

**HYDROLOGIC, SEDIMENTOLOGIC, AND CHEMICAL
DATA DESCRIBING SURFICIAL BED SEDIMENTS IN THE
NAVIGATION POOLS OF THE UPPER MISSISSIPPI RIVER,
AFTER THE FLOOD OF 1993**

Edited by John A. Moody

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OVERVIEW

Surficial bed-sediment samples were collected from the navigation pools (Pools 1-26) in the Upper Mississippi River between July 1991 and April 1992 before the flood of 1993. The purpose was to assess the longitudinal distribution of inorganic and organic compounds in the surficial sediments. This study assesses the longitudinal distribution of inorganic and organic compounds in surficial bed sediments collected after the flood of 1993, using the same procedures. In both studies a single composite sample was collected from each pool by combining samples from 12 to 23 individual sampling sites. Subsamples were taken from this composite sample for sediment characteristics and for organic chemical analyses of sterols, polynuclear aromatic hydrocarbons, linear alkylbenzene sulfonates, organochlorines, and polychlorinated biphenyls. Bed-sediment cores were also collected from the 12 to 23 individual sampling sites, composited in the laboratory, and then analyzed for major and trace elements. This was a cooperative study with the National Biological Service, which collected samples for bioaccumulation tests, biotoxicity tests, and additional chemical analyses. Their results are published in other reports.

Concentration of chemical compounds in the surficial bed sediments was greatest in fine-grain sediments. The median particle diameter of the sediment ranged from 0.002 millimeter (Pool 4, Lake Pepin) to 0.419 millimeter (Pool 20). Fine-grain sediment (median diameter less than 0.063 millimeter) was found generally in the upstream pools (2, 4, 9, 11, 12, and 13) but some was found in downstream pools (19, 25, and 26). Thus, generally, the maximum concentration of chemical compounds and elements was greatest in upstream pools: organic carbon was 3.79 percent in Pool 4, coprostanol was 4.41 milligrams per kilogram (mg/kg) in Pool 9, total polynuclear aromatic hydrocarbons were 5.28 mg/kg in Pool 1, linear alkylbenzene sulfonates were 1.07 mg/kg in Pool 13, technical chlordane was 2 nanogram per gram (ng/g) in Pools 4 and 21, polychlorinated biphenyls were 92.8 ng/g in Pool 4 (Lake Pepin), lead was 32 and 48 micrograms per gram ($\mu\text{g/g}$) in Pools 4 and 12, and mercury was 0.191 $\mu\text{g/g}$ in Pool 2. However, the maximum concentration of dieldrin was 0.7 ng/g in Pool 26, the pool that is farthest downstream.

ACKNOWLEDGMENTS

Collecting surficial bed-sediment samples from all the navigation pools of the Upper Mississippi River after the flood is definitely a job which involved many people. The captains, Craig LeBoeuf and Wayne Simoneaux, and the crew of the research vessel *Acadiana* from the Louisiana University Marine Consortium, Cheryl Blanchard, Wilton Delaune, Mike Detraz, Derral Dupre, Chuck Guidry, and Jonathan Landry, provided excellent field support for other members of the sampling crews, Ron Antweiler, LaDonna Bishop, Terry Brinton, John Garbarino, Gary Johnson, Deborah Martin, Bob Meade, Ted Noyes, Dale Peart, Dave Roth, and Jeff Writer. Harold Wiegner from the Minnesota Pollution Control Agency designed and built the sediment corer used for collecting samples for inorganic analyses. Theodore Young of Sandwich, Massachusetts, designed and built the van Veen sampler. The research vessel itself served as a floating laboratory, and more than once, as an excellent refuge from severe and violent weather. Eric Brunson, from the Biologic Resources Division, was extremely cooperative in helping to plan and execute the field sampling after the flood and in providing the biological information. Funding for field collection and some chemical analyses was provided by the U.S. Environmental Protection Agency's Office of Water.

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CONVERSION FACTORS AND ABBREVIATIONS

| <u>Multiply</u> | <u>By</u> | <u>To obtain</u> |
|--|------------------------|-----------------------|
| | <u>Length</u> | |
| angstrom (Å) | 3.937×10^{-9} | inch |
| centimeter (cm) | 0.3937 | inch |
| micrometer (μm) | 0.00003937 | inch |
| millimeter (mm) | 0.03937 | inch |
| meter (m) | 3.281 | foot |
| kilometer (km) | 0.6214 | mile |
| | <u>Area</u> | |
| square meter (m ²) | 10.76 | square foot |
| square kilometer (km ²) | 0.3861 | square mile |
| | <u>Volume</u> | |
| milliliter (mL) | 0.03382 | ounces, fluid |
| liter (L) | 0.2642 | gallon |
| cubic meter (m ³) | 35.31 | cubic foot |
| | <u>Flow</u> | |
| centimeter per second (cm/s) | 0.03281 | foot per second |
| meter per second (m/s) | 3.281 | foot per second |
| cubic meter per second (m ³ /s) | 35.31 | cubic foot per second |
| cubic meter per year (m ³ /yr) | 35.31 | cubic foot per year |
| hour per kilometer (h/km) | 0.6214 | hour per mile |
| | <u>Mass</u> | |
| milligram (mg) | 0.00003527 | ounce, avoirdupois |
| gram (g) | 0.002205 | pound, avoirdupois |
| metric ton | 2,205 | pound, avoirdupois |

Degree Celsius (°C) may be converted to degree Fahrenheit (°F) by using the following equation:

$$F = 1.8 (°C) + 32$$

The following terms and abbreviations also were used in these chapters:

| | |
|-------------------------------------|--------------------------------|
| atomic mass unit (amu) | milligrams per liter (mg/L) |
| electron volts (eV) | milligram per kilogram (mg/kg) |
| gram per milliliter (g/mL) | nanogram per liter (ng/L) |
| megohms per centimeter (Mohm/cm) | nanogram per gram (ng/g) |
| microangstrom (μA) | normal (N) |
| microgram (μg) | parts per million (ppm) |
| microliter (μL) | parts per billion (ppb) |
| microgram per liter (μg/L) | picogram (pg) |
| microgram per gram (μg/g) | revolutions per minute (rpm) |
| micrometer (μm) | torr |
| microsiemens per centimeter (μS/cm) | |

Sea level: In this report, "sea level" refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929)--a geodetic datum derived from a general adjustment of the first-order level nets of both the United States and Canada, formerly called Sea Level Datum of 1929.

CHAPTER 1 - Sampling Strategy, Hydrology, and Sediment Characteristics

By John A. Moody

ABSTRACT

Twenty-nine navigation pools are present along the reach of the Mississippi River from Minneapolis, Minnesota, to St. Louis, Missouri. A representative composite surficial bed-sediment sample was collected from the downstream one-third of 24 of the 29 navigation pools during a research cruise to assess the distribution of sewage-derived contaminants, selected organic contaminants, and major and trace elements after the flood of 1993 on the Upper Mississippi River. The particle-size distribution of a subsample of surficial bed sediment from each pool was determined by sieve, visual-accumulation tube, and SediGraph methods. Bulk chemistry (percent nitrogen, carbonate carbon, total carbon, total organic carbon, and total volatile solids) was determined for a second subsample of the surficial bed sediment.

The hydraulic conditions present at the time the surficial bed-sediment samples were collected were measured, and about 40 percent of the water discharge was measured outside the navigation channel in backwater areas ranging from 0.3 to 3.0 meters deep. The water velocities in the backwater areas were about 60 percent of the velocities in the navigation channel. Flushing rates ranged from 0.3 hour per kilometer to about 1.7 hours per kilometer. The median particle diameter of the surficial bed sediments ranged from 0.002 millimeter to 0.419 millimeter, and the organic carbon associated with these sediments ranged from 0.12 to 3.79 percent.

INTRODUCTION

The major hydraulic characteristic of the Upper Mississippi River is the series of locks and dams that create pools along its reach. Because the navigation pools are known to trap and store sediments and their associated pollutants, the U.S. Geological Survey (USGS) has undertaken studies of the Upper Mississippi River as part of a larger assessment of the environmental status of the entire Mississippi River. Twenty-nine locks and dams form 29 navigation pools on the Mississippi River between Minneapolis, Minn., and St. Louis, Mo. The first navigation pool (Pool 19, see table 1.1 and fig. 1.1) was formed behind a lock and dam built across the Mississippi River at Keokuk, Iowa, for electrical power generation in 1913 (Tweet, 1984; Whitacre, 1992). The second and third pools were formed by the construction of Lock and Dam 1 in 1917 at Minneapolis, Minn., and by Lock and Dam 2 in 1930 at Hastings, Minn., which provided 4.5- and 6-ft navigation channels (U.S. Army Corps of Engineers, 1988a).

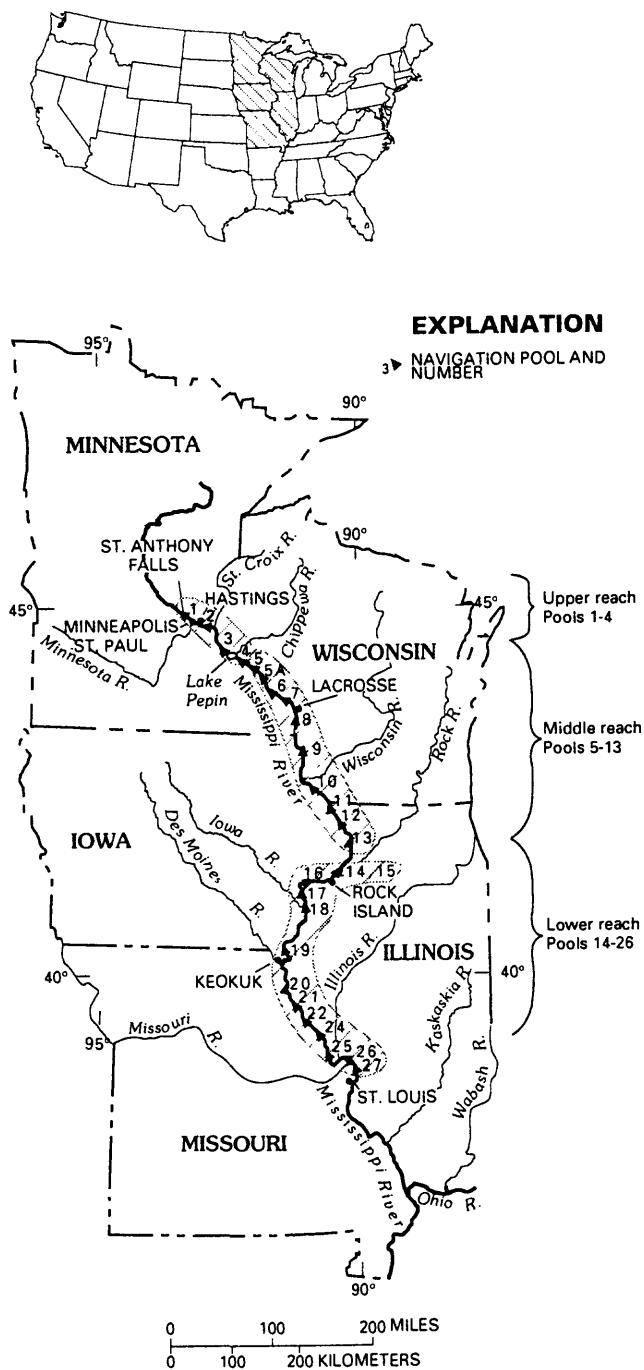


Figure 1.1--Location of navigation pools upstream from dams on the Upper Mississippi River. Cities are shown as solid circles and lock and dams as solid triangles.

Twenty-three additional pools (there is no Pool 23, but there is a Pool 5A) were formed by construction of locks and dams for the 9-foot channel project between Minneapolis, Minn., and St. Louis, Mo., in the 1930's. The 9-foot channel was extended upstream in Minneapolis, and two small pools (1.0 and 19 km long) were formed when the Lower and Upper St. Anthony Falls Lock and Dams were finished in 1963, making navigation possible around the 23-m-high St. Anthony Falls. The last lock and dam downstream, near St. Louis, Mo. (Lock and Dam 27), was completed in 1964, just downstream from the confluence of the Mississippi and Missouri Rivers. Lock and Dam 26, downstream from the confluence of the Mississippi and Illinois Rivers, was demolished and replaced in 1990 by the larger Melvin Price Lock and Dam, completing the series of 29 pools (Whitacre, 1992).

The system of navigation pools covers 36 percent of the reach of the Mississippi River from Minneapolis, Minn., to the Gulf of Mexico. The mean annual water discharge increases about twenty-fold from Minneapolis ($230 \text{ m}^3/\text{s}$), at the beginning of the pool reach, to St. Louis ($5,100 \text{ m}^3/\text{s}$), at the end of the pool reach.

The average length of the navigation pools is about 40 km, and approximately 8 percent of the surface area of the pools is maintained as a 9-foot navigation channel, leaving about 92 percent of the pool area as backwater areas with typical depths between 0.5 and 1.5 m. The average width-to-length ratio of the upper pools (Pools 1–15) is about twice the ratio of the lower pools (Pools 16–26), reflecting the general narrowing of the Mississippi River Valley in the downstream direction.

A navigation pool can be divided into three morphologically distinct regions (fig . 1.2). The first region (riverine) is immediately downstream from the preceding dam, where the flow is confined in a relatively narrow channel. The second region (deltaic) is characterized by several channels or sloughs that branch off from the navigation channel and return to the channel farther downstream. This deltaic region consists of numerous islands, which often bifurcate in the downstream direction, sheltering quiescent bays that face downstream out of the main current velocity. The third region (lacustrine) is characterized by the broad open water just upstream from the dam. These three types of regions produce a complex, heterogeneous benthic environment within each pool in contrast to the homogeneous (mostly medium to fine sand) benthic environment of the free-flowing lower Mississippi River downstream from St. Louis. These regions also may have different retention times for contaminants associated with the water.

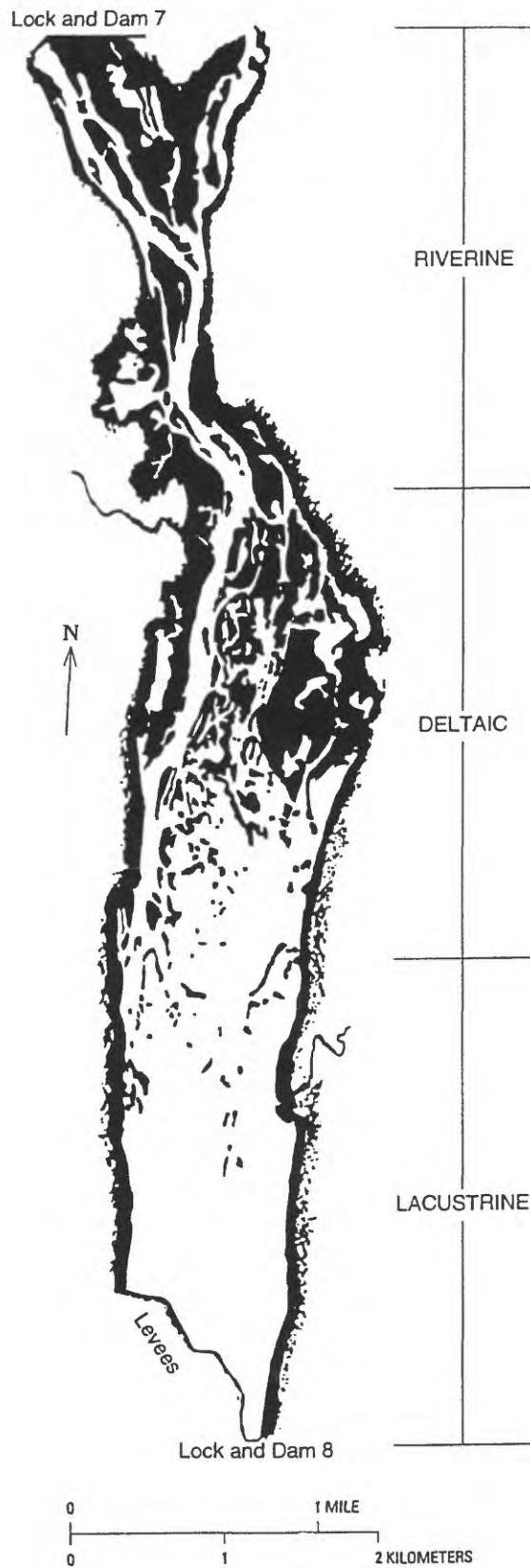


Figure 1.2--Typical navigation pool divided into three regions.

Table 1.1.--Physical and hydrologic characteristics of navigation pools in the Upper Mississippi River

[NGVD National Geodetic Vertical Datum of 1929; km, kilometers; m, meters, %, percent; m³/s, cubic meter per second; T, tributaries that contribute less than 2 percent of the discharge of the Mississippi River are not listed; there is no Pool 23; NA, data not available; <, less than; --, not measured]

| Pool | Length (km) | Project pool elevation above sea level | Surface area ¹ (km ²) | Navigation channel area ² (%) | Storage volume ³ (10 ⁶ m ³) | Mean depth (m) | Mean annual discharge ⁴ (m ³ /s) | Percentage of time at open river ⁵ | Tributary | |
|------|-------------|--|--|--|---|----------------|--|---|--------------|---|
| | | | | | | | | | Name | Percentage of discharge of Mississippi River down-stream from mouth of tributary ⁴ |
| 1 | 10 | 221.0 | 2 | 50 | NA | NA | 230 | NA | | |
| 2 | 53 | 209.5 | 48 | 11 | 85 | 1.8 | 340 | 1 | Minnesota | 34 |
| 3 | 29 | 205.7 | ⁶ 36 | 4 | 35 | 0.5 | 480 | 14 | St. Croix | 25 |
| 4 | 71 | 203.3 | 157 | 5 | 515 | 3.3 | 710 | 4 | Chippewa | 28 |
| 5 | 24 | 201.2 | 51 | 5 | 73 | 1.4 | 800 | 1 | T | -- |
| 5A | 14 | 198.4 | 28 | 5 | 35 | 1.3 | 800 | 13 | T | -- |
| 6 | 24 | 196.7 | 36 | 7 | 51 | 1.4 | 850 | 7 | T | -- |
| 7 | 19 | 194.8 | 54 | 4 | 92 | 1.7 | 850 | 5 | Black | 5 |
| 8 | 39 | 192.3 | 84 | 5 | 134 | 1.6 | 1,020 | 4 | T | -- |
| 9 | 50 | 189.0 | 118 | 4 | 226 | 1.9 | 1,020 | 15 | T | -- |
| 10 | 53 | 186.2 | 69 | 8 | 145 | 2.1 | 1,300 | 18 | Wisconsin | 18 |
| 11 | 51 | 183.8 | ⁸ 75 | 7 | 191 | 2.5 | 1,300 | 3 | Turkey | 2 |
| 12 | 42 | 180.4 | ⁸ 47 | 11 | 46 | 1.0 | 1,300 | 4 | T | -- |
| 13 | 55 | 177.7 | 120 | 5 | NA | NA | 1,400 | 4 | Maquoketa | 2 |
| 14 | 48 | 174.3 | 42 | 11 | NA | NA | 1,400 | <1 | Wapsipinicon | 3 |
| 15 | 16 | 171.0 | 15 | 11 | NA | NA | NA | 1 | T | -- |
| 16 | 42 | 166.1 | 51 | 8 | 131 | 2.6 | 1,530 | 12 | Rock | 11 |
| 17 | 32 | 163.4 | 32 | 10 | 86 | 2.7 | 1,530 | 22 | T | -- |
| 18 | 42 | 160.9 | 55 | 8 | NA | NA | 1,560 | 7 | Iowa | 11 |
| 19 | 76 | 157.9 | 125 | 6 | 360 | 2.9 | 1,800 | 0 | Skunk | 3 |
| 20 | 34 | 146.3 | 31 | 11 | 108 | 3.5 | 2,000 | 21 | Des Moines | 8 |

**Table 1.1.--Physical and hydrologic characteristics of navigation pools in the
Upper Mississippi River--Continued**

| Pool | Length (km) | Project pool eleva- tion above sea level | Surface area ¹ (km ²) | Navi- gation chan- nel area ² (%) | Storage volume ³ (10 ⁶ m ³) | Mean depth (m) | Mean annual dis- charge ⁴ (m ³ /s) | Percent- age of time at open river ⁵ | Tributary | |
|------|----------------|---|--|---|---|----------------------|--|---|-----------|---|
| | | | | | | | | | Name | Percentage discharge c Mississipp River down-strea from mout of tributary |
| 21 | 29 | 143.3 | 26 | 11 | 86 | 3.3 | 2,000 | 15 | T | -- |
| 22 | 39 | 140.1 | 36 | 11 | 105 | 2.9 | 2,000 | 12 | T | -- |
| 24 | 45 | 136.9 | ⁸ 51 | 9 | NA | NA | 2,040 | NA | Salt | 2 |
| 25 | 51 | 132.2 | ⁸ 69 | 7 | 192 | 2.8 | 2,040 | NA | T | |
| 26 | 61 | 127.7 | 121 | 8 | 424 | 3.5 | 2,600 | NA | Illinois | 24 |
| 27 | 17 | NA | NA | 50 | NA | NA | 5,100 | NA | Missouri | 43 |

¹References for surface area are: Pools 2–10, U.S. Army Corps of Engineers, St. Paul District, Gordon Heitzman, oral commun., 1991; Pools 11–22, U.S. Army Corps of Engineers, Rock Island District, Harry Bottorff, oral commun., 1991; Nakato, Tatsuaki, 1980; Bhowmik and others, 1987; and Pools 24–26, St. Louis District, Ray psky, oral commun., 1991, Bhowmik and others, 1987.

²Navigation channel area was computed by assuming a 100-meter-wide channel in all pools. The values in the table are about 3–4 percent lower than some given by Gilbertson and Kelly (1981).

³References for storage volume are: Pools 2–10, U.S. Army Corps of Engineers, St. Paul District reservoir regulation manuals; Pools 11, 16, 17, 20, 21, 22, 25 26, Nord, R.C., 1966; Pool 19; Union Electric Co., Keokuk, Iowa, oral commun., 1991.

⁴Discharges were taken from USGS Water Resources Data published annually by each State.

⁵References for percent of time at open river are: Pools 2–10, U.S. Army Corps of Engineers, St. Paul District, Gordon Heitzman, oral commun., 1991; Pools 11–22, U.S. Army Corps of Engineers, Rock Island District, Harry Bottorff, oral commun., 1991; and Pools 24–26, U.S. Army Corps of Engineers, St. Louis District, Don Coler oral commun., 1991.

⁶Lake St. Croix is not included so that the original value of 73 km² (which includes Lake St. Croix) was reduced (Gordon Heitzman, U.S. Army Corps of Engineers, St. Louis District, oral commun., 1991).

⁷Where two or three different values were obtained, the average value is reported in this table.

These pools do not have sufficient storage capacity to be operated as flood-control structures; they are maintained at a nearly constant elevation (table 1.1), creating an environment conducive to the deposition and storage of sediment. In Pools 1-10, the St. Paul District of the U.S. Army Corps of Engineers used a primary control point that is approximately at midpool and maintains the pool elevation within a range of about 0.1 m (U.S. Army Corps of Engineers, 1988b). In Pools 11-22, the Rock Island District uses a primary control point at the dam, and the range of the pool elevation fluctuates between 0.03 m above to 0.12 m below project pool elevation (Bryan Goodrum, U.S. Army Corps of Engineers Rock Island District, oral commun., 1992). In Pools 24-26, the St. Louis District uses a primary control point located about one-third of the distance upstream to the next dam and maintains pool elevations within a range of 0.2 to 0.6 m. During times when the water discharge is high, all the gates in the dams are opened (referred to as "open river" in table 1.1) and the increased water velocity in the pools inhibits the settling of suspended sediment. As the inflow to the pools decreases, the gates are partially closed to maintain the 9-foot channel for navigation; this decreases the water velocities and decreases the flushing rate of water in the pools, creating conditions favorable for the deposition of sediment.

Between 1987 and 1990, the U.S. Geological Survey investigated the transport of contaminants by suspended sediment in the free-flowing Mississippi River between St. Louis, Mo., and New Orleans, La. (Leenheer and others, 1989, 1995; Meade and Stevens, 1990; Pereira and others, 1990, 1992, 1995; Taylor and others, 1990; Moody and Meade 1992, 1993). In 1991, the investigations were expanded to include a study of the transport of contaminants by suspended sediment (Moody and Meade, 1995) and a study of the storage of contaminants in the surficial bed sediments in the navigation-pool reach of the Upper Mississippi River before the flood of 1993 (Moody, 1997; Meade and others, 1995).

The navigation pools are known to trap and store sediments with associated contaminants during normal flow conditions. Dredging activities, commercial navigation, recreational boating, and natural resuspension processes can result in the remobilization of contaminated sediments. What is not known is how large flood events affect contaminants stored with the bed sediments in impounded river systems.

The primary objective of this study was to assess the effects of the flood of 1993 on the contaminants stored in the bed sediments of the navigation pools of the Upper Mississippi River by comparing post-flood contaminant levels with those that had been measured just prior to the flood in 1991-92. This primary objective evolved into the following components:

1. To locate the original sampling sites by using a Global Positioning System (GPS) so that the future sampling would be easier.
2. To collect samples of surficial bed sediments during the summer of 1994, following previously established bed-sampling methods at the sites used by the U.S. Geological Survey in 1991-92 in the navigation pools of the Upper Mississippi River.
3. To repeat chemical analyses of these surficial bed sediments so that the chemical characteristics before and after the flood of 1993 could be compared.
4. To collect additional hydraulic data to estimate the remobilization of sediment during flood conditions.

PURPOSE AND SCOPE

The purposes of this chapter are to provide a general introduction to this study of the effects of the flood of 1993 on the surficial sediments in the navigation pools of the Upper Mississippi River and to discuss the sampling strategy and the data-collection methods. The navigation pools were resampled during June and July of 1994. Some hydraulic characteristics related to flushing rates are discussed and listed in tables. The particle-size characteristics and bulk chemical characteristics of the surficial bed sediments necessary for normalizing chemical data in succeeding chapters are listed in this chapter.

Sterols, polynuclear aromatic hydrocarbons (PAH), and linear alkylbenzene sulfonates (LAS) are discussed in Chapter 2; polychlorinated biphenyls (PCB) in Chapter 3; organochlorines in Chapter 4; and major and trace elements in Chapter 5. The location of each sample combined to make the composite sample and ancillary data at each sampling site in each pool are listed and shown on maps in Chapter 6.

SAMPLING STRATEGY

The same sampling strategy was used to collect surficial bed sediments from the navigation pools after the flood of 1993 as was used to collect samples in 1991 and 1992. This strategy recognizes that the navigation-pool reach of the Upper Mississippi River is a complex aquatic system. Wilcox (1993) lists at least 26 different aquatic habitats associated with the navigation channel and backwater areas of a pool. This diversity makes it difficult to obtain a bed-sediment sample that is representative of a pool. The number of habitats is reduced significantly if only the lacustrine region, which usually occupies the downstream one-third of a pool just upstream from the lock and dam structure, is considered. This region is generally shallow, has weak currents, and also is morphologically simpler; thus, the bed sediment may be more homogeneous. The rate of deposition of fine particulate matter in this region is probably more rapid than in the higher energy environment downstream from the dams or in the deltaic regions. The association of nonionic, nonpolar contaminants with fine particulate matter has been addressed by several researchers (Leenheer, 1991). A correlation of clay-size sediment with trace-metal concentrations in Upper Mississippi River pools was shown by Bailey and Rada (1984). For these reasons, the bed-sediment sampling focused on the downstream one-third of each pool.

To obtain a representative sample within this region of the pool, one to five transects (consisting of 2–13 sampling sites each) were sampled across the pool, approximately perpendicular to the flow direction, so that a variety of different shallow benthic habitats was sampled. These gave 12–23 individual samples that were combined to form one composite representative sample. The number of individual samples was based on a study of standard error as a function of number of individual samples in a composite sample for polychlorinated biphenyl data collected from Pool 7 (Sullivan, 1988). The results showed that the relative standard error decreased 37 percent from 5 to 20 samples but only 3 percent from 20 to 30 samples.

The pools upstream from the Lower and Upper St. Anthony Locks and Dams and the last pool (Pool 27) were not sampled because they were predominantly riverine and were assumed to have little stored sediment. Most of the surface area and volume of Pool 4 is Lake Pepin—a lake formed by a natural dam consisting of sediment transported across the Mississippi River by the Chippewa River. Lake Pepin is deep; consequently, water velocities are less than 10 cm/s (Randy Burkhardt, U.S. Fish and Wildlife Service, oral commun., 1991), allowing sediment to be deposited. Since Lake Pepin is essentially a long sediment trap, the upper (Upper Mississippi River Mile 773–785) and lower (Upper Mississippi River Mile 765–773) parts of Lake Pepin were sampled separately.

The sampling strategy after the flood of 1993 differed in two ways from the sampling done before the flood of 1993. All the navigation pools were sampled during one research cruise in June-July 1994 rather than during three separate cruises as was done before the flood (table 1.2). Also, more field replicate samples were collected after the flood to determine the field-sampling uncertainty.

Table 1.2--Location of pool transects in the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri

[X, single composite sample was collected; XX, duplicate composite samples were collected; SC, St. Croix River mile]

| Pool | Transect number | Location in river miles upstream from mouth of Ohio River | Maximum number of samples along transect | Cruise | | | |
|-----------------|-----------------|---|--|------------------|-----------------------|----------------|----------------|
| | | | | July-August 1991 | October-November 1991 | April-May 1992 | June-July 1994 |
| 1 | 1 | 848.0 | 4 | X | | | X |
| | 2 | 848.5 | 4 | X | | | X |
| | 3 | 849.2 | 4 | X | | | X |
| 2 | 1 | 816.1 | 7 | X | X | X | XX |
| | 2 | 818.1 | 7 | X | X | X | XX |
| | 3 | 821.1 | 4 | X | X | X | XX |
| St. Croix River | 1 | SC1.3 | 3 | | | | X |
| | 2 | SC1.9 | 3 | | | | X |
| | 3 | SC2.5 | 3 | | | | X |
| | 4 | SC3.3 | 3 | | | | X |
| | 5 | SC4.2 | 3 | | | | X |
| 3 | ¹ 1 | 798.1 | 8 | | X | | |
| | ¹ 2 | 798.1 | 6 | | X | | X |
| | 3 | 797.3 | 2 | | X | | X |
| ² 4 | 4 | 774.0 | 6 | | X | | X |
| | 5 | 776.0 | 5 | | X | | X |
| | 6 | 778.0 | 4 | | X | | X |
| ³ 4 | 1 | 772.0 | 7 | | X | | X |
| | 2 | 770.0 | 7 | | X | | X |
| | 3 | 768.0 | 7 | | X | | X |
| 5 | 1 | 744.7 | 9 | X | | | X |
| | 2 | 741.0 | 6 | X | | | X |

Table1.2--Location of pool transects in the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri--Continued

[X, single composite sample was collected; XX, duplicate composite samples were collected; SC, St. Croix River mile]

| Pool | Transect number | Location in river miles upstream from mouth of Ohio River | Maximum number of samples along transect | Cruise | | | |
|------|-----------------|---|--|------------------|-----------------------|----------------|----------------|
| | | | | July-August 1991 | October-November 1991 | April-May 1992 | June-July 1994 |
| | 3 | 739.8 | 3 | X | | | X |
| 5A | ¹ 1 | 729.8 | 7 | X | | | not sampled |
| | ¹ 2 | 729.8 | 7 | X | | | |
| | | | | | | | |
| 6 | ¹ 1 | 721.1 | 7 | | | X | X |
| | ¹ 2 | 714.9 | 7 | | | X | X |
| | ¹ 3 | 714.9 | 6 | | | X | X |
| 7 | ¹ 1 | 702.7 | 13 | X | | | X |
| | ¹ 2 | 702.7 | 7 | X | | | X |
| 8 | 1 | 684.7 | 7 | X | Only two samples | X | XX |
| | 2 | 683.3 | 7 | X | | X | XX |
| | 3 | 682.1 | 6 | X | | X | XX |
| 9 | ¹ 1 | 648.0 | 7 | | X | | X |
| | ¹ 2 | 655.0 | 8 | | X | | X |
| | ¹ 3 | 655.0 | 3 | | | | X |
| 10 | ¹ 1 | 615.0 | 3 | X | | | X |
| | ¹ 2 | 615.0 | 6 | X | | | X |
| | 3 | 616.1 | 6 | X | | | X |
| | 4 | 617.2 | 5 | X | | | X |
| 11 | 1 | 591.9 | 7 | | X | | X |
| | 2 | 587.4 | 8 | | X | | X |
| | 3 | 585.1 | 5 | | X | | X |
| 12 | ¹ 1 | 558.2 | 8 | | | X | X |
| | ¹ 2 | 558.2 | 7 | | | X | X |
| | 3 | 560.7 | 5 | | | X | X |
| 13 | 1 | 526.0 | 10 | | X | | X |
| | 2 | 523.7 | 10 | | X | | X |
| 14 | ¹ 1 | 499.8 | 3 | X | | | X |
| | ¹ 2 | 499.8 | 3 | X | | | X |
| | ¹ 3 | 494.8 | 7 | X | | | X |
| | ¹ 4 | 494.8 | 3 | X | | | X |
| 15 | 1 | 484.0 | 2 | | | X | X |
| | 2 | 485.8 | 10 | | | X | X |
| | 3 | 487.8 | 6 | | | X | X |
| 16 | ¹ 1 | 458.7 | 8 | | X | | X |
| | ¹ 2 | 458.7 | 6 | | X | | X |
| | 3 | 457.0 | 5 | | X | | X |

Table1.2--Location of pool transects in the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri--Continued

[X, single composite sample was collected; XX, duplicate composite samples were collected; SC, St. Croix River mile]

| Pool | Transect number | Location in river miles upstream from mouth of Ohio River | Maximum number of samples along transect | Cruise | | | |
|------|-----------------|---|--|------------------|-----------------------|----------------|----------------|
| | | | | July-August 1991 | October-November 1991 | April-May 1992 | June-July 1994 |
| 18 | 1 | 414.5 | 9 | | | X | X |
| | 2 | 411.8 | 9 | | | X | X |
| 19 | 1 | 371.6 | 4 | | X | | XX |
| | 2 | 370.2 | 5 | | X | | XX |
| | 3 | 368.9 | 5 | | X | | XX |
| | 4 | 367.5 | 5 | | X | | XX |
| | 5 | 366.3 | 4 | | X | | XX |
| 20 | 1 | 346.6 | 6 | X | | | X |
| | 2 | 344.2 | 6 | X | | | X |
| 21 | 1 | 331.4 | 7 | | | X | X |
| | ¹ 2 | 326.6 | 9 | | | X | X |
| | ¹ 3 | 326.6 | 3 | | | X | X |
| 22 | 1 | 306.0 | 7 | X | | | X |
| | ¹ 2 | 303.0 | 7 | X | | | X |
| | ¹ 3 | 303.0 | 7 | X | | | X |
| 24 | 1 | 273.4 | 4 | | X | | X |
| | 2 | 274.4 | 7 | | X | | X |
| | 3 | 275.3 | 7 | | X | | X |
| 25 | ¹ 1 | 243.1 | 8 | | | X | XX |
| | ¹ 2 | 243.1 | 7 | | | X | XX |
| | 3 | 241.5 | 4 | | | X | XX |
| 26 | 1 | 206.1 | 13 | | X | | XX |

¹Transects were in different directions.

²Upper Lake Pepin.

³Lower Lake Pepin.

SAMPLING PROCEDURE

In this section, the procedures are described for relocating the original 1991-92 sampling sites, for collecting samples from shallow and deep water, and for estimating the field-sampling uncertainty.

Locating the Original 1991-92 Sampling Sites

Two variations of the differential Global Positioning System (GPS) were used to locate the original sampling sites. A differential GPS system with a local reference station was used to locate the sampling sites in the upper pools (1-14) and in the St. Croix River. The latitude and longitude of the original sampling sites were scaled from U.S. Geological Survey's 7.5-minute quadrangles (accuracy $\pm 0.005^\circ$ or about ± 8 m) and were based on the North American Datum for 1927 (NAD27). A local reference GPS station (Trimble model 4000 SSE 18-channel receiver, GPS antenna, modem, Motorola radio, and radio antenna) was set up at a prominent landmark, and the reference station's latitude and longitude were scaled from the 7.5-minute quadrangle (accuracy ± 8 m). Corrections (RTCM-104 format) for the reference station were then generated by the GPS unit and transmitted by radio to a second GPS station (Trimble model 4000 SE 9-channel receiver, radio antenna, radio, and modem) in the small boat used for collecting the samples. The sites were relocated to within ± 5 m (differential GPS error) plus the accuracy of the location of the reference station. The present accuracy of the reference station is ± 8 m, but this can be improved by reoccupying the site of the reference station (see description of the location of the reference station in Chapter 6) at a later date and averaging GPS fixes for 1 to 2 hours.

A differential GPS system using the navigation beacon near St. Louis, Mo., as the reference station was used to relocate the sites in the lower pools (15-26). The accuracy of the resampled sites is about $\pm 0.001^\circ$ latitude or longitude because the navigation beacon location is known more precisely. Because the navigation beacon was used to locate sampling sites in the lower pools, the latitude and longitude for these sites are based on the North American Datum for 1983 (NAD83). The differential GPS was checked twice. At Dam 16, the GPS-derived coordinates for the tip of the guidewall closest to the dam were $41^\circ 25.588$ N., $021^\circ 00.456$ W., (NAD83) and the coordinates scaled from the Muscatine, Iowa-Ill. quadrangle were $41^\circ 25.580$ N., $091^\circ 00.460$ W., (NAD27). The difference was 14.4 m in latitude and 5.6 m in longitude. Similarly, the GPS coordinates for the southwest corner of the Union Electric Powerplant house at Dam 19, Keokuk, Iowa, were $40^\circ 23.851$ N., $091^\circ 22.309$ W. (NAD83) and coordinates scaled from the 7.5-minute quadrangle were $40^\circ 23.845$ N., $091^\circ 22.315$ W. (NAD27). The difference was 10.8 m in latitude and 8.4 m in longitude. Most of the difference is a result of scaling from a 1:24,000 map.

Shallow-Water Sampling

The backwater regions of the pools generally are less than 3 m deep, allowing all the bed samples to be collected from a small, 4.3-m-long boat (fig. 1.3) launched from the research vessel *Acadiana* (owned and operated by Louisiana Universities Marine Consortium). At each sampling site, the small boat was anchored on a short anchor line to prevent swinging, and three people measured surface temperature, specific conductance, water depth, and water velocity and collected two bed-sediment samples. The surface temperature and specific conductance (listed in Chapter 6) were measured with a LabComp model SCT-100 meter in a bucket after allowing about 30 seconds for the sensors to come to equilibrium. The accuracy of the unit was listed by the manufacturer as $\pm 10 \mu\text{S}/\text{cm}$ for the 0–2,000 $\mu\text{S}/\text{cm}$ range with resolutions of 1 $\mu\text{S}/\text{cm}$ and 0.1°C. This was checked before and after the cruise, and the specific conductance was within $\pm 5 \mu\text{S}/\text{cm}$ of a laboratory standard. The resolution of this meter was $\pm 1 \mu\text{S}/\text{cm}$ and $\pm 0.1^\circ\text{C}$. The depth was measured with a Lowrance Model X-16 analog recorder, and depths were recorded to the nearest 0.1 m. For depths less than about 1.3 m, a pole marked at 0.1-m intervals was used to measure the depth. The mean velocity was measured at 0.6 of the depth by using a standard Price AA current meter (Rantz and others, 1982), and the direction was determined by noting the direction, relative to a compass in the small boat, of the current meter and sounding weight after they were quickly raised a short distance (usually 1–3 m) to the surface. Depth, temperature, specific conductance, mean velocity, and direction are listed in Chapter 6.

The two bed-sediment samples were collected using a modified van Veen grab sampler and a gravity corer (fig. 1.4). The modified van Veen grab (fig. 1.4, Theodore E. Young, Sandwich, Mass., written commun., 1990) was operated from a small davit (fig. 1.3) with a hand winch. The sampler collects a 20-cm by 20-cm sample of the bed sediments (0.04 m²), which had a maximum thickness of 10 cm. The sampler consistently collected a full sample if the bed was mud without debris. In fine and medium sand, the sampler was usually 50 to 80 percent full. The only problem was clam shells, bark, sticks, or cobbles, which got caught between the jaws and allowed the sample to wash out. From the small boat, this sampler collected samples in water velocities as great as 90 cm/s and in water depths as great as 6 m.

After the sampler was brought aboard, subsamples were taken for particle size determination; carbon and nitrogen; sterols, PAH, and LAS; PCB; and organochlorine analyses. The subsamples were collected by using cores of various diameters made from Teflon cylinders (about 12–25-mm diameter) fitted with a Teflon-covered syringe plunger. The individual subsamples were added to glass or plastic jars as they were collected, then refrigerated and shipped to the laboratory for analysis (see this Chapter, and Chapters 2, 3, 4, and 5). The subsample for particle-size determination was collected by inserting a piece of U-shaped brass (0.4 cm wide, 0.2 cm deep, and 10 cm long) straight down into the sample, rotating the bottom of the U-shaped brass sampler, scraping off any excess sediment protruding above the sides of the sampler with a spatula, and then washing the sample into a plastic bottle with river water.

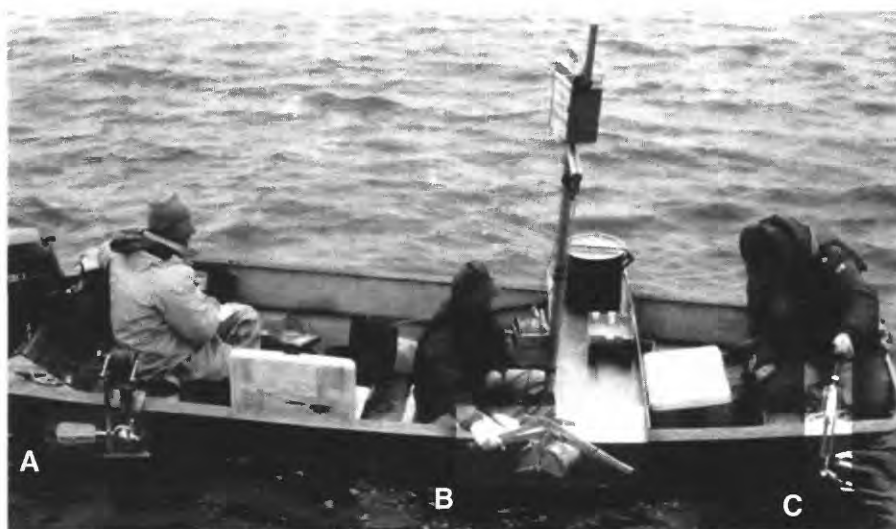
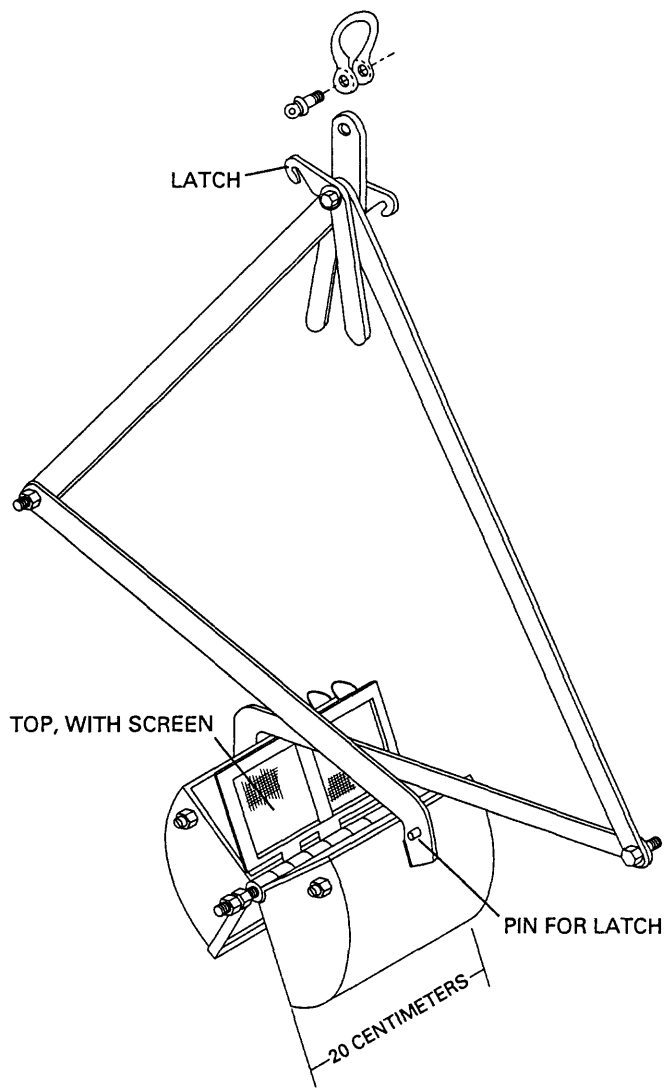
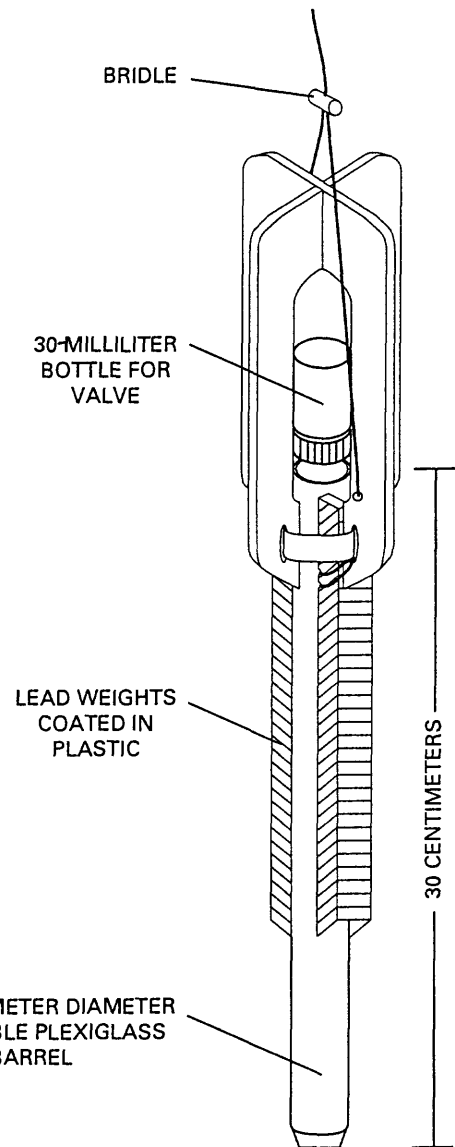


Figure 1.3--Shallow-water sampling equipment. At the bow of the 4.3-m-long boat, the small gravity corer (C) is being held over the side on a handline. Forward of the middle of the small boat, the modified van Veen grab sample (B) is hanging from a davit and boom assembly in the open position. On top of the davit is a microwave receiver/transmitter. Hanging over the side, just forward of the stern of the small boat, is a Price AA current meter (A). Photograph by R.H. Meade.



MODIFIED VAN VEEN GRAB



GRAVITY CORER

Figure 1.4--Details of the modified van Veen grab and gravity corer.

The second sampler was a gravity corer (designed and built by Harold Wiegner, Minnesota Pollution Control Agency, St. Paul, Minn.). The core tube was made of plexiglass (methyl methacrylate polymer) and other parts were plastic coated (fig. 1.4). The corer was designed to collect a maximum 30-cm-long core, 1.9 cm in diameter, for major and trace-element analysis (Chapter 5). The plastic core barrel was removed, the ends capped with a plastic cap, and each individual core sample was put in a plastic bag, sealed, and frozen. After being shipped to the laboratory, the cores were subsampled and combined to form a composite sample. It was difficult to obtain a gravity core if the water velocities were greater than about 40 cm/s or if the bed sediment was sand. Some samples for major and trace elements were collected from the modified van Veen grab sampler if the gravity corer failed to get a sample after three to six attempts.

Deep-Water Sampling

In Lake Pepin (Pool 4) and in Pool 19, the water depths were great enough to permit sampling from the *Acadiana*. This sampling procedure was similar to the shallow-water procedure because the bed-sediment samples were collected with the same equipment. The depth was determined with the same depth recorder mounted on the research vessel, and the surface temperature and specific conductance were measured in the same manner, but no velocity measurements were made. Since the research vessel was the sampling platform, it had to be positioned at the sampling site. The vessel's operator positioned the vessel upwind of the sampling site by using the GPS unit, which displayed latitude and longitude. As the vessel drifted downwind, samples were collected when the latitude and longitude scaled from the map agreed with the display on the GPS unit.

Field-Sampling Uncertainty

Samples were collected from the downstream one-third of each pool in order to reduce the inhomogeneity of the surficial sediments. However, it was assumed that there was still some inhomogeneity and, consequently, corresponding field-sampling uncertainty. For this reason, field duplicates were collected from five different pools and in a different manner from each pool as listed below:

Pool 2--A duplicate composite sample was taken at the same sampling site along each transect.

Pool 4--A duplicate composite sample was collected from sampling sites along three separate transects (upper Lake Pepin) separated by about 5 km from sampling sites along three other transects (lower Lake Pepin).

Pool 8--A duplicate composite sample was collected from a sampling site on each transect that was about 2-20 meters from the original sampling site.

Pool 19--A duplicate composite sample was collected at distances ranging from 70 to 800 meters (average 280 meters) from the original sampling site along each transect.

Pool 25--A duplicate composite sample was obtained by collecting twice as much material from one-half the sampling sites (every other sampling site) along the transects such that the final volume of the duplicate composite was approximately the same size as the first composite sample.

Because all laboratory measurements are a function of both the field and laboratory analytical uncertainty, the estimate of the field-sampling uncertainty for each duplicate sample was based on six parameters (measured for the duplicate samples above) that had the smallest laboratory analytical uncertainty. The estimate of the field-sampling uncertainty was the relative percent difference (difference of the duplicate values divided by the average of the two values times 100) for each duplicate described above (see table 1.3). Because each pool varies in the character of the sediment, the five individual estimates of the field-sampling uncertainty were averaged for each parameter, and then the six values for each parameter were averaged to give a field sampling uncertainty of 25 percent.

