

LEVEL II SCOUR ANALYSIS FOR BRIDGE 26 (BRIDTH00340026) on TOWN HIGHWAY 34, crossing OTTAUQUECHEE RIVER, BRIDGEWATER, VERMONT

U.S. Geological Survey
Open-File Report 96-157

Prepared in cooperation with
VERMONT AGENCY OF TRANSPORTATION
and
FEDERAL HIGHWAY ADMINISTRATION



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By ERICK M. BOEHMLER

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Pembroke, New Hampshire

1996

U.S. DEPARTMENT OF THE INTERIOR
BRUCE BABBITT, Secretary

U.S. GEOLOGICAL SURVEY
Gordon P. Eaton, Director

For additional information
write to:

District Chief
U.S. Geological Survey
361 Commerce Way
Pembroke, NH 03304

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CONVERSION FACTORS, ABBREVIATIONS, AND VERTICAL DATUM

Multiply	By	To obtain
Length		
inch (in.)	25.4	millimeter (mm)
foot (ft)	0.3048	meter (m)
mile (mi)	1.609	kilometer (km)
Slope		
foot per mile (ft/mi)	0.1894	meter per kilometer (m/km)
Area		
square mile (mi ²)	2.590	square kilometer (km ²)
Volume		
cubic foot (ft ³)	0.02832	cubic meter (m ³)
Velocity and Flow		
foot per second (ft/s)	0.3048	meter per second (m/s)
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second (m ³ /s)
cubic foot per second per square mile [(ft ³ /s)/mi ²]	0.01093	cubic meter per second per square kilometer [(m ³ /s)/km ²]

OTHER ABBREVIATIONS

BF	bank full	LWW	left wingwall
cfs	cubic feet per second	MC	main channel
D ₅₀	median diameter of bed material	RAB	right abutment
DS	downstream	RABUT	face of right abutment
elev.	elevation	RB	right bank
f/p	flood plain	ROB	right overbank
ft ²	square feet	RWW	right wingwall
ft/ft	feet per foot	TH	town highway
JCT	junction	UB	under bridge
LAB	left abutment	US	upstream
LABUT	face of left abutment	USGS	United States Geological Survey
LB	left bank	VT AOT	Vermont Agency of Transportation
LOB	left overbank	WSPRO	water-surface profile model

In this report, the words “right” and “left” refer to directions that would be reported by an observer facing downstream.

Sea level: In this report, “sea level” refers to the National Geodetic Vertical Datum of 1929-- a geodetic datum derived from a general adjustment of the first-order level nets of the United States and Canada, formerly called Sea Level Datum of 1929.

In the appendices, the above abbreviations may be combined. For example, USLB would represent upstream left bank.

LEVEL II SCOUR ANALYSIS FOR BRIDGE 26 (BRIDTH00340026) ON TOWN HIGHWAY 34, CROSSING OTTAUQUECHEE RIVER, BRIDGEWATER, VERMONT

By Erick M. Boehmler

INTRODUCTION

This report provides the results of a detailed Level II analysis of scour potential at structure BRIDTH00340026 on town highway 34 crossing the Ottauquechee River, Bridgewater, Vermont (figures 1–8). A Level II study is a basic engineering analysis of the site, including a quantitative analysis of stream stability and scour (U.S. Department of Transportation, 1993). A Level I study is included in Appendix E of this report. A Level I study provides a qualitative geomorphic characterization of the study site. Information on the bridge available from VTAOT files were compiled prior to conducting Level I and Level II analyses and can be found in Appendix D.

The site is in the Green Mountain physiographic province of central Vermont in the town of Bridgewater. The 38.0-mi² drainage area is in a predominantly rural and forested basin. In the vicinity of the study site, the banks have dense woody vegetation coverage except for the upstream right bank, which is grass covered.

In the study area, the Ottauquechee River has an incised, sinuous channel with a slope of approximately 0.01 ft/ft, an average channel top width of 62.5 ft and an average channel depth of 4.5 ft. The predominant channel bed material is cobble (D_{50} is 97.3 mm or 0.319 ft). The geomorphic assessment at the time of the Level I and Level II site visit on November 8, 1994, indicated that the reach was stable.

The town highway 34 crossing of the [Ottauquechee River](#) is a 69-ft-long, [two-lane](#) bridge consisting of [one 63-foot clear-span steel-pony truss-type superstructure](#) ([Vermont Agency of Transportation, written commun., August 24, 1994](#)). The bridge is supported by [vertical, concrete](#) abutments with [wingwalls](#). The channel is skewed approximately 40 degrees to the opening while the opening-skew-to-roadway is 45 degrees.

A scour hole 4.5 ft deeper than the mean thalweg depth was observed along the upstream left wingwall during the Level I assessment. The only scour protection measure at the site was type-1 stone fill (less than 12 inches diameter) at the upstream end of the upstream left wingwall. Additional details describing conditions at the site are included in the Level II Summary and Appendices D and E.

Scour depths were computed using the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993). These guidelines provide scour equations, which assume an infinite depth of erosive material and a homogeneous particle-size distribution. The scour analysis results are presented in tables 1 and 2 and a graph of the scour depths is presented in figure 8.

