0914	2	-.7									
130.0	426.5	.0929	2	-1.2									
135.0	442.9	.0974	2	-.3									
140.0	459.3	.1004	4	.0									
145.0	475.7	.1019	2	-.6									
150.0	492.1	.1069	4	.3									
155.0	508.5	.1099	2	.8									
160.0	524.9	.1124	3	.5									
165.0	541.3	.1139	2	.3									
170.0	557.7	.1155	2	-.2									
175.0	574.1	.1185	1	.0									
180.0	590.6	.1215	3	.1									
185.0	607.0	.1240	4	.1									

Explanation:

d(m) = depth in meters
d(ft) = depth in feet
t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
sig = sigma, standard deviation normalized to the standard deviation of best picks
rsdl/sig = least-squares residual divided by sigma
dtb(m) = depth to bottom of layer in meters
dtb(ft) = depth to bottom of layer in feet
tth(s) = arrival time in seconds to bottom of layer
v(m/s) = velocity in meters per second
vl(m/s) = lower limit of velocity in meters per second
vu(m/s) = upper limit of velocity in meters per second
v(ft/s) = velocity in feet per second
vl(ft/s) = lower limit of velocity in feet per second
vu(ft/s) = upper limit of velocity in feet per second
* see text for explanation of velocity limits

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SAN MATEO QUADRANGLE
CALIFORNIA—SAN MATEO CO.
7.5 MINUTE SERIES (TOPOGRAPHIC)

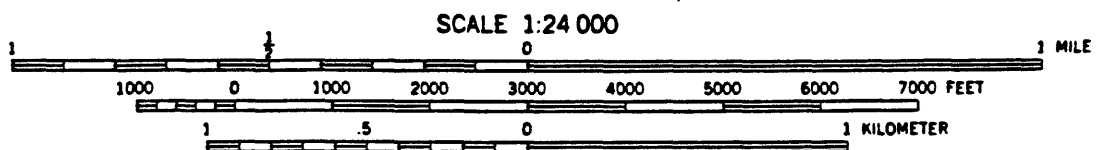


Figure 15. Site location map for APEEL #2 (Portside Park).

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
> 100	> 36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

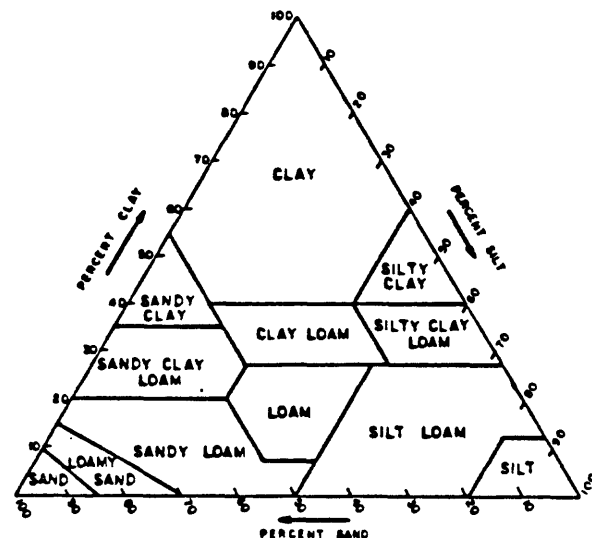
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
> 50	v. dense	15-30	v. stiff
		> 30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 16. Explanation of geologic log for APEEL #2 (Portside Park).

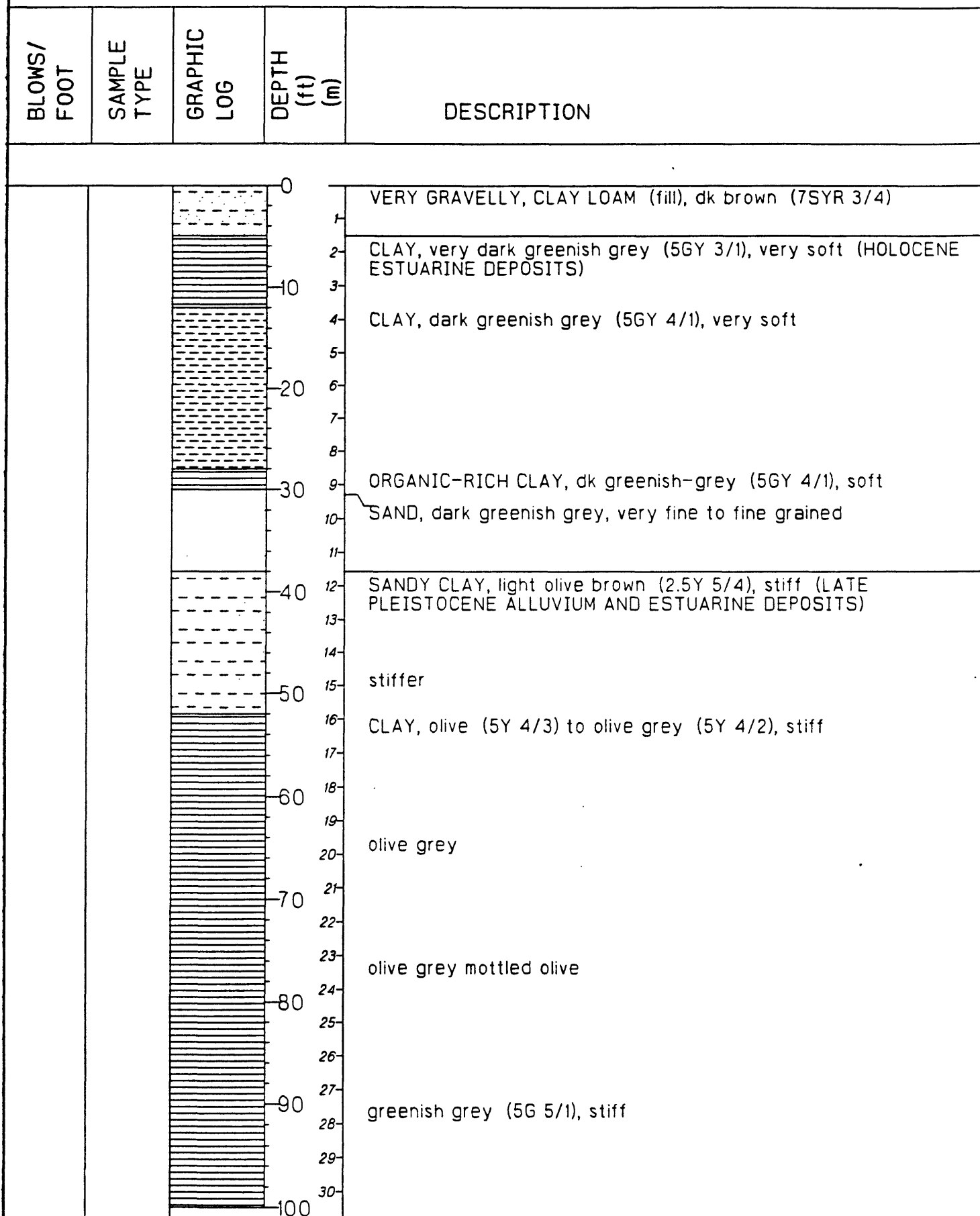


Figure 17. Geologic log for APEEL #2.

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			100 31	
			32	CLAY TO CLAY LOAM, brown (10YR 5/3)
			33	
			110 34	FINE GRAVELLY SAND
			35	FINE SANDY CLAY LOAM, dark yellowish brown (10YR 4/4), stiff
			36	
			120 37	grading to CLAY, greenish grey (5GY 4/1)
			38	
			39	FINE GRAVELLY SAND, mixed greenish grey, dark brown, and olive brown
			130 40	CLAY LOAM, dark greyish brown (2.5Y 4/2)
			41	
			42	
			140 43	CLAY LOAM, dark greyish brown (2.5Y 4/2) to olive brown (2.5Y 4/4), poorly sorted (some fine gravel), very stiff
			44	
			45	
			150 46	CLAY LOAM, olive brown (2.5Y 4/4), poorly sorted
			47	
			48	
			160 49	CLAY, dark yellowish brown (10YR 4/4)
			50	
			51	
			170 52	CLAY, dark yellowish brown (10YR 4/6)
			53	
			54	CLAY LOAM, strong brown (7.5YR 4/6)
			180 55	
			56	
			57	
			190 58	GRAVEL, dark brown, poorly sorted
			59	
			60	
			200	

Figure 17. (Continued).

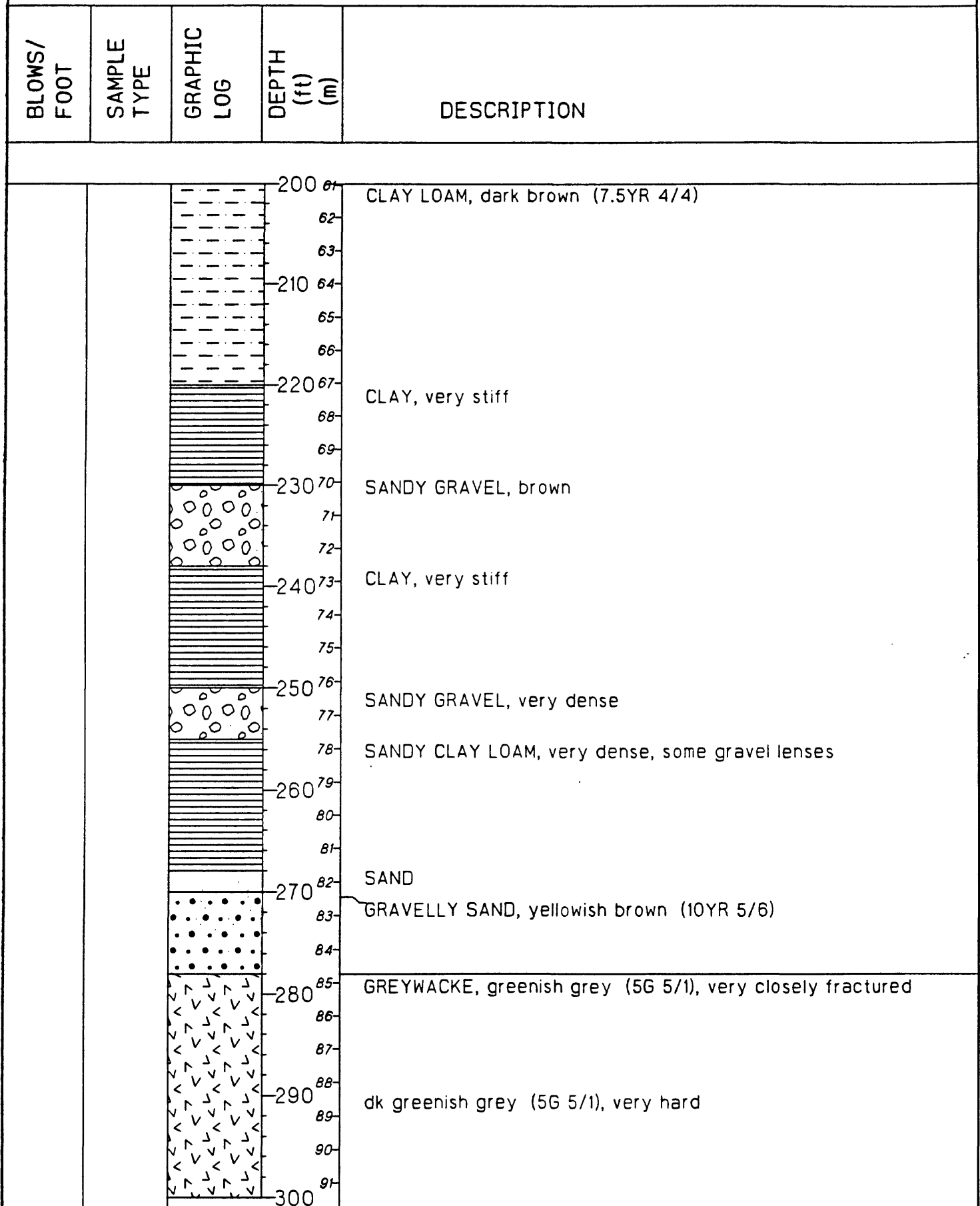


Figure 17. (Continued).


BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			300 92 93 94 310 95 96 97 320 98 99 100 330 101 102 103 340 104 105 106 350 107 108 109 360 110 111 112 370 113 114 115 380 116 117 118 390 119 120 121 400	

Figure 17. (Continued).

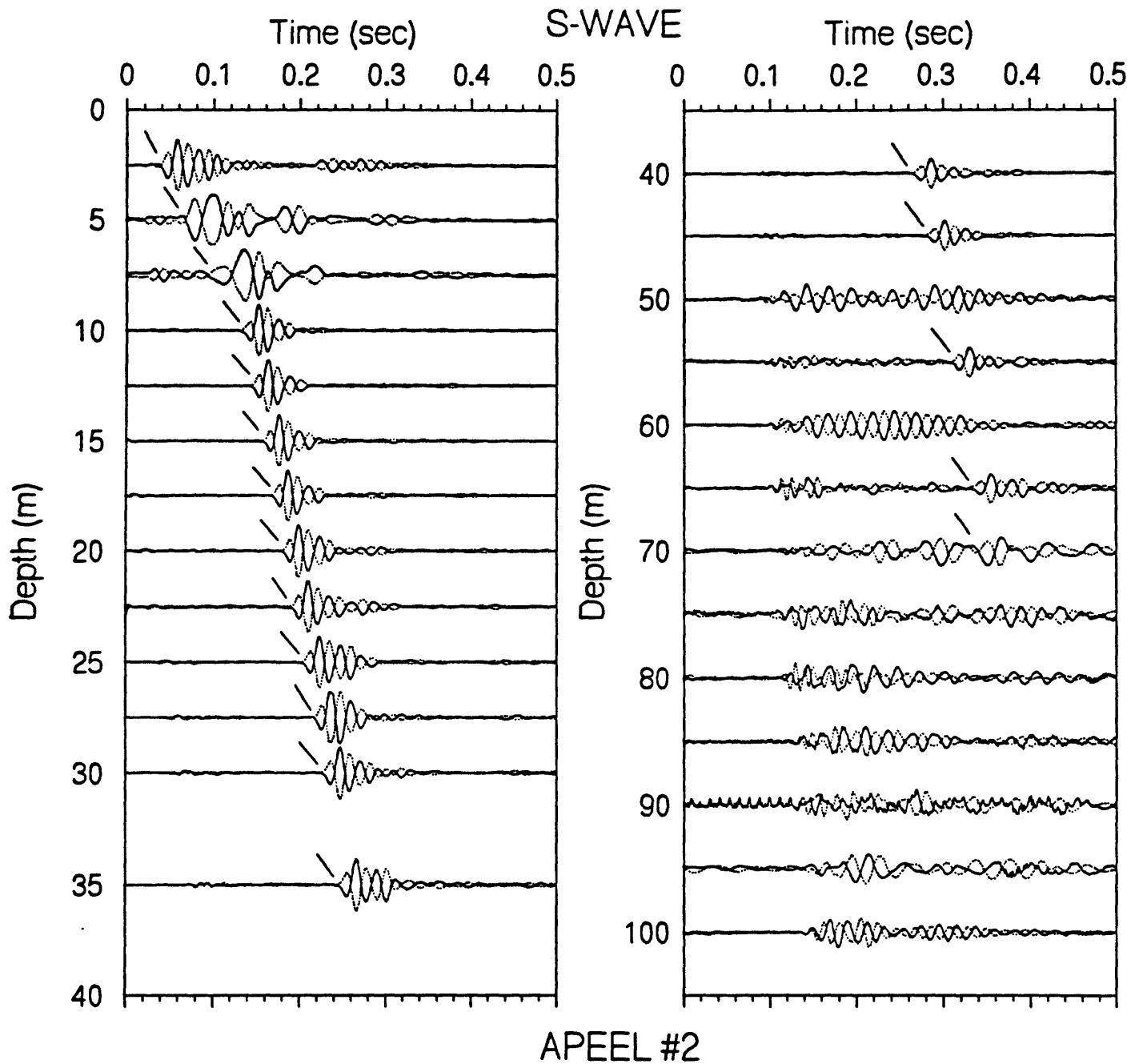


Figure 18. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks. An early arriving wave-train starts to build in amplitude at about 50 meters and continues to the bottom of the borehole. Interference to S-wave arrivals below 70 meters made picks too uncertain for velocity determinations .

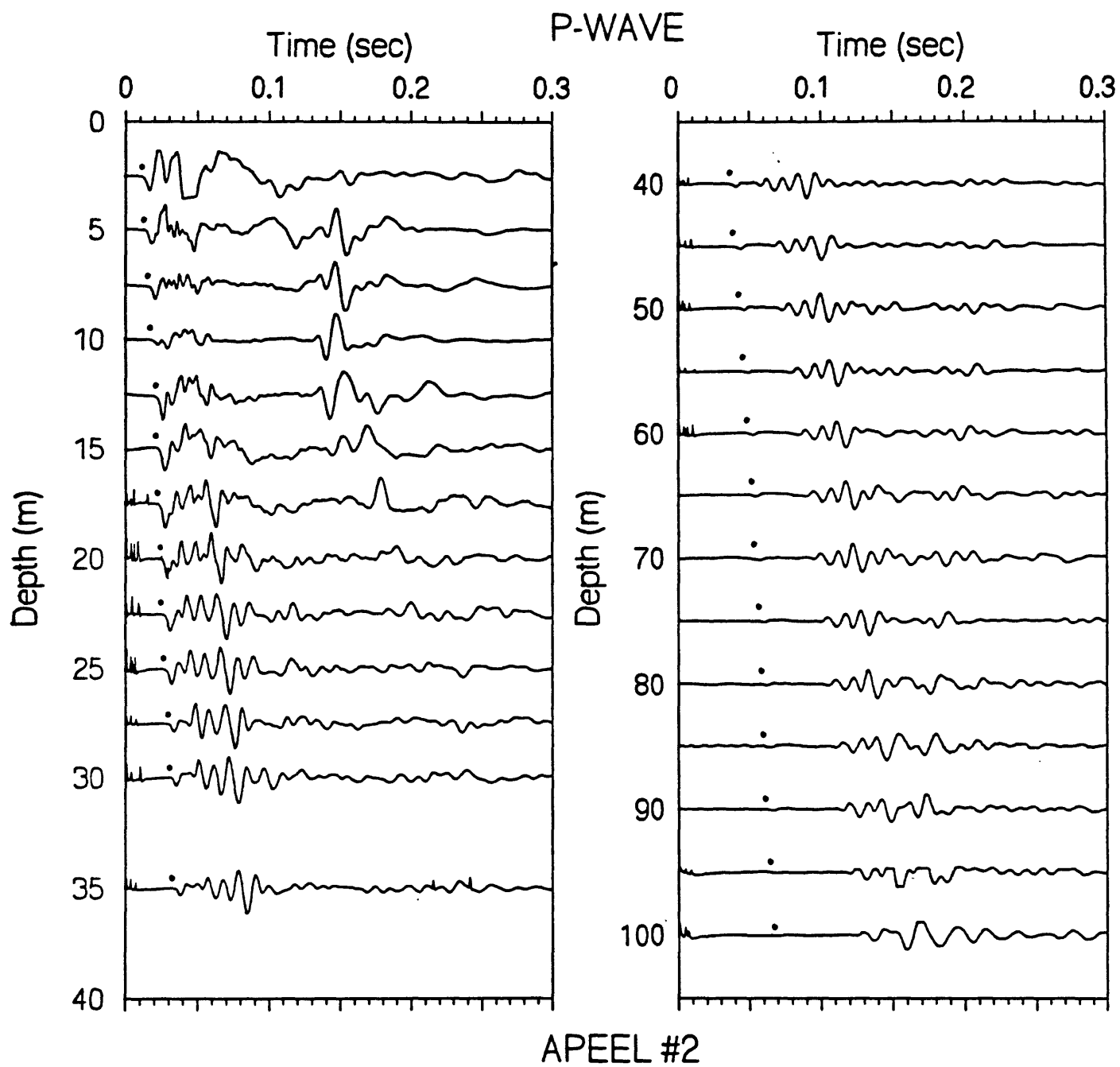


Figure 19. Vertical-component record section. P-waves are shown by the solid circles.

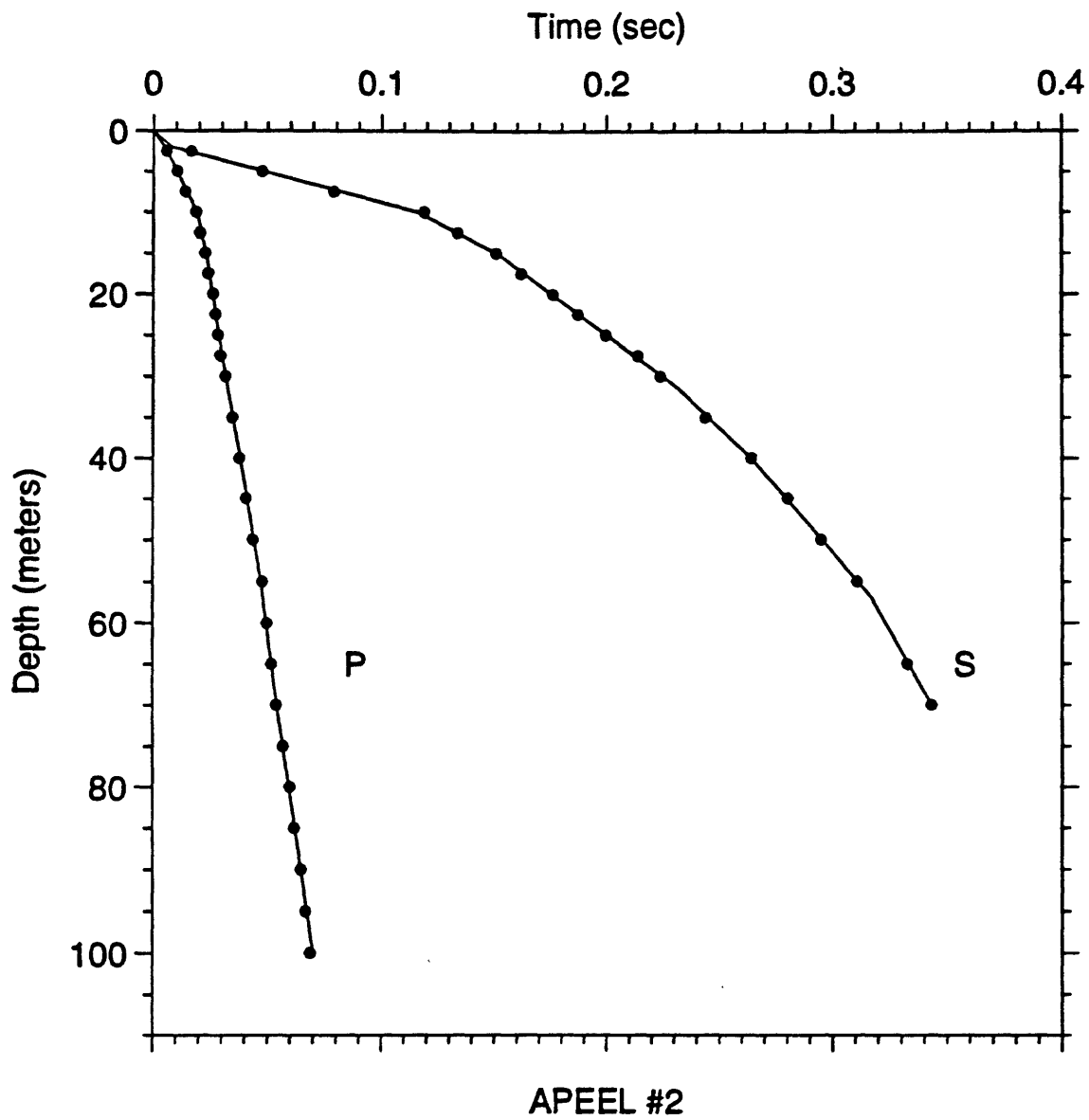


Figure 20. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

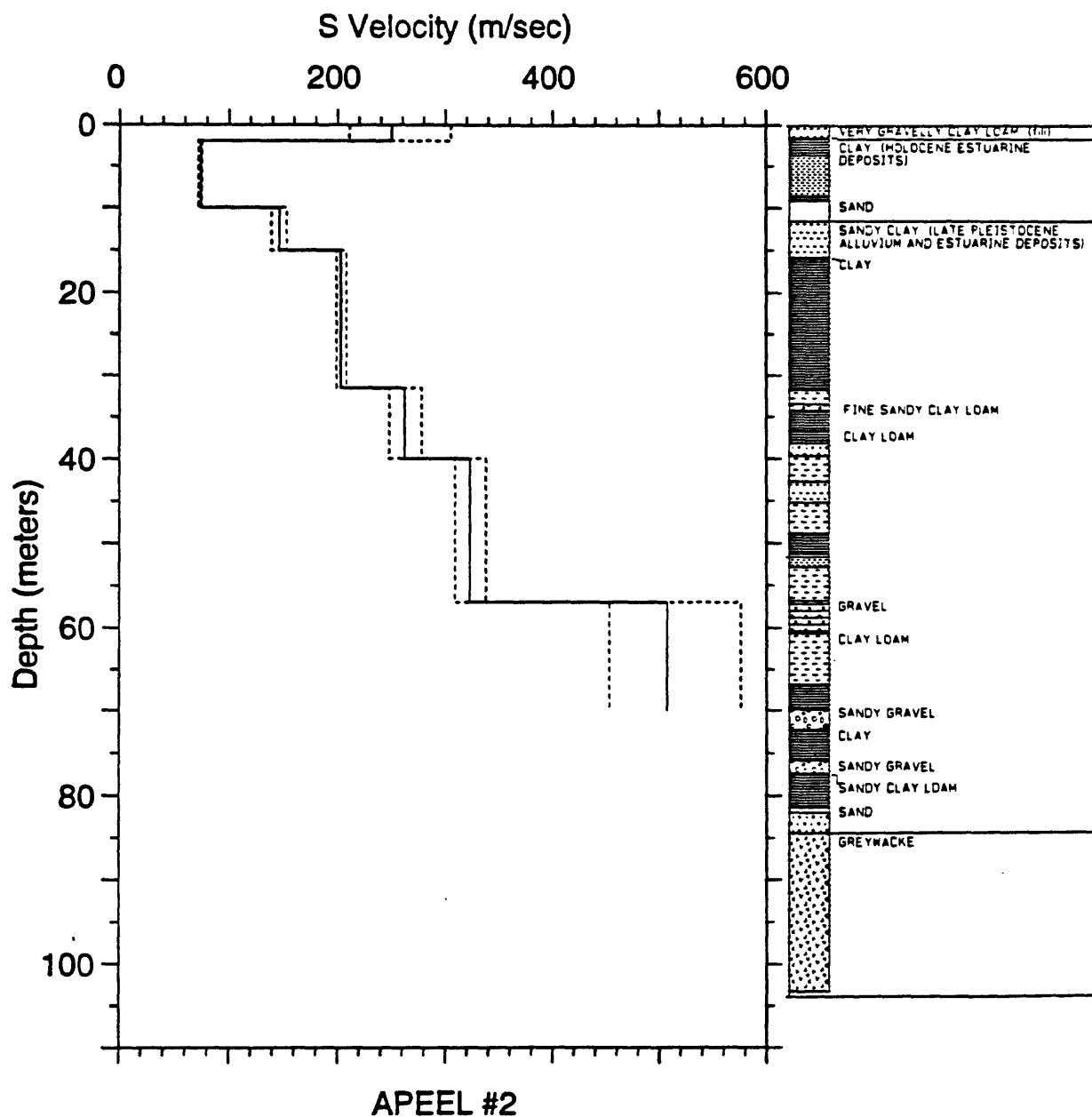


Figure 21. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

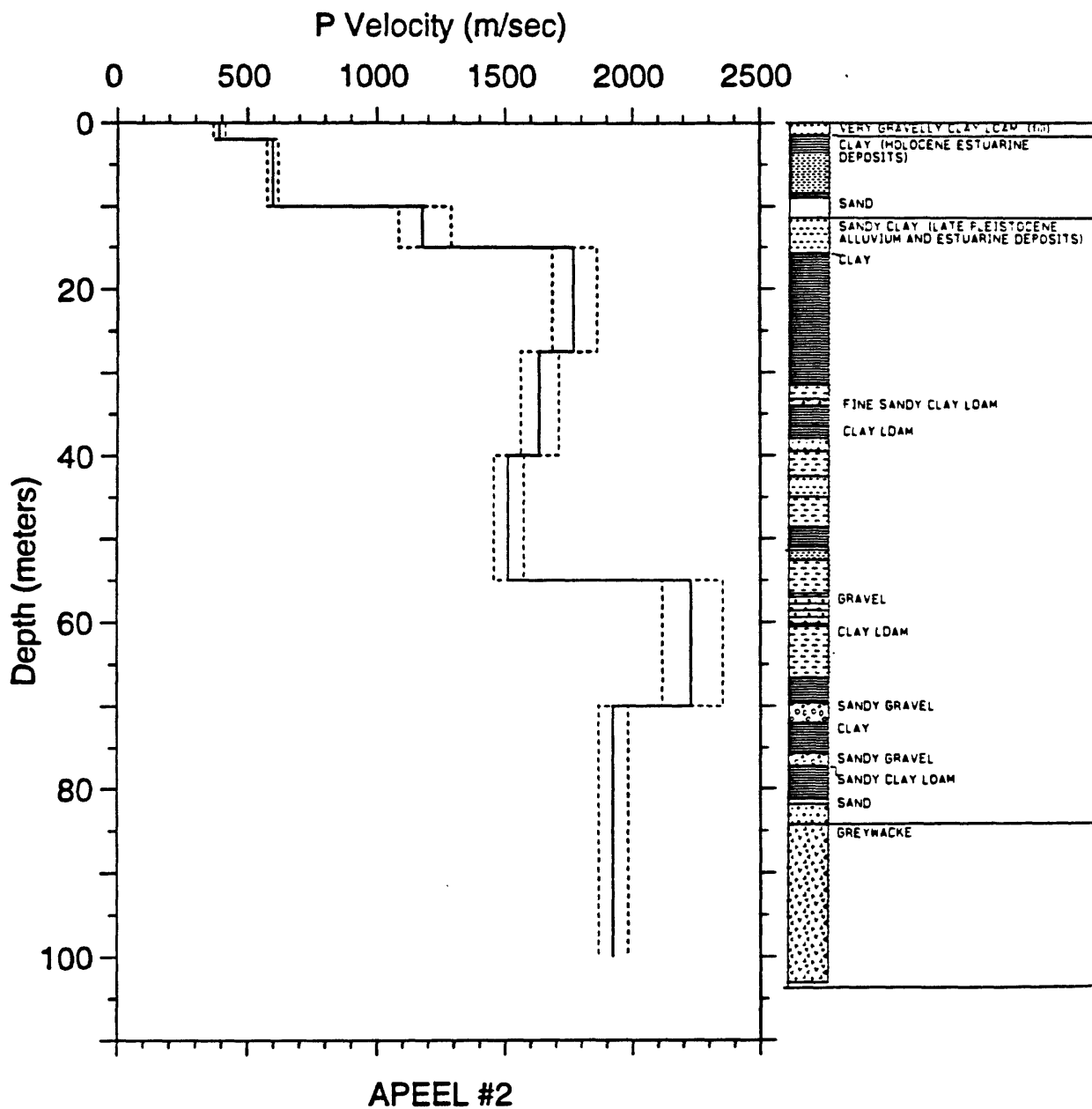


Figure 22. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope of the line segments (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 3. S-wave arrival times and velocity summaries for APEEL #2.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0166	1	1.8	.0	.0	.000	250	211	305	819	694	999
5.0	16.4	.0477	1	-1.0	2.0	6.6	.008	250	211	305	819	694	999
7.5	24.6	.0790	1	-3.5	10.0	32.8	.116	74	72	75	242	237	247
10.0	32.8	.1190	1	2.6	15.0	49.2	.151	146	139	153	478	455	503
12.5	41.0	.1337	1	.1	31.5	103.3	.232	203	199	208	667	653	683
15.0	49.2	.1508	1	.1	40.0	131.2	.264	262	248	278	860	814	911
17.5	57.4	.1620	1	-1.0	57.0	187.0	.317	323	309	338	1059	1013	1109
20.0	65.6	.1761	1	.8	70.0	229.7	.343	507	453	576	1664	1487	1809
22.5	73.8	.1874	1	-2									
25.0	82.0	.1996	1	-3									
27.5	90.2	.2140	1	1.8									
30.0	98.4	.2239	1	-6									
35.0	114.8	.2440	1	-1.2									
40.0	131.2	.2644	1	.1									
45.0	147.6	.2803	1	.5									
50.0	164.0	.2950	2	-1									
55.0	180.4	.3107	1	.0									
65.0	213.3	.3325	1	-2									
70.0	229.7	.3431	2	.3									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