Table 1.3--Estimates of field-sampling uncertainty for surficial bed sediments collected from the downstream one-third of 25 sampled navigation pools of the Upper Mississippi River, June-July 1994

| Parameter | Uncertainty (relative percent difference) | | | | | Average |
|-------------------------------------|--|--------|--------|---------|---------|---------|
| | Pool 2 | Pool 4 | Pool 8 | Pool 19 | Pool 25 | |
| Median particle diameter | 10 | 40 | 2 | 78 | 12 | 28 |
| Percent finer than 0.062 millimeter | 4 | 14 | 2 | 16 | 1 | 7 |
| Total volatile solids | 2 | 5 | 32 | 28 | 28 | 19 |
| Total organic carbon | 24 | 4 | 56 | 12 | 141 | 47 |
| Copper | 82 | 16 | 12 | 46 | 13 | 34 |
| Lead | 14 | 10 | 10 | 11 | 13 | 12 |
| Average | 23 | 15 | 19 | 32 | 35 | 25 |

HYDROLOGY

Cross-sectional profiles of rivers are commonly plotted with a vertical exaggeration to make variations in depth look more pronounced. It should be kept in mind that the Mississippi River is a very thin, ribbonlike layer of water. The width-to-depth ratio in the riverine reach of the pools just downstream from dams averages about 100:1. This ratio is about one-tenth that in the lacustrine reach (table 1.4) of the pools where the dams cause water to back up over wide, flat valleys. If the Upper Mississippi River were as wide as this page, its maximum depth (about 8 m in the navigation channel) would be represented by a line less than 2 mm thick, and a line representing the depths of the shallow, off-channel, backwater areas would be less than 0.5 mm thick.

Discharge

The water discharge was computed from velocity measurements made at 0.6 of the depth at each sampling site along the sampling transect and at an additional three to six locations across the navigation and secondary channels. The standard error in the water discharge for triplicate measurements was 12 and 2 percent in Pools 8 and 11, respectively and was 39 and 7 percent for duplicates in Pools 2 and 5, respectively. Standard error averaged 4 percent for duplicates in Pools 13, 18, and 20. The discharges in the pools were compared to the discharges reported by the U.S. Army Corps of Engineers at the dam downstream and ranged from 24 percent less to 22 percent greater (and averaged about 6 percent less) than the Corps of Engineers measurements.

Sixty-three percent of the water discharge in the lacustrine regions of the pools was in the navigation channel (table 1.4). In the regions of the pool occupied by the navigation or secondary channels, the current direction was the same as in the navigation channels. In areas outside the channels, the current direction was variable and affected by wind direction and topography but generally was downriver (see Chapter 6 for current magnitudes and directions). The mean velocity in these areas averaged 60 percent of the velocity in the navigation channel (table 1.4).

Table 1.4--Measured hydraulic parameters for the lacustrine regions of some navigation pools in the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994

[m, meters; m³/s, cubic meter per second; cm/s, centimeter per second]

| Pool and transect number | Location in river miles upstream from mouth of Ohio River | Date | Cross section | | | Water discharge | | | Mean velocities | | |
|--------------------------|---|----------|----------------|----------------------|------------------------|------------------------------|--|---|-------------------|------------------------|----------------------|
| | | | Mean depth (m) | Width-to-depth ratio | Area (m ²) | Measured (m ³ /s) | Ratio of discharge to mean annual discharge ¹ | Percentage of total discharge in channels (%) | In channel (cm/s) | Outside channel (cm/s) | Cross section (cm/s) |
| 2-2 | 818.1 | 06-12-94 | 2.0 | 670 | 2,740 | 700 | 2.1 | 52 | 29 | 23 | 26 |
| 2-1 | 816.1 | | 1.7 | 840 | 2,410 | 470 | 1.4 | 66 | 26 | 13 | 19 |
| 5-2 | 741.0 | 06-16-94 | 1.7 | 1,500 | 4,520 | 860 | 1.1 | 65 | 31 | 11 | 19 |
| 5-3 | 739.8 | | 2.7 | 440 | 3,150 | 920 | 1.1 | 68 | 34 | 22 | 29 |
| 6-1 | 721.0 | 06-17-94 | 3.1 | 500 | 4,860 | 1,210 | 1.5 | 80 | 54 | 9 | 26 |
| 8-1 | 684.7 | 06-19-94 | 1.4 | 2,400 | 5,250 | 1,130 | 1.1 | 34 | 33 | 18 | 21 |
| 8-2 | 683.3 | | 1.4 | 2,800 | 5,480 | 900 | 0.9 | 49 | 28 | 12 | 16 |
| 8-3 | 682.1 | | 1.8 | 1,700 | 5,530 | 940 | 0.9 | 48 | 25 | 13 | 17 |
| 9-2 | 655.0 | 06-20-94 | 1.6 | 2,100 | 5,340 | 870 | 0.9 | 52 | 22 | 13 | 16 |
| 11-1 | 591.9 | 06-21-94 | 2.1 | 1,200 | 5,430 | 1,540 | 1.2 | 86 | 38 | 11 | 28 |
| 11-2 | 587.4 | | 2.1 | 1,400 | 6,260 | 1,510 | 1.2 | 42 | 32 | 20 | 24 |
| 11-3 | 585.1 | | 2.9 | 730 | 6,110 | 1,580 | 1.2 | 79 | 30 | 17 | 26 |
| 13-1 | 526.0 | 06-23-94 | 1.3 | 3,800 | 6,450 | 1,250 | 0.9 | 64 | 36 | 11 | 19 |
| 13-2 | 523.7 | | 1.7 | 2,800 | 7,860 | 1,290 | 0.9 | 43 | 22 | 14 | 16 |
| 18-1 | 414.5 | 06-28-94 | 2.4 | 770 | 4,370 | 2,720 | 1.7 | 73 | 68 | 51 | 62 |
| 18-2 | 411.8 | | 2.3 | 890 | 4,700 | 2,530 | 1.6 | ¹ 78 | 62 | 37 | 54 |
| 20-1 | 346.6 | 06-30-94 | 2.5 | 600 | 3,840 | 2,980 | 1.5 | ¹ 93 | 78 | 75 | 78 |
| 20-2 | 344.2 | | 4.2 | 240 | 4,240 | 3,080 | 1.5 | 85 | 78 | 53 | 73 |
| 21-1 | 331.4 | 07-01-94 | 3.2 | 360 | 3,730 | 2,780 | 1.4 | 44 | 88 | 66 | 74 |
| 22-1 | 306.0 | 07-02-94 | 3.3 | 320 | 3,580 | 2,910 | 1.5 | 42 | 87 | 77 | 81 |
| 24-2 | 274.4 | 07-03-94 | 2.8 | 720 | 5,620 | 2,880 | 1.4 | ¹ 74 | 52 | 48 | 51 |

¹Ratio of discharge is the measured discharge divided by the discharge listed in table 1.1 for the dam closest to the sampling transect unless a major tributary was between the sampling transect and the dam.

²Includes flow in secondary channels.

Mixing

Lateral gradients of specific conductance greater than $10\ \mu\text{S}/\text{cm}$ (twice the precision of the conductivity meter) were measured in 13 pools (table 1.5). Some of these pools have tributaries that contribute 2 percent or more of the discharge of the Mississippi River (Pool 2-Minnesota River; Pool 11-Turkey River; Pool 13-Maquoketa,; Pool 14-Wapsipinicon; Pool 16-Rock River; Pool 18-Iowa River; and Pool 20-Des Moines River) while other pools (5, 6, 8, 15, and 22) have smaller tributaries contributing less than 2 percent of the discharge. Pools 2, 5, 8, 11, 14, 16, 18, 20 and 22 had lateral gradients with difference across the pool that were greater than $10\ \mu\text{S}/\text{cm}$ before and after the flood of 1993.

Table 1.5 --Magnitude of specific-conductance difference between the ends of cross-pool sampling transects in some navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, July 1991-April 1992 and June-July 1994

[Only differences greater than 10 $\mu\text{S}/\text{cm}$ across the pool are listed; $\mu\text{S}/\text{cm}$, microsiemens per centimeter at 25 degrees Celsius; --, does not apply]

| Pool | Transect number | Specific-conductance differences ($\mu\text{S}/\text{cm}$) | |
|------|-----------------|--|----------------|
| | | July 1991-April 1992 | June-July 1994 |
| 2 | 1 | ¹ 17 | 20 |
| | 2 | ² 13 | 16 |
| 4 | 5 | 16 | -- |
| | 1 | -- | 27 |
| | 2 | -- | 25 |
| 5 | 2 | 80 | 17 |
| | 3 | 90 | 22 |
| 6 | 1 | 50 | -- |
| | 2 | 56 | -- |
| 8 | 1 | ¹ 12 | 35 |
| | 2 | ¹ 32 | 13 |
| | 3 | ¹ 16 | 17 |
| 8 | 2 | ³ 20 | -- |
| | 3 | ³ 17 | -- |
| 8 | 1 | ² 99 | -- |
| | 2 | ² 78 | -- |
| 11 | 1 | 20 | -- |
| | 2 | 19 | 25 |
| | 3 | 12 | -- |
| 13 | 1 | -- | 17 |
| | 2 | -- | -- |
| 14 | 3 | 16 | 13 |
| | 4 | 18 | 32 |
| 15 | 1 | 27 | -- |
| | 2 | 32 | -- |
| 16 | 1,2 | 141 | 76 |
| 18 | 1 | 83 | 27 |
| 20 | 1 | 52 | 53 |
| | 2 | 59 | 61 |
| 22 | 1 | 50 | 47 |
| | 2 | 37 | -- |

¹July-August 1991 cruise.

²April-May 1992 cruise.

³October-November 1991 cruise.

Flushing Rates

Governing officials of cities and towns along a river are concerned about pollution and the length of time that contaminated water may remain in their area (Ketchum, 1951; Ketchum and Keen, 1953; Rutherford and others, 1980). The Upper Mississippi River presents a difficult problem because the navigation pools are not water storage reservoirs nor are they like a free-flowing river, so standard methods for estimating retention times may not be applicable. The simplest standard method of computing an average retention time is to divide the volume of the pool by the mean annual discharge. Using data in table 1.1, this method gives a retention time for each pool that is a function of the length and changing cross-sectional area of the pool (table 1.6). This simple method is based on a conceptual model in which the water velocities are the same throughout the length of the pool, and the retention time is the time it takes for the water to flow from the upstream end to the downstream end of the pool. For a given discharge, the changing cross-sectional area of the pools in the riverine, deltaic, and lacustrine regions (table 1.4) will affect the water velocities in the longitudinal direction, and changes in depth and the presence or absence of islands will affect the water velocities in the lateral direction. Thus, the flushing rate, in hours per kilometer (h/km) of river, is perhaps a more applicable measure to use in constructing models that include downstream variations of the flushing rate. Different rates can be applied to the appropriate regions in the pool. By multiplying the flushing rate by the length of each appropriate region and summing over the length of the pool, an improved estimate for the retention time can be obtained that includes the effects of the downstream variation due to changes in morphology of the pool. The flushing rate is the reciprocal of the mean cross-sectional velocity for a specific cross section. The estimated flushing rates, equivalent to the retention times in table 1.6, were calculated by dividing the retention time by the length of the pool.

Flushing-rate measurements were made at 21 transects on the Upper Mississippi River during June-July 1994. The discharges ranged from one to two times the mean annual discharge, and the measured flushing rates are listed in table 1.6. The measured flushing rates ranged from 1.1 to 1.7 hr/km in the more lacustrine pools (2-13) and from 0.3 to 0.5 hour/km in the more riverine pools (14-24). The measured flushing rates were generally greater than or equal to the estimated flushing rates (see table 1.6).

Table 1.6--Estimated retention time, predicted flushing rates, and measured flushing rates in some navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994

[Measured flushing rate is the reciprocal of the average cross-sectional velocities listed in table 1.4 for June-July 1994; Q is the average of the measured discharges in the pool divided by the mean annual discharge in table 1.1; NA, data not available; h, hour, and km, kilometer]

| Pool | Estimated retention time ¹ (h) | Estimated flushing rate (h/km) | Measured flushing rate (h/km) | Q | Normalized distance ² |
|----------------|--|-----------------------------------|-------------------------------|-----|----------------------------------|
| 1 | NA | NA | NA | NA | NA |
| 2 | 69 | 1.3 | 1.2 | 1.8 | 0.06 |
| 3 | 20 | 0.7 | NA | NA | NA |
| ³ 4 | 200 | 2.8 | NA | NA | NA |
| 5 | 25 | 1.0 | 1.2 | 1.1 | 0.16 |
| 5A | 12 | 0.9 | NA | NA | NA |
| 6 | 17 | 0.7 | 1.1 | 1.5 | 0.46 |
| 7 | 30 | 1.6 | NA | NA | NA |
| 8 | 36 | 0.9 | 1.5 | 1.0 | 0.18 |
| 9 | 62 | 1.2 | 1.7 | 0.9 | 0.22 |
| 10 | 31 | 0.6 | NA | NA | NA |
| 11 | 41 | 0.8 | 1.1 | 1.2 | 0.16 |
| 12 | 10 | 0.2 | NA | NA | NA |
| 13 | NA | NA | 1.5 | 0.9 | 0.06 |
| 14 | NA | NA | NA | NA | NA |
| 15 | NA | NA | NA | NA | NA |
| 16 | 24 | 0.6 | NA | NA | NA |
| 17 | 16 | 0.5 | NA | NA | NA |
| 18 | NA | NA | 0.5 | 1.6 | 0.08 |
| 19 | 56 | 0.7 | NA | NA | NA |
| 20 | 15 | 0.4 | 0.4 | 1.5 | 0.11 |
| 21 | 12 | 0.4 | 0.4 | 1.4 | 0.36 |
| 22 | 15 | 0.4 | 0.3 | 1.5 | 0.21 |
| 24 | NA | NA | 0.5 | 1.4 | 0.05 |
| 25 | 26 | 0.5 | NA | NA | NA |
| 26 | 45 | 0.7 | NA | NA | NA |

¹Based on estimates of storage volumes and mean annual discharges from table 1.1.

²Normalized distance is the average distance of the transect(s) upstream from the dam divided by the length of the pool.

³Based on volume of Lake Pepin.

SEDIMENT CHARACTERISTICS

The surficial bed sediment was subsampled and analyzed for physical (particle-size) and bulk chemical (nitrogen, carbonate carbon, total carbon, and total organic carbon) characteristics. These characteristics have been used in some of the other chapters to normalize chemical data.

Particle Size

The composite samples for particle-size analysis were between 40 and 150 g and were sent to the U.S. Geological Survey Sediment Laboratory in Iowa City, Iowa. Each composite sample was first sieved to separate the fine fraction (less than 63 μm) from the coarse fraction (greater than 63 μm). The size distribution of the coarse fraction was determined by the sieve method for particle diameters greater than 1 mm and by the visual-accumulation tube method for particle diameters greater than 63 μm but less than 1 mm (Guy, 1969). Particle size of the fine fraction less than 63 μm was determined by the SediGraph method described by Lara and Matthes (1986). The U.S. Geological Survey is working with the American Society for Testing and Materials to develop standard reference samples for determining the accuracy of the sieve and visual accumulation-tube methods. At the present time, only a garnet reference sample is used to determine the accuracy of the SediGraph analysis, which is ± 1.5 percent (Matthes and others, 1992). The precision is determined by laboratory splits or by reanalyzing a sample. For the sieve analysis, one sample in 20 is reanalyzed; for the visual-accumulation-tube analysis, one sample each day is reanalyzed; and for the SediGraph analysis, one sample in 10 is reanalyzed. The reanalyzed sample must be within 5 percent for all analyses (Matthes and others, 1992).

The median diameter (table 1.7) was computed by linearly interpolating between particle diameters that bracket the value of "50 percent finer than." Surficial bed sediments in Lake Pepin in Pool 4 were predominantly clay sized and had the smallest median diameters ranging from 0.002 to 0.003 mm. Downstream from Lake Pepin and the Chippewa River, the median diameter increased to 0.22 mm in Pool 6. Other pools with sediment of relatively large median particle diameter are Pools 1, 14, 15, 16, 18, 20, 21, 22, and 24. Some pools have relatively large tributaries such as the Wisconsin River (Pool 10) and the Des Moines River (Pool 20); some pools (for example Pools 1, 2, 10, 14, and 19) are relatively narrow with a width-to-length ratio ($\text{Surface area}/\text{Length}^2$ from table 1.1) less than or equal to 0.03; and some (for example, Pool 10) have essentially no lacustrine region, and sampling transects were nearly parallel to the flow, reducing the heterogeneity of the samples and biasing the samples toward sand. The percentage of clay in the surficial bed sediments is shown in figure 1.5.

Table 1.7--Particle size of the surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994

[Analyses by U.S. Geological Survey Sediment Laboratory in Iowa City, Iowa; mm, millimeters; ns, not sampled]

| Pool and duplicate | Date 1994 | Number of samples in composite | Percent finer than indicated size in millimeters | | | | | | | | | | | | | | | | Median diameter ¹ (mm) |
|--------------------|-----------|--------------------------------|--|-----------|-------|-------|-------|-------|---------------------|-------|-------|-------|-----------|-------|-------|-------|------------|-----|-----------------------------------|
| | | | SediGraph | | | | | | Visual accumulation | | | | Sieve | | | | | | |
| | | | Clay (mm) | | | | | | Silt (mm) | | | | Sand (mm) | | | | Grave (mm) | | |
| | | | 1994 | 1991-1992 | 0.001 | 0.002 | 0.004 | 0.008 | 0.016 | 0.031 | 0.063 | 0.125 | 0.250 | 0.500 | 1.0 | 2.0 | 4.0 | 8.0 | |
| 1 | 06-11 | 12 | 12 | 1.3 | 1.8 | 2.3 | 2.7 | 3.1 | 3.3 | 3.4 | 6.3 | 33.8 | 88.7 | 97.4 | 99.5 | 100.0 | 0.324 | | |
| 2-1 | 06-12 | 18 | 18 | 9.4 | 12.8 | 16.2 | 20.5 | 26.6 | 37.2 | 48.3 | 74.6 | 90.2 | 94.1 | 95.3 | 97.5 | 100.0 | 0.066 | | |
| 2-2 | 06-12 | 18 | 18 | 1.8 | 5.1 | 9.2 | 14.2 | 21.1 | 33.9 | 50.8 | 77.3 | 90.6 | 95.1 | 96.2 | 98.3 | 100.0 | 0.060 | | |
| St. Croix | 06-13 | ns | 15 | 7.9 | 13.5 | 20.0 | 26.5 | 33.0 | 58.6 | 60.5 | 66.0 | 79.6 | 93.1 | 98.2 | 99.5 | 100.0 | 0.027 | | |
| 3 | 06-14 | 15 | 16 | 0.5 | 1.7 | 3.3 | 5.6 | 8.3 | 12.9 | 17.6 | 45.0 | 60.8 | 82.0 | 97.2 | 100.0 | | 0.165 | | |
| 24 | 06-15 | 14 | 15 | 27.2 | 42.0 | 62.8 | 82.0 | 92.9 | 97.8 | 98.8 | 99.0 | 99.3 | 99.9 | 100.0 | | | 0.003 | | |
| 34 | 06-15 | 20 | 21 | 34.2 | 48.8 | 65.5 | 77.5 | 83.5 | 84.7 | 85.6 | 85.7 | 89.3 | 98.7 | 100.0 | | | 0.002 | | |
| 5 | 06-16 | 18 | 18 | 0.9 | 3.4 | 6.8 | 11.2 | 15.5 | 27.4 | 45.6 | 60.7 | 73.1 | 88.2 | 100.0 | | | 0.080 | | |
| 6 | 06-17 | 20 | 20 | 4.0 | 5.2 | 6.2 | 6.9 | 7.5 | 7.9 | 8.0 | 23.0 | 56.8 | 87.8 | 93.5 | 99.8 | 100.0 | 0.220 | | |
| 7 | 06-18 | 20 | 20 | 0.6 | 2.6 | 5.4 | 8.7 | 11.7 | 20.7 | 40.3 | 63.6 | 85.2 | 98.5 | 99.4 | 100.0 | | 0.088 | | |
| 8-1 | 06-19 | 19 | 20 | 1.1 | 2.6 | 4.8 | 7.1 | 9.7 | 17.9 | 30.9 | 54.0 | 86.7 | 95.2 | 96.9 | 99.0 | 100.0 | 0.113 | | |
| 8-2 | 06-19 | 19 | 20 | 3.6 | 5.9 | 8.3 | 11.2 | 14.2 | 21.0 | 30.2 | 55.3 | 86.2 | 94.9 | 98.7 | 100.0 | | 0.111 | | |
| 9 | 06-20 | 18 | 18 | 3.1 | 9.2 | 16.6 | 24.9 | 36.7 | 67.3 | 87.4 | 96.7 | 99.3 | 99.6 | 99.6 | 100.0 | | 0.023 | | |
| 10 | 06-21 | 20 | 20 | 3.9 | 7.0 | 11.3 | 16.2 | 20.5 | 30.3 | 40.9 | 50.1 | 76.5 | 93.1 | 98.5 | 100.0 | | 0.125 | | |
| 11 | 06-21 | 20 | 20 | 1.3 | 4.6 | 8.4 | 13.56 | 20.47 | 37.1 | 51.2 | 69.1 | 87.0 | 98.2 | 99.7 | 100.0 | | 0.059 | | |
| | 06-22 | | | | | | | | | | | | | | | | | | |
| 12 | 06-22 | 20 | 20 | 0.5 | 4.5 | 10.3 | 18.3 | 30.0 | 56.8 | 89.4 | 95.8 | 99.3 | 99.9 | 99.9 | 100.0 | | 0.028 | | |
| 13 | 06-23 | 20 | 20 | 2.1 | 5.8 | 11.9 | 18.5 | 26.7 | 50.1 | 78.1 | 87.5 | 96.2 | 99.5 | 99.5 | 100.0 | | 0.031 | | |
| 14 | 06-23 | 16 | 16 | 2.7 | 5.3 | 10.4 | 16.2 | 22.9 | 31.8 | 33.8 | 35.5 | 58.6 | 97.9 | 99.3 | 100.0 | | 0.203 | | |
| | 06-24 | | | | | | | | | | | | | | | | | | |
| 15 | 06-26 | 15 | 18 | 5.7 | 8.1 | 11.3 | 15.1 | 22.2 | 34.9 | 40.4 | 42.8 | 50.2 | 78.9 | 93.7 | 98.4 | 100.0 | 0.250 | | |
| 16 | 06-27 | 419 | 19 | 1.2 | 2.9 | 5.7 | 9.6 | 14.6 | 24.7 | 33.5 | 37.1 | 54.3 | 90.5 | 99.4 | 100.0 | | 0.219 | | |

Table 1.7--Particle size of the surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994--Continued

| Pool and duplicate | Date 1994 | Number of samples in composite | Percent finer than indicated size in millimeters | | | | | | | | | | | | | | | Median diameter ¹ (mm) |
|--------------------|-----------|--------------------------------|--|-------|-------|-------|-------|---------------------|-------|-------|-------|-------|-----------|-------|-------|-------|-------|-----------------------------------|
| | | | SediGraph | | | | | Visual accumulation | | | | | Sieve | | | | | |
| | | | Clay (mm) | | | | | Silt (mm) | | | | | Sand (mm) | | | | | |
| | | | 0.001 | 0.002 | 0.004 | 0.008 | 0.016 | 0.031 | 0.063 | 0.125 | 0.250 | 0.500 | 1.0 | 2.0 | 4.0 | 8.0 | | |
| 1994 | 1991-1992 | | | | | | | | | | | | | | | | | |
| 18 | 06-28 | 518 | 0.4 | 2.6 | 6.0 | 10.1 | 15.9 | 28.4 | 39.8 | 45.5 | 62.3 | 92.3 | 97.4 | 99.8 | 100.0 | | 0.158 | |
| 19-1 | 06-29 | 23 | 9.2 | 14.9 | 22.2 | 32.0 | 44.4 | 59.9 | 63.4 | 64.2 | 66.2 | 84.2 | 96.4 | 99.0 | 100.0 | | 0.022 | |
| 19-2 | 06-29 | 22 | 2.2 | 6.7 | 12.4 | 20.2 | 29.1 | 44.2 | 53.8 | 54.0 | 55.0 | 85.0 | 96.3 | 99.3 | 100.0 | | 0.050 | |
| 20 | 06-30 | 612 | 3.3 | 3.8 | 4.4 | 4.8 | 5.4 | 6.5 | 8.2 | 12.0 | 19.7 | 64.4 | 91.8 | 97.6 | 100.0 | | 0.419 | |
| 21 | 07-01 | 16 | 3.2 | 5.2 | 7.5 | 10.3 | 14.1 | 23.0 | 28.2 | 33.7 | 47.2 | 90.2 | 97.2 | 99.2 | 100.0 | | 0.266 | |
| 22 | 07-02 | 20 | 2.6 | 4.8 | 8.2 | 12.5 | 18.8 | 27.6 | 32.0 | 34.8 | 52.2 | 93.9 | 98.9 | 100.0 | | | 0.234 | |
| 24 | 07-03 | 18 | 2.7 | 5.6 | 10.6 | 16.2 | 24.3 | 34.4 | 36.0 | 38.3 | 49.9 | 79.3 | 95.5 | 98.8 | 100.0 | | 0.250 | |
| 25-1 | 07-04 | 18 | 4.1 | 9.2 | 16.8 | 26.7 | 41.6 | 59.6 | 63.4 | 67.3 | 72.0 | 88.1 | 96.7 | 99.5 | 100.0 | | 0.023 | |
| 25-2 | 07-04 | 9 | 6.6 | 11.3 | 16.6 | 24.8 | 38.0 | 57.5 | 62.8 | 65.1 | 70.0 | 90.5 | 97.0 | 98.9 | 99.6 | 100.0 | 0.026 | |
| 26 | 07-05 | 11 | 7.6 | 13.6 | 23.0 | 33.6 | 49.1 | 71.0 | 75.5 | 82.4 | 95.9 | 99.2 | 99.5 | 100.0 | | | 0.017 | |

¹Median diameter determined by straight-line interpolation.

²Upper Lake Pepin.

³Lower Lake Pepin.

⁴Eight sites were not resampled in the same locations.

⁵Five sites were not resampled in the same locations.

⁶Two sites were sampled out of the water.

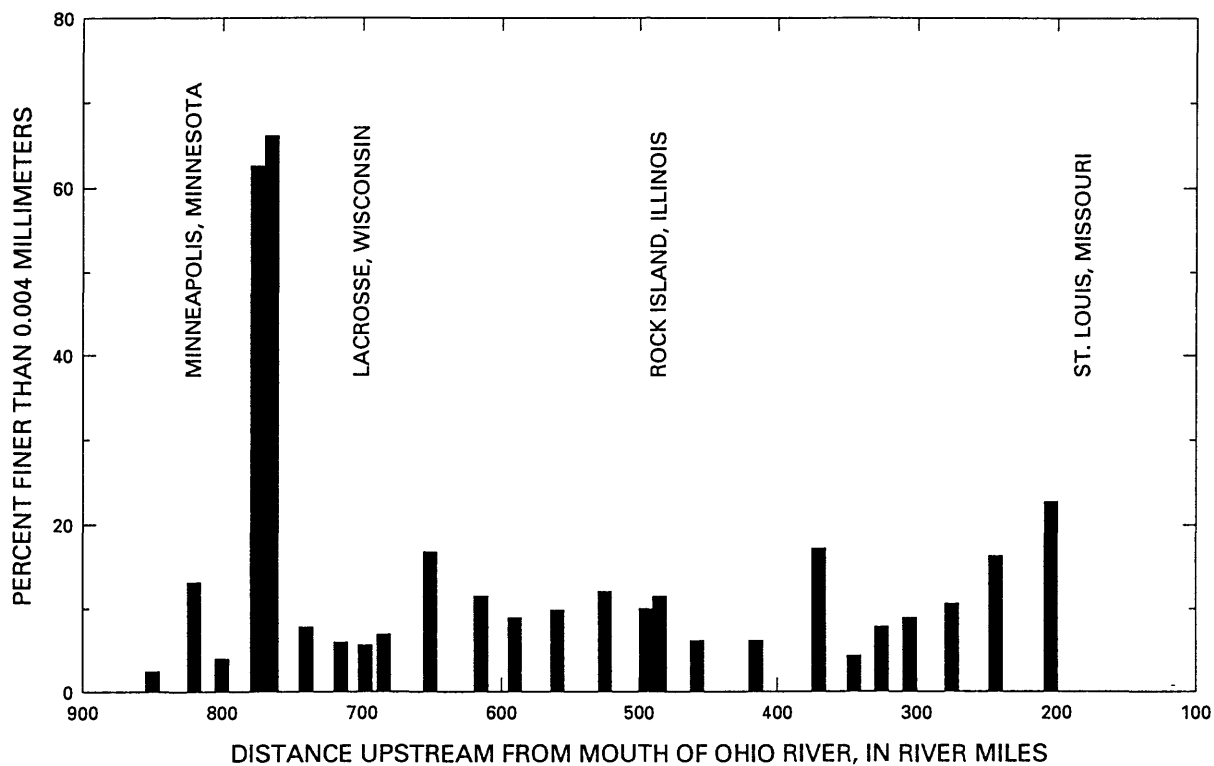


Figure 1.5--Percentage of surficial bed sediments finer than 0.004 millimeter collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994. See table 1.2 for location of pools.

Bulk Chemistry

Subsamples were analyzed for the bulk chemical composition of percent nitrogen, percent carbonate carbon, percent total carbon, and percent organic carbon. Percentage values are based on dry weight. All samples were dried at a temperature of 105°C until a constant weight was obtained. Nitrogen was determined by high-temperature combustion on a Carlo Erba nitrogen detector. Total organic carbon was determined by combustion and infrared detection (total carbon samples collected before the flood of 1993 were analyzed by combustion and coulometric detection; Moody and Anderson, 1997). Carbonate carbon was determined by acidification and coulometric detection. Organic carbon was determined by difference between the percentages of carbonate carbon and total carbon and is plotted in figure 1.6. Total volatile solids was measured as 100 percent minus the loss of mass (percent) on ignition at 750°C. Huffman Laboratories, Inc., Golden, Colo., performed all the analyses, and the laboratory accuracy and precision uncertainty were determined by multiple measurements of the standard homogeneous reference material of total carbon (CaCO₃, triphenyl methane, steric acid, and National Institute for Standards and Technology Buffalo River Sediment), carbonate carbon (CaCO₃ and Na₂CO₃), and nitrogen (acetanilide, atropine, sulfanilamide, and nicotinic acid p-toluene sulfonate). The accuracy is the average percent difference from the "true" value, and the precision is the average of the relative standard deviations (table 1.8).

The precision uncertainty for measurements of field samples (which may be inhomogeneous) was also determined by multiple laboratory replicates (four or more) taken from samples from pools which were known (Moody and Anderson, 1997) to have high and low values of nitrogen (0.14 and 0.02 percent), carbonate carbon (0.55 and 0.03 percent), total carbon (4.34 and 0.15), and total volatile solids (13.93 and 0.91). The precision is measured as the relative standard deviations of these replicates (table 1.8). The bulk chemistry data are listed in table 1.9.

Table 1.8--Accuracy and precision estimates for total carbon, carbonate carbon, nitrogen measurements, and total volatile solids

[% , percent; and na, not available]

| Analysis | Accuracy | | Precision | |
|-----------------------|--------------------|--------------------|--------------|------------|
| | Reference standard | Reference standard | Field sample | |
| | | | Low value | High value |
| | (%) | (%) | (%) | (%) |
| Total carbon | 0.6 | 1.0 | 15 | 6 |
| Carbonate carbon | 0.2 | 0.4 | 30 | 22 |
| Nitrogen | 0.4 | 0.8 | 50 | 27 |
| Total volatile solids | 4 | na | 13 | 6 |

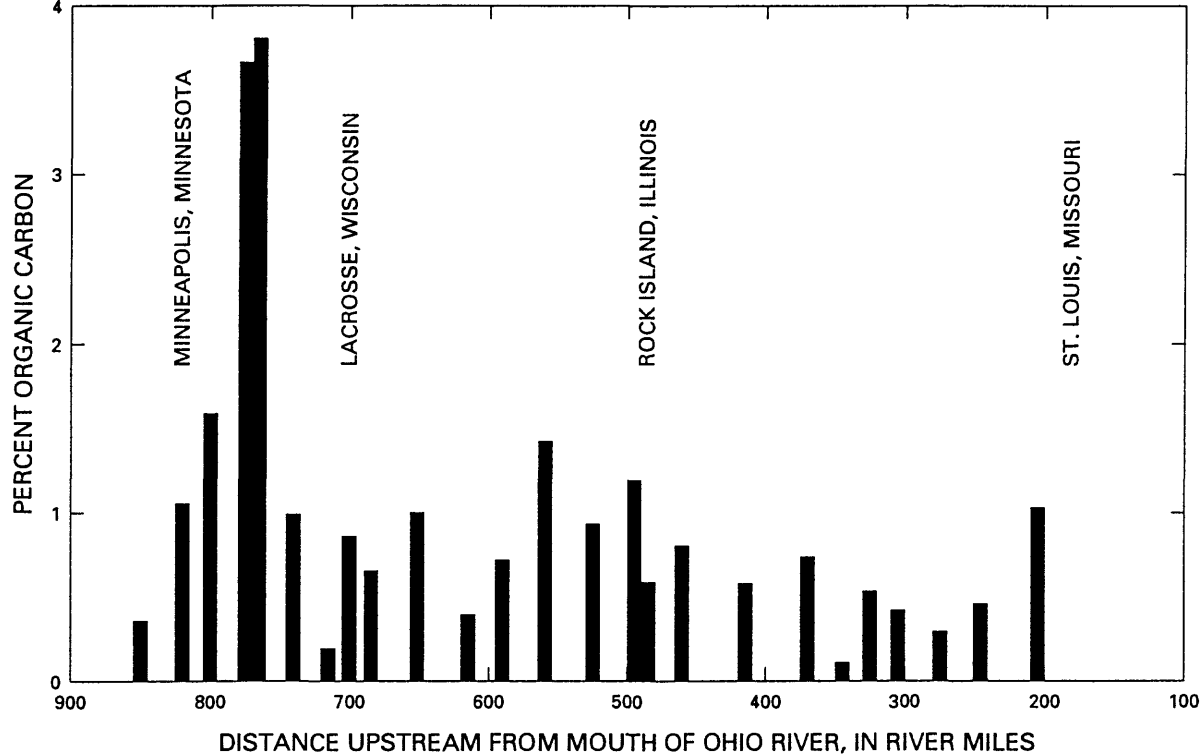


Figure 1.6--Percent organic carbon in surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994. See table 1.2 for location of pools.

Table 1.9--Bulk chemical characteristics of surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994

[Samples were analyzed by Huffman Laboratories, Inc., Golden, Colorado; Reference, Lake Pepin reference standard; --, not measured]

| Pool and duplicate | Date | Number of samples in composite | | Percentage of dry weight | | | | |
|--------------------|--------------------|--------------------------------|-----------|--------------------------|------------------|--------------|----------------------|-----------------------|
| | | 1994 | 1991-1992 | Nitrogen | Carbonate carbon | Total carbon | Total organic carbon | Total volatile solids |
| Reference | 05-15-91 | | | 0.53 | 0.73 | 5.39 | 4.66 | 16.33 |
| 1 | 06-11-94 | 12 | 12 | 0.02 | 0.17 | 0.54 | 0.37 | 1.90 |
| 2-1 | 06-12-94 | 18 | 18 | 0.12 | 1.22 | 2.15 | 0.93 | 7.79 |
| 2-2 | 06-12-94 | 18 | 18 | 0.11 | 1.15 | 2.33 | 1.18 | 7.60 |
| St. Croix River | 06-13-84 | 15 | 15 | 0.24 | 0.25 | 2.79 | 2.54 | 9.16 |
| 3 | 06-14-94 | 15 | 16 | 0.20 | 1.07 | 2.67 | 1.60 | 8.07 |
| ¹ 4 | 06-15-94 | 14 | 15 | 0.43 | 1.23 | 4.88 | 3.65 | 14.70 |
| ² 4 | 06-15-94 | 20 | 21 | 0.14 | 0.55 | 4.34 | 3.79 | 13.93 |
| 5 | 06-16-94 | 18 | 18 | 0.15 | 0.30 | 1.29 | 0.99 | 3.90 |
| 6 | 06-17-94 | 20 | 20 | 0.01 | 0.06 | 0.26 | 0.20 | 1.22 |
| 7 | 06-18-94 | 20 | 20 | 0.10 | 0.25 | 1.13 | 0.88 | 3.58 |
| 8-1 | 06-19-94 | 19 | 20 | 0.05 | 0.32 | 1.17 | 0.85 | 4.34 |
| 8-2 | | 19 | 20 | 0.05 | 0.39 | 0.87 | 0.48 | 3.13 |
| 9 | 06-20-94 | 18 | 18 | 0.14 | 0.71 | 1.71 | 1.00 | 5.90 |
| 10 | 06-21-94 | 20 | 20 | 0.05 | 0.61 | 1.00 | 0.39 | 4.37 |
| 11 | 06-21 and 06-22-94 | 20 | 20 | 0.06 | 0.73 | 1.46 | 0.73 | 5.08 |
| 12 | 06-22-94 | 20 | 20 | 0.12 | 0.51 | 1.94 | 1.43 | 4.98 |
| 13 | 06-23-94 | 20 | 20 | 0.12 | 0.65 | 1.60 | 0.95 | 5.00 |
| 14 | 06-23 and 06-24-94 | 16 | 16 | 0.06 | 0.14 | 1.35 | 1.21 | 5.47 |
| 15 | 06-26-94 | 15 | 18 | 0.06 | 0.20 | 0.78 | 0.58 | 2.80 |
| 16 | 06-27-94 | ³ 19 | 19 | 0.07 | 0.33 | 1.16 | 0.83 | 3.85 |
| 18 | 06-28-94 | ⁴ 18 | 18 | 0.06 | 0.32 | 0.91 | 0.59 | 3.55 |

**Table 1.9--Bulk chemical characteristics of surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River between Minneapolis, Minnesota, and St. Louis, Missouri, June-July 1994--
Continued**

| Pool and duplicate | Date | Number of samples in composite | | Percentage of dry weight | | | | |
|--------------------|----------|--------------------------------|-----------|--------------------------|------------------|--------------|----------------------|-----------------------|
| | | 1994 | 1991-1992 | Nitrogen | Carbonate carbon | Total carbon | Total organic carbon | Total volatile solids |
| 19-1 | 06-29-94 | 23 | 23 | 0.09 | 0.23 | 1.03 | 0.80 | 4.07 |
| 19-2 | | 22 | 23 | 0.08 | 0.52 | 1.23 | 0.71 | 5.40 |
| 20 | 06-30-94 | ⁵ 12 | 12 | ⁶ 0.02 | 0.03 | 0.15 | 0.12 | 0.91 |
| 21 | 07-01-94 | 16 | 19 | 0.05 | 0.11 | 0.66 | 0.55 | 3.07 |
| 22 | 07-02-94 | 20 | 20 | 0.04 | 0.13 | 0.58 | 0.45 | 2.16 |
| 24 | 07-03-94 | 18 | 18 | 0.03 | 0.10 | 0.41 | 0.31 | 2.03 |
| 25-1 | 07-04-94 | 18 | 19 | 0.11 | 0.19 | 1.00 | 0.81 | 5.18 |
| 25-2 | | 9 | 19 | 0.09 | 0.60 | 0.74 | 0.14 | 3.90 |
| 26 | 07-05-94 | 11 | 13 | 0.12 | 0.15 | 1.20 | 1.05 | 5.52 |

¹Upper Lake Pepin.

²Lower Lake Pepin.

³Eight sites were not resampled in the same locations.

⁴Five sites were not resampled in the same locations.

⁵Two sites were sampled out of the water.

⁶Two laboratory replicate analyses were reported as less than 0.01 and were not included in the values listed here.

SUMMARY

A representative, composite, surficial bed-sediment sample was collected from the downstream one-third of 24 navigation pools by compositing 12 to 23 individual samples from 1 to 5 transects across the pools. These individual samples were collected away from the main navigation channel in backwater regions where the water depths ranged from about 0.3 m to about 3.0 m and where the water velocities were about 60 percent of the velocity in the main navigation channel. Estimates of flushing rates varied from 0.3 hr/km to about 1.7 hr/km. The median particle diameter of the surficial bed sediments ranged from 0.002 mm in lower Lake Pepin (or Pool 4) to 0.42 mm in Pool 20. The organic carbon associated with the surficial bed sediments ranged from 0.12 percent in Pool 20 to 3.8 percent in Lower Lake Pepin (or Pool 4). Nitrogen was lowest in Pool 6 (0.01 percent) and highest (0.43 percent) in Upper Lake Pepin (or Pool 4).

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CHAPTER 2 - Sterols, Polynuclear Aromatic Hydrocarbons, and Linear Alkylbenzene Sulfonates

By Larry B. Barber, II, and Jeffrey H. Writer

ABSTRACT

Fecal sterols, polynuclear aromatic hydrocarbons, and linear alkylbenzene sulfonates were measured in surficial bed-sediment samples collected from 24 of the navigation pools on the Upper Mississippi River in June and July 1994. These samples were collected 1 year after the flood of 1993. Fecal sterols, polynuclear aromatic hydrocarbons, and linear alkylbenzene sulfonates are relatively biorefractory compounds that accumulate in the bed sediments and are indicative of sewage and industrial contamination. The rates of biodegradation vary; fecal sterols are the most stable, polynuclear aromatic hydrocarbons show a range of degradation rates, and linear alkylbenzene sulfonates are the most degradable. Coprostanol concentrations ranged from 0.23 to 4.41 milligrams per kilogram in the postflood samples, total polynuclear aromatic hydrocarbons concentrations ranged from 0.10 to 5.28 milligrams per kilogram, and linear alkylbenzene sulfonate concentrations ranged from 0.03 to 1.07 milligrams per kilogram.

INTRODUCTION

The Upper Mississippi River between Minneapolis, Minn., and St. Louis, Mo., contains a series of 29 pools formed by navigation locks and dams which trap sediment and sediment-bound organic contaminants at accumulation rates of 1 to 4 cm/yr (McHenry and others, 1984). The Mississippi River receives many organic contaminants from a variety of both point and nonpoint sources; of particular interest to this study was the effect of municipal wastewater discharge on the bed sediments of the Upper Mississippi River.

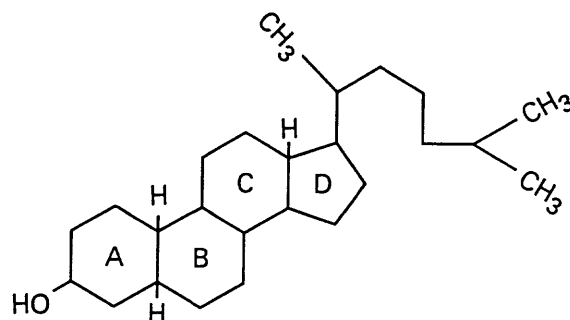


Figure 2.1--Chemical structure of coprostanol. A, B, C, and D are ring labels for the molecule; HO is the hydroxyl group; H is the point of reductive hydrogenation of the molecule; CH₃ are methyl groups.

Fecal sterols are present in the feces of humans, livestock, and birds (Walker and others, 1982; Subbiah and others, 1972; Nishimura and Koyama, 1977), are associated primarily with particulate matter, and accumulate in the bed sediments (Hatcher and McGillvary, 1979; Brown and Wade, 1984). Routinely monitored parameters such as nutrients, oxygen demand, and fecal coliform bacteria are fairly transient in the river environment in contrast to nonionic-organic contaminants such as coprostanol (fig. 2.1). Because coprostanol is biodegraded slowly, it can be used as a molecular indicator of long-term sewage effects on the environment (Hatcher and McGillvary, 1979; Brown and Wade, 1984; Venkatsen and Kaplan, 1990). Tabak and others (1977) conducted a limited analysis of coprostanol in the Mississippi River around the Burlington, Iowa, wastewater-treatment plant and found that the sediments in that reach of the river had been contaminated by fecal sterols.

Polynuclear aromatic hydrocarbons (PAH) are an important class of organic contaminants that include many individual compounds (fig. 2.2). PAH come primarily from the combustion of plant material and fossil fuels such as coal and petroleum. Because of their many natural and anthropogenic sources and their widespread occurrence (Jones and Leber, 1979; Hoffman and others, 1984; Boehm and Farrington, 1984; Barrick and others, 1984), PAH are general indicators of sediment contamination. These compounds have a wide range of molecular structures and consequently have a wide range of environmental behaviors such as sorption, volatilization, and biodegradation.

Linear alkylbenzene sulfonates (LAS) are the most common anionic surfactants used in the United States for detergent formulations. Their annual consumption is about 4×10^5 metric tons (Modler and others, 1993). Most LAS are consumed in domestic and commercial applications and disposed of in wastewater. LAS formulations are a mixture of homologues and isomers (fig. 2.3). The alkyl-chain length varies from C₁₀ to C₁₄, and the point of attachment for the alkyl chain varies from the 2-phenyl to the 7-phenyl position. LAS are readily biodegraded under aerobic conditions, and sewage treatment is effective in removing more than 90 percent of LAS (Rapaport and Eckhoff, 1990). However, LAS slowly biodegrade under anaerobic conditions (Larson and Payne, 1981; Federle and Schwab, 1992). Because of their high water solubility and anionic character, LAS are not as strongly sorbed to sediments as compounds such as sterols and PAH (Hand and Williams, 1987).

The sorption of organic contaminants to sediments depends primarily on the water solubility of the compounds and the characteristics of the sediment (Chiou and others, 1983; Karickhoff, 1984; Leenheer, 1991). As the water solubility of a compound decreases, its sorption to sediments typically increases. The most important sediment variables for sorption of organic contaminants are sediment-organic-matter concentrations and clay content. Smaller particles have a higher percentage of organic coatings because of the large surface area:volume ratio, and an inverse relation between particle size and percentage of organic carbon commonly exists in natural sediments (Barber, 1994).

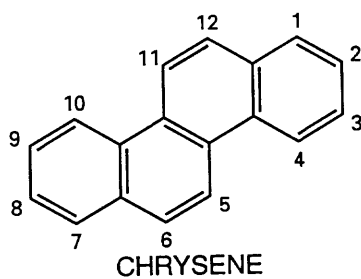
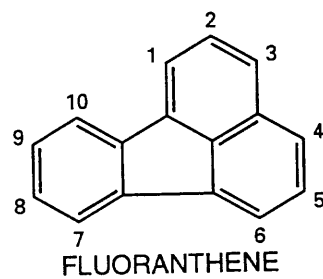
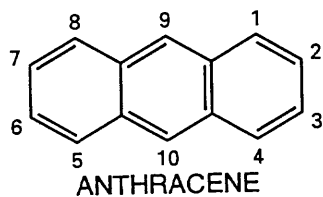
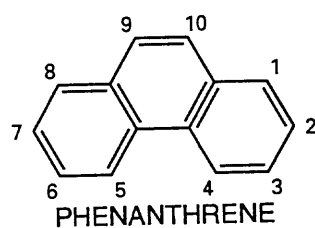
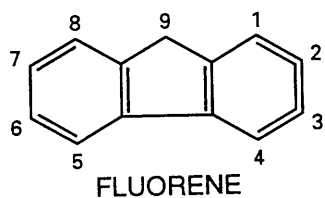
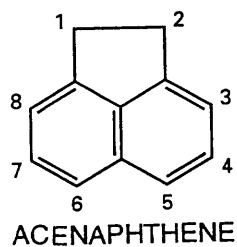
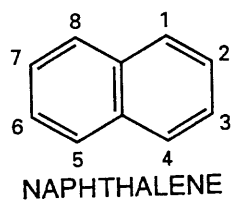


Figure 2.2--Chemical structure of some polynuclear aromatic hydrocarbons.

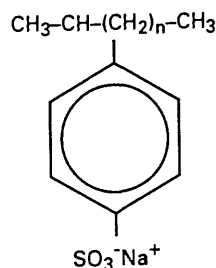


Figure 2.3--Chemical structure of linear alkylbenzene sulfonate. This example shows a 2-phenyl isomer where n ranges from 7 to 11.

PURPOSE AND SCOPE

In the summer of 1993, the Upper Mississippi River flooded extensively. The purpose of this chapter is to (1) report the concentrations of fecal sterols, PAH, and LAS in surficial bed sediments collected from the navigation pools of the Upper Mississippi River after the flood, and (2) describe the analytical methods. Tables and graphs of the data are presented to show the longitudinal distribution of the concentrations of these compounds. These data and data obtained prior to the flood (Barber and others, 1997; Writer and others, 1995; Tabor and Barber, 1996) can be used to evaluate changes caused by the flood.

METHODS

Sample Collection and Preservation

Samples were collected in the Upper Mississippi River from the lower one-third of 24 of the 29 navigation pools. A composite sample also was collected from the St. Croix River upstream from the confluence with the Upper Mississippi River. Locations of the pools are shown in figure.1.1, and the method for collecting a representative composite sample is described in Chapter 1. All composite samples were preserved with 10 mL of chloroform and stored at 4°C.

Sterols and Polynuclear Aromatic Hydrocarbons

The sterols were extracted from the bed sediments and measured by gas chromatography-mass spectroscopy (GC-MS). The analytical procedures were similar to those used for analyzing samples collected in 1991-92 (Barber and others, in press) with a few minor exceptions that are discussed herein. The extraction procedure (Brown and Wade, 1984) entailed saponification/extraction of 50 g of wet sediment for 2.5 hours with a 100-mL solution of 0.5 N potassium hydroxide in methanol and 10 mL benzene. The extract was filtered to remove sediment, the potassium hydroxide was neutralized with hydrochloric acid, and the extract was partitioned between water and methylene chloride. The methylene chloride extract was evaporated under nitrogen gas to dryness, and the residue was taken up in 10 mL of hexane. The hexane extract was evaporated under nitrogen gas to 2 mL and applied to a column using a Waters 1A Millilab robotics system. The preflood analytical procedures utilized a column of neutral silica (0.35 g) over neutral alumina (0.75 g), while the postflood analytical procedure utilized only neutral silica (690 g). Evaluation of the two columns indicated little difference in compound separation. The extract was then fractionated using a sequential elution procedure of hexane (5 mL), benzene (5 mL), and methanol (5 mL). The PAH were eluted from the column in the initial hexane fraction because of residual benzene in the robotics system. The methanol fraction was derivatized using Tri-Sil 'Z' (Pierce, Rockford, Ill.) to convert the free sterols to their trimethyl silyl ethers. Sterols were quantified by comparison with the surrogate deuterated standard d_7 -cholesterol added at the beginning of the analytical procedure. PAH were quantified by comparison with five deuterated PAH added at the beginning of the analytical procedure (d_8 -naphthalene, d_{10} -cenaphthalene, d_{12} -phenanthrene, d_{12} -chrysene, and d_{12} -perylene).

