

LEVEL II SCOUR ANALYSIS FOR BRIDGE 20 (IRASTH00080020) on TOWN HIGHWAY 8, crossing the BLACK RIVER, IRASBURG, VERMONT

U.S. Geological Survey
Open-File Report 96-154

Prepared in cooperation with
VERMONT AGENCY OF TRANSPORTATION
and
FEDERAL HIGHWAY ADMINISTRATION



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By SCOTT A. OLSON

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Pembroke, New Hampshire

1996

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CONVERSION FACTORS, ABBREVIATIONS, AND VERTICAL DATUM

Multiply	By	To obtain
Length		
inch (in.)	25.4	millimeter (mm)
foot (ft)	0.3048	meter (m)
mile (mi)	1.609	kilometer (km)
Slope		
foot per mile (ft/mi)	0.1894	meter per kilometer (m/km)
Area		
square mile (mi ²)	2.590	square kilometer (km ²)
Volume		
cubic foot (ft ³)	0.02832	cubic meter (m ³)
Velocity and Flow		
foot per second (ft/s)	0.3048	meter per second (m/s)
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second (m ³ /s)
cubic foot per second per square mile [(ft ³ /s)/mi ²]	0.01093	cubic meter per second per square kilometer [(m ³ /s)/km ²]

OTHER ABBREVIATIONS

BF	bank full	LWW	left wingwall
cfs	cubic feet per second	MC	main channel
D ₅₀	median diameter of bed material	RAB	right abutment
DS	downstream	RABUT	face of right abutment
elev.	elevation	RB	right bank
f/p	flood plain	ROB	right overbank
ft ²	square feet	RWW	right wingwall
ft/ft	feet per foot	TH	town highway
JCT	junction	UB	under bridge
LAB	left abutment	US	upstream
LABUT	face of left abutment	USGS	United States Geological Survey
LB	left bank	VT AOT	Vermont Agency of Transportation
LOB	left overbank	WSPRO	water-surface profile model

In this report, the words “right” and “left” refer to directions that would be reported by an observer facing downstream.

Sea level: In this report, “sea level” refers to the National Geodetic Vertical Datum of 1929-- a geodetic datum derived from a general adjustment of the first-order level nets of the United States and Canada, formerly called Sea Level Datum of 1929.

In the appendices, the above abbreviations may be combined. For example, USLB would represent upstream left bank.

LEVEL II SCOUR ANALYSIS FOR BRIDGE 20 (IRASTH00080020) ON TOWN HIGHWAY 8, CROSSING THE BLACK RIVER, IRASBURG, VERMONT

By Scott A. Olson

INTRODUCTION

This report provides the results of a detailed Level II analysis of scour potential at structure IRASTH00080020 on town highway 8 crossing the Black River, Irasburg, Vermont (figures 1–8). A Level II study is a basic engineering analysis of the site, including a quantitative analysis of stream stability and scour (U.S. Department of Transportation, 1993). A Level I study is included in Appendix E of this report. A Level I study provides a qualitative geomorphic characterization of the study site. Information on the bridge, available from VTAOT files, was compiled prior to conducting Level I and Level II analyses and can be found in Appendix D.

The site is in the New England Upland physiographic province of north-central Vermont in the town of Irasburg. The 110-mi² drainage area is in a predominantly rural basin. In the vicinity of the study site, the left bank surface cover is pasture and row crops and the right bank is covered by shrub and brush and is adjacent to woods.

In the study area, the Black River has a sinuous channel with a slope of approximately 0.002 ft/ft, an average channel top width of 90 ft and an average channel depth of 5 ft. The predominant channel bed material is gravel and cobbles (D_{50} is 49.7 mm or 0.163 ft). The geomorphic assessment at the time of the Level I and Level II site visit on October 4, 1994, indicated that the reach was laterally unstable.

The town highway 8 crossing of the Black River is a 88-ft-long, one-lane covered bridge consisting of one 80-foot span (Vermont Agency of Transportation, written commun., August 2, 1994). The bridge is supported by vertical, concrete abutments with wingwalls on the upstream and downstream sides of the right abutment. The right abutment has stone fill protection. The channel is skewed approximately 25 degrees to the opening while the opening-skew-to-roadway is zero degrees. Additional details describing conditions at the site are included in the Level II Summary and Appendices D and E.

Scour depths and rock rip-rap sizes were computed using the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution. The scour analysis results are presented in tables 1 and 2 and a graph of the scour depths is presented in figure 8.