t(b(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

TABLE 4. P-wave arrival times and velocity summaries for APEEL#2.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tbb(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0058	1	-.2	.0	.0	.000	389	367	413	1276	1205	1356
5.0	16.4	.0106	1	-.4	2.0	6.6	.005	389	367	413	1276	1205	1356
7.5	24.6	.0141	1	-.3	10.0	32.8	.019	595	575	616	1951	1887	2021
10.0	32.8	.0188	1	-.2	15.0	49.2	.023	1177	1084	1289	3863	3555	4229
12.5	41.0	.0204	1	-.3	27.5	90.2	.030	1769	1686	1861	5804	5530	6107
15.0	49.2	.0228	1	.0	40.0	131.2	.038	1633	1561	1711	5356	5121	5614
17.5	57.4	.0240	1	-.2	55.0	180.4	.047	1511	1455	1572	4958	4773	5159
20.0	65.6	.0262	1	.5	70.0	229.7	.054	2228	2116	2333	7310	6941	7719
22.5	73.8	.0273	1	-.2	100.0	328.1	.070	1922	1865	1982	6306	6119	6504
25.0	82.0	.0284	1	-.1									
27.5	90.2	.0295	1	-.4									
30.0	98.4	.0316	1	-.2									
35.0	114.8	.0346	1	.1									
40.0	131.2	.0377	1	.1									
45.0	147.6	.0407	1	-.2									
50.0	164.0	.0438	1	-.4									
55.0	180.4	.0478	1	.3									
60.0	196.9	.0498	1	.1									
65.0	213.3	.0518	1	-.2									
70.0	229.7	.0539	1	-.3									
75.0	246.1	.0569	1	.1									
80.0	262.5	.0599	1	.5									
85.0	278.9	.0619	1	-.1									
90.0	295.3	.0649	1	.3									
95.0	311.7	.0669	2	-.2									
100.0	328.1	.0689	2	-.5									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

tbb(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

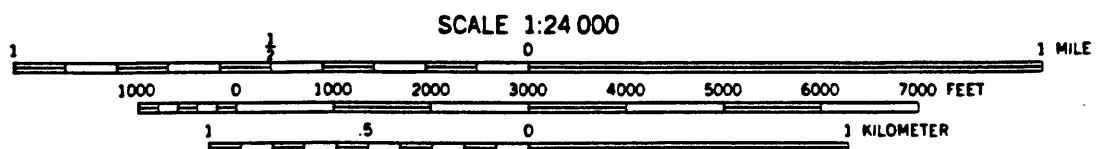
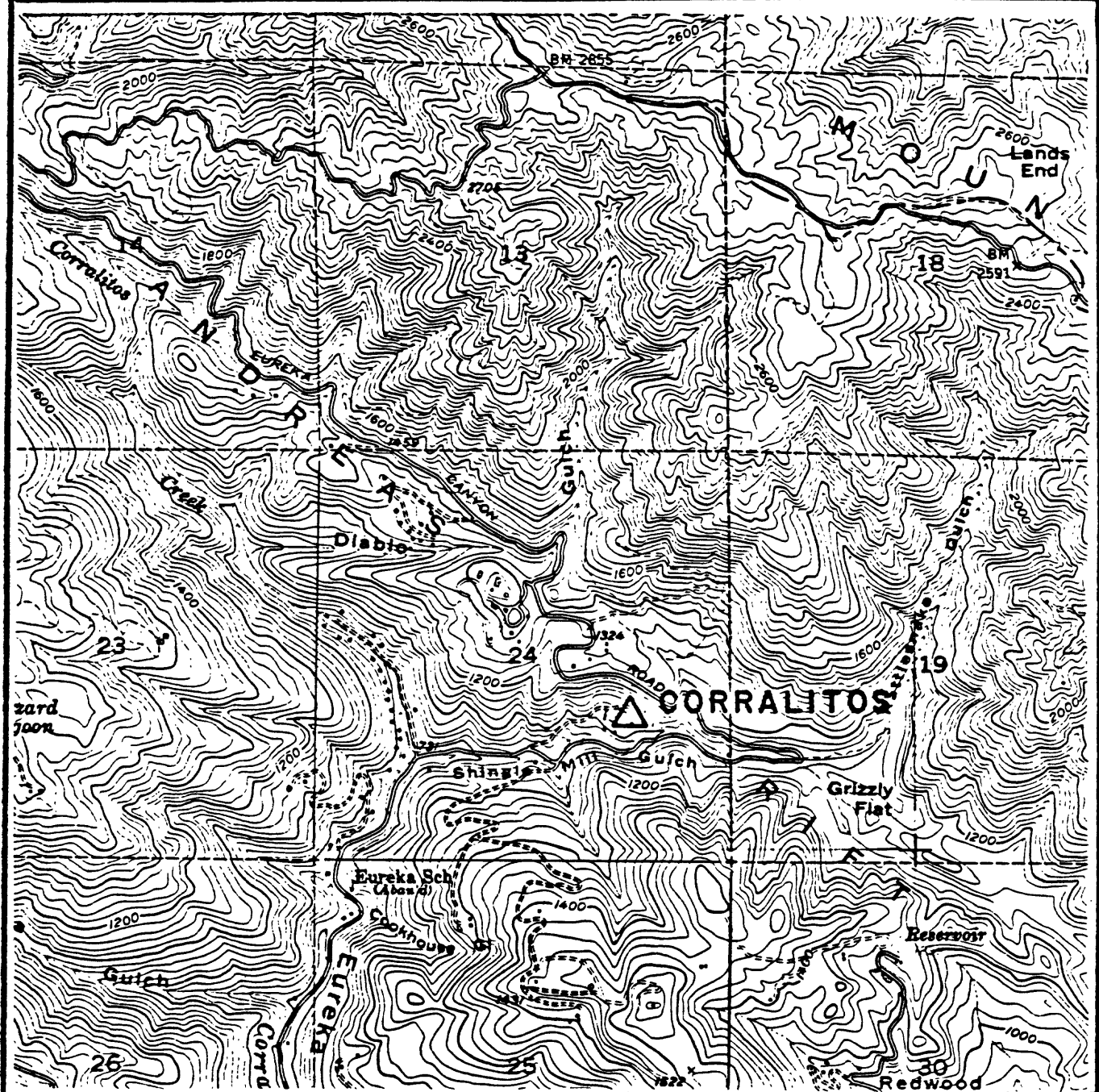


Figure 23. Location map for Corralitos borehole. The borehole is located within 10 meters of the strong-motion accelerometer.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound
firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
> 100	> 36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

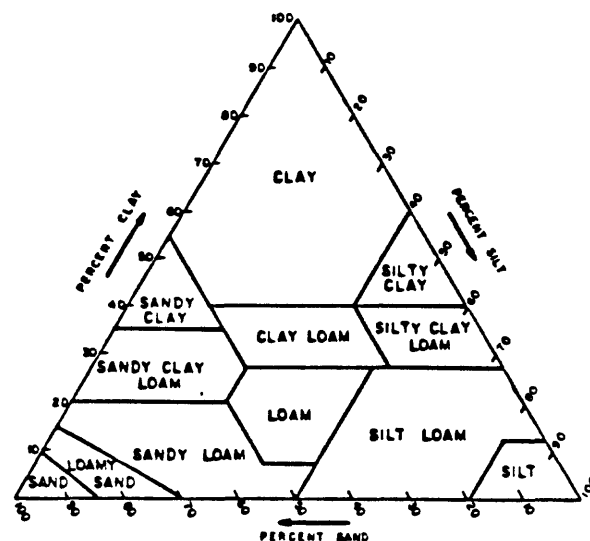
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	< 2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
> 50	v. dense	15-30	v. stiff
		> 30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in-in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 24. Explanation of geologic log.

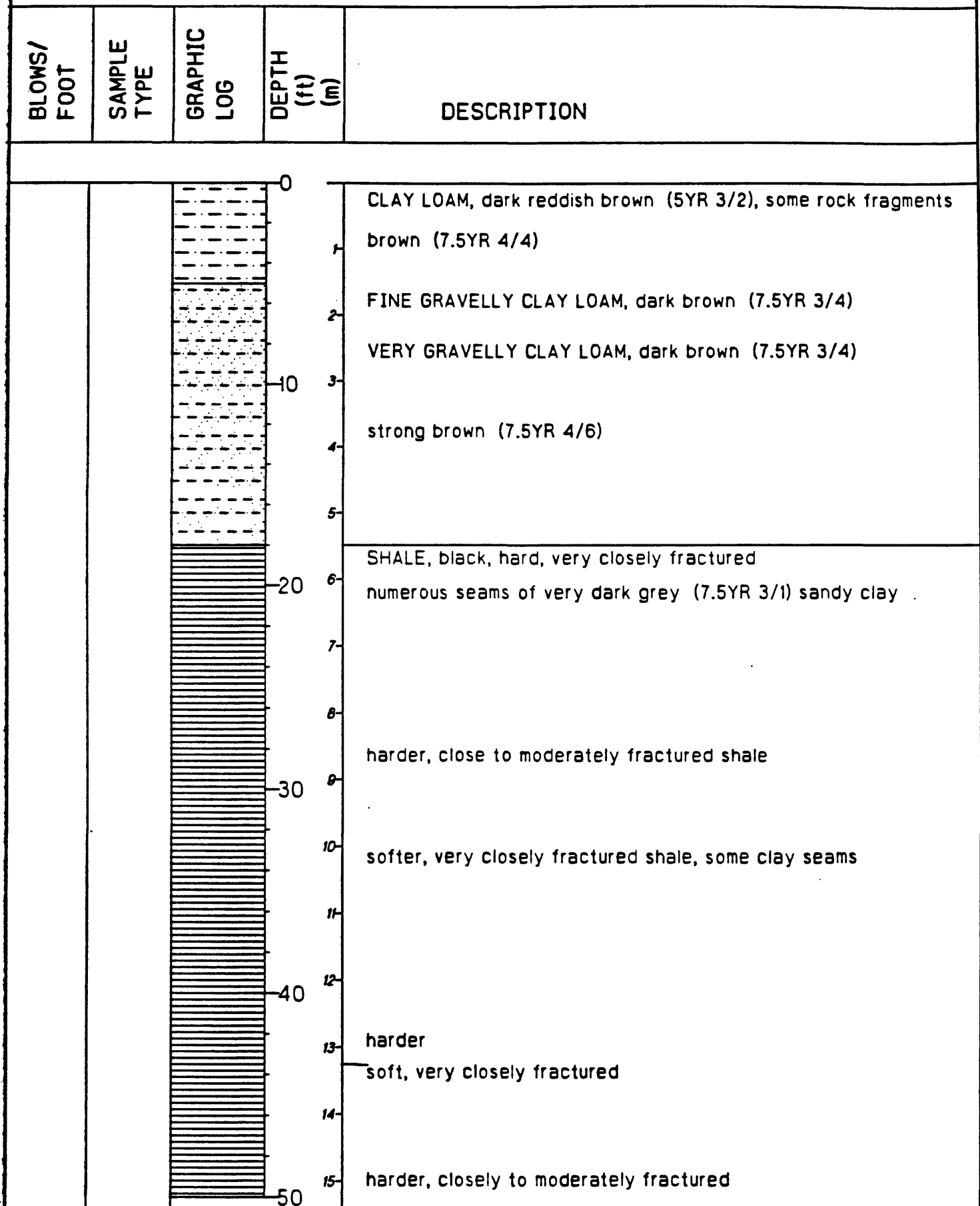


Figure 25. Geologic log of Corralitos borehole.

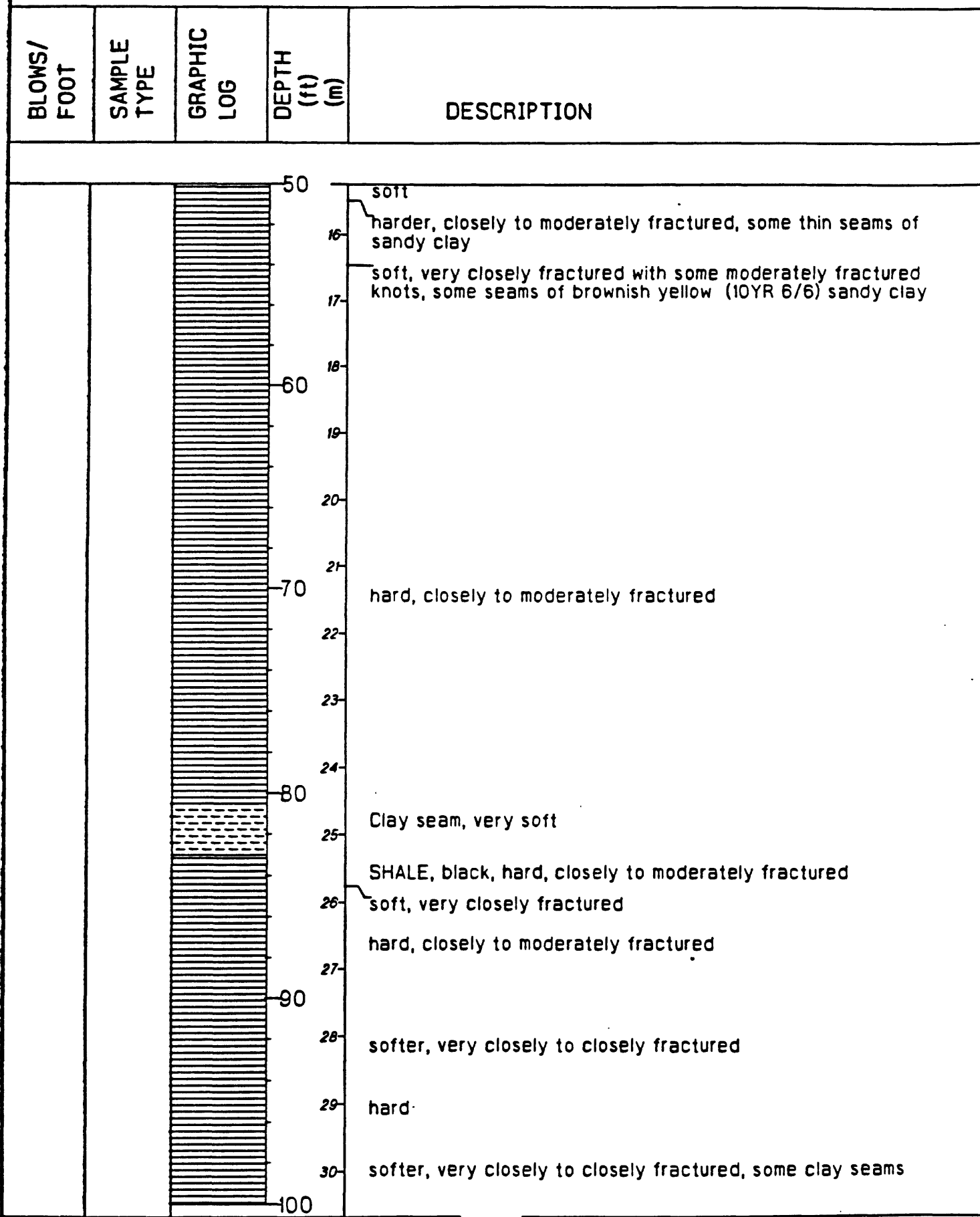


Figure 25. (Continued).

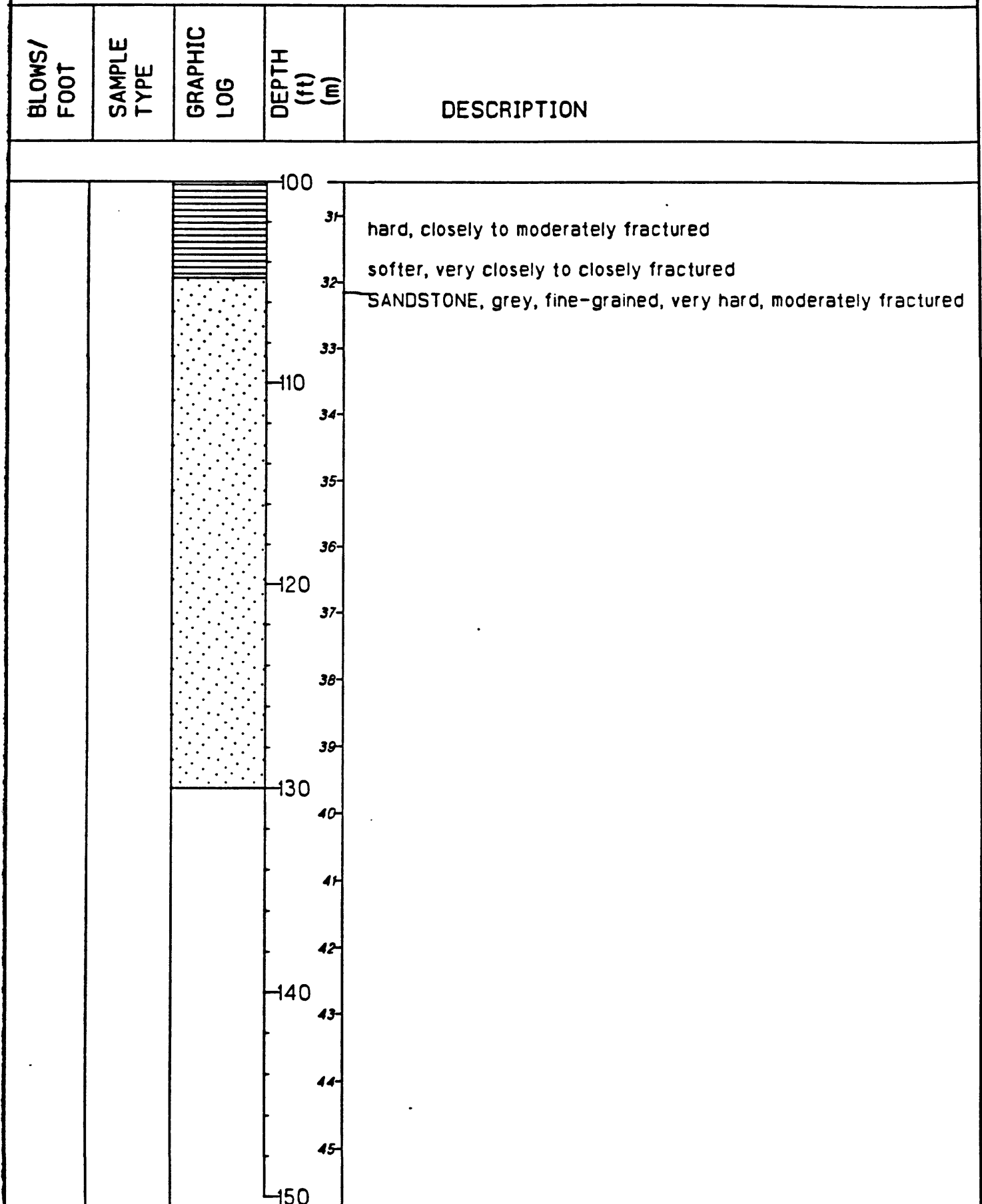


Figure 25. (Continued).

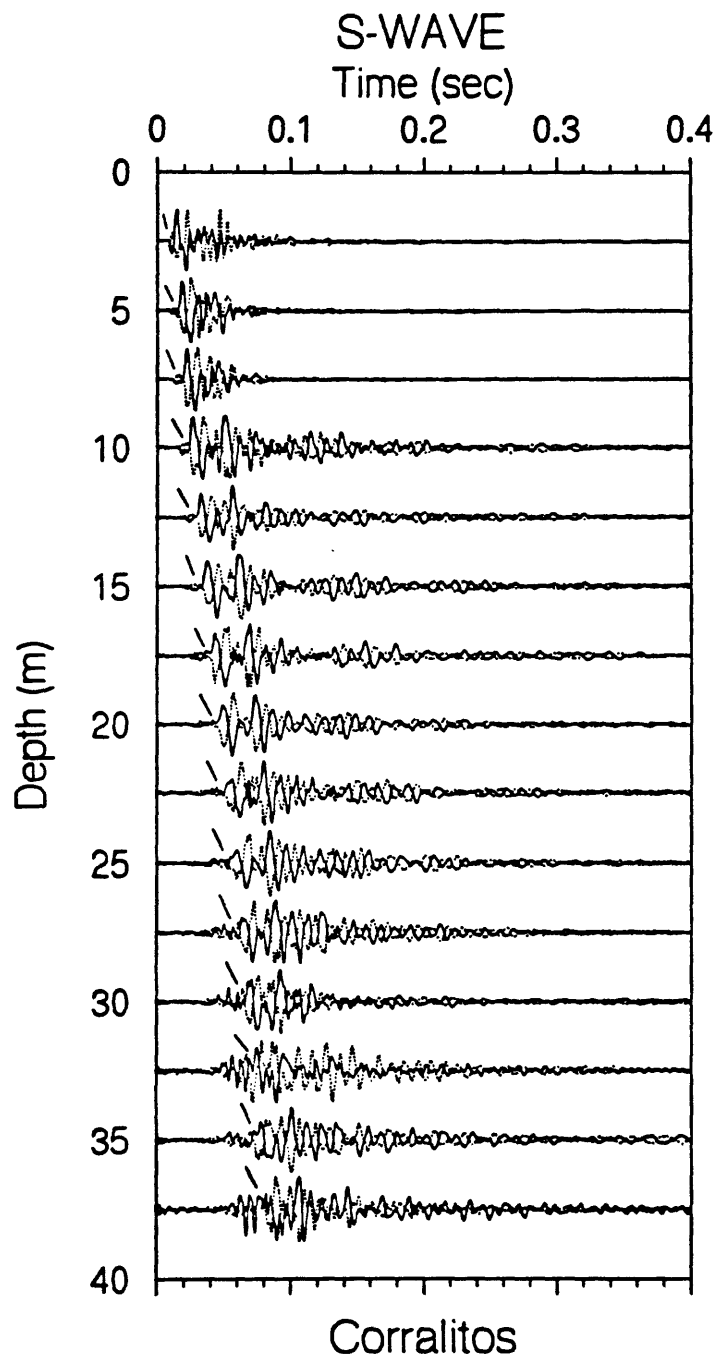


Figure 26. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

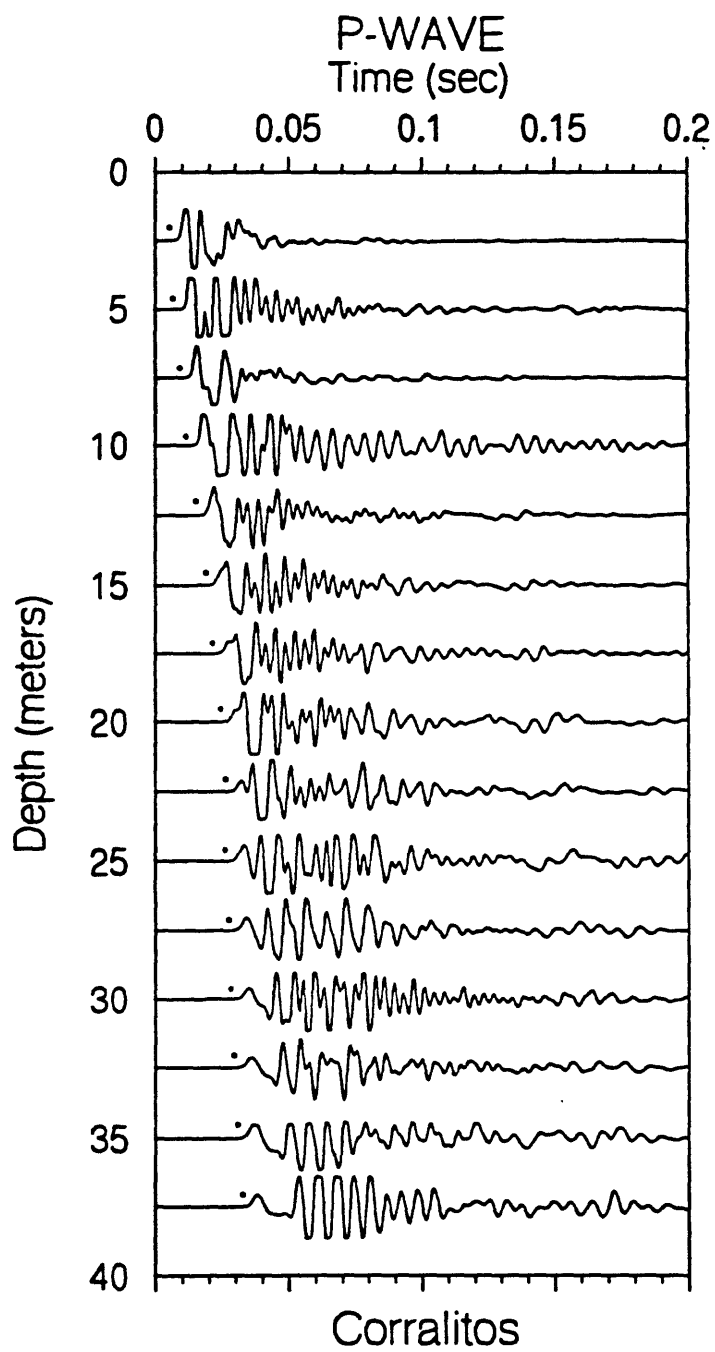


Figure 27. P-wave record section. Approximate location of the picks are shown by the dots.

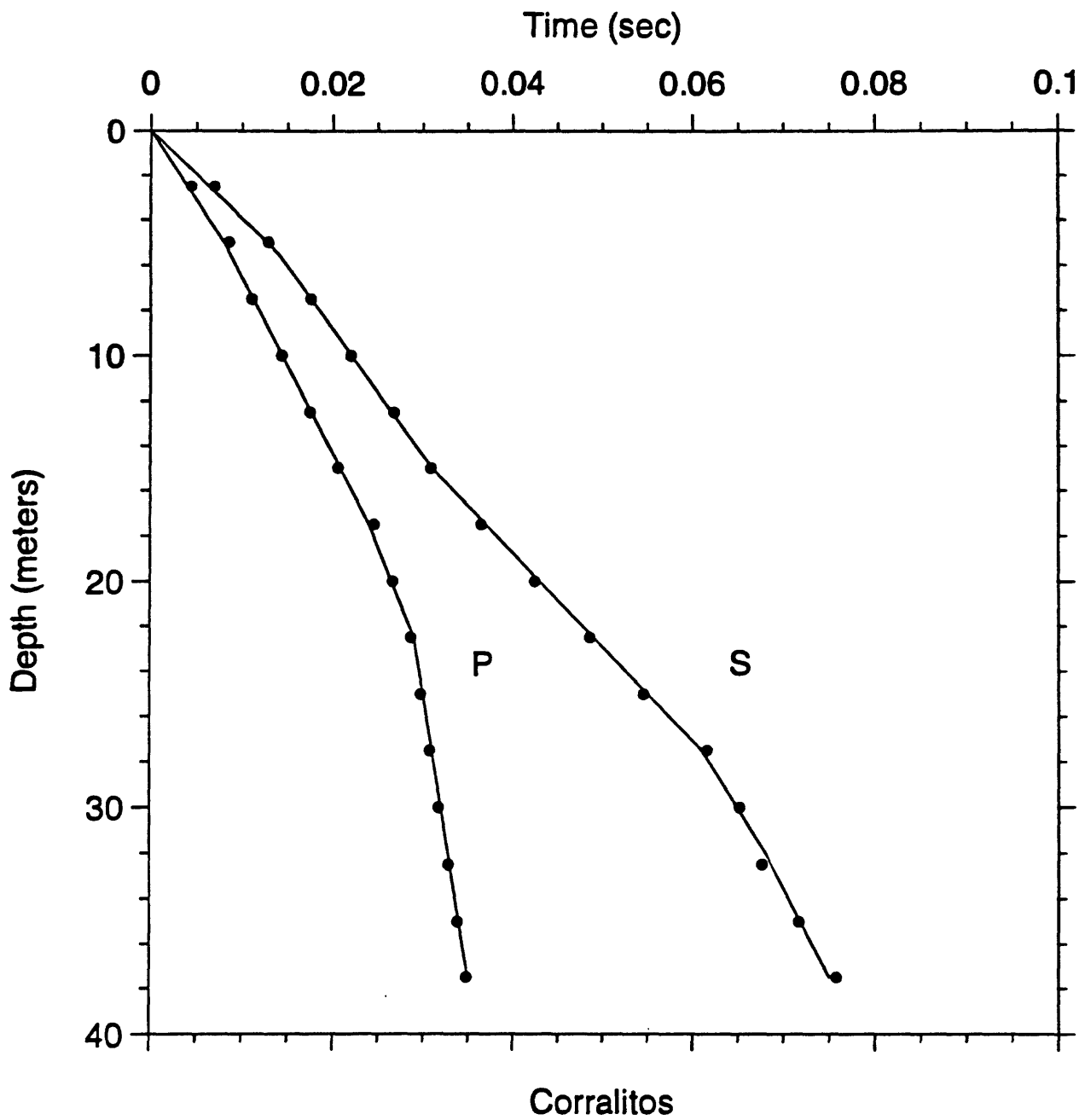


Figure 28. Time-depth graph of P-wave and S-wave picks. Line segments show the hinge-least-squares fit to the data.