Gas Chromatography-Mass Spectrometry Analysis

Gas chromatography-mass spectrometry analysis was performed on a Hewlett-Packard 5890 gas chromatograph with a Hewlett-Packard Ultra II column (25-m \times 0.2-mm inside diameter and 20- μ m film thickness), a splitless injection port, ultrahigh-purity helium as the carrier gas (27 cm/s liner flow velocity), and a mass spectrometer interface temperature of 280°C. A Hewlett-Packard 5970 mass selective detector (MSD) was used with a source temperature of 250°C, a source pressure of 1.5×10^{-5} torr, and an ionization energy of 70 eV. Additional GC-MS operating conditions are listed in table 2.1. The sample extracts were analyzed in full-scan mode [mass-to-charge ratios (m/z) range from 45 to 550 atomic mass units/electron unit (amu/eu)] at a rate of one scan per second and in selected-ion monitoring (SIM) mode with a dwell time of 50 milliseconds. Identification was achieved by comparison of full-scan mass spectra and retention times with authentic standards and library searches. Quantitation was based on the SIM data. Sterols were determined by analysis of the methanol fraction of the sediment extract, and PAH were determined in the hexane/benzene extracts. Because of the similar chemical characteristics between the target compounds and the deuterated surrogate standards, concentrations were not corrected for recovery.

Table 2.1--Gas chromatograph operating conditions for sterol, polynuclear aromatic hydrocarbon, and linear alkylbenzene sulfonate analyses

[°C, degree Celsius; min, minute]

| Condition | Sterol | Polynuclear aromatic hydrocarbon | Linear alkylbenzene sulfonate |
|---------------------------------|--------|----------------------------------|-------------------------------|
| Injection port temperature (°C) | 290 | 290 | 280 |
| Initial temperature (°C) | 60 | 60 | 110 |
| Initial time (min) | 2 | 2 | 1 |
| Ramp rate °C/min | 10 | 10 | 8 |
| Final temperature (°C) | 300 | 300 | 300 |
| Final time (min) | 20 | 20 | 5 |

Linear Alkylbenzene Sulfonates

Linear alkylbenzene sulfonates were extracted from the bed sediments by placing 15-30 g of wet sediment in a centrifuge tube, removing pore water by centrifuging at 3,500 rpm for 20 minutes, and pipetting off the supernatant for later analysis. Ten mL of methanol was added to the sediment and the sediment was extracted on a rotary mixer for 1 hour. Each sample was then centrifuged at 3,500 rpm for 20 minutes and the supernatant liquid transferred to a holding vial. The extraction process was repeated two more times, using an extraction time of 12 hours. The extracts were combined, quantitatively transferred to a 5-mL reaction vial, and evaporated to dryness under nitrogen gas.

The extract residues were derivatized with phosphorus pentachloride and 2,2,2-trifluoroethanol to form the trifluoroethyl esters of LAS (Trehy and others, 1990). All samples were analyzed using a Hewlett-Packard 5890 GC coupled to a Hewlett-Packard 5970 MSD mass spectrometer (table 2.1). Linear alkylbenzene sulfonates were quantified by comparison with the surrogate standard C₉-LAS (provided by the Procter Gamble Company, Cincinnati, Ohio) added to the sediment before extraction. A C₈-LAS (Aldrich) derivatization standard was added to the sample residue after extraction but before derivatization. Further discussion on LAS analytical methodology is presented by Barber and others (1997).

Accuracy and Precision

Estimates of accuracy were determined from the standard deviation of the percent recovery of deuterated compounds added to the extracts (tables 2.2 and 2.3). The LAS accuracy is the percent recovery of C₉-LAS normalized to the C₈-LAS derivatization standard (each added in equal concentrations). The precision is the relative standard deviation from multiple analyses of a surrogate compound for each class of compounds (sterols, d₇-cholesterol; LAS, C₉-LAS; and PAH, average of d₈-naphthalene, d₁₀-acenaphthalene, d₁₀-phenanthrene, d₁₂-chrysene, and d₁₂-perylene).

Table 2.2--Accuracy and precision estimates for sterol, polynuclear aromatic hydrocarbon, and linear alkylbenzene sulfonate measurements

[%, percent; >, greater than]

| Class | Accuracy (%) | Precision (%) |
|-----------------------------------|------------------|---------------|
| Sterols | >95 ¹ | 20 |
| Polynuclear aromatic hydrocarbons | >95 ¹ | 22 |
| Linear alkylbenzene sulfonates | 34 | 40 |

¹Quantified by comparison against a surrogate standard added at the beginning of the analytical procedure; thus, the accuracy is assumed to be greater than 95 percent.

Table 2.3--Variability of cholestanol, cholesterol, coprostanol, and polynuclear aromatic hydrocarbons in duplicate samples collected from Pools 2, 8, and 19, and triplicate extraction of surficial sediment from Pool 3

[S, sample; mg, milligram; kg, kilogram; %, percent; RPD, relative percent difference; STD, standard deviation; RSTD, relative standard deviation; nd, not detected; na, not applicable; PAH, polynuclear aromatic hydrocarbons]

| | Extractions | | | | | | | | | Triplicate extraction | | |
|--|--------------------|--------------------|-------------|--------------------|--------------------|-------------|--------------------|--------------------|-------------|-----------------------|--------------------|-------------|
| | Pool 2 | | | Pool 8 | | | Pool 19 | | | Pool 3 | | |
| | S 1 (mg/ kg) | S 2 (mg/ kg) | RPD (%) | S 1 (mg/ kg) | S 2 (mg/ kg) | RPD (%) | S 1 (mg/ kg) | S 2 (mg/ kg) | RPD (%) | Average (mg/kg) | STD (mg/ kg) | RSTD (%) |
| Sterols | | | | | | | | | | | | |
| Cholestanol | 0.89 | 1.11 | 21.7 | 0.46 | 0.47 | 2.55 | 1.12 | 1.16 | 2.91 | 1.11 | 0.02 | 1.55 |
| Cholesterol | 2.70 | 2.55 | 5.71 | 1.63 | 1.58 | 2.86 | 4.08 | 3.24 | 22.9 | 2.37 | 0.10 | 4.06 |
| Coprostanol | 0.78 | 1.01 | 26.1 | 0.18 | 0.15 | 18.0 | 0.31 | 0.27 | 12.7 | 0.38 | 0.04 | 10.7 |
| Polynuclear aromatic hydrocarbons | | | | | | | | | | | | |
| Corrected Naphthalene | 0.034 | 0.029 | 17.0 | nd | nd | na | nd | nd | na | 1.03 | 0.05 | 5.28 |
| Acenaphthathene | 0.017 | 0.014 | 16.6 | 0.080 | 0.002 | 188 | 0.319 | 0.041 | 154 | 0.38 | 0.44 | 115 |
| Acenaphthene | 0.015 | 0.016 | 3.48 | nd | 0.002 | na | nd | 0.009 | na | 0.00 | 0.00 | 141 |
| Fluorene | 0.019 | 0.023 | 18.2 | nd | 0.003 | na | nd | 0.022 | na | 0.05 | 0.03 | 51.3 |
| Phenanthrene | 0.248 | 0.205 | 19.1 | 0.010 | 0.024 | 79.3 | 0.026 | 0.028 | 8.76 | 0.09 | 0.01 | 8.75 |
| Anthracene | 0.027 | 0.015 | 55.8 | 0.001 | 0.004 | 134 | 0.008 | 0.009 | 10.9 | 0.01 | 0.00 | 21.7 |
| Fluoranthene | 0.539 | 0.359 | 39.9 | 0.030 | 0.041 | 29.5 | 0.068 | 0.053 | 23.9 | 0.21 | 0.02 | 10.8 |
| Pyrene | 0.606 | 0.329 | 59.3 | 0.027 | 0.034 | 24.9 | 0.075 | 0.058 | 25.7 | 0.19 | 0.02 | 11.3 |
| Benzo[a] anthracene | 0.178 | 0.106 | 50.9 | 0.005 | 0.010 | 63.3 | 0.023 | 0.023 | 3.46 | 0.06 | 0.00 | 1.71 |
| Chrysene | 0.332 | 0.216 | 42.3 | 0.016 | 0.020 | 22.9 | 0.035 | 0.038 | 8.47 | 0.14 | 0.00 | 1.05 |
| Benzo[b] fluoranthene | 0.357 | 0.293 | 19.6 | 0.015 | 0.025 | 48.2 | 0.051 | 0.061 | 16.7 | 0.21 | 0.01 | 4.20 |
| Benzo[k] fluoranthene | nd | nd | na | nd | nd | na | nd | nd | na | 0.00 | 0.00 | 0.00 |
| Benzo[a]pyrene | 0.142 | 0.076 | 61.1 | nd | 0.005 | na | 0.021 | 0.023 | 7.94 | 0.04 | 0.00 | 2.72 |
| Benzo[ghi] perylene | 0.176 | 0.115 | 41.8 | nd | nd | na | 0.008 | 0.015 | 55.2 | 0.04 | 0.01 | 19.4 |
| Indeno [1,2,3-cd] pyrene | 0.259 | 0.155 | 50.4 | nd | nd | na | 0.010 | 0.017 | 53.7 | 0.05 | 0.01 | 21.5 |
| Dibenzo- [a,h] anthracene | 0.076 | 0.046 | 48.9 | nd | nd | na | 0.004 | 0.008 | 53.3 | 0.01 | 0.01 | 75.6 |
| Total PAH | 3.025 | 1.997 | 41.0 | 0.185 | 0.171 | 7.95 | 0.647 | 0.404 | 46.3 | 2.53 | 0.55 | 21.6 |

RESULTS

Concentrations of coprostanol and polynuclear aromatic hydrocarbons were greatest just downstream from the Minneapolis-St. Paul metropolitan area and then decreased with increasing distance downstream. Concentrations of linear alkylbenzene sulfonates, however, did not have any distinct longitudinal distribution pattern.

Sterols

Coprostanol concentrations measured in the surficial bed sediments ranged from 0.23 mg/kg to 4.41 mg/kg (table 2.4). Sterol ratios ranged from 0.02 to 0.28. Analysis of duplicate samples collected from Pools 2, 8, and 19 indicated an average relative percent difference in coprostanol concentrations of 18.9 percent. Triplicate extractions on the Pool 3 sample indicated a relative standard deviation in coprostanol concentrations of 10.7 percent (see table 2.3). Triplicate extractions on preflood samples collected from Pools 1, 10, and 13 showed a relative standard deviation in coprostanol concentrations of 22.8 percent (Barber and others, 1997).

The longitudinal distribution pattern of sterols in the postflood sampling indicated an increased sterol concentration downstream from Minneapolis-St. Paul to Lake Pepin (Pool 4) (fig. 2.4). Sediment-bound contaminants are deposited in the large sediment trap formed by Lake Pepin, and sterol concentrations in pools downstream from pool 4 were less than those in pool 4.

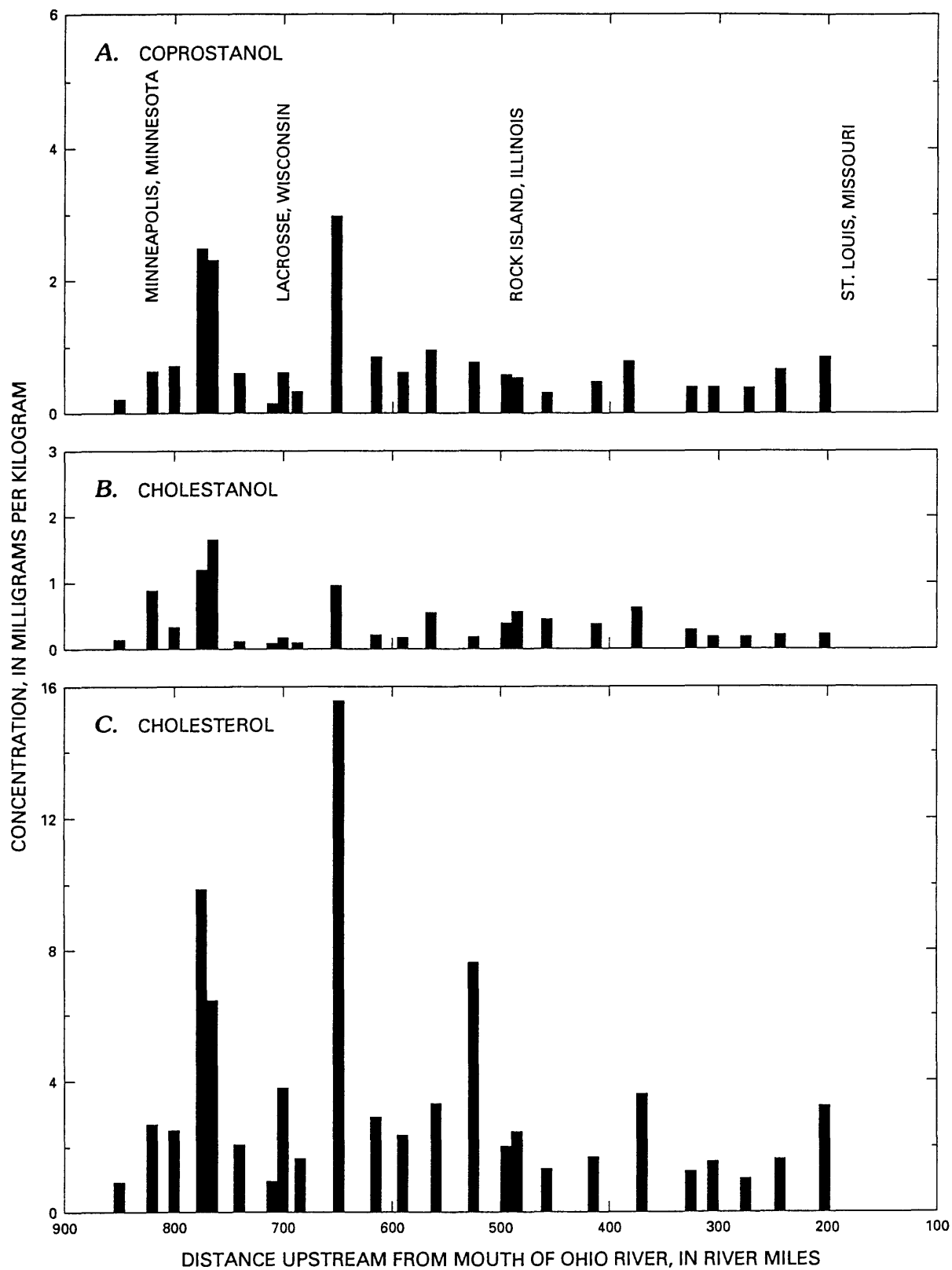


Figure 2.4--Sterol concentrations in surficial bed sediments from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

Table 2.4--Fecal sterol concentrations in surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July, 1994

[mg, milligram; kg, kilogram]

| Pool-duplicate | Date | Coprostanol (mg/kg) | Cholesterol (mg/kg) | Cholestanol (mg/kg) | Sterol ratio ¹ |
|-------------------|----------|---------------------|---------------------|---------------------|---------------------------|
| 1 | 06-11-94 | 0.27 | 0.88 | 0.18 | 0.15 |
| ² 2-1 | 06-12-94 | 0.89 | 2.70 | 0.78 | 0.22 |
| ² 2-2 | | 1.11 | 2.55 | 1.01 | 0.28 |
| St. Croix River | 06-13-94 | 2.26 | 5.38 | 0.75 | 0.10 |
| ³ 3 | 06-14-94 | 1.12 | 2.34 | 0.33 | 0.10 |
| | | 1.13 | 2.50 | 0.43 | 0.12 |
| | | 1.09 | 2.27 | 0.38 | 0.11 |
| ⁴ 4 | 06-15-94 | 3.76 | 9.83 | 1.22 | 0.09 |
| ⁵ 4 | | 3.54 | 7.43 | 1.64 | 0.15 |
| 5 | 06-16-94 | 0.89 | 1.97 | 0.11 | 0.04 |
| 6 | 06-17-94 | 0.23 | 0.94 | 0.07 | 0.06 |
| 7 | 06-18-94 | 0.92 | 3.76 | 0.18 | 0.04 |
| ² 8-1 | 06-19-94 | 0.46 | 1.63 | 0.18 | 0.09 |
| ² 8-2 | | 0.47 | 1.58 | 0.15 | 0.08 |
| 9 | 06-20-94 | 4.41 | 15.63 | 0.96 | 0.05 |
| 10 | 06-21-94 | 1.27 | 3.07 | 0.19 | 0.04 |
| 11 | 06-21-94 | 0.89 | 2.34 | 0.19 | 0.06 |
| 12 | 06-22-94 | 1.39 | 3.31 | 0.56 | 0.12 |
| 13 | 06-23-94 | 1.09 | 7.60 | 0.20 | 0.02 |
| 14 | 06-23-94 | 0.82 | 2.03 | 0.35 | 0.12 |
| 15 | 06-26-94 | 0.76 | 2.40 | 0.52 | 0.16 |
| 16 | 06-27-94 | 0.44 | 1.29 | 0.39 | 0.23 |
| 18 | 06-28-94 | 0.65 | 1.69 | 0.35 | 0.15 |
| ² 19-1 | 06-29-94 | 1.12 | 4.08 | 0.31 | 0.06 |
| ² 19-2 | | 1.16 | 3.24 | 0.27 | 0.06 |
| 20 | 06-30-94 | 0.21 | 0.44 | 0.04 | 0.06 |
| 21 | 07-01-94 | 0.51 | 1.22 | 0.24 | 0.14 |
| 22 | 07-02-94 | 0.52 | 1.48 | 0.13 | 0.07 |
| 24 | 07-03-94 | 0.53 | 1.09 | 0.12 | 0.07 |
| 25 | 07-04-94 | 0.88 | 1.78 | 0.17 | 0.07 |
| 26 | 07-05-94 | 1.20 | 3.28 | 0.29 | 0.06 |

¹Sterol ratio is equal to concentrations of coprostanol/(cholestanol + cholesterol).

²Duplicate sample collected in the field.

³Analysis performed in triplicate to assess analytical variability.

⁴Upper Lake Pepin.

⁵Lower Lake Pepin.

Polynuclear Aromatic Hydrocarbons

Preflood concentrations of polynuclear aromatic hydrocarbons were determined using an external standard, whereas postflood concentrations were based on comparison with surrogate standards added at the beginning of the analytical procedure. The preflood sample collected from upper Lake Pepin was reanalyzed with a surrogate standard added at the beginning of the analytical procedure to assess the variability between these two techniques; total PAH concentrations were 2.18 mg/kg for the preflood and 2.05 mg/kg for the postflood analyses. Total PAH concentrations of postflood samples ranged from 0.10 to 5.28 mg/kg (table 2.5). Analysis of duplicate samples collected from Pools 2, 8, and 19 indicated that the average relative percent difference was about 32 percent (table 2.3). Analytical variability as indicated by triplicate extractions of Pool 3 indicated a relative standard deviation of 21.6 percent (table 2.3). The greatest PAH concentrations were measured at Pool 1 and decreased downstream (fig. 2.5).

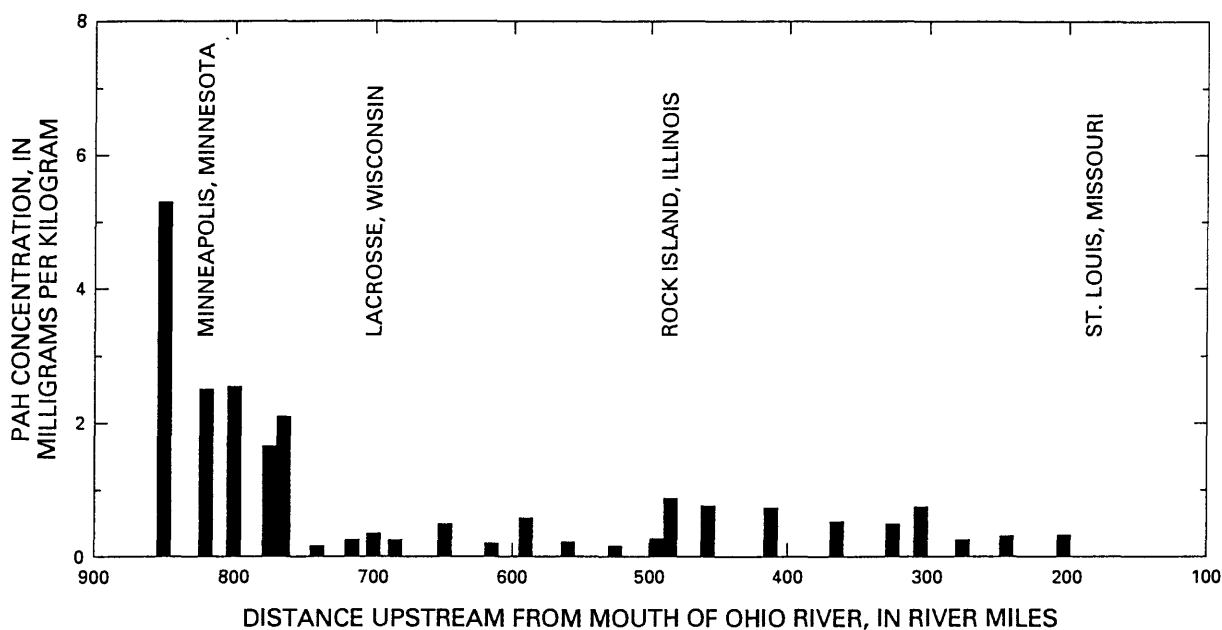


Figure 2.5--Total polynuclear aromatic hydrocarbon concentrations in surficial bed sediments from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

**Table 2.5--Polynuclear aromatic hydrocarbon concentrations in surficial bed sediments
of the Upper Mississippi**

[All units are milligrams per kilogram;

| Pool- duplicate | Date | Corrected naph- thalene ¹ | Ace- naphthalene | Ace- naphthene | Fluorene | Phen- anthrene | Anthracene | Fluor- anthene | Pyrene |
|--------------------|----------|--|---------------------|-------------------|----------|-------------------|------------|-------------------|--------|
| 1 | 06-11-94 | <1.08 | 0.23 | 0.04 | 0.20 | 0.30 | 0.04 | 0.60 | 0.58 |
| ² 2-1 | 06-12-94 | 0.03 | 0.02 | 0.02 | 0.02 | 0.25 | 0.03 | 0.54 | 0.61 |
| ² 2-2 | | 0.03 | 0.01 | 0.02 | 0.02 | 0.21 | 0.02 | 0.36 | 0.33 |
| St. Croix River | 06-13-94 | 0.00 | 0.61 | 0.07 | 0.00 | 0.05 | 0.01 | 0.23 | 0.21 |
| ³ 3 | 06-14-94 | 1.06 | 0.99 | 0.00 | 0.08 | 0.10 | 0.01 | 0.24 | 0.22 |
| | | 1.08 | 0.13 | 0.00 | 0.06 | 0.10 | 0.01 | 0.21 | 0.19 |
| | | 0.96 | 0.02 | 0.01 | 0.02 | 0.08 | 0.01 | 0.19 | 0.17 |
| ⁴ 4 | 06-15-94 | 0.00 | 0.02 | 0.01 | 0.02 | 0.10 | 0.01 | 0.30 | 0.31 |
| ⁵ 4 | | 0.00 | 0.59 | 0.00 | 0.00 | 0.05 | 0.01 | 0.35 | 0.42 |
| 5 | 06-16-94 | 0.00 | 0.05 | 0.00 | 0.00 | 0.01 | 0.00 | 0.03 | 0.03 |
| 6 | 06-17-94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.09 | 0.10 |
| 7 | 06-18-94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.11 | 0.13 |
| ² 8-1 | 06-19-94 | 0.00 | 0.08 | 0.00 | 0.00 | 0.01 | 0.00 | 0.03 | 0.03 |
| ² 8-2 | | 0.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.04 | 0.03 |
| 9 | 06-20-94 | 0.01 | 0.00 | 0.00 | 0.01 | 0.04 | 0.00 | 0.08 | 0.07 |
| 10 | 06-21-94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.02 | 0.02 |
| 11 | 06-21-94 | 0.00 | 0.23 | 0.00 | 0.00 | 0.02 | 0.00 | 0.09 | 0.08 |
| 12 | 06-22-94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.06 | 0.05 |
| 13 | 06-23-94 | 0.00 | 0.02 | 0.00 | 0.00 | 0.01 | 0.00 | 0.03 | 0.03 |
| 14 | 06-23-94 | 0.00 | 0.03 | 0.00 | 0.04 | 0.02 | 0.00 | 0.03 | 0.03 |
| 15 | 06-26-94 | 0.00 | 0.14 | 0.00 | 0.00 | 0.07 | 0.00 | 0.21 | 0.17 |
| 16 | 06-27-94 | 0.00 | 0.05 | 0.00 | 0.05 | 0.07 | 0.07 | 0.14 | 0.12 |
| 18 | 06-28-94 | 0.00 | 0.33 | 0.00 | 0.00 | 0.02 | 0.00 | 0.08 | 0.09 |
| ² 19-1 | 06-29-94 | 0.00 | 0.32 | 0.00 | 0.00 | 0.03 | 0.01 | 0.07 | 0.07 |
| ² 19-2 | | 0.00 | 0.04 | 0.01 | 0.02 | 0.03 | 0.01 | 0.05 | 0.06 |
| 20 | 06-30-94 | 0.00 | 0.03 | 0.00 | 0.00 | 0.01 | 0.00 | 0.03 | 0.03 |
| 21 | 07-01-94 | 0.00 | 0.03 | 0.00 | 0.00 | 0.07 | 0.01 | 0.22 | 0.19 |
| 22 | 07-02-94 | 0.00 | 0.26 | 0.00 | 0.00 | 0.02 | 0.00 | 0.07 | 0.08 |
| 24 | 07-03-94 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.06 | 0.07 |
| 25 | 07-04-94 | 0.00 | 0.01 | 0.00 | 0.00 | 0.02 | 0.00 | 0.05 | 0.05 |
| 26 | 07-05-94 | 0.00 | 0.01 | 0.00 | 0.00 | 0.02 | 0.00 | 0.05 | 0.05 |

¹Naphthalene concentration based on comparison with surrogate standard (dg-naphthalene) added at the beginning of analytical procedure. Concentration was assumed to be greater than surrogate standard if naphthalene, but not dg-naphthalene was recovered.

²Average of duplicate samples.

³Average of triplicate analysis.

⁴Upper Lake Pepin.

⁵Lower Lake Pepin.

collected from the downstream one-third of the 25 sampled navigation pools
River, June-July 1994

and PAH, polynuclear aromatic hydrocarbons]

| Pool- duplicate | Benzo[a] anthracene | Chrysene | Benzo[b] fluoranthene | Benzo[k] fluoranthene | Benzo[a] pyrene | Benzo- [ghi] perylene | Indeno [123-cd] pyrene | Dibenzo- [a,h] anthracene | Total PAH |
|--------------------|------------------------|----------|--------------------------|--------------------------|--------------------|-----------------------------|------------------------------|---------------------------------|--------------|
| 1 | 0.19 | 0.28 | 0.39 | 0.00 | 0.13 | 0.06 | 0.08 | 0.00 | 5.28 |
| ² 2-1 | 0.18 | 0.33 | 0.36 | 0.00 | 0.14 | 0.18 | 0.26 | 0.08 | 3.03 |
| ² 2-2 | 0.11 | 0.22 | 0.29 | 0.00 | 0.08 | 0.12 | 0.15 | 0.05 | 2.00 |
| St. Croix River | 0.04 | 0.13 | 0.14 | 0.00 | 0.02 | 0.05 | 0.08 | 0.02 | 1.66 |
| ³ 3 | 0.06 | 0.14 | 0.20 | 0.00 | 0.04 | 0.05 | 0.06 | 0.02 | 3.28 |
| | 0.06 | 0.14 | 0.21 | 0.00 | 0.04 | 0.04 | 0.05 | 0.00 | 2.31 |
| | 0.06 | 0.14 | 0.22 | 0.00 | 0.05 | 0.03 | 0.04 | 0.01 | 1.99 |
| ⁴ 4 | 0.07 | 0.19 | 0.29 | 0.00 | 0.06 | 0.09 | 0.13 | 0.03 | 1.63 |
| ⁵ 4 | 0.05 | 0.14 | 0.23 | 0.00 | 0.05 | 0.08 | 0.12 | 0.02 | 2.13 |
| 5 | 0.00 | 0.01 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.15 |
| 6 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.21 |
| 7 | 0.00 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.27 |
| ² 8-1 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.19 |
| ² 8-2 | 0.01 | 0.02 | 0.03 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.17 |
| 9 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.42 |
| 10 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.10 |
| 11 | 0.02 | 0.03 | 0.04 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.52 |
| 12 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.16 |
| 13 | 0.01 | 0.01 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.12 |
| 14 | 0.01 | 0.01 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.20 |
| 15 | 0.04 | 0.07 | 0.10 | 0.02 | 0.02 | 0.00 | 0.00 | 0.00 | 0.85 |
| 16 | 0.03 | 0.07 | 0.09 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.71 |
| 18 | 0.02 | 0.04 | 0.05 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.65 |
| ² 19-1 | 0.02 | 0.03 | 0.05 | 0.00 | 0.02 | 0.01 | 0.01 | 0.00 | 0.65 |
| ² 19-2 | 0.02 | 0.04 | 0.06 | 0.00 | 0.02 | 0.01 | 0.02 | 0.01 | 0.40 |
| 20 | 0.01 | 0.01 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.00 | 0.18 |
| 21 | 0.04 | 0.06 | 0.09 | 0.00 | 0.03 | 0.00 | 0.00 | 0.00 | 0.73 |
| 22 | 0.01 | 0.02 | 0.03 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.52 |
| 24 | 0.01 | 0.02 | 0.02 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.22 |
| 25 | 0.02 | 0.03 | 0.04 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.22 |
| 26 | 0.02 | 0.03 | 0.05 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.25 |

Linear Alkylbenzene Sulfonates

Linear alkylbenzene sulfonate concentrations in the postflood samples ranged from 0.03 to 1.07 mg/kg (table 2.6). Field-and-analytical variability for LAS was 47 percent based on multiple extractions of Pool 2 and Pool 8 samples (4 and 5 extractions, respectively). The longitudinal distribution pattern of LAS (fig. 2.6) in the Upper Mississippi River bed sediments is more variable than the patterns for sterols and PAH.

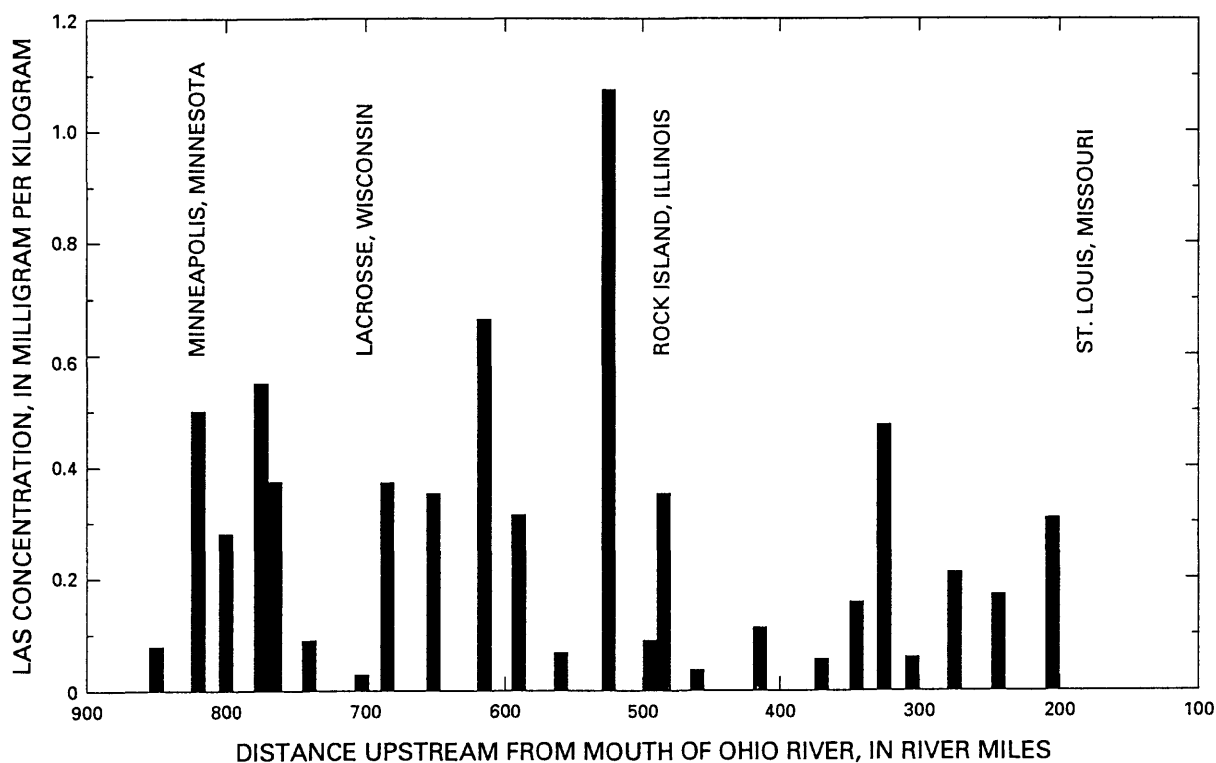


Figure 2.6--Total linear alkylbenzene sulfonate concentrations in surficial bed sediments from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

**Table 2.6--Linear alkylbenzene sulfonate concentrations in surficial bed sediments,
of the Upper Mississippi River, June-July 1994**

[Data are the average from duplicate analyses; g, gram; mg, milligram; kg, kilogram; LAS, linear alkylbenzene]

| Pool-duplicate | Date | Dry weight (g) | LAS concentration (mg/kg) | Average chain length | Homologues (percent of total LAS) | | | | Isomers (as percent of total LAS) | | | | |
|-------------------|----------|----------------|---------------------------|----------------------|--------------------------------------|-----------------|-----------------|-----------------|--------------------------------------|-------------------|-------------------|-------------------|-------------------------|
| | | | | | C ₁₀ | C ₁₁ | C ₁₂ | C ₁₃ | C ₁₀₋₅ | C ₁₀₋₄ | C ₁₀₋₃ | C ₁₀₋₂ | C _{11-5&6} |
| 1 | 06-11-94 | 20.25 | 0.08 | 10.7 | 50 | 28 | 22 | 0 | 24 | 0 | 26 | 0 | 0 |
| ¹ 2-1 | 06-12-94 | 17.54 | 0.52 | 10.9 | 26 | 58 | 15 | 0 | 8 | 6 | 9 | 3 | 20 |
| 2-1 | | 18.37 | 0.37 | 11.3 | 22 | 20 | 59 | 0 | 5 | 0 | 8 | 9 | 7 |
| 2-2 | | 15.00 | 0.26 | 10.6 | 44 | 46 | 9 | 0 | 15 | 0 | 22 | 7 | 10 |
| ² 2-2 | | 20.39 | 0.78 | 11.0 | 34 | 33 | 28 | 5 | 9 | 14 | 7 | 5 | 6 |
| ² 2-2 | | 20.61 | 0.38 | 10.6 | 67 | 14 | 9 | 10 | 17 | 33 | 17 | 0 | 0 |
| ² 2-2 | | 22.63 | 0.68 | 11.3 | 24 | 34 | 32 | 11 | 7 | 6 | 7 | 5 | 5 |
| St. Croix River | 06-13-94 | 5.61 | 0.14 | 10.2 | 77 | 23 | 0 | 0 | 45 | 0 | 32 | 0 | 0 |
| 3 | 06-14-94 | 15.62 | 0.28 | 10.1 | 90 | 10 | 0 | 0 | 30 | 22 | 38 | 0 | 0 |
| ³ 4 | 06-15-94 | 5.73 | 0.55 | 10.1 | 90 | 10 | 0 | 0 | 40 | 21 | 30 | 0 | 0 |
| ⁴ 4 | | 4.68 | 0.37 | 10.0 | 100 | 0 | 0 | 0 | 44 | 24 | 32 | 0 | 0 |
| 5 | 06-16-94 | 17.07 | 0.09 | 10.0 | 100 | 0 | 0 | 0 | 0 | 60 | 40 | 0 | 0 |
| 6 | 06-17-94 | 31.64 | 0.03 | 10.9 | 28 | 51 | 21 | 0 | 10 | 0 | 18 | 0 | 0 |
| 7 | 06-18-94 | 19.04 | 0.16 | 11.2 | 22 | 31 | 47 | 0 | 0 | 0 | 17 | 5 | 6 |
| ¹ 8-1 | 06-19-94 | 21.40 | 0.14 | 11.1 | 21 | 46 | 32 | 0 | 5 | 0 | 8 | 8 | 12 |
| ¹ 8-1 | | 21.98 | 0.19 | 10.9 | 29 | 50 | 20 | 0 | 10 | 0 | 10 | 10 | 10 |
| ¹ 8-1 | | 21.98 | 0.77 | 11.1 | 20 | 45 | 35 | 0 | 4 | 2 | 4 | 10 | 9 |
| ¹ 8-2 | | 21.64 | 0.38 | 11.2 | 10 | 58 | 32 | 0 | 0 | 0 | 10 | 0 | 12 |
| ¹ 8-2 | | 21.75 | 0.39 | 11.2 | 15 | 45 | 40 | 0 | 3 | 0 | 6 | 6 | 8 |
| 9 | 06-20-94 | 6.45 | 0.35 | 10.6 | 54 | 30 | 16 | 0 | 18 | 0 | 22 | 15 | 14 |
| 10 | 06-21-94 | 14.33 | 0.66 | 11.2 | 27 | 26 | 47 | 0 | 0 | 12 | 12 | 4 | 5 |
| 11 | 06-21-94 | 17.56 | 0.31 | 10.9 | 25 | 59 | 16 | 0 | 0 | 0 | 16 | 8 | 11 |
| 12 | 06-22-94 | 18.99 | 0.07 | 11.0 | 38 | 23 | 39 | 0 | 20 | 0 | 18 | 0 | 0 |
| 13 | 06-23-94 | 18.92 | 1.07 | 11.5 | 21 | 29 | 34 | 16 | 4.7 | 4 | 9 | 4 | 5 |
| 14 | 06-23-94 | 23.85 | 0.09 | 10.0 | 100 | 0 | 0 | 0 | 32 | 30 | 38 | 0 | 0 |
| 15 | 06-26-94 | 20.99 | 0.35 | 11.7 | 11 | 26 | 46 | 17 | 3 | 2 | 4 | 2 | 5 |
| 16 | 06-27-94 | 19.85 | 0.04 | 10.7 | 34 | 66 | 0 | 0 | 0 | 14 | 21 | 0 | 0 |
| 18 | 06-28-94 | 23.06 | 0.11 | 10.9 | 44 | 31 | 20 | 5 | 13 | 13 | 13 | 5 | 8 |
| ¹ 19-1 | 06-29-94 | 16.74 | 0.16 | 10.3 | 77 | 16 | 7 | 0 | 25 | 21 | 32 | 0 | 0 |
| ¹ 19-1 | | 16.41 | 0.00 | 0.0 | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| ¹ 19-2 | | 18.34 | 0.08 | 10.3 | 71 | 29 | 0 | 0 | 27 | 44 | 0 | 0 | 0 |
| ¹ 19-2 | | 17.26 | 0.00 | 0.0 | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| 20 | 06-30-94 | 31.25 | 0.16 | 11.0 | 32 | 34 | 34 | 0 | 6 | 12 | 8 | 6 | 8 |
| 21 | 07-01-94 | 22.45 | 0.47 | 11.6 | 18 | 28 | 32 | 21 | 4 | 4 | 5 | 6 | 9 |
| 22 | 07-02-94 | 19.87 | 0.06 | 10.2 | 83 | 17 | 0 | 0 | 30 | 33 | 19 | 0 | 0 |
| 24 | 07-03-94 | 26.80 | 0.21 | 10.9 | 43 | 43 | 0 | 14 | 15 | 13 | 15 | 0 | 43 |
| 25 | 07-04-94 | 21.30 | 0.17 | 10.5 | 68 | 16 | 11 | 5 | 24 | 23 | 19 | 2 | 3 |
| 26 | 07-05-94 | 17.57 | 0.31 | 10.9 | 40 | 33 | 22 | 5 | 15 | 12 | 14 | 0 | 9 |

¹Analysis performed in duplicate to assess analytical variability.

²Analysis performed in triplicate to assess analytical variability.

³Upper Lake Pepin.

⁴Lower Lake Pepin.

collected from the downstream one-third of the 25 sampled navigation pools

sulfonate; I/E, internal/external isomer ratio; c_{ii}-k, ii is the homologue and k is the phenyl position; nd, not detected]

| Pool-duplicate | Isomers (as percent of total LAS) | | | | | | | | | | | | |
|-------------------|--------------------------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|------------------------------------|--------------------|--------------------|--------------------|--------------------|
| | C ₁₁ -4 | C ₁₁ -3 | C ₁₁ -2 | C ₁₂ -6 | C ₁₂ -5 | C ₁₂ -4 | C ₁₂ -3 | C ₁₂ -2 | C ₁₃ ^{6&7} | C ₁₃ -5 | C ₁₃ -4 | C ₁₃ -3 | C ₁₃ -2 |
| 1 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 22 | 0 | 0 | 0 | 0 | 0 |
| ¹ 2-1 | 32 | 3 | 4 | 2 | 2 | 4 | 2 | 4 | 0 | 0 | 0 | 0 | 0 |
| ¹ 2-1 | 0 | 0 | 13 | 10 | 10 | 7 | 11 | 20 | 0 | 0 | 0 | 0 | 0 |
| 2-2 | 6 | 16 | 15 | 0 | 0 | 4 | 0 | 5 | 0 | 0 | 0 | 0 | 0 |
| ² 2-2 | 7 | 8 | 11 | 6 | 5 | 6 | 4 | 7 | 0 | 0 | 5 | 0 | 0 |
| ² 2-2 | 0 | 8 | 5 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 10 | 0 | 0 |
| ² 2-2 | 8 | 10 | 10 | 4 | 6 | 5 | 6 | 11 | 0 | 0 | 7 | 0 | 0 |
| St. Croix River | 0 | 16 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ³ 4 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ⁴ 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 | 16 | 12 | 23 | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 |
| 7 | 6 | 7 | 13 | 8 | 9 | 11 | 7 | 12 | 0 | 0 | 0 | 0 | 0 |
| ¹ 8-1 | 8 | 13 | 13 | 5 | 5 | 5 | 7 | 11 | 0 | 0 | 0 | 0 | 0 |
| ¹ 8-1 | 13 | 11 | 17 | 4 | 4 | 3 | 3 | 7 | 0 | 0 | 0 | 0 | 0 |
| ¹ 8-1 | 10 | 10 | 17 | 7 | 7 | 5 | 6 | 11 | 0 | 0 | 0 | 0 | 0 |
| ¹ 8-2 | 15 | 11 | 20 | 5 | 5 | 5 | 8 | 10 | 0 | 0 | 0 | 0 | 0 |
| ¹ 8-2 | 13 | 9 | 14 | 5 | 6 | 6 | 8 | 15 | 0 | 0 | 0 | 0 | 0 |
| 9 | 0 | 7 | 9 | 3 | 3 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 0 |
| 10 | 4 | 6 | 11 | 7 | 8 | 7 | 11 | 14 | 0 | 0 | 0 | 0 | 0 |
| 11 | 8 | 14 | 26 | 5 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 23 | 18 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 | 6 | 6 | 12 | 7 | 5 | 5 | 7 | 9 | 6 | 10 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15 | 4 | 5 | 12 | 5 | 5 | 7 | 9 | 20 | 4 | 3 | 3 | 2 | 4 |
| 16 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18 | 4 | 12 | 7 | 2 | 4 | 8 | 2 | 5 | 0 | 0 | 5 | 0 | 0 |
| ¹ 19-1 | 0 | 16 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ¹ 19-1 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| ¹ 19-2 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ¹ 19-2 | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd | nd |
| 20 | 6 | 8 | 13 | 6 | 5 | 6 | 8 | 8 | 0 | 0 | 0 | 0 | 0 |
| 21 | 4 | 6 | 8 | 4 | 6 | 7 | 6 | 9 | 5 | 4 | 4 | 3 | 4 |
| 22 | 0 | 7 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 |
| 25 | 0 | 8 | 4 | 1 | 2 | 1 | 3 | 4 | 1 | 1 | 2 | 1 | 0 |
| 26 | 7 | 9 | 9 | 0 | 8 | 7 | 0 | 7 | 0 | 0 | 5 | 0 | 0 |

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Chapter 3 - Polychlorinated Biphenyl Congeners

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ABSTRACT

Representative subsamples of surficial bed sediments were collected from the Mississippi River and analyzed for polychlorinated biphenyl congeners by two different laboratories. Samples from the upstream navigation pools (mainly above Lock and Dam 11) were analyzed by the Wisconsin State Laboratory of Hygiene in Madison, Wisconsin. Samples from the downstream navigation pools were analyzed by the University of Minnesota Trace Organic Laboratory in Duluth, Minnesota. The maximum total polychlorinated biphenyl concentration (92.8 nanograms per gram) was from Pool 4 (Lake Pepin), but the highest total polychlorinated biphenyls normalized by the amount of organic carbon was calculated for Pool 20 (6,500 nanograms per gram organic carbon). Spatial evaluation of these data are complicated by method differences and low total organic-carbon content in some samples from the downstream navigation pools.

INTRODUCTION

Polychlorinated biphenyls (PCB) are a group of organic compounds that were produced commercially by the chlorination of biphenyl with anhydrous chlorine (Eisler, 1986; Alford-Stevens, 1986). This process yielded a complex array of individual PCB molecules (congeners) with various chlorine contents. In the United States, PCB mixtures were commonly sold under the trade name of Aroclor. There are 209 potential PCB congeners (Mullin and Pochini, 1984), but not all congeners are found in the original formulations (Alford-Stevens, 1986). The actual number of congeners present in environmental samples is substantially less (McFarland and Clarke, 1989) as a result of differential partitioning and degradation.

PCB have been widely used since the 1930's, especially in electrical equipment, lubricants, and fire retardants (Eisler, 1986; Alford-Stevens, 1986). State and Federal regulations were enacted in the mid-1970's to restrict the production, use, and disposal of these compounds. The input of PCB to the Upper Mississippi River has been a water-quality problem for more than 20 years and has been especially apparent in the river reach extending from the Twin Cities metropolitan area to Lake Pepin (Sullivan, 1988; Steingraeber and others, 1994).

Like other organochlorine compounds, PCB generally have low solubility in water and have a strong affinity to adsorb to soil and sediment particles, especially those high in organic content (Karickhoff and others, 1979). As a result, contaminated sediment presents a major source of exposure of aquatic organisms to PCB (Lyman and others, 1987; Baudo and others, 1990). Volatilization of PCB from contaminated aquatic and terrestrial systems contributes to the transport of these compounds to the atmosphere (Hornbuckle and others, 1993).

PURPOSE AND SCOPE

One purpose of the bed-sediment sampling was to provide the concentrations of PCB congeners in surficial bed sediments collected in the downstream one-third of each navigation pool of the Upper Mississippi River after the flood of 1993. Congener PCB analysis provides a lower level of detection and is generally less subjective than older Aroclor-based methods. Congener data provide more specific information on the longitudinal distribution of PCB in Upper Mississippi River surficial bed sediments and allows for a more accurate assessment of their fate and partitioning to other environmental matrices. Two analytical laboratories were utilized as a result of laboratory work loads and a need to ensure consistency with previous congener PCB analysis of suspended sediment samples from the Mississippi River. The results from the two different methods are listed in two tables and the spatial distribution of total PCB (congener sums) and selected congeners are shown graphically.

ANALYTICAL METHODS

The subsamples collected for PCB congener analysis were kept refrigerated at about 4°C in glass jars with Teflon-lined lids until they were analyzed by either the Wisconsin State Laboratory of Hygiene in Madison, Wis. (hereinafter referred to as the WSLOH), or the University of Minnesota Trace Organic Analytical Laboratory in Duluth, Minn. (hereinafter referred to as the TOAL). The WSLOH analyzed bed-sediment samples from Pools 1-11, except 5A and 10, and the TOAL analyzed Pools 10 and 12-26, except 17. A reference sediment, collected from lower Lake Pepin in May 1991 by State and Federal agencies, was analyzed by both laboratories for comparison purposes.

Wisconsin State Laboratory of Hygiene Method

The WSLOH method identified 85 PCB congeners (some co-eluting) in surficial bed sediments using capillary column gas chromatography and electron-capture detection (Wisconsin State Laboratory of Hygiene, 1993). The sum of the individual congener concentrations provided an estimate of total PCB.

Sample Preparation

The sediment sample was air-dried at room temperature to about 10-30 percent moisture for about 2 to 5 days and then passed through a #10 sieve. Remaining material that did not pass through the sieve was discarded. A 10- to 25-g subsample of the homogenized sample was dried at 103°C for at least 10 hours in order to determine the percent moisture. If the moisture content exceeded 30 percent, the sample was redried. A 40- to 50-g subsample of air-dried sediment was then weighed into an acetone-washed paper extraction thimble and placed in an acetone-washed Soxhlet extraction apparatus. Each dry sample was spiked with a surrogate mixture (consisting of PCB congeners #14, #65, and #166 at concentrations of 100, 75, and 25 ng/mL, respectively) at two to five times the detection level to measure analytical recoveries for establishing upper and lower warning limits (equal to two standard deviations either side of the average analytical recovery). The average analytical recoveries (\pm the standard deviation) for 321 sediment samples for PCB congeners #14, #65, and #166 were 87 ± 13 , 91 ± 12 , and 102 ± 11 percent, respectively. This information is from laboratory quality-assurance information reported by the WSLOH on August 18, 1993, and includes several years of data.

A few glass beads or boiling chips were placed in the Soxhlet flask with 300 mL of 50:50 (v : v) acetone : hexane mixture. Granular activated copper was added to the flask to minimize sulfur interferences. The Soxhlet extraction apparatus was placed on a hot plate and the sample was extracted for approximately 8 hours. The temperature was adjusted so that the Soxhlet cycled 5-8 times per hour. The acetone-hexane mixture was then concentrated under a gentle stream of filtered air or in a rotary evaporation apparatus to about 10 mL. Anhydrous sodium sulfate was added to aid in the removal of water.

Extract cleanup was performed using florisil and silica-gel fractionation. The PCB were eluted from the florisil column with 200 mL of a 94:6 (v : v) hexane-ethyl ether mixture. The extract was concentrated to approximately 5 mL and added to a silica-gel column. The silica-gel column was eluted with 50 mL of hexane at a rate of 1-2 mL/min. The final extract volume was reduced under a gentle stream of filtered air to 10 mL.