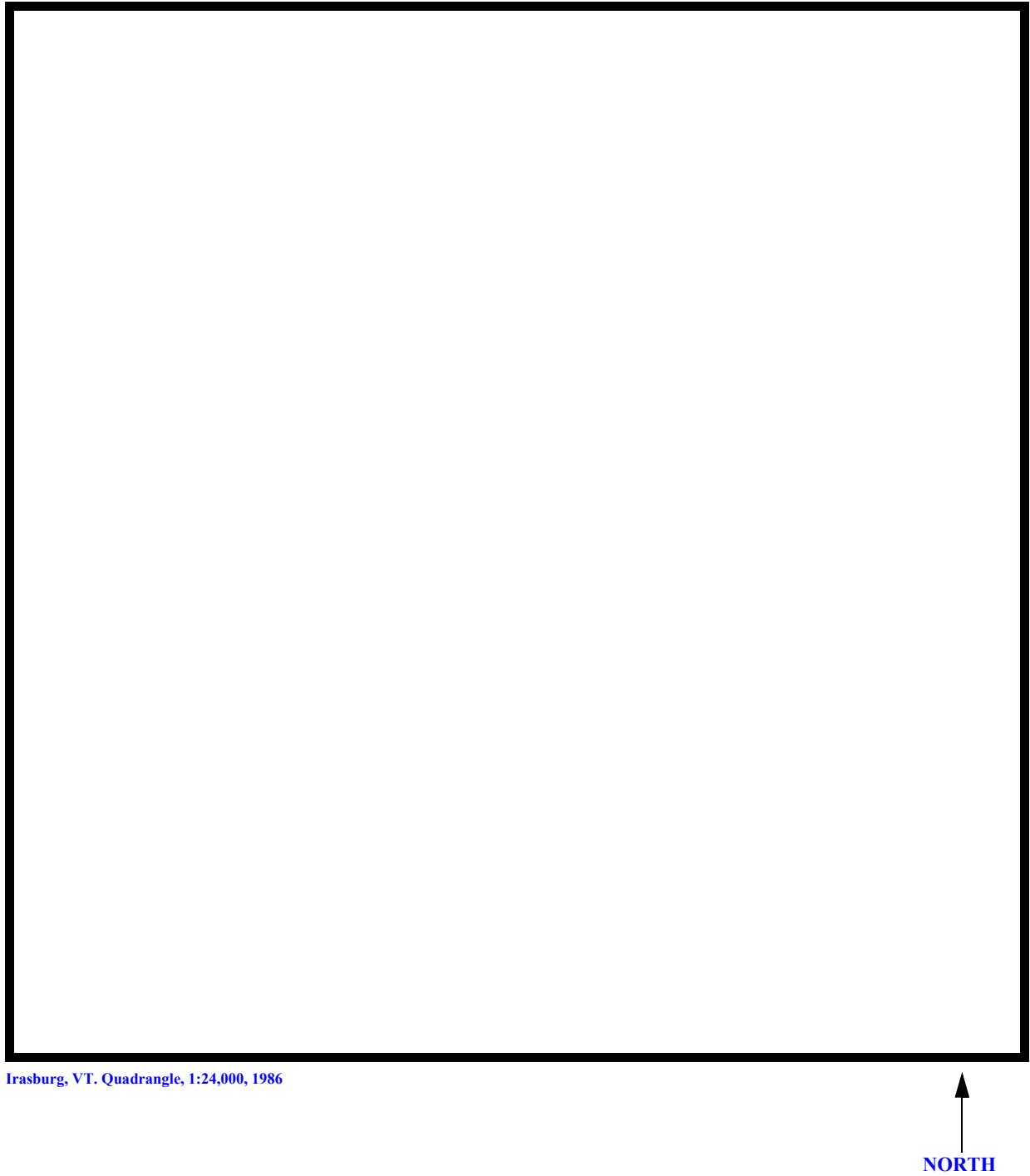


Figure 1. Location of study area on USGS 1:24,000 scale map.

Figure 2. Location of study area on Vermont Agency of Transportation town highway map.





LEVEL II SUMMARY

Structure Number IRASTH00080020 **Stream** Black River
County Orleans **Road** TH008 **District** 09

Description of Bridge

Bridge length 88 **ft** **Bridge width** 22 **ft** **Max span length** 80 **ft**
Alignment of bridge to road (on curve or straight) sharp curve at right road approach
Abutment type Concrete, vertical **Embankment type** sloping
Abutment type on right **Embankment type** 10/4/94
Stone fill on abutment? Type-2 stone fill on right abutment, upstream right wingwall, and the
Description of stone fill upstream and downstream sides of the right road approach. Type-3 stone fill on upstream side of
the left road approach.

Is bridge skewed to flood flow according to Y **' survey?** 25
Angle

The river severely curves at the approach to the bridge. This curve results in a skew of 25 degrees
and in the flow impacting the right abutment also at approximately 25 degrees.

Debris accumulation on bridge at time of Level I or Level II site visit:

	Date of inspection	Percent of channel blocked horizontally	Percent of channel blocked vertically
Level I	<u>10/4/94</u>	<u>0</u>	<u>0</u>
Level II	<u>10/4/94</u>	<u>--</u>	<u>--</u>

Potential for debris Accumulation potential is moderate due to sharp bend just upstream of the bridge.

On 10/4/94 it was noted that flood flows will impact the right abutment heavily and may cause
Describe any features near or at the bridge that may affect flow (include observation date)
pile-up of water and increase scour.

Description of the Geomorphic Setting

General topography Moderate relief valley with wide flood plains and no apparent incision of the channel.

Geomorphic conditions at bridge site: downstream (DS), upstream (US)

Date of inspection 10/4/94

DS left: wide flood plain

DS right: steep valley wall

US left: two-lane gravel road, then wide flood plain

US right: narrow flood plain, then steep valley wall

Description of the Channel

<p>Average top width <u>90</u></p> <p style="text-align: center;"><u>gravel</u> [#]</p>	<p>Average depth <u>5</u></p> <p style="text-align: center;"><u>cobble</u> [#]</p>
---	--

Predominant bed material gravel **Bank material** sinuous, with flood plains. Stream boundaries are alluvial and semi-alluvial and are laterally unstable

Vegetative cover 10/4/94
Pasture and row crops

DS left: Shrub and brush with forest further from river

DS right: Pasture

US left: Shrub and brush

US right: N

Do banks appear stable? 10/4/94--In the downstream channel a cut-bank is noted along the left bank as well as a mid-channel bar.
date of observation.

08/16/94--None

Describe any obstructions in channel and date of observation.

Hydrology

$$\text{Drainage area} \quad \frac{110}{\text{mi}^2}$$

Percentage of drainage area in physiographic provinces: (approximate)

<i>Physiographic province</i>	<i>Percent of drainage area</i>
New England Upland	100

Is drainage area considered rural or urban? Rural *Describe any significant urbanization:* None

<i>Is there a USGS gage on the stream of interest?</i>	<u>Yes</u>	
<i>USGS gage description</i>	<u>Black River at Coventry, Vermont</u>	
<i>USGS gage number</i>	<u>04296000</u>	
<i>USGS gage number</i>	<u>122</u>	
<i>Gage drainage area</i>	<i>mi</i> ²	No

Is there a lake? _____

3,800 **Calculated Discharges** 4,460
Q100 *ft³/s* *Q500* *ft³/s*
 Discharges are based on analysis of the continuous

record from the Black River gage. The computed 100-year and 500-year discharges at the gage were reduced by a drainage area relationship $[(110/122) \text{ to the } 0.8 \text{ power}]$ to determine the discharges at the bridge site.

Description of the Water-Surface Profile Model (WSPRO) Analysis

Datum for WSPRO analysis (USGS survey, sea level, VTAOT plans) USGS survey

Datum tie between USGS survey and VTAOT plans Add 265.4 feet to VTAOT datum.