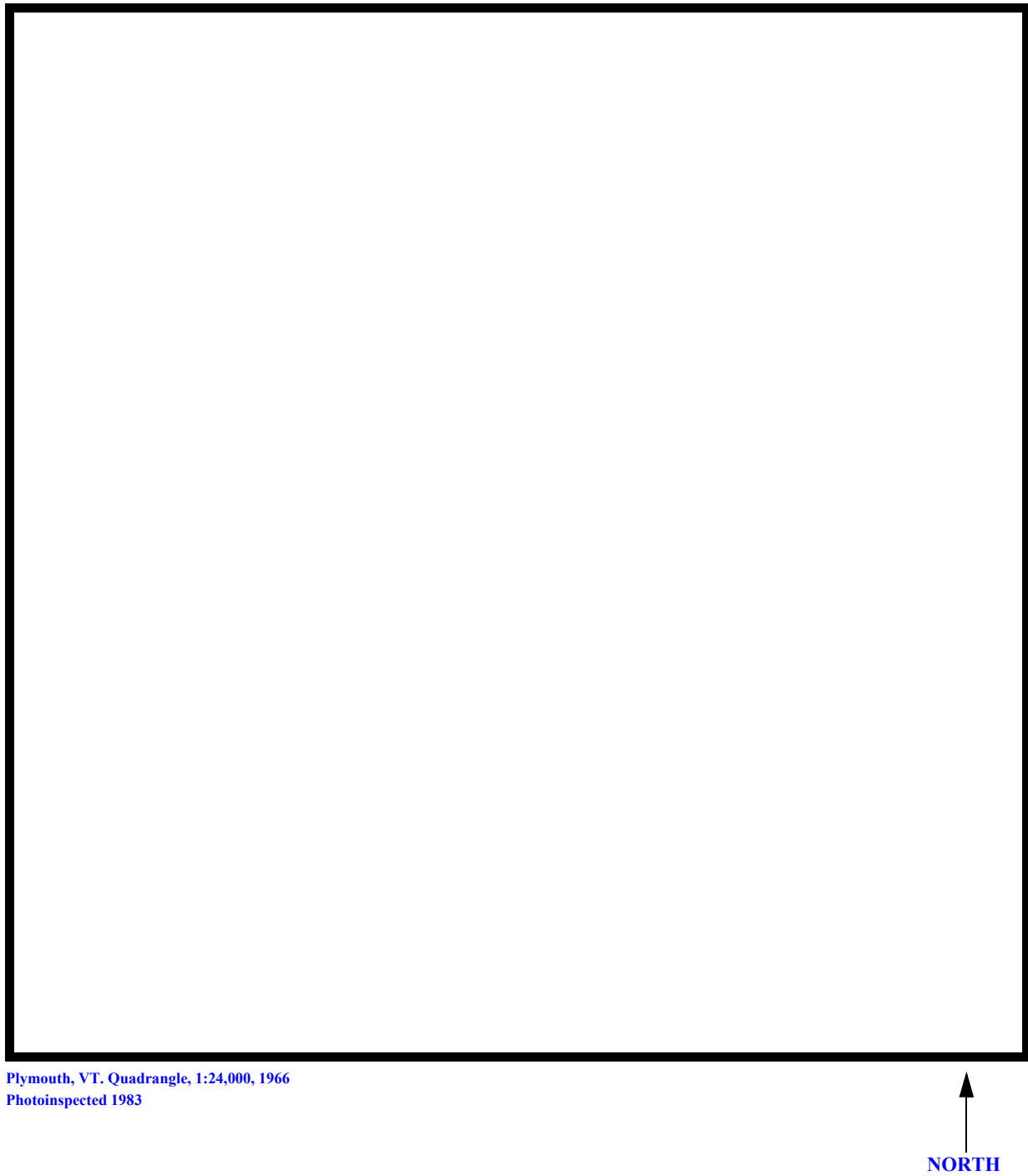


Figure 1. Location of study area on USGS 1:24,000 scale map.

Figure 2. Location of study area on Vermont Agency of Transportation town highway map.





LEVEL II SUMMARY

Structure Number BRIDTH00340026 **Stream** Ottauquechee River
County Windsor **Road** TH034 **District** 04

Description of Bridge

Bridge length 69 **ft** **Bridge width** 21.1 **ft** **Max span length** 63 **ft**
Alignment of bridge to road (on curve or straight) Curve
Abutment type Vertical **Embankment type** Sloping
Stone fill on abutment? No **Date of inspection** 11/08/94
Description of stone fill Type-1, around the upstream end of the upstream left wingwall in good condition.

Abutments and wingwalls are concrete. There is a three to four foot deep scour hole in front of the upstream left wingwall.

Is bridge skewed to flood flow according to Y **' survey?** 40 **Angle**
There is a mild channel bend in the upstream reach. The scour hole has developed in the location where the bend impacts the upstream left wingwall.

Debris accumulation on bridge at time of Level I or Level II site visit:

	Date of inspection	Percent of channel blocked horizontally	Percent of channel blocked vertically
Level I	<u>11/08/94</u>	<u>0</u>	<u>0</u>
Level II	<u>11/08/94</u>	<u>--</u>	<u>--</u>
Potential for debris	<u>Moderate. There is some debris caught on boulders and trees leaning over the channel upstream.</u>		

A large pile of boulders on the upstream left bank set up an eddy current at the upstream left wingwall resulting in a significant scour hole as of 11/08/94.
Describe any features near or at the bridge that may affect flow (include observation date)

Description of the Geomorphic Setting

General topography The channel is located within a 280 foot-wide, flat to slightly irregular flood plain with steep valley walls on both sides.

Geomorphic conditions at bridge site: downstream (DS), upstream (US)

Date of inspection 11/08/95

DS left: Steep channel bank to a narrow terrace

DS right: Narrow flood plain

US left: Steep valley wall

US right: Moderately sloped overbank

Description of the Channel

Average top width 62.5 **Average depth** 4.5
Gravel / Cobbles Gravel/Cobbles

Predominant bed material **Bank material** Sinuuous but stable
with semi-alluvial to non-alluvial channel boundaries and a narrow flood plain.

Vegetative cover 11/08/95
Trees and brush

DS left: Trees and brush

DS right: Trees

US left: Short grass and brush with a few trees.

US right: Y

Do banks appear stable? - if not, describe location and type of instability and date of observation.

The assessment of 11/8/95 noted flow conditions up to bank-full level are influenced by a pile of boulders on the left bank side of the channel upstream. In addition, some debris is caught on boulders in the channel upstream.

Hydrology

Drainage area 38.0 mi^2

Percentage of drainage area in physiographic provinces: (approximate)

Physiographic province	Percent of drainage area
<u>Green Mountain</u>	<u>100</u>

Is drainage area considered rural or urban? Rural Describe any significant urbanization: There are a couple houses and a motor lodge on the upstream right overbank area

Is there a USGS gage on the stream of interest? Yes
Ottauquechee River near W. Bridgewater

USGS gage description 01150900

USGS gage number 23.4

Gage drainage area mi^2 No

Is there a lake? No

	Calculated Discharges	
<u>8,030</u>	<u>11,600</u>	
Q_{100}	Q_{500}	ft^3/s

The 100- and 500-year discharges are based on a drainage area relationship $[(38.0/41.9)^{\text{exp } 0.7}]$ with bridge number 48 in Bridgewater. Bridge number 48 crosses the Ottauquechee River downstream of this site and has flood frequency estimates available from the VTAOT database. The drainage area above bridge number 48 is 41.9 square miles.

Description of the Water-Surface Profile Model (WSPRO) Analysis

Datum for WSPRO analysis (USGS survey, sea level, VTAOT plans) USGS survey

Datum tie between USGS survey and VTAOT plans None

Description of reference marks used to determine USGS datum. RM1 is a chiseled X on top of the DS end of the left abutment (elev. 507.54 ft, arbitrary datum). RM2 is a chiseled X on top of the US end of the right abutment (elev. 507.57ft, arbitrary datum).

Cross-Sections Used in WSPRO Analysis

¹ <i>Cross-section</i>	<i>Section Reference Distance (SRD) in feet</i>	² <i>Cross-section development</i>	<i>Comments</i>
EXITX	-64	1	Exit section
FULLV	0	2	Downstream Full-valley section (Templated from EXITX)
BRIDG	0	1	Bridge section
RDWAY	20.8	1	Road Grade section
APPRO	82	2	Modelled Approach section (Templated from SURVA)
SURVA	132	1	Approach section as surveyed (Used as a template)

¹ For location of cross-sections see plan-view plot included with Level I field form, Appendix E.
For more detail on how cross-sections were developed see WSPRO input file.

Data and Assumptions Used in WSPRO Model

Hydraulic analyses of the reach were done by use of the Federal Highway Administration's WSPRO step-backwater computer program (Shearman and others, 1986, and Shearman, 1990). Results of the hydraulic model are presented in the Bridge Hydraulic Summary, Appendix B, and figure 7.

Channel roughness factors (Manning's "n") used in the hydraulic model were estimated using field inspections at each cross section following the general guidelines described by Arcement, Jr. and Schneider (1989). Final adjustments to the values were made during the modelling of the reach. Channel "n" values for the reach ranged from 0.040 to 0.060, and overbank "n" values ranged from 0.040 to 0.095.