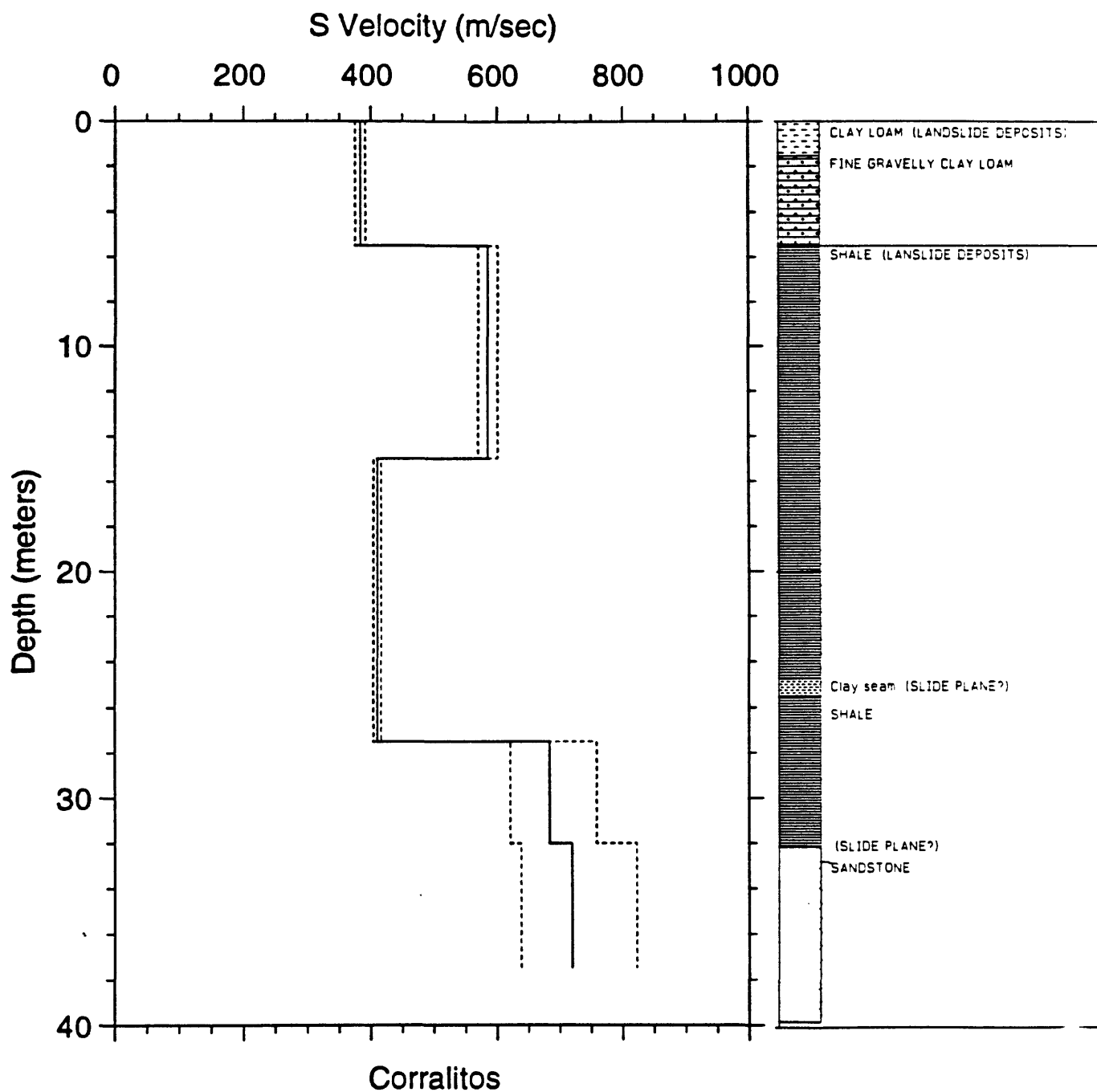


Figure 29. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

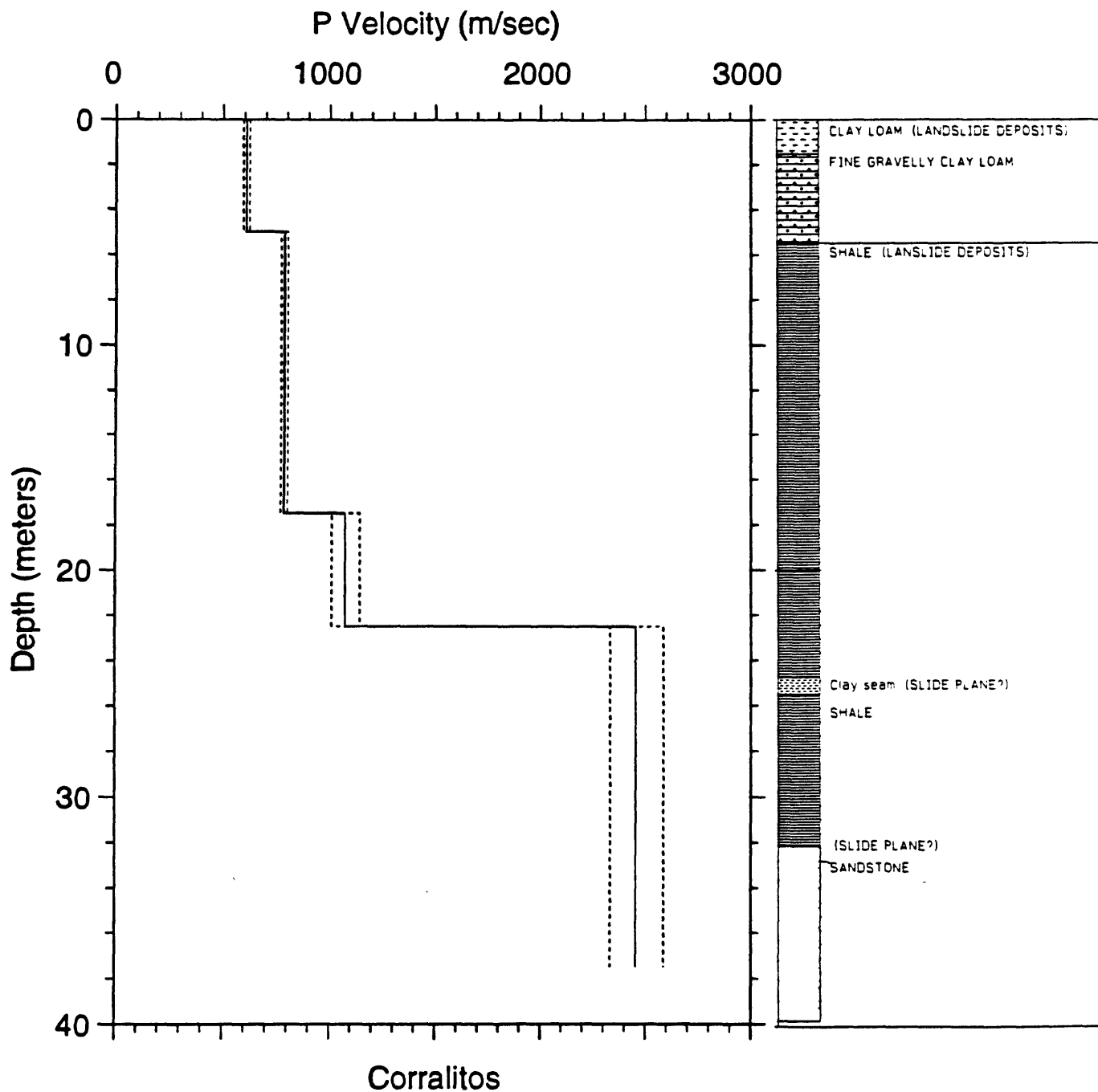


Figure 30. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 5. S-wave arrival times and velocity summaries for Corralitos.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tth(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0070	1	.5	.0	.0	.000	383	375	391	1256	1230	1282
5.0	16.4	.0129	1	-.2	5.5	18.0	.014	383	375	391	1256	1230	1282
7.5	24.6	.0176	1	-.2	15.0	49.2	.031	585	570	601	1919	1869	1972
10.0	32.8	.0220	1	-.1	27.5	90.2	.061	410	404	416	1345	1326	1364
12.5	41.0	.0268	1	.5	32.0	105.0	.068	683	621	758	2240	2037	2488
15.0	49.2	.0309	1	.3	37.5	123.0	.075	719	638	822	2358	2094	2698
17.5	57.4	.0365	1	-.2									
20.0	65.6	.0425	1	-.3									
22.5	73.8	.0486	1	-.3									
25.0	82.0	.0546	1	-.4									
27.5	90.2	.0616	1	.5									
30.0	98.4	.0652	1	.4									
32.5	106.6	.0677	2	-.3									
35.0	114.8	.0717	1	-.2									
37.5	123.0	.0758	2	.2									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

tth(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

TABLE 6. P-wave arrival times and velocity summaries for Corralitos.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tth(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0045	1	.4	.0	.0	.000	607	593	622	1991	1945	2039
5.0	16.4	.0086	1	.4	5.0	16.4	.008	607	593	622	1991	1945	2039
7.5	24.6	.0111	1	.3	17.5	57.4	.024	787	771	803	2580	2530	2633
10.0	32.8	.0144	1	.2	22.5	73.8	.029	1074	1012	1143	3523	3321	3751
12.5	41.0	.0175	1	.3	37.5	123.0	.035	2453	2333	2586	8047	7654	8483
15.0	49.2	.0206	1	.4									
17.5	57.4	.0246	1	.5									
20.0	65.6	.0267	1	.2									
22.5	73.8	.0287	1	.1									
25.0	82.0	.0298	1	.0									
27.5	90.2	.0308	1	.0									
30.0	98.4	.0318	1	.0									
32.5	106.6	.0329	1	.0									
35.0	114.8	.0339	1	.0									
37.5	123.0	.0349	1	.0									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

tth(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

GILROY HOT SPRINGS QUADRANGLE
CALIFORNIA—SANTA CLARA CO.
7.5 MINUTE SERIES (TOPOGRAPHIC)

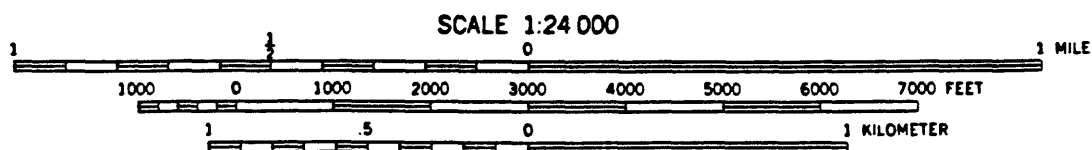
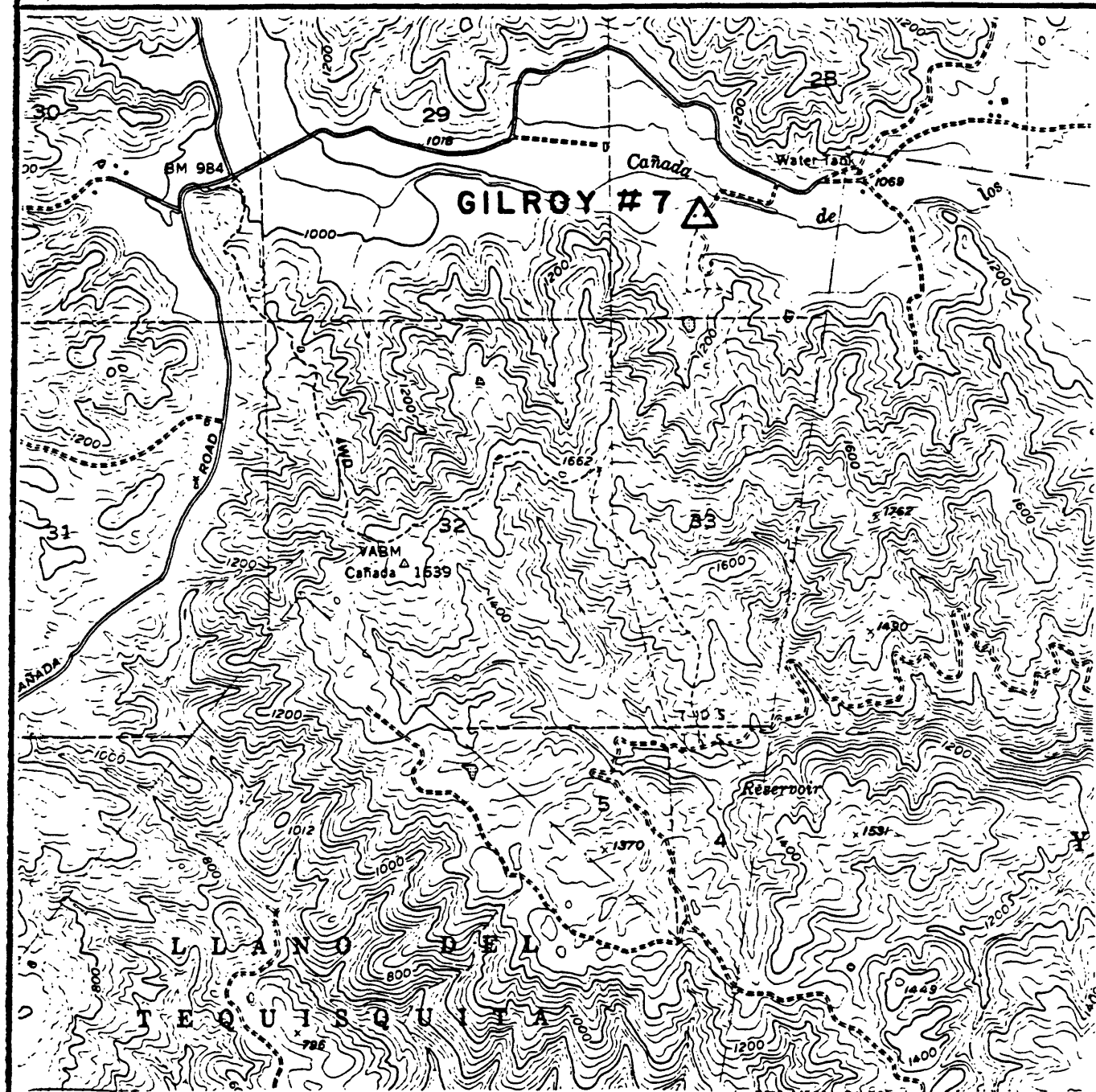


Figure 31. Location map for Gilroy #7 borehole. The strong-motion accelerograph is located within 10 meters of the borehole.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
> 100	> 36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

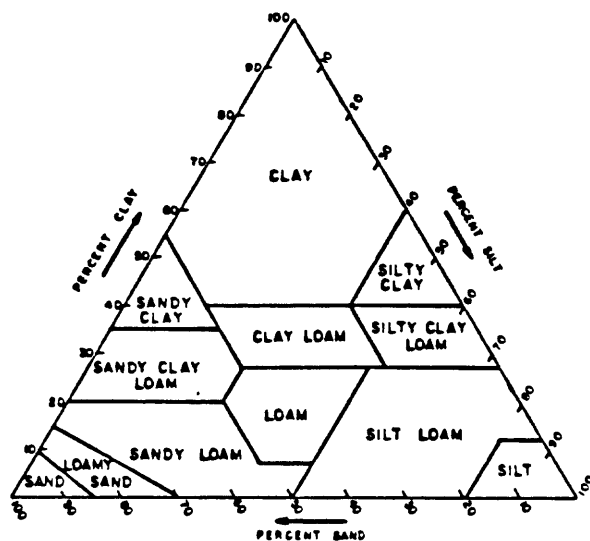
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
> 50	v. dense	15-30	v. stiff
		> 30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration (1 + 3/8 in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 32. Explanation of geologic log.

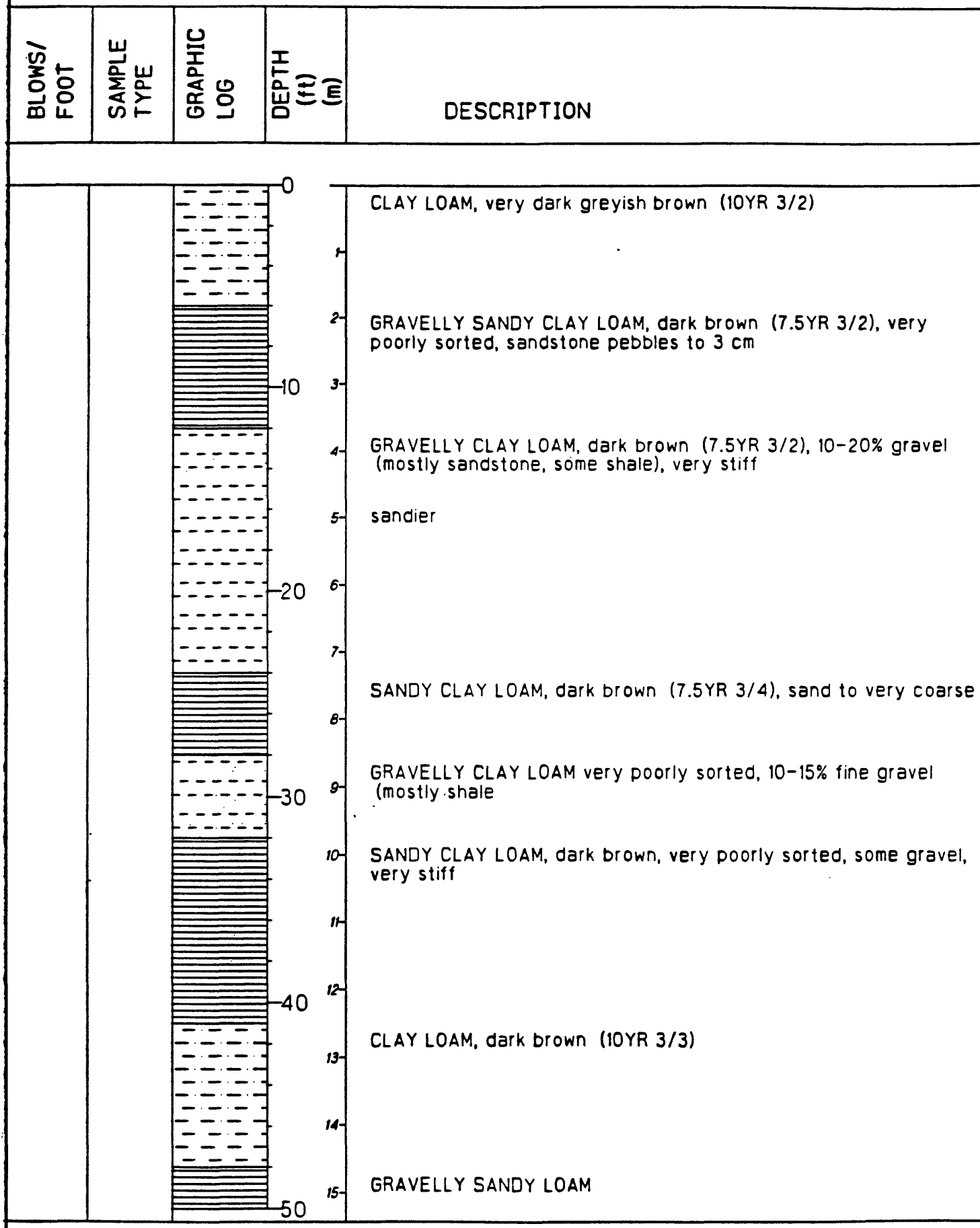


Figure 33. Geologic log of Gilroy #7 borehole.

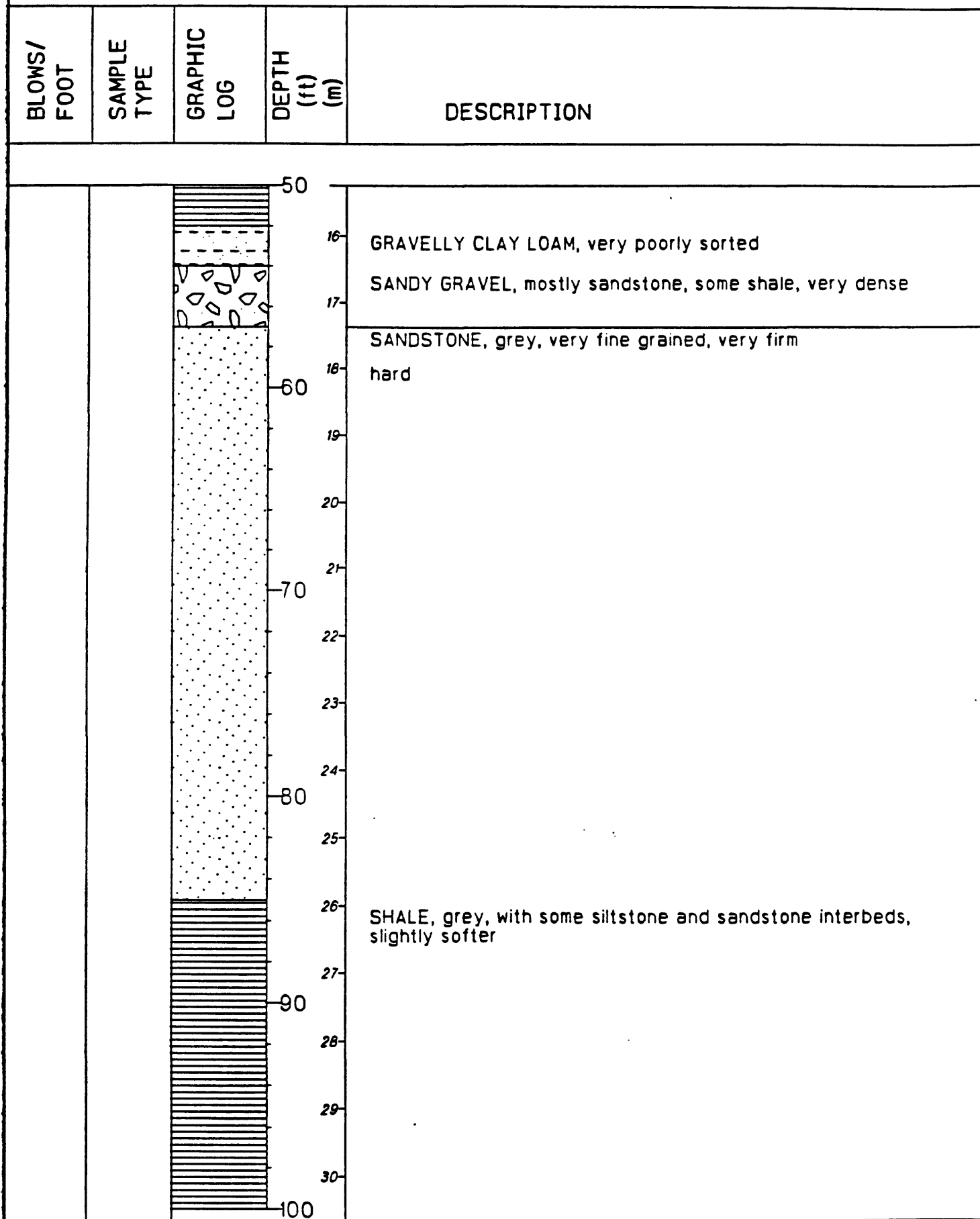
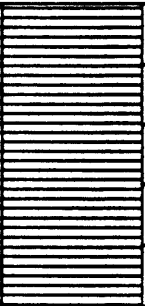


Figure 33 (Continued).

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			100 31 32 33 110 34 35 36 120 37 38 39 130 40 41 42 140 43 44 45 150	

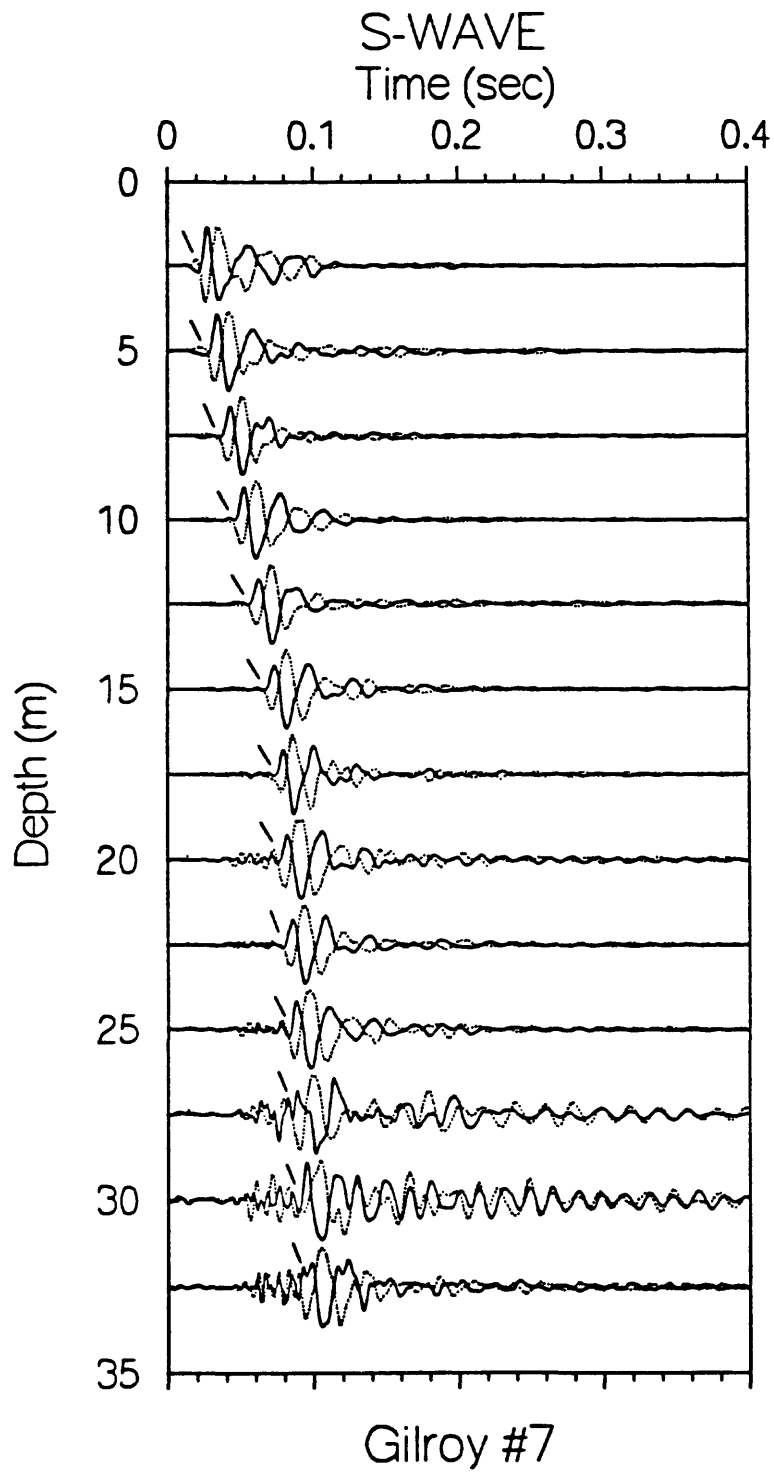


Figure 34. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

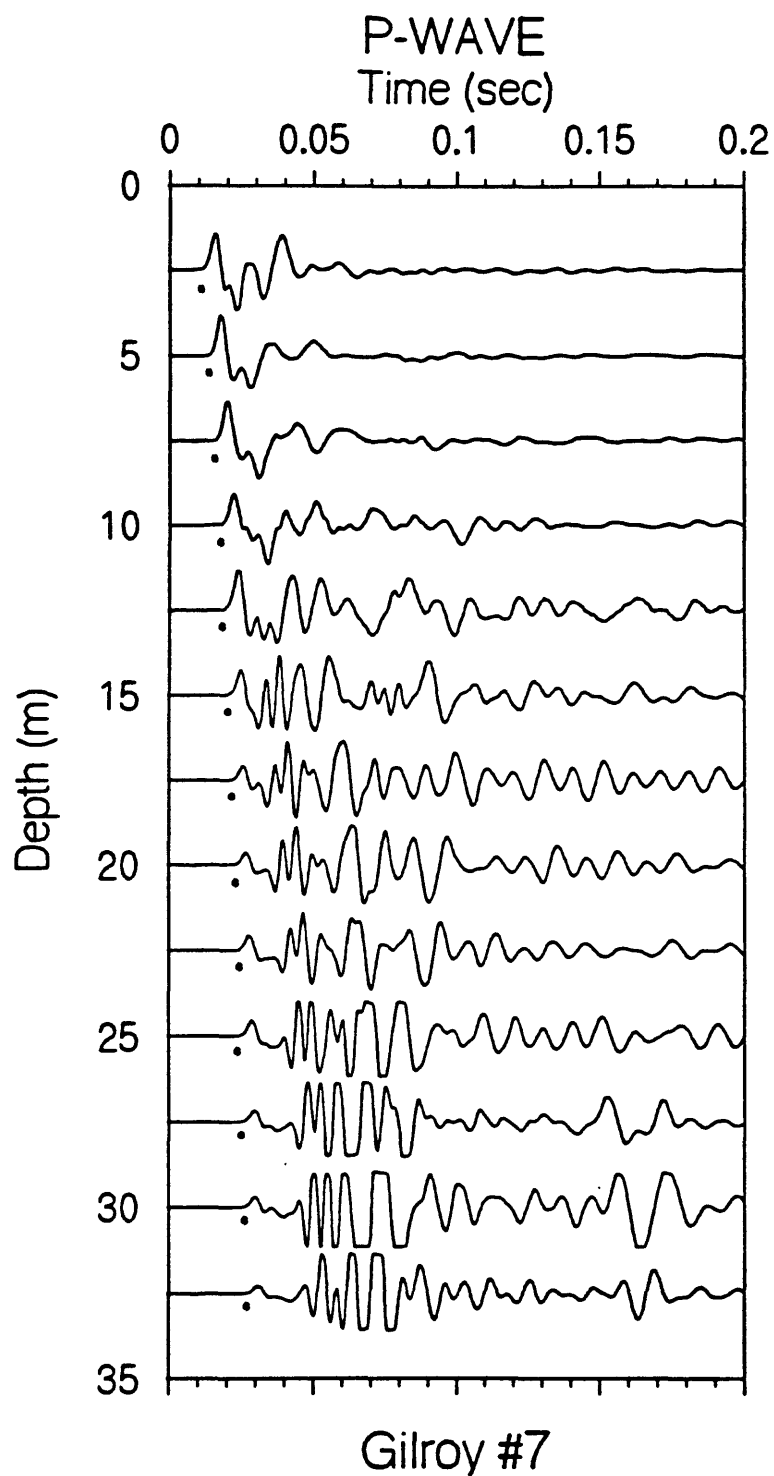


Figure 35. Vertical-component record section. P-wave arrivals are shown by the solid circles.