RM1 is a chiseled X on top of the downstream end of the left abutment wall with an arbitrary

Description of reference marks used to determine USGS datum. survey elevation of
1008.62 feet.

Cross-Sections Used in WSPRO Analysis

¹ <i>Cross-section</i>	<i>Section Reference Distance (SRD) in feet</i>	² <i>Cross-section development</i>	<i>Comments</i>
EXIT2	-121	1	Downstream section
EXIT1	-39	1	Exit section
FV	0	2	Downstream Full-valley section (Templated from EXIT1)
BRIDG	0	1	Bridge section
RDWAY	10	1	Road Grade section
APPR1	110	1	Approach section

¹ For location of cross-sections see plan-view sketch included with Level I field form, Appendix E.
 For more detail on how cross-sections were developed see WSPRO input file.

Data and Assumptions Used in WSPRO Model

Hydraulic analyses of the reach were done by use of the Federal Highway Administration's WSPRO step-backwater computer program (Shearman and others, 1986, and Shearman, 1990). Results of the hydraulic model are presented in the Bridge Hydraulic Summary, Appendix B, and figure 7.

Channel roughness factors (Manning's "n") used in the hydraulic model were estimated using field inspections at each cross section following the general guidelines described by Arcement, Jr. and Schneider (1989). Final adjustments to the values were made during the modelling of the reach. Channel "n" values for the reach ranged from 0.040 to 0.045, and overbank "n" values ranged from 0.035 to 0.095.

Normal depth was assumed at the downstream-most section (EXIT2) for the starting water surface. This depth was computed by use of the slope-conveyance method outlined in the User's manual for WSPRO (Shearman, 1990). The slope used was 0.0005 ft/ft which was water-surface slope on the day of the field inspection.

The modeled 100- and 500-year discharges did not overtop the roadway embankments or the bridge deck.

Bridge Hydraulics Summary

Average bridge embankment elevation 1008.0 *ft*
Average low steel elevation 1005.1 *ft*

100-year discharge 3,800 *ft³/s*
Water-surface elevation in bridge opening 1000.5 *ft*
Road overtopping? no *Discharge over road* *ft³/s*
Area of flow in bridge opening 526 *ft²*
Average velocity in bridge opening 7.23 *ft/s*
Maximum WSPRO tube velocity at bridge 9.11 *ft/s*

Water-surface elevation at Approach section with bridge 1001.6
Water-surface elevation at Approach section without bridge 1000.9
Amount of backwater caused by bridge 0.7 *ft*

500-year discharge 4,460 *ft³/s*
Water-surface elevation in bridge opening 1000.8 *ft*
Road overtopping? no *Discharge over road* *ft³/s*
Area of flow in bridge opening 542 *ft²*
Average velocity in bridge opening 8.23 *ft/s*
Maximum WSPRO tube velocity at bridge 10.38 *ft/s*

Water-surface elevation at Approach section with bridge 1002.3
Water-surface elevation at Approach section without bridge 1001.2
Amount of backwater caused by bridge 1.1 *ft*

Incipient overtopping discharge -- *ft³/s*
Water-surface elevation in bridge opening -- *ft*
Area of flow in bridge opening -- *ft²*
Average velocity in bridge opening -- *ft/s*
Maximum WSPRO tube velocity at bridge -- *ft/s*

Water-surface elevation at Approach section with bridge --
Water-surface elevation at Approach section without bridge --
Amount of backwater caused by bridge -- *ft*

Scour Analysis Summary

Special Conditions or Assumptions Made in Scour Analysis

Scour depths were computed using the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution. The results of the scour analysis are presented in tables 1 and 2 and a graph of the scour depths is presented in figure 8.

Contraction scour was computed by use of the [clear-water contraction scour equation \(Richardson and others, 1993, p. 35, equation 18\)](#). For contraction scour computations, the average depth in the contracted section (AREA/TOPWIDTH) is subtracted from the depth of flow computed by the scour equation (Y2) to determine the actual amount of scour.

Abutment scour [for the left abutment](#) was computed by use of the [Froehlich equation \(Richardson and others, 1993, p. 49, equation 24\)](#). The [Froehlich equation](#) gives “[excessively conservative estimates of scour depths](#)” (Richardson and others, 1993, p. 48). Variables for the [Froehlich](#) equation include the Froude number of the flow approaching the embankments, the length of the embankment blocking flow, and the depth of flow approaching the embankment less any roadway overtopping.

Scour at the right abutment was computed by use of the [HIRE equation \(Richardson and others, 1993, p. 50, equation 25\)](#) because the HIRE equation is recommended when the length to depth ratio of the embankment blocking flow exceeds 25. Variables for the [HIRE abutment scour equation](#) are the same as the [Froehlich abutment scour equation](#).

Scour Results

<i>Contraction scour:</i>	<i>100-yr discharge</i>	<i>500-yr discharge</i>	<i>Incipient overtopping discharge</i>
	<i>(Scour depths in feet)</i>		
<i>Main channel</i>			
<i>Live-bed scour</i>	--	--	--
	0.0	0.0	--
<i>Clear-water scour</i>	0.5	1.2	--
<i>Depth to armoring</i>	--	--	--
<i>Left overbank</i>	--	--	--
<i>Right overbank</i>	--	--	--
<i>Local scour:</i>			
<i>Abutment scour</i>	15.9	17.3	--
<i>Left abutment</i>	13.5	14.8	--
<i>Right abutment</i>			
<i>Pier scour</i>	--	--	--
<i>Pier 1</i>	--	--	--
<i>Pier 2</i>	--	--	--
<i>Pier 3</i>			

Rock Riprap Sizing

	<i>100-yr discharge</i>	<i>500-yr discharge</i>	<i>Incipient overtopping discharge</i>
	<i>(D₅₀ in feet)</i>		
<i>Abutments:</i>	1.4	1.8	--
<i>Left abutment</i>	1.4	1.8	--
<i>Right abutment</i>	--	--	--
<i>Piers:</i>	--	--	--
<i>Pier 1</i>	--	--	--
<i>Pier 2</i>	--	--	--