Sample Analysis

Sample analysis was performed with a gas chromatograph (HP 5880 Gas Chromatograph) using a capillary column (60-meter DB-5 column, 0.2-mm inside diameter, and 0.1- μ m film; and an electron-capture detector. The calibration standard included a mixture of Aroclors 1232, 1248, and 1262 at concentrations of 0.250, 0.180, and 0.180 mg/L, respectively. The concentration of each congener in this mixture was provided by Mullin (1985). This standard also contained PCB congeners #30 (12 ng/mL) and #204 (13.8 ng/mL), which were used as retention-time reference peaks and as internal standards for quantitation. Internal standards were added to sample extracts just prior to gas chromatographic analysis.

Precision estimates (average absolute difference of duplicate sediment samples) and accuracy measurements (based on percent recoveries of spiked sediment samples) were conducted over a period of several years. One matrix spike sediment sample was analyzed for every 10 unknown sediment samples. Matrix spike solutions consisted of the same PCB Aroclor mixture used as the calibration standard above. Average and standard deviation values for precision and accuracy measurements are utilized to establish warning limits (average ± 2 SD) and control limits (average ± 3 SD) for PCB congener determinations. Sample results falling outside the control limits were reanalyzed or flagged for further evaluation. The method detection limit, limit of quantification, average precision, and average percent recovery for PCB congeners are listed in table 3.1. This table represents typical laboratory performance for several years ending in August 1993. The method detection limit is defined as the minimum concentration of a substance which can be measured and reported with 99-percent confidence that the analyte concentration is greater than zero and is determined from an analysis of a sample in a given matrix containing the analyte (U.S. Environmental Protection Agency, 1991). The limit of quantification is approximately 3.3 times the method detection limit (American Chemical Society, 1983).

Table 3.1--Method detection limit, limit of quantification, precision, and accuracy information for polychlorinated biphenyl congener analysis at the Wisconsin State Laboratory of Hygiene, Madison, Wisconsin

[Congeners are listed in order as reported by the laboratory; IUPAC, International Union of Pure and Applied Chemistry; ng/g, nanogram per gram of dry weight; N, number of replicate analyses; and %, percent]

| IUPAC number | Structure | Method detection limit (ng/g) | Limit of quantification (ng/g) | Precision ¹ | | Accuracy ² | |
|--------------|-----------------------------|-------------------------------|--------------------------------|------------------------|------|-----------------------|------|
| | | | | N | % | N | % |
| 7 | 2,4 | 0.20 | 0.70 | 30 | 6.7 | 45 | 85.9 |
| 6 | 2,3' | 0.45 | 1.5 | 36 | 8.5 | 44 | 89.7 |
| 5/8 | 2,3/2,4' | 1.3 | 4.3 | 42 | 8.3 | 45 | 87.3 |
| 19 | 2,2',6 | 0.30 | 1.0 | 30 | 10.0 | 42 | 69.0 |
| 18 | 2,2'5 | 0.35 | 1.2 | 41 | 5.8 | 45 | 87.3 |
| 17 | 2,2',4 | 0.30 | 1.0 | 41 | 5.1 | 45 | 87.4 |
| 24/27 | 2,3,6/2,3',6 | 0.30 | 1.0 | 36 | 5.9 | 44 | 85.5 |
| 16/32 | 2,2',3/2,4',6 | 0.40 | 1.5 | 42 | 7.4 | 44 | 85.9 |
| 26 | 2,3',5 | 0.35 | 1.2 | 40 | 9.6 | 44 | 90.0 |
| 28/31 | 2,4,4'/2,4',5 | 1.4 | 4.6 | 43 | 7.0 | 44 | 90.7 |
| 33 | 2',3,4 | 0.45 | 1.5 | 36 | 8.8 | 45 | 89.8 |
| 22 | 2,3,4' | 0.60 | 2.0 | 39 | 8.4 | 45 | 91.7 |
| 45 | 2,2',3,6 | 0.30 | 1.0 | 38 | 7.0 | 45 | 83.0 |
| 46 | 2,2',3,6' | 0.35 | 1.2 | 35 | 6.3 | 45 | 82.7 |
| 52 | 2,2',5,5' | 0.30 | 1.0 | 44 | 4.8 | 45 | 92.3 |
| 49 | 2,2',4,5' | 0.30 | 1.0 | 42 | 5.0 | 45 | 91.1 |
| 47/48 | 2,2',4,4'/2,2',4,5 | 0.50 | 1.6 | 38 | 5.1 | 45 | 89.0 |
| 44 | 2,2',3,5' | 0.30 | 1.0 | 42 | 5.3 | 45 | 91.2 |
| 37/42 | 3,4,4'/2,2',3,4' | 0.40 | 1.3 | 40 | 7.4 | 45 | 91.1 |
| 41/64/71 | 2,2',3,4/2,3,4',6/2,3',4',6 | 0.50 | 1.6 | 39 | 7.4 | 45 | 88.1 |
| 40 | 2,2',3,3' | 0.30 | 1.0 | 37 | 6.1 | 45 | 87.7 |
| 74 | 2,4,4',5 | 0.30 | 1.0 | 43 | 8.0 | 45 | 94.8 |
| 70/76 | 2,3',4',5/2',3,4,5 | 0.45 | 1.5 | 45 | 7.6 | 45 | 96.4 |
| 66/95 | 2,3',4,4'/2,2',3,5',6 | 0.60 | 2.0 | 43 | 6.1 | 45 | 93.2 |
| 91 | 2,2',3,4',6 | 0.40 | 1.3 | 39 | 5.5 | 45 | 96.1 |
| 56/60 | 2,3,3',4'/2,3,4,4' | 0.80 | 2.6 | 43 | 7.8 | 45 | 94.3 |
| 84/92 | 2,2',3,3',6/2,2',3,5,5' | 0.70 | 2.3 | 39 | 6.2 | 44 | 93.8 |
| 101 | 2,2',4,5,5' | 0.30 | 1.0 | 45 | 7.0 | 44 | 97.1 |
| 99 | 2,2',4,4',5 | 0.30 | 1.0 | 42 | 6.5 | 44 | 94.8 |
| 97 | 2,2',3',4,5 | 0.30 | 1.0 | 40 | 4.9 | 44 | 96.1 |
| 87 | 2,2',3,4,5' | 0.35 | 1.2 | 42 | 8.7 | 44 | 98.0 |
| 85 | 2,2',3,4,4' | 0.35 | 1.0 | 32 | 5.4 | 45 | 98.4 |
| 136 | 2,2',3,3',6,6' | 0.20 | 0.70 | 21 | 6.1 | 45 | 94.6 |
| 77/110 | 3,3',4,4'/2,3,3',4',6 | 0.40 | 1.3 | 45 | 7.4 | 44 | 96.1 |

Table 3.1--Method detection limit, limit of quantification, precision, and accuracy information for polychlorinated biphenyl congener analysis at the Wisconsin State Laboratory of Hygiene, Madison, Wisconsin--Continued

| IUPAC number | Structure | Method detection limit (ng/g) | Limit of quantification (ng/g) | Precision ¹ | | Accuracy ² | |
|--------------|--|-------------------------------|--------------------------------|------------------------|------|-----------------------|-------|
| | | | | N | % | N | % |
| 82 | 2,2',3,3',4 | 0.30 | 1.0 | 36 | 7.8 | 44 | 93.8 |
| 151 | 2,2',3,5,5',6 | 0.30 | 1.0 | 40 | 9.8 | 45 | 93.4 |
| 135/144 | 2,2',3,3',5,6'/2,2',3,4,5',6 | 0.30 | 1.0 | 36 | 9.1 | 45 | 92.5 |
| 149 | 2,2',3,4',5',6 | 0.30 | 1.0 | 41 | 7.0 | 45 | 93.6 |
| 118 | 2,3',4,4',5 | 0.45 | 1.5 | 44 | 8.5 | 44 | 95.6 |
| 146 | 2,2',3,4',5,5' | 0.35 | 1.2 | 33 | 6.2 | 44 | 102.0 |
| 132/153 | 2,2',3,3',4,6'/2,2',4,4',5,5' | 0.45 | 1.5 | 44 | 8.8 | 45 | 95.4 |
| 141 | 2,2',3,4,5,5' | 0.30 | 1.0 | 31 | 7.1 | 45 | 93.0 |
| 137/176 | 2,2',3,4,4',5/2,2',3,3',4,6,6' | 0.30 | 1.0 | 45 | 10.0 | 45 | 95.5 |
| 138/163 | 2,2',3,4,4',5'/2,3,3',4',5,6 | 0.40 | 1.3 | 45 | 10.0 | 45 | 96.8 |
| 178 | 2,2',3,3',5,5',6 | 0.40 | 1.3 | 22 | 13.0 | 45 | 94.6 |
| 182/187 | 2,2',3,4,4',5,6'/2,2',3,4',5,5',6 | 0.40 | 1.3 | 40 | 9.8 | 45 | 94.3 |
| 183 | 2,2',3,4,4',5',6 | 0.40 | 1.3 | 32 | 12.0 | 45 | 95.4 |
| 185 | 2,2',3,4,5,5',6 | 0.30 | 1.0 | 13 | 7.6 | 45 | 94.9 |
| 174 | 2,2',3,3',4,5,6' | 0.30 | 1.0 | 39 | 8.3 | 45 | 93.7 |
| 177 | 2,2',3,3',4',5,6 | 0.35 | 1.2 | 34 | 8.2 | 45 | 95.5 |
| 171/202 | 2,2',3,3',4,4',6/2,2',3,3',5,5',6,6' | 0.30 | 1.0 | 27 | 11.0 | 45 | 96.2 |
| 172/197 | 2,2',3,3',4,5,5'/2,2',3,3',4,4',6,6' | 0.50 | 1.6 | 14 | 14.0 | 45 | 93.9 |
| 180 | 2,2',3,4,4',5,5' | 0.35 | 1.2 | 41 | 8.4 | 45 | 96.0 |
| 199 | 2,2',3,3',4,5,6,6' | 0.30 | 1.0 | 5 | 7.6 | 45 | 92.6 |
| 170/190 | 2,2',3,3',4,4',5/2,3,3',4,4',5,6 | 0.70 | 2.3 | 32 | 9.0 | 45 | 95.4 |
| 201 | 2,2',3,3',4,5,5',6 | 0.50 | 1.6 | 39 | 11.0 | 45 | 95.3 |
| 196/203 | 2,2',3,3',4,4',5,6'/2,2',3,4,4',5,5',6 | 0.70 | 2.3 | 38 | 10.0 | 45 | 94.8 |
| 195/208 | 2,2',3,3',4,4',5,6/2,2',3,3',4,5,5',6,6' | 0.70 | 2.3 | 30 | 13.0 | 45 | 93.8 |
| 194 | 2,2',3,3',4,4',5,5' | 0.50 | 1.6 | 36 | 12.0 | 45 | 96.5 |
| 206 | 2,2',3,3',4,4',5,5',6 | 0.40 | 1.3 | 39 | 17.0 | 45 | 93.8 |
| 128 | 2,2',3,3',4,4' | 0.50 | 1.6 | -----no data----- | | | |
| 167 | 2,3',4,4',5,5' | 0.50 | 1.6 | -----no data----- | | | |

¹Precision-average absolute difference between duplicate analyses over several years ending August 18, 1993.

²Accuracy-average percent recoveries of sediment samples spiked with standard solutions analyzed under similar test conditions over several years ending August 18, 1993.

Trace Organic Analytical Laboratory Method

The TOAL determined 117 PCB congeners (some co-eluting) by appropriate sample preparation, extraction, and cleanup, followed by analysis using capillary-column gas chromatography with electron-capture detection. Total PCB represented a sum of detected congeners.

Sample Preparation

The wet sediment was air-dried for several days under ambient laboratory conditions, then ground to a fine powder and stored in a freezer until the extraction step. Representative laboratory subsamples were collected from two samples, and simple grab samples were collected from the remaining samples.

Five representative subsamples each for Pool 19-1 and Lake Pepin reference sediment were utilized for laboratory replicates. Representative subsamples were prepared using a Sieving Riffler (Quantachrome, Model SRR-2). This consisted of eight stainless-steel collector bins placed upon a rotating platform. The dried and ground sediment sample was placed in a bowl attached to a vibrator. A chute with a gate delivered the dried sediment from the bowl to the collector bins. The amplitude of the vibrator, the speed of rotation of the platform, and the gate opening were adjusted to obtain a rotation speed that was faster than the delivery rate. A number of passes were required using combinations of representative subsamples in order to prepare final representative subsamples of about 10 g for analysis.

The subsamples obtained from the other sediments were grab samples. The samples were run in three sets with the extractions starting on October 12, 17, and 19, 1994. Approximately 10 g of the dried and ground sediment was mixed with sodium sulfate; the mixture was transferred to a Soxhlet thimble and spiked with 1,000 ng each of surrogate congeners #14 and #166 (recovery standards). The thimble was placed in a Soxhlet apparatus and extracted overnight with 250 mL 1:1 (v : v) acetone : hexane solution. Copper beads were added to the extraction flask to remove sulfur. The extract was reduced to 1 mL, using a Kuderna-Danish evaporative concentrator, and transferred to a florisil column for adsorption cleanup. PCB were eluted from the column using 75 mL of 20 percent (v:v) dichloromethane: hexane. This extract was again reduced to 1 mL, transferred to a 4-mL vial with three rinses of iso-octane, and spiked with 500 ng each of instrument internal standard consisting of congeners #30 and #204.

Sample Analysis

Sample analysis was performed using a Hewlett-Packard gas chromatograph (HP5890II) equipped with an autosampler (HP7672A) and an electron-capture detector. The column was a DB-5 (30 m by 0.25-mm inside diameter) with 0.25- μ m film. Quantitation of individual congeners was accomplished by the determination of average response factors, relative to congeners #30 and #204 (15 ng/mL in the standards), from running a series of three calibration standards. The concentrations of total PCB Aroclors in these standards were 100, 200 and 400 ng/mL. The proportion of Aroclors was 1:1:1:1 (v:v) of 1242, 1248, 1254, and 1260 (Schwartz and others, 1990). The mixed Aroclor calibration standards were run with each sample set, which contains three quality-assurance samples (see below) and nine sediment extracts for analysis. A summary of PCB congener precision and accuracy data for a fortified sediment sample (West Bearskin Lake) is provided in table 3.2.

Five replicates of the Lake Pepin reference sediment and Pool 19-1 sample were analyzed by the TOAL. Generally, the standard deviation decreases with the mean concentration; this is observed by plotting the standard deviation against mean concentrations for congeners within each homologue group (plots not shown). Extrapolation of the mean concentration to zero provides an estimate of the limit of detection, as the t-estimator at the 99-percent confidence interval multiplied by the standard deviation. The estimates are 0.2 ng/g for tri- and tetra-chlorinated biphenyls, 0.02 ng/g for penta-chlorinated biphenyls, 0.01 ng/g for hexa-chlorinated biphenyls, and 0.008 ng/g for hepta- and octa-chlorinated biphenyls. Values below 0.01 ng/g are not reported here, although a satisfactory peak may be present.

Quality-assurance samples consisted of a method blank, containing only reagents to test for laboratory-derived contamination; a sediment spiked with PCB (West Bearskin Lake sediment fortified with 200 ng each of Aroclors 1242, 1248, 1254, and 1260) or a standard reference sediment (HS-1, National Research Council of Canada); and a duplicate sediment sample to test for precision (two replicates in table 3.4). The five replicate samples, each for Pool 19-1 and Lake Pepin, were not considered as quality-assurance samples in the composition of the sample sets. Samples not meeting the accepted requirements for recovery (40-120 percent of the surrogates), precision (relative difference \leq 50 percent), and accuracy (relative difference \leq 50 percent) were reanalyzed or flagged.

Table 3.2--Precision and accuracy data for polychlorinated biphenyl congeners analyzed by University of Minnesota Total Organic Analytical Laboratory, June-July 1994

[Five replicates were analyzed from a sample with a high concentration (Reference, 290 ng/g) and from a sample with a low concentration (Pool 19, 15.3 ng/g) to determine Precision, which is measured as the percent relative standard deviation; Accuracy is the percent spike recovery of a fortified sediment sample (West Bearskin Lake measured twice); IUPAC, International Union of Pure and Applied Chemistry; i, interference in the peak; d, detected congener but expected concentration was zero; and --, not detected; <, less than]

| Con- gener IUPAC number | Precision | | Accuracy | Con- gener IUPAC | Precision | | Accuracy | Con- gener IUPAC | Precision | | Accuracy |
|----------------------------------|---------------------|---------|--------------------------|------------------------|---------------------|---------|--------------------------|------------------------|---------------------|---------|--------------------------|
| | Reference sample | Pool 19 | West Bearskin Lake | | Reference sample | Pool 19 | West Bearskin Lake | | Reference sample | Pool 19 | West Bearskin Lake |
| 4/10 | -- | 38 | 80 | 89 | 14 | -- | ¹ 79 | 174 | 12 | 14 | 58 |
| 7 | 12 | 8 | 64 | 101 | 4 | 20 | 110 | 177 | 6 | 14 | 86 |
| 6 | 17 | 9 | 62 | 99 | 4 | -- | 70 | 202/171 | 10 | 33 | 85 |
| 5/8 | 31 | 7 | 80 | 119 | 8 | 40 | ¹ 190 | 156 | 6 | 29 | 77 |
| 19 | -- | -- | 63 | 83 | 5 | 33 | ¹ 93 | 173 | 15 | 33 | -- |
| 18 | 33 | 34 | 127 | 97 | 4 | 15 | 103 | 172/197 | 6 | 50 | ¹ 86 |
| 17 | 5 | 16 | 108 | 87 | 3 | 10 | 84 | 180 | 5 | 36 | 75 |
| 24/27 | 42 | 33 | ¹ 90 | 85 | 4 | 11 | 96 | 193 | 25 | 0 | 84 |
| 16/32 | 16 | 24 | 51 | 136 | -- | -- | -- | 191 | 14 | 50 | ¹ 220 |
| 29 | -- | 50 | ¹ 280 | 77/110 | 4 | 30 | 94 | 199 | 7 | 50 | ¹ 100 |
| 26 | 42 | -- | 130 | 82 | 5 | 25 | 63 | 170/190 | 5 | 17 | ¹ 66 |
| 25 | 29 | 25 | 68 | 151 | 5 | 8 | 185 | 198 | 45 | -- | d |
| 28/31 | 10 | 25 | 101 | 135/144 | 4 | 0 | 58 | 201 | 6 | 57 | 88 |
| 21/33/53 | 11 | 27 | 91 | 124 | 5 | 33 | ¹ 51 | 203/196 | 3 | 75 | 84 |
| 51 | 43 | 50 | ¹ 150 | 147 | 3 | 33 | ¹ 99 | 189 | 35 | -- | d |
| 22 | -- | -- | 80 | 107 | 2 | 25 | ¹ 87 | 208/195 | 3 | 25 | ¹ 79 |
| 45 | 21 | 47 | 130 | 123/149 | 4 | 5 | 66 | 207 | 5 | 100 | d |
| 46 | 23 | 25 | 51 | 118 | 3 | 10 | 110 | 194 | 15 | 50 | 84 |
| 52 | 3 | 8 | 68 | 134 | 3 | 33 | 87 | 205 | 27 | -- | d |
| 43 | -- | 20 | ¹ 220 | 114 | 3 | 10 | ¹ 420 | | | | |
| 49 | 4 | 11 | 72 | 131/122 | 6 | 25 | ¹ 55 | | | | |
| 47/48 | 3 | 14 | 90 | 146 | 4 | 20 | 67 | | | | |
| 44 | 4 | 12 | 68 | 132/153/105 | 5 | 9 | 69 | | | | |
| 42 | i | -- | i | 141 | 4 | 6 | 86 | | | | |
| 41/71 | 4 | 11 | 72 | 137/176 | 4 | 17 | 150 | | | | |
| 64 | 9 | 7 | 73 | 130 | 5 | 25 | ¹ 580 | | | | |
| 40 | 14 | -- | -- | 163/138 | 4 | 6 | 67 | | | | |
| 100 | 18 | 28 | ¹ 420 | 158 | 5 | 0 | 68 | | | | |
| 63 | 56 | -- | ¹ 310 | 126/129 | -- | 12 | ¹ 49 | | | | |
| 74 | 7 | 15 | 79 | 178 | 14 | 50 | ¹ 56 | | | | |
| 70/76 | 3 | 24 | 85 | 187/182 | 7 | 12 | 29 | | | | |
| 95/66 | 3 | 29 | 86 | 183 | 4 | 20 | 76 | | | | |
| 91 | 3 | 27 | 130 | 128 | 5 | 10 | 54 | | | | |
| 56/60 | 6 | 0 | 65 | 167 | 13 | -- | ¹ 330 | | | | |
| 84/92 | 4 | 9 | 117 | 185 | 18 | 50 | ¹ 170 | | | | |

¹Poor accuracy may be associated with low expected concentrations (less than 0.2 ng/g) of these congeners.

RESULTS

The concentrations of PCB congeners reported in bed sediments by the WSLOH and TOAL are provided in tables 3.3 and 3.4, respectively. The Lake Pepin reference sediment was analyzed by both laboratories. The WSLOH method identified 67 of 89 assayed congeners in this sample. The TOAL method detected 110 of 117 measured congeners. The total PCB (congener sum) concentration reported by the WSLOH and TOAL in this reference sample was very similar and averaged 280 and 290 ng/g, respectively. There were no reference sediment comparisons between the two laboratories at lower PCB concentrations.

The concentration of total PCB and selected congeners (IUPAC #28/31, #118, and #180) are shown in figs. 3.1 and 3.2. Greatest PCB concentrations (about 30-90 ng/g) were in samples collected from Pools 2 through 4. Individual congener concentrations (#118 and #180) were distinctly greater in Pools 2 through 4. In general sample results for Pools 9 through 12 revealed a greater number of detected congeners (about 100 more) and greater PCB concentrations (about 17 ng/g) with the TOAL method (tables 3.3 and 3.4). Organic carbon-normalized total PCB concentrations (fig. 3.1) exhibited the largest values (3,900-6,500 ng/g of carbon) in Pools 10, 15, and 20. Differences in PCB congener methods and low total organic-carbon concentrations (Chapter 1) makes the interpretation of the spatial trends difficult.

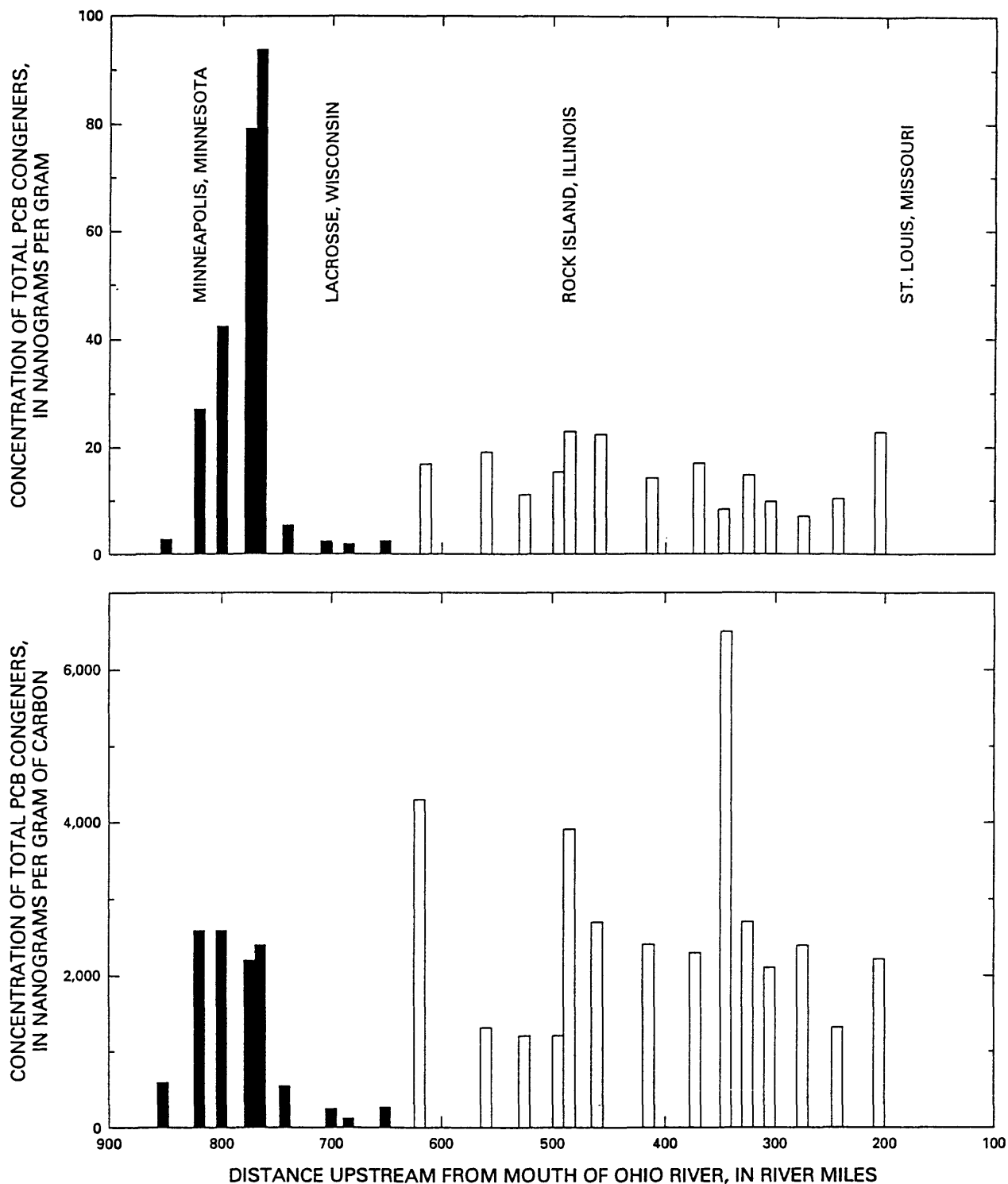


Figure 3.1--Concentration of total polychlorinated biphenyl congeners (upper panel) and concentration of total polychlorinated biphenyl congeners per gram of organic carbon (lower panel) in surficial sediment from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. Solid black bars are data from Wisconsin State Laboratory of Hygiene, Madison, Wisconsin, and the white bars are data from the University of Minnesota Total Organics Analytical Laboratory. See table 1.2 for location of pools.

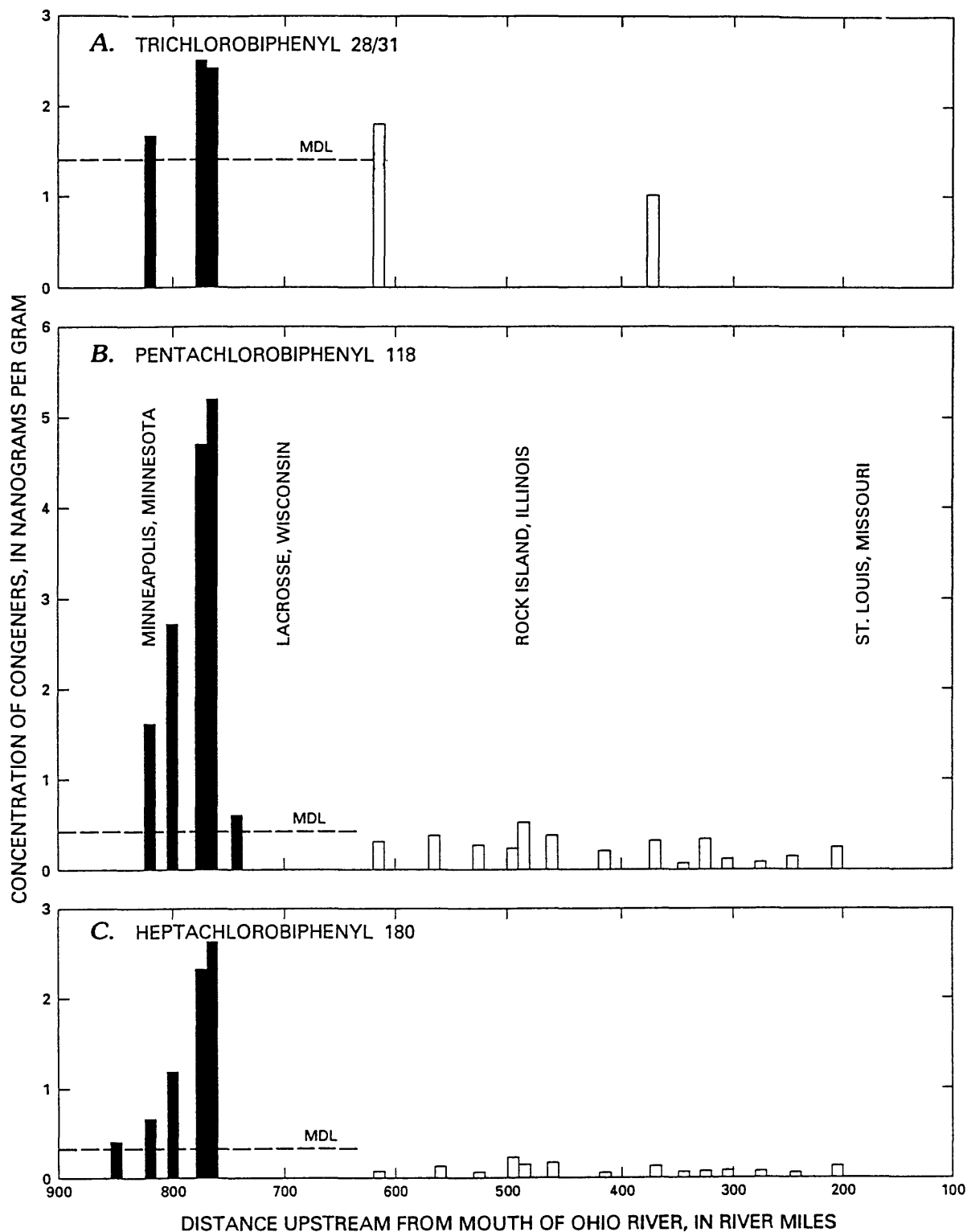


Figure 3.2--Concentration of three selected congeners in surficial sediment from downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994.

A. Trichlorobiphenyl pair numbers 28 and 31.

B. Pentachlorobiphenyl number 118.

C. Heptachlorobiphenyl number 180.

Solid black bars are data from Wisconsin State Laboratory of Hygiene, Madison, Wisconsin. The white bars are data from the University of Minnesota Total Organics Analytical Laboratory, and MDL is the method detection limit. See table 1.2 for location of pools.

Table 3.3--Concentration of polychlorinated biphenyl congeners in surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River and analyzed by Wisconsin State Laboratory of Hygiene method, June-July 1994

[Concentrations are in nanograms per gram, ng/g IUPAC, International Union of Pure and Applied Chemistry; Reference, Lake Pepin reference sample; U, Upper Lake Pepin; L, Lower Lake Pepin; --, no congener detected; and gTOC, gram of total organic carbon in table 1.9 in Chapter 1]

| Congener IUPAC number | Refer- ence ¹ | Pool and date collected in 1994 | | | | | | | | | | | | Lake St. Croix | |
|-----------------------------|-----------------------------|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|-------------------|----|
| | | 1 | 2-1 | 2-2 | 3 | 4U | 4L | 5 | 6 | 7 | 8-1 | 8-2 | 9 | | 11 |
| | | 5-15-91 | 6-11 | 6-12 | 6-14 | 6-15 | 6-16 | 6-17 | 6-18 | 6-19 | 6-20 | 6-21 | 6-13 | | |
| 7 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 6 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 5/8 | 1.4 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 19 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 18 | 0.45 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 17 | 0.61 | -- | -- | -- | -- | -- | 0.32 | -- | -- | -- | -- | -- | -- | -- | |
| 24/27 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 16/32 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 26 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 28/31 | 5.5 | -- | 1.6 | 1.8 | -- | 2.5 | 2.4 | -- | -- | -- | -- | -- | -- | -- | |
| 33 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 22 | 0.80 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 45 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 46 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 52 | 4.6 | -- | 1 | 1.2 | 1.2 | 1.8 | 1.8 | -- | -- | -- | -- | -- | -- | 0.86 | |
| 49 | 3.4 | -- | 1.2 | 1.2 | 0.93 | 1.5 | 1.5 | -- | -- | -- | -- | -- | -- | 0.34 | |
| 47/48 | 2.8 | -- | 1.5 | 1.7 | 0.97 | 1.8 | 1.5 | -- | -- | -- | -- | -- | -- | 0.57 | |
| 44 | 3.2 | -- | 0.69 | 0.73 | 0.89 | 1.4 | 1.3 | -- | -- | -- | -- | -- | -- | -- | |
| 37/42 | 2.9 | -- | 0.59 | 0.65 | 0.54 | 1.0 | 1.1 | -- | -- | -- | -- | -- | -- | -- | |
| 41/64/71 | 2.9 | -- | -- | 0.58 | 0.65 | 1.1 | 1.1 | -- | -- | -- | -- | -- | -- | -- | |
| 40 | 0.52 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 74 | 2.3 | -- | -- | -- | -- | -- | 0.95 | -- | -- | -- | -- | -- | -- | -- | |
| 70/76 | 8.0 | -- | 1.6 | 1.8 | 2.3 | 3.5 | 3.2 | -- | -- | -- | -- | -- | -- | 1.2 | |
| 66/95 | 22 | 0.60 | 2.7 | 3.1 | 4.6 | 7.2 | 8.1 | 1.2 | -- | -- | -- | 0.74 | -- | 2.9 | |
| 91 | 3.2 | -- | 0.58 | 0.93 | 0.70 | 1.2 | 1.3 | -- | -- | -- | -- | -- | -- | 0.40 | |
| 56/60 | 4.3 | -- | -- | -- | 0.81 | 1.6 | 1.7 | -- | -- | -- | -- | -- | -- | 0.86 | |
| 84/92 | 7.5 | -- | 0.97 | 0.93 | 1.6 | 2.3 | 2.6 | -- | -- | -- | -- | -- | -- | 1.1 | |
| 101 | 12 | -- | 1.3 | 1.5 | 2.2 | 3.4 | 4.1 | 0.50 | -- | 0.34 | -- | -- | 0.35 | 1.4 | |
| 99 | 7.5 | -- | 0.70 | 0.77 | 1.2 | 2.1 | 2.5 | -- | -- | -- | -- | -- | -- | 0.79 | |
| 97 | 5.3 | -- | 0.46 | 0.49 | 0.82 | 1.4 | 1.7 | -- | -- | -- | -- | -- | -- | 0.54 | |
| 87 | 8.3 | -- | 0.70 | -- | 1.4 | 2.3 | 2.7 | -- | -- | -- | -- | -- | -- | 1.2 | |
| 85 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |
| 136 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | |

Table 3.3--Concentration of polychlorinated biphenyl congeners in surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River and analyzed by Wisconsin State Laboratory of Hygiene method, June-July 1994--Continued

| Congener IUPAC number | Refer- ence ¹ | Pool and date collected in 1994 | | | | | | | | | | | | | Lake St. Croix |
|-----------------------------|-----------------------------|---------------------------------|-------|-------|-------|-------|-------|------|------|------|------|------|------|----|-------------------|
| | | 1 | 2-1 | 2-2 | 3 | 4U | 4L | 5 | 6 | 7 | 8-1 | 8-2 | 9 | 11 | |
| | | 5-15-91 | 6-11 | 6-12 | 6-14 | 6-15 | 6-16 | 6-17 | 6-18 | 6-19 | 6-20 | 6-21 | 6-13 | | |
| 77/110 | 28 | 0.40 | 2.7 | 3.4 | 4.6 | 7.8 | 9.5 | 1.1 | -- | 0.83 | 0.43 | 0.47 | 0.83 | -- | 2.7 |
| 82 | 2.2 | -- | -- | -- | 0.31 | 0.56 | 0.64 | -- | -- | -- | -- | -- | -- | -- | -- |
| 151 | 3.0 | -- | -- | -- | 0.42 | 0.77 | 0.96 | -- | -- | -- | -- | -- | -- | -- | -- |
| 135/144 | 2.4 | -- | -- | -- | 0.35 | 0.68 | 0.82 | -- | -- | -- | -- | -- | -- | -- | -- |
| 149 | 10 | -- | 0.98 | 1.0 | 1.6 | 2.7 | 3.3 | 0.37 | -- | -- | -- | -- | -- | -- | 1.0 |
| 118 | 18 | -- | 1.6 | 1.6 | 2.7 | 4.7 | 5.2 | 0.60 | -- | -- | -- | -- | -- | -- | 1.3 |
| 146 | 4.1 | -- | -- | -- | 0.48 | 0.98 | 1.3 | -- | -- | -- | -- | -- | -- | -- | -- |
| 132/153 | 24 | 0.47 | 2.2 | 2.2 | 3.6 | 6.5 | 7.8 | 0.84 | -- | 0.60 | -- | -- | 0.64 | -- | 2.2 |
| 141 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 137/176 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 138 | 28 | 0.42 | 2.3 | 2.5 | 3.9 | 7.3 | 9.0 | 0.88 | -- | 0.66 | 0.42 | -- | 0.62 | -- | 2.1 |
| 178 | 0.81 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 182/187 | 2.7 | -- | -- | -- | -- | 0.66 | 0.69 | -- | -- | -- | -- | -- | -- | -- | -- |
| 183 | 2.5 | -- | -- | -- | -- | 0.72 | 0.75 | -- | -- | -- | -- | -- | -- | -- | 0.42 |
| 185 | 0.6 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 174 | 2.9 | -- | -- | -- | 0.42 | 0.81 | 0.96 | -- | -- | -- | -- | -- | -- | -- | -- |
| 177 | 2.5 | -- | -- | -- | -- | 0.71 | 0.87 | -- | -- | -- | -- | -- | -- | -- | -- |
| 171/202 | 1.2 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 172/197 | 1.1 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 180 | 8.0 | 0.39 | 0.67 | 0.68 | 1.2 | 2.3 | 2.6 | -- | -- | -- | -- | -- | -- | -- | 0.73 |
| 199 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 170/190 | 9.4 | -- | -- | 0.76 | 1.1 | 2.4 | 2.8 | -- | -- | -- | -- | -- | -- | -- | -- |
| 201 | 2.8 | -- | -- | -- | -- | 0.83 | 0.96 | -- | -- | -- | -- | -- | -- | -- | -- |
| 196/203 | 3.4 | -- | -- | -- | -- | 1.0 | 1.1 | -- | -- | -- | -- | -- | -- | -- | -- |
| 195/208 | 2.2 | -- | -- | -- | -- | -- | 0.78 | -- | -- | -- | -- | -- | -- | -- | -- |
| 194 | 1.8 | -- | -- | -- | -- | -- | 0.56 | -- | -- | -- | -- | -- | -- | -- | -- |
| 206 | 1.6 | -- | -- | -- | -- | 0.52 | 0.55 | -- | -- | -- | -- | -- | -- | -- | -- |
| 128 | 6.2 | -- | -- | -- | 0.75 | 1.4 | 1.8 | -- | -- | -- | -- | -- | -- | -- | -- |
| 167 | 1.2 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| Sum | 280.1 | 2.3 | 26.0 | 29.5 | 42.2 | 79.4 | 92.8 | 5.5 | -- | 2.4 | 0.8 | 1.2 | 2.4 | -- | 22.6 |
| Sum/gTOC | 5,600 | 620 | 2,800 | 2,500 | 2,600 | 2,200 | 2,400 | 560 | -- | 270 | 110 | 250 | 240 | -- | 890 |

¹Values are the average of two separate samples.

Table 3.4--Concentration of polychlorinated biphenyl congeners in surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River and analyzed by University of Minnesota Total Organics Analytical Laboratory, June-July 1994

[Concentrations are in nanograms per gram, ng/g; IUPAC, International Union of Pure and Applied Chemistry; Reference, Lake Pepin reference sample; i, interference present in the peak; ic, interference present in the peak as determined by the software program COMSTAR; --, below reporting limit (0.01 ng/g); and gTOC, gram of total organic carbon in table 1.9 in Chapter 1]

| Con- gener IUPAC number | Refer- ence ¹ | Pool and date collected in 1994 | | | | | | | | | | | | | | |
|----------------------------------|-----------------------------|---------------------------------|------|------|------|------|------|------|-------------------|------|-------------------|------|------|------|-------------------|-------------------|
| | | 10 | 12 | 13 | 14 | 15 | 16 | 18 | 19-1 ¹ | 19-2 | 20 ² | 21 | 22 | 24 | 25 ² | 26 ² |
| | | 5-15-91 | 6-21 | 6-22 | 6-23 | 6-23 | 6-26 | 6-27 | 6-28 | 6-29 | 6-30 | 7-01 | 7-02 | 7-03 | 7-04 | 7-05 |
| 4/10 | -- | 0.09 | 2.5 | 1.8 | 2.5 | i | i | i | 0.29 | 0.30 | -- | i | 0.89 | i | -- | -- |
| 7 | 0.43 | 0.06 | 0.15 | 0.27 | 0.40 | 0.51 | 1.02 | 0.33 | 0.12 | 0.14 | 0.40 | 0.75 | 0.09 | 0.13 | 0.22 | 0.34 |
| 6 | 0.35 | 0.04 | 0.07 | 0.04 | 0.03 | 0.08 | -- | 0.06 | 0.11 | 0.15 | -- | 0.05 | 0.03 | 0.01 | 0.05 | 0.20 |
| 5/8 | 1.01 | 0.04 | 0.13 | 0.05 | 0.04 | 0.20 | 0.22 | 0.04 | 0.14 | 0.13 | 0.06 | 0.12 | 0.05 | 0.04 | 0.06 | 0.26 |
| 19 | -- | 0.15 | 0.10 | 0.17 | 0.17 | 0.10 | 0.19 | 0.22 | -- | -- | 0.24 | 0.16 | -- | -- | -- | 0.10 |
| 18 | 3.9 | 1.97 | i | i | i | i | i | i | 1.1 | 1.7 | -- | ic | ic | ic | -- | -- |
| 17 | 3.3 | 0.23 | -- | -- | -- | -- | -- | -- | 0.45 | 0.69 | -- | -- | -- | -- | -- | -- |
| 24/27 | 0.12 | 0.01 | 0.01 | -- | -- | 0.02 | -- | -- | 0.06 | 0.06 | ³ 0.01 | 0.01 | 0.07 | 0.02 | ³ 0.03 | 0.06 |
| 16/32 | 0.32 | 0.32 | i | ic | ic | ic | ic | ic | 0.21 | 0.18 | -- | ic | ic | ic | -- | 1.56 |
| 29 | -- | 0.08 | 0.01 | -- | -- | 0.09 | 0.09 | -- | 0.14 | 0.23 | ³ 0.01 | 0.04 | -- | 0.03 | -- | 0.06 |
| 26 | 0.19 | -- | -- | -- | -- | 0.06 | -- | -- | -- | -- | -- | -- | 0.15 | -- | -- | ³ 0.14 |
| 25 | 0.14 | 0.04 | 0.09 | -- | 0.05 | -- | 0.16 | -- | 0.08 | 0.12 | ³ 0.04 | 0.05 | 0.19 | 0.06 | 0.06 | -- |
| 28/31 | 4.1 | 1.6 | i | ic | ic | ic | ic | i | 0.92 | 1.1 | -- | ic | ic | i | -- | -- |
| 21/33/53 | 2.2 | 0.23 | 0.73 | i | 1.3 | 2.6 | 5.3 | 2.0 | 0.30 | 0.35 | 2.9 | 4.0 | 0.79 | 0.58 | 0.84 | 1.58 |
| 51 | 0.28 | 0.13 | 0.24 | 0.09 | 0.21 | 1.10 | 1.4 | 0.55 | 0.14 | 0.18 | 0.10 | 0.91 | 0.03 | 0.04 | 0.10 | 0.30 |
| 22 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | 0.09 | -- | 0.08 | -- | -- | -- |
| 45 | 0.68 | 0.31 | 1.4 | 1.8 | 2.8 | 3.9 | i | 3.5 | 0.17 | 0.19 | -- | i | -- | 0.77 | 1.2 | 3.1 |
| 46 | 0.30 | 0.08 | 0.18 | -- | -- | -- | -- | -- | 0.08 | 0.08 | -- | -- | 0.25 | 0.19 | -- | 0.53 |
| 52 | 7.9 | 0.20 | 0.67 | 0.41 | 0.40 | 0.98 | 0.76 | 0.41 | 0.76 | 0.82 | 0.28 | 0.47 | 0.48 | 0.34 | 0.54 | 0.76 |
| 43 | -- | 0.08 | 0.19 | -- | 0.22 | 0.19 | 0.54 | 0.10 | 0.10 | 0.12 | 0.32 | 0.57 | 0.06 | 0.04 | 0.12 | 0.16 |
| 49 | 6.0 | 0.39 | 0.65 | 0.36 | 0.41 | 0.90 | 0.71 | 0.29 | 0.47 | 0.59 | 0.08 | 0.24 | 0.23 | 0.13 | 0.34 | 0.56 |
| 47/48 | 4.3 | 0.46 | 0.94 | 0.60 | 0.58 | 1.22 | 1.10 | 0.54 | 0.63 | 0.80 | 0.48 | 0.70 | 0.43 | 0.45 | 0.64 | ³ 0.89 |
| 44 | 3.4 | 0.16 | 0.19 | 0.26 | 0.12 | 0.48 | 0.39 | 0.21 | 0.34 | 0.44 | 0.06 | 0.18 | 0.16 | 0.19 | 0.24 | 0.36 |
| 42 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 41/71 | 1.1 | 0.12 | 0.09 | 0.05 | 0.03 | 0.16 | 0.10 | 0.04 | 0.09 | 0.17 | 0.02 | 0.06 | 0.04 | 0.04 | 0.04 | 0.08 |
| 64 | 7.4 | 1.2 | 1.3 | 1.0 | 0.74 | 0.83 | 0.68 | 1.0 | 0.88 | 1.1 | 0.74 | 1.11 | 0.59 | 0.74 | 0.62 | 0.60 |
| 40 | 0.28 | 0.03 | -- | -- | -- | -- | -- | -- | ³ 0.02 | -- | -- | -- | -- | -- | -- | -- |
| 100 | 0.50 | 0.15 | 0.20 | 0.15 | 0.13 | 0.24 | 0.29 | 0.16 | 0.26 | 0.28 | 0.09 | 0.25 | 0.29 | 0.18 | 0.18 | 0.52 |
| 63 | 0.36 | 0.05 | -- | 0.01 | 0.01 | -- | -- | -- | -- | 0.04 | 0.01 | -- | -- | -- | 0.01 | -- |
| 74 | 2.1 | 0.17 | 0.26 | 0.11 | 0.06 | 0.25 | 0.20 | 0.13 | 0.27 | 0.24 | 0.04 | 0.07 | 0.31 | 0.05 | 0.16 | 0.40 |
| 70/76 | 4.6 | 0.20 | 0.74 | 0.16 | 0.11 | 0.59 | 0.65 | 0.21 | 0.34 | 0.37 | 0.07 | 0.19 | 0.33 | 0.16 | 0.21 | 0.57 |
| 95/66 | 6.9 | 0.21 | 0.17 | 0.11 | 0.09 | 0.43 | 0.39 | 0.07 | 0.17 | 0.09 | 0.07 | 0.16 | 0.13 | 0.12 | 0.16 | 0.34 |
| 91 | 1.8 | 0.38 | 0.56 | 0.10 | 0.20 | 0.32 | 0.33 | 0.09 | 0.15 | 0.10 | 0.06 | 0.13 | 0.29 | 0.18 | 0.10 | 0.46 |