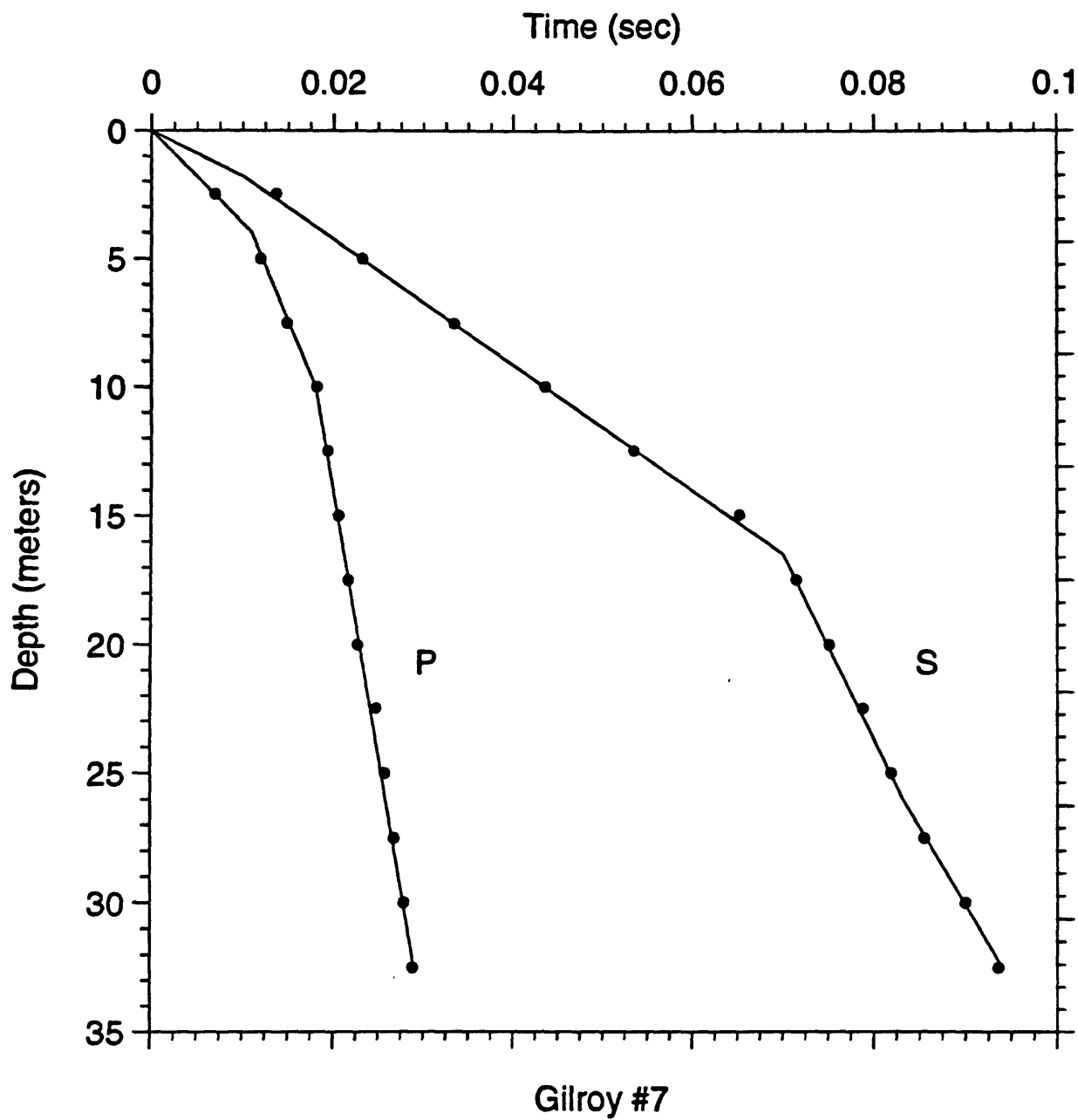


Figure 36. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

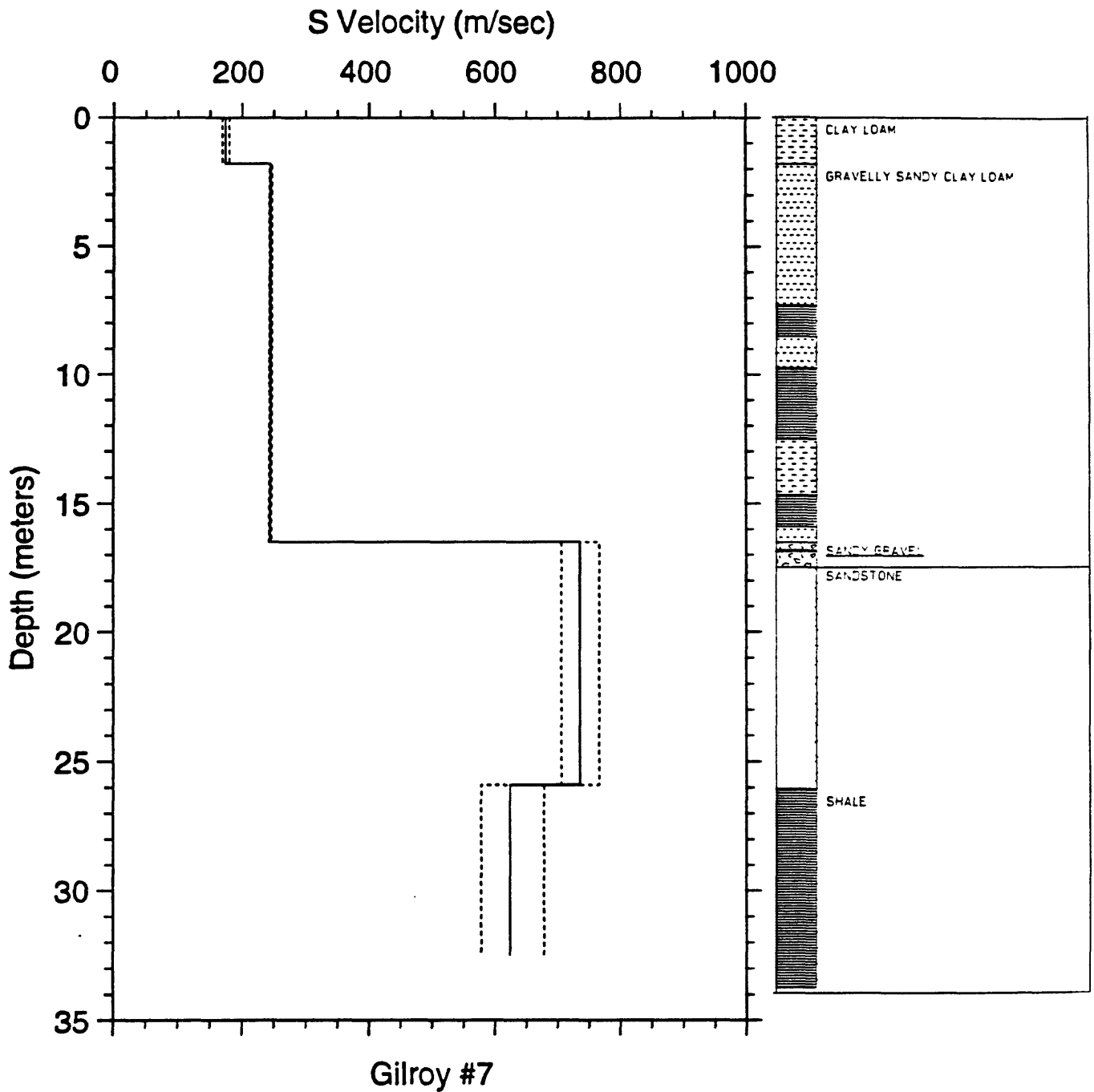


Figure 37. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

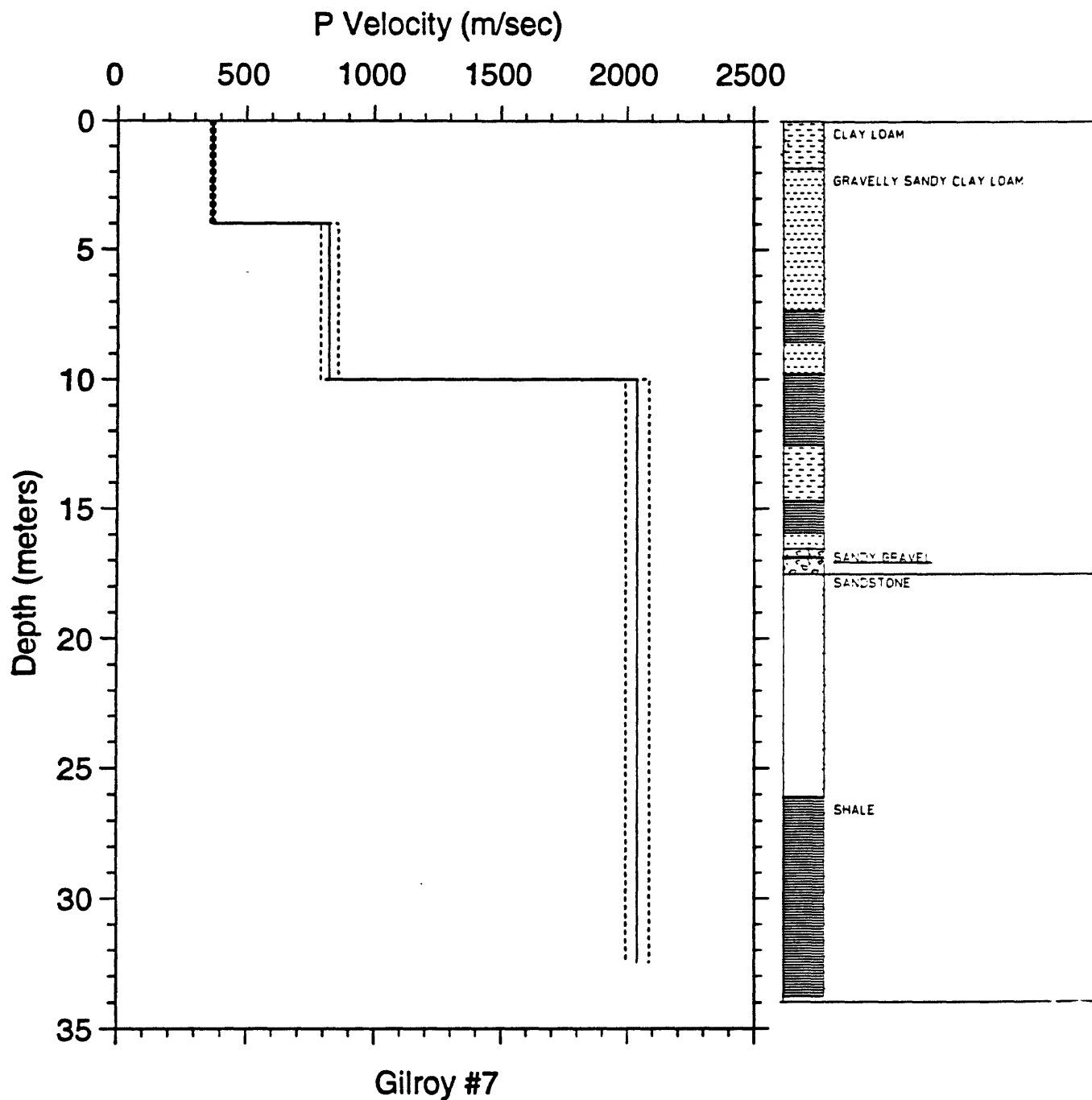


Figure 38. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 7. S-wave arrival times and velocity summaries for Gilroy #7 (USGS).

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0137	1	.5	.0	.0	.000	174	169	180	571	553	590
5.0	16.4	.0232	1	-.2	1.8	5.9	.010	174	169	180	571	553	590
7.5	24.6	.0334	1	-.2	16.5	54.1	.070	245	243	247	803	796	810
10.0	32.8	.0436	1	-.2	25.9	85.0	.083	735	706	766	2410	2315	2514
12.5	41.0	.0535	1	-.6	32.5	106.6	.094	624	578	678	2049	1897	2226
15.0	49.2	.0652	1	.9									
17.5	57.4	.0715	1	-.3									
20.0	65.6	.0751	1	-.1									
22.5	73.8	.0788	1	.2									
25.0	82.0	.0819	1	-.1									
27.5	90.2	.0855	2	-.2									
30.0	98.4	.0900	2	-.2									
32.5	106.6	.0936	2	-.1									

Explanation:

d(m) = depth in meters
d(ft) = depth in feet
t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
sig = sigma, standard deviation normalized to the standard deviation of best picks
rsdl/sig = least-squares residual divided by sigma
dtb(m) = depth to bottom of layer in meters
dtb(ft) = depth to bottom of layer in feet
t(b(s) = arrival time in seconds to bottom of layer
v(m/s) = velocity in meters per second
vl(m/s) = lower limit of velocity in meters per second *
vu(m/s) = upper limit of velocity in meters per second
v(ft/s) = velocity in feet per second
vl(ft/s) = lower limit of velocity in feet per second
vu(ft/s) = upper limit of velocity in feet per second
* see text for explanation of velocity limits

TABLE 8. P-wave arrival times and velocity summaries for Gilroy #7 (USGS).

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tbt(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0070	1	.2	.0	.0	.000	369	361	377	1210	1184	1237
5.0	16.4	.0120	1	-.1	4.0	13.1	.011	369	361	377	1210	1184	1237
7.5	24.6	.0149	1	-.2	10.0	32.8	.018	822	789	857	2696	2589	2813
10.0	32.8	.0182	1	.1	32.5	106.6	.029	2038	1993	2086	6687	6538	6844
12.5	41.0	.0194	1	.0									
15.0	49.2	.0206	1	.0									
17.5	57.4	.0217	1	-.1									
20.0	65.6	.0227	1	-.4									
22.5	73.8	.0248	1	.5									
25.0	82.0	.0258	1	.3									
27.5	90.2	.0268	1	.1									
30.0	98.4	.0279	1	-.1									
32.5	106.6	.0289	1	-.3									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

tbt(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

OAKLAND WEST QUADRANGLE
CALIFORNIA
7.5 MINUTE SERIES (TOPOGRAPHIC)

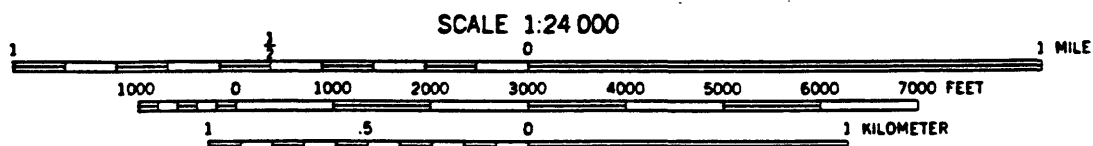


Figure 39. Site location map for Oakland 2-Story (Snow Park) and Emeryville (not in this report). The strong-motion accelerograph is located approximately 150 to 200 meters from the borehole.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

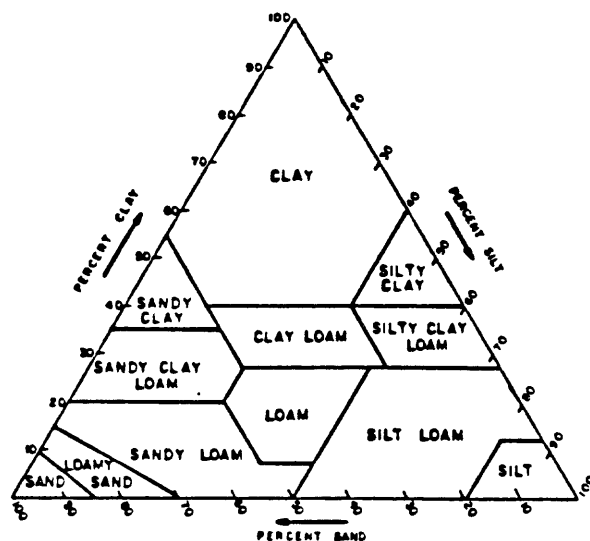
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 40. Explanation of geologic logs.

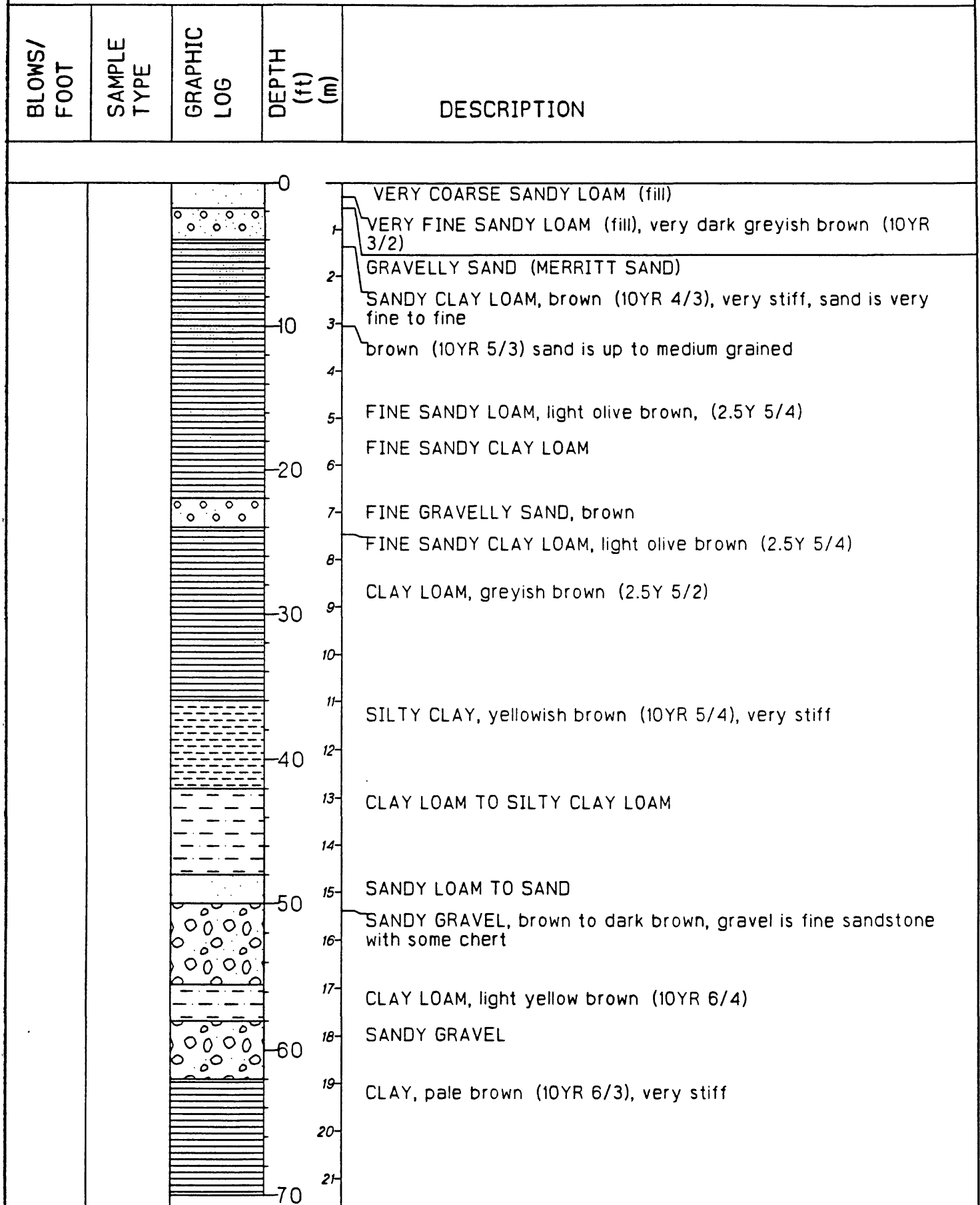


Figure 41. Geologic log for Oakland 2-Story (Snow Park).

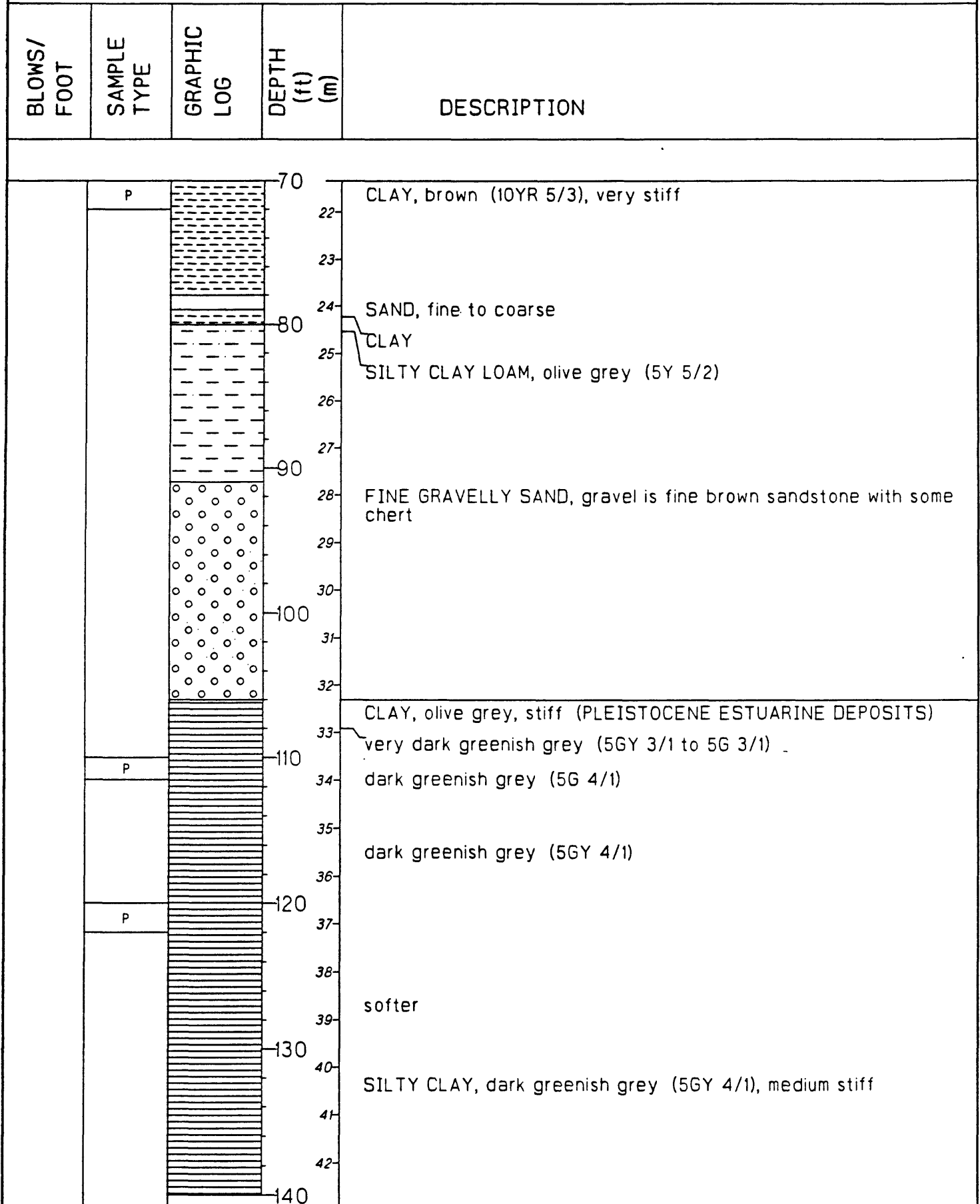


Figure 41. (Continued).

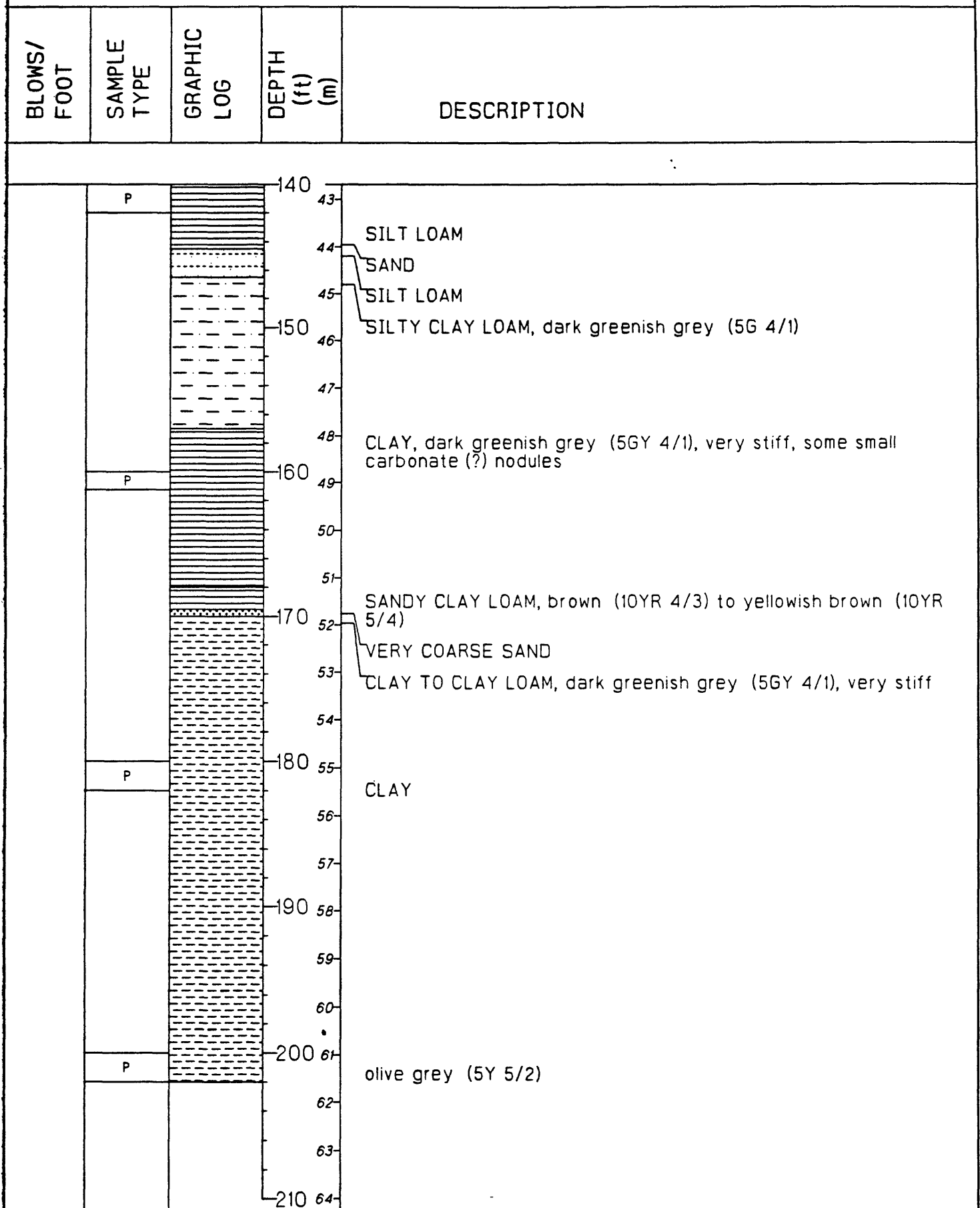


Figure 41. (Continued).

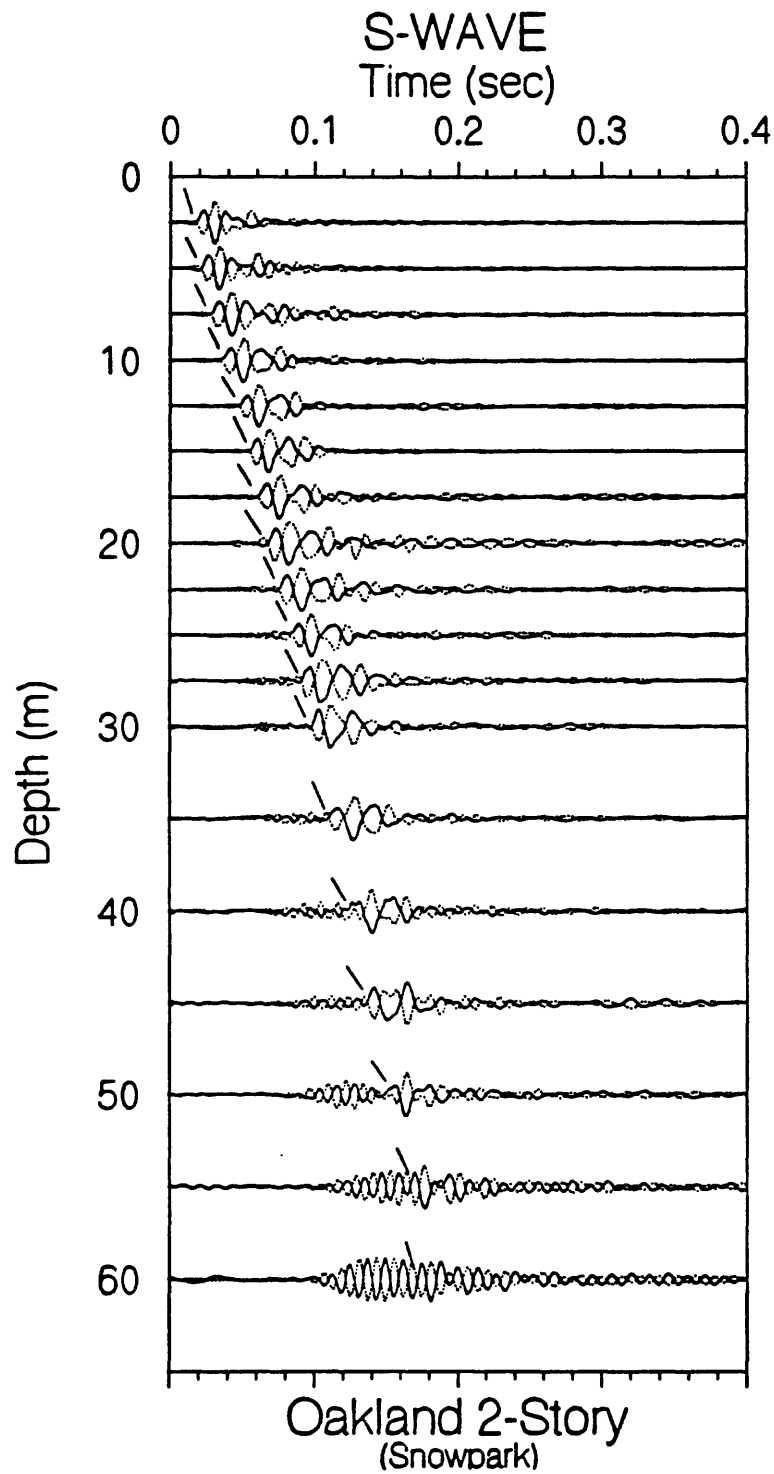


Figure 42. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

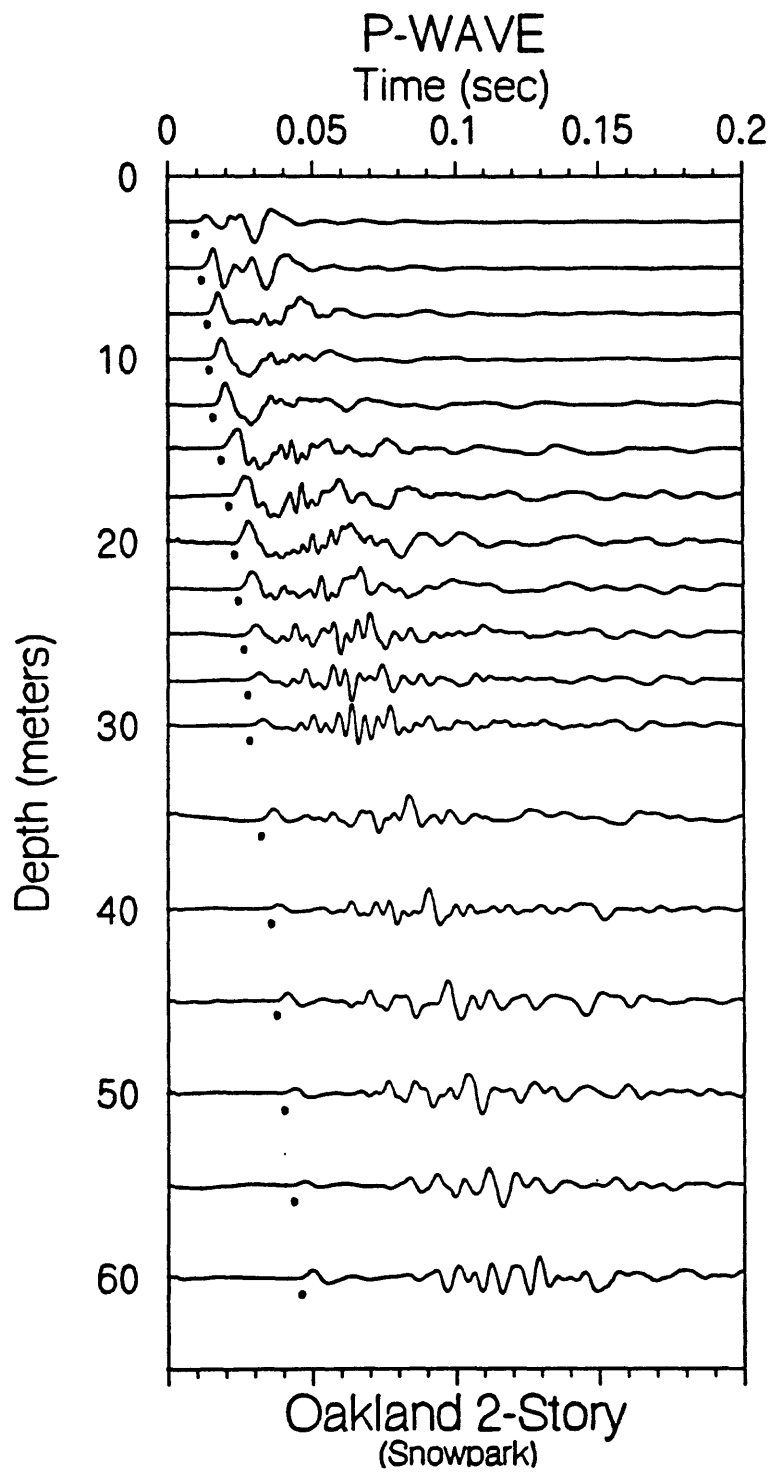


Figure 43. Vertical-component record section. P-wave arrivals are shown by the solid circles.