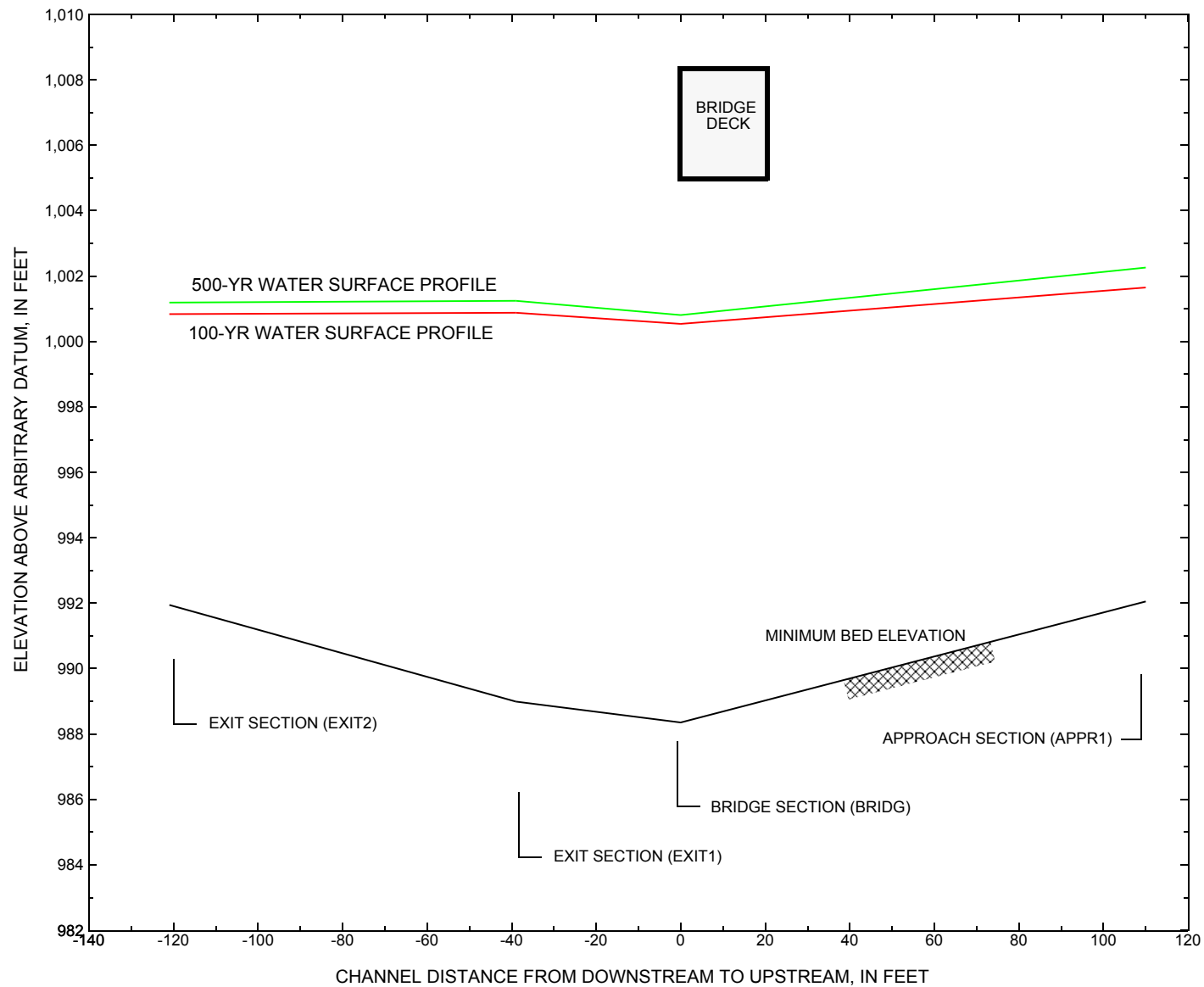


Figure 7. Water-surface profiles for the 100- and 500-yr discharges at structure [IRASTH00080020](#) on town highway 8, crossing the [Black River, Irasburg, Vermont](#).