Normal depth at the exit section (EXITX) was assumed as the starting water surface. This depth was computed by use of the slope-conveyance method outlined in the User's manual for WSPRO (Shearman, 1990). The slope used was 0.0095 ft/ft which was estimated from the topographic map (U.S. Geological Survey, 1966).

The surveyed approach section (SURVA) was moved along the approach channel slope (0.014 ft/ft) to establish the modelled approach section (APPRO), one bridge length upstream of the upstream face as recommended by Shearman and others (1986). This approach also provides a consistent method for determining scour variables.

The modeled 100- and 500-year discharges overtop the roadway embankments but not the bridge deck. The truss structure was assumed to collect debris, effectively blocking flow from passing over the deck.

Bridge Hydraulics Summary

Average bridge embankment elevation 510.4 ft
 Average low steel elevation 507.7 ft

100-year discharge 8,030 ft³/s
 Water-surface elevation in bridge opening 507.7 ft
 Road overtopping? Y Discharge over road 1,890 ft³/s
 Area of flow in bridge opening 466 ft²
 Average velocity in bridge opening 13.2 ft/s
 Maximum WSPRO tube velocity at bridge 15.6 ft/s

Water-surface elevation at Approach section with bridge 512.8
 Water-surface elevation at Approach section without bridge 509.5
 Amount of backwater caused by bridge 3.3 ft

500-year discharge 11,600 ft³/s
 Water-surface elevation in bridge opening 507.7 ft
 Road overtopping? Y Discharge over road 5,490 ft³/s
 Area of flow in bridge opening 466 ft²
 Average velocity in bridge opening 13.1 ft/s
 Maximum WSPRO tube velocity at bridge 15.6 ft/s

Water-surface elevation at Approach section with bridge 514.7
 Water-surface elevation at Approach section without bridge 511.3
 Amount of backwater caused by bridge 3.4 ft

Incipient overtopping discharge 4,850 ft³/s
 Water-surface elevation in bridge opening 505.1 ft
 Area of flow in bridge opening 359 ft²
 Average velocity in bridge opening 13.5 ft/s
 Maximum WSPRO tube velocity at bridge 16.8 ft/s

Water-surface elevation at Approach section with bridge 508.1
 Water-surface elevation at Approach section without bridge 507.1
 Amount of backwater caused by bridge 1.0 ft

Scour Analysis Summary

Special Conditions or Assumptions Made in Scour Analysis

Scour depths were computed using the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution. The results of the scour analysis are presented in tables 1 and 2 and a graph of the scour depths is presented in figure 8.

The 100-year and 500-year discharges resulted in submerged orifice flow. Contraction scour at bridges with orifice flow is best estimated by use of the Chang pressure-flow scour equation (oral communication, J. Sterling Jones, October 4, 1996). Therefore, contraction scour for the 100-year and 500-year discharges was computed by use of the Chang equation (Richardson and others, 1995, p. 145-146). Contraction scour was computed by use of the clear-water contraction scour equation (Richardson and others, 1993, p. 35, equation 18) for the incipient road-overflow discharges. For contraction scour computations using the Laursen's equation, the average depth in the contracted section (AREA/TOPWIDTH) is subtracted from the depth of flow computed by the scour equation (Y2) to determine the actual amount of scour. The 500-year model resulted in the worst case contraction and total scour.

Abutment scour for the left abutment at all modelled discharges and the right abutment at the incipient overtopping discharge was computed by use of the Froehlich equation (Richardson and others, 1993, p. 49, equation 24). The Froehlich equation gives "excessively conservative estimates of scour depths" (Richardson and others, 1993, p. 48). Parameters for the Froehlich equation include the Froude number of the flow approaching the embankments, the length of the embankment blocking flow, and the depth of flow approaching the embankment less any roadway overtopping.

Scour at the right abutment for the 100- and 500-year discharges was computed by use of the HIRE equation (Richardson and others, 1993, p. 50, equation 25) because the HIRE equation is recommended when the length to depth ratio of the embankment blocking flow exceeds 25. Variables for the HIRE abutment scour equation are the same as the Froehlich abutment scour equation.

Scour Results

<i>Contraction scour:</i>	<i>100-yr discharge</i>	<i>500-yr discharge</i>	<i>Incipient overtopping discharge</i>
	<i>(Scour depths in feet)</i>		
<i>Main channel</i>			
<i>Live-bed scour</i>	--	--	--
<i>Clear-water scour</i>	2.7 2.9	1.2	9.3
<i>Depth to armoring</i>	9.1	16.3	--
<i>Left overbank</i>	--	--	--
<i>Right overbank</i>	--	--	24.8
<i>Local scour:</i>			
<i>Abutment scour</i>	25.4	23.6	7.3
<i>Left abutment</i>	7.6	12.7	--
<i>Right abutment</i>			
<i>Pier scour</i>	--	--	--
<i>Pier 1</i>	--	--	--
<i>Pier 2</i>	--	--	4.5
<i>Pier 3</i>			

Rock Riprap Sizing

	<i>100-yr discharge</i>	<i>500-yr discharge</i>	<i>Incipient overtopping discharge</i>
	<i>(D₅₀ in feet)</i>		
<i>Abutments:</i>	4.5	3.5	4.5
<i>Left abutment</i>	4.5	3.5	--
<i>Right abutment</i>	--	--	--
<i>Piers:</i>	--	--	--
<i>Pier 1</i>	--	--	--
<i>Pier 2</i>	--	--	--