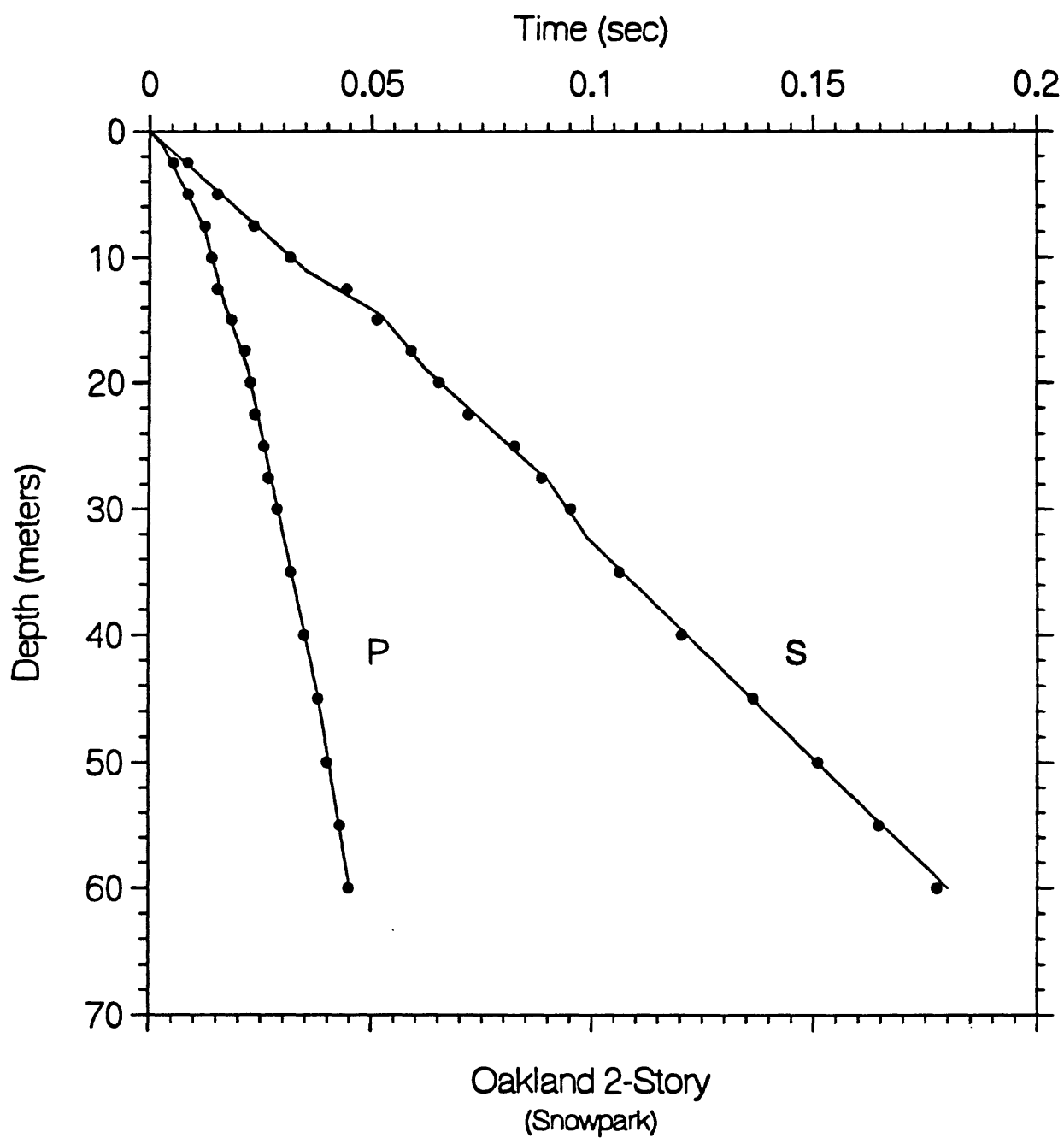


Figure 44. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

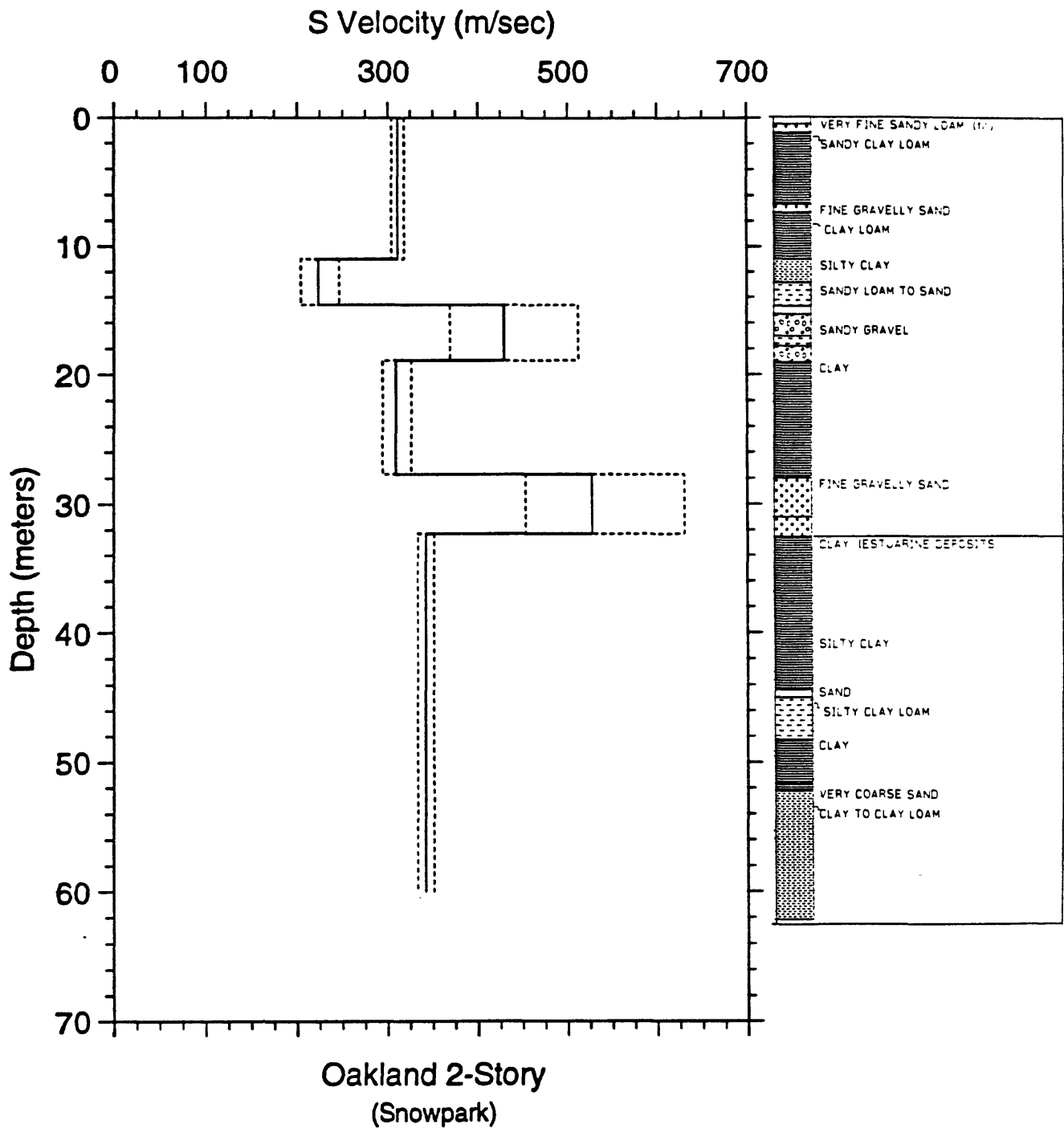


Figure 45. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

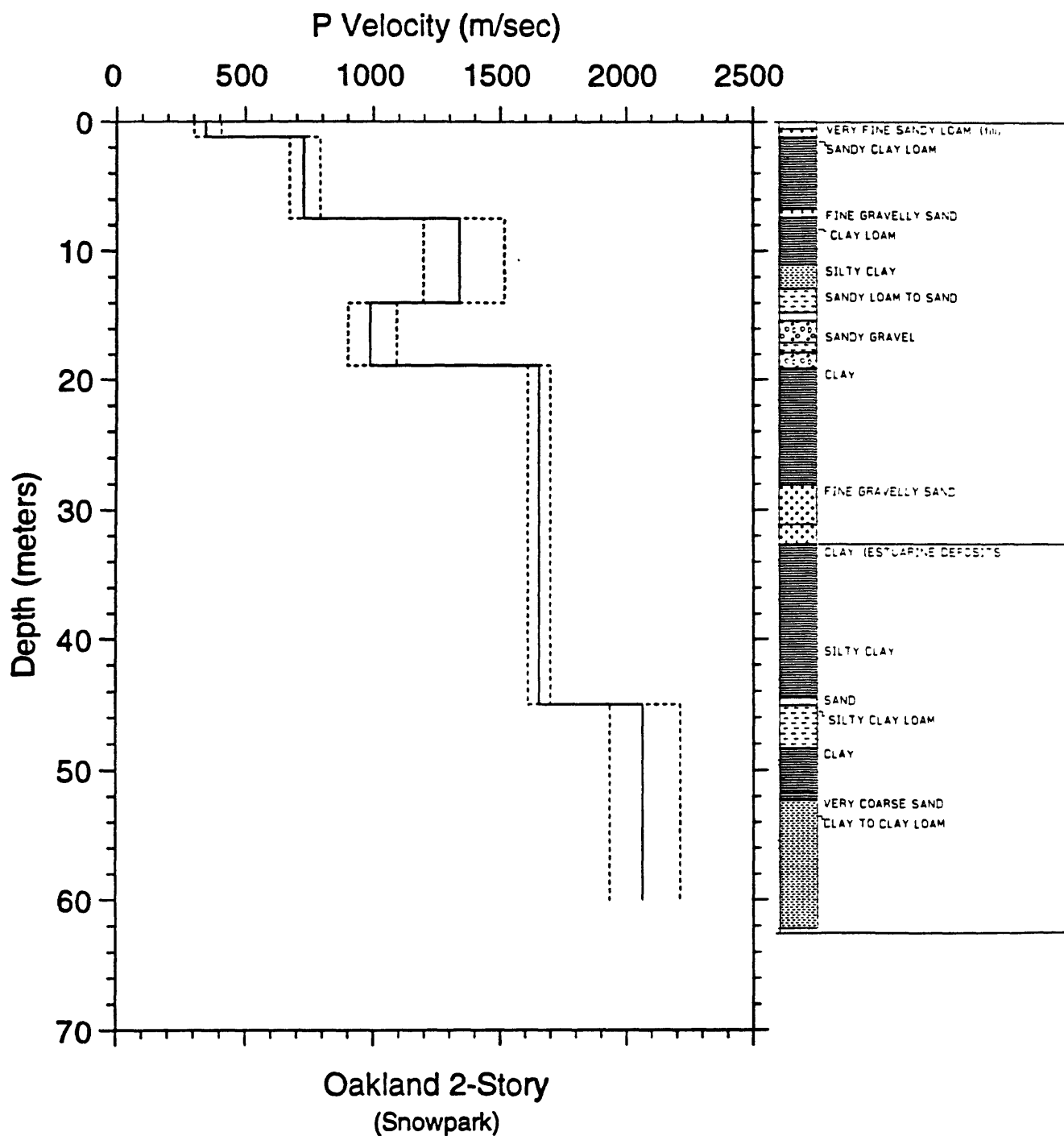


Figure 46. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 9. S-wave arrival times and velocity summaries for Oakland 2-Story (Snow Park).

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b/s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0085	1	.5	.0	.0	.000	311	304	318	1020	997	1045
5.0	16.4	.0152	1	-.9	11.0	36.1	.035	311	304	318	1020	997	1045
7.5	24.6	.0234	1	-.7	14.6	47.9	.052	223	204	246	732	670	807
10.0	32.8	.0316	1	-.6	18.9	62.0	.062	429	369	512	1407	1210	1680
12.5	41.0	.0443	1	2.2	27.7	90.9	.090	309	294	326	1014	963	1070
15.0	49.2	.0512	1	-1.2	32.3	106.0	.099	527	453	630	1730	1488	2068
17.5	57.4	.0589	1	.6	60.0	196.9	.180	342	333	351	1122	1094	1152
20.0	65.6	.0652	1	.1									
22.5	73.8	.0719	1	-1.3									
25.0	82.0	.0825	1	1.2									
27.5	90.2	.0886	1	-.8									
30.0	98.4	.0952	1	.8									
35.0	114.8	.1063	1	-.3									
40.0	131.2	.1204	1	-.9									
45.0	147.6	.1365	1	.6									
50.0	164.0	.1510	1	-.5									
55.0	180.4	.1646	2	-.3									
60.0	196.9	.1776	3	-.7									

Explanation:

d(m) = depth in meters
d(ft) = depth in feet
t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
sig = sigma, standard deviation of best picks
rsdl/sig = least-squares residual divided by sigma
dtb(m) = depth to bottom of layer in meters
dtb(ft) = depth to bottom of layer in feet
t(b/s) = arrival time in seconds to bottom of layer
v(m/s) = velocity in meters per second
vl(m/s) = lower limit of velocity in meters per second *
vu(m/s) = upper limit of velocity in meters per second
v(ft/s) = velocity in feet per second
vl(ft/s) = lower limit of velocity in feet per second
vu(ft/s) = upper limit of velocity in feet per second
* see text for explanation of velocity limits

TABLE 10. P-wave arrival times and velocity summaries for Oakland 2-Story (Snow Park).

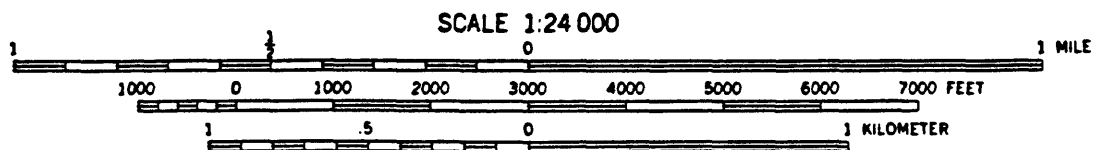
d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b/s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0053	1	.0	.0	.0	.000	346	302	406	1137	991	1333
5.0	16.4	.0086	1	-.1	1.2	3.9	.003	346	302	406	1137	991	1333
7.5	24.6	.0124	1	-.3	7.5	24.6	.012	727	672	791	2384	2204	2596
10.0	32.8	.0139	1	-.1	14.0	45.9	.017	1338	1197	1516	4388	3926	4973
12.5	41.0	.0152	1	-.7	18.9	62.0	.022	986	900	1091	3236	2954	3579
15.0	49.2	.0184	1	-.4	45.0	147.6	.038	1654	1610	1699	5425	5284	5575
17.5	57.4	.0214	1	-.9	60.0	196.9	.045	2063	1933	2212	6769	6343	7256
20.0	65.6	.0226	1	.0									
22.5	73.8	.0236	1	-.5									
25.0	82.0	.0257	1	-.5									
27.5	90.2	.0267	1	-.5									
30.0	98.4	.0287	1	.0									
35.0	114.8	.0318	1	.1									
40.0	131.2	.0348	1	.1									
45.0	147.6	.0379	1	-.2									
50.0	164.0	.0399	1	-.3									
55.0	180.4	.0429	1	-.3									
60.0	196.9	.0449	1	-.1									

Explanation:

- d(m) = depth in meters
- d(ft) = depth in feet
- t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
- sig = sigma, standard deviation normalized to the standard deviation of best picks
- rsdl/sig = least-squares residual divided by sigma
- dtb(m) = depth to bottom of layer in meters
- dtb(ft) = depth to bottom of layer in feet
- t(b/s) = arrival time in seconds to bottom of layer
- v(m/s) = velocity in meters per second
- vl(m/s) = lower limit of velocity in meters per second *
- vu(m/s) = upper limit of velocity in meters per second
- v(ft/s) = velocity in feet per second
- vl(ft/s) = lower limit of velocity in feet per second
- vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

**MOUNTAIN VIEW QUADRANGLE
CALIFORNIA
7.5 MINUTE SERIES (TOPOGRAPHIC)**



82

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
> 100	> 36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

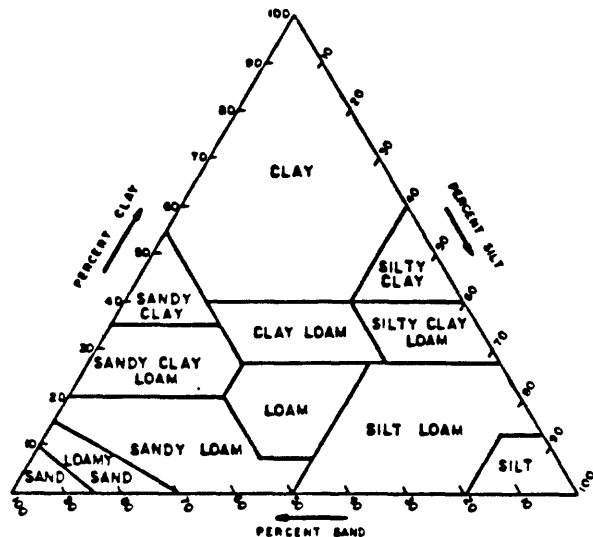
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	< 2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
> 50	v. dense	15-30	v. stiff
		> 30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 48. Explanation of geologic log.

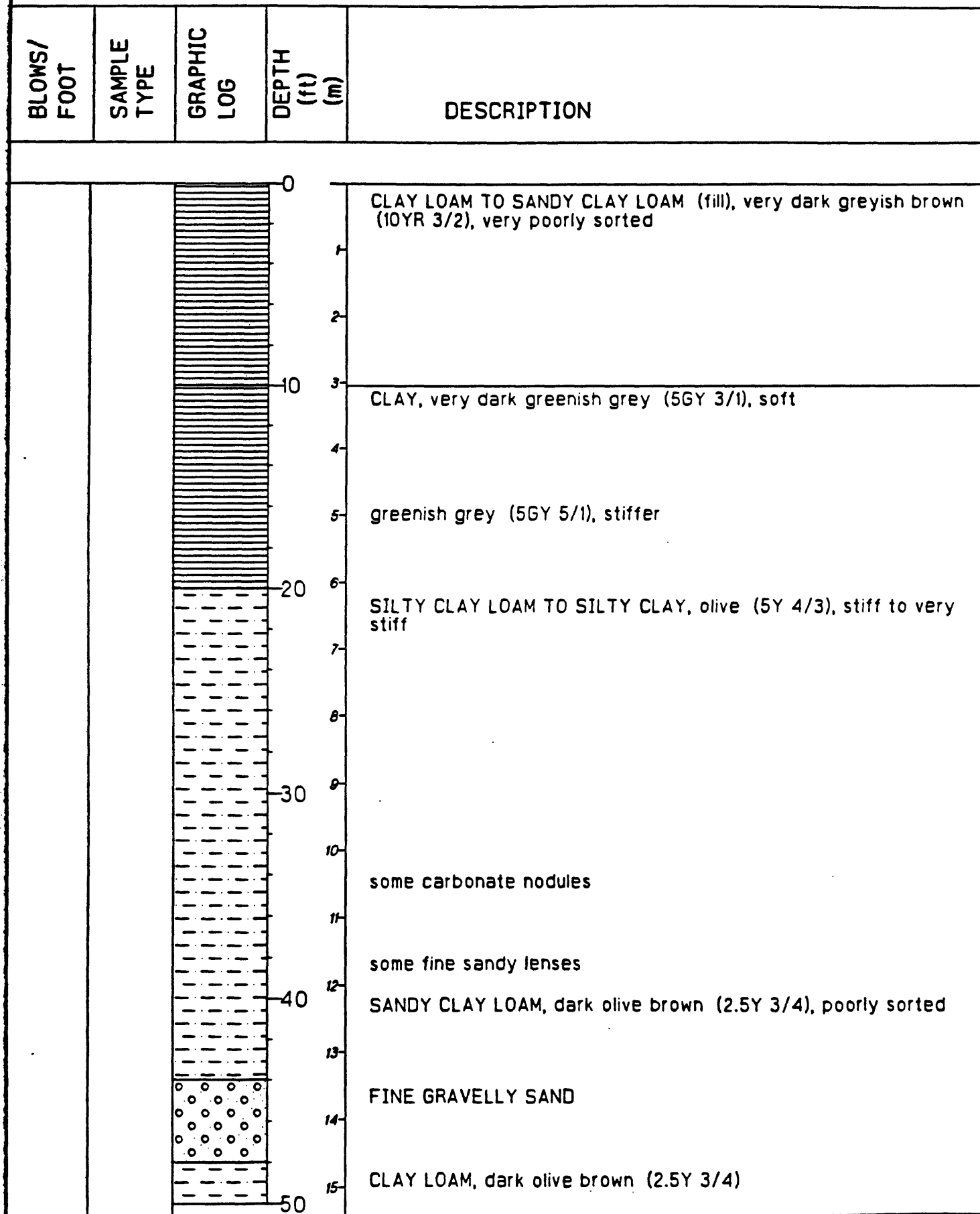


Figure 49. Geologic log for Palo Alto 2-Story.

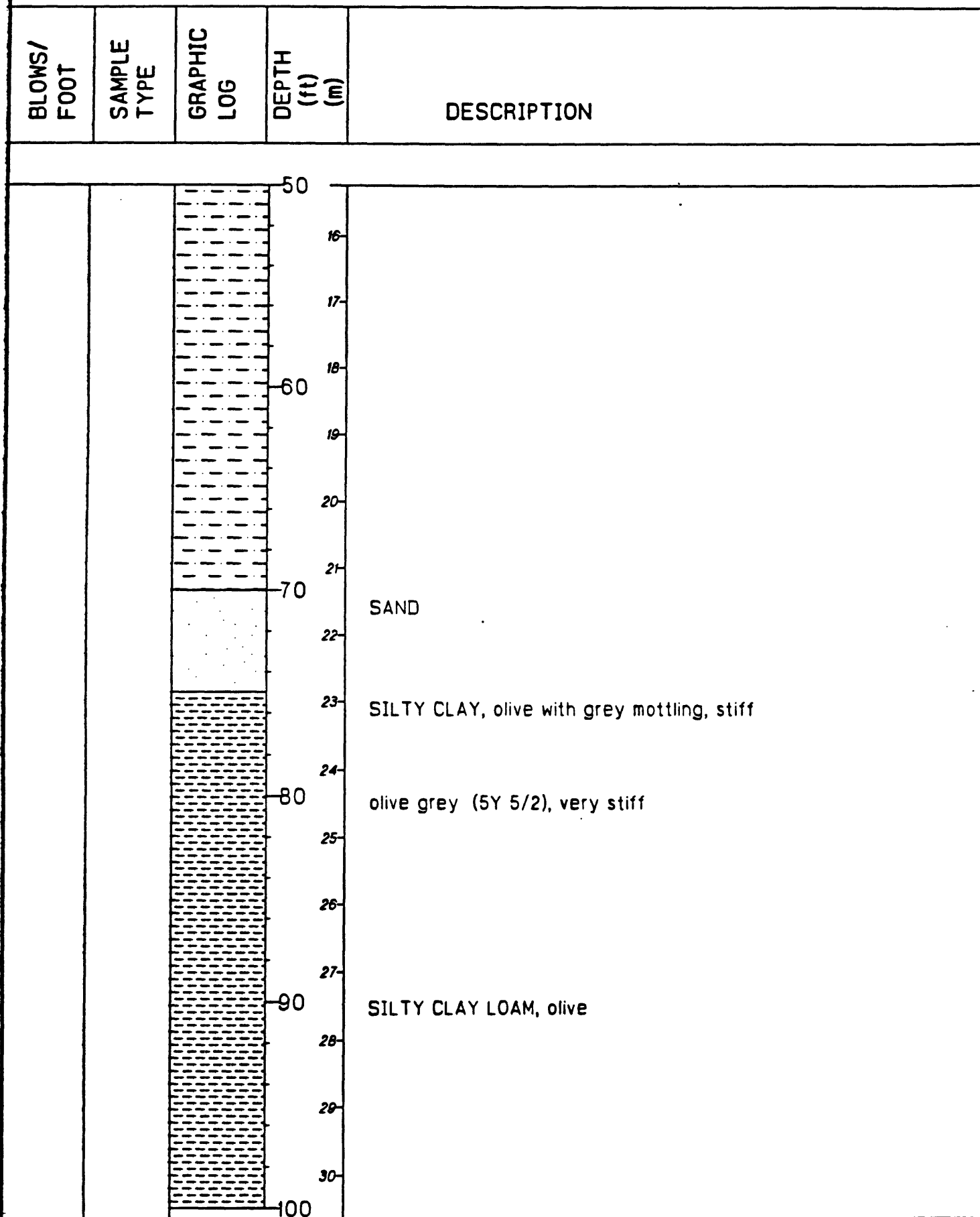


Figure 49. (Continued).

Figure 49. (Continued).

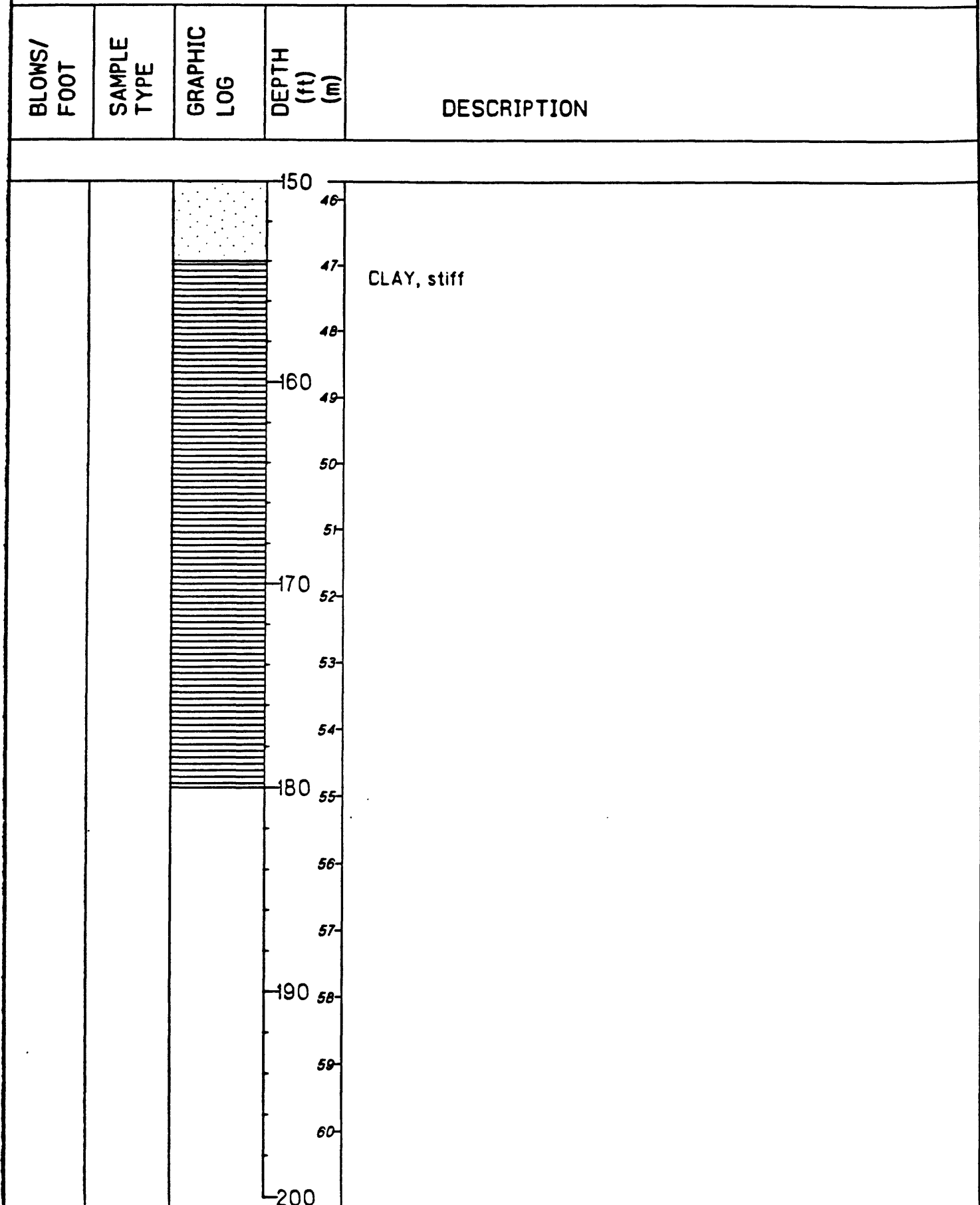


Figure 49. (Continued).