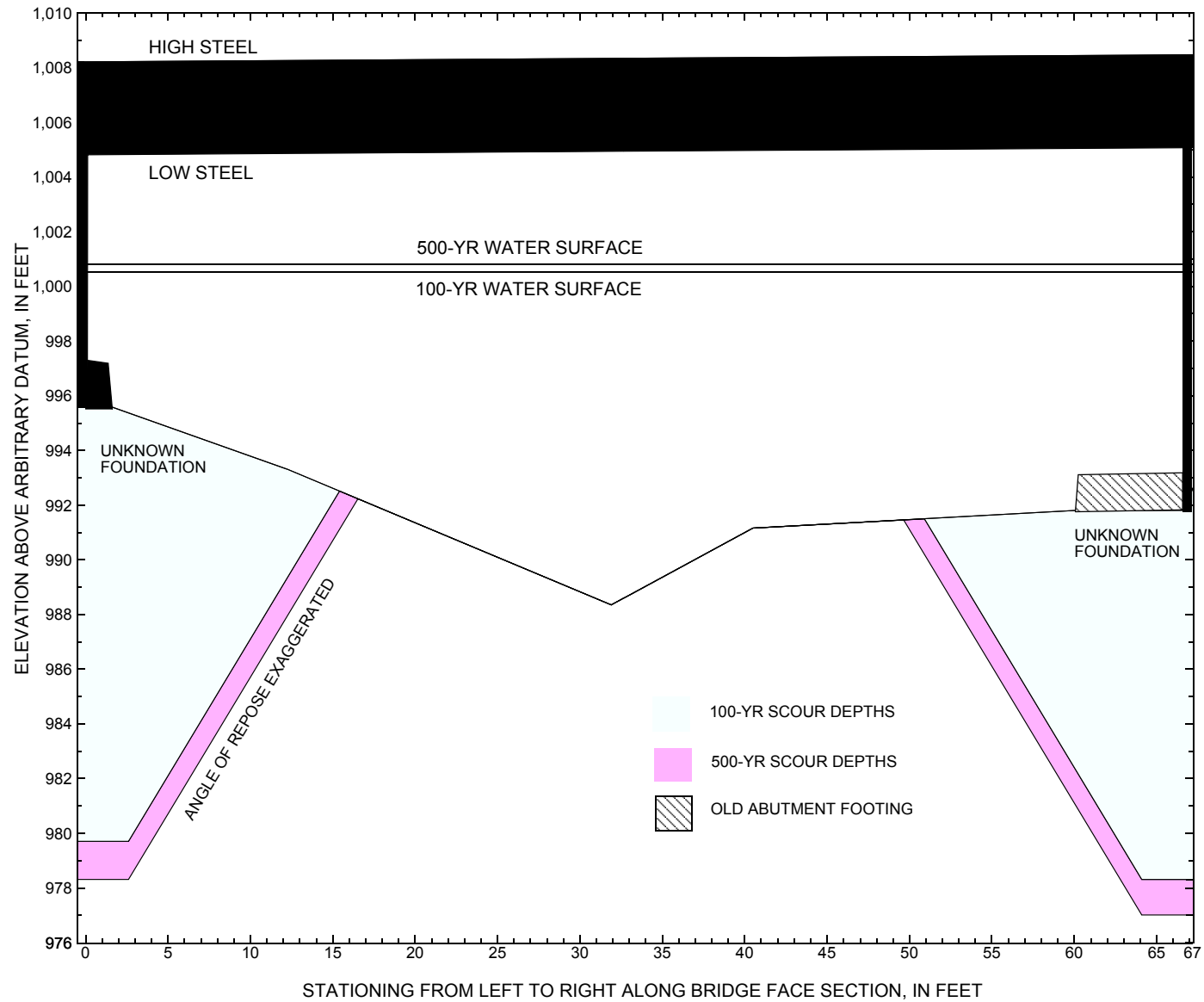


Figure 8. Scour elevations for the 100-yr and 500-yr discharges at structure [IRASTH00080020](#) on town highway 8, crossing the [Black River, Irasburg, Vermont](#).

Table 1. Remaining footing/pile depth at abutments for the 100-year discharge at structure [IRASTH00080020](#) on [Town Highway 8](#), crossing [the Black River](#), [Irasburg](#), Vermont.

[VTAOT, Vermont Agency of Transportation; --, no data]

Description	Station ¹	VTAOT minimum low-chord elevation (feet)	Surveyed minimum low-chord elevation ² (feet)	Bottom of footing elevation ² (feet)	Channel elevation at abutment/pier ² (feet)	Contraction scour depth (feet)	Abutment scour depth (feet)	Pier scour depth (feet)	Depth of total scour (feet)	Elevation of scour ² (feet)	Remaining footing/pile depth (feet)
100-yr. discharge is 3,800 cubic-feet per second											
Left abutment	0.0	739.4	1004.8	--	995.6	0.0	15.9	--	15.9	979.7	--
Right abutment	66.7	--	1005.3	--	991.8	0.0	13.5	--	13.5	978.3	--

¹. Measured along the face of the most constricting side of the bridge.

². Arbitrary datum for this study.

Table 2. Remaining footing/pile depth at abutments for the 500-year discharge at structure [IRASTH00080020](#) on [Town Highway 8](#), crossing [the Black River](#), [Irasburg](#), Vermont.

[VTAOT, Vermont Agency of Transportation; --, no data]

Description	Station ¹	VTAOT minimum low-chord elevation (feet)	Surveyed minimum low-chord elevation ² (feet)	Bottom of footing elevation ² (feet)	Channel elevation at abutment/pier ² (feet)	Contraction scour depth (feet)	Abutment scour depth (feet)	Pier scour depth (feet)	Depth of total scour (feet)	Elevation of scour ² (feet)	Remaining footing/pile depth (feet)
500-yr. discharge is 4,460 cubic-feet per second											
Left abutment	0.0	739.4	1004.8	--	995.6	0.0	17.3	--	17.3	978.3	--
Right abutment	66.7	--	1005.3	--	991.8	0.0	14.8	--	14.8	977.0	--

¹. Measured along the face of the most constricting side of the bridge.

². Arbitrary datum for this study.

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- Shearman, J.O., Kirby, W.H., Schneider, V.R., and Flippo, H.N., 1986, Bridge waterways analysis model; research report: Federal Highway Administration Publication FHWA-RD-86-108, 112 p.
- U.S. Department of Transportation, 1993, Stream stability and scour at highway bridges, Participant Workbook: Federal Highway Administration Publication FHWA HI-91-011.
- [U.S. Geological Survey, 1986, Irasburg, Vermont 7.5 Minute Series quadrangle map: U.S. Geological Survey Topographic Maps, Scale 1:24,000.](#)

APPENDIX A:

WSPRO INPUT FILE

WSPRO INPUT FILE

```

T1      U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE iras020.wsp
T2      CREATED ON 19-APR-95 FOR BRIDGE IRASTH00080020 USING FILE iras020.dca
T3      HYDRAULIC ANALYSIS OF IRAS020 OVER THE BLACK RIVER IN COVENTRY, VT
*
J3      6 29 30 552 553 551 5 16 17 13 3 * 15 14 23 21 11 12 4 7 3
*
*      Discharges from the log Pearson type 3 analysis of
*      gage data from station 04296000 Black River at Coventry, VT
*      and adjusted by drainage area relationship
*
Q      3800 4460
SK      0.0005 0.0005
*
*      Valley slope determined from survey data between exit and appr.
*
*      Since EXIT1 had been surveyed through as deep section, EXIT2 was
*      surveyed. EXIT2 consisted of only the channel geometry so the
*      overbank sections of EXIT1 were appended to EXIT2. EXIT2 is
*      shallower and better represents the river for starting
*      step-backwater analysis.
*
XS      EXIT2      -121
GR      0.0,1003.48      23.1,1001.22      23.6,1001.21      72.6,1000.11
GR      141.3, 997.90      207.0, 997.05      267.6, 996.96      318.7, 996.93
GR      376.9, 999.11      399.7, 999.16      418.6,1000.46      484.1, 999.68
GR      577.6, 998.80      594.0, 993.34      599.4, 992.04      614.3, 992.88
GR      629.2, 991.94      654.9, 993.15      671.7, 998.80      686.7,1001.08
GR      704.0,1006.87      723.8,1006.58      727.8,1006.03      732.3,1008.24
N      0.035 0.045 0.045
SA      577.6 671.7
*
XS      EXIT1      -39
GR      0.0,1003.48      23.1,1001.22      23.6,1001.21      72.6,1000.11
GR      141.3, 997.90      207.0, 997.05      267.6, 996.96      318.7, 996.93
GR      376.9, 999.11      399.7, 999.16      418.6,1000.46      484.1, 999.68
GR      577.6, 998.80      594.0, 993.34      607.3, 990.96      616.7, 988.99
GR      621.6, 989.24      628.5, 990.37      637.5, 991.82      648.9, 993.19
GR      665.7, 998.80      680.7,1001.08      698.0,1006.87      717.8,1006.58
GR      721.8,1006.03      726.3,1008.24
N      0.035 0.045 0.045
SA      577.6 665.7
*
XS      FULLV      0 * * * 0.002
*
BR      BRIDG      0 1005.1 25.0
GR      0.0,1004.77      0.0,997.23      1.3, 997.28      1.5, 995.61
GR      12.2, 993.32      31.9, 988.35      40.5, 991.16      60.2, 991.81
GR      60.4, 993.12      66.6, 993.22      66.7,1005.34      0.0,1004.77
CD      1 27 * 1008 45 0
N      0.040
*
XR      RDWAY      10 22 2