Table 3.4--Concentration of polychlorinated biphenyl congeners in surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River and analyzed by University of Minnesota Total Organics Analytical Laboratory, June-July 1994--Continued

| Con- gener IUPAC number | Refer- ence ¹ | Pool and date collected in 1994 | | | | | | | | | | | | | | |
|----------------------------------|-----------------------------|---------------------------------|------|------|------|------|------|------|-------------------|------|-------------------|------|------|------|-------------------|-------------------|
| | | 10 | 12 | 13 | 14 | 15 | 16 | 18 | 19-1 ¹ | 19-2 | 20 ² | 21 | 22 | 24 | 25 ² | 26 ² |
| | 5-15-91 | 6-21 | 6-22 | 6-23 | 6-23 | 6-26 | 6-27 | 6-28 | 6-29 | 6-30 | 7-01 | 7-02 | 7-03 | 7-04 | 7-05 | |
| 56/60 | 1.1 | -- | -- | -- | -- | 0.27 | 0.08 | 0.05 | 0.06 | 0.08 | 0.02 | 0.07 | 0.04 | -- | 0.02 | 0.26 |
| 84/92 | 6.4 | 0.73 | ic | ic | ic | ic | 0.61 | ic | 0.43 | 0.62 | 0.12 | ic | ic | 0.19 | 0.32 | 1.1 |
| 89 | 0.21 | 0.05 | -- | 0.02 | 0.04 | 0.12 | 0.08 | 0.07 | -- | -- | 0.04 | 0.09 | 0.03 | -- | -- | 0.27 |
| 101 | 13.6 | 0.27 | 0.34 | 0.24 | 0.28 | ic | 0.74 | 0.21 | 0.61 | 0.42 | 0.24 | ic | 0.36 | 0.23 | 0.42 | 1.4 |
| 99 | 8.1 | 0.64 | 0.45 | ic | ic | ic | 0.61 | ic | 0.68 | 0.89 | 0.19 | ic | ic | ic | -- | 1.5 |
| 119 | 0.71 | -- | -- | -- | -- | 0.08 | 0.06 | 0.07 | 0.05 | 0.06 | ³ 0.01 | 0.04 | 0.04 | 0.02 | 0.02 | 0.05 |
| 83 | 1.41 | -- | 0.09 | 0.03 | 0.02 | 0.06 | 0.13 | 0.02 | 0.09 | 0.14 | 0.01 | 0.03 | 0.01 | 0.05 | 0.07 | 0.14 |
| 97 | 4.8 | 0.12 | 0.22 | 0.13 | 0.10 | 0.26 | 0.17 | 0.04 | 0.27 | 0.28 | 0.02 | 0.17 | 0.06 | 0.02 | 0.18 | 0.28 |
| 87 | 5.1 | 0.16 | 0.23 | 0.12 | 0.10 | 0.27 | 0.22 | 0.11 | 0.21 | 0.25 | 0.06 | 0.17 | 0.09 | 0.08 | 0.12 | 0.23 |
| 85 | 1.9 | 0.10 | 0.13 | 0.04 | 0.03 | 0.09 | 0.07 | 0.04 | 0.09 | 0.11 | 0.01 | 0.06 | 0.03 | 0.01 | 0.06 | 0.13 |
| 136 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | 1.2 |
| 77/110 | 20.5 | 0.54 | 0.59 | 0.35 | 0.28 | 0.72 | 0.59 | 0.28 | 0.45 | 0.54 | 0.10 | 0.38 | 0.22 | 0.18 | 0.26 | 0.42 |
| 82 | 2.4 | 0.05 | 0.06 | 0.03 | 0.05 | 0.07 | 0.17 | 0.07 | 0.07 | 0.12 | 0.04 | 0.06 | 0.04 | 0.04 | 0.04 | 0.17 |
| 151 | 5.3 | 0.35 | 0.40 | 0.18 | 0.22 | 0.24 | 0.32 | 0.28 | 0.12 | 0.12 | 0.12 | 0.21 | 0.09 | 0.07 | 0.08 | 0.16 |
| 135/144 | 4.2 | 0.08 | 0.10 | 0.06 | 0.06 | 0.09 | 0.06 | 0.06 | 0.09 | 0.10 | 0.04 | 0.07 | 0.08 | 0.07 | 0.08 | 0.16 |
| 124 | 0.57 | -- | -- | 0.02 | 0.01 | 0.06 | -- | 0.02 | 0.03 | 0.04 | ³ 0.01 | -- | 0.02 | 0.03 | 0.02 | -- |
| 147 | 1.1 | 0.03 | 0.04 | 0.03 | 0.03 | 0.11 | 0.05 | 0.03 | 0.03 | 0.05 | 0.02 | 0.06 | 0.03 | 0.02 | 0.03 | 0.13 |
| 107 | 2.6 | 0.05 | 0.05 | 0.05 | 0.05 | 0.21 | 0.08 | 0.07 | 0.04 | 0.06 | 0.02 | 0.10 | 0.02 | 0.03 | 0.03 | ³ 0.08 |
| 123/149 | 16.7 | 0.26 | 0.31 | 0.22 | 0.20 | 0.37 | 0.25 | 0.17 | 0.38 | 0.41 | 0.08 | 0.28 | 0.18 | 0.19 | 0.24 | 0.50 |
| 118 | 12.9 | 0.30 | 0.37 | 0.25 | 0.19 | 0.50 | 0.38 | 0.19 | 0.29 | 0.34 | 0.06 | 0.33 | 0.11 | 0.09 | 0.14 | 0.23 |
| 134 | 1.9 | 0.02 | -- | 0.01 | 0.01 | 0.03 | -- | 0.01 | 0.03 | 0.03 | 0.01 | 0.02 | 0.01 | 0.01 | 0.01 | 0.04 |
| 114 | 1.8 | 0.07 | 0.11 | 0.07 | 0.14 | 0.24 | 0.14 | 0.08 | 0.20 | 0.22 | 0.03 | 0.36 | 0.08 | 0.07 | 0.18 | 0.30 |
| 131/122 | 1.6 | 0.04 | 0.08 | -- | -- | 0.05 | -- | -- | ³ 0.04 | 0.05 | -- | 0.01 | -- | 0.01 | ³ 0.02 | -- |
| 146 | 4.7 | 0.09 | 0.11 | 0.04 | 0.04 | 0.09 | 0.05 | 0.05 | 0.10 | 0.10 | 0.01 | 0.06 | 0.04 | 0.03 | 0.04 | 0.10 |
| 132/153/105 | 31.0 | 0.54 | 0.64 | 0.42 | 0.37 | 0.71 | 0.60 | 0.36 | 0.64 | 0.74 | 0.10 | 0.44 | 0.29 | 0.28 | 0.38 | 0.75 |
| 141 | 6.4 | 0.21 | 0.24 | 0.08 | 0.13 | 0.21 | 0.20 | 0.15 | 0.16 | 0.18 | 0.03 | 0.13 | 0.14 | 0.11 | 0.10 | 0.18 |
| 137/176 | 2.9 | 0.24 | 0.35 | 0.09 | 0.12 | 0.14 | 0.11 | 0.21 | 0.12 | 0.09 | 0.04 | 0.10 | 0.17 | 0.07 | 0.08 | 0.16 |
| 130 | 3.2 | 0.62 | 0.90 | 0.18 | 0.19 | 0.22 | 0.21 | 0.36 | 0.08 | 0.10 | 0.05 | 0.15 | 0.09 | 0.02 | 0.07 | 0.20 |
| 163/138 | 19.5 | 0.19 | 0.17 | 0.15 | 0.12 | 0.26 | 0.26 | 0.13 | 0.32 | 0.37 | 0.05 | 0.22 | 0.23 | ic | 0.20 | 0.46 |
| 158 | 2.2 | 0.06 | 0.07 | 0.02 | 0.02 | 0.03 | 0.04 | 0.04 | ³ 0.03 | 0.04 | ³ 0.01 | 0.02 | 0.04 | 0.01 | 0.02 | 0.06 |
| 126/129 | 0.4 ³ | 0.28 | 0.22 | 0.14 | 0.10 | 0.08 | 0.16 | 0.18 | 0.41 | 0.37 | 0.10 | 0.11 | 0.38 | 0.39 | 0.41 | 0.60 |
| 178 | 1.6 | -- | 0.11 | -- | -- | -- | 0.06 | -- | ³ 0.06 | 0.09 | -- | -- | -- | -- | ³ 0.02 | -- |
| 187/182 | 3.2 | 0.08 | 0.05 | 0.09 | 0.14 | 0.10 | 0.10 | 0.12 | 0.17 | 0.18 | 0.08 | 0.11 | 0.05 | 0.13 | 0.10 | 0.15 |
| 183 | 1.9 | 0.12 | 0.14 | 0.03 | 0.07 | 0.12 | 0.05 | 0.03 | 0.05 | 0.06 | ³ 0.01 | 0.03 | 0.03 | 0.03 | 0.03 | 0.06 |
| 128 | 5.8 | 0.20 | 0.23 | 0.08 | 0.05 | 0.09 | 0.13 | 0.04 | 0.10 | 0.13 | ³ 0.01 | 0.06 | 0.05 | 0.03 | 0.06 | 0.11 |

Table 3.4--Concentration of polychlorinated biphenyl congeners in surficial bed sediment collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River and analyzed by University of Minnesota Total Organics Analytical Laboratory, June-July 1994--Continued

| Con- gener IUPAC number | Refer- ence ¹ 5-15-91 | Pool and date collected in 1994 | | | | | | | | | | | | | | |
|----------------------------------|--|---------------------------------|-------|-------|-------|-------|-------|-------|-------------------|-------|-------------------|-------|-------|-------|-----------------|-----------------|
| | | 10 | 12 | 13 | 14 | 15 | 16 | 18 | 19-1 ¹ | 19-2 | 20 ² | 21 | 22 | 24 | 25 ² | 26 ² |
| | | 6-21 | 6-22 | 6-23 | 6-23 | 6-26 | 6-27 | 6-28 | 6-29 | 6-30 | 7-01 | 7-02 | 7-03 | 7-04 | 7-05 | |
| 167 | 2.0 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- |
| 185 | 0.4 | 0.05 | 0.04 | 0.04 | 0.04 | 0.18 | 0.08 | 0.03 | 0.02 | 0.03 | ³ 0.01 | 0.03 | 0.03 | 0.02 | 0.02 | 0.04 |
| 174 | 2.4 | 0.03 | 0.06 | 0.03 | 0.07 | 0.17 | 0.05 | 0.06 | 0.07 | 0.06 | 0.02 | 0.07 | 0.03 | 0.03 | 0.04 | 0.15 |
| 177 | 2.1 | 0.08 | 0.11 | 0.07 | 0.10 | 0.28 | 0.08 | 0.10 | 0.07 | 0.07 | 0.04 | 0.07 | 0.06 | 0.04 | 0.05 | 0.12 |
| 202/171 | 1.2 | 0.05 | 0.04 | 0.01 | 0.05 | 0.13 | 0.04 | 0.04 | 0.03 | 0.03 | 0.05 | 0.03 | 0.02 | 0.02 | 0.02 | 0.05 |
| 156 | 3.7 | 0.08 | 0.16 | 0.02 | 0.03 | 0.20 | 0.13 | 0.06 | 0.07 | 0.10 | ³ 0.02 | 0.02 | 0.02 | 0.06 | 0.03 | 0.12 |
| 173 | 0.19 | 0.03 | 0.04 | 0.01 | 0.01 | 0.03 | 0.03 | 0.02 | 0.033 | 0.04 | -- | 0.02 | -- | 0.01 | 0.02 | 0.06 |
| 172/197 | 0.68 | 0.06 | -- | 0.03 | -- | 0.07 | 0.03 | 0.03 | 0.02 | 0.03 | -- | 0.04 | 0.02 | 0.02 | 0.02 | 0.02 |
| 180 | 5.2 | 0.05 | 0.13 | 0.05 | 0.22 | 0.12 | 0.13 | 0.04 | 0.11 | 0.15 | 0.03 | 0.10 | 0.05 | 0.08 | 0.06 | 0.12 |
| 193 | 0.2 | 0.01 | 0.02 | -- | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | -- | 0.02 | -- | 0.01 | -- | 0.01 |
| 191 | 0.67 | -- | 0.01 | 0.03 | 0.03 | 0.04 | 0.06 | -- | 0.02 | 0.05 | -- | 0.04 | 0.03 | 0.01 | 0.02 | 0.04 |
| 199 | 0.3 | 0.03 | 0.03 | 0.02 | 0.04 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | -- | 0.02 | 0.01 | -- | 0.01 | 0.02 |
| 170/190 | 3.2 | 0.08 | 0.05 | 0.06 | 0.05 | 0.03 | 0.07 | 0.03 | 0.06 | 0.05 | 0.01 | 0.04 | 0.03 | 0.03 | 0.03 | 0.08 |
| 198 | 0.17 | 0.25 | i | i | i | i | i | i | -- | i | -- | i | i | i | -- | -- |
| 201 | 1.3 | 0.04 | 0.07 | -- | 0.12 | 0.03 | 0.08 | 0.04 | 0.07 | 0.06 | 0.02 | 0.02 | 0.04 | 0.06 | 0.03 | 0.08 |
| 203/196 | 1.2 | 0.02 | 0.02 | 0.01 | 0.12 | -- | 0.03 | -- | 0.04 | 0.03 | 0.01 | -- | 0.01 | 0.02 | 0.01 | 0.04 |
| 189 | 0.21 | -- | 0.00 | -- | -- | 0.06 | 0.03 | 0.03 | -- | -- | -- | -- | 0.04 | -- | -- | 0.03 |
| 208/195 | 0.68 | 0.03 | 0.03 | 0.02 | 0.05 | 0.03 | 0.03 | 0.02 | 0.03 | 0.02 | 0.01 | 0.02 | 0.03 | 0.01 | 0.01 | 0.03 |
| 207 | 0.22 | 0.01 | 0.03 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 194 | 1.6 | 0.02 | 0.09 | -- | 0.10 | 0.04 | 0.07 | 0.03 | 0.06 | 0.05 | 0.01 | 0.04 | 0.05 | 0.03 | 0.02 | 0.04 |
| 205 | 0.72 | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | -- | 0.03 |
| Sum | 290 | 17 | 19 | 11 | 15 | 23 | 22 | 14 | 15 | 19 | 8 | 15 | 10 | 7 | 10 | 23 |
| Sum/gTOC | 6,200 | 4,300 | 1,300 | 1,200 | 1,200 | 3,900 | 2,700 | 2,400 | 1,900 | 2,700 | 6,500 | 2,700 | 2,100 | 2,400 | 1,300 | 2,200 |

¹Five replicate samples.

²Two replicate samples.

³There is at least one nondetection not included in the average.

SUMMARY

Surficial bed-sediment samples from the navigation pools of the Upper Mississippi River were analyzed for PCB congeners at two laboratories. The Wisconsin State Laboratory of Hygiene in Madison, Wis., analyzed samples from Pools 1 to 11, except 5A and 10. The University of Minnesota Trace Organic Analytical Laboratory in Duluth, Minn., was used for Pools 10, and 12 through 26, except 17.

Maximum total PCB concentrations in surficial bed sediments were found in Pools 2 through 4 immediately downstream from the Twin Cities metropolitan area. This was consistent with previous PCB data in environmental samples for the Upper Mississippi River. Total organic carbon-normalized PCB values were largest in samples collected from the downstream portion of the study area (Pools 10, 15, and 20). PCB method differences and lower total organic carbon contents in bed sediments collected from the lower navigation pools influenced the spatial results.

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CHAPTER 4 - Organochlorine Compounds

By Dawn E. Hrinko and John A. Moody

ABSTRACT

Representative subsamples of surficial bed sediment were collected from 24 navigation pools on the Upper Mississippi River and analyzed for organochlorine compounds (aldrin; *p,p'*-DDD; *p,p'*-DDE; *p,p'*-DDT; dieldrin; endosulfan I; endrin; heptachlor; heptachlor epoxide; lindane; *p,p'*-methoxychlor; mirex; perthane; gross polychlorinated biphenyls; gross polychlorinated naphthalenes; technical chlordane; and toxaphene). The samples were analyzed at the U.S. Geological Survey National Water Quality Laboratory in Arvada, Colorado, using an analytical method that uses shake-extraction with acetone-hexane and analysis of the extract by capillary gas chromatography with electron-capture detection.

The concentrations of most organochlorine compounds in the surficial bed sediments were below reporting levels. However, the maximum concentration of *p,p'*-DDT [1.8 nanograms per gram (ng/g)] was in Pool 15, dieldrin (0.7 ng/g) was in Pool 26, gross polychlorinated biphenyls (33 ng/g) was in Pool 3, and technical chlordane (2ng/g) was in Pools 4 (Lake Pepin) and 21.

INTRODUCTION

Organochlorine compounds are widespread in the environment and are derived both from manufactured and natural sources. The manufacture, distribution, and use of insecticides, pesticides, and industrial chemicals [like polychlorinated biphenyls (PCB) and polychlorinated naphthalenes (PCN)] have contributed to a large array of organic contaminants and their degradation products in the environment. Anthropogenic activities such as incineration of manufactured organic compounds and combustion of fossil fuels have contributed to the production and airborne release of contaminants such as dioxins, furans, and polynuclear aromatic hydrocarbons (Voldner and Li, 1995). The organochlorine contaminants associated with surficial bed sediments determined in this study are aldrin, *p,p'*-DDD; *p,p'*-DDE; *p,p'*-DDT; dieldrin; endosulfan I; endrin; heptachlor; heptachlor epoxide; lindane; *p,p'*-methoxychlor; mirex; perthane; gross polychlorinated biphenyls; gross polychlorinated naphthalenes; technical chlordane; and toxaphene.

Organochlorine compounds have been released to the air, water, and land over many years through their use and disposal. As a result of their chemical structure, organochlorine compounds are often highly persistent contaminants in aquatic and terrestrial ecosystems. This is true even though the production and use of some of these compounds such as DDT and PCB have been eliminated or greatly restricted since 1977. Their solubility in water is generally low; as a result, in aquatic systems they are mainly found adsorbed to suspended particulate matter and in bed sediments, especially silt-sized and clay-sized sediment (less than 63 μm) with high organic carbon content. Thus, contaminated sediments provide a major source of present-day exposure of these chemicals to aquatic organisms (Lyman and others, 1987; Baudo and others, 1990).

Runoff from contaminated soils or improper disposal are important pathways that have led to serious contamination problems in both riverine and lacustrine systems. Volatilization of organochlorine compounds to the atmosphere has resulted in their global distribution. When present at acute concentrations these organochlorine compounds can directly affect the distribution and abundance of aquatic organisms. Furthermore, long-term exposure at low concentrations may contribute to carcinogenic, teratogenic, and mutagenic effects. The transfer of organochlorine contaminants through the aquatic food chain contributes to contamination problems in fish, piscivorous mammals and birds, and eventually humans. In some instances, PCB and chlordane contamination in fish from the Mississippi River resulted in certain States issuing consumption advisories for the commercial and sport fishery.

PURPOSE AND SCOPE

The purpose of this chapter is to describe the method used to determine the concentration of organochlorine compounds in the surficial bed sediments collected during June 1994 from the downstream one-third of 24 navigation pools of the Upper Mississippi River after the flood of 1993 and to list the results in tables. The spatial distribution of some of the more abundant compounds in the Upper Mississippi River are shown graphically.

ANALYTICAL METHOD

After the composite samples were collected in the field (see Chapter 1), they were kept refrigerated at about 4°C in glass jars with Teflon-lined lids until they were analyzed by the U.S. Geological Survey National Water Quality Laboratory's Schedule 1325 method (hereinafter referred to as the Schedule 1325 method).

A large volume (240 L) of surficial bed sediment was collected from lower Lake Pepin in May 1991 and prepared as a reference sample by personnel from the U.S. Army Corps of Engineers (St. Paul and Rock Island Districts), the Minnesota Pollution Control Agency, the Wisconsin Department of Natural Resources, and the U.S. Fish and Wildlife Service. The wet sediment was mixed in three batches (approximately 80 L each) using a large Hobart blender and then portioned into individual glass containers and frozen. Samples of the Lake Pepin reference sample were analyzed by the Schedule 1325 method, and the results are listed in the data tables as "Reference."

The Schedule 1325 method is used for the determination of organochlorines in sediment in the following order: lindane; heptachlor; aldrin; heptachlor epoxide; technical chlordane; endosulfan I; dieldrin; *p,p'*-DDE; endrin; perthane; *p,p'*-DDD; *p,p'*-DDT; *p,p'*-methoxychlor; mirex; toxaphene; gross polychlorinated biphenyls (PCB); and gross polychlorinated naphthalenes (PCN) (Wershaw and others, 1987). Gross PCB are the sum of Aroclors 1242, 1254, and 1260.

Sample Preparation

The sample preparation consisted of three steps: extraction, concentration, and cleanup. Organochlorine compounds were extracted from 50 g of equivalent dry sediment. The homogenized wet sediment was shaken on a wrist-action shaker for 20 minutes with 20 mL of acetone, then shaken for 10 minutes with 80 mL of hexane. The solvent was decanted and the process repeated two additional times. The combined extracts were gently rolled in a separatory funnel containing 500 mL of distilled water to remove the acetone. The hexane layer was removed and concentrated to approximately 4 mL in a 500-mL Kuderna-Danish apparatus. It was concentrated to exactly 4 mL by using a gentle stream of nitrogen.

The first step in the cleanup procedure was to fractionate the sample on an 8.5-percent deactivated alumina column using 2 mL of the 4-mL Kuderna-Danish extract. The sample was eluted with 43 mL of hexane to obtain the A1 fraction (18 mL) and the A2 fraction (25 mL). The A3 fraction (20 mL) was collected by eluting with 20 mL of benzene. The A1 fraction was evaporated to exactly 1 mL under a gentle stream of nitrogen. Sulfur was removed by shaking the A1 fraction with elemental mercury. The A1 fraction was further fractionated on a 3.0-percent deactivated silica column that was prerinsed with hexane and eluted with 19 mL of hexane to obtain the S1 fraction (20 mL). The S2 fraction (20 mL) was collected by eluting the column with 20 mL of benzene. A portion of the final extract from the A2 and A3 fractions was archived and a portion used for analysis.

Sample Analysis

Organochlorine analytes are confirmed on a dual-column capillary gas chromatograph (Hewlett-Packard 5890) with dual electron-capture detectors. Rtx-5 and Rtx-1701 columns (30-m by 0.25-mm, Restek Corporation) were preceded with an uncoated guard column connected to the injector by a glass Y union and a splitless deactivated liner. The oven temperature ramp was from 60°C (held for 2 minutes) to 180°C at 30°C per minute (held for 2 minutes at 180°C), to 210°C at 1°C per minute and finally to 280°C at 4°C per minute, and held for 5 to 25 minutes. The injector port temperature was 220°C and the detector temperature was 350°C. The carrier gas was helium and the make-up gas was nitrogen.

A solution containing *p,p'*-DDT and endrin was used to evaluate the percent breakdown of these analytes in the injection port. This solution was followed by standards containing aldrin; *p,p'*-DDD; *p,p'*-DDE; *p,p'*-DDT; dieldrin; endosulfan I; endrin; heptachlor; heptachlor epoxide; lindane; *p,p'*-methoxychlor; mirex; and perthane at 1, 5, 10, 20, 50, and 100 pg/μL; Aroclors 1242, 1254, and 1260 at 50 and 100 pg/μL; toxaphene at 400 and 800 pg/μL; technical chlordane at 40, 80, and 160 pg/μL; and a third-party standard containing at least six of the organochlorine analytes at 20 pg/μL. Standards were measured to within 20 percent of their acceptable value. A method blank was analyzed for every 10 samples, and a reagent spike containing all of the individual organochlorine analytes was used to monitor method accuracy.

The method detection limits were determined using the procedure outlined in the Code of Federal Regulations (U.S. Environmental Protection Agency, 1991) and were rounded up to the reporting levels. The reporting levels (see table 4.1) are listed for the analytes in the order that they elute from the Rtx-5 column. Each sample was spiked with a surrogate, isodrin, at 0.200 ng/g. The accuracy data (table 4.1) are the mean percent recovery of 20 samples for each spike analyte. The precision data (table 4.1) are the mean relative percent differences for each analyte calculated from 10 sets of sample duplicates. A midrange standard (20 pg/μL) was run every 10 samples to monitor analytical performance.

A minimum 5-point calibration curve bracketing the targeted concentration range (generally 1 to 100 pg/μL) must requantitate within 20 percent of the expected values based on a linear regression coefficient (r^2) greater than 0.995. Continuing calibration checks (± 20 percent) and performance check standards (breakdown less than or equal to 20 percent) were run every 8 to 10 samples. One blank was run for every 10 samples, and analyte concentrations in the blanks were all less than the reporting level. A third-party check standard was run at the beginning of each batch (± 30 percent) to ensure the standards were accurate. Surrogates were added to all samples, blanks, and spikes; the surrogates had to measure within three standard deviations of the mean. Two compounds, tetrachloro-*m*-xylene and decachloro-biphenyl, were added to all samples as retention-time markers (Hrinko, 1994).

Table 4.1--Accuracy estimates, precision estimates, and reporting levels of organochlorine measurements made using the U.S. Geological Survey National Water Quality Laboratory Schedule 1325 method

[These values reflect the analytical laboratory uncertainty and do not include the field sampling uncertainty; accuracy is given as the mean percent recovery (%) for 20 samples; precision is given as the mean relative percent difference (RPD) for each analyte calculated from 10 sets of sample duplicates; ng/g, nanograms per gram; na, not available]

| Analyte | Reporting level ¹ (ng/g) | Accuracy (%) | Precision (RPD) |
|---------------------------|--|-----------------|--------------------|
| Lindane | 0.1 | 78 | 11 |
| Heptachlor | 0.1 | 73 | 10 |
| Aldrin | 0.1 | 75 | 1.1 |
| Heptachlor epoxide | 0.1 | 74 | 2.5 |
| Technical chlordane | 1. | 70 | 5.7 |
| Endosulfan I | 0.1 | 67 | 2.6 |
| Dieldrin | 0.1 | 79 | 2.2 |
| <i>p,p'</i> -DDE | 0.1 | 82 | 5.3 |
| Endrin | 0.1 | 63 | na |
| Perthane | 1. | 103 | na |
| <i>p,p'</i> -DDD | 0.1 | 91 | 5.8 |
| <i>p,p'</i> -DDT | 0.1 | 77 | 5.8 |
| <i>p,p'</i> -methoxychlor | 0.1 | 103 | na |
| Mirex | 0.1 | 68 | 32 |
| Toxaphene | 10 | 71 | na |
| Gross PCB | 1 | 99 | 3.1 |
| Gross PCN | 1 | na | na |

¹Reporting level for ideal matrix; if there are interferences, the reporting level is raised.

RESULTS

The concentrations of organochlorine compounds associated with the reference sample and the surficial sediments from the navigation pools are listed in table 4.2. Two samples of the Lake Pepin reference sample were analyzed separately, and one sample was split into two duplicates. Most organochlorine compounds in the reference sample were below the reporting level. Organochlorine compounds in the reference sample that were above the reporting level were technical chlordane, *p,p'*-DDE, *p,p'*-DDD, and gross PCB; the relative standard deviations of the three analyses were 0, 26, 36, and 17 percent, respectively.

Most of the organochlorines compounds in the surficial bed sediments were less than the reporting level; however, *p,p'*-DDE, *p,p'*-DDD, and gross PCB were found in all composite samples. Dieldrin, *p,p'*-DDT, and technical chlordane were found in some composite samples, generally with highest concentrations in samples collected from the upper one-half of the navigation pool reach. The concentrations of *p,p'*-DDE and dieldrin are shown in figures 4.1 and 4.2.

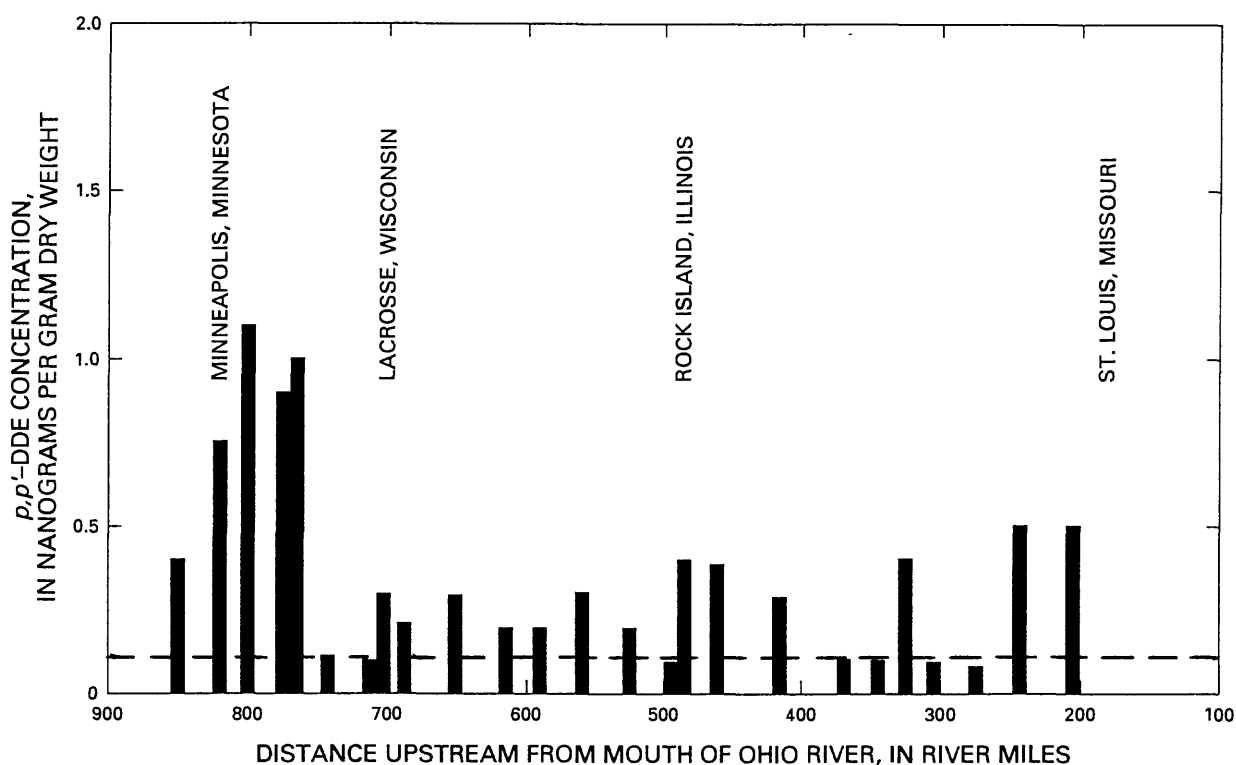


Figure 4.1--Concentration of *p,p'*-DDE in surficial bed sediment in the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. No composite samples were collected from pools 5A and 17. The dashed line is at the reporting level equal to 0.1 nanogram per gram. See table 1.2 for location of pools.

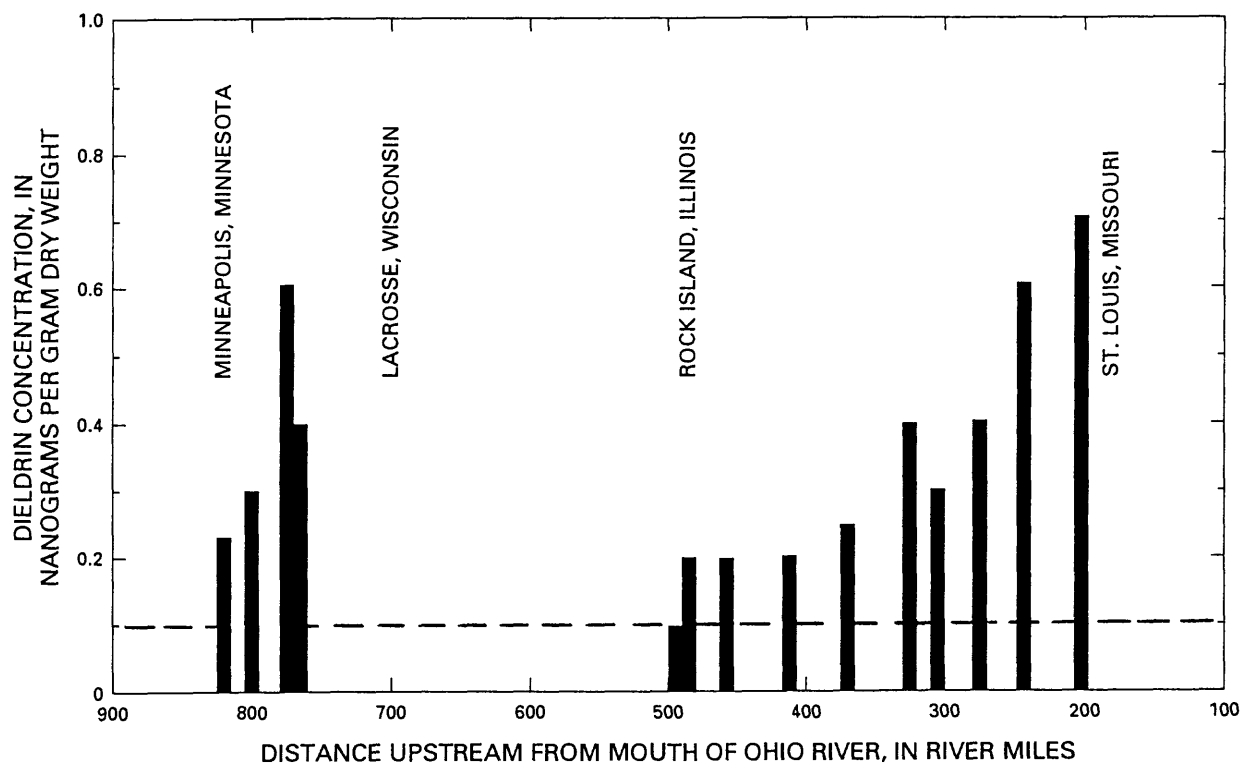


Figure 4.2--Concentration of dieldrin in bed sediments in the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. No composite samples were collected from pools 5A and 17. Dieldrin was detected in pools 5-13 (between river miles 500 and 750) but it was below the reporting limit so no bar is drawn. The dashed line is at the reporting level equal to 0.1 nanogram per gram. See table 1.2 for location of pools.

SUMMARY

Composite surficial bed-sediment samples were collected from the downstream one-third of 24 navigation pools of the Upper Mississippi River and were analyzed for organochlorine compounds by the U.S. Geological Survey National Water Quality Laboratory Schedule 1325 method.

The concentration of most organochlorine compounds in the surficial bed sediments was below the reporting level; however, concentrations of *p,p'*-DDE, *p,p'*-DDD and gross PCB were above the reporting level in all pools. Maximum concentration of *p,p'*-DDD [3.8 nanogram per gram, ng/g]; *p,p'*-DDE (1.1 ng/g); and PCB (33 ng/g) were all in Pool 3. Concentration of *p,p'*-DDT was a maximum in Pool 15 (1.8 ng/g), but in most other pools it was less than the reporting level. The concentration of dieldrin was a maximum in Pool 26 (0.7 ng/g).

Table 4.2--Concentration of organochlorine compounds on surficial bed sediments collected from based on the Schedule 1325 method,

[Analyzed by gas chromatography/electron-capture detector; one blank was run for every 10 samples and all blanks had analyte PCB, polychlorinated biphenyls; PCN, polychlorinated naphthalenes; Ref., Lake Pepin reference sample;

| Pool duplicate | Date | Number of samples in composite | | Lindane | Hepta-chlor | Aldrin | Hepta-chlor epoxide | Technical chlordane | Endo-sulfan I | Dieldrin | p-p'-DDE | Endrin |
|-----------------|--------------------|--------------------------------|-----------|---------|-------------|--------|---------------------|---------------------|---------------|----------|----------|--------|
| | | 1994 | 1991-1992 | | | | | | | | | |
| Ref. 1-1 | 05-15-91 | -- | -- | <0.1 | <0.1 | <0.1 | <0.1 | 2. | <0.3 | 0.4 | 2.9 | <0.1 |
| Ref. 2-1 | | -- | -- | <0.1 | <0.1 | <0.1 | <0.1 | 2. | <0.1 | <0.4 | 1.9 | <0.1 |
| Ref. 2-2 | | -- | -- | <0.1 | <0.1 | <0.1 | <0.1 | 2. | <0.1 | <0.4 | 1.9 | <0.1 |
| 1 | 06-11-94 | 12 | 12 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | <0.2 | 0.4 | <0.1 |
| 2-1 | 06-12-94 | 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | 0.2 | 0.6 | <0.1 |
| 2-2 | 06-12-94 | 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | 0.3 | 0.9 | <0.1 |
| St. Croix River | 06-13-84 | 15 | ns | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.7 | <0.1 |
| 3 | 06-14-94 | 15 | 16 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.3 | 1.1 | <0.1 |
| ¹⁴ | 06-15-94 | 14 | 15 | <0.3 | <0.3 | <0.3 | <0.3 | 2. | <0.3 | 0.6 | 0.9 | <0.3 |
| ²⁴ | 06-15-94 | 20 | 21 | <0.1 | <0.1 | <0.1 | <0.1 | 2. | <0.1 | 0.4 | 1.0 | <0.1 |
| 5 | 06-16-94 | 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.1 | <0.1 |
| 6 | 06-17-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.1 | <0.1 |
| 7 | 06-18-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.3 | <0.1 |
| 8-1 | 06-19-94 | 19 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.3 | <0.1 |
| 8-2 | | 19 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.1 | <0.1 |
| 9 | 06-20-94 | 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.3 | <0.1 |
| 10 | 06-21-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.2 | <0.1 |
| 11 | 06-21 and 06-22-94 | 20 | 20 | <0.1 | ns | <0.1 | <0.2 | <1. | <0.1 | <0.2 | 0.2 | <0.1 |
| 12 | 06-22-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.3 | <0.1 |
| 13 | 06-23-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.2 | <0.1 |
| 14 | 06-23 and 06-24-94 | 16 | 16 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.1 | 0.1 | <0.1 |
| 15 | 06-26-94 | 15 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | 0.2 | 0.4 | <0.1 |
| 16 | 06-27-94 | ³ 19 | 19 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.2 | 0.4 | <0.1 |
| 18 | 06-28-94 | ⁴ 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.2 | 0.3 | <0.1 |
| 19-1 | 06-29-94 | 23 | 23 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.3 | 0.1 | <0.1 |
| 19-2 | | 22 | 23 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.2 | 0.1 | <0.1 |

the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994

concentrations which were less than the reporting level; concentrations are nanogram per gram of dry weight;

ns, not sampled, and <, less than the reporting limit]

| Pool duplicate | Perthane | <i>p-p'</i> -DDD | <i>p-p'</i> -DDT | <i>p-p'</i> -Methoxychlor | Mirex | Toxaphene | Gross PCB | Gross PCN | Percent isodrin recovery |
|-----------------|----------|------------------|------------------|---------------------------|-------|-----------|-----------|-----------|--------------------------|
| Ref. 1-1 | <1. | 1.7 | 0.2 | <0.1 | <0.1 | <10. | 92. | <1. | 72 |
| Ref. 2-1 | <1. | 1.0 | <0.1 | <4. | <0.1 | <10. | 130 | <1. | 42 |
| Ref. 2-2 | <1. | 0.9 | <0.1 | <4 | <0.1 | <10. | 113 | <1. | 38 |
| 1 | <1. | 0.5 | <0.1 | <0.2 | <0.1 | <10. | 5. | <1. | 52 |
| 2-1 | <1. | 0.6 | <0.1 | <0.2 | <0.2 | <10. | 12. | <1. | 39 |
| 2-2 | <1. | 2.6 | 0.2 | <0.2 | <0.1 | <10. | 16. | <1. | 70 |
| St. Croix River | <1. | 0.4 | 0.1 | <0.2 | <0.1 | <10. | 6. | <1. | 74 |
| 3 | <1. | 3.8 | 0.2 | <0.2 | <0.1 | <10. | 33. | <1. | 64 |
| ¹ 4 | <3. | 0.9 | <0.3 | <0.5 | <0.3 | <30. | 21. | <3. | 79 |
| ² 4 | <1. | 1. | <0.1 | <0.2 | <0.1 | <10. | 20. | <1. | |
| 5 | <1. | 0.1 | <0.1 | <0.2 | <0.1 | <10. | 4. | <1. | 40 |
| 6 | <1. | 0.3 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 66 |
| 7 | <1. | 1. | 0.1 | <0.2 | <0.1 | <10. | 7. | <1. | 82 |
| 8-1 | <1. | 0.6 | <1.0 | <0.2 | <0.1 | <10. | 4. | <1. | 76 |
| 8-2 | <1. | 0.1 | <0.1 | <0.2 | <0.1 | <10. | 4. | <1. | 82 |
| 9 | <1. | 1. | 0.1 | <0.2 | <0.1 | <10. | 6. | <1. | 71 |
| 10 | <1. | 0.1 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 66 |
| 11 | <1. | 0.4 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 86 |
| 12 | <1. | 0.6 | <0.1 | <0.2 | <0.1 | <10. | 4. | <1. | 77 |
| 13 | <1. | 0.4 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 71 |
| 14 | <1. | 0.2 | <0.1 | <0.2 | <0.1 | <10. | 2. | <1. | 39 |
| 15 | <1. | 0.5 | 1.8 | <0.2 | <0.1 | <10. | 5. | <1. | 40 |
| 16 | <1. | 0.4 | <0.1 | <0.2 | <0.1 | <10. | 10. | <1. | 71 |
| 18 | <1. | 0.6 | <0.1 | <0.2 | <0.1 | <10. | 5. | <1. | 75 |
| 19-1 | <1. | 0.2 | <0.1 | <0.2 | <0.1 | <10. | 2. | <1. | 44 |
| 19-2 | <1. | 0.2 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 22 |

Table 4.2--Concentration of organochlorine compounds on surficial bed sediments collected from based on the Schedule 1325 method,

| Pool duplicate | Date | Number of samples in composite | | Lindane | Hepta-chlor | Aldrin | Hepta-chlor epoxide | Technical chlordane | Endo-sulfan I | Dieldrin | p-p'-DDE | Endrin |
|----------------|----------|--------------------------------|-----------|---------|-------------|--------|---------------------|---------------------|---------------|----------|----------|--------|
| | | 1994 | 1991-1992 | | | | | | | | | |
| 20 | 06-30-94 | ⁵ 12 | 12 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | <0.2 | 0.1 | <0.1 |
| 21 | 07-01-94 | 16 | 19 | <0.1 | <0.1 | <0.1 | <0.1 | 2. | <0.1 | 0.4 | 0.4 | <0.1 |
| 22 | 07-02-94 | 20 | 20 | <0.1 | <0.1 | <0.1 | <0.1 | <1. | <0.1 | 0.3 | 0.1 | <0.1 |
| 24 | 07-03-94 | 18 | 18 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | 0.4 | 0.1 | <0.1 |
| 25 | 07-04-94 | 18 | 19 | <0.1 | <0.1 | <0.1 | <0.1 | 1. | <0.1 | 0.6 | 0.5 | <0.1 |
| 26 | 07-05-94 | 11 | 13 | <0.1 | <0.1 | <0.1 | <0.2 | <2. | <0.1 | 0.7 | 0.5 | <0.1 |

¹Upper Lake Pepin.

²Lower Lake Pepin.

³Eight sites were not resampled in the same locations.

⁴Five sites were not resampled in the same locations.

⁵Two sites were sampled out of the water.

the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River,
June-July 1994--Continued

| Pool duplicate | Perthane | <i>p-p'</i> - DDD | <i>p-p'</i> - DDT | <i>p-p'</i> - Meth- oxychlor | Mirex | Toxaphene | Gross PCB | Gross PCN | Percent isodrin recovery |
|-------------------|----------|----------------------|----------------------|------------------------------------|-------|-----------|-----------|-----------|--------------------------------|
| 20 | <1. | 0.2 | <0.1 | <0.2 | <0.1 | <10. | 1. | <1. | 83 |
| 21 | <1. | 0.8 | 0.3 | <0.2 | <0.1 | <10. | 4. | <1. | 45 |
| 22 | <1. | 0.1 | <0.1 | <0.2 | <0.1 | <10. | 2. | <1. | 46 |
| 24 | <1. | 0.1 | <0.1 | <0.2 | <0.1 | <10. | 2. | <1. | 46 |
| 25 | <1. | 0.5 | <0.1 | <0.2 | <0.1 | <10. | 3. | <1. | 35 |
| 26 | <1. | 1.0 | <0.1 | <0.2 | <0.1 | <10. | 6. | <1. | 46 |

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CHAPTER 5 - Major and Trace Elements

**By David A. Roth, Ronald C. Antweiler, Terry I. Brinton,
and Howard E. Taylor**

ABSTRACT

Bed-sediment cores were collected in the backwater areas of the navigation pools of the Upper Mississippi River. The bed-sediment cores from each pool were composited and subsampled; sediment fraction with diameter of less than 2 millimeters was chemically digested and analyzed for major and trace elements.

Digestion methods include a three-part sequential extraction, for which only the values of the sums are reported, and a total digestion using aqua regia and hydrofluoric acid. Methods of analysis for the major and trace elements were inductively coupled plasma-atomic emission spectrometry for the major elements and high-concentration trace elements, inductively coupled plasma-mass spectrometry for the low-concentration trace elements, and cold vapor-atomic fluorescence spectrometry for mercury. For elements in which the detection limit was similar, the analytical results from the two methods were in good agreement. For 30 samples, the ratio of the concentration of calcium (major element) based on the sequential-extraction method to the concentration based on the total digestion method ranged from 0.75 to 1.61 with a mean and standard deviation of 0.9 ± 0.17 , and the ratio for lead (trace element) ranged from 0.50 to 1.14 with a mean and standard deviation of 0.85 ± 0.19 .

INTRODUCTION

The Mississippi River from Minneapolis, Minn., to St. Louis, Mo., is characterized by a series of 29 locks and dams that make 29 navigation pools, which creates a very different hydrological system compared to the free-flowing Lower Mississippi River and hinders the transport and deposition of major and trace elements. The navigation pools of the Upper Mississippi act as sediment traps. Large proportions of the major and trace elements are associated with these sediments; thus, these elements can be stored in the pools for long periods of time.

Major and trace elements in the Mississippi River come from both natural and anthropogenic sources. Naturally introduced elements are primarily from rock weathering, soil erosion, or the dissolution of water-soluble salts. Other elements are introduced as a result of anthropogenic activities such as mining, sewage outfalls, and industrial discharge. The Upper Mississippi River flows through two major lead-zinc mining districts located along Pools 9, 10, 11, and 12. Numerous industries and several major metropolitan areas are located along this reach of the river: Minneapolis near Pools 1 and 2, Quad Cities area near Pools 15 and 16, and St. Louis, Mo., downstream from Pool 26.

Many of the metallic elements categorized as lighter metals, or those with a specific gravity of less than 5, which include sodium, magnesium, and potassium, are found in the tissue of living organisms and are essential to life. The heavy elements have a specific gravity of greater than 5 and include copper, iron, and lead. Some of these heavy elements in very small amounts are also essential to human life, but in larger amounts are toxic. Several of these elements such as cadmium, lead, and mercury are not needed in any amount, are toxic at extremely low concentrations, and can accumulate in body tissues to toxic levels over long periods of exposure.

PURPOSE AND SCOPE

The purpose of the bed-sediment sampling was to determine the concentrations of major and trace elements in representative samples from each navigation pool. Samples were collected during June and July of 1994, from 24 of the 29 navigation pools between Minneapolis, Minn., and St. Louis, Mo. The results are listed in tables, and the spatial distribution of some elements are shown graphically. Sampling locations are shown in figure 1.1 of this report (Chapter 1).

METHODS

The core collection method and the gravity corer used to collect the bed sediment cores are described in Chapter 1. After the core was collected, the water column above the core in the plastic core cylinder was decanted and the ends capped. The core cylinder was put in plastic whirl-pak bags, then placed in a cooler and frozen no more than 3 hours after collection. The integrity of the vertical layering in the core sample was maintained through all aspects of sample collection and preservation. The cores were shipped to the laboratory frozen and stored, still frozen, until they were subsampled and composited.

Subsampling

Each of the individual cores collected from the same pool were thawed around the edges only and extruded from the core tube. Only the top 2 cm were subsampled by cutting the measured core with a perpendicular cut in order to sample a consistent section of the core. The core was divided longitudinally into two equal sections, one for analysis and the other for archiving. The core sections for each transect were combined and sieved through a 2-mm nylon mesh screen to produce a transect composite sample. The transect composite sample was representatively subsampled through a Jones-type splitter made of Teflon, and the correct amount from each transect was combined proportionally, according to the number of cores collected per transect, producing a pool composite.

Dewatering of the pool composite sample was accomplished by centrifugation at 35,800 times the force of gravity. The resulting paste was mixed by coning (a mixing technique that requires the paste to be folded over on itself by alternating the fold axis by 90 degrees until the sample is homogeneous), and subsampled with Teflon utensils. Two or more subsamples were taken from the pool composite sample and weighed wet. One was used for chemical analysis, and the other was used to determine the percent moisture to obtain a final dry weight for the sample that was used in the chemical analysis.

Sequential Extraction and Total Digestion

The data from a sediment sequential extraction listed in this chapter represent a sum of three different phase extractions of a single sample. The purpose of the first two extractions were to leach the various coatings found on the particles. The third was a total digestion of the leftover residual. Therefore, the final sum of this extraction/digestion process represents a complete digestion of the sediment sample; however, the additional handling involved in this multistep extraction process has the potential to increase the error in the final sum value. A comparison between the sum of the extraction phase concentrations and total digestion concentrations for the Standard Reference Material NIST (National Institute of Technology) no. 2704 Buffalo River is found in table 5.1. Additional information regarding the sequential-extraction method is described by Hayes (1993).

The total digestion was identical to the final step of the extraction procedure. It entailed a one-step aqua-regia/hydrofluoric microwave digestion of the sample. Reagent amounts were adjusted to account for the additional material to be digested because of the absence of previous leaching treatments in this step. The entire procedure is outlined in detail by Hayes (1993).

Table 5.1--Comparison of certified values, total digestion, and the sum of the sequential extraction concentrations for National Institute of Standards and Technology Standard reference material

[Reference material was Standard Reference Material NIST no. 2704 Buffalo River sediment; \pm , the uncertainty represents 1 standard deviation of the analysis of 10 samples for the total digestion and 4 samples for the sum of sequential extraction; NA, data not available]

| Element | Concentration (micrograms of analyte per gram of dry sediment) | | | | | | | | |
|-----------|---|-------|-------|-----------------|-------|--------|------------------------------|-------|--------|
| | Certified value | | | Total digestion | | | Sum of sequential extraction | | |
| Aluminum | 61,000 | \pm | 1,600 | 48,000 | \pm | 3,000 | 44,000 | \pm | 7,000 |
| Barium | 414 | \pm | 12 | 330 | \pm | 30 | 420 | \pm | 80 |
| Cadmium | 3.45 | \pm | 0.22 | 3.9 | \pm | 0.3 | 3.19 | \pm | 0.10 |
| Calcium | 26,000 | \pm | 300 | 25,500 | \pm | 1,100 | 25,700 | \pm | 2,000 |
| Chromium | 135 | \pm | 5 | 130 | \pm | 6.4 | 130 | \pm | 9 |
| Copper | 99 | \pm | 5 | 125 | \pm | 7.5 | 105 | \pm | 7 |
| Iron | 41,100 | \pm | 1,000 | 40,500 | \pm | 900 | 39,200 | \pm | 2,500 |
| Lead | 161 | \pm | 17 | 166 | \pm | 14 | 180 | \pm | 7 |
| Magnesium | 12,000 | \pm | 200 | 6,300 | \pm | 1,400 | 6,700 | \pm | 300 |
| Manganese | 555 | \pm | 19 | 610 | \pm | 10 | 550 | \pm | 40 |
| Mercury | 1.47 | \pm | 0.07 | NA | \pm | NA | 1.52 | \pm | 0.12 |
| Silicon | 291,000 | \pm | 1,300 | 280,000 | \pm | 20,000 | 270,000 | \pm | 10,000 |
| Vanadium | 95 | \pm | 4 | 96 | \pm | 3 | 125 | \pm | 16 |
| Zinc | 438 | \pm | 12 | 440 | \pm | 11 | 420 | \pm | 16 |

Analysis of Bed-Sediment Digestion Extracts

Analytical methods used for the analysis of the extract of the digestion included inductively coupled plasma-atomic emission spectrometry, inductively coupled plasma-mass spectrometry, and cold vapor-atomic fluorescence spectrometry. Elements determined by the inductively coupled plasma-atomic emission spectrometry method (Garbarino and Taylor, 1979) included aluminum, barium, calcium, chromium, iron, magnesium, manganese, silicon (as silica), strontium, vanadium, and zinc. Cadmium, chromium, copper, and lead were determined using an inductively coupled plasma-mass spectrometry method described by Garbarino and Taylor (1993) and Hayes (1993). Mercury was determined using cold vapor-atomic fluorescence spectrometry following the method outlined by Roth (1994).

Accuracy and Precision

Accuracy and precision data for the sum of the sequential extractions and the total digestions (based on the analysis of Standard Reference Material NIST no. 2704 Buffalo River sediment) for selected major and trace elements are in table 5.1. All samples were analyzed in a random fashion, background corrected, and reagent blank subtracted.