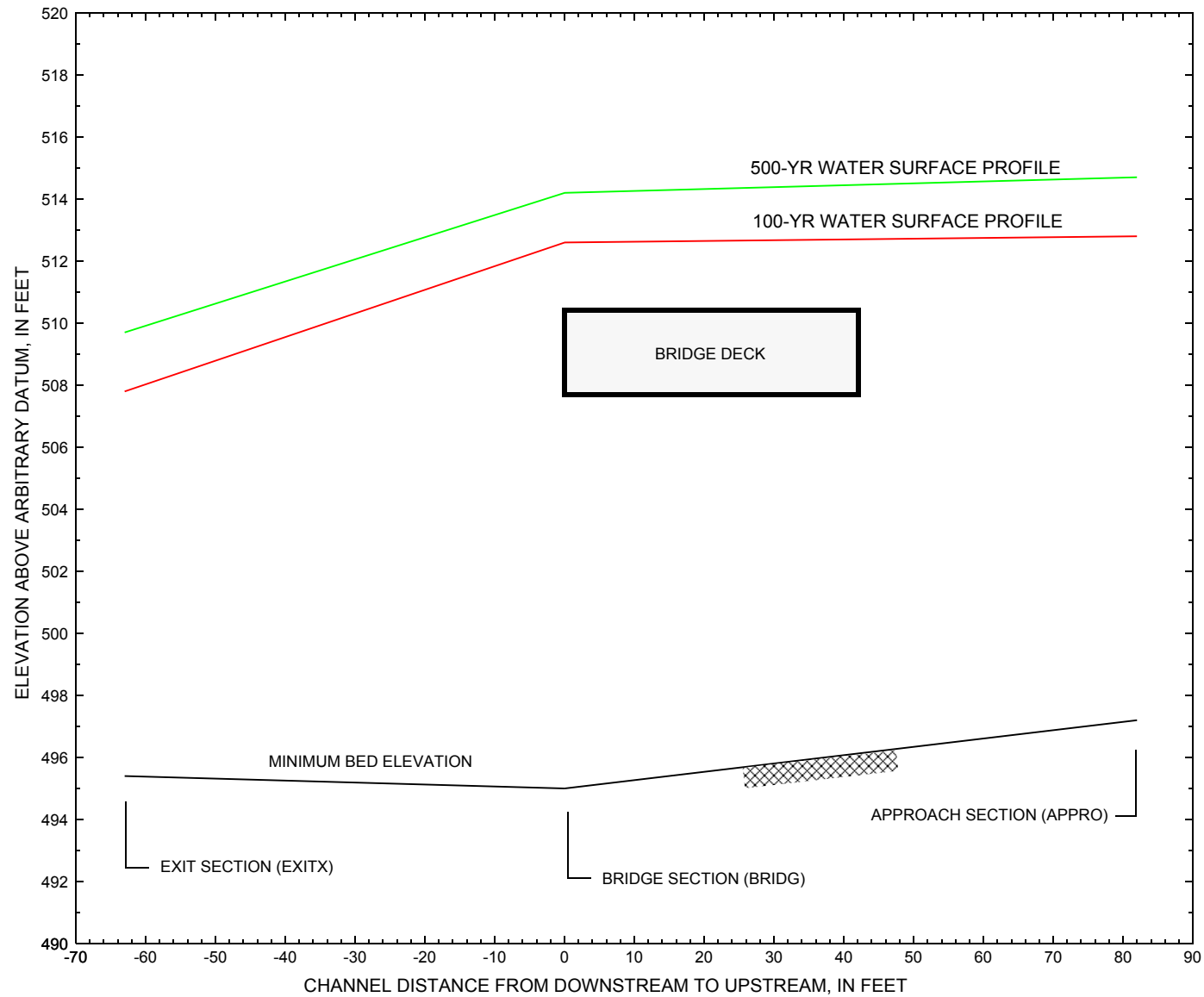


Figure 7. Water-surface profiles for the 100- and 500-yr discharges at structure [BRIDTH00340026](#) on town highway 34, crossing [Ottauquechee River, Bridgewater, Vermont](#).

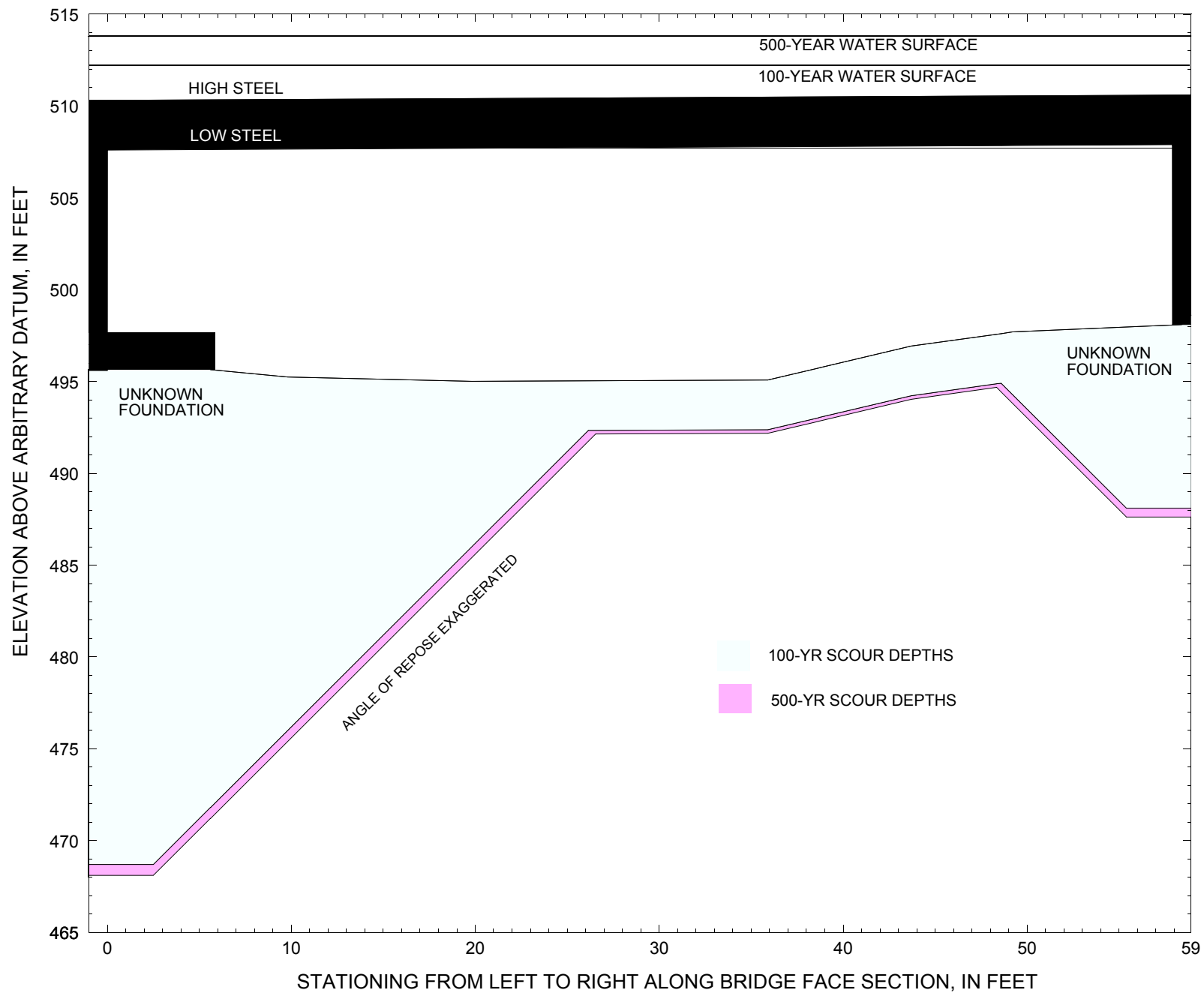


Figure 8. Scour elevations for the 100-yr and 500-yr discharges at structure [BRIDTH00340026](#) on town highway 34, crossing [Ottauquechee River, Bridgewater, Vermont](#).

Table 1. Remaining footing/pile depth at abutments for the 100-year discharge at structure [BRIDTH00340026](#) on [Town Highway 34](#), crossing [Ottauquechee River, Bridgewater](#), Vermont.

[VTAOT, Vermont Agency of Transportation; --, no data]

Description	Station ¹	VTAOT minimum low-chord elevation (feet)	Surveyed minimum low-chord elevation ² (feet)	Bottom of footing elevation ² (feet)	Channel elevation at abutment/pier ² (feet)	Contraction scour depth (feet)	Abutment scour depth (feet)	Pier scour depth (feet)	Depth of total scour (feet)	Elevation of scour ² (feet)	Remaining footing/pile depth (feet)
100-yr. discharge is 8,030 cubic-feet per second											
Left abutment	0	--	507.71	--	495.6	2.7	24.8	--	27.5	468.1	--
Right abutment	57.9	--	507.62	--	498.1	2.7	7.3	--	10.0	488.1	--

¹. Measured along the face of the most constricting side of the bridge.

². Arbitrary datum for this study.

Table 2. Remaining footing/pile depth at abutments for the 500-year discharge at structure [BRIDTH00340026](#) on [Town Highway 34](#), crossing [Ottauquechee River, Bridgewater](#), Vermont.