```

WSPRO INPUT FILE (continued)

GR	0.0,1007.01	73.5,1004.89	170.1,1004.47	256.1,1003.55
GR	355.2,1003.22	460.6,1002.68	499.9,1003.21	567.1,1005.99
GR	594.5,1007.29	623.4,1008.17	673.2,1007.90	710.0,1008.55
GR	727.3,1008.27	753.8,1007.54	756.0,1005.87	762.6,1013.47
BP	623.4			
*				

AS	APPR1	110			
GR		-553.7,1007.0	-480.2,1004.9	-383.6,1004.5	
GR		-297.6,1003.6	-198.5, 1003.2	-93.1, 1002.7	-53.8, 1003.2
GR		0.0,1004.85	18.0, 999.24	36.0, 998.65	40.7, 996.15
GR		52.7, 993.38	72.8, 992.14	79.5, 992.05	99.7, 992.15
GR		120.1, 993.36	128.6, 995.55	158.9, 996.72	183.3, 995.95
GR		209.1, 998.97	263.1,1003.54	291.8,1012.07	
N		0.065 0.045 0.095			
SA		36.0 128.6			
BP		40.7			
*					

HP	1	BRIDG	1000.54	1	1000.54
HP	2	BRIDG	1000.54	*	* 3800
HP	1	APPR1	1001.65	1	1001.65
HP	2	APPR1	1001.65	*	* 3800

*

HP	1	BRIDG	1000.81	1	1000.81
HP	2	BRIDG	1000.81	*	* 4460
HP	1	APPR1	1002.26	1	1002.26
HP	2	APPR1	1002.26	*	* 4460

*

EX
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APPENDIX B:

WSPRO OUTPUT FILE

WSPRO OUTPUT FILE

U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE iras020.wsp
 CREATED ON 19-APR-95 FOR BRIDGE IRASTH00080020 USING FILE iras020.dca
 HYDRAULIC ANALYSIS OF IRAS020 OVER THE BLACK RIVER IN COVENTRY, VT

*** RUN DATE & TIME: 04-20-95 14:45

CROSS-SECTION PROPERTIES: ISEQ = 4; SECID = BRIDG; SRD = 0.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	526.	71649.	60.	75.				8797.
1000.54		526.	71649.	60.	75.	1.00	0.	67.	8797.

VELOCITY DISTRIBUTION: ISEQ = 4; SECID = BRIDG; SRD = 0.

WSEL	LEW	REW	AREA	K	Q	VEL
1000.54	0.0	66.7	525.6	71649.	3800.	7.23

X STA.	0.0	9.1	14.0	17.8	20.8	23.5
A(I)	44.0	31.5	27.9	25.1	23.9	
V(I)	4.32	6.04	6.81	7.57	7.96	

X STA.	23.5	26.0	28.2	30.2	32.2	34.1
A(I)	23.0	22.2	21.3	20.9	21.1	
V(I)	8.25	8.55	8.92	9.11	9.00	

X STA.	34.1	36.3	38.7	41.3	44.1	46.8
A(I)	21.3	22.5	22.7	23.5	23.2	
V(I)	8.92	8.43	8.35	8.07	8.19	

X STA.	46.8	49.8	52.8	56.1	59.8	66.7
A(I)	24.2	25.1	26.3	29.6	46.2	
V(I)	7.84	7.58	7.21	6.42	4.11	

CROSS-SECTION PROPERTIES: ISEQ = 6; SECID = APPR1; SRD = 110.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	58.	2264.	26.	26.				494.
	2	781.	106125.	93.	94.				12866.
	3	447.	17610.	112.	112.				5069.
1001.65		1286.	125999.	231.	232.	1.65	10.	241.	13435.

VELOCITY DISTRIBUTION: ISEQ = 6; SECID = APPR1; SRD = 110.

WSEL	LEW	REW	AREA	K	Q	VEL
1001.65	10.3	240.8	1286.2	125999.	3800.	2.95

X STA.	10.3	44.9	52.3	58.0	63.2	68.2
A(I)	103.1	53.9	48.2	46.1	45.0	
V(I)	1.84	3.53	3.94	4.12	4.22	

X STA.	68.2	72.9	77.4	81.9	86.4	90.9
A(I)	43.9	42.8	43.4	42.8	42.7	
V(I)	4.32	4.44	4.38	4.44	4.45	

X STA.	90.9	95.3	99.8	104.4	109.3	114.4
A(I)	42.5	42.4	43.7	43.7	45.2	
V(I)	4.47	4.48	4.35	4.35	4.20	

X STA.	114.4	119.8	126.7	147.5	175.2	240.8
A(I)	46.0	51.3	120.5	143.1	195.8	
V(I)	4.13	3.71	1.58	1.33	0.97	

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*** RUN DATE & TIME: 04-20-95 14:45

CROSS-SECTION PROPERTIES: ISEQ = 4; SECID = BRIDG; SRD = 0.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	542.	75035.	60.	76.				9210.
1000.81		542.	75035.	60.	76.	1.00	0.	67.	9210.