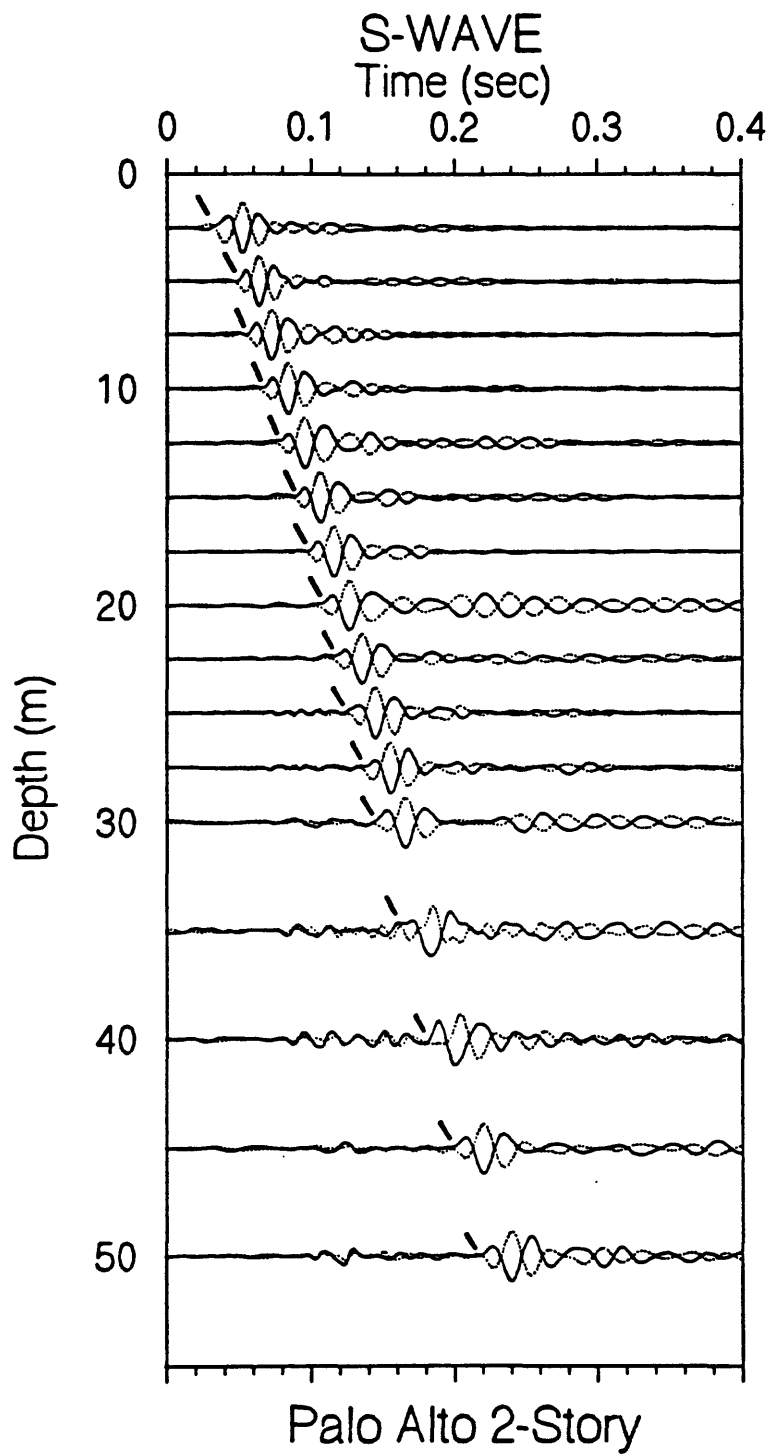


Figure 50. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

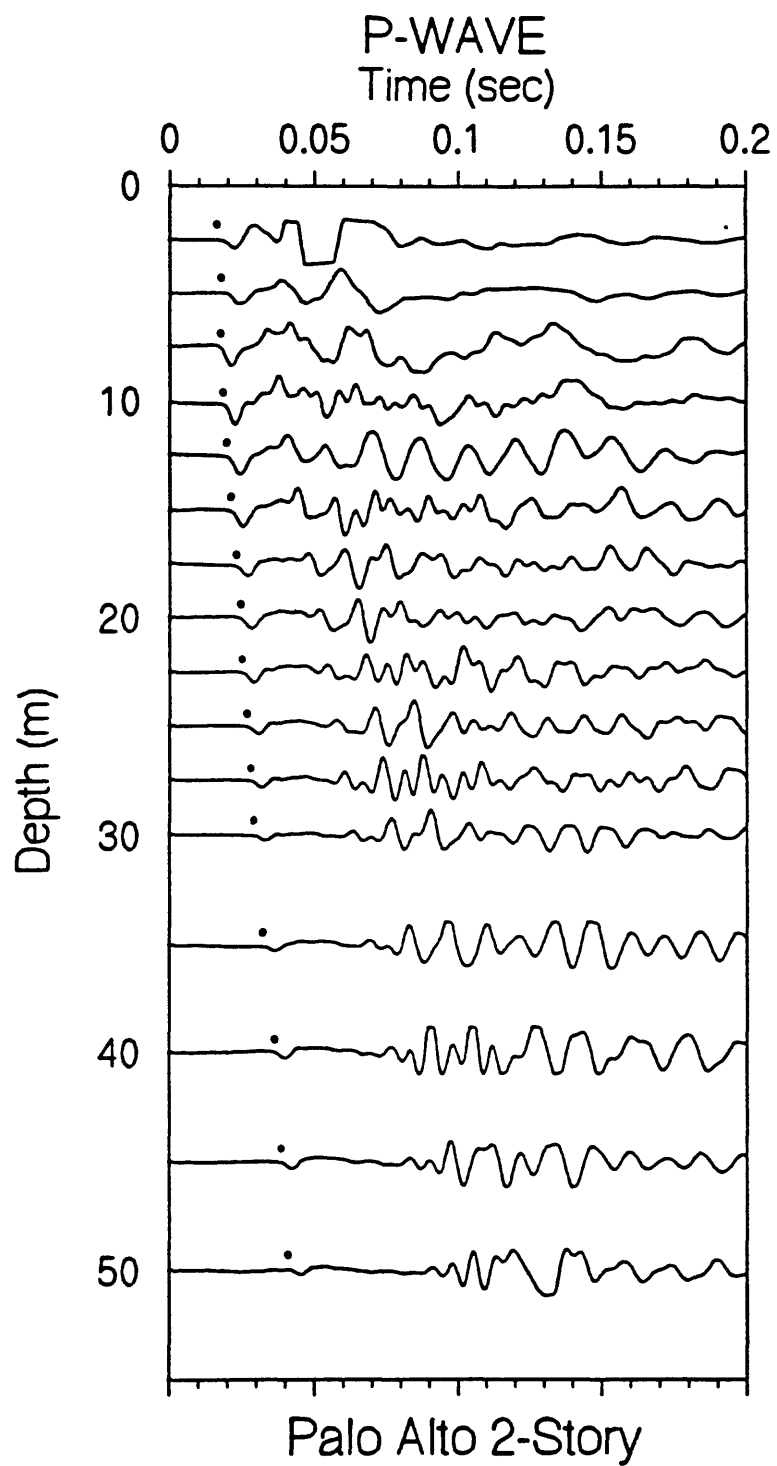


Figure 51. Vertical-component record section. P-wave arrivals are shown by the solid circles.

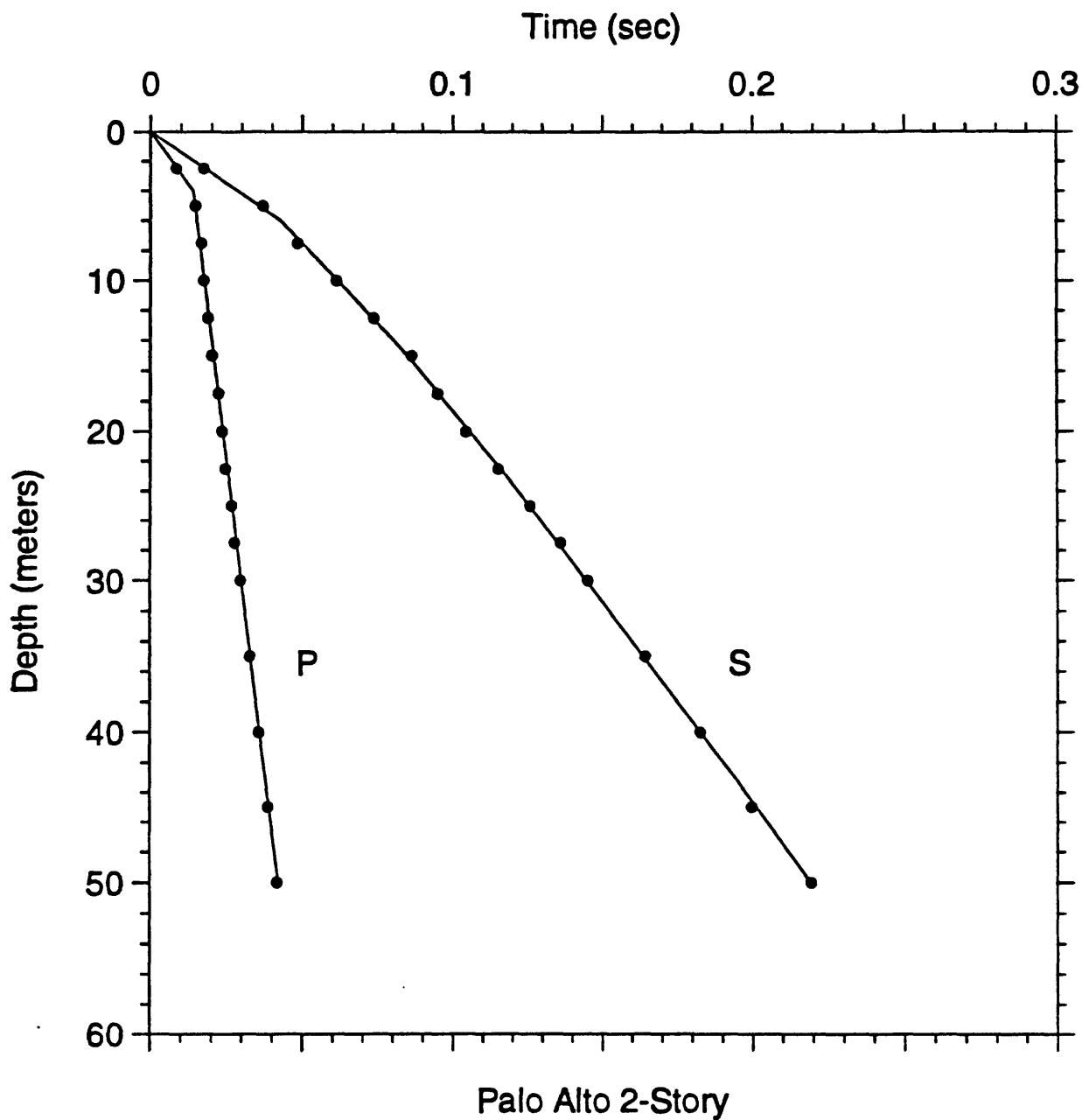


Figure 52. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

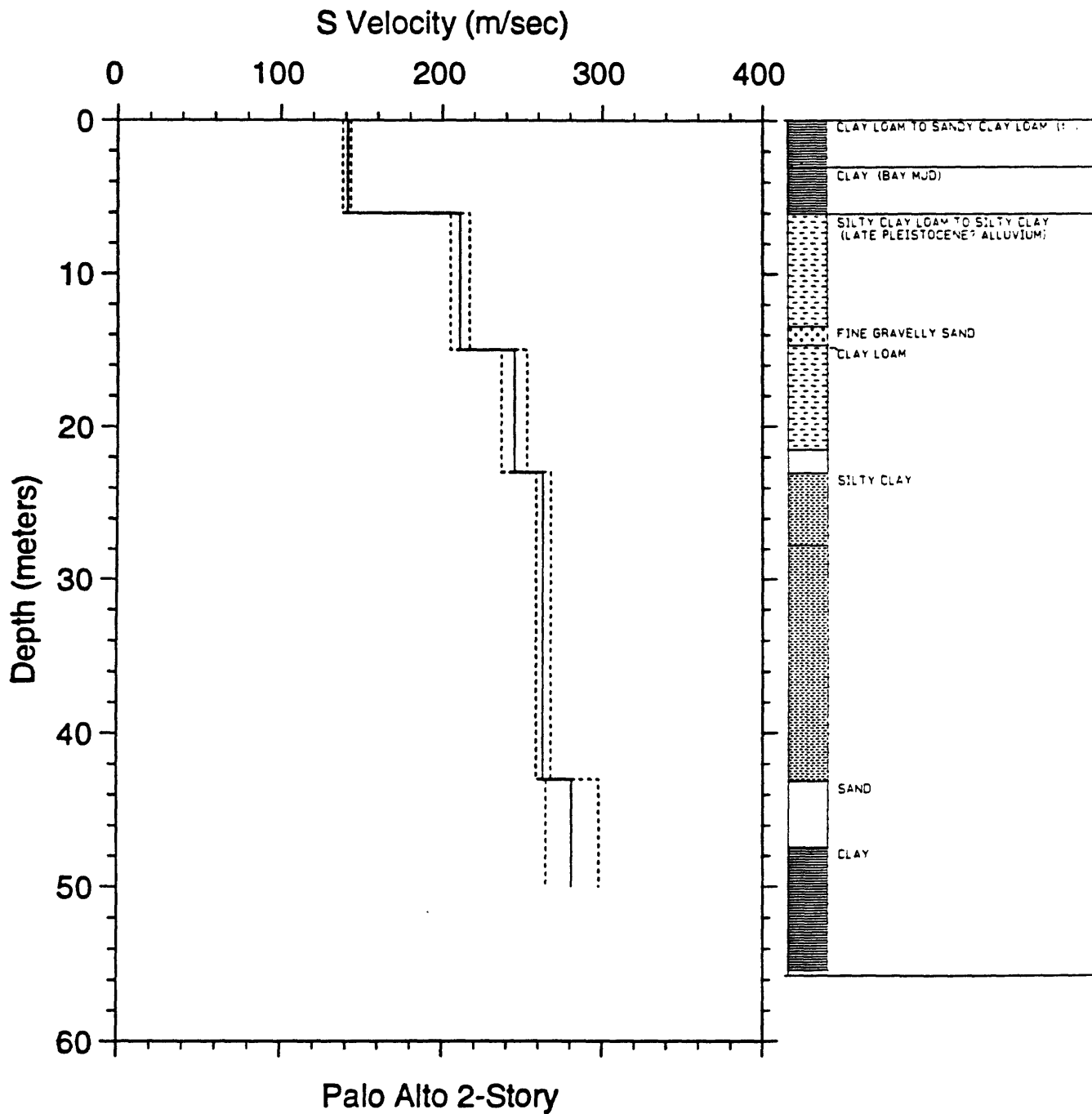


Figure 53. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

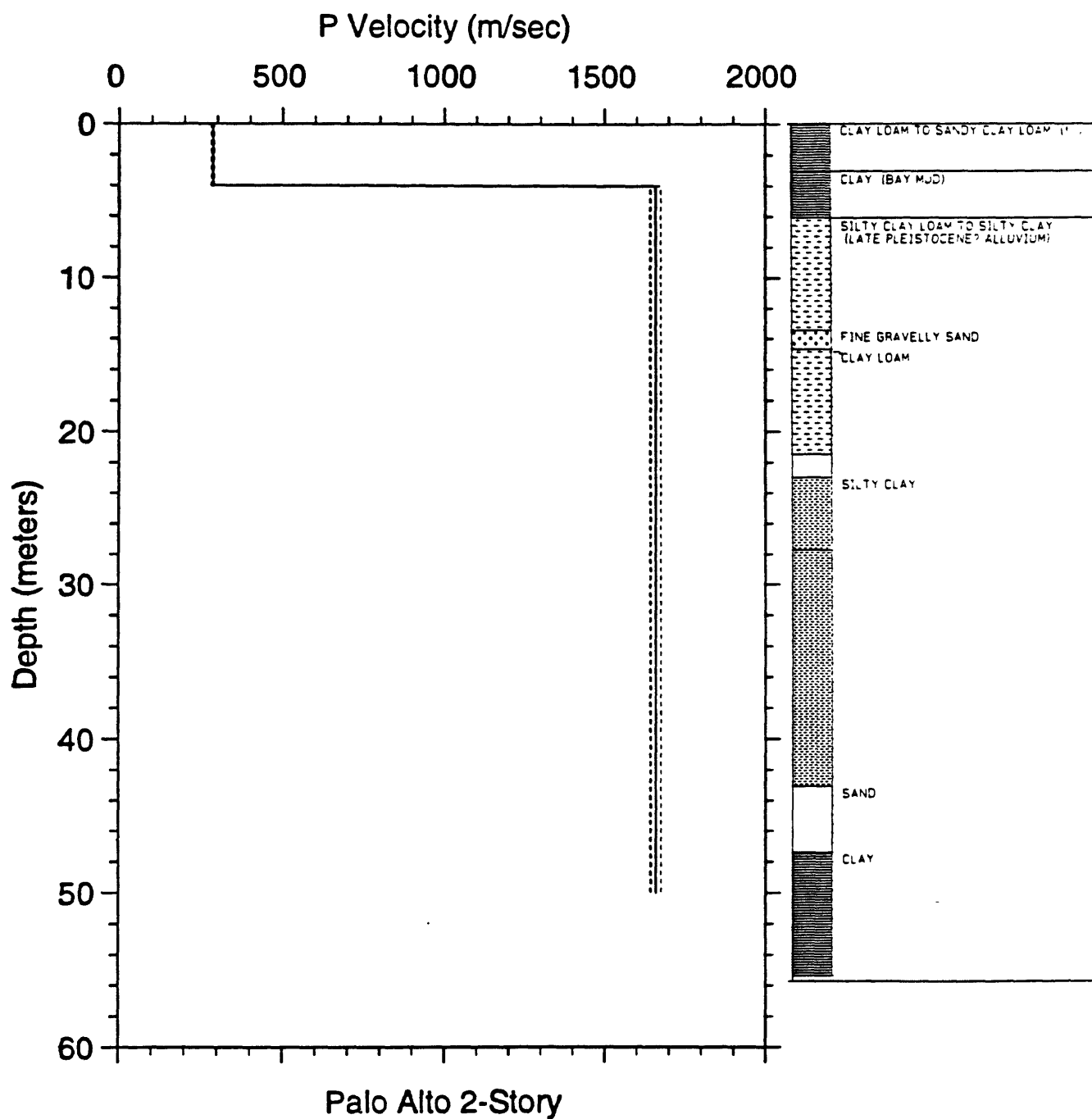


Figure 54. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 11. S-wave arrival times and velocity summaries for Palo Alto 2-Story.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	ttb(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0175	1	-.3	.0	.0	.000	141	138	143	461	453	470
5.0	16.4	.0371	1	1.5	6.0	19.7	.043	141	138	143	461	453	470
7.5	24.6	.0485	1	-1.3	15.0	49.2	.085	211	205	217	692	673	713
10.0	32.8	.0613	1	-.3	23.0	75.5	.118	245	237	253	803	778	830
12.5	41.0	.0738	1	-.3	43.0	141.1	.194	263	259	268	864	850	878
15.0	49.2	.0864	1	1.1	50.0	164.0	.219	281	265	298	920	870	977
17.5	57.4	.0950	1	-.5									
20.0	65.6	.1044	1	-1.4									
22.5	73.8	.1152	1	-.8									
25.0	82.0	.1259	1	-.3									
27.5	90.2	.1361	1	1.0									
30.0	98.4	.1452	1	-.6									
35.0	114.8	.1644	1	-.8									
40.0	131.2	.1826	1	-.0									
45.0	147.6	.1997	1	-1.4									
50.0	164.0	.2193	1	-.4									

Explanation:

d(m) = depth in meters
 d(ft) = depth in feet
 t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
 sig = sigma, standard deviation normalized to the standard deviation of best picks
 rsdl/sig = least-squares residual divided by sigma
 dtb(m) = depth to bottom of layer in meters
 dtb(ft) = depth to bottom of layer in feet
 ttb(s) = arrival time in seconds to bottom of layer
 v(m/s) = velocity in meters per second
 vl(m/s) = lower limit of velocity in meters per second *
 vu(m/s) = upper limit of velocity in meters per second
 v(ft/s) = velocity in feet per second
 vl(ft/s) = lower limit of velocity in feet per second
 vu(ft/s) = upper limit of velocity in feet per second
 * see text for explanation of velocity limits

TABLE 12. P-wave arrival times and velocity summaries for Palo Alto 2-Story.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tth(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0085	1	-.2	.0	.0	.000	286	283	289	938	928	947
5.0	16.4	.0148	1	-.2	4.0	13.1	.014	286	283	289	938	928	947
7.5	24.6	.0168	1	-.7	50.0	164.0	.042	1659	1643	1675	5443	5390	5497
10.0	32.8	.0176	1	.0									
12.5	41.0	.0190	1	-.1									
15.0	49.2	.0203	1	-.3									
17.5	57.4	.0224	1	-.3									
20.0	65.6	.0235	1	-.1									
22.5	73.8	.0246	1	-.5									
25.0	82.0	.0267	1	.0									
27.5	90.2	.0277	1	-.5									
30.0	98.4	.0297	1	.0									
35.0	114.8	.0328	1	-.1									
40.0	131.2	.0358	1	-.1									
45.0	147.6	.0388	1	-.1									
50.0	164.0	.0419	1	-.2									

Explanation:

- d(m) = depth in meters
- d(ft) = depth in feet
- t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
- sig = sigma, standard deviation normalized to the standard deviation of best picks
- rsdl/sig = least-squares residual divided by sigma
- dtb(m) = depth to bottom of layer in meters
- dtb(ft) = depth to bottom of layer in feet
- tth(s) = arrival time in seconds to bottom of layer
- v(m/s) = velocity in meters per second
- vl(m/s) = lower limit of velocity in meters per second *
- vu(m/s) = upper limit of velocity in meters per second
- v(ft/s) = velocity in feet per second
- vl(ft/s) = lower limit of velocity in feet per second
- vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SAN FRANCISCO NORTH QUADRANGLE
CALIFORNIA
7.5 MINUTE SERIES (TOPOGRAPHIC)



Figure 55. Site location map for Presidio borehole. The borehole is located within 75 meters of the strong-motion recorder.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
>100	>36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

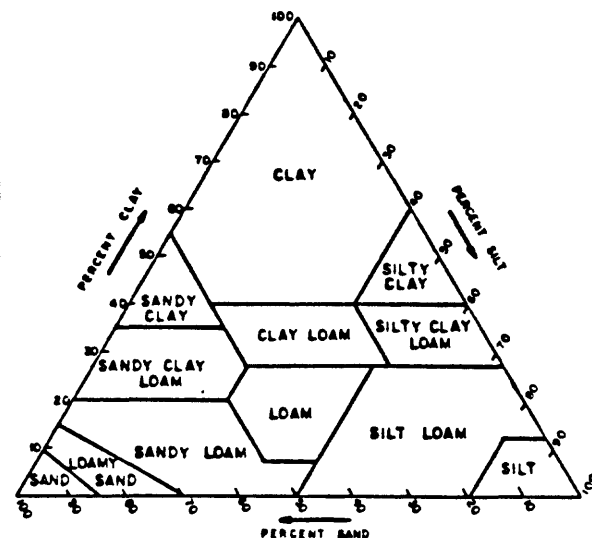
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	<2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
>50	v. dense	15-30	v. stiff
		>30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration 1 + 3/8 in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 56. Explanation of geologic log.

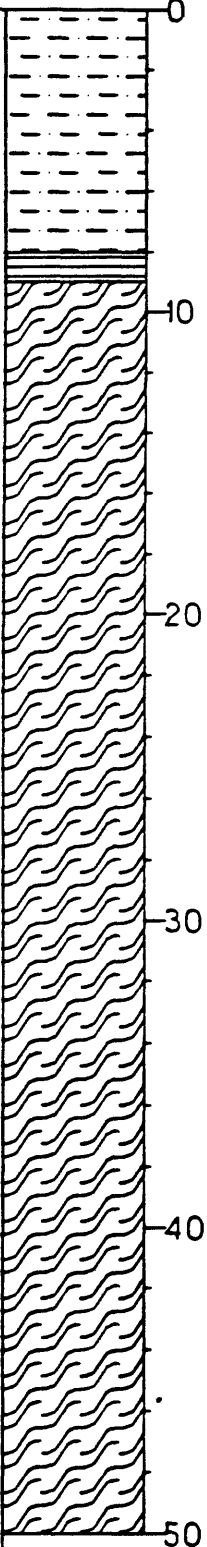
BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			0	SILTY CLAY LOAM, very dark brown, (7.5YR 3/2)
			1	brown (7.5YR 4/4)
			2	
			3	SANDY LOAM, light olive brown, (2.5Y 5/4)
			10	SERPENTINITE, light olive brown (2.5Y 5/4), very closely fractured, hard
			4	
			5	olive grey to black (5Y 4/2), closely to moderately fractured
			6	very closely to closely fractured
			20	
			7	
			8	
			9	greenish grey (5GY 5/1), sheared, texture is very coarse sandy clay
			30	
			10	sheared to very closely fractured
			11	
			12	very closely to closely fractured
			40	sheared to very closely fractured
			13	
			14	
			15	
			50	

Figure 57. Geologic log for the Presidio borehole.

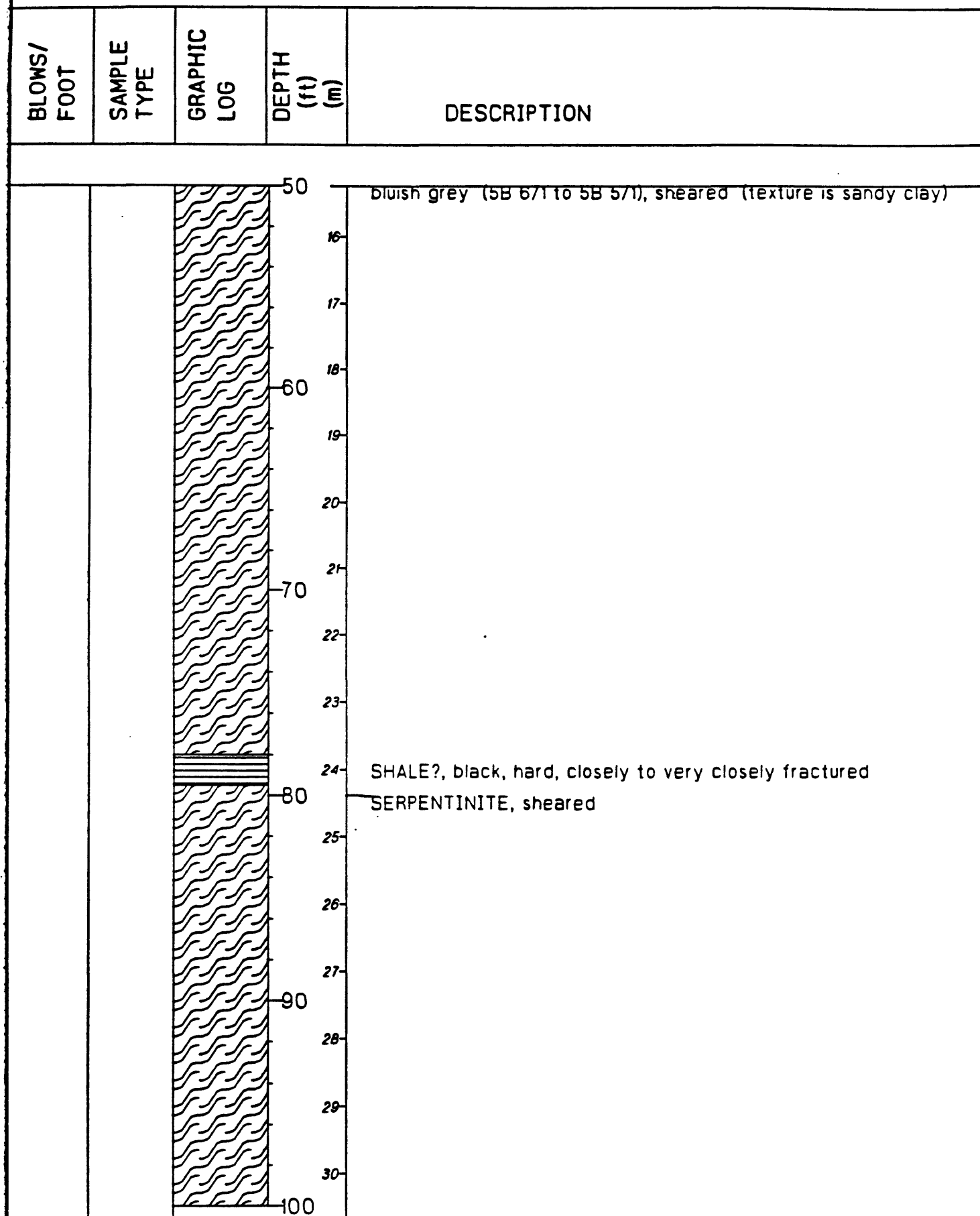


Figure 57. (Continued).

BLOWS/ FOOT	SAMPLE TYPE	GRAPHIC LOG	DEPTH (ft) (m)	DESCRIPTION
			100	
			31	SHALE, black, hard
			32	
			33	
			110	SERPENTINITE, sheared (texture is sandy clay)
			34	
			35	
			36	
			120	
			37	
			38	rocky
				very firm, sheared (texture is sandy clay)
			39	
			130	
			40	
			41	
			42	rocky
			140	
			43	very firm, sheared
			44	
			45	rocky
			150	very firm, sheared

Figure 57. (Continued).

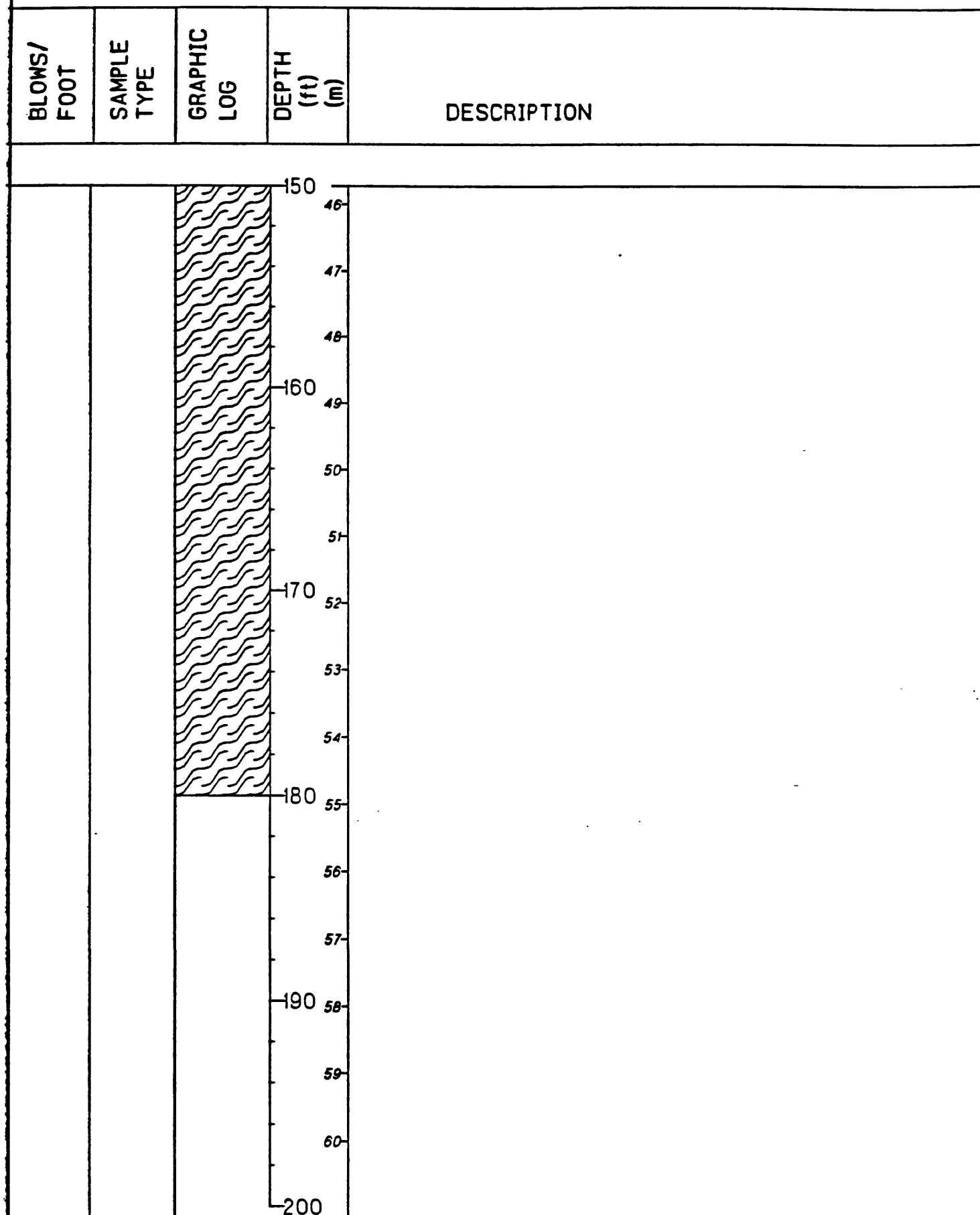


Figure 57. (Continued).