[VTAOT, Vermont Agency of Transportation; --, no data]

Description	Station ¹	VTAOT minimum low-chord elevation (feet)	Surveyed minimum low-chord elevation ² (feet)	Bottom of footing elevation ² (feet)	Channel elevation at abutment/pier ² (feet)	Contraction scour depth (feet)	Abutment scour depth (feet)	Pier scour depth (feet)	Depth of total scour (feet)	Elevation of scour ² (feet)	Remaining footing/pile depth (feet)
500-yr. discharge is 11,600 cubic-feet per second											
Left abutment	0	--	507.71	--	495.6	2.9	25.4	--	28.3	467.3	--
Right abutment	57.9	--	507.62	--	498.1	2.9	7.6	--	10.5	487.6	--

¹. Measured along the face of the most constricting side of the bridge.

². Arbitrary datum for this study.

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APPENDIX A:

WSPRO INPUT FILE

WSPRO INPUT FILE

```

T1      U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE brid0026.wsp
T2      CREATED ON 24-APR-95 FOR BRIDGE BRIDTH00340026 USING FILE brid0026.dca
T3      Ottauquechee River, Town Highway 34, Town of Bridgewater
*
J1      * * 0.002
J3      6 29 30 552 553 551 5 16 17 13 3 * 15 14 23 21 11 12 4 7 3
*
Q      8030 11600 4853
SK      0.0095 0.0095 0.0095
*
XS      EXITX      -64
GR      -89.5, 522.44      -77.3, 512.94      -64.6, 511.49      -59.6, 512.17
GR      -32.4, 511.01      -20.6, 500.65      -5.2, 498.47      0.0, 497.42
GR      2.5, 496.23      7.2, 495.44      13.6, 495.39      20.2, 495.92
GR      26.0, 497.48      39.0, 501.48      52.2, 502.36      63.8, 504.56
GR      113.4, 506.55      186.7, 508.39      247.0, 510.48      322.8, 527.45
N      0.055      0.055      0.095
SA      -32.      52.2
*
XS      FULLV      0
*
BR      BRIDG      0 507.7 45
GR      0.0, 507.71      1.1, 497.48      5.6, 497.11      5.6, 495.65
GR      9.8, 495.25      19.8, 495.01      35.9, 495.08      43.7, 496.93
GR      49.2, 497.70      56.6, 498.07      57.9, 507.62      0.0, 507.71
N      0.040
CD      4 41.5 2.1 508 52.5 8.6
*
XR      RDWAY      20.8 22 1
GR      -78.6, 523.19      -69.8, 511.92      -61.1, 511.18      -55.2, 511.67
GR      -48.2, 511.37      -5.0, 510.17      -5.0, 514.60      2.5, 514.50
GR      3.9, 515.71      52.8, 516.09      54.2, 514.86      60.7, 514.91
GR      60.7, 510.65      111.4, 510.57      147.1, 511.16      228.1, 512.83
GR      373.5, 521.12
BP      0
*
*
XT      SURVA      132
GR      -25.8, 516.12      -3.2, 501.03      -0.5, 499.48      4.1, 498.61
GR      18.3, 498.03      28.9, 497.90      40.0, 499.26      54.4, 499.73
GR      62.5, 502.09      100.9, 510.59      156.7, 511.29      248.0, 514.30
GR      323.3, 518.84
*
AS      APPRO      82
GT      -0.72
N      .060 .040
SA      100.9
BP      17
*
HP 1 BRIDG      507.71 1 507.71
HP 2 BRIDG      507.71 * * 6138
HP 2 RDWAY      512.63 * * 1893
HP 1 APPRO      512.80 1 512.80
HP 2 APPRO      512.80 * * 8030
*
HP 1 BRIDG      507.71 1 507.71
HP 2 BRIDG      507.71 * * 6114
HP 2 RDWAY      514.24 * * 5489
HP 1 APPRO      514.66 1 514.66
HP 2 APPRO      514.66 * * 11600
*
HP 1 BRIDG      505.06 1 505.06

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WSPRO INPUT FILE (continued)

HP 2 BRIDG	505.06	*	*	4853
HP 1 APPRO	508.08	1	508.08	
HP 2 APPRO	508.08	*	*	4853

*

EX

ER

APPENDIX B:

WSPRO OUTPUT FILE

WSPRO OUTPUT FILE

U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE brid0026.wsp
 CREATED ON 24-APR-95 FOR BRIDGE BRIDTH00340026 USING FILE brid0026.dca
 Ottauguechee River, Town Highway 34, Town of Bridgewater
 *** RUN DATE & TIME: 11-01-95 13:12

CROSS-SECTION PROPERTIES: ISEQ = 3; SECID = BRIDG; SRD = 0.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	466	47759	0	102				0
507.71		466	47759	0	102	1.00	0	58	0

VELOCITY DISTRIBUTION: ISEQ = 3; SECID = BRIDG; SRD = 0.

WSEL	LEW	REW	AREA	K	Q	VEL
507.71	0.0	57.9	465.7	47759.	6138.	13.18

X STA.	0.0	6.0	8.9	11.6	14.0	16.4
A(I)	40.6	25.4	22.9	21.5	21.1	
V(I)	7.56	12.09	13.38	14.30	14.55	

X STA.	16.4	18.6	20.8	23.1	25.3	27.5