To ensure that a mass balance of the extracted elements was obtained during the sequential extraction procedure, elemental concentrations in the total digestion were compared to the concentrations of the sum of the sequential extraction for 15 Mississippi River sediment samples. The sum of the sequential extractions divided by the total digestion concentrations yields a value of 96 to 120 percent for all the elements analyzed with the exception of silicon. The results are listed in table 5.2. In addition, the Standard Reference Material NIST no. 2704 Buffalo River sediment sum of extracted element concentrations were compared to the total digestion concentrations as well as to the certified values. The results, tabulated in table 5.1, show comparisons between values of the total digestion concentrations, sum of sequential extract concentrations, and the certified concentrations

To evaluate the precision of the sequential extraction and total digestion, a Standard Reference Material NIST no. 2704 Buffalo River sediment sample was extracted along with each set of sample extractions or digestions. These reference samples were analyzed in the same manner as the samples and distributed periodically throughout the analysis run sequence. The resulting precision represents the variability associated with the entire process, from subsampling and extracting the sediment to the analysis of the sample digestion extracts. The calculated relative standard deviations for the total digestions are 9.1 percent or less for all elements reported except for magnesium (which is 22 percent). All reported element results from the sums of the sequential digests have relative standard deviations less than 7.9 percent except for vanadium, aluminum, and barium, which are 13, 16, and 19 percent, respectively.

Table 5.2 --Mass balance results of sequential extractions

[Sum is the summation of the concentrations in the hydroxylamine, persulfate, and residual extracts; total is the concentration in the total digestion of the sample; \pm , the uncertainty represents 1 standard deviation of 15 Mississippi River samples; %, percent]

| Element | Sum/Total (%) |
|-----------|---------------|
| Aluminum | 98 \pm 2 |
| Barium | 96 \pm 2 |
| Calcium | 103 \pm 5 |
| Chromium | 107 \pm 6 |
| Copper | 120 \pm 11 |
| Iron | 104 \pm 1 |
| Lead | 112 \pm 3 |
| Magnesium | 99 \pm 1 |
| Manganese | 98 \pm 2 |
| Silicon | 135 \pm 4 |
| Vanadium | 99 \pm 2 |
| Zinc | 115 \pm 10 |

Quality Control and Quality Assurance

In all sampling methods, extreme care was used to minimize possible contamination by using Teflon, high-density polyethylene, and, where necessary, Teflon-coated stainless-steel sample-processing equipment. The use of Teflon or non-talc, polyvinyl chloride gloves was required for all sample-handling and processing procedures. All processing devices used to collect the sample were cleaned with deionized water with a resistivity of 17.0 megohms/cm prior to sampling.

Reference standards were used to monitor the accuracy of the analyses. Multiple analyses of the same samples were used to check analytical precision. The accuracy of the sample data was ensured by analyzing two to three standard reference materials periodically within each set of unknown samples. Reference standards routinely composed about 30 to 50 percent of the suite of samples for analysis, or about two or three in every six. Calibration of the instruments varied, depending on the particular instrument, and the appropriate reference should be consulted for further information. Sample unknowns were reanalyzed whenever the duplicates deviated from one another by an amount that depended on the particular instrument and analyte (see the reference for the applicable method) or when standard reference water samples deviated more than 1.5 standard deviations from the certified value. Quality-control data from the standard reference sediment used in the analysis of the extracts from the sediment digests for metals are listed in table 5.1.

RESULTS

Results for the sum of sequential extractions of surficial bed sediment are listed in table 5.3, and those for the total digestions are in table 5.4. They are the mean of two or more replicate analyses from a single sequential extraction or total digestion. These numbers represent the total amount of analyte found in the sediment sample. The results of the two methods are compared in figure 5.1. When sample concentrations are less than or equal to the detection limit, the results are identified as "less than" values with < preceding the detection limit value. Detection limits were calculated on an individual analysis set basis and were dependent on the dry weight of each individual sample.

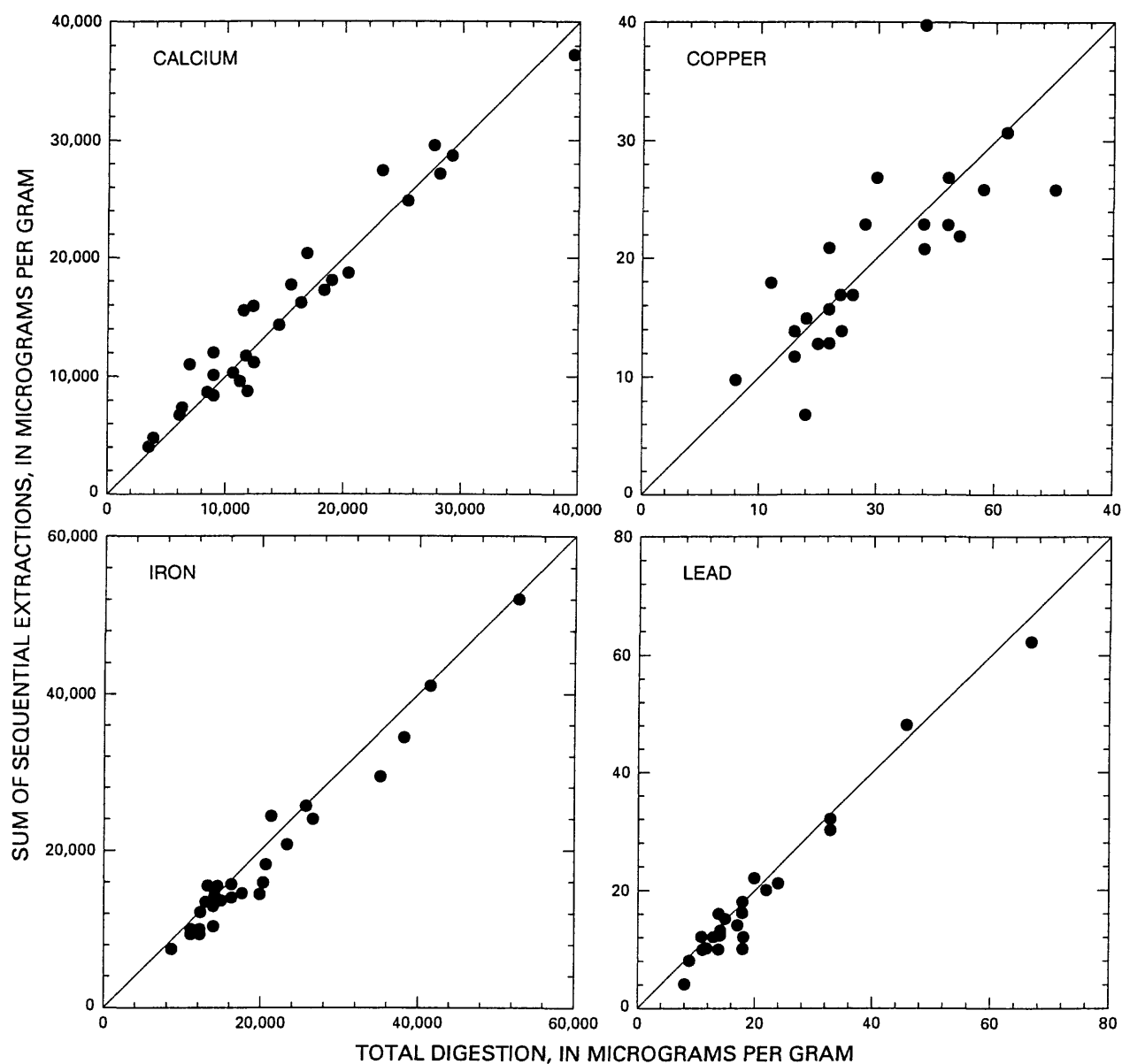


Figure 5.1--Comparison of the sum of sequential extraction with total digestion for calcium, copper, iron, and lead.

Table 5.3 --Concentration of major and trace elements as the sum of sequential extractions of navigation pools of the Upper

[Ref., Lake Pepin reference sample; <, less than the detection limit; units in

| Pool | Date | Aluminum | Barium | Cad-mium | Calcium | Chromium | Copper | Iron |
|----------------|----------|----------|--------|----------|---------|----------|--------|--------|
| Ref. | 05-15-91 | 55,000 | 660 | 3.5 | 29,700 | 110 | 70 | 51,700 |
| 1 | 06-11-94 | 24,000 | 380 | 0.3 | 8,800 | <44 | 18 | 9,100 |
| 2-1 | 06-12-94 | 34,000 | 560 | <0.3 | 27,200 | <44 | 40 | 13,700 |
| 2-2 | 06-12-94 | 33,000 | 540 | <0.3 | 28,700 | <63 | 21 | 14,100 |
| St. Croix R. | 06-13-94 | 34,000 | 490 | <0.3 | 10,100 | 40 | 26 | 28,900 |
| 3 | 06-14-94 | 32,000 | 460 | <0.3 | 27,600 | 50 | 23 | 14,300 |
| ¹ 4 | 06-15-94 | 43,000 | 520 | <0.3 | 24,900 | 70 | 38 | 34,000 |
| ² 4 | 06-15-94 | 39,000 | 480 | 1.2 | 37,300 | 70 | 43 | 40,500 |
| 5 | 06-16-94 | 31,000 | 510 | 0.5 | 15,600 | <61 | 21 | 15,300 |
| 6 | 06-17-94 | 14,000 | 220 | <0.3 | 4,100 | <52 | 7 | 9,800 |
| 7 | 06-18-94 | 27,000 | 530 | 0.4 | 8,600 | 50 | 21 | 13,500 |
| 8-1 | 06-19-94 | 29,000 | 470 | <0.3 | 14,400 | <57 | 17 | 12,600 |
| 8-2 | 06-19-94 | 27,000 | 440 | <0.3 | 11,900 | <49 | 13 | 12,600 |
| 9 | 06-20-94 | 38,000 | 560 | <0.3 | 16,300 | <64 | 23 | 20,400 |
| 10 | 06-21-94 | 28,000 | 450 | <0.3 | 10,400 | 60 | 16 | 15,100 |
| 11 | 06-21-94 | 29,000 | 460 | <0.3 | 17,800 | <50 | 17 | 13,400 |
| 12 | 06-22-94 | 45,000 | 690 | <0.3 | 20,400 | 70 | 27 | 24,100 |
| 13 | 06-23-94 | 33,000 | 580 | 0.4 | 18,700 | 50 | 23 | 14,100 |
| 14 | 06-23-94 | 24,000 | 380 | 0.3 | 8,800 | <58 | 15 | 9,200 |
| 15 | 06-26-94 | 27,000 | 370 | <0.3 | 12,100 | <60 | 13 | 13,100 |
| 16 | 06-27-94 | 26,000 | 450 | <0.3 | 11,300 | <61 | 14 | 10,200 |
| 18 | 06-28-94 | 32,000 | 410 | <0.3 | 16,000 | 50 | 17 | 13,200 |
| 19-1 | 06-29-94 | 40,000 | 590 | <0.3 | 18,200 | 40 | 23 | 17,800 |
| 19-2 | 06-29-94 | 29,000 | 290 | <0.3 | 17,300 | 50 | 26 | 23,500 |
| 20 | 06-30-94 | 24,000 | 510 | <0.3 | 4,900 | <58 | 10 | 7,100 |
| 21 | 07-01-94 | 25,000 | 360 | <0.3 | 7,600 | <93 | 12 | 9,800 |
| 22 | 07-02-94 | 28,000 | 420 | 0.3 | 6,900 | <67 | 14 | 11,900 |
| 24 | 07-03-94 | 35,000 | 520 | <0.3 | 11,100 | <114 | 15 | 15,200 |
| 25-1 | 07-04-94 | 36,000 | 470 | <0.3 | 9,700 | <60 | 22 | 15,500 |
| 25-2 | 07-04-94 | 34,000 | 470 | <0.3 | 8,600 | <70 | 27 | 15,300 |
| 26-2 | 07-05-94 | 47,000 | 640 | <0.3 | 10,400 | 70 | 31 | 25,200 |

¹Upper Lake Pepin.

²Lower Lake Pepin.

surficial bed-sediment samples collected from the downstream one-third of the 25 sampled Mississippi River, June–July 1994

micrograms per gram dry sediment weight]

| Pool | Date | Lead | Magnesium | Manganese | Mercury | Silica | Strontium | Vanadium | Zinc |
|----------------|----------|------|-----------|-----------|---------|---------|-----------|----------|------|
| Ref. | 05-15-91 | 62 | 10,000 | 2,750 | 0.384 | 490,000 | 110 | 156 | 210 |
| 1 | 06-11-94 | 10 | 2,000 | 190 | 0.032 | 620,000 | 140 | 10 | <41 |
| 2-1 | 06-12-94 | 13 | 8,900 | 550 | 0.191 | 560,000 | 170 | 50 | <56 |
| 2-2 | 06-12-94 | 12 | 9,900 | 530 | 0.175 | 540,000 | 160 | 44 | <48 |
| St. Croix R. | 06-13-94 | 21 | 4,400 | 1,240 | 0.100 | 590,000 | 100 | 61 | 60 |
| 3 | 06-14-94 | 12 | 10,300 | 690 | 0.095 | 420,000 | 140 | 49 | <46 |
| ¹ 4 | 06-15-94 | 30 | 6,600 | 1,690 | 0.167 | 480,000 | 130 | 98 | 110 |
| ² 4 | 06-15-94 | 32 | 8,900 | 2,100 | 0.137 | 500,000 | 120 | 135 | 130 |
| 5 | 06-16-94 | 12 | 4,300 | 640 | 0.052 | 550,000 | 100 | 47 | <45 |
| 6 | 06-17-94 | 4 | 1,700 | 240 | 0.017 | 610,000 | 60 | 3 | <39 |
| 7 | 06-18-94 | 10 | 2,500 | 460 | 0.030 | 650,000 | 100 | 36 | <44 |
| 8-1 | 06-19-94 | 11 | 3,800 | 420 | 0.050 | 740,000 | 100 | 5 | <41 |
| 8-2 | 06-19-94 | 10 | 3,800 | 450 | 0.048 | 660,000 | 90 | 25 | <40 |
| 9 | 06-20-94 | 16 | 4,700 | 800 | 0.071 | 560,000 | 120 | 60 | 60 |
| 10 | 06-21-94 | 10 | 4,100 | 560 | 0.046 | 740,000 | 80 | 37 | <62 |
| 11 | 06-21-94 | 12 | 7,800 | 580 | 0.064 | 620,000 | 100 | 109 | <39 |
| 12 | 06-22-94 | 48 | 6,500 | 810 | 0.044 | 750,000 | 150 | 51 | 330 |
| 13 | 06-23-94 | 15 | 6,300 | 580 | 0.027 | 620,000 | 120 | 27 | <49 |
| 14 | 06-23-94 | 10 | 3,000 | 310 | 0.046 | 700,000 | 80 | 6 | <50 |
| 15 | 06-26-94 | 12 | 3,600 | 450 | 0.049 | 620,000 | 90 | 27 | <45 |
| 16 | 06-27-94 | 12 | 4,100 | 350 | 0.089 | 630,000 | 90 | 52 | <46 |
| 18 | 06-28-94 | 12 | 4,300 | 450 | 0.054 | 600,000 | 110 | 33 | <40 |
| 19-1 | 06-29-94 | 18 | 3,900 | 670 | 0.085 | 610,000 | 120 | 66 | 25 |
| 19-2 | 06-29-94 | 20 | 3,000 | 910 | 0.071 | 550,000 | 50 | 49 | 80 |
| 20 | 06-30-94 | 8 | 1,200 | 170 | 0.017 | 640,000 | 160 | 17 | <39 |
| 21 | 07-01-94 | 12 | 2,300 | 310 | 0.056 | 520,000 | 90 | 6 | <66 |
| 22 | 07-02-94 | 10 | 1,900 | 290 | 0.046 | 640,000 | 100 | 14 | <46 |
| 24 | 07-03-94 | 10 | 3,500 | 410 | 0.097 | 590,000 | 110 | 13 | <79 |
| 25-1 | 07-04-94 | 14 | 3,300 | 450 | 0.087 | 540,000 | 110 | 66 | <44 |
| 25-2 | 07-04-94 | 16 | 2,900 | 420 | 0.130 | 590,000 | 100 | 58 | <55 |
| 26 | 07-05-94 | 22 | 3,600 | 900 | 0.042 | 620,000 | 120 | 88 | 50 |

Table 5.4--Concentration of major and trace elements from total digestions of surficial bed-pools of the Upper

[Ref., Lake Pepin reference sample, total mercury concentrations are not listed due to

| Pool | Date | Aluminum | Barium | Cadmium | Calcium | Chromium | Copper | Iron |
|----------------|----------|----------|--------|---------|---------|----------|--------|--------|
| Ref. | 05-15-91 | 47,000 | 530 | 4.1 | 27,600 | 110 | 72 | 52,700 |
| 1 | 06-11-94 | 27,000 | 320 | 0.3 | 11,800 | 20 | 11 | 11,700 |
| 2-1 | 06-12-94 | 35,000 | 460 | 0.7 | 28,000 | 40 | 24 | 16,000 |
| 2-2 | 06-12-94 | 35,000 | 500 | 1.0 | 29,100 | 40 | 24 | 19,500 |
| St. Croix R. | 06-13-94 | 33,000 | 380 | 0.6 | 8,900 | 50 | 29 | 34,900 |
| 3 | 06-14-94 | 30,000 | 390 | 0.8 | 23,200 | 40 | 24 | 17,200 |
| ¹ 4 | 06-15-94 | 42,000 | 450 | 1.3 | 25,300 | 60 | 41 | 37,800 |
| ² 4 | 06-15-94 | 52,000 | 500 | 1.6 | 39,400 | 80 | 53 | 41,600 |
| 5 | 06-16-94 | 22,000 | 330 | 0.4 | 11,500 | 20 | 16 | 14,100 |
| 6 | 06-17-94 | 15,000 | 300 | 0.2 | 3,400 | 10 | 14 | 11,700 |
| 7 | 06-18-94 | 22,000 | 390 | 0.4 | 8,900 | 20 | 16 | 14,400 |
| 8-1 | 06-19-94 | 23,000 | 420 | 0.4 | 14,500 | 26 | 17 | 13,600 |
| 8-2 | 06-19-94 | 21,000 | 400 | 0.3 | 11,600 | 25 | 16 | 13,600 |
| 9 | 06-20-94 | 31,000 | 440 | 0.6 | 16,300 | 60 | 26 | 23,100 |
| 10 | 06-21-94 | 22,000 | 320 | 0.4 | 10,800 | 20 | 16 | 14,300 |
| 11 | 06-21-94 | 21,000 | 380 | 0.3 | 15,500 | 20 | 18 | 14,700 |
| 12 | 06-22-94 | 29,000 | 430 | 1.0 | 16,800 | 50 | 26 | 21,000 |
| 13 | 06-23-94 | 26,000 | 450 | 0.4 | 20,300 | 40 | 19 | 13,800 |
| 14 | 06-23-94 | 25,000 | 340 | 0.1 | 8,600 | 20 | 14 | 10,500 |
| 15 | 06-26-94 | 21,000 | 290 | 0.3 | 8,900 | 20 | 15 | 12,500 |
| 16 | 06-27-94 | 25,000 | 350 | 0.8 | 12,300 | 30 | 17 | 13,500 |
| 18 | 06-28-94 | 25,000 | 400 | 0.4 | 12,300 | 30 | 18 | 13,900 |
| 19-1 | 06-29-94 | 32,000 | 420 | 0.6 | 19,000 | 40 | 24 | 20,300 |
| 19-2 | 06-29-94 | 50,000 | 520 | 0.8 | 18,200 | 50 | 35 | 26,300 |
| 20 | 06-30-94 | 19,000 | 310 | 0.1 | 3,800 | 10 | 8 | 8,200 |
| 21 | 07-01-94 | 22,000 | 290 | 0.3 | 6,200 | 20 | 13 | 10,700 |
| 22 | 07-02-94 | 22,000 | 310 | 0.3 | 6,000 | 30 | 13 | 11,800 |
| 24 | 07-03-94 | 27,000 | 330 | 0.3 | 6,900 | 20 | 14 | 13,000 |
| 25-1 | 07-04-94 | 31,000 | 400 | 0.6 | 11,200 | 40 | 27 | 20,000 |
| 25-2 | 07-04-94 | 29,000 | 330 | 0.5 | 8,200 | 30 | 20 | 16,000 |
| 26 | 07-05-94 | 33,000 | 290 | 0.8 | 8,900 | 60 | 31 | 25,400 |

¹Upper Lake Pepin.

²Lower Lake Pepin.

sediment samples collected from the downstream one-third of the 25 sampled navigation Mississippi River, June-July, 1994

the instability of mercury in the digested sample; units in micrograms per gram dry sediment weight]

| Pool | Date | Lead | Magnesium | Manganese | Silica | Strontium | Vanadium | Zinc |
|----------------|----------|------|-----------|-----------|---------|-----------|----------|------|
| Ref. | 05-15-91 | 67 | 4,600 | 2,910 | 510,000 | 110 | 132 | 210 |
| 1 | 06-11-94 | 12 | 2,700 | 280 | 810,000 | 150 | 30 | 24 |
| 2-1 | 06-12-94 | 14 | 8,700 | 740 | 700,000 | 170 | 56 | 48 |
| 2-2 | 06-12-94 | 18 | 10,000 | 760 | 670,000 | 170 | 56 | 55 |
| St. Croix R. | 06-13-94 | 24 | 2,300 | 1,520 | 770,000 | 100 | 66 | 69 |
| 3 | 06-14-94 | 18 | 6,300 | 730 | 740,000 | 150 | 52 | 52 |
| ¹ 4 | 06-15-94 | 33 | 5,600 | 2,050 | 570,000 | 110 | 104 | 140 |
| ² 4 | 06-15-94 | 33 | 1,600 | 2,400 | 590,000 | 140 | 124 | 150 |
| 5 | 06-16-94 | 11 | 1,600 | 590 | 740,000 | 90 | 34 | 38 |
| 6 | 06-17-94 | 8 | 900 | 360 | 820,000 | 60 | 28 | 14 |
| 7 | 06-18-94 | 11 | 700 | 540 | 740,000 | 90 | 34 | 30 |
| 8-1 | 06-19-94 | 11 | 2,500 | 500 | 790,000 | 100 | 35 | 25 |
| 8-2 | 06-19-94 | 18 | 1,600 | 530 | 740,000 | 90 | 32 | 31 |
| 9 | 06-20-94 | 18 | 1,100 | 1,000 | 660,000 | 120 | 58 | 65 |
| 10 | 06-21-94 | 11 | 1,600 | 550 | 810,000 | 80 | 40 | 37 |
| 11 | 06-21-94 | 14 | 2,600 | 630 | 730,000 | 90 | 37 | 47 |
| 12 | 06-22-94 | 46 | 1,400 | 780 | 670,000 | 120 | 54 | 280 |
| 13 | 06-23-94 | 15 | 2,800 | 610 | 770,000 | 120 | 39 | 48 |
| 14 | 06-23-94 | 11 | 2,500 | 450 | 840,000 | 90 | 32 | 39 |
| 15 | 06-26-94 | 13 | 1,300 | 490 | 700,000 | 90 | 30 | 46 |
| 16 | 06-27-94 | 14 | 1,800 | 510 | 790,000 | 100 | 39 | 42 |
| 18 | 06-28-94 | 14 | 1,300 | 490 | 740,000 | 120 | 38 | 48 |
| 19-1 | 06-29-94 | 18 | 1,100 | 780 | 710,000 | 110 | 55 | 66 |
| 19-2 | 06-29-94 | 22 | 4,800 | 1,030 | 730,000 | 110 | 82 | 100 |
| 20 | 06-30-94 | 9 | 900 | 250 | 690,000 | 90 | 16 | 13 |
| 21 | 07-01-94 | 14 | 800 | 360 | 790,000 | 90 | 31 | 31 |
| 22 | 07-02-94 | 12 | 700 | 330 | 720,000 | 80 | 31 | 31 |
| 24 | 07-03-94 | 14 | 800 | 360 | 830,000 | 90 | 35 | 38 |
| 25-1 | 07-04-94 | 17 | 1,000 | 650 | 740,000 | 90 | 58 | 53 |
| 25-2 | 07-04-94 | 14 | 800 | 440 | 820,000 | 100 | 46 | 41 |
| 26 | 07-05-94 | 20 | 800 | 880 | 700,000 | 70 | 78 | 62 |

SUMMARY

The bed-sediment data listed in this report represents a complete digestion of the <2-mm fraction of surficial bed sediment. These samples were composited from a number of individual cores collected from the downstream one-third of the 25 sampled navigation pools on the Upper Mississippi River. For 30 samples, the ratio of the concentration of calcium (major element) based on the sequential-extraction method to the concentration based on the total digestion method ranged from 0.75 to 1.61 with a mean and standard deviation of 0.9 ± 0.17 , and the ratio for lead (trace element) ranged from 0.50 to 1.14 with a mean and standard deviation of 0.85 ± 0.19 . Results summarizing the spatial distribution of calcium, lead, mercury, and strontium as sums of sequential extraction in the bed sediments of the Upper Mississippi River pools are shown in figures 5.2 to 5.5. The concentration of samples that were sequentially extracted and summed is compared to the concentration of samples that were totally digested in a single step in figure 5.1.

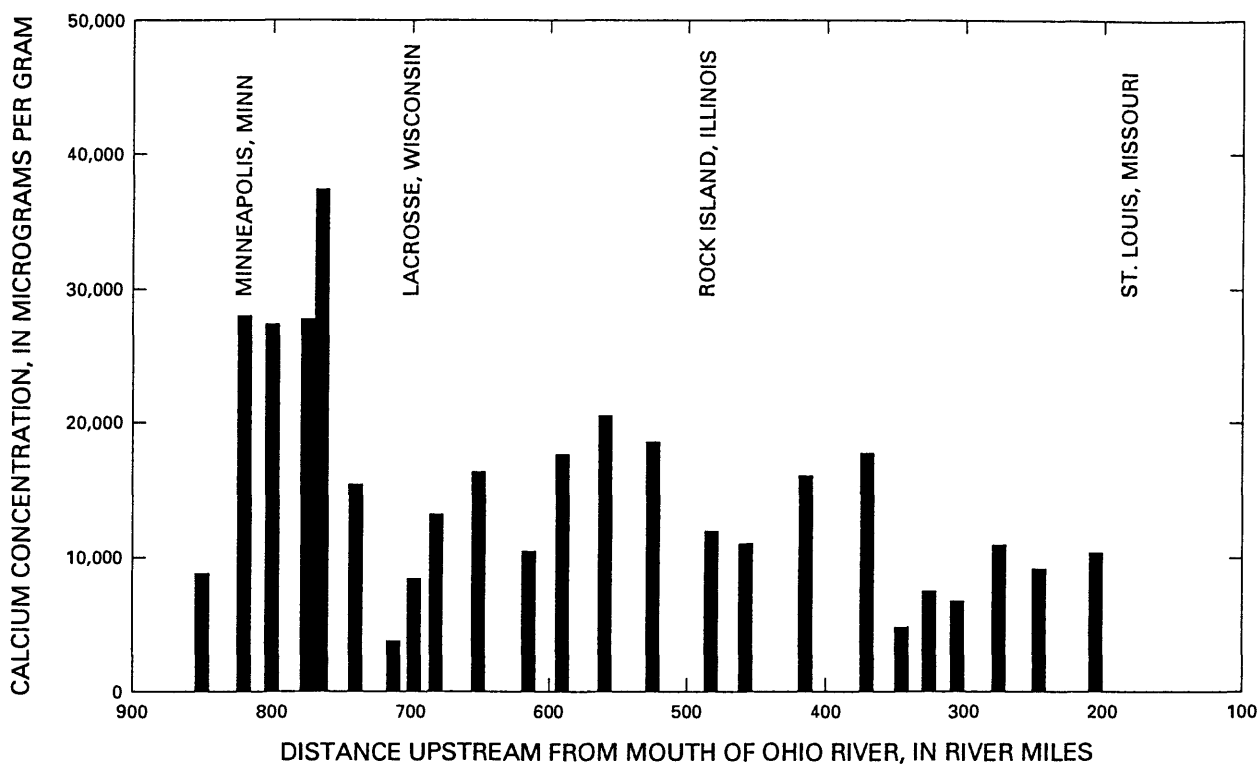


Figure 5.2--Concentration of calcium (sum of sequential extractions) in the surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

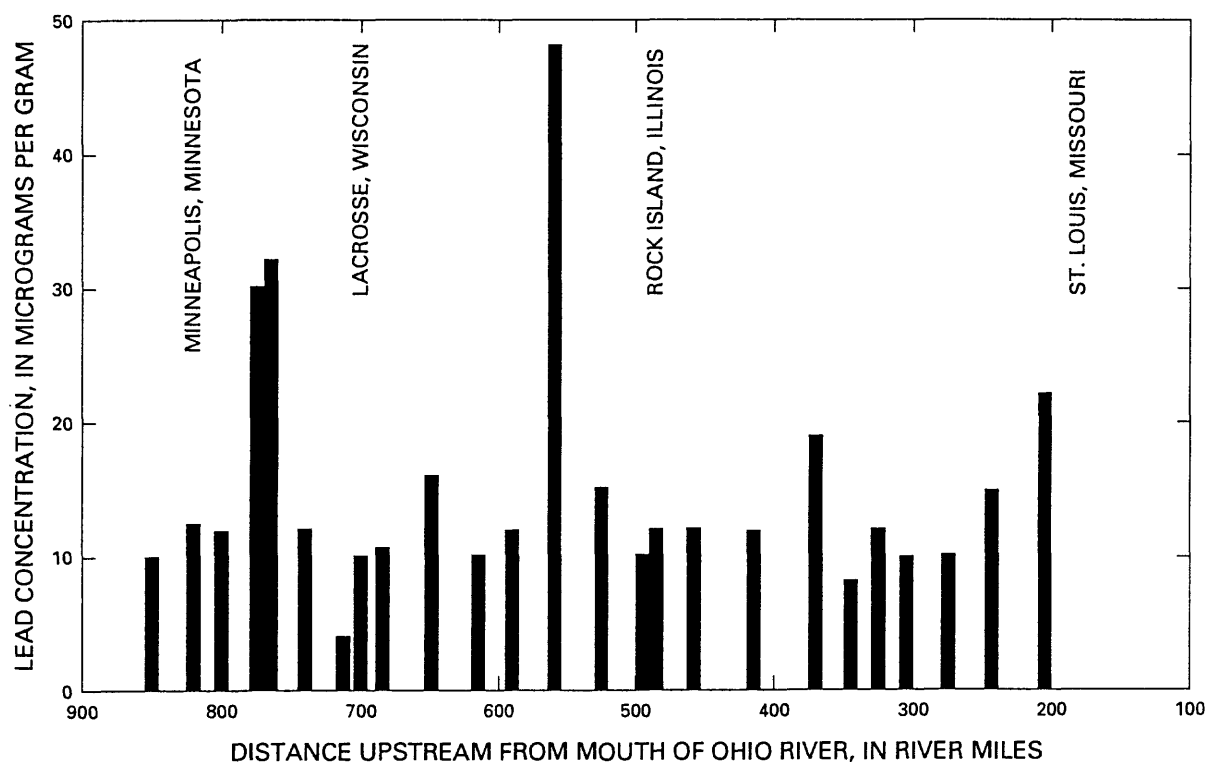


Figure 5.3--Concentration of lead (sum of sequential extractions) in the surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

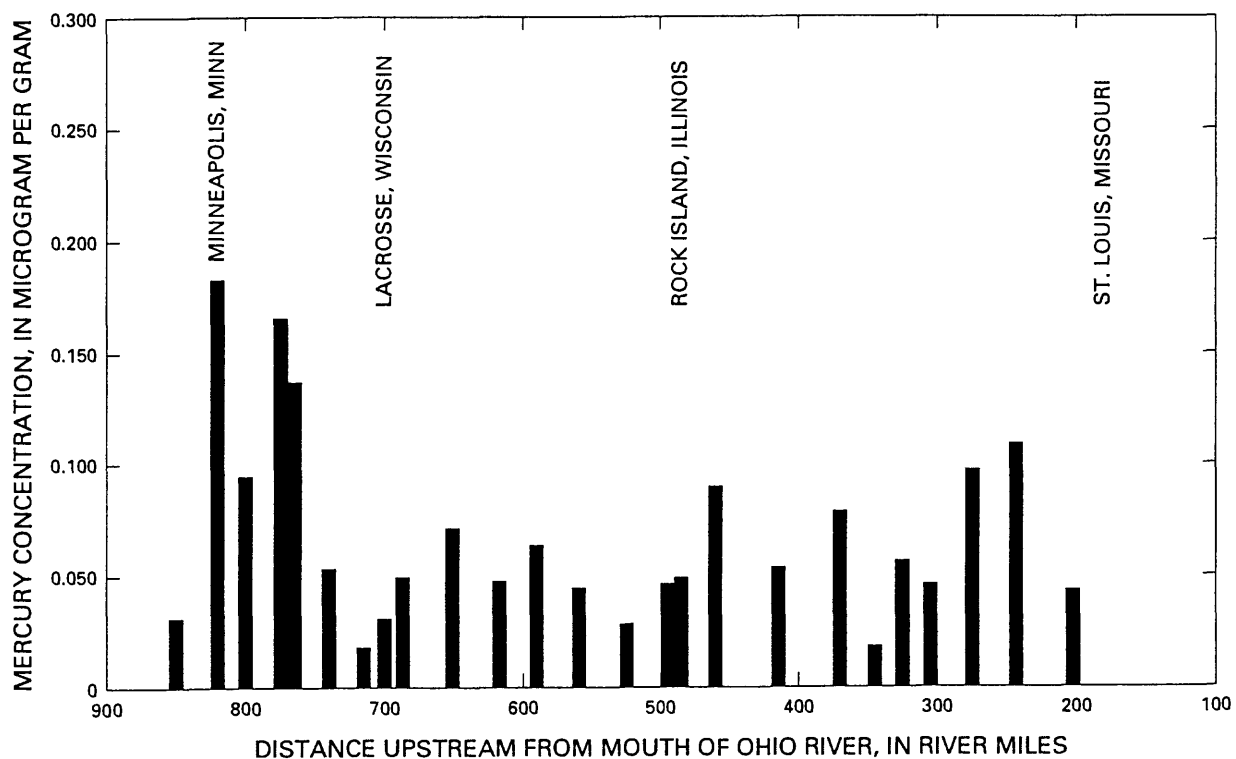


Figure 5.4--Concentration of mercury (sum of sequential extractions) in the surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

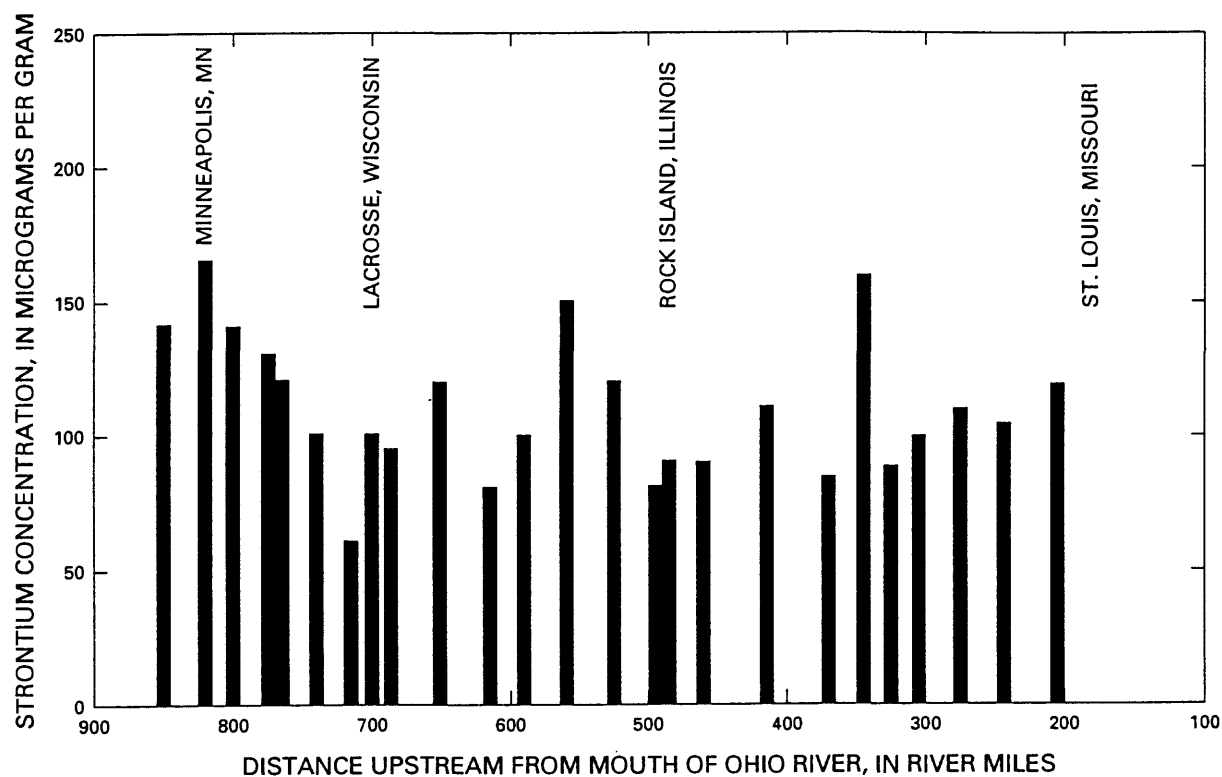


Figure 5.5--Concentration of strontium (sum of sequential extractions) in the surficial bed sediments collected from the downstream one-third of the 25 sampled navigation pools of the Upper Mississippi River, June-July 1994. See table 1.2 for location of pools.

REFERENCES

- Garbarino, J.R., and Taylor, H.E., 1979, An inductively coupled plasma-atomic emission spectrometric method for routine water quality testing: *Applied Spectroscopy*, v. 33, p. 220-226.
- Garbarino, J.R., and Taylor, H.E., 1993, Inductively coupled plasma-mass spectrometric method for the determination of dissolved trace elements in water: U.S. Geological Survey Open-File Report 94-358, 92 p.
- Hayes, H.C., 1993, Metal associations in suspended sediments and bed sediments from the Mississippi River: Golden, Colorado School of Mines, Department of Chemistry and Geochemistry, Masters thesis, 131 p.
- Roth, D.A., 1994, Ultratrace analysis of mercury and its distribution in some natural waters in the United States: Fort Collins, Colorado State University, Department of Chemistry, Ph.D. dissertation, 309 p.

Chapter 6 - Sampling-Site Information

By John A. Moody and Deborah A. Martin

ABSTRACT

One purpose of this study was to locate the individual sampling sites so that the sampling could be repeated at a future time. With this in mind, sampling-site information is presented in three ways: (1) a map showing the location of sampling sites in each pool, (2) a vertical profile of each transect in each pool showing the water depth at each sampling site, and (3) a table that lists the latitude and longitude of each sampling site and field data collected at each site.

EXPLANATION

The sampling-site information consists of three parts for each pool:

A map, adapted from U.S. Geological Survey 7.5-minute quadrangle maps, shows the transects and location of each individual sampling site (a solid circle) where a sample was collected and combined to make a composite sample for each pool. The navigation lights and daymarks are shown as open circles and their locations are approximate. Island locations and shapes are approximate because they are constantly changing. The navigation channel is also approximate and is shown as two dashed lines.

A profile of each transect in each pool shows the location of each sampling site and the water depth. Profiles with dashed lines are based on depths measured in 1991 or 1992 (see Moody, 1997).

A table for each transect in a pool lists the sampling sites and field data collected at each site. Each individual sampling site is identified by an identifier under the column labeled "Site." The first two characters are the pool number, the third digit is the transect number, and the last digit (or two digits) is the sample number. Single-digit numbers identify additional sites where only velocity measurements were made. The field data are: latitude and longitude, depth, surface specific conductance, surface-water temperature, dissolved oxygen (Pools 1-11), mean velocity measured at 0.6 of the water depth, the estimated magnetic direction of the velocity, and surficial bed-sediment type. Gage heights are listed in feet for ease of comparison with data published by the U.S. Army Corps of Engineers.

REFERENCES

Moody, J.A., 1997, editor, Hydrologic, sedimentologic, and chemical data describing surficial bed sediments and water in the navigation pools of the Upper Mississippi River, July 1991-April 1992: U.S. Geological Survey Open-File Report 95-708, 276 p.

The following additional abbreviations are used:

BM = benchmark

cm = centimeters

°C = degrees Celsius

ft = foot

GPS = Global Positioning System

m = meters

m/s = meters per second

m³/s = cubic meters per second

LEW = left edge of water

N = North

na = not applicable

NAD27 = North American Datum 1927

NAD83 = North American Datum 1983

rev/s = revolutions per second

S = South

SAFL = St. Anthony Falls Lower

SC = St. Croix River

T = Township

TW = Tailwater

UMR = Upper Mississippi River

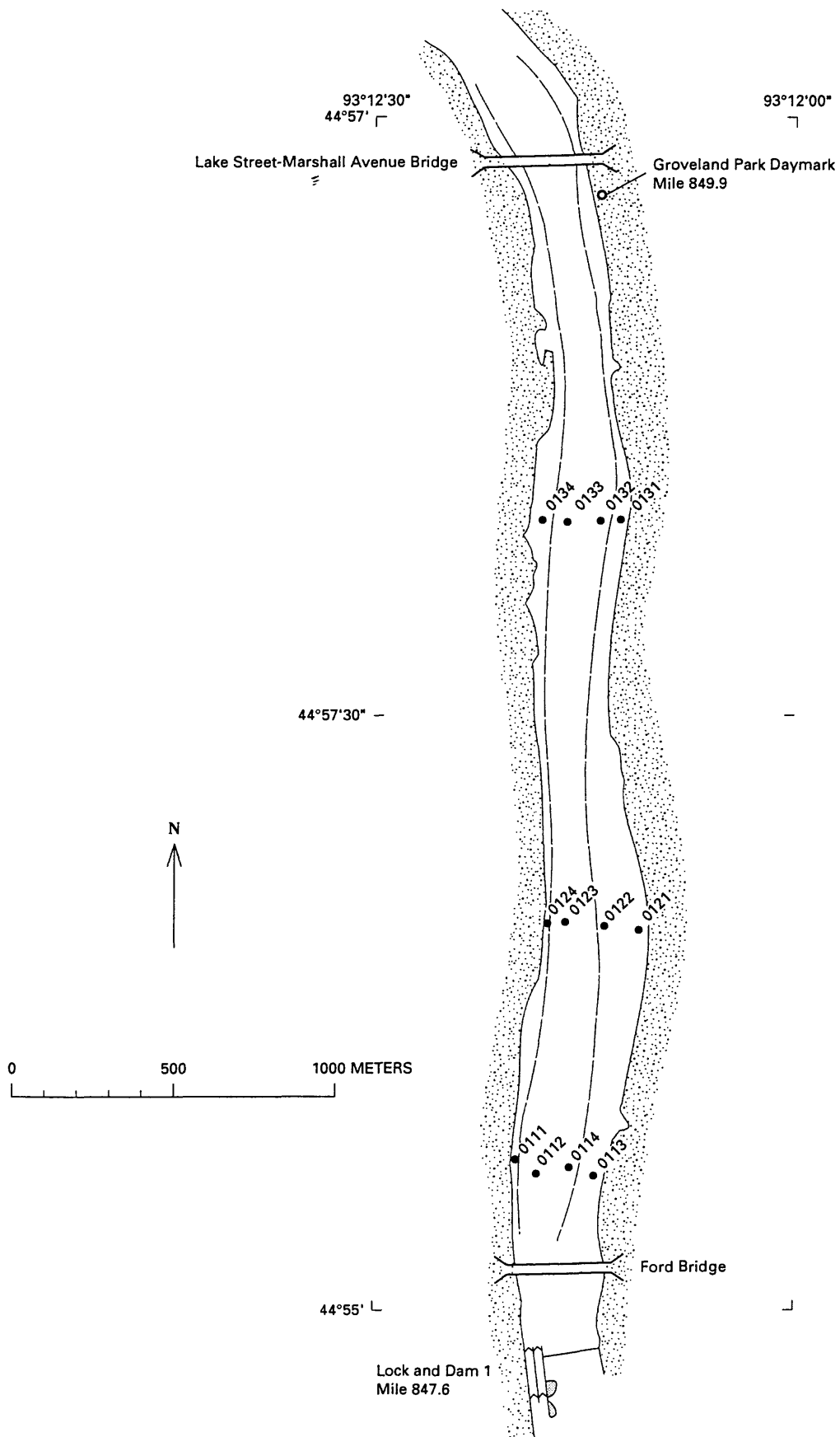
USGS = United States Geological Survey

W = West

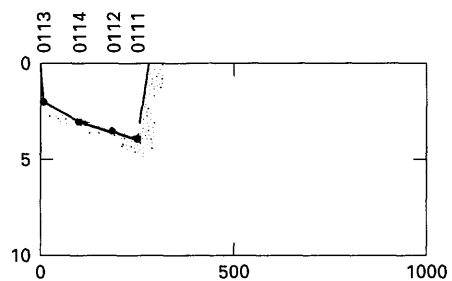
~ = approximate

-- = no measurement taken

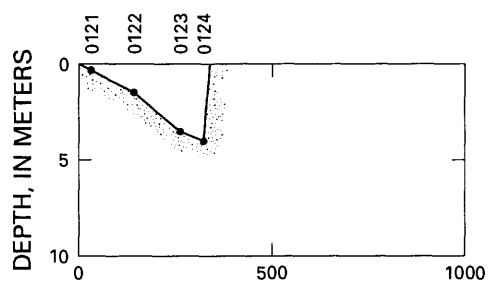
μS/cm - microsiemens per centimeter at 25 degrees Celsius



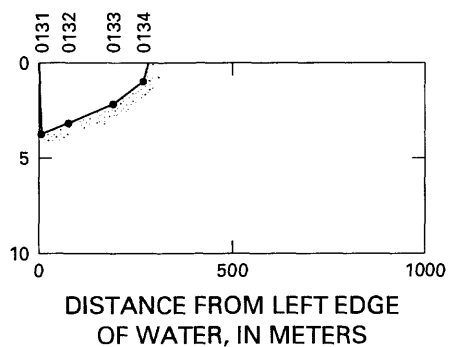
Transect 1 - UMR mile 848.0



Transect 2 - UMR mile 848.5



Transect 3 - UMR mile 849.2



STATION: Mississippi River in Pool 1, Transect 1--UMR mile 848.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at SAFL TW: na

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul West, Minn.

DATE: June 11, 1994

GAGE HEIGHT at Dam 1: 724.25 ft

RIVER SLOPE: na

DATE RATED: 06-25-92

REMARKS:

Resampled sites within ±5 m by using differential GPS. The GPS reference station was at end of center guidewall (44°54.945 N, 093°12.130 W, NAD27, accuracy ±25 m). Velocity was not measured at 0.6 depth but at the surface. Oxygen was measured by using the Yellow Springs Instrument (Model 57). Surface specific conductance and temperature were measured by using a LabComp meter. Biological Resources Division collected a sample from site 0114.

CURRENT METER EQUATION: $V(m/s)=0.666 \cdot rev/s + 0.006$

BEARING OF TRANSECT: 096° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|-----------|------------|--------------|-----------------|------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude | Longitude | | Conduct- | Tem- | | | | |
| | N | W | | ance (μS/cm) | perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0113 | 44°55.221 | 093°11.977 | 2.0 | 399 | 22.4 | 11.2 | -- | -- | sand |
| 0114 | 55.221 | 12.049 | 2.8 | 401 | 21.8 | 10.4 | -- | -- | sand |
| 0112 | 55.211 | 12.117 | 3.3 | 404 | 21.8 | 10.3 | -- | -- | sand |
| 0111 | 44°55.234 | 093°12.160 | 4.0 | 392 | 23.2 | -- | -- | -- | sand |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 1, Transect 2--UMR mile 848.5

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at SAFL TW: na

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul West, Minn.

DATE: June 11, 1994

GAGE HEIGHT at Dam 1: 724.25 ft

RIVER SLOPE: na

DATE RATED: 06-25-92

REMARKS:

Resampled sites within ± 5 m by using differential GPS. The GPS reference station was at end of center guidewall (44°54.945 N, 093°12.130 W, NAD27, accuracy ± 25 m). Velocity was not measured at 0.6 depth but at the surface.

Oxygen was measured by using the Yellow Springs Instrument (Model 57). Surface specific conductance and temperature were measured by using a LabComp meter. New sandbar at old site 0121.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 104° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0121 | 44°55.627 | 093°11.900 | 0.3 | 402 | 22.3 | 10.8 | 0.11 | ~180 | sand |
| 0122 | 55.627 | 11.954 | 1.4 | 404 | 21.8 | 11.0 | 0.29 | ~180 | sand |
| 0123 | 55.626 | 12.032 | 3.7 | 406 | 21.2 | 10.6 | 0.40 | 180 | sand |
| 0124 | 44°55.636 | 093°12.079 | 4.0 | 403 | 21.8 | 11.0 | 0.48 | 170 | sand |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 1, Transect 3--UMR mile 849.2

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at SAFL TW: na

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul West, Minn.

DATE: June 11, 1994

GAGE HEIGHT at Dam 1: 724.25 ft

RIVER SLOPE: na

DATE RATED: 06-25-92

REMARKS:

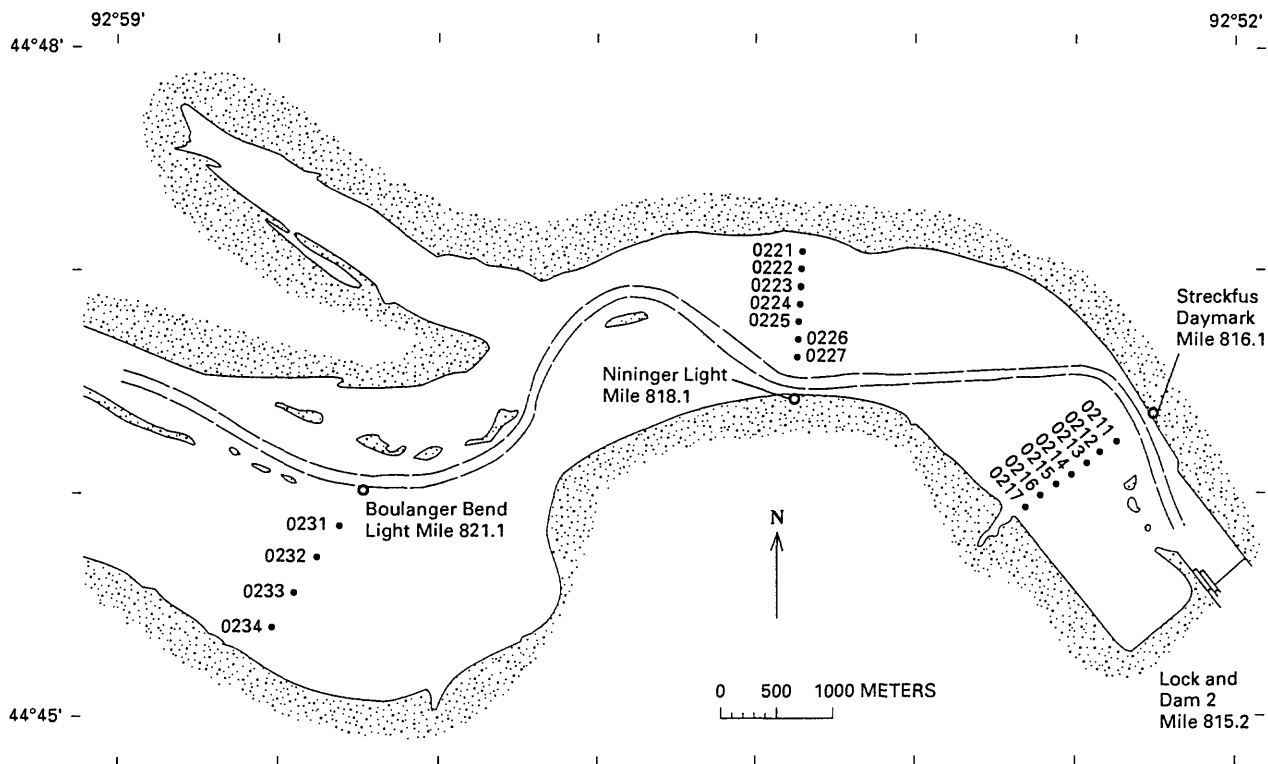
Resampled sites within ± 5 m by using differential GPS. The GPS reference station was at end of center guidewall (44°54.945 N, 093°12.130 W, NAD27, accuracy ± 25 m). Velocity was not measured at 0.6 depth but at the surface.