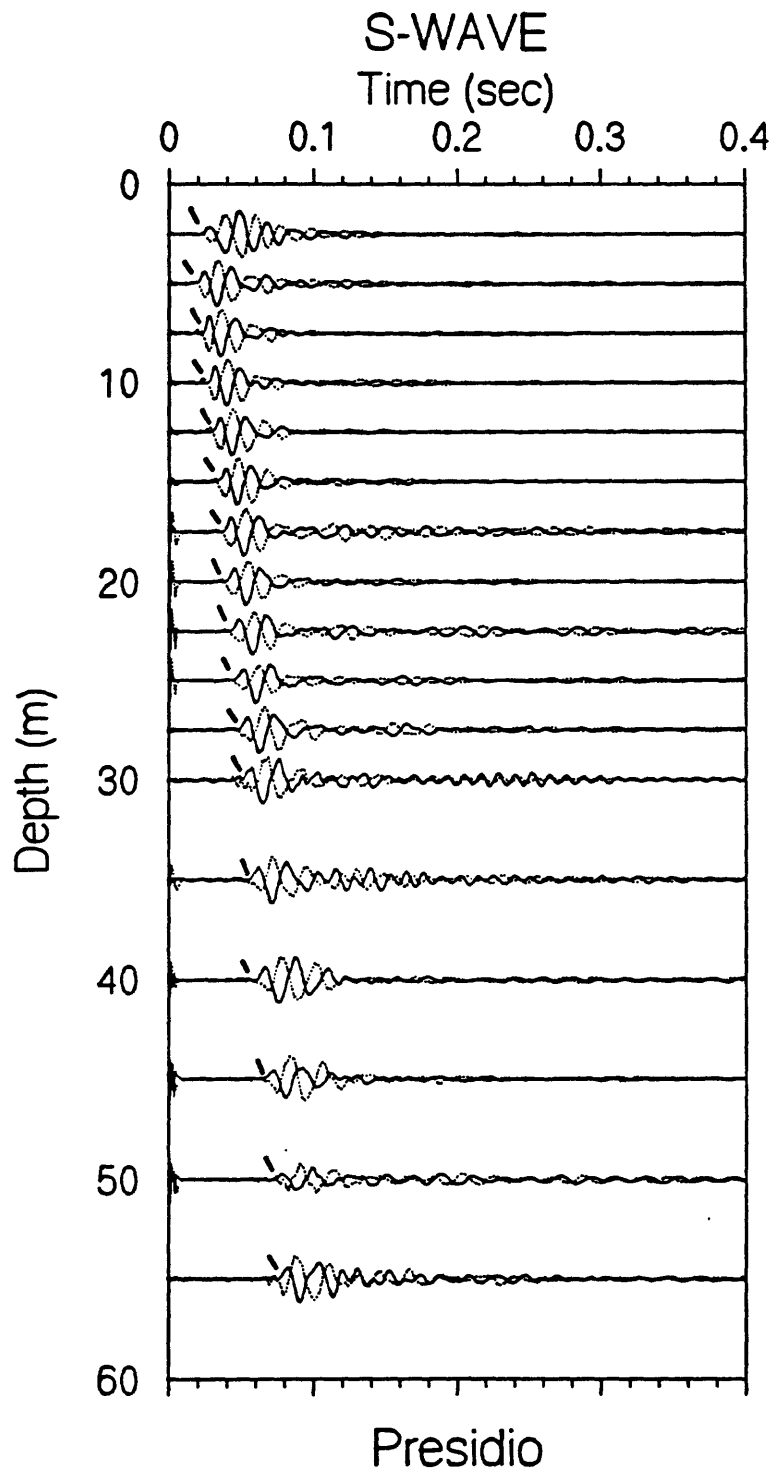


Figure 58. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

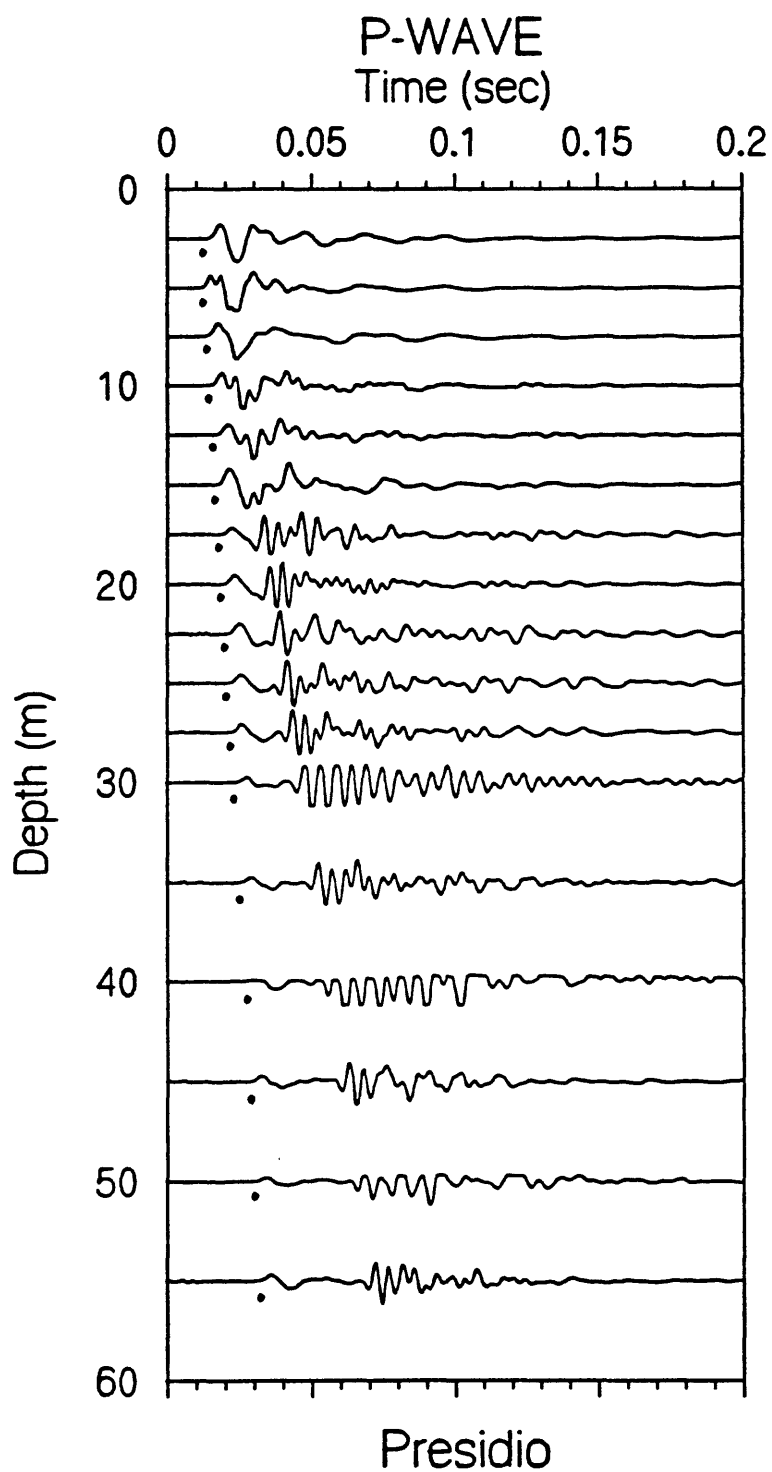


Figure 59. Vertical-component record section. P-wave arrivals are shown by the solid circles.

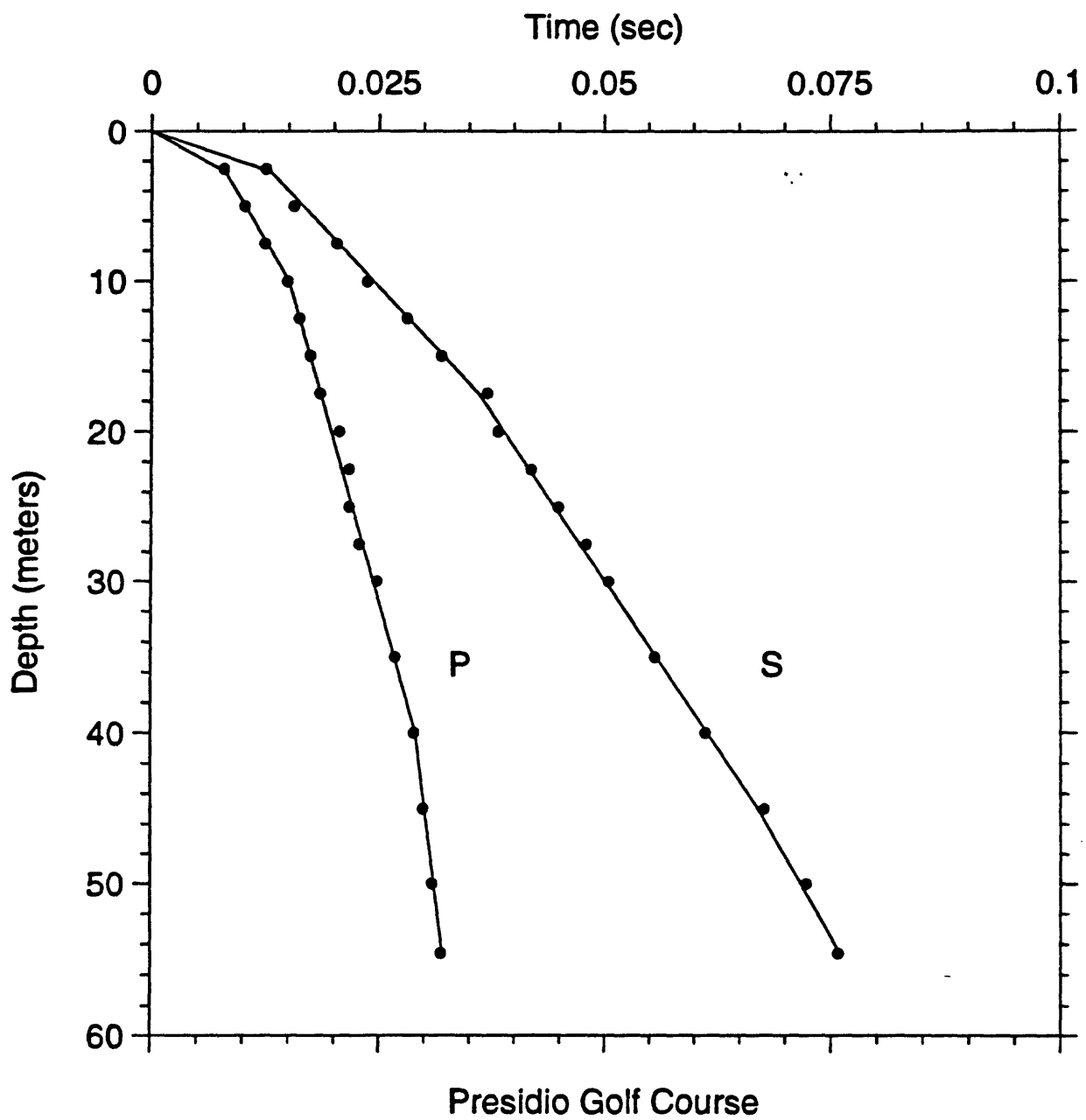


Figure 60. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

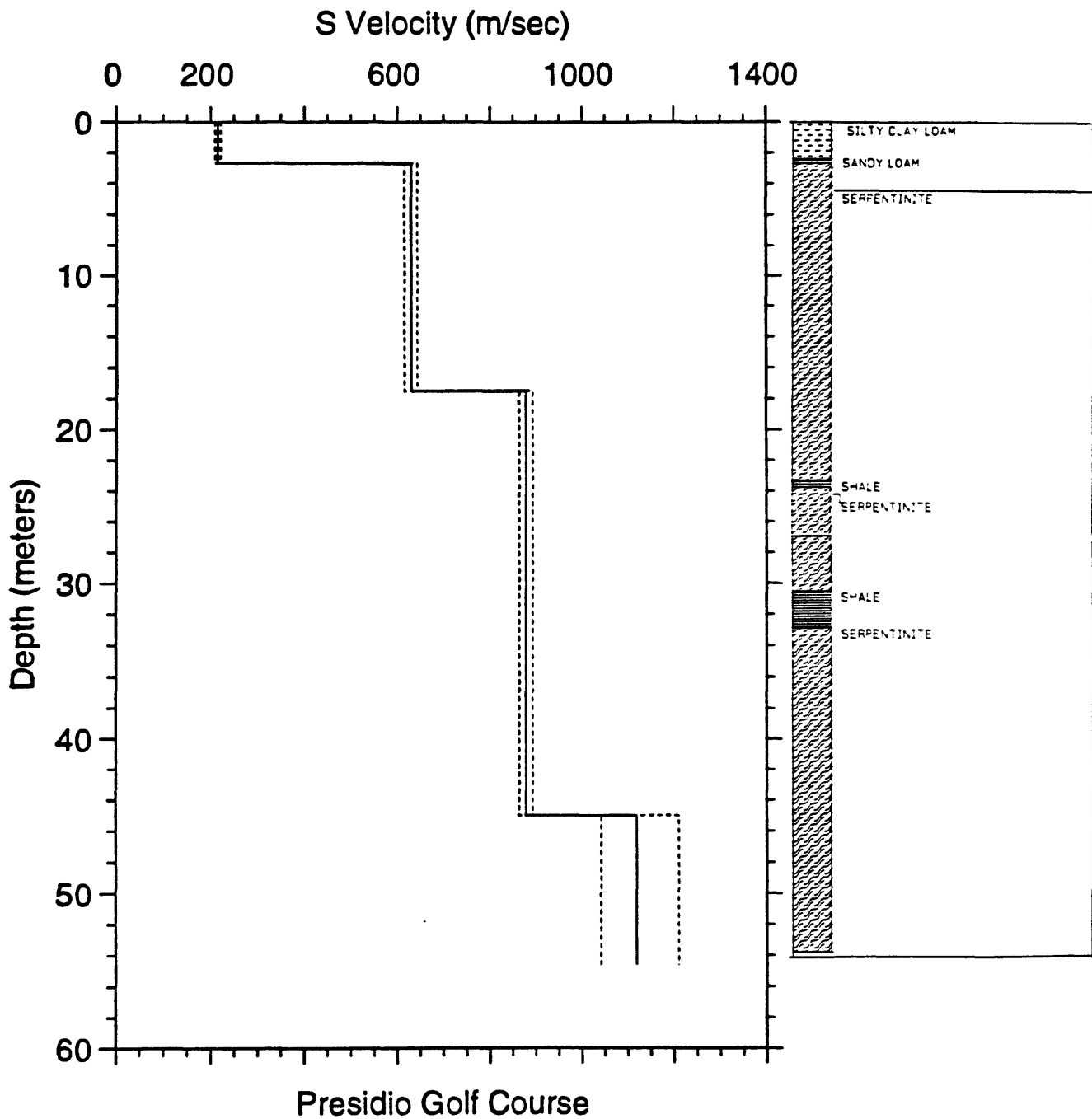


Figure 61. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

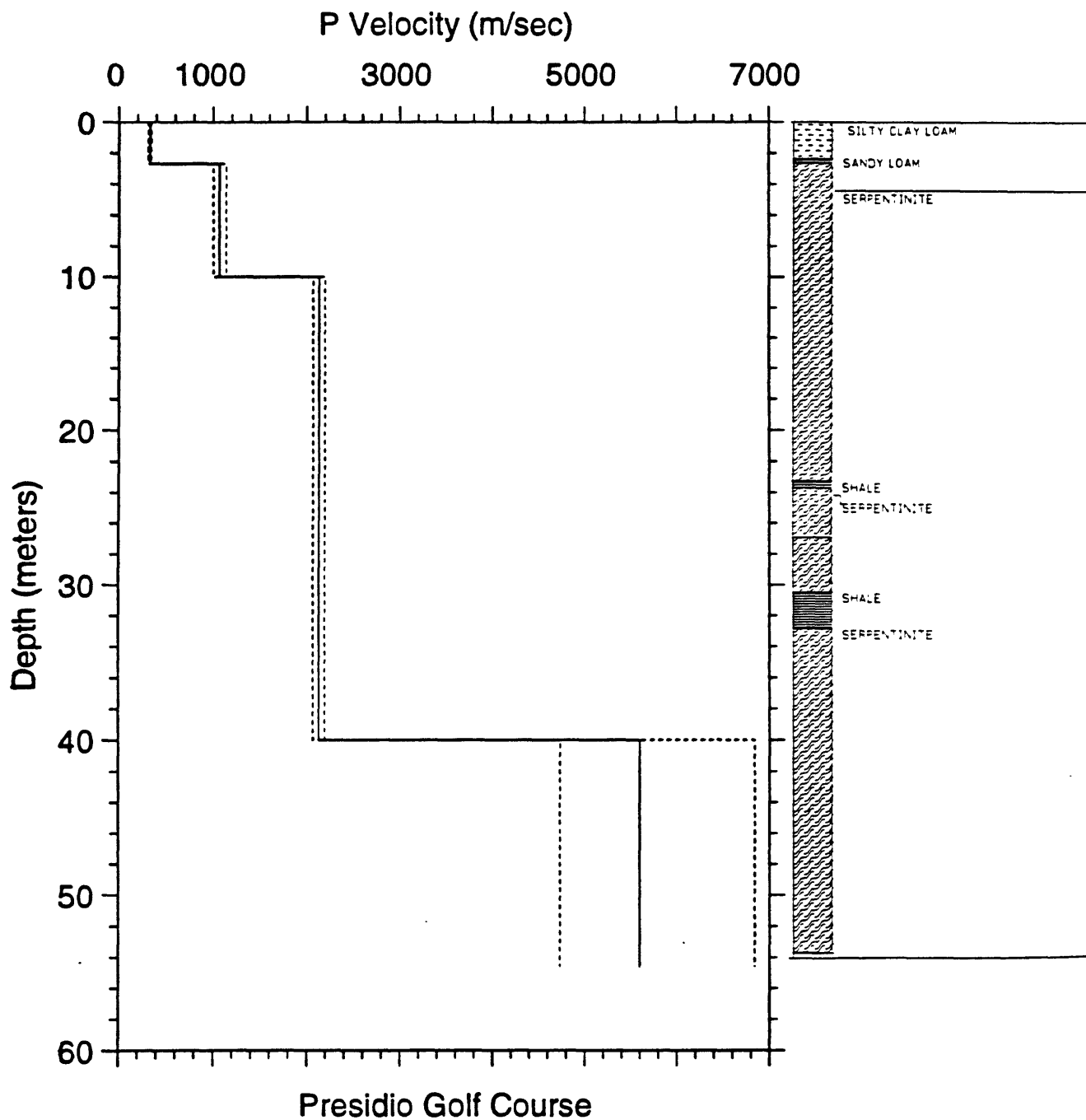


Figure 62. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 13. S-wave arrival times and velocity summaries for Presidio Golf Course.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	tbb(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0125	1	.9	.0	.0	.000	215	209	221	704	684	725
5.0	16.4	.0156	1	-.6	2.7	8.9	.013	215	209	221	704	684	725
7.5	24.6	.0203	1	.1	17.5	57.4	.036	629	615	642	2062	2019	2108
10.0	32.8	.0237	1	-.5	45.0	147.6	.067	878	864	893	2882	2836	2930
12.5	41.0	.0281	1	-.1	54.6	179.1	.076	1119	1041	1210	3671	3414	3969
15.0	49.2	.0319	1	-.2									
17.5	57.4	.0370	1	.9									
20.0	65.6	.0382	1	-.8									
22.5	73.8	.0419	1	.1									
25.0	82.0	.0449	1	.2									
27.5	90.2	.0480	1	.5									
30.0	98.4	.0505	1	.1									
35.0	114.8	.0556	1	-.4									
40.0	131.2	.0612	1	-.5									
45.0	147.6	.0677	1	.3									
50.0	164.0	.0723	1	.4									
54.6	179.1	.0758	1	-.2									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

tbb(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

TABLE 14. P-wave arrival times and velocity summaries for Presidio Golf Course.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b(s)	v(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0079	1	.3	.0	.0	.000	328	342	1075	1032	1122
5.0	16.4	.0102	1	-.2	2.7	8.9	.008	328	342	1075	1032	1122
7.5	24.6	.0124	1	-.3	10.0	32.8	.015	1066	1137	3497	3290	3732
10.0	32.8	.0149	1	-.2	40.0	131.2	.029	2128	2193	6983	6783	7194
12.5	41.0	.0162	1	-.1	54.6	179.1	.032	5596	6839	18358	15534	22439
15.0	49.2	.0174	1	.0								
17.5	57.4	.0185	1	-.1								
20.0	65.6	.0206	1	.8								
22.5	73.8	.0217	1	.7								
25.0	82.0	.0217	1	-.4								
27.5	90.2	.0228	1	.5								
30.0	98.4	.0248	1	.3								
35.0	114.8	.0268	1	.0								
40.0	131.2	.0289	2	-.1								
45.0	147.6	.0299	1	-.2								
50.0	164.0	.0309	1	-.1								
54.6	179.1	.0319	1	.1								

Explanation:

- d(m) = depth in meters
- d(ft) = depth in feet
- t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
- sig = sigma, standard deviation normalized to the standard deviation of best picks
- rsdl/sig = least-squares residual divided by sigma
- dtb(m) = depth to bottom of layer in meters
- dtb(ft) = depth to bottom of layer in feet
- t(b(s) = arrival time in seconds to bottom of layer
- v(m/s) = velocity in meters per second
- vl(m/s) = lower limit of velocity in meters per second *
- vu(m/s) = upper limit of velocity in meters per second
- v(ft/s) = velocity in feet per second
- vl(ft/s) = lower limit of velocity in feet per second
- vu(ft/s) = upper limit of velocity in feet per second
- * see text for explanation of velocity limits

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

WOODSIDE, CALIF.
NE/4 HALF MOON BAY 15 QUADRANGLE
N3722.5 - W12215/7.5

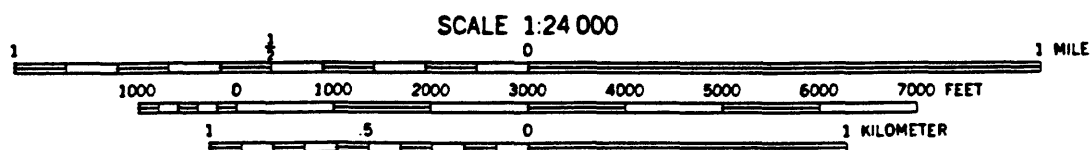
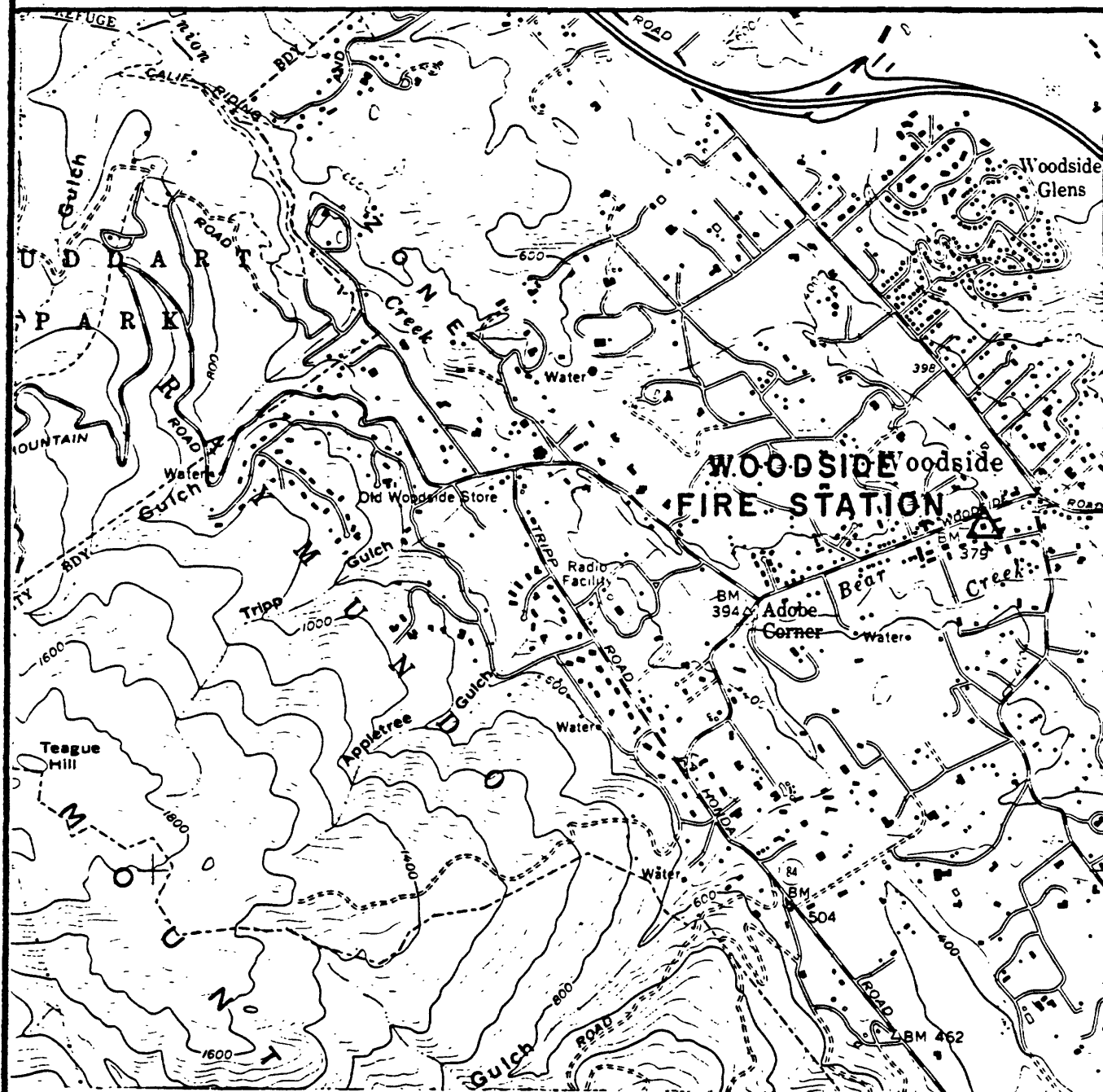


Figure 63. Site location map for Woodside Fire Station. The borehole is located within 20 meters of the strong-motion recorder.

Definitions of terms used for descriptions of sedimentary deposits and bedrock materials

Rock hardness: response to hand and geologic hammer: (Ellen et al., 1972)

hard - hammer bounces off with solid sound

firm - hammer dents with thud, pick point dents or penetrates slightly

soft - pick points penetrates

friable material can be crumbled into individual grains by hand.

Fracture spacing: (Ellen et al., 1972)

cm	in	fracture spacing
0-1	0-1/2	v. close
1-5	1/2-2	close
5-30	2-12	moderate
30-100	12-36	wide
> 100	> 36	v. wide

Weathering:

Fresh: no visible signs of weathering

Slight: no visible decomposition of minerals, slight discoloration

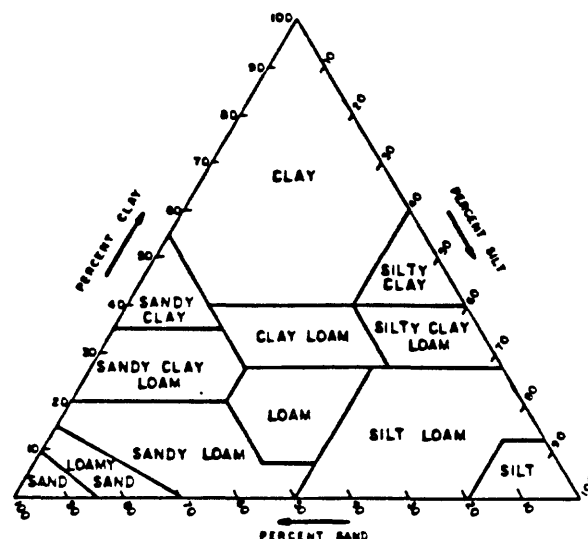
Moderate: slight decomposition of minerals and disintegration of rock, deep and thorough discoloration

Deep: extensive decomposition of minerals and complete disintegration of rock but original structure is preserved.

Relative density of sand and consistency of clay is correlated with penetration resistance: (Terzaghi and Peck, 1948)

blows/ft.	relative density	blows/ft.	consistency
0-4	v. loose	< 2	v. soft
4-10	loose	2-4	soft
10-30	medium	4-8	medium
30-50	dense	8-15	stiff
> 50	v. dense	15-30	v. stiff
		> 30	hard

Texture: the relative proportions of clay, silt, and sand below 2mm. Proportions of larger particles are indicated by modifiers of textural class names. Determination is made in the field mainly by feeling the moist soil (Soil Survey, Staff, 1951).



Color: Standard Munsell color names are given for the dominant color of the moist soil and for prominent mottles.

Types of samples

SP - Standard Penetration (1 + 3/8 in in ID sampler)

S - Thin-wall push sampler

O - Osterberg fixed-piston sampler

P - Pitcher Barrel sampler

CH - California Penetration (2 in ID sampler)

DC - Diamond Core

Figure 64. Explanation of geologic log.

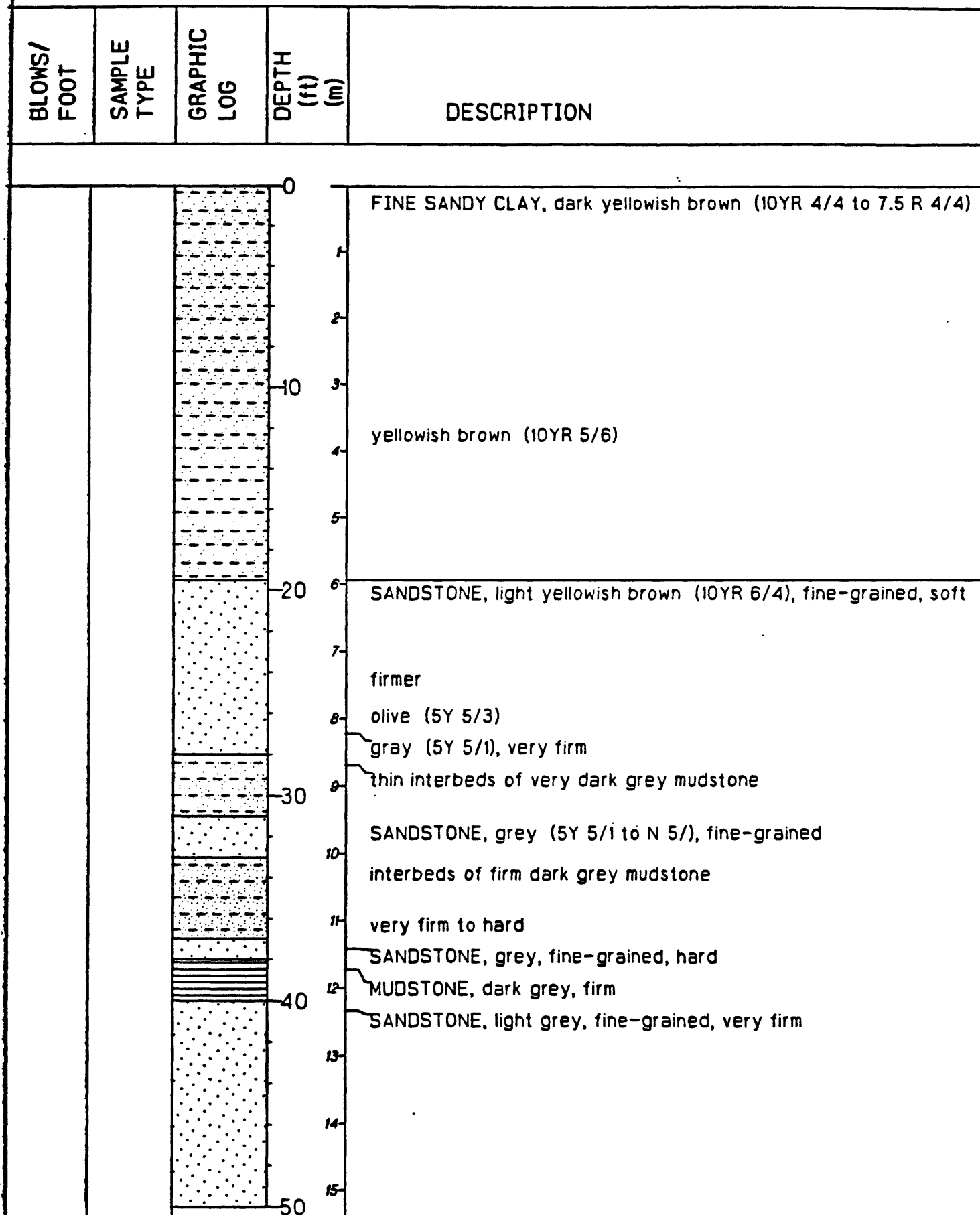


Figure 65. Geologic log for Woodside Fire Station borehole.