A(I)	20.2	19.8	20.0	19.7	19.7	
V(I)	15.22	15.46	15.35	15.55	15.56	

X STA.	27.5	29.7	31.9	34.1	36.4	38.9
A(I)	19.7	19.6	19.9	20.1	21.4	
V(I)	15.60	15.62	15.45	15.29	14.32	

X STA.	38.9	41.5	44.5	47.7	51.5	57.9
A(I)	21.5	23.0	23.8	26.4	39.4	
V(I)	14.29	13.33	12.90	11.64	7.78	

VELOCITY DISTRIBUTION: ISEQ = 4; SECID = RDWAY; SRD = 21.

WSEL	LEW	REW	AREA	K	Q	VEL
512.63	-70.4	218.4	322.7	8077.	1893.	5.87

X STA.	-70.4	-57.7	-45.7	-37.3	-30.7	-25.2
A(I)	14.1	13.6	12.2	10.9	9.9	
V(I)	6.72	6.94	7.76	8.67	9.59	

X STA.	-25.2	-20.3	-16.0	-11.9	-8.2	65.0
A(I)	9.7	9.1	8.9	8.7	16.2	
V(I)	9.75	10.43	10.61	10.86	5.83	

X STA.	65.0	73.5	81.9	90.5	99.2	107.9
A(I)	16.9	17.0	17.3	17.7	17.9	
V(I)	5.60	5.57	5.46	5.36	5.30	

X STA.	107.9	116.8	127.6	140.6	158.5	218.4
A(I)	18.1	20.2	21.9	25.3	37.0	
V(I)	5.23	4.68	4.32	3.74	2.56	

CROSS-SECTION PROPERTIES: ISEQ = 5; SECID = APPRO; SRD = 82.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
	1	1346	159974	123	128				25275
	2	219	11987	123	123				1660
512.80		1565	171962	246	252	1.11	-21	224	21285

VELOCITY DISTRIBUTION: ISEQ = 5; SECID = APPRO; SRD = 82.

WSEL	LEW	REW	AREA	K	Q	VEL
512.80	-21.9	224.3	1565.0	171962.	8030.	5.13

X STA.	-21.9	-3.1	2.5	7.1	11.4	15.4
A(I)	118.3	77.9	67.6	65.5	61.4	
V(I)	3.39	5.16	5.94	6.13	6.53	

X STA.	15.4	19.4	23.2	27.0	30.8	34.8
A(I)	60.8	59.9	59.1	58.6	60.7	
V(I)	6.61	6.70	6.79	6.85	6.61	

X STA.	34.8	38.9	43.4	47.8	52.6	57.7
A(I)	60.8	62.9	63.2	65.8	68.7	
V(I)	6.61	6.39	6.36	6.11	5.84	

X STA.	57.7	63.9	71.9	84.2	119.2	224.3
A(I)	74.7	81.6	98.7	131.0	167.9	
V(I)	5.37	4.92	4.07	3.06	2.39	

WSPRO OUTPUT FILE (continued)

CROSS-SECTION PROPERTIES: ISEQ = 3; SECID = BRIDG; SRD = 0.
WSEL SA# AREA K TOPW WETP ALPH LEW REW QCR
1 466 47759 0 102 0 0 58 0
507.71 466 47759 0 102 1.00 0 58 0

VELOCITY DISTRIBUTION: ISEQ = 3; SECID = BRIDG; SRD = 0.
WSEL LEW REW AREA K Q VEL
507.71 0.0 57.9 465.7 47759. 6114. 13.13

X STA. 0.0 6.0 8.9 11.6 14.0 16.4
A(I) 40.6 25.4 22.9 21.5 21.1
V(I) 7.53 12.05 13.33 14.24 14.50

X STA. 16.4 18.6 20.8 23.1 25.3 27.5
A(I) 20.2 19.8 20.0 19.7 19.7
V(I) 15.16 15.40 15.29 15.49 15.50

X STA. 27.5 29.7 31.9 34.1 36.4 38.9
A(I) 19.7 19.6 19.9 20.1 21.4
V(I) 15.54 15.56 15.39 15.23 14.27

X STA. 38.9 41.5 44.5 47.7 51.5 57.9
A(I) 21.5 23.0 23.8 26.4 39.4
V(I) 14.24 13.28 12.85 11.60 7.75

VELOCITY DISTRIBUTION: ISEQ = 4; SECID = RDWAY; SRD = 21.
WSEL LEW REW AREA K Q VEL
514.24 -71.6 252.8 714.9 26605. 5489. 7.68

X STA. -71.6 -60.2 -50.8 -42.5 -34.9 -28.3
A(I) 28.2 25.8 24.2 23.6 22.0
V(I) 9.74 10.65 11.36 11.64 12.46

X STA. -28.3 -22.2 -16.5 -11.1 63.6 74.3
A(I) 21.4 20.8 20.7 34.9 38.5
V(I) 12.80 13.22 13.26 7.86 7.13

X STA. 74.3 84.6 95.0 105.4 115.8 127.2
A(I) 37.4 37.6 38.2 37.9 39.8
V(I) 7.33 7.30 7.18 7.24 6.90

X STA. 127.2 140.0 154.4 171.9 195.6 252.8
A(I) 42.4 44.2 48.2 55.1 74.1
V(I) 6.47 6.21 5.69 4.98 3.71

CROSS-SECTION PROPERTIES: ISEQ = 5; SECID = APPRO; SRD = 82.
WSEL SA# AREA K TOPW WETP ALPH LEW REW QCR
1 1577 204776 126 132 0 0 266 31698
2 493 38136 165 165 0 0 0 4842
514.66 2070 242912 291 297 1.10 -24 266 29880

VELOCITY DISTRIBUTION: ISEQ = 5; SECID = APPRO; SRD = 82.
WSEL LEW REW AREA K Q VEL
514.66 -24.7 265.9 2070.0 242912. 11600. 5.60

X STA. -24.7 -3.2 3.0 8.4 13.2 18.0
A(I) 154.8 97.7 89.6 82.4 82.2
V(I) 3.75 5.93 6.47 7.04 7.06

X STA. 18.0 22.5 26.9 31.4 36.0 40.9
A(I) 77.9 78.0 78.0 77.9 80.1
V(I) 7.44 7.44 7.44 7.45 7.24

X STA. 40.9 46.0 51.1 56.7 63.1 71.1
A(I) 81.7 80.8 86.0 89.9 98.3
V(I) 7.10 7.18 6.74 6.45 5.90

X STA. 71.1 82.4 104.1 132.9 167.5 265.9
A(I) 115.0 141.8 131.3 143.2 203.5
V(I) 5.04 4.09 4.42 4.05 2.85

CROSS-SECTION PROPERTIES: ISEQ = 3; SECID = BRIDG; SRD = 0.
WSEL SA# AREA K TOPW WETP ALPH LEW REW QCR
1 360 46408 40 56 0 0 58 6081
505.06 360 46408 40 56 1.00 0 58 6081

WSPRO OUTPUT FILE (continued)

VELOCITY DISTRIBUTION: ISEQ = 3; SECID = BRIDG; SRD = 0.

WSEL	LEW	REW	AREA	K	Q	VEL
505.06	0.3	57.6	359.6	46408.	4853.	13.49

X STA.	0.3	6.7	9.8	12.3	14.7	16.9