Oxygen was measured by using the Yellow Springs Instrument (Model 57). Surface specific conductance and temperature were measured by using a LabComp meter.

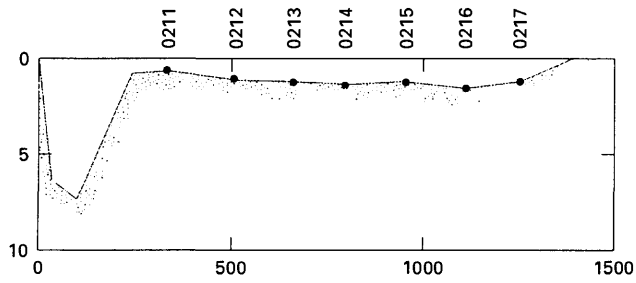
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 100° magnetic

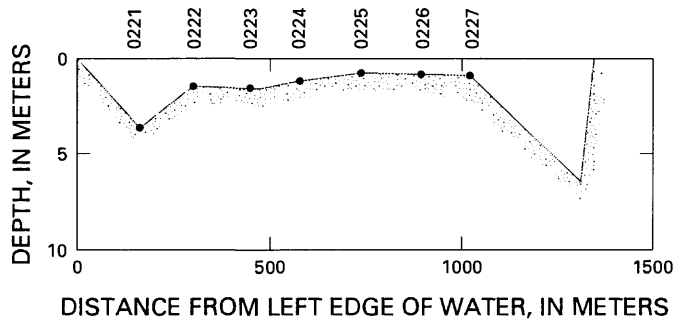
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0131 | 44°56.307 | 093°11.913 | 3.6 | 405 | 21.5 | 10.2 | 0.21 | 160 | sand |
| 0132 | 56.301 | 11.973 | 3.2 | 404 | 21.7 | 10.2 | 0.44 | 150 | sand |
| 0133 | 56.303 | 12.069 | 2.2 | 405 | 22.2 | 10.6 | 0.20 | 190 | sand |
| 0134 | 44°56.315 | 093°12.104 | 1.0 | 404 | 22.7 | 10.5 | 0.11 | -- | mud |
| REW | | | 0.0 | | | | | | |



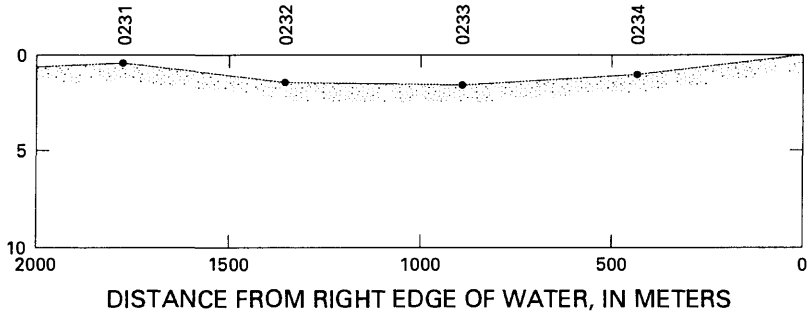
Transect 1 - UMR mile 816.1



Transect 2 - UMR mile 818.1



Transect 3- UMR mile 821.1



STATION: Mississippi River in Pool 2, Transect 1--UMR mile 816.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 690.53 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul Park, Minn.

REMARKS:

Resampled sites within ± 5 m by using differential GPS. The GPS reference station was at a box culvert which drained a pond on the left bank opposite mile 818.1 ($44^{\circ}47.110$ N, $092^{\circ}55.040$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57). Surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $470 \text{ m}^3/\text{s}$ and the discharge at Dam 2 (provided by the U.S. Army Corps of Engineers) was $575 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 035° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 04 | $44^{\circ}46.325$ | $092^{\circ}52.549$ | 6.5 | 674 | 23.0 | 8.0 | 0.20 | 110 | -- |
| 05 | ~ 46.300 | ~ 52.600 | 7.3 | 657 | 23.1 | 8.0 | 0.37 | 130 | -- |
| 06 | 46.281 | 52.646 | 4.6 | 661 | 23.2 | 8.5 | 0.32 | 090 | -- |
| 07 | 46.239 | 52.714 | 0.9 | 652 | 21.7 | 7.5 | 0.15 | 120 | -- |
| 0211 | 46.241 | 52.759 | 0.5 | 656 | 21.7 | 7.5 | 0.13 | 140 | sand |
| 0212 | 46.185 | 52.841 | 1.0 | 654 | 23.1 | 7.5 | 0.18 | 110 | mud |
| 0213 | 46.139 | 52.950 | 1.1 | 648 | 22.9 | 7.8 | 0.15 | 110 | mud |
| 0214 | 46.093 | 53.040 | 1.4 | 645 | 22.7 | 8.0 | 0.13 | 120 | mud |
| 0215 | 46.044 | 53.132 | 1.2 | 657 | 21.9 | 8.0 | 0.15 | 090 | mud |
| 0216 | 45.974 | 53.232 | 1.6 | 656 | 22.2 | 8.0 | 0.19 | 110 | mud |
| 0217 | $44^{\circ}45.931$ | $093^{\circ}53.327$ | 1.2 | 654 | 22.1 | 7.7 | 0.17 | 090 | mud |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 2, Transect 2--UMR mile 818.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 690.53 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul West, Minn.

DATE: June 12, 1994

GAGE HEIGHT at Dam 2: 686.64 ft

RIVER SLOPE: 22.3×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites within ± 5 m by using differential GPS. The GPS reference station was at a box culvert which drained a pond on the left bank opposite mile 818.1 ($44^{\circ}47.110$ N, $092^{\circ}55.040$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $700 \text{ m}^3/\text{s}$ and the discharge at Dam 2 (provided by the U.S. Army Corps of Engineers) was $575 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 000° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0221 | $44^{\circ}47.049$ | $092^{\circ}54.747$ | 3.5 | 660 | 21.4 | 8.0 | 0.30 | 080 | sand |
| 0222 | 46.970 | 54.749 | 1.1 | 665 | 21.5 | 7.6 | 0.15 | 090 | mud |
| 0223 | 46.885 | 54.756 | 1.5 | 659 | 21.5 | 7.8 | 0.21 | 080 | mud |
| 0224 | 46.821 | 54.764 | 1.4 | 660 | 21.5 | 7.7 | 0.20 | 080 | mud |
| 0225 | 46.745 | 54.770 | 1.1 | 661 | 21.5 | 7.8 | 0.20 | 090 | mud |
| 0226 | 46.660 | 54.780 | 0.8 | 661 | 21.9 | 7.9 | 0.14 | 090 | mud |
| 0227 | 46.589 | 54.774 | 1.0 | 661 | 21.8 | 8.0 | 0.23 | 090 | mud |
| 01 | 46.521 | 54.778 | 3.3 | 660 | 22.9 | 8.0 | 0.28 | 100 | -- |
| 02 | 46.456 | 54.772 | 6.0 | 662 | 22.6 | 7.8 | 0.29 | 070 | -- |
| 03 | $44^{\circ}46.413$ | $092^{\circ}54.773$ | 6.5 | 644 | 22.1 | 7.3 | 0.36 | 080 | -- |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 2, Transect 3--UMR mile 821.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 690.53 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is St. Paul West, Minn.

DATE: June 12, 1994

GAGE HEIGHT at Dam 1: 686.64 ft

RIVER SLOPE: 22.3×10^{-6}

DATE RATED: 06-25-92

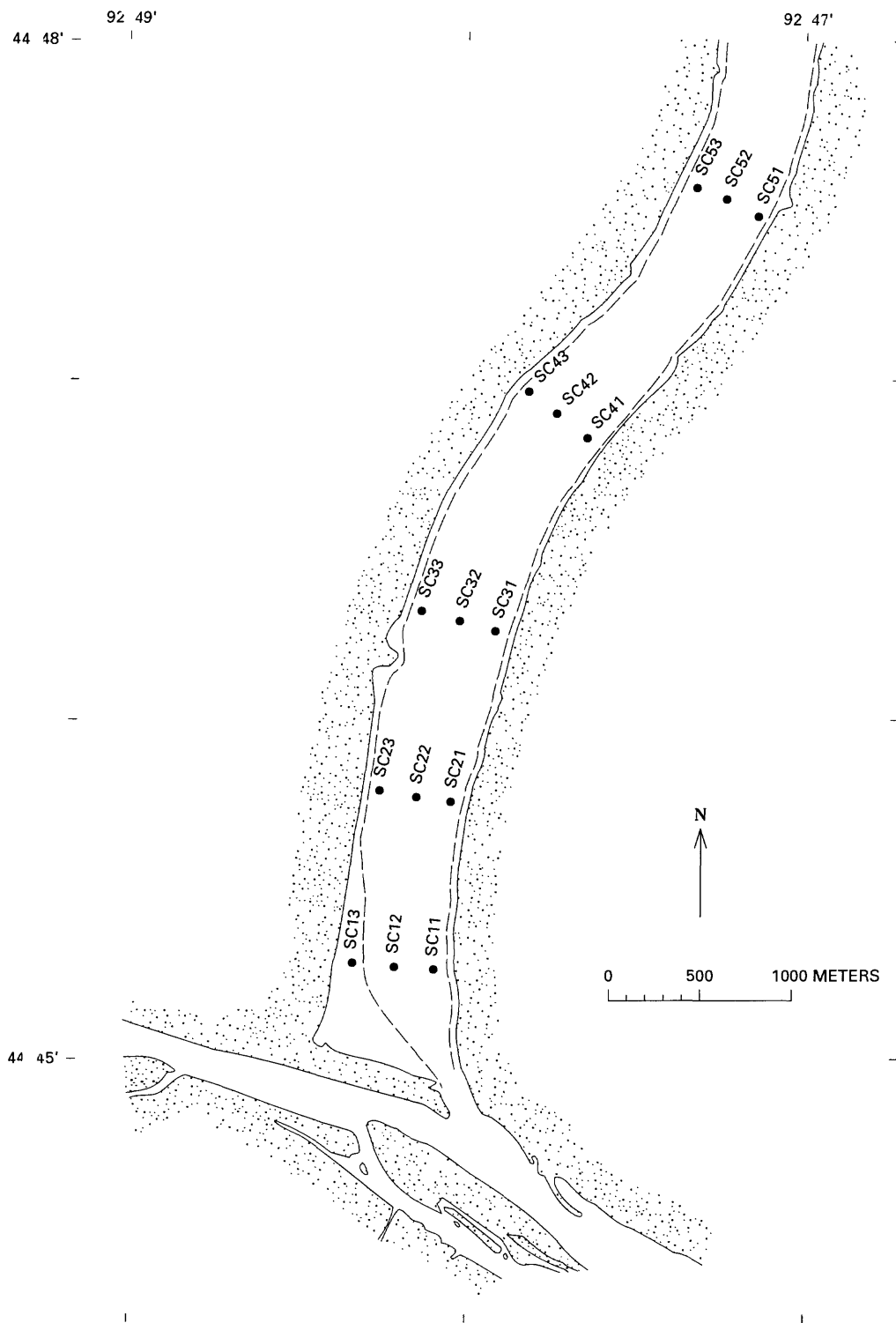
REMARKS:

Resampled sites within ± 5 m by using differential GPS. The GPS reference station was at a box culvert which drained a pond on the left bank opposite mile 818.1 ($44^{\circ}47.110$ N, $092^{\circ}55.040$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Biological Resources Division collected a sample from site 0232.

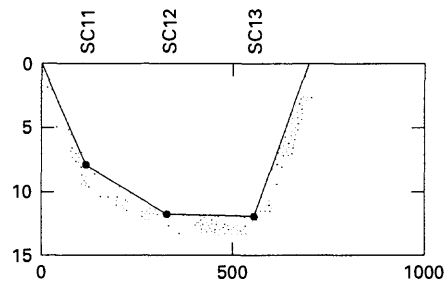
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 019° magnetic

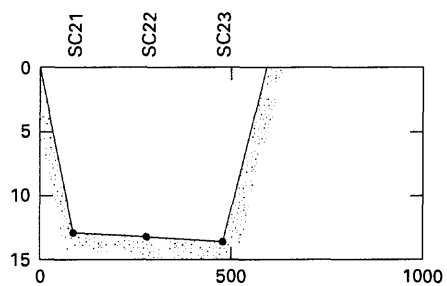
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| 0231 | 44°45.804 | 092°57.699 | 0.6 | 660 | 20.7 | 7.8 | 0.07 | 040 | mud |
| 0232 | 45.662 | 57.820 | 1.4 | 660 | 20.7 | 7.6 | 0.12 | 090 | mud |
| 0233 | 45.511 | 57.947 | 1.4 | 661 | 20.8 | 7.7 | 0.12 | 120 | mud |
| 0234 | 45.350 | 58.096 | 1.3 | 662 | 20.9 | 7.8 | 0.10 | 110 | mud |
| REW | | | 0.0 | | | | | | |



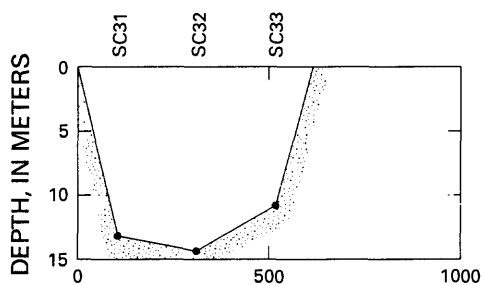
Transect 1 - St. Croix River mile 1.3



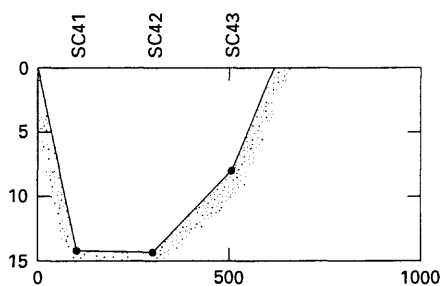
Transect 2 - St. Croix River mile 1.9



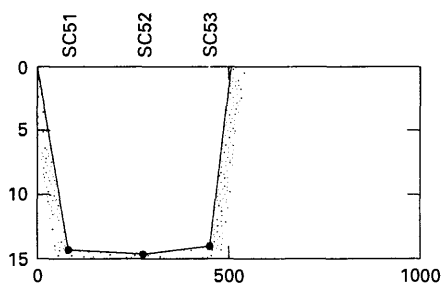
Transect 3 - St. Croix River mile 2.5



Transect 4 - St. Croix River mile 3.3



Transect 5 - St. Croix River mile 4.2



DEPTH, IN METERS

DISTANCE FROM LEFT EDGE
OF WATER, IN METERS

STATION: St. Croix River, Transect 1, St. Croix River mile 1.3

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT: na

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Prescott, Minn.-Wis.

DATE: June 13, 1994

GAGE HEIGHT: na

RIVER SLOPE: na

DATE RATED: na

REMARKS:

Sampled 15 new sites using differential GPS. The GPS reference station was on the right bank just south of a small inlet near the lettering "BR 697" on the quadrangle (1967) (44°46.985 N, 092°48.015 W, NAD 27, accuracy ± 25 m). Oxygen and temperature were measured at three depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Samples were collected from the *ACADIANA* and estimated to be within ± 20 m of the locations listed below, which were recorded when the van Veen grab hit bottom. Site SC11 had lots of pieces of bark on the bottom and no van Veen grab was collected but a core sample was collected.

BEARING OF TRANSECT: 093° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| SC11 | 44°45.278 | 092°48.328 | 8.0 | 189 | 22.7 | 0.1 | 10.1 | 22.0 |
| | | | | | | 4.0 | 9.7 | 21.3 |
| | | | | | | 7.5 | 9.1 | 21.0 |
| SC12 | 45.285 | 48.508 | 11.7 | 187 | 23.4 | 0.1 | 9.9 | 21.9 |
| | | | | | | 6.0 | 9.4 | 21.2 |
| | | | | | | 11.0 | 2.0 | 14.3 |
| SC13 | 44°45.313 | 092°48.698 | 12.0 | 190 | 25.2 | 0.1 | 10.1 | 24.6 |
| | | | | | | 6.0 | 9.1 | 21.2 |
| | | | | | | 11.5 | 1.0 | 14.0 |
| REW | | | 0.0 | | | | | |

STATION: St. Croix River, Transect 2, St. Croix River mile 1.9

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT: na

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Prescott, Minn.-Wis.

DATE: June 13, 1994

GAGE HEIGHT: na

RIVER SLOPE: na

DATE RATED: na

REMARKS:

Sampled 15 new sites using differential GPS. The GPS reference station was on the right bank just south of a small inlet near the lettering "BR 697" on the quadrangle (1967) (44°46.985 N, 092°48.015 W, NAD 27, accuracy ± 25 m). Oxygen and temperature were measured at three depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Samples were collected from the ACADIANA and estimated to be within ± 20 m of the locations listed below, which were recorded when the van Veen grab hit bottom.

BEARING OF TRANSECT: 100° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| SC21 | 44°45.752 | 092°48.272 | 12.9 | 190 | 24.5 | 0.1 | 10.1 | 22.7 |
| | | | | | | 6.5 | 9.2 | 21.0 |
| | | | | | | 12.0 | 1.5 | 14.0 |
| SC22 | 45.770 | 48.401 | 13.2 | 192 | 23.2 | 0.1 | 10.4 | 22.6 |
| | | | | | | 6.5 | 9.2 | 21.0 |
| | | | | | | 12.0 | 2.1 | 13.4 |
| SC23 | 44°45.805 | 092°48.552 | 13.4 | 190 | 23.0 | 0.1 | 10.1 | 22.5 |
| | | | | | | 6.5 | 9.3 | 21.1 |
| | | | | | | 12.0 | 1.2 | 13.2 |
| REW | | | 0.0 | | | | | |

STATION: St. Croix River, Transect 3, St. Croix River mile 2.5

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT: na

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Prescott, Minn.-Wis.

DATE: June 13, 1994

GAGE HEIGHT: na

RIVER SLOPE: na

DATE RATED: na

REMARKS:

Sampled 15 new sites using differential GPS. The GPS reference station was on the right bank just south of a small inlet near the lettering "BR 697" on the quadrangle (1967) (44°46.985 N, 092°48.015 W, NAD 27, accuracy ± 25 m). Oxygen and temperature were measured at three depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Samples were collected from the *ACADIANA* and estimated to be within ± 20 m of the locations listed below, which were recorded when the van Veen grab hit bottom.

BEARING OF TRANSECT: 101° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| SC31 | 44°46.267 | 092°48.083 | 13.3 | 193 | 24.1 | 0.1 | 10.1 | 23.3 |
| | | | | | | 7.0 | 9.0 | 21.0 |
| | | | | | | 12.0 | 2.6 | 14.5 |
| SC32 | 46.288 | 48.245 | 14.4 | 191 | 23.3 | 0.1 | 10.2 | 22.6 |
| | | | | | | 7.0 | 8.7 | 20.8 |
| | | | | | | 12.0 | 3.1 | 14.8 |
| SC33 | 44°46.325 | 092°48.370 | 10.7 | 191 | 23.7 | 0.1 | 10.1 | 23.4 |
| | | | | | | 7.0 | 8.3 | 21.0 |
| REW | | | 0.0 | | | | | |

STATION: St. Croix River, Transect 4, St. Croix River mile 3.3

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT: na

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Prescott, Minn.-Wis.

DATE: June 13, 1994

GAGE HEIGHT: na

RIVER SLOPE: na

DATE RATED: na

REMARKS:

Sampled 15 new sites using differential GPS. The GPS reference station was on the right bank just south of a small inlet near the lettering "BR 697" on the quadrangle (1967) (44°46.985 N, 092°48.015 W, NAD 27, accuracy ±25 m). Oxygen and temperature were measured at three depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Samples were collected from the ACADIANA and estimated to be within ±20 m of the locations listed below, which were recorded when the van Veen grab hit bottom. Biological Resources Division collected a sample from site SC42.

BEARING OF TRANSECT: 123° magnetic

| Site | NAD27 | | Depth (m) | Surface | | | | |
|------|---------------|----------------|--------------|-----------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μS/cm) | Tem- perature (°C) | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
| LEW | | | 0.0 | | | | | |
| SC41 | 44°46.841 | 092°47.694 | 13.9 | 192 | 22.2 | 0.1 | 10.0 | 21.6 |
| | | | | | | 7.0 | 8.5 | 20.7 |
| | | | | | | 12.0 | 4.0 | 16.4 |
| SC42 | 46.880 | 47.816 | 14.2 | 194 | 22.2 | 0.1 | 9.6 | 22.3 |
| | | | | | | 7.0 | 8.0 | 20.4 |
| | | | | | | 12.0 | 3.1 | 14.2 |
| SC43 | 44°46.980 | 092°47.941 | 7.8 | 193 | 23.0 | 0.1 | 9.8 | 23.2 |
| | | | | | | 4.0 | 9.3 | 21.2 |
| | | | | | | 7.5 | 8.5 | 20.5 |
| REW | | | 0.0 | | | | | |

STATION: St. Croix River, Transect 5, St. Croix River mile 4.2

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT: na

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Prescott, Minn.-Wis.

DATE: June 13, 1994

GAGE HEIGHT: na

RIVER SLOPE: na

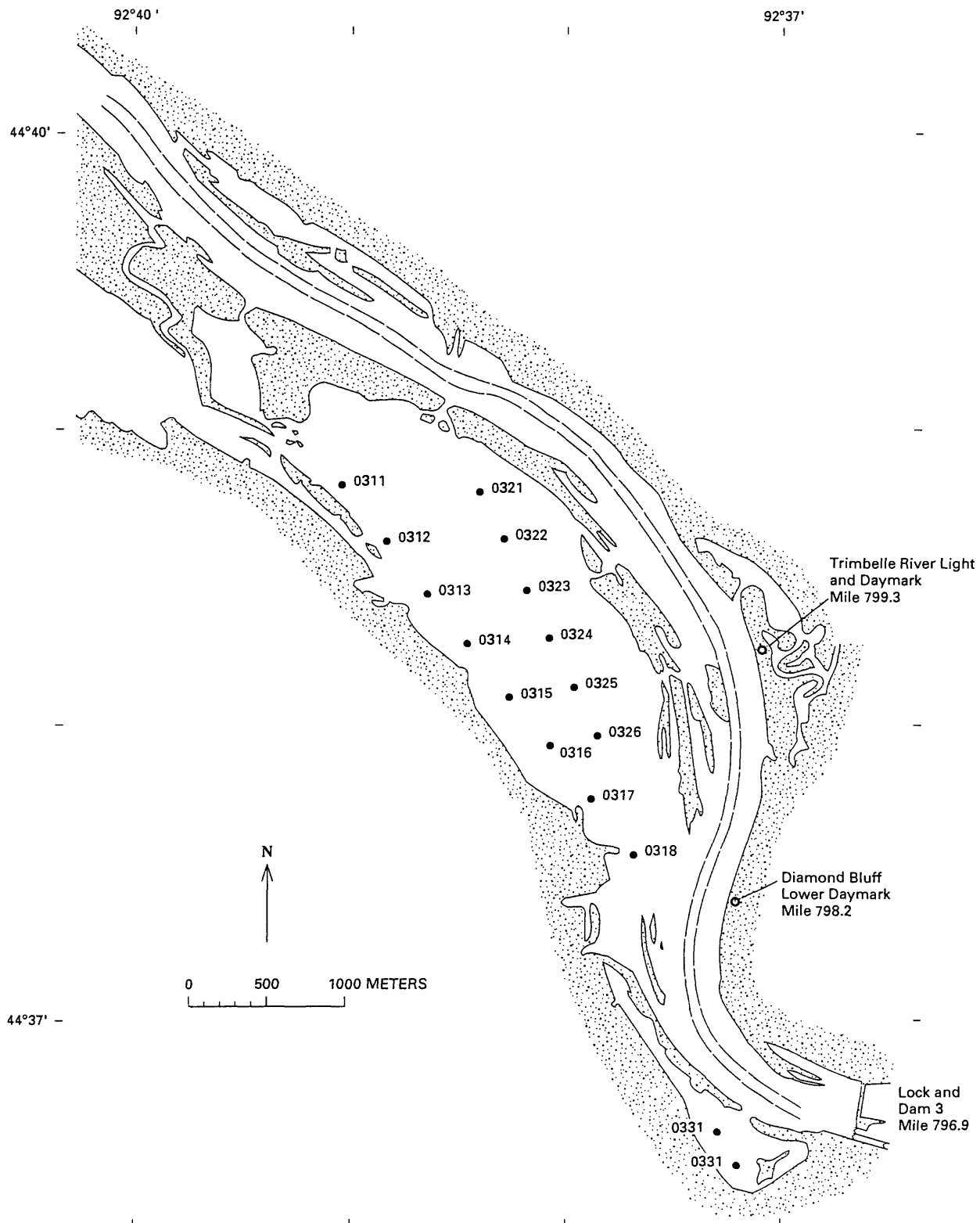
DATE RATED: na

REMARKS:

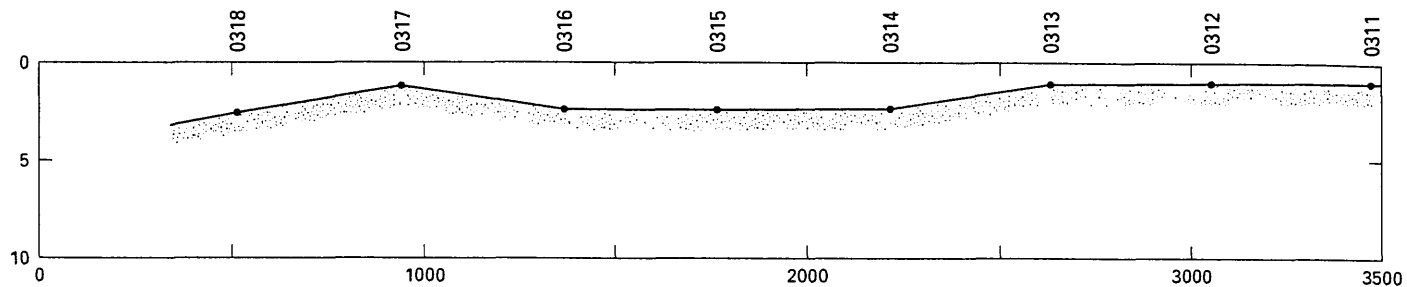
Sampled 15 new sites using differential GPS. The GPS reference station was on the right bank just south of a small inlet near the lettering "BR 697" on the quadrangle (1967) (44°46.985 N, 092°48.015 W, NAD 27, accuracy ± 25 m). Oxygen and temperature were measured at three depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Samples were collected from the ACADIANA and estimated to be within ± 20 m of the locations listed below, which were recorded when the van Veen grab hit bottom.

BEARING OF TRANSECT: 106° magnetic

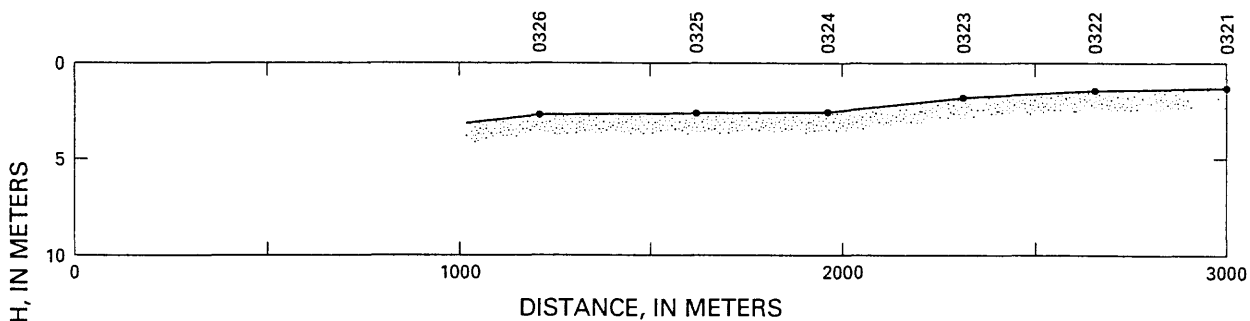
| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Temp- erature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| SC51 | 44°47.486 | 092°46.998 | 14.3 | 195 | 22.3 | 0.1 | 9.5 | 21.8 |
| | | | | | | 7.0 | 7.8 | 20.2 |
| | | | | | | 12.0 | 4.6 | 16.5 |
| SC52 | 47.532 | 47.131 | 14.8 | 192 | 22.1 | 0.1 | 10.0 | 21.5 |
| | | | | | | 7.0 | 7.8 | 20.2 |
| | | | | | | 12.0 | 3.7 | 15.8 |
| SC53 | 44°47.557 | 092°47.255 | 14.0 | 193 | 22.6 | 0.1 | 10.1 | 22.8 |
| | | | | | | 7.0 | 8.4 | 20.6 |
| | | | | | | 12.0 | 3.0 | 14.9 |
| REW | | | 0.0 | | | | | |



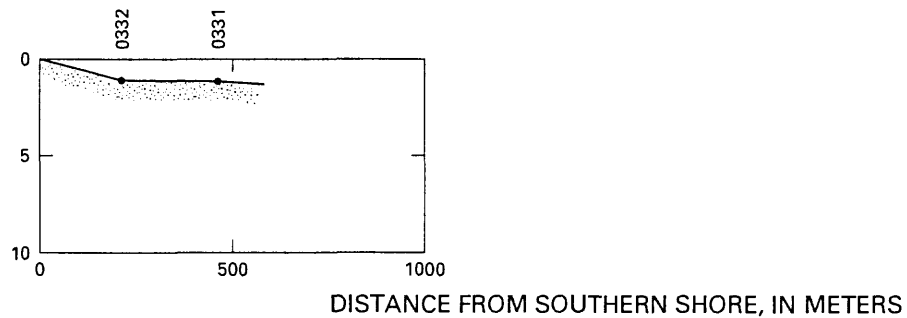
Transect 1 - UMR mile 798.1



Transect 2 - UMR mile 798.1



Transect 3 - UMR mile 797.3



STATION: Mississippi River in Pool 3, Transect 1--UMR mile 798.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 677.30 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Diamond Bluff West, Wis.-Minn.

DATE: June 14, 1994

GAGE HEIGHT at Dam 3: 673.98 ft

RIVER SLOPE: 34.6×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites within ± 5 m by using differential GPS. The error is estimated to be about ± 5 m because of the choppy water conditions. The GPS reference station was located on a small dock at the end of a peninsula extending westward from the longest guidewall for Lock 3 at UMR mile 797.3 (44°36.690 N, 092°37.080 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Location of site 0318 was not recorded at the time the measurements were made so that the target location was used which is within ± 5 m. Discharge at Dam 3 (provided by the U.S. Army Corps of Engineers) was about 650 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 140° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| REW | | | 0.0 | | | | | | |
| 0311 | 44°38.774 | 092°39.052 | 0.8 | 633 | 23.3 | 7.7 | 0.29 | 120 | sand |
| 0312 | 38.602 | 38.856 | 0.6 | 641 | 23.4 | 7.4 | 0.18 | 090 | mud |
| 0313 | 38.425 | 38.652 | 0.8 | 630 | 23.7 | 7.6 | 0.35 | 120 | sand |
| 0314 | 38.270 | 38.475 | 2.0 | ----- no measurements at new marina. ----- | | | | | -- |
| 0315 | 38.079 | 38.254 | 2.2 | 623 | 23.9 | 7.5 | 0.24 | 170 | mud |
| 0316 | 37.913 | 38.065 | 2.3 | 630 | 24.0 | 7.5 | 0.21 | 170 | mud |
| 0317 | 37.736 | 37.862 | 1.0 | 620 | 24.0 | 7.4 | 0.37 | 120 | sand |
| 0318 | 44°37.560 | 092°37.665 | 2.4 | 602 | 25.1 | 7.3 | 0.23 | 180 | -- |

STATION: Mississippi River in Pool 3, Transect 2--UMR mile 798.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 677.30 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Diamond Bluff West, Wis.-Minn.

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m because of the choppy water conditions. The GPS reference station was located on a small dock at the end of a peninsula extending westward from the longest guidewall for Lock 3 at UMR mile 797.3 (44°36.690 N, 092°37.080 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Steep waves were encountered at site 0323. Discharge at Dam 3 (provided by the U.S. Army Corps of Engineers) was about 650 m³/s. Biological Resources Division collected a sample from site 0324.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 153° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| REW | | | 0.0 | | | | | | |
| 0321 | 44°38.783 | 092°38.413 | 1.1 | 630 | 23.3 | 7.0 | 0.15 | 120 | mud |
| 0322 | 38.613 | 38.287 | 1.3 | 633 | 23.1 | 7.4 | 0.34 | 090 | mud |
| 0323 | 38.474 | 38.171 | 1.7 | 650 | 22.6 | 7.6 | 0.31 | -- | mud |
| 0324 | 38.319 | 38.042 | 2.4 | 646 | 22.4 | 7.4 | 0.25 | 170 | mud |
| 0325 | 38.108 | 37.944 | 2.2 | 650 | 22.2 | 7.3 | 0.16 | 160 | mud |
| 0326 | 44°37.974 | 092°37.824 | 2.4 | 644 | 22.1 | 7.2 | 0.18 | 150 | mud |

STATION: Mississippi River in Pool 3, Transect 3--UMR mile 797.3

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 1 TW: 677.30 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Diamond Bluff West, Wis.-Minn.

DATE: June 14, 1994

GAGE HEIGHT at Dam 3: 673.98 ft

RIVER SLOPE: 34.6×10^{-6}

DATE RATED: 06-25-92

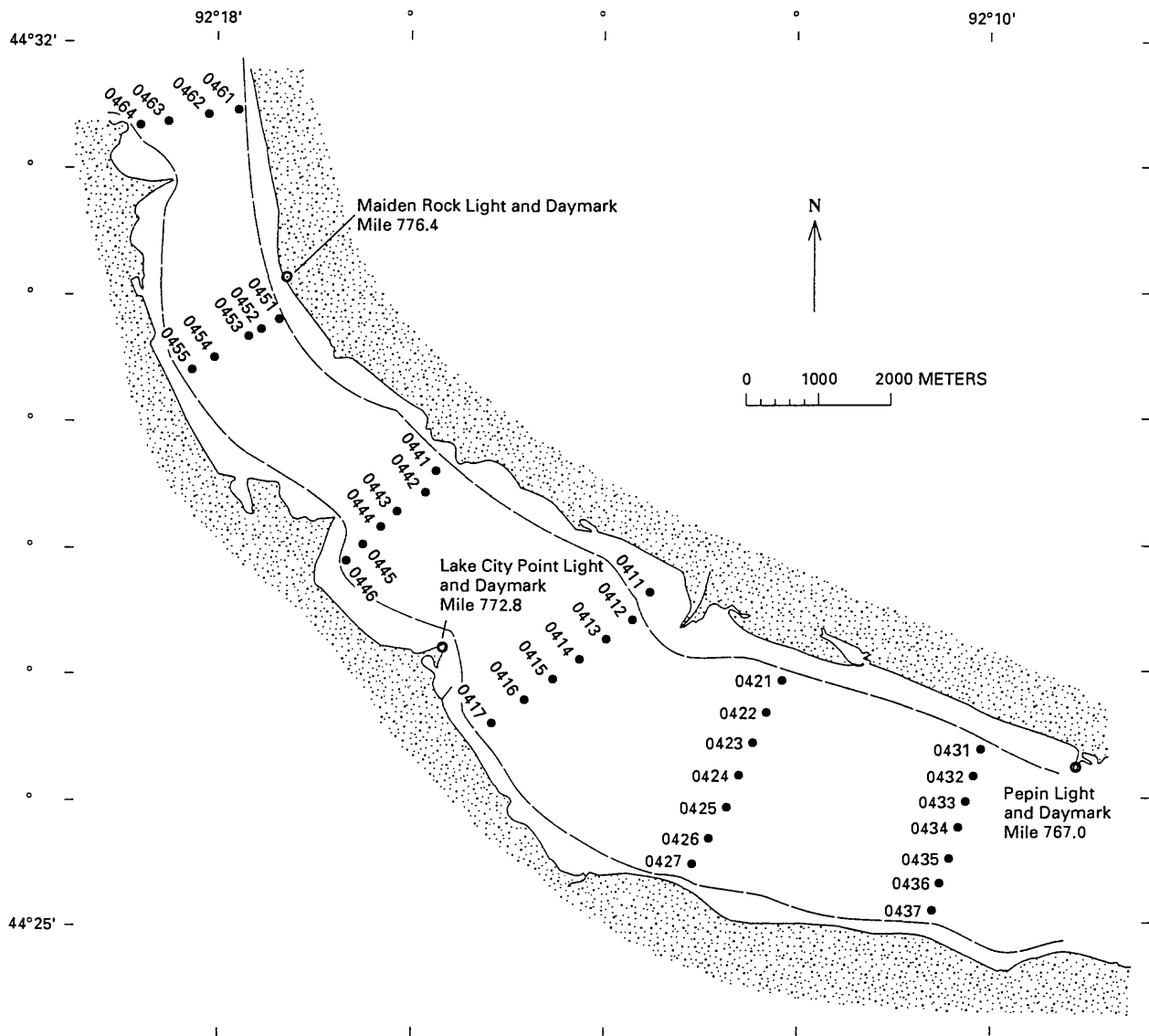
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 3 m. The GPS reference station was located on a small dock at the end of a peninsula extending westward from the longest guidewall for Lock 3 at UMR mile 797.3 ($44^{\circ}36.690$ N, $092^{\circ}37.080$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 3 (provided by the U.S. Army Corps of Engineers) was about $650 \text{ m}^3/\text{s}$.

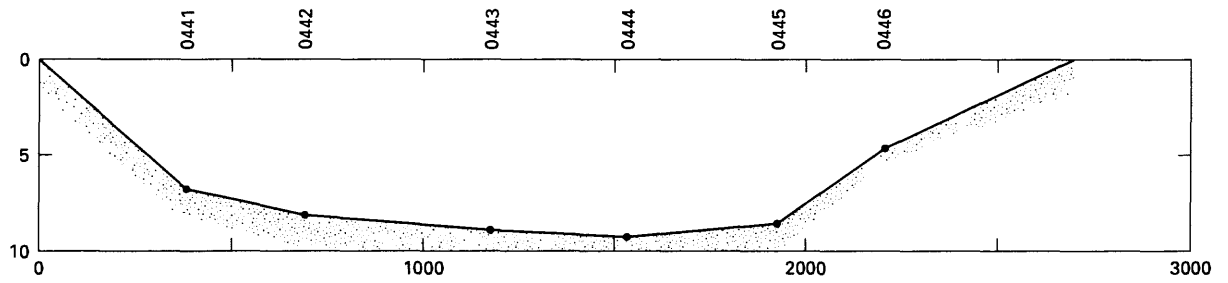
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 148° magnetic

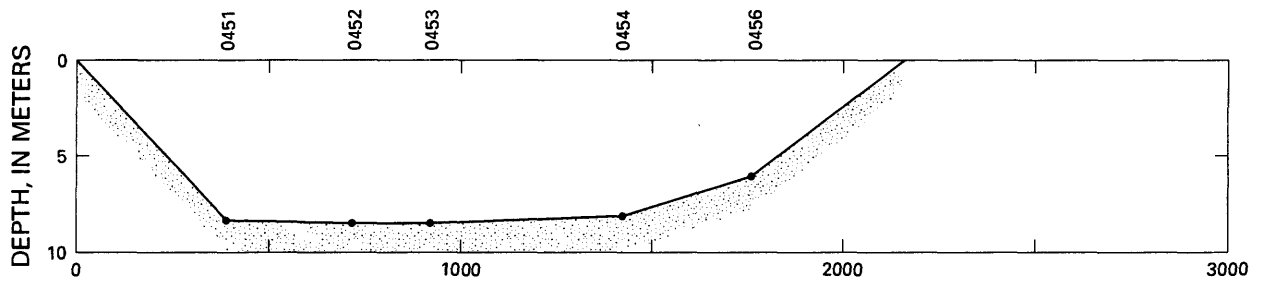
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| 0331 | $44^{\circ}36.631$ | $092^{\circ}37.235$ | 1.0 | 623 | 25.7 | 7.4 | 0.06 | 320 | mud |
| 0332 | $44^{\circ}36.525$ | $092^{\circ}37.158$ | 1.0 | 625 | 25.8 | 7.4 | 0.09 | 270 | mud |
| REW | | | 0.0 | | | | | | |



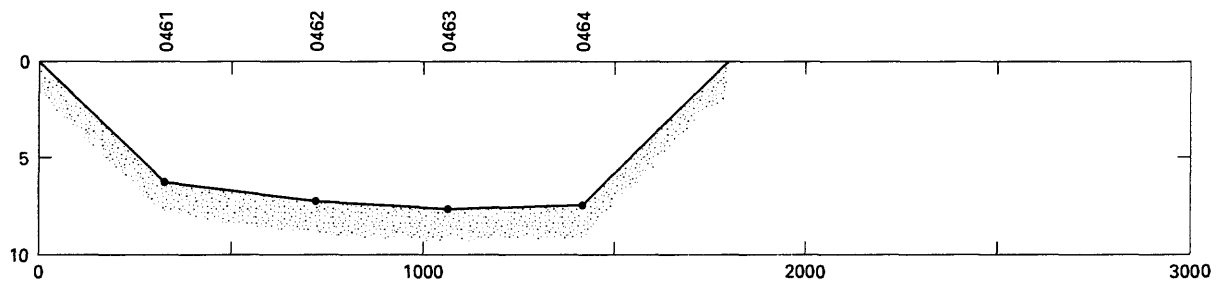
Transect 4 - UMR mile 774.0



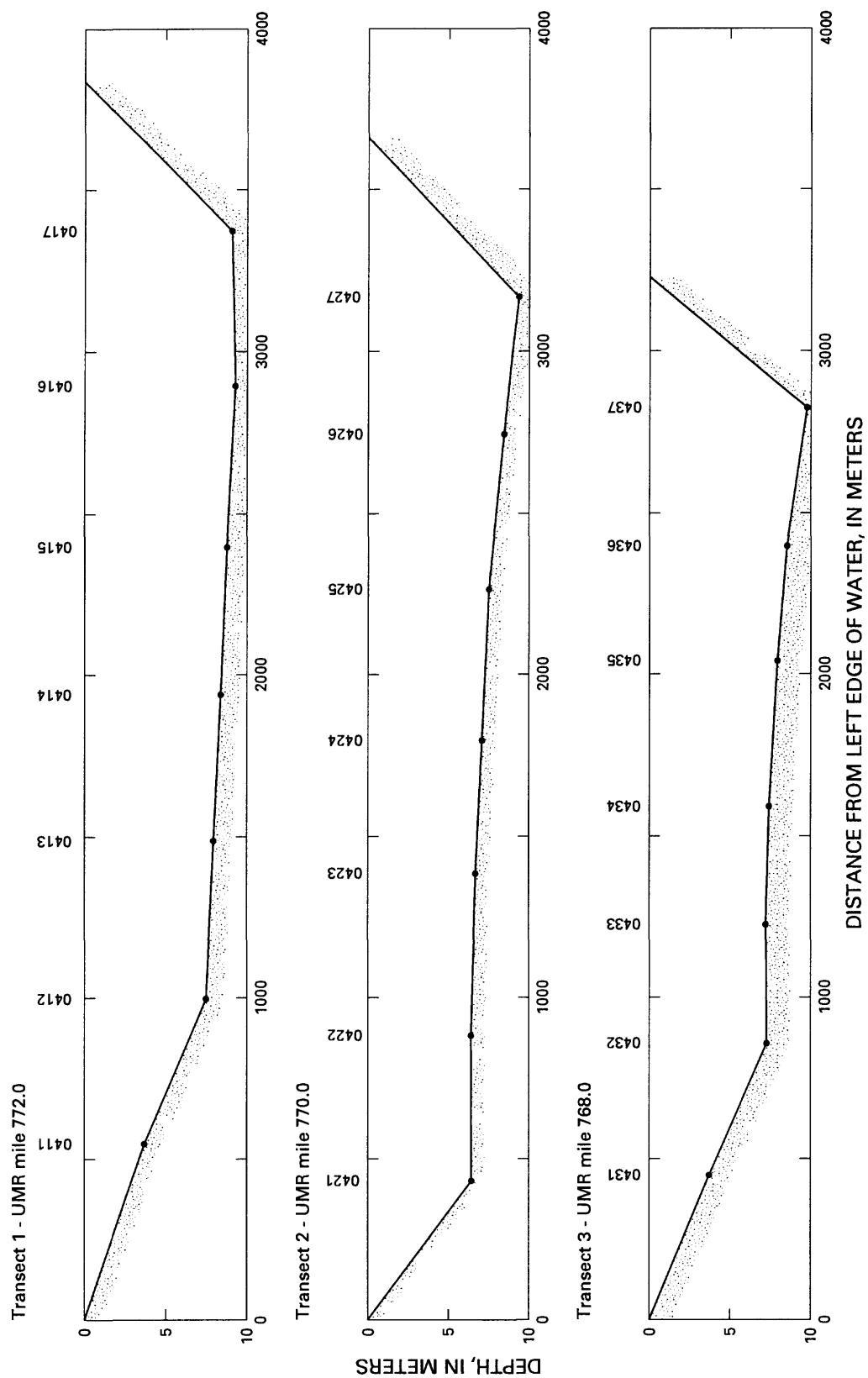
Transect 5 - UMR mile 776.0



Transect 6 - UMR mile 778.0



DISTANCE FROM LEFT EDGE OF WATER, IN METERS



STATION: Mississippi River in Pool 4, Transect 6--UMR mile 778.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Maiden Rock, Wis.-Minn.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

DATE RATED: na

REMARKS:

Resampled four sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 60 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was $1,050 \text{ m}^3/\text{s}$ at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan.

BEARING OF TRANSECT: 084° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|---|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0461 | 44°31.23 | 092°17.82 | 6.7 | 582 | 24.7 | 0.1 | 7.4 | 24.4 |
| | | | | | | 6.0 | 6.2 | 23.8 |
| 0462 | 31.21 | 18.15 | 7.4 | 586 | 24.9 | 0.1 | 7.3 | 24.8 |
| | | | | | | 6.0 | 6.1 | 23.6 |
| 0463 | 31.24 | 18.39 | 7.8 | 588 | 25.1 | 0.1 | 7.0 | 24.7 |
| | | | | | | 7.0 | 3.5 | 23.4 |
| 0464 | 44°31.19 | 092°18.67 | 7.8 | 588 | 24.9 | 0.1 | 6.3 | 24.2 |
| | | | | | | 7.0 | 5.5 | 23.6 |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 4, Transect 5--UMR mile 776.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Lake City, Minn.-Wis.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

DATE RATED: na

REMARKS:

Resampled five sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 70 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was 1,050 m³/s at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan.

BEARING OF TRANSECT: 056° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μS/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0451 | 44°29.74 | 092°17.41 | 8.4 | 576 | 24.8 | 0.1 | 7.2 | 24.2 |
| | | | | | | 7.0 | 4.7 | 23.1 |
| 0452 | 29.62 | 17.60 | 8.4 | 577 | 24.6 | 0.1 | 6.9 | 24.1 |
| | | | | | | 7.5 | 5.7 | 23.1 |
| 0453 | 29.56 | 17.73 | 8.6 | 576 | 24.7 | 0.1 | 6.9 | 24.2 |
| | | | | | | 7.0 | 5.8 | 23.5 |
| 0454 | 29.43 | 18.08 | 8.3 | 578 | 24.6 | 0.1 | 6.8 | 24.0 |
| | | | | | | 7.5 | 6.0 | 23.2 |
| 0455 | 44°29.36 | 092°18.30 | 6.3 | 579 | 24.3 | 0.1 | 6.8 | 23.8 |
| | | | | | | 5.5 | 6.3 | 23.3 |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 4, Transect 4--UMR mile 774.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Lake City, Minn.-Wis.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

DATE RATED: na

REMARKS:

Resampled six sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 80 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. No grab sample was obtained at site 0446 because of sand and shells. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was 1,050 m³/s at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan.

BEARING OF TRANSECT: 041° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0441 | 44°28.56 | 092°15.75 | 6.6 | 570 | 24.5 | 0.1 | 7.0 | 24.3 |
| | | | | | | 5.0 | 6.9 | 24.2 |
| 0442 | 28.42 | 15.83 | 8.1 | 573 | 24.3 | 0.1 | 6.7 | 24.0 |
| | | | | | | 7.5 | 5.6 | 23.0 |
| 0443 | 28.25 | 16.15 | 9.1 | 579 | 23.9 | 0.1 | 6.3 | 23.7 |
| | | | | | | 8.0 | 5.0 | 22.9 |
| 0444 | 28.11 | 16.33 | 9.5 | 580 | 23.8 | 0.1 | 6.1 | 23.3 |
| | | | | | | 8.5 | 5.5 | 23.0 |
| 0445 | 27.95 | 16.58 | 8.8 | 580 | 23.7 | 0.1 | 6.4 | 23.2 |
| | | | | | | 8.0 | 5.8 | 22.8 |
| 0446 | 44°27.88 | 092°16.74 | 4.7 | 578 | 24.1 | 0.1 | 6.3 | 23.2 |
| | | | | | | 4.0 | 5.7 | 22.7 |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 4, Transect 1--UMR mile 772.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: --

MAP: USGS 7.5-minute quadrangle are Lake City, Minn.-Wis., and Pepin, Wis.-Minn.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

DATE RATED: na

REMARKS:

Resampled seven sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 150 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. No grab sample was obtained at site 0446 because of sand and shells. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was $1,050 \text{ m}^3/\text{s}$ at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan.