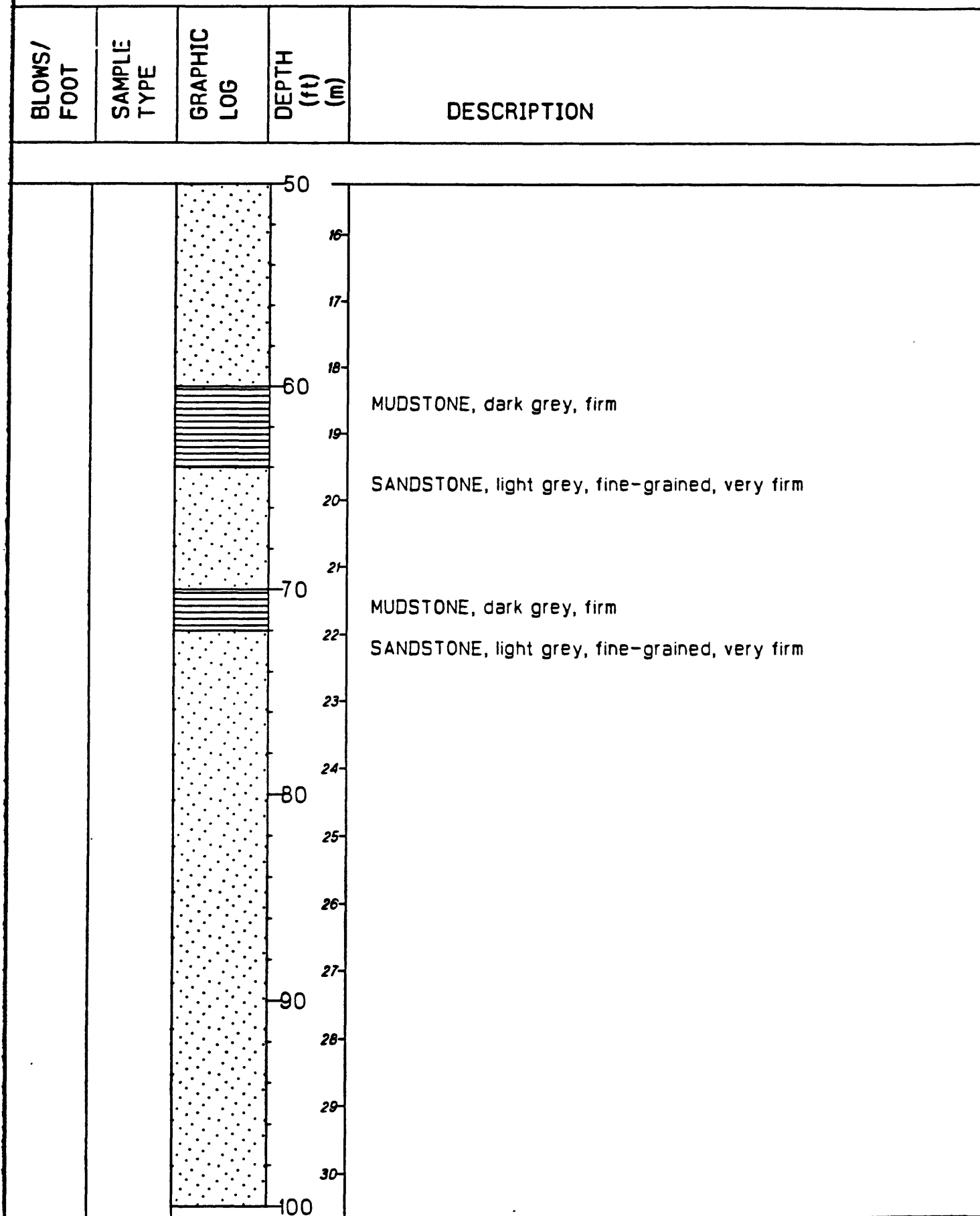


Figure 65. (Continued).

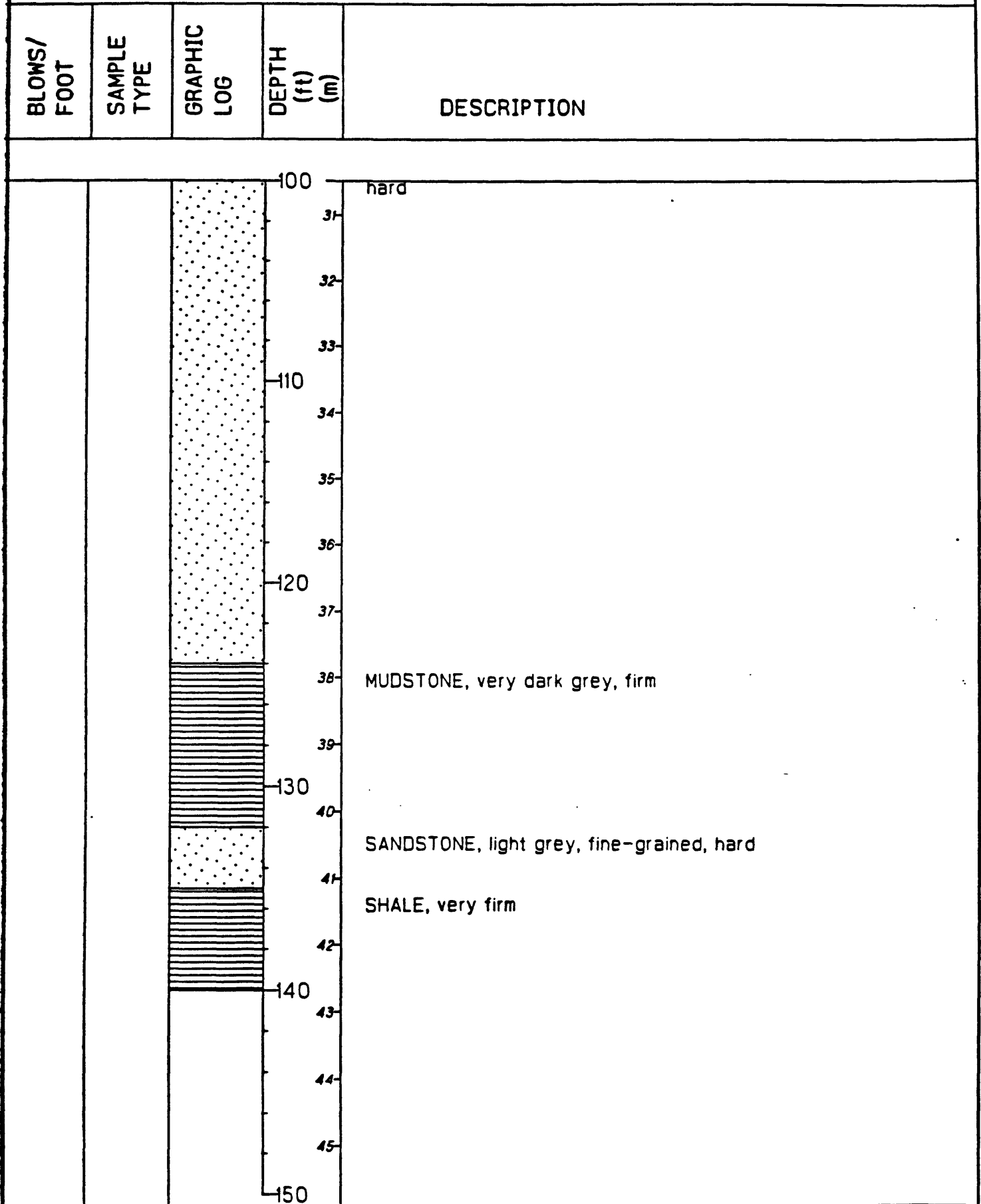


Figure 65. (Continued).

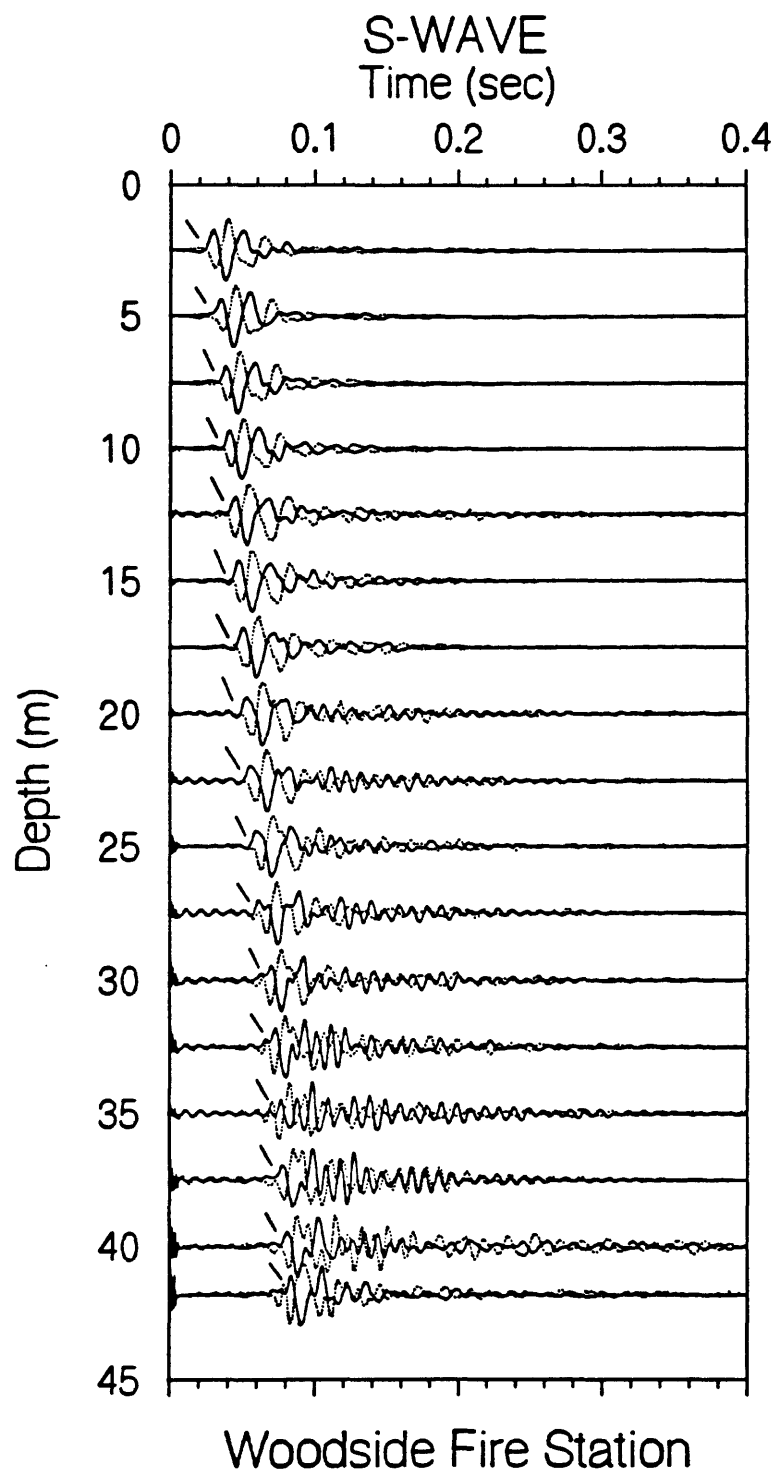


Figure 66. Horizontal-component record section from impacts in opposite horizontal directions superimposed for identification of shear arrivals. S-wave arrivals are shown by the accent marks.

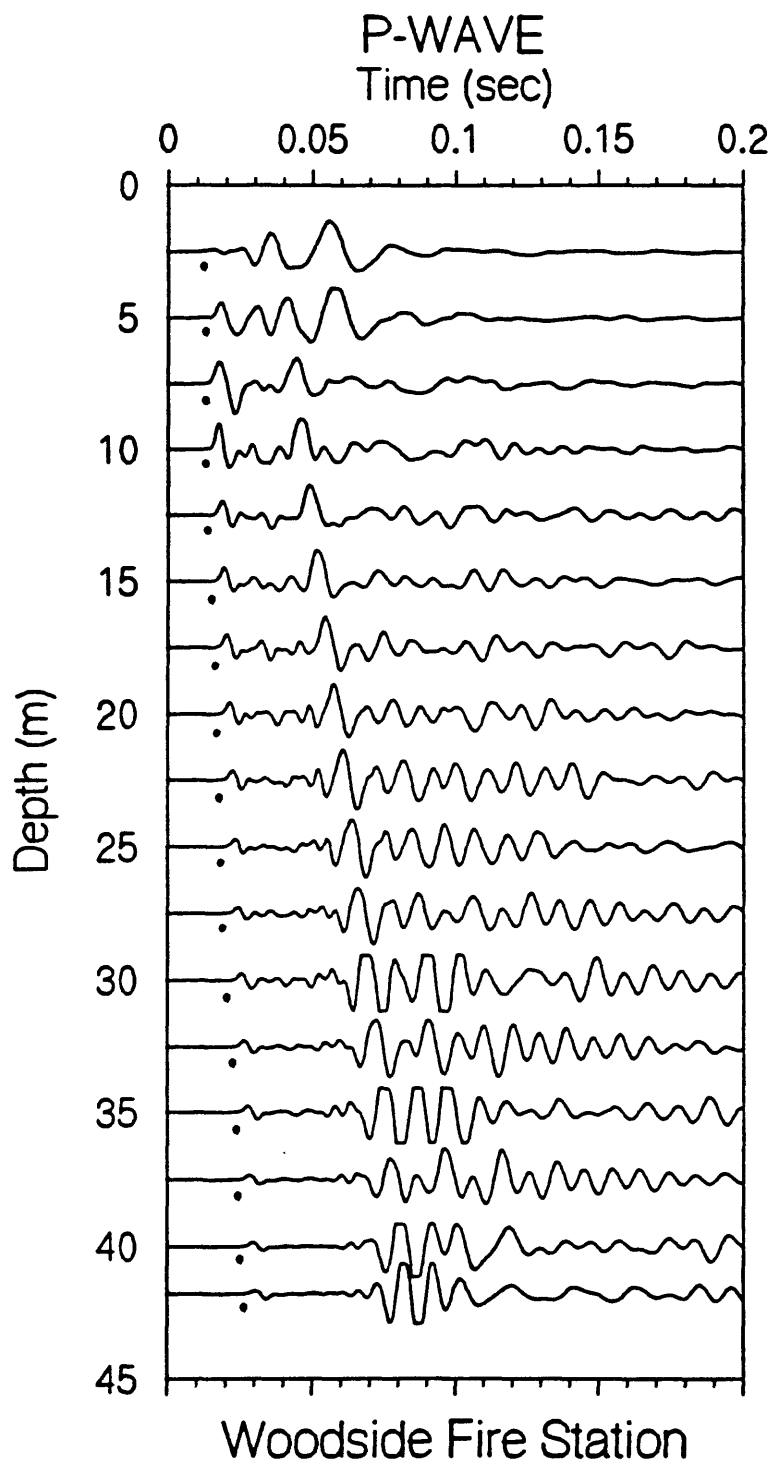


Figure 67. Vertical-component record section. P-wave arrivals are shown by the solid circles.

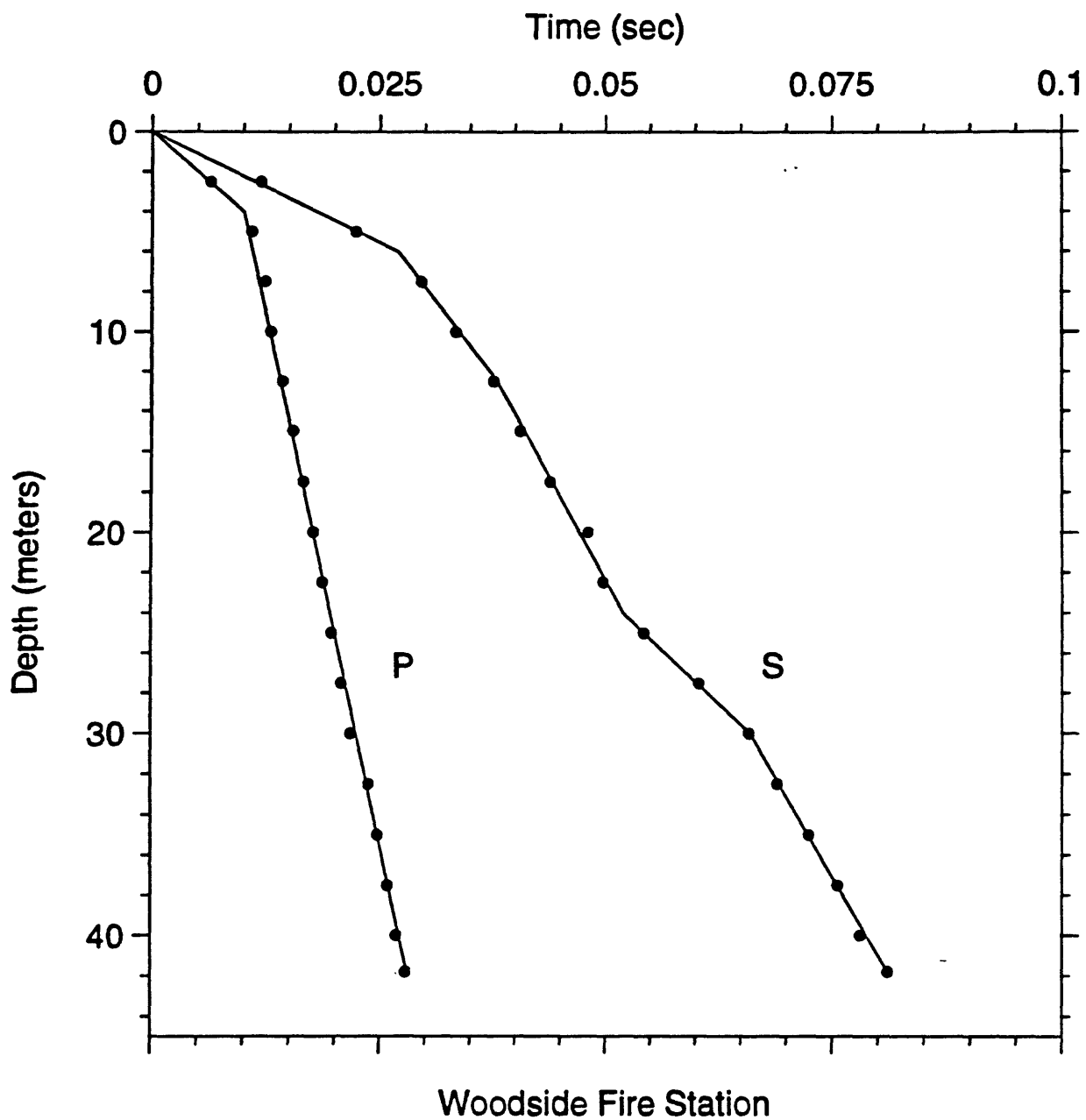


Figure 68. Time-depth graph of P-wave and S-wave picks. Line segments show the hinged-least-squares fit to the data points.

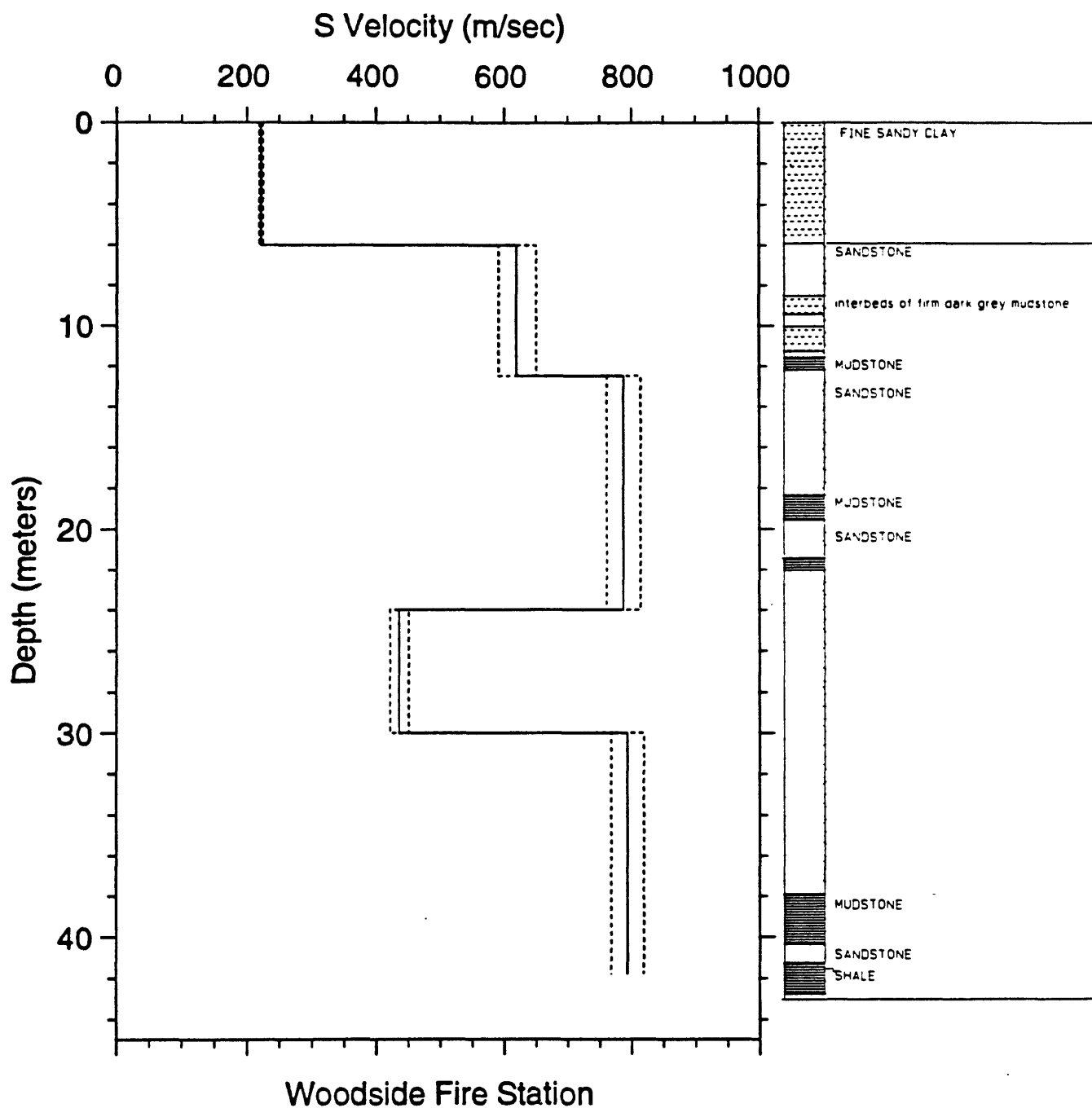


Figure 69. S-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

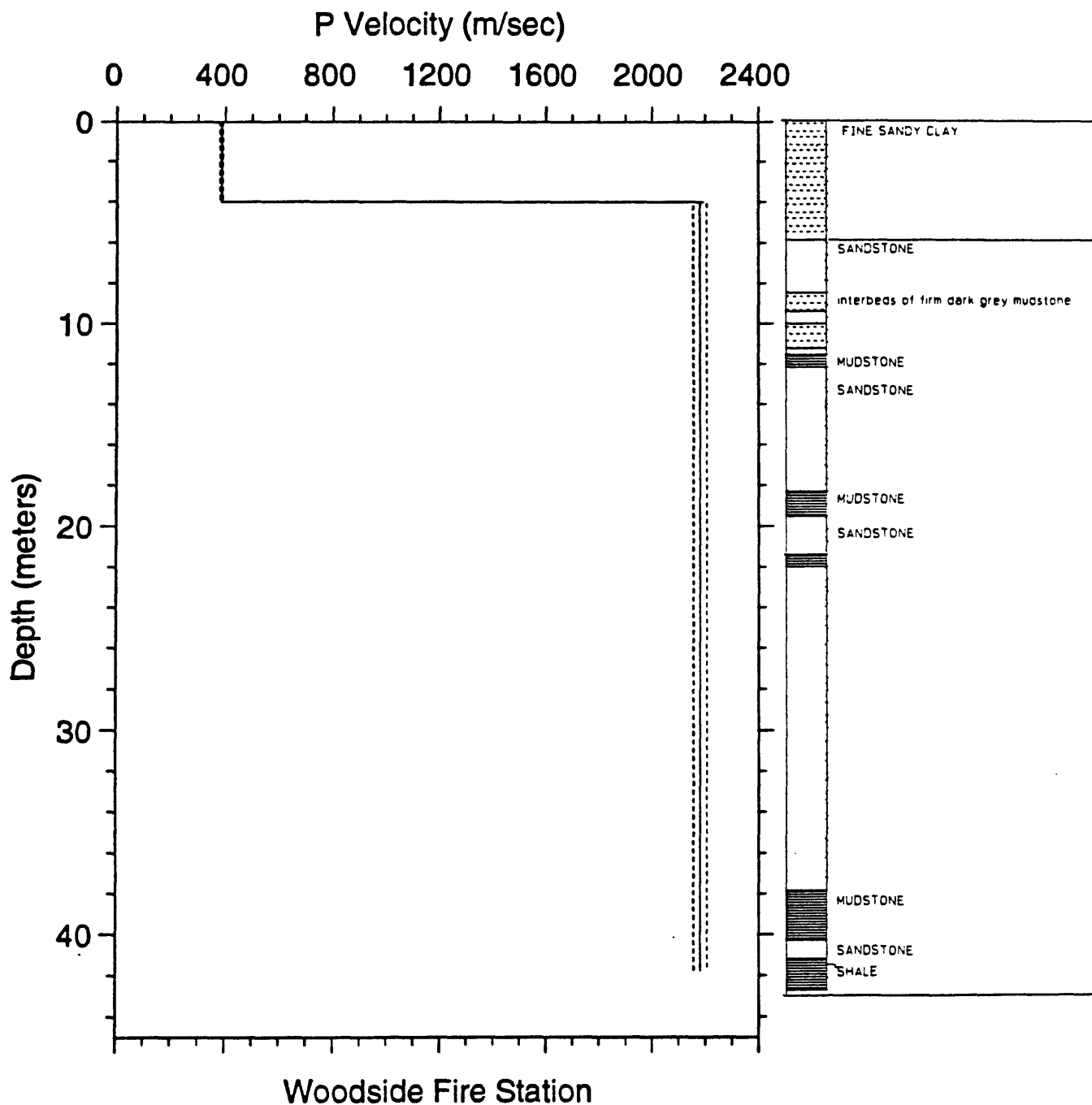


Figure 70. P-wave velocity profiles with dashed lines representing plus and minus one standard deviation. The statistics are done on the slope (reciprocal velocity) so that some of the limits will not appear symmetrical. Simplified geologic log is shown for correlation with velocities.

TABLE 15. S-wave arrival times and velocity summaries for Woodside Fire Station.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b(s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0119	1	.6	.0	.0	.000	221	219	224	726	717	736
5.0	16.4	.0223	1	-.3	6.0	19.7	.027	221	219	224	726	717	736
7.5	24.6	.0296	1	.1	12.5	41.0	.038	619	591	650	2032	1940	2133
10.0	32.8	.0334	1	-.2	24.0	78.7	.052	787	761	814	2581	2498	2669
12.5	41.0	.0376	1	.0	30.0	98.4	.066	436	422	451	1432	1386	1481
15.0	49.2	.0406	1	-.2	41.8	137.1	.081	793	768	819	2600	2520	2686
17.5	57.4	.0439	1	-.1									
20.0	65.6	.0481	1	1.0									
22.5	73.8	.0498	1	-.5									
25.0	82.0	.0543	1	-.2									
27.5	90.2	.0604	1	-.2									
30.0	98.4	.0659	1	-.1									
32.5	106.6	.0690	1	-.1									
35.0	114.8	.0725	1	-.2									
37.5	123.0	.0756	1	-.2									
40.0	131.2	.0781	1	-.5									
41.8	137.1	.0811	1	.2									

Explanation:

d(m) = depth in meters

d(ft) = depth in feet

t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)

sig = sigma, standard deviation normalized to the standard deviation of best picks

rsdl/sig = least-squares residual divided by sigma

dtb(m) = depth to bottom of layer in meters

dtb(ft) = depth to bottom of layer in feet

t(b(s) = arrival time in seconds to bottom of layer

v(m/s) = velocity in meters per second

vl(m/s) = lower limit of velocity in meters per second *

vu(m/s) = upper limit of velocity in meters per second

v(ft/s) = velocity in feet per second

vl(ft/s) = lower limit of velocity in feet per second

vu(ft/s) = upper limit of velocity in feet per second

* see text for explanation of velocity limits

TABLE 16. P-wave arrival times and velocity summaries for Woodside Fire Station.

d(m)	d(ft)	t(sec)	sig	rsdl/sig	dtb(m)	dtb(ft)	t(b/s)	v(m/s)	vl(m/s)	vu(m/s)	v(ft/s)	vl(ft/s)	vu(ft/s)
2.5	8.2	.0064	1	-.1	.0	.0	.000	386	381	390	1265	1251	1279
5.0	16.4	.0109	1	.1	4.0	13.1	.010	386	381	390	1265	1251	1279
7.5	24.6	.0124	1	.4	41.8	137.1	.028	2180	2155	2205	7152	7071	7235
10.0	32.8	.0130	1	-.1									
12.5	41.0	.0143	1	.0									
15.0	49.2	.0155	1	.1									
17.5	57.4	.0166	1	.0									
20.0	65.6	.0177	1	.0									
22.5	73.8	.0187	1	-.2									
25.0	82.0	.0197	1	-.3									
27.5	90.2	.0208	1	-.4									
30.0	98.4	.0218	1	-.5									
32.5	106.6	.0238	1	.4									
35.0	114.8	.0248	1	.2									
37.5	123.0	.0259	1	.2									
40.0	131.2	.0269	1	.0									
41.8	137.1	.0279	1	.2									

Explanation:

- d(m) = depth in meters
- d(ft) = depth in feet
- t(sec) = arrival time in seconds (S-wave arrival times are the average of picks from traces obtained from hammer blows differing in direction by 180°)
- sig = sigma, standard deviation normalized to the standard deviation of best picks
- rsdl/sig = least-squares residual divided by sigma
- dtb(m) = depth to bottom of layer in meters
- dtb(ft) = depth to bottom of layer in feet
- t(b/s) = arrival time in seconds to bottom of layer
- v(m/s) = velocity in meters per second
- vl(m/s) = lower limit of velocity in meters per second *
- vu(m/s) = upper limit of velocity in meters per second
- v(ft/s) = velocity in feet per second
- vl(ft/s) = lower limit of velocity in feet per second
- vu(ft/s) = upper limit of velocity in feet per second
- * see text for explanation of velocity limits