VELOCITY DISTRIBUTION: ISEQ = 4; SECID = BRIDG; SRD = 0.

WSEL	LEW	REW	AREA	K	Q	VEL
1000.81	0.0	66.7	541.9	75035.	4460.	8.23

X STA.	0.0	9.1	13.8	17.6	20.7	23.4
A(I)	46.2	31.2	28.9	26.0	24.7	
V(I)	4.83	7.15	7.71	8.59	9.04	

X STA.	23.4	25.9	28.1	30.2	32.1	34.1
A(I)	23.8	22.9	21.9	21.5	21.8	
V(I)	9.38	9.73	10.16	10.38	10.22	

X STA.	34.1	36.3	38.6	41.2	44.0	46.8
A(I)	22.2	22.8	23.4	24.2	23.9	
V(I)	10.04	9.78	9.52	9.20	9.33	

X STA.	46.8	49.8	52.8	56.1	59.8	66.7

WSPRO OUTPUT FILE (continued)

A(I)	25.0	25.9	27.2	30.5	48.0
V(I)	8.93	8.62	8.21	7.30	4.65

CROSS-SECTION PROPERTIES: ISEQ = 6; SECID = APPR1; SRD = 110.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	74.	3252.	28.	28.				691.
	2	837.	119226.	93.	94.				14287.
	3	518.	21568.	119.	120.				6122.
1002.26		1430.	144047.	240.	242.	1.68	8.	248.	15273.

VELOCITY DISTRIBUTION: ISEQ = 6; SECID = APPR1; SRD = 110.

	WSEL	LEW	REW	AREA	K	Q	VEL
	1002.26	8.3	248.0	1429.6	144047.	4460.	3.12
X STA.		8.3	43.5	51.3	57.2	62.6	67.7
A(I)		115.4	59.7	52.8	50.5	49.3	
V(I)		1.93	3.73	4.23	4.41	4.53	
X STA.		67.7	72.7	77.3	81.9	86.5	91.0
A(I)		48.9	46.6	47.2	46.6	46.5	
V(I)		4.56	4.78	4.72	4.78	4.79	
X STA.		91.0	95.7	100.4	105.1	110.1	115.5
A(I)		47.2	47.1	46.8	48.9	49.9	
V(I)		4.73	4.74	4.77	4.56	4.47	
X STA.		115.5	121.1	128.4	151.6	178.1	248.0
A(I)		50.7	56.2	145.3	153.8	220.2	
V(I)		4.40	3.97	1.53	1.45	1.01	

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 HYDRAULIC ANALYSIS OF IRAS020 OVER THE BLACK RIVER IN COVENTRY, VT
 *** RUN DATE & TIME: 04-20-95 14:45

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
	SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL
EXIT2:XS	*****	40.	1895.	0.08	*****	1000.92	997.97	3800.	1000.84
-121.	*****	685.	169776.	1.21	*****	*****	0.23	2.01	
EXIT1:XS	82.	38.	1948.	0.07	0.04	1000.96	*****	3800.	1000.88
-39.	82.	679.	181936.	1.26	0.00	0.00	0.22	1.95	
FULLV:FV	39.	41.	1909.	0.08	0.02	1000.98	*****	3800.	1000.90
0.	39.	679.	177071.	1.27	0.00	0.00	0.23	1.99	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS.
 "APPR1" KRATIO = 0.59

APPR1:AS	110.	13.	1113.	0.29	0.09	1001.17	*****	3800.	1000.88
110.	110.	232.	104927.	1.60	0.11	0.00	0.34	3.41	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

<<<<RESULTS REFLECTING THE CONSTRICTED FLOW FOLLOW>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
	SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL
BRIDG:BR	39.	0.	526.	1.12	0.04	1001.66	996.78	3800.	1000.54
0.	39.	67.	71644.	1.38	0.66	0.00	0.51	7.23	

TYPE	PCPD FLOW	C	P/A	LSEL	BLEN	XLAB	XRAB
1.	****	1.	0.853	*****	1005.10	*****	*****

XSID:CODE	SRD	FLEN	HF	VHD	EGL	ERR	Q	WSEL
RDWAY:RG	10.							

<<<<EMBANKMENT IS NOT OVERTOPPED>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
	SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL
APPR1:AS	83.	10.	1287.	0.22	0.14	1001.88	997.05	3800.	1001.65
110.	90.	241.	126097.	1.65	0.08	0.01	0.28	2.95	

WSPRO OUTPUT FILE (continued)

M(G) M(K) KQ XLKQ XRKQ OTEL
0.695 0.301 87927. 56. 123. 1001.57

<<<<END OF BRIDGE COMPUTATIONS>>>>

FIRST USER DEFINED TABLE.

XSID:CODE	SRD	LEW	REW	Q	K	AREA	VEL	WSEL
EXIT2:XS	-121.	40.	685.	3800.	169776.	1895.	2.01	1000.84
EXIT1:XS	-39.	38.	679.	3800.	181936.	1948.	1.95	1000.88
FULLV:FV	0.	41.	679.	3800.	177071.	1909.	1.99	1000.90
BRIDG:BR	0.	0.	67.	3800.	71644.	526.	7.23	1000.54
RDWAY:RG	10.	*****		0.	*****		2.00	*****
APPR1:AS	110.	10.	241.	3800.	126097.	1287.	2.95	1001.65
XSID:CODE	XLKQ	XRKQ	KQ					
APPR1:AS	56.	123.	87927.					

SECOND USER DEFINED TABLE.

XSID:CODE	CRWS	FR#	YMIN	YMAX	HF	HO	VHD	EGL	WSEL
EXIT2:XS	997.97	0.23	991.94	1008.24	*****		0.08	1000.92	1000.84
EXIT1:XS	*****	0.22	988.99	1008.24	0.04	0.00	0.07	1000.96	1000.88
FULLV:FV	*****	0.23	989.07	1008.32	0.02	0.00	0.08	1000.98	1000.90
BRIDG:BR	996.78	0.51	988.35	1005.34	0.04	0.66	1.12	1001.66	1000.54
RDWAY:RG	*****		1002.68	1013.47	*****				
APPR1:AS	997.05	0.28	992.05	1012.07	0.14	0.08	0.22	1001.88	1001.65

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XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
EXIT2:XS	*****	24.	2125.	0.08	*****	1001.27	998.24	4460.	1001.19
-121.	*****	687.	199299.	1.17	*****	*****	0.22	2.10	
EXIT1:XS	82.	23.	2177.	0.08	0.04	1001.31	*****	4460.	1001.24
-39.	82.	681.	211837.	1.22	0.00	0.00	0.22	2.05	
FULLV:FV	39.	25.	2137.	0.08	0.02	1001.34	*****	4460.	1001.25
0.	39.	681.	206515.	1.22	0.00	0.00	0.23	2.09	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS.