A(I)	34.5	20.9	17.7	16.4	15.7	
V(I)	7.04	11.60	13.74	14.77	15.48	

X STA.	16.9	19.1	21.2	23.3	25.3	27.4
A(I)	15.3	15.2	14.7	14.5	14.5	
V(I)	15.86	16.00	16.55	16.76	16.78	

X STA.	27.4	29.4	31.5	33.5	35.7	38.0
A(I)	14.6	14.5	14.7	15.2	15.7	
V(I)	16.67	16.69	16.51	15.98	15.41	

X STA.	38.0	40.5	43.4	46.7	50.7	57.6
A(I)	16.3	17.4	18.7	21.2	32.1	
V(I)	14.85	13.95	12.99	11.47	7.56	

CROSS-SECTION PROPERTIES: ISEQ = 5; SECID = APPRO; SRD = 82.

WSEL	SA#	AREA	K	TOPW	WETP	ALPH	LEW	REW	QCR
508.08	1	790	72275	108	112				12141
		790	72275	108	112	1.00	-14	93	12141

VELOCITY DISTRIBUTION: ISEQ = 5; SECID = APPRO; SRD = 82.

WSEL	LEW	REW	AREA	K	Q	VEL
508.08	-14.8	92.8	789.9	72275.	4853.	6.14

X STA.	-14.8	-1.3	3.0	6.5	9.8	12.9
A(I)	60.7	41.3	35.6	34.5	32.5	
V(I)	4.00	5.87	6.81	7.02	7.47	

X STA.	12.9	16.0	19.0	22.0	24.9	27.8
A(I)	32.8	32.2	32.0	31.7	31.9	
V(I)	7.40	7.52	7.58	7.64	7.62	

X STA.	27.8	30.8	34.0	37.5	41.2	45.1
A(I)	32.5	33.4	35.0	35.1	36.8	
V(I)	7.47	7.26	6.94	6.92	6.59	

X STA.	45.1	49.1	53.5	58.7	66.4	92.8
A(I)	37.9	40.5	44.3	51.9	77.1	
V(I)	6.40	5.99	5.47	4.67	3.15	

U.S. GEOLOGICAL SURVEY WSPRO INPUT FILE brid0026.wsp
 CREATED ON 24-APR-95 FOR BRIDGE BRIDTH00340026 USING FILE brid0026.dca
 Ottawaquechee River, Town Highway 34, Town of Bridgewater
 *** RUN DATE & TIME: 11-01-95 13:12

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
	SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL
EXITX:XS	*****	-28	900	1.72	*****	509.55	506.02	8030	507.84
-63	*****	165	82357	1.39	*****	*****	0.86	8.92	

FULLV:FV	64	-29	1098	1.27	0.50	510.04	*****	8030	508.77
0	64	198	99790	1.53	0.00	-0.01	0.73	7.32	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

APPRO:AS	82	-16	948	1.12	0.57	510.61	*****	8030	509.49
	82	99	92934	1.00	0.00	-0.01	0.52	8.47	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

WSPRO OUTPUT FILE (continued)

===255 ATTEMPTING FLOW CLASS 3 (6) SOLUTION.

WS3N,LSEL = 508.77 507.70

<<<<RESULTS REFLECTING THE CONSTRICTED FLOW FOLLOW>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
BRIDG:BR	64	0	466	2.70	*****	510.41	505.12	6138	507.71
0	*****	58	47759	1.00	*****	*****	0.82	13.18	

TYPE	PCPD	FLOW	C	P/A	LSEL	BLEN	XLAB	XRAB
4.	****	6.	0.800	0.000	507.70	*****	*****	*****

XSID:CODE	SRD	FLEN	HF	VHD	EGL	ERR	Q	WSEL
RDWAY:RG	21.	60.	0.13	0.45	513.13	0.00	1893.	512.63

	Q	WLEN	LEW	REW	DMAX	DAVG	VMAX	VAVG	HAVG	CAVG
LT:	612.	65.	-70.	-5.	2.5	1.6	6.7	5.8	2.1	3.1
RT:	1281.	158.	61.	219.	2.1	1.4	6.5	5.9	1.9	3.2

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
APPRO:AS	41	-21	1566	0.45	0.27	513.26	505.97	8030	512.80
82	45	224	172117	1.11	0.00	0.00	0.38	5.13	

<<<<END OF BRIDGE COMPUTATIONS>>>>

FIRST USER DEFINED TABLE.

XSID:CODE	SRD	LEW	REW	Q	K	AREA	VEL	WSEL
EXITX:XS	-64.	-29.	165.	8030.	82357.	900.	8.92	507.84
FULLV:FV	0.	-30.	198.	8030.	99790.	1098.	7.32	508.77
BRIDG:BR	0.	0.	58.	6138.	47759.	466.	13.18	507.71
RDWAY:RG	21.	*****	612.	1893.	*****	*****	1.00	512.63
APPRO:AS	82.	-22.	224.	8030.	172117.	1566.	5.13	512.80

SECOND USER DEFINED TABLE.

XSID:CODE	CRWS	FR#	YMIN	YMAX	HF	HO	VHD	EGL	WSEL
EXITX:XS	506.02	0.86	495.39	527.45	*****	*****	1.72	509.55	507.84
FULLV:FV	*****	0.73	495.39	527.45	0.50	0.00	1.27	510.04	508.77
BRIDG:BR	505.12	0.82	495.01	507.71	*****	*****	2.70	510.41	507.71
RDWAY:RG	*****	*****	510.17	523.19	0.13	*****	0.45	513.13	512.63
APPRO:AS	505.97	0.38	497.18	518.12	0.27	0.00	0.45	513.26	512.80

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
EXITX:XS	*****	-30	1312	2.00	*****	511.66	508.25	11600	509.66
-63	*****	223	118966	1.64	*****	*****	0.88	8.84	

FULLV:FV		64	-31	1593	1.43	0.50	512.14	*****	11600	510.70
0	64	248	145117	1.74	0.00	-0.02	0.71	7.28		

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

APPRO:AS		82	-19	1228	1.47	0.59	512.76	*****	11600	511.28
82	82	178	129199	1.06	0.02	0.01	0.69	9.44		

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

===255 ATTEMPTING FLOW CLASS 3 (6) SOLUTION.

WS3N,LSEL = 510.70 507.70