"APPR1" KRATIO = 0.55

APPR1:AS	110.	12.	1186.	0.36	0.09	1001.56	*****	4460.	1001.21
110.	110.	236.	113677.	1.62	0.14	0.00	0.37	3.76	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

<<<<RESULTS REFLECTING THE CONSTRICTED FLOW FOLLOW>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
BRIDG:BR	39.	0.	542.	1.44	0.05	1002.25	997.38	4460.	1000.81
0.	39.	67.	75041.	1.37	0.89	0.00	0.57	8.23	

TYPE	PPCD	FLOW	C	P/A	LSEL	BLEN	XLAB	XRAB
1.	****	1.	0.855	*****	1005.10	*****	*****	*****

XSID:CODE	SRD	FLEN	HF	VHD	EGL	ERR	Q	WSEL
RDWAY:RG	10.							

<<<<EMBANKMENT IS NOT OVERTOPPED>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
APPR1:AS	83.	8.	1429.	0.25	0.17	1002.51	997.48	4460.	1002.26
110.	90.	248.	143933.	1.68	0.10	0.00	0.29	3.12	

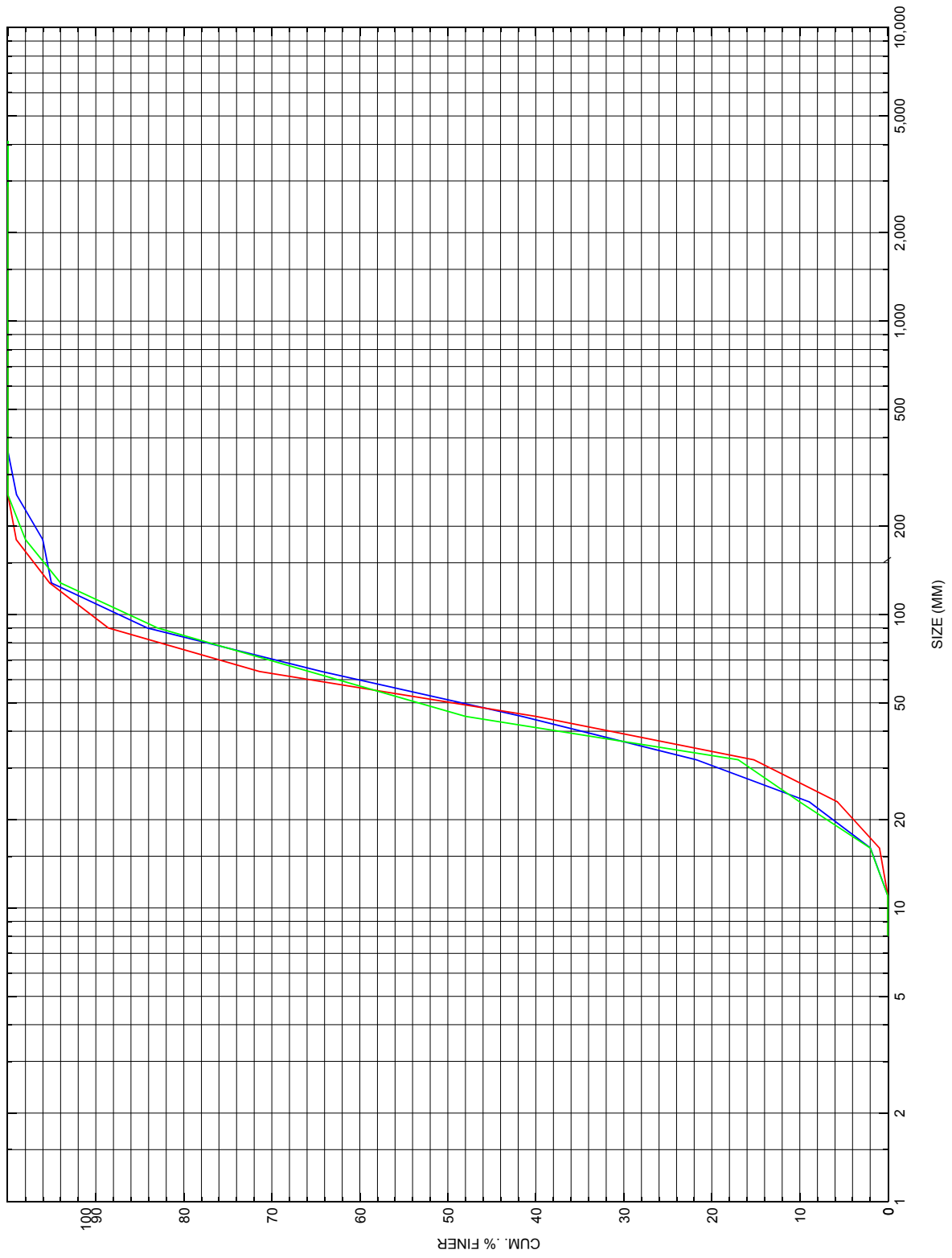
M(G) M(K) KQ XLKQ XRKQ OTEL
0.702 0.319 97945. 57. 123. 1002.17

<<<<END OF BRIDGE COMPUTATIONS>>>>

U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE iras020.wsp
CREATED ON 19-APR-95 FOR BRIDGE IRASTH00080020 USING FILE iras020.dca

APPENDIX C:

BED-MATERIAL PARTICAL-SIZE DISTRIBUTION



Appendix C. Bed material particle-size distribution at the approach cross-section for structure [IRASTH00080020](#), in [Irasburg](#), Vermont.

APPENDIX D:
HISTORICAL DATA FORM