<<<<RESULTS REFLECTING THE CONSTRICTED FLOW FOLLOW>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
BRIDG:BR	64	0	466	2.68	*****	510.39	505.09	6114	507.71
0	*****	58	47759	1.00	*****	*****	0.82	13.13	

TYPE	PCPD	FLOW	C	P/A	LSEL	BLEN	XLAB	XRAB
4.	****	6.	0.800	0.000	507.70	*****	*****	*****

WSPRO OUTPUT FILE (continued)

XSID:CODE	SRD	FLEN	HF	VHD	EGL	ERR	Q	WSEL
RDWAY:RG	21.	60.	0.14	0.54	515.06	0.00	5489.	514.24

	Q	WLEN	LEW	REW	DMAX	DAVG	VMAX	VAVG	HAVG	CAVG
LT: 1630.	67.	-72.	-5.	4.1	3.2	9.2	7.7	4.0	3.1	
RT: 3860.	192.	61.	253.	3.7	2.6	8.8	7.6	3.4	3.1	

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
APPRO:AS	41	-24	2070	0.54	0.31	515.20	507.83	11600	514.66
82	46	266	242834	1.10	0.00	0.00	0.39	5.61	

<<<<END OF BRIDGE COMPUTATIONS>>>>

FIRST USER DEFINED TABLE.

XSID:CODE	SRD	LEW	REW	Q	K	AREA	VEL	WSEL
EXITX:XS	-64.	-31.	223.	11600.	118966.	1312.	8.84	509.66
FULLV:FV	0.	-32.	248.	11600.	145117.	1593.	7.28	510.70
BRIDG:BR	0.	0.	58.	6114.	47759.	466.	13.13	507.71
RDWAY:RG	21.	*****	1630.	5489.	*****	*****	1.00	514.24
APPRO:AS	82.	-25.	266.	11600.	242834.	2070.	5.61	514.66

SECOND USER DEFINED TABLE.

XSID:CODE	CRWS	FR#	YMIN	YMAX	HF	HO	VHD	EGL	WSEL
EXITX:XS	508.25	0.88	495.39	527.45	*****	*****	2.00	511.66	509.66
FULLV:FV	*****	0.71	495.39	527.45	0.50	0.00	1.43	512.14	510.70
BRIDG:BR	505.09	0.82	495.01	507.71	*****	*****	2.68	510.39	507.71
RDWAY:RG	*****	*****	510.17	523.19	0.14	*****	0.54	515.06	514.24
APPRO:AS	507.83	0.39	497.18	518.12	0.31	0.00	0.54	515.20	514.66

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
EXITX:XS	*****	-25	563	1.28	*****	506.88	503.79	4853	505.60
-63	*****	90	49753	1.11	*****	*****	0.73	8.62	
FULLV:FV	64	-26	663	0.99	0.50	507.38	*****	4853	506.39
0	64	109	60072	1.19	0.00	-0.01	0.64	7.32	

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

APPRO:AS 82 -12 691 0.77 0.54 507.91 ***** 4853 507.14

82 82 89 60064 1.00 0.00 0.00 0.48 7.02

<<<<THE ABOVE RESULTS REFLECT "NORMAL" (UNCONSTRICTED) FLOW>>>>

===220 FLOW CLASS 1 (4) SOLUTION INDICATES POSSIBLE PRESSURE FLOW.

WS3,WSIU,WS1,LSEL = 505.06 507.80 508.12 507.70

===245 ATTEMPTING FLOW CLASS 2 (5) SOLUTION.

===240 NO DISCHARGE BALANCE IN 15 ITERATIONS.

WS,QBO,QRD = 510.71 4818. 19.

===270 REJECTED FLOW CLASS 2 (5) SOLUTION.

<<<<RESULTS REFLECTING THE CONSTRICTED FLOW FOLLOW>>>>

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
BRIDG:BR	64	0	359	2.83	0.65	507.89	503.80	4853	505.06
0	64	58	46381	1.00	0.36	0.00	0.80	13.50	

TYPE PPCD FLOW C P/A LSEL BLEN XLAB XRAB

4. **** 1. 1.000 ***** 507.70 ***** ***** *****

XSID:CODE	SRD	FLEN	HF	VHD	EGL	ERR	Q	WSEL
RDWAY:RG	21.							

<<<<EMBANKMENT IS NOT OVERTOPPED>>>>

WSPRO OUTPUT FILE (continued)

XSID:CODE	SRDL	LEW	AREA	VHD	HF	EGL	CRWS	Q	WSEL
SRD	FLEN	REW	K	ALPH	HO	ERR	FR#	VEL	
APPRO:AS	41	-14	795	0.58	0.32	508.70	503.89	4853	508.12
82	46	93	72866	1.00	0.50	0.00	0.40	6.11	
M(G)	M(K)	KQ	XLKQ	XRKQ	OTEL				
0.435	0.082	66863.	0.	57.	507.86				

<<<<END OF BRIDGE COMPUTATIONS>>>>

FIRST USER DEFINED TABLE.

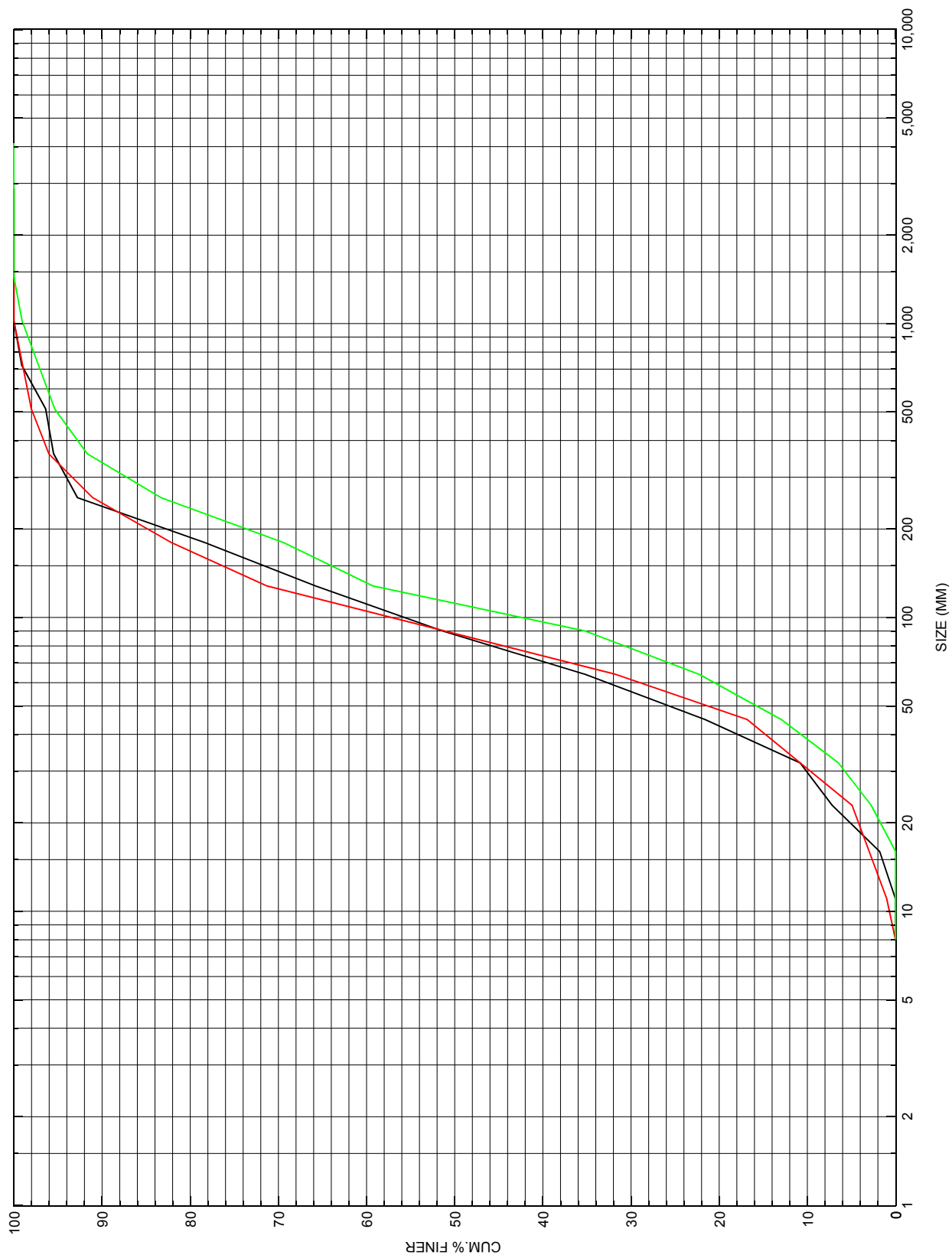
XSID:CODE	SRD	LEW	REW	Q	K	AREA	VEL	WSEL
EXITX:XS	-64.	-26.	90.	4853.	49753.	563.	8.62	505.60
FULLV:FV	0.	-27.	109.	4853.	60072.	663.	7.32	506.39
BRIDG:BR	0.	0.	58.	4853.	46381.	359.	13.50	505.06
RDWAY:RG	21.	*****		0.	0.	0.	1.00*****	
APPRO:AS	82.	-15.	93.	4853.	72866.	795.	6.11	508.12

SECOND USER DEFINED TABLE.

XSID:CODE	CRWS	FR#	YMIN	YMAX	HF	HO	VHD	EGL	WSEL
EXITX:XS	503.79	0.73	495.39	527.45*****			1.28	506.88	505.60
FULLV:FV	*****	0.64	495.39	527.45	0.50	0.00	0.99	507.38	506.39
BRIDG:BR	503.80	0.80	495.01	507.71	0.65	0.36	2.83	507.89	505.06
RDWAY:RG	*****		510.17	523.19*****			0.30	510.91*****	
APPRO:AS	503.89	0.40	497.18	518.12	0.32	0.50	0.58	508.70	508.12

APPENDIX C:

BED-MATERIAL PARTICAL-SIZE DISTRIBUTION



Appendix C. Bed material particle-size distributions for three pebble count transects at the approach cross-section for structure BRIDTH00340026, in Bridgewater, Vermont.

APPENDIX D:
HISTORICAL DATA FORM