BEARING OF TRANSECT: 047° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|---|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0411 | 44°27.59 | 092°13.38 | 3.7 | 554 | 24.9 | 0.1 | 8.9 | 23.9 |
| | | | | | | 3.0 | 7.6 | 23.7 |
| 0412 | 27.41 | 13.58 | 7.4 | 568 | 24.5 | 0.1 | 6.8 | 23.7 |
| | | | | | | 7.0 | 6.7 | 23.3 |
| 0413 | 27.24 | 13.98 | 8.0 | 570 | 24.3 | 0.1 | 6.5 | 23.1 |
| | | | | | | 7.0 | 6.0 | 23.1 |
| 0414 | 27.11 | 14.24 | 8.3 | 577 | 24.0 | 0.1 | 7.2 | 23.8 |
| | | | | | | 7.0 | 6.2 | 22.8 |
| 0415 | 26.94 | 14.42 | 8.8 | 579 | 24.1 | 0.1 | 7.1 | 23.8 |
| | | | | | | 8.0 | 5.6 | 22.7 |
| 0416 | 26.79 | 14.78 | 9.3 | 580 | 24.1 | 0.1 | 7.2 | 23.7 |
| | | | | | | 9.0 | 5.8 | 22.7 |
| 0417 | 44°26.63 | 092°15.11 | 9.0 | 581 | 24.1 | 0.1 | 6.9 | 23.5 |
| | | | | | | 8.5 | 6.1 | 22.8 |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 4, Transect 2--UMR mile 770.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Pepin, Wis.-Minn.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

DATE RATED: na

REMARKS:

Resampled seven sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 110 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was 1,050 m³/s at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan.

BEARING OF TRANSECT: 021° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μS/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0421 | 44°26.89 | 092°12.03 | 6.6 | 552 | 24.1 | 0.1 | 7.7 | 24.0 |
| | | | | | | 5.0 | 6.7 | 23.0 |
| 0422 | 26.68 | 12.18 | 7.6 | 564 | 23.7 | 0.1 | 7.3 | 23.2 |
| | | | | | | 7.0 | 6.2 | 22.8 |
| 0423 | 26.47 | 12.32 | 7.7 | 569 | 23.5 | 0.1 | 6.9 | 23.1 |
| | | | | | | 7.0 | 6.2 | 22.7 |
| 0424 | 26.22 | 12.46 | 8.2 | 572 | 23.5 | 0.1 | 6.6 | 23.1 |
| | | | | | | 7.5 | 6.4 | -- |
| 0425 | 25.95 | 12.59 | 8.4 | 579 | 23.7 | 0.1 | 6.6 | 23.1 |
| | | | | | | 7.0 | 6.2 | 22.8 |
| 0426 | 25.78 | 12.73 | 8.9 | 578 | 23.9 | 0.1 | 6.5 | 23.3 |
| | | | | | | 8.0 | 5.6 | 22.7 |
| 0427 | 44°25.52 | 092°12.95 | 9.6 | 577 | 24.2 | 0.1 | 6.7 | 23.2 |
| | | | | | | 8.0 | 5.8 | 22.7 |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 4, Transect 3--UMR mile 768.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 3 TW: 670.4 ft

SUSPENSION: no velocity measurements

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Pepin, Wis.-Minn.

DATE: June 15, 1994

GAGE HEIGHT at Dam 4: 666.87 ft

RIVER SLOPE: 15.2×10^{-6}

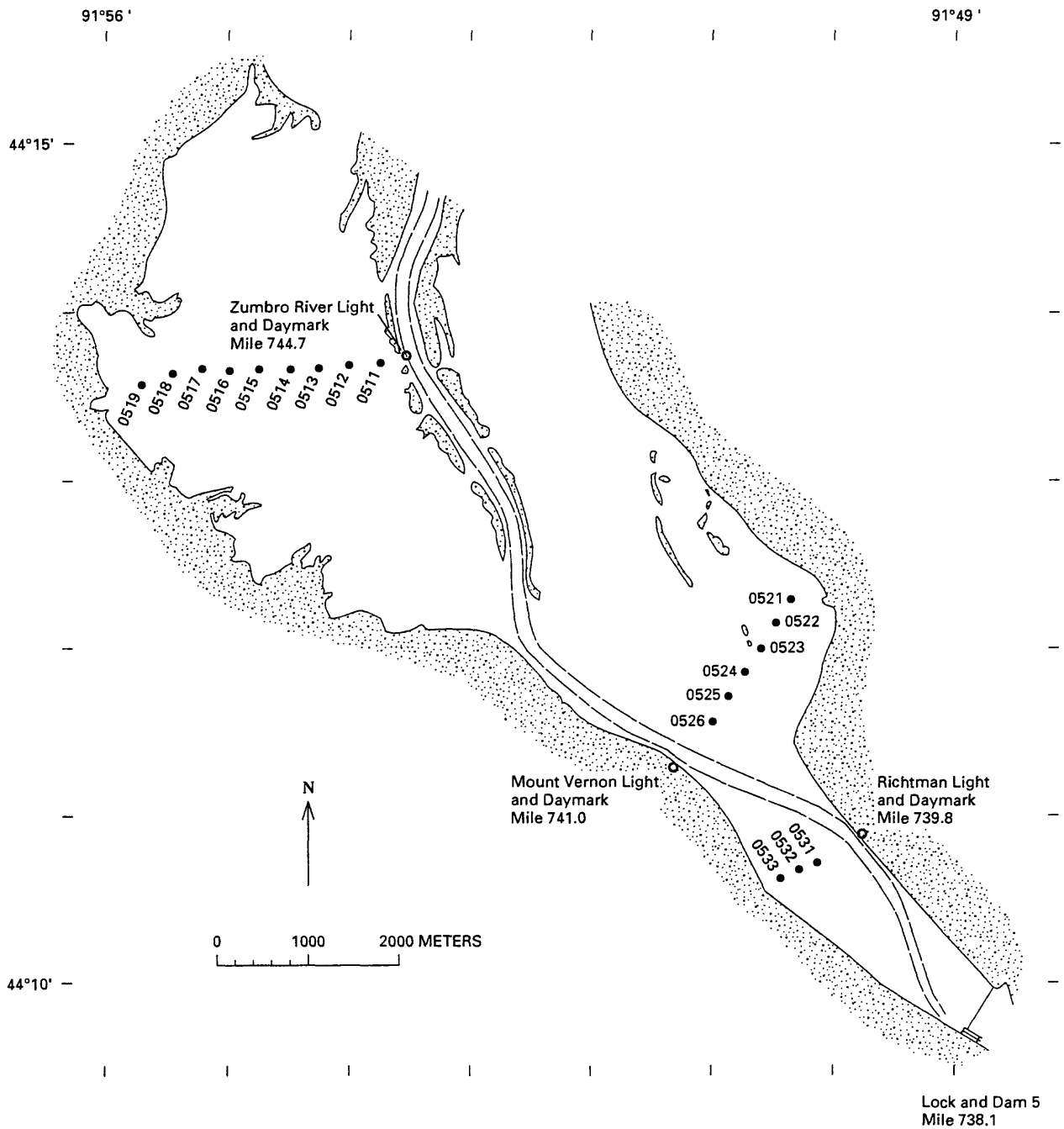
DATE RATED: na

REMARKS:

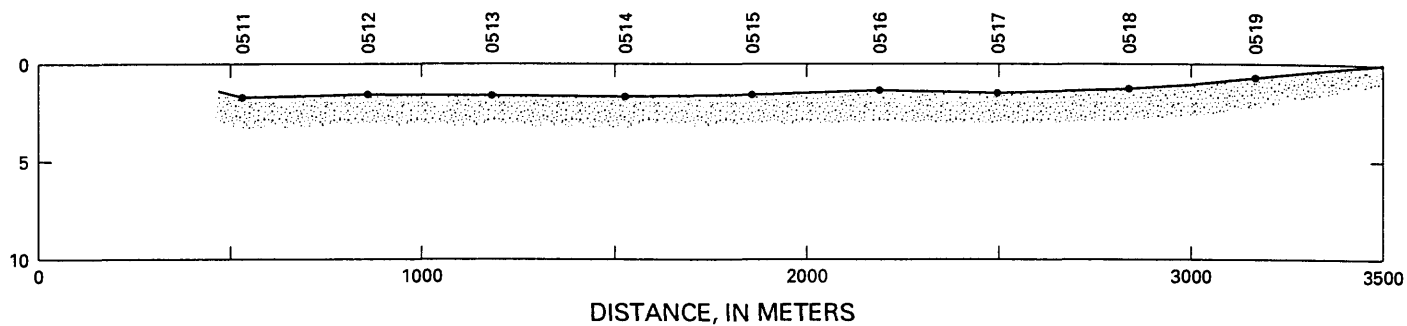
Resampled 7 sites using autonomous GPS because of the necessity of drifting over the target site when sampling from ACADIANA, because of the homogenous bed sediments, and trying to collect both upper and lower Lake Pepin sites in one day. Resampled sites were within ± 80 m. Locations listed below were recorded when the van Veen grab hit bottom. The core sample was collected immediately after the grab. Oxygen and temperature were measured at two depths by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. No velocity measurements were made because the speeds were estimated to be less than 0.05 m/s. Discharge was 1,050 m³/s at Dam 4 (provided by the U.S. Army Corps of Engineers). The blue-green alga, *Aphanizomenon flos-aquae*, was beginning a bloom according to John Sullivan. Biological Resources Division collected a sample from site 0437.

BEARING OF TRANSECT: 013° magnetic

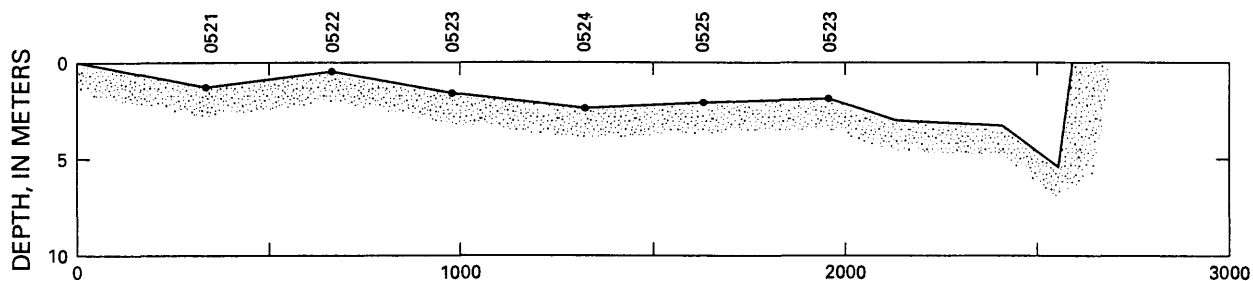
| Site | NAD27 | | Depth (m) | Surface | | Depth of sensor (m) | Dissolved oxygen (mg/L) | Tem- perature (°C) |
|------|---------------|----------------|--------------|-----------------------------------|--------------------------|---------------------------|-------------------------------|--------------------------|
| | Latitude N | Longitude W | | Conduct- ance (μ S/cm) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 0431 | 44°26.39 | 092°09.99 | 5.0 | 565 | 23.1 | 0.1 | 6.3 | 22.8 |
| | | | | | | 2.0 | 6.3 | 22.8 |
| 0432 | 26.21 | 10.06 | 7.6 | 580 | 23.1 | 0.1 | 6.0 | 22.8 |
| | | | | | | 6.0 | 5.9 | 22.7 |
| 0433 | 25.98 | 10.13 | 7.7 | 583 | 23.1 | 0.1 | 5.7 | 22.8 |
| | | | | | | 7.0 | 5.6 | 22.7 |
| 0434 | 25.80 | 10.23 | 7.7 | 580 | 23.2 | 0.1 | 5.8 | 22.8 |
| | | | | | | 7.0 | 5.5 | 22.8 |
| 0435 | 25.54 | 10.28 | 8.2 | 580 | 23.4 | 0.1 | 5.8 | 22.9 |
| | | | | | | 7.0 | 5.5 | 22.7 |
| 0436 | 25.35 | 10.39 | 8.9 | 583 | 23.4 | 0.1 | 5.8 | 22.9 |
| | | | | | | 4.0 | 5.5 | 22.8 |
| | | | | | | 8.0 | 5.1 | 22.6 |
| 0437 | 44°25.12 | 092°10.52 | 9.9 | 581 | 23.7 | -- | -- | -- |
| REW | | | 0.0 | | | | | |



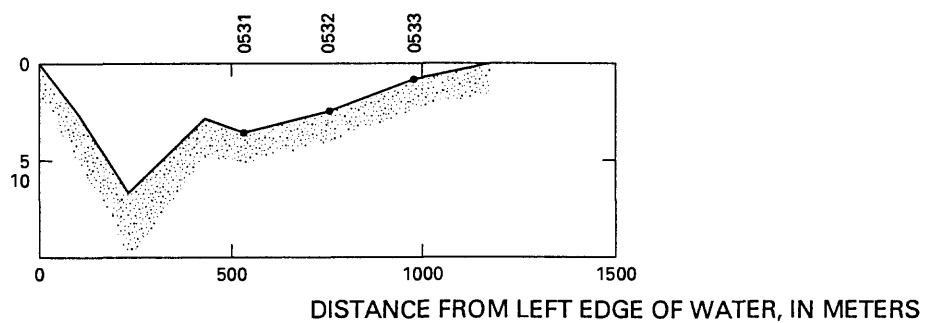
Transect 1 - UMR mile 744.7



Transect 2 - UMR mile 741.0



Transect 3 - UMR mile 739.8



STATION: Mississippi River in Pool 5, Transect 1--UMR mile 744.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 4 TW: 661.51 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Weaver, Minn.-Wis.

DATE: June 16, 1994

GAGE HEIGHT at Dam 5: 659.80 ft

RIVER SLOPE: 34.6×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the 120° corner of the levee (UMR mile 740.6) opposite the lookout tower on the Cochrane, Wis.-Minn. quadrangle (44°11.380 N, 091°50.180 W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample at site 0515. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 5 (provided by the U.S. Army Corps of Engineers) was about 1,060 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 082° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| 0511 | 44°13.662 | 091°53.799 | 0.9 | 497 | 24.2 | 8.0 | 0.07 | 300 | hard mud |
| 0512 | 13.649 | 54.046 | 1.4 | 497 | 24.3 | 8.2 | 0.06 | 280 | hard mud |
| 0513 | 13.640 | 54.293 | 1.5 | 498 | 24.5 | 8.2 | 0.07 | 280 | hard mud |
| 0514 | 13.636 | 54.530 | 1.3 | 495 | 25.6 | 8.2 | 0.08 | 280 | mud |
| 0515 | 13.641 | 54.773 | 1.3 | 496 | 25.9 | 8.4 | 0.07 | 330 | mud |
| 0516 | 13.626 | 55.022 | 1.0 | 464 | 26.6 | 7.5 | 0.07 | 010 | mud |
| 0517 | 13.667 | 55.254 | 0.9 | 477 | 27.0 | 8.1 | 0.09 | 330 | mud |
| 0518 | 13.621 | 55.504 | 0.8 | 482 | 27.3 | 8.9 | 0.07 | 310 | mud |
| 0519 | 44°13.571 | 091°55.790 | 0.6 | 473 | 27.6 | 12.6 | 0.06 | 290 | |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 5, Transect 2--UMR mile 741.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 4 TW: 661.51 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Cochrane, Wis.-Minn.

REMARKS:

DATE: June 16, 1994

GAGE HEIGHT at Dam 5: 659.80 ft

RIVER SLOPE: 34.6×10^{-6}

DATE RATED: 06-25-92

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the 120° corner of the levee (UMR mile 740.6) opposite the lookout tower on the Cochrane, Wis.-Minn. quadrangle (44°11.380 N, 091°50.180 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was 860 m³/s, and the discharge at Dam 5 (provided by the U.S. Army Corps of Engineers) was 1,060 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 032° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0521 | 44°12.223 | 091°50.229 | 1.2 | 470 | 26.2 | 9.0 | 0.09 | 310 | mud |
| 0522 | 12.084 | 50.368 | 0.8 | 467 | 26.7 | 10.4 | 0.07 | 290 | sand |
| 0523 | 11.951 | 50.433 | 1.3 | 467 | 26.6 | 10.4 | 0.09 | 270 | mud, sand |
| 0524 | 11.798 | 50.624 | 2.2 | 469 | 26.3 | 9.4 | 0.23 | 140 | sand, mud |
| 0525 | 11.658 | 50.756 | 1.9 | 470 | 26.7 | 9.5 | 0.24 | 110 | sand |
| 0526 | 11.518 | 50.885 | 1.5 | 466 | 26.9 | 9.6 | 0.25 | 120 | sand |
| 01 | 11.452 | 50.910 | 2.7 | 469 | 26.8 | 9.5 | 0.28 | 120 | -- |
| 02 | 11.309 | 50.992 | 2.9 | 480 | 26.2 | 8.7 | 0.32 | 110 | -- |
| 03 | 44°11.224 | 091°51.033 | 5.5 | 487 | 25.8 | 8.5 | 0.36 | 110 | -- |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 5, Transect 3--UMR mile 739.8

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 4 TW: 661.51 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Cochrane, Wis.-Minn.

DATE: June 16, 1994

GAGE HEIGHT at Dam 5: 659.80 ft

RIVER SLOPE: 34.6×10^{-6}

DATE RATED: 06-25-92

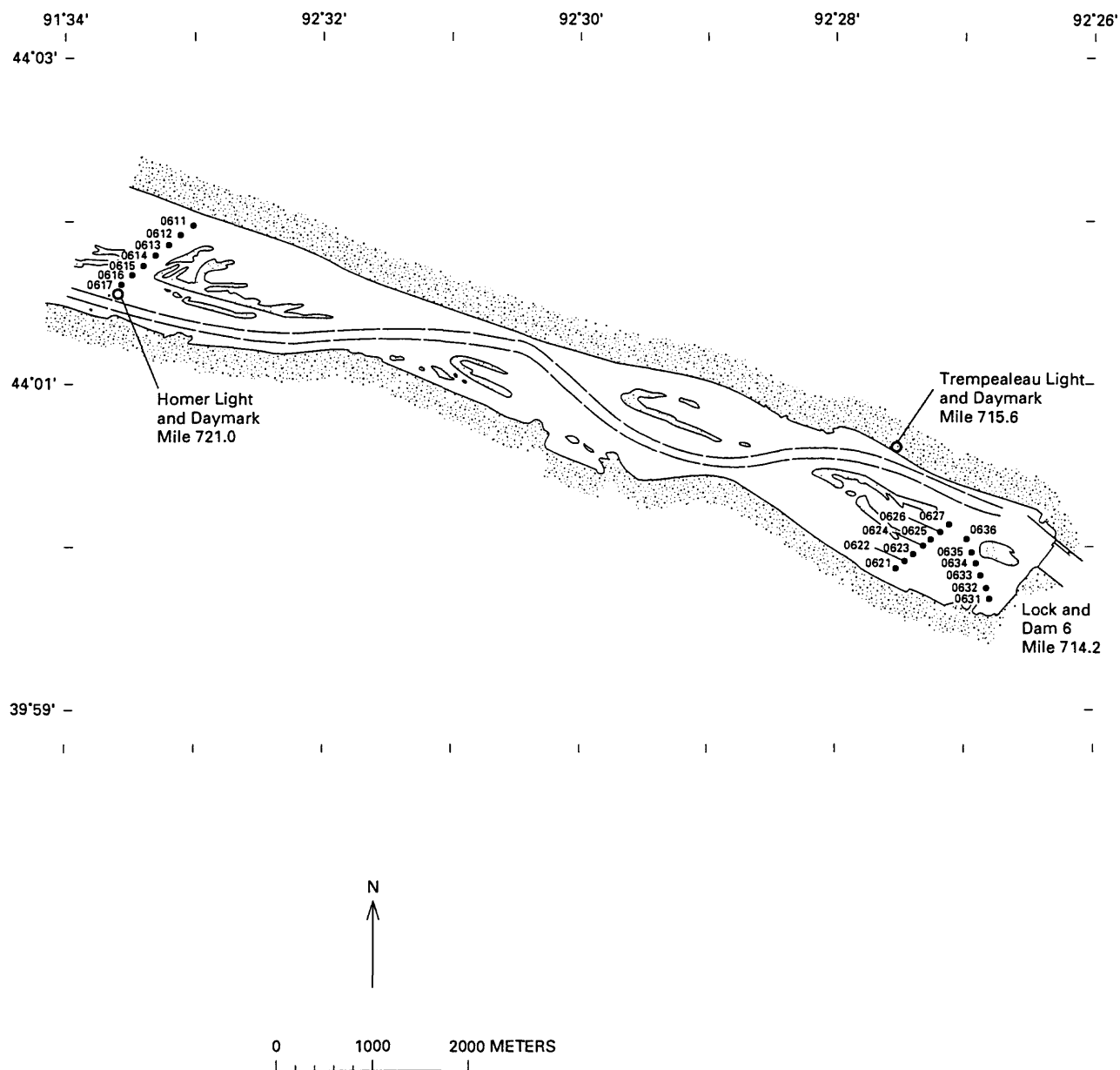
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the 120° corner of the levee (UMR mile 740.6) opposite the lookout tower on the Cochrane, Wis.-Minn. quadrangle (44°11.380 N, 091°50.180 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was 920 m³/s, and the discharge at Dam 5 (provided by the U.S. Army Corps of Engineers) was 1,060 m³/s.

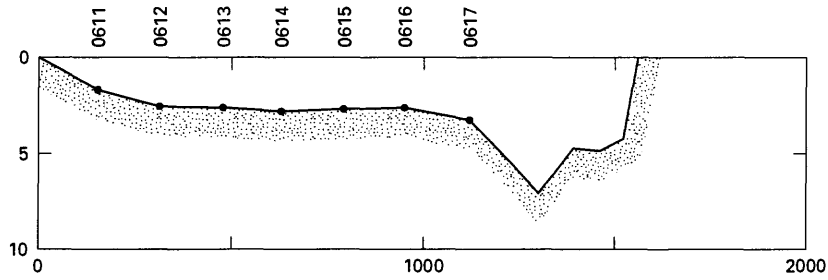
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 060° magnetic

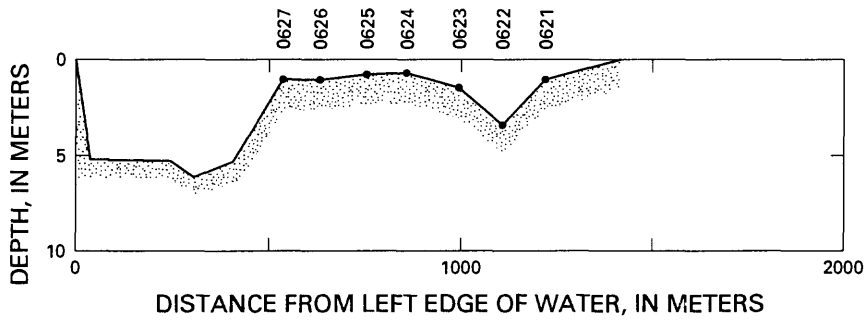
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 07 | 44°10.805 | 091°49.757 | 3.3 | 471 | 26.6 | 10.1 | 0.16 | 130 | -- |
| 06 | 10.771 | 49.799 | 6.4 | 480 | 25.6 | 10.0 | 0.43 | 120 | -- |
| 05 | 10.745 | 49.839 | 3.6 | 476 | 25.7 | 9.9 | 0.40 | 120 | -- |
| 04 | 10.703 | 49.904 | 2.8 | 484 | 25.5 | 9.1 | 0.48 | 120 | -- |
| 0531 | 10.666 | 49.960 | 3.5 | 492 | 25.1 | 8.5 | 0.29 | 120 | sand |
| 0532 | 10.614 | 50.125 | 2.4 | 494 | 25.2 | 8.6 | 0.25 | 120 | sand |
| 0533 | 44°10.560 | 091°50.279 | 1.0 | 493 | 26.4 | 9.0 | 0.14 | 120 | sand |
| REW | | | 0.0 | | | | | | |



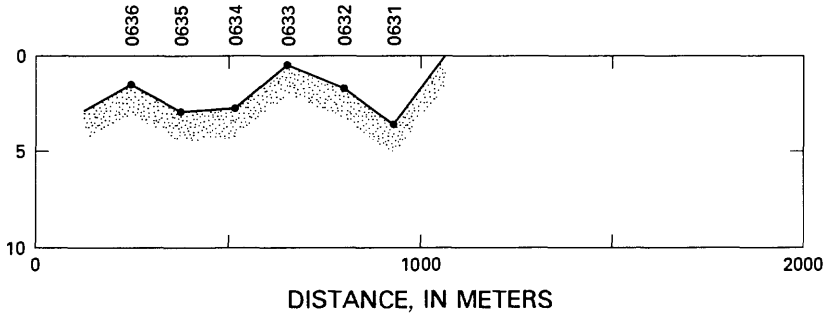
Transect 1 - UMR mile 721.1



Transect 2 - UMR mile 714.95



Transect 2 - UMR mile 714.95



STATION: Mississippi River in Pool 6, Transect 1--UMR mile 721.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 5A TW: 647.04 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Winona East, Wis.-Minn.

DATE: June 16, 1994

GAGE HEIGHT at Dam 6: 644.69 ft

RIVER SLOPE: 29.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located 240 m upstream from a railroad bridge over a small creek which enters the Mississippi River west of Homer, Minn., and east of BM 679 on the Winona East quadrangle ($44^{\circ}01.460$ N, $091^{\circ}33.830$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $1,280 \text{ m}^3/\text{s}$, and the discharge at Dam 6 (provided by the U.S. Army Corps of Engineers) was $1,060 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 047° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0611 | $44^{\circ}01.956$ | $091^{\circ}33.017$ | 1.5 | 483 | 25.4 | 8.5 | 0.27 | 080 | sand |
| 0612 | 01.879 | 33.108 | 4.4 | 482 | 25.3 | 8.5 | 0.40 | 070 | sand |
| 0613 | 01.847 | 33.192 | 2.2 | 484 | 25.3 | 8.4 | 0.57 | 060 | sand |
| 0614 | 01.787 | 33.298 | 2.7 | 483 | 25.2 | 8.3 | 0.53 | 040 | sand |
| 0615 | 01.737 | 33.393 | 2.5 | 487 | 25.2 | 8.3 | 0.53 | 040 | sand |
| 0616 | 01.681 | 33.477 | 2.5 | 485 | 25.2 | 8.3 | 0.51 | 040 | sand |
| 0617 | 01.632 | 33.568 | 2.7 | 486 | 25.2 | 8.2 | 0.36 | 070 | sand |
| 04 | 01.556 | 33.679 | 7.3 | 488 | 25.2 | -- | -- | -- | -- |
| 03 | 01.529 | 33.726 | 4.4 | 490 | 25.2 | -- | -- | -- | -- |
| 02 | 01.500 | 33.771 | 4.5 | 489 | 25.2 | -- | -- | -- | -- |
| 01 | $44^{\circ}01.470$ | $091^{\circ}33.850$ | 4.0 | 490 | 25.1 | -- | -- | -- | -- |
| REW | | | 0.0 | 483 | 24.8 | | | | |

STATION: Mississippi River in Pool 6, Transect 2--UMR mile 714.95

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 5A TW: 647.04 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Trempealeau, Wis.

DATE: June 17, 1994

GAGE HEIGHT at Dam 6: 644.69 ft

RIVER SLOPE: 29.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the dam side wall of the auxiliary lock (43°59.980 N, 091°26.320 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 6 (provided by the U.S. Army Corps of Engineers) was about 1,060 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 049° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | | |
| 0621 | 43°59.868 | 091°27.494 | 1.2 | 473 | 27.3 | 10.1 | 0.32 | 070 | sand |
| 0622 | 59.902 | 27.429 | 1.5 | 478 | 27.3 | 10.2 | 0.29 | 090 | sand |
| 0623 | 59.934 | 27.358 | 2.6 | 465 | 28.5 | 10.4 | 0.28 | 070 | sand |
| 0624 | 59.977 | 27.284 | 0.1 | 461 | 29.2 | 11.5 | <0.05 | -- | sand |
| 0625 | 44°00.010 | 27.222 | 1.0 | 480 | 28.6 | 11.7 | 0.06 | 270 | sand, mud |
| 0626 | 00.047 | 27.147 | 1.1 | 477 | 28.3 | 12.2 | 0.14 | 110 | sand, mud |
| 0627 | 44°00.087 | 091°27.081 | 0.8 | 473 | 27.4 | 10.9 | 0.14 | 110 | sand |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 6, Transect 3--UMR mile 714.95

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 5A TW: 647.04 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Trempealeau, Wis.

DATE: June 17, 1994

GAGE HEIGHT at Dam 6: 644.69 ft

RIVER SLOPE: 29.7×10^{-6}

DATE RATED: 06-25-92

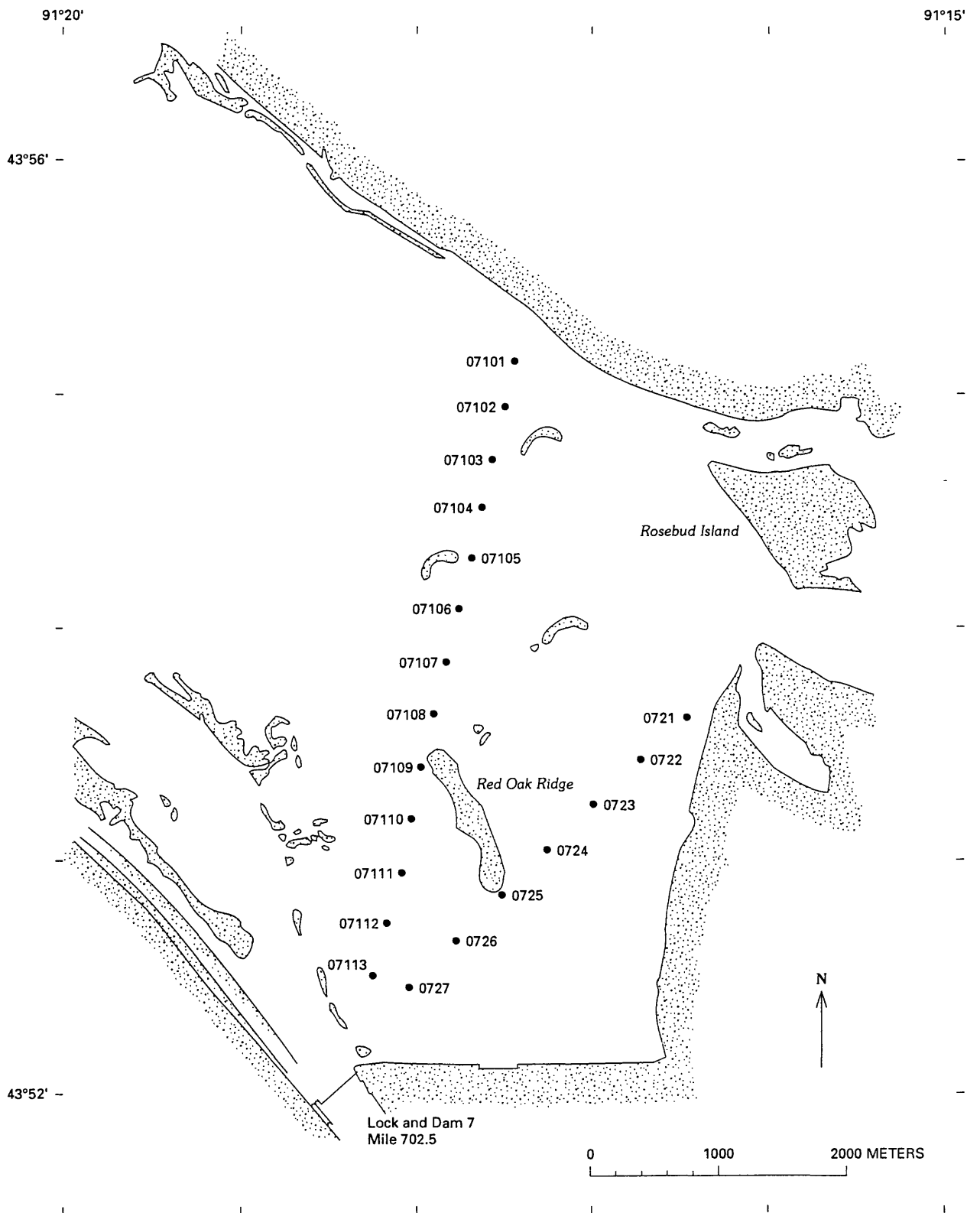
REMARKS:

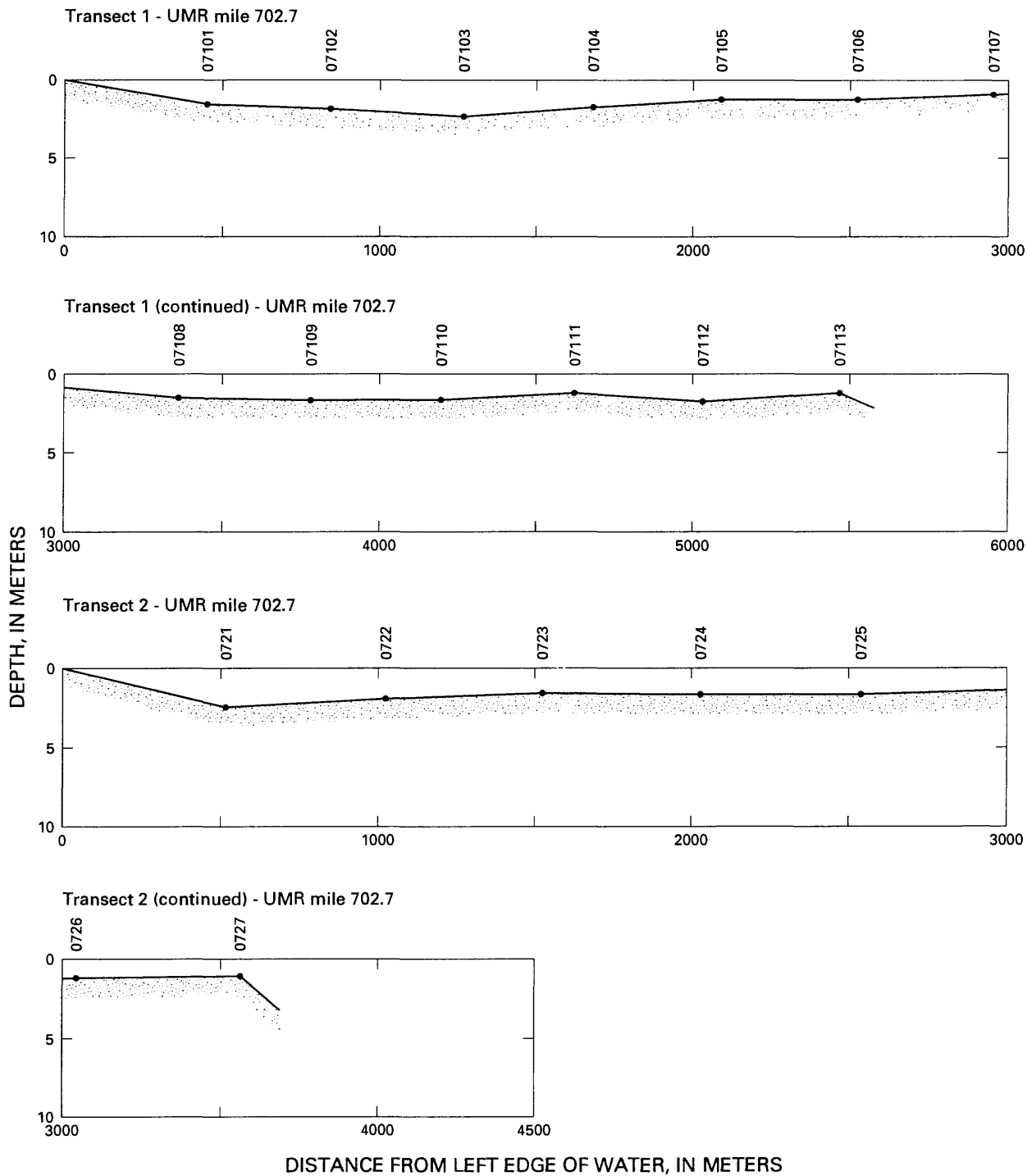
Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the dam side wall of the auxiliary lock ($43^{\circ}59.980$ N, $091^{\circ}26.320$ W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample from site 0632. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 6 (provided by the U.S. Army Corps of Engineers) was about $1,060 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 150° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| 0631 | $43^{\circ}59.660$ | $091^{\circ}26.755$ | 3.1 | 478 | 26.8 | 10.2 | 0.29 | 090 | sand |
| 0632 | 59.728 | 26.803 | 1.6 | 483 | 26.5 | 10.2 | 0.10 | 290 | mud, sand |
| 0633 | 59.796 | 26.828 | 0.4 | 493 | 27.6 | 10.8 | <0.05 | 050 | sand |
| 0634 | 59.872 | 26.873 | 2.2 | 476 | 27.2 | 10.9 | 0.07 | 060 | mud |
| 0635 | 59.935 | 26.904 | 2.9 | 474 | 27.5 | 11.6 | 0.07 | 090 | sand, mud |
| 0636 | $44^{\circ}00.001$ | $091^{\circ}26.947$ | 1.1 | 471 | 27.8 | 11.8 | 0.14 | 120 | sand |
| REW | | | 0.0 | | | | | | |





STATION: Mississippi River in Pool 7, Transect 1--UMR mile 702.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 6 TW: 640.78 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Holmen, Wis., and LaCrescent, Minn.-Wis.

DATE: June 18, 1994

GAGE HEIGHT at Dam 7: 639.17 ft

RIVER SLOPE: 27.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the dam side wall of the auxiliary lock (43°51.995 N, 091°18.550 W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample from site 07103. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 7 (provided by the U.S. Army Corps of Engineers) was about 1,090 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 013° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|-------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 07101 | 43°55.054 | 091°17.449 | 1.6 | 300 | 28.2 | 12.0 | 0.06 | 040 | sand, mud |
| 07102 | 54.908 | 17.494 | 1.7 | 400 | 27.5 | 11.2 | 0.06 | 070 | mud |
| 07103 | 54.689 | 17.564 | 2.0 | 475 | 26.5 | 10.3 | 0.08 | 090 | mud |
| 07104 | 54.476 | 17.621 | 1.8 | 477 | 26.3 | 9.8 | 0.09 | 090 | mud, sand |
| 07105 | 54.266 | 17.692 | 1.1 | 474 | 25.9 | 8.9 | 0.11 | 100 | sand |
| 07106 | 54.030 | 17.757 | 0.9 | 475 | 25.8 | 8.5 | <0.05 | 120 | mud |
| 07107 | 53.810 | 17.832 | 0.8 | 478 | 25.6 | 8.6 | 0.05 | 100 | sand |
| 07108 | 53.599 | 17.890 | 1.2 | 477 | 25.7 | 8.4 | 0.08 | 130 | mud, sand |
| 07109 | 53.376 | 17.958 | 1.7 | 476 | 26.0 | 8.4 | 0.14 | 130 | mud |
| 07110 | 53.150 | 18.027 | 1.5 | 478 | 25.7 | 8.2 | 0.08 | 140 | mud, roots |
| 07111 | 52.925 | 18.099 | 1.2 | 478 | 26.2 | 8.4 | 0.10 | 150 | sand |
| 07112 | 52.712 | 18.168 | 1.8 | 477 | 26.1 | 8.7 | 0.11 | 180 | sand, mud |
| 07113 | 43°52.486 | 091°18.233 | 1.2 | 475 | 26.4 | 9.1 | 0.15 | 170 | sand |

STATION: Mississippi River in Pool 7, Transect 2--UMR mile 702.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 6 TW: 640.78 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Holmen, Wis., and LaCrescent, Minn.-Wis.

DATE: June 18, 1994

GAGE HEIGHT at Dam 7: 639.17 ft

RIVER SLOPE: 27.7×10^{-6}

DATE RATED: 06-25-92

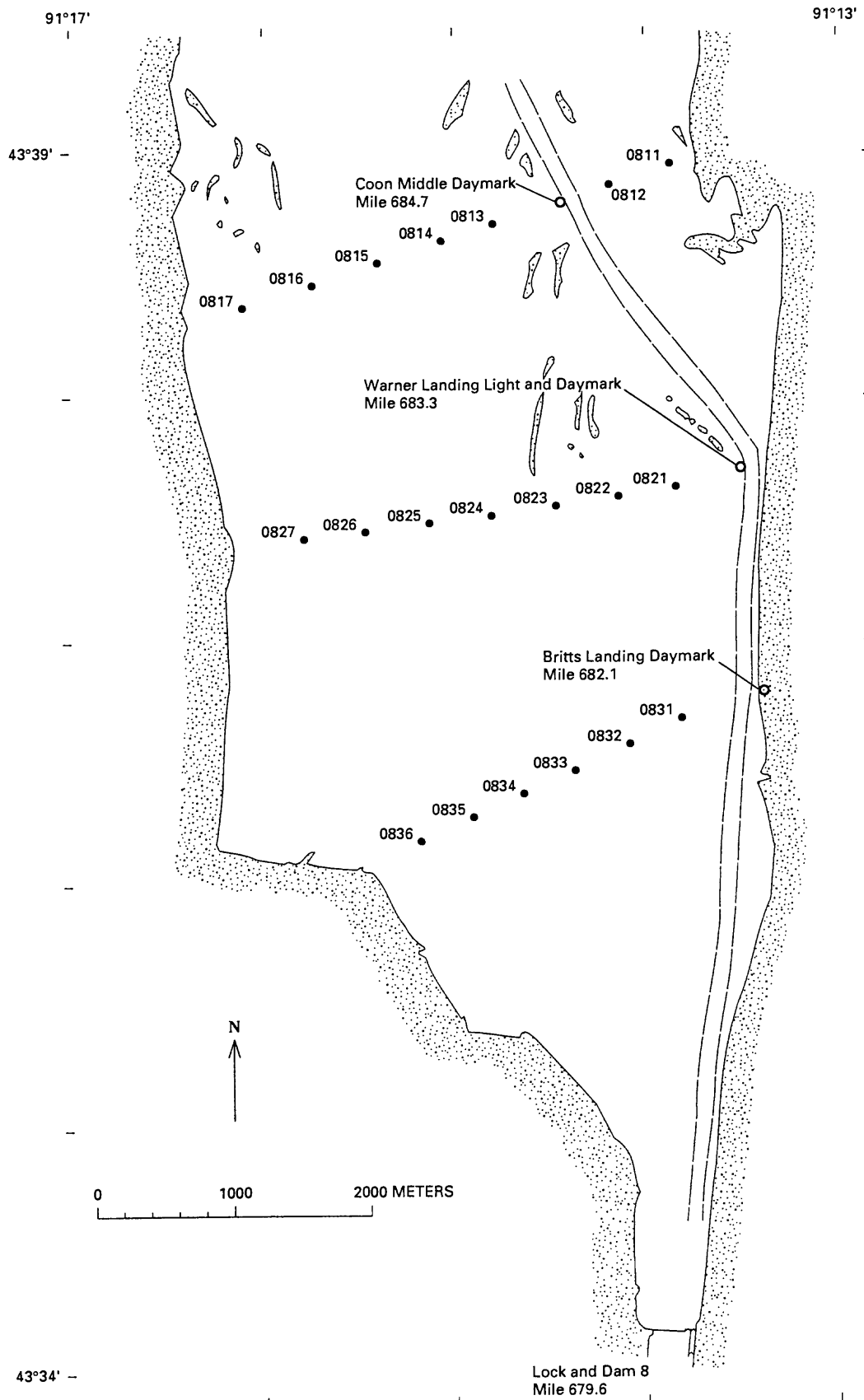
REMARKS:

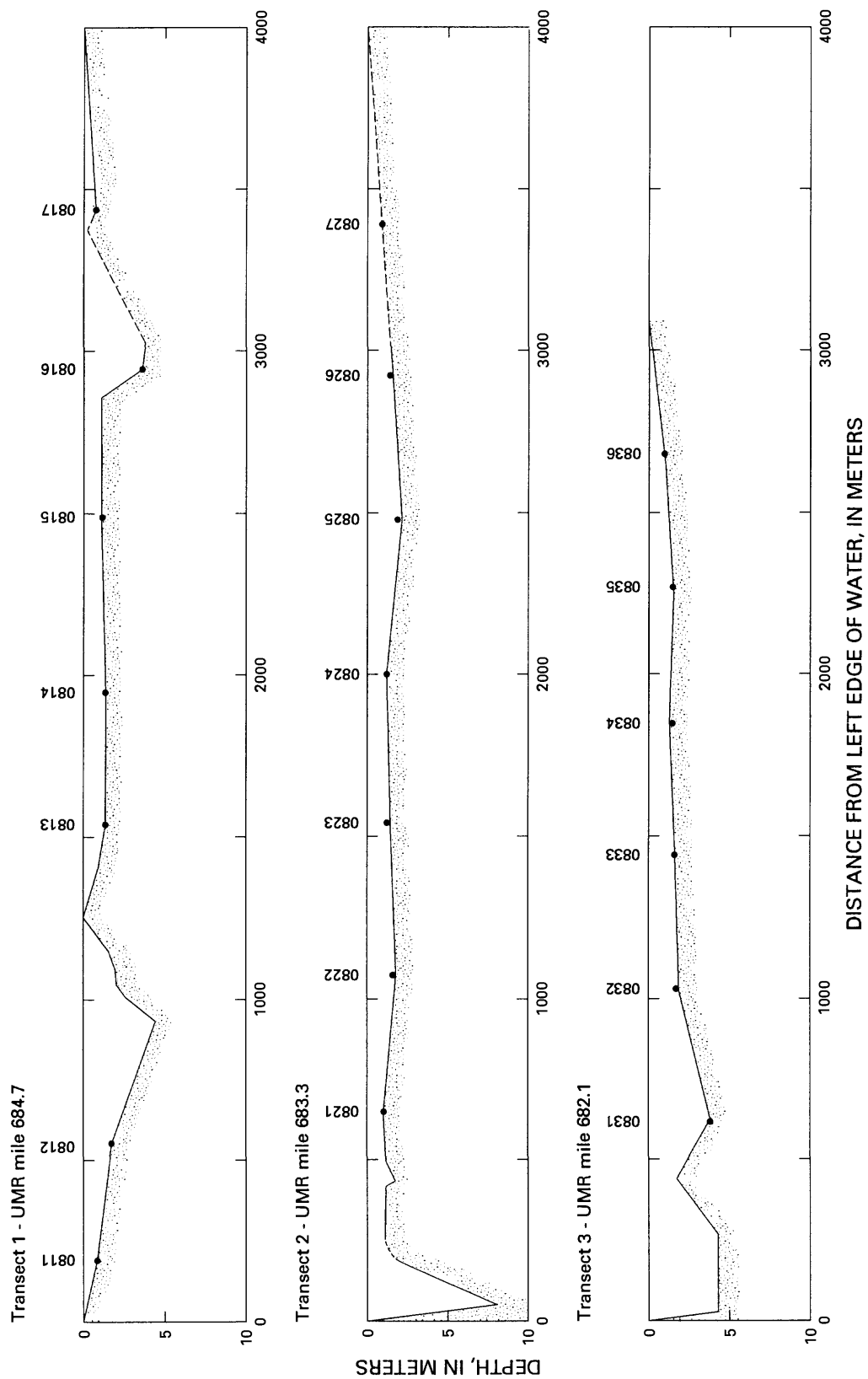
Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the dam side of the wall of the auxiliary lock ($43^{\circ}51.995$ N, $091^{\circ}18.550$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 7 (provided by the U.S. Army Corps of Engineers) was about $1,090 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 046° magnetic

| Site | NAD27 | | Depth (m) | Surface | | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | Dissolved oxygen (mg/L) | | | |
| LEW | | | 0.0 | | | | | | |
| 0721 | $43^{\circ}53.609$ | $091^{\circ}16.420$ | 2.2 | 441 | 28.1 | 11.9 | 0.07 | 140 | mud |
| 0722 | 53.423 | 16.692 | 1.9 | 458 | 28.1 | 12.6 | 0.12 | 150 | mud,shells |
| 0723 | 53.238 | 16.946 | 1.7 | 469 | 27.9 | 10.0 | 0.09 | 130 | mud |
| 0724 | 53.035 | 17.224 | 1.4 | 470 | 27.9 | 10.0 | 0.12 | 160 | mud |
| 0725 | 52.849 | 17.481 | 1.5 | 462 | 28.6 | 10.0 | 0.16 | 180 | sand |
| 0726 | 52.664 | 17.749 | 1.6 | 465 | 28.6 | 11.0 | 0.14 | 170 | -- |
| 0727 | $43^{\circ}52.466$ | $091^{\circ}18.024$ | 1.1 | 464 | 28.4 | 10.8 | 0.14 | 200 | -- |





STATION: Mississippi River in Pool 8, Transect 1--UMR mile 684.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 7 TW: 632.86 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Brownsville, Minn.-Wis., and Stoddard, Wis.

DATE: June 19, 1994

GAGE HEIGHT at Dam 8: 630.14 ft

RIVER SLOPE: 21.5×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on a dogleg of the earth dam next to a dirt road with an elevation of 640 ft ($43^{\circ}36.040$ N, $091^{\circ}15.470$ W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample from site 0817. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $1,340 \text{ m}^3/\text{s}$, and the discharge at Dam 8 (provided by the U.S. Army Corps of Engineers) was $1,190 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 067° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduc- tance ($\mu\text{S}/\text{cm}$) | Temp- erature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0811 | $43^{\circ}38.839$ | $091^{\circ}13.794$ | 1.0 | 450 | 29.6 | 8.6 | 0.22 | 170 | -- |
| 0812 | 38.759 | 14.120 | 2.0 | 466 | 27.8 | 8.8 | 0.20 | 160 | sand |
| 09 | 38.736 | 14.233 | 3.4 | 466 | 28.0 | 8.5 | 0.14 | 110 | -- |
| 08 | 38.725 | 14.300 | 4.3 | 476 | 27.2 | 9.5 | 0.51 | 140 | -- |
| 07 | 38.706 | 14.365 | 2.2 | 468 | 27.9 | 9.2 | 0.40 | 120 | -- |
| 06 | 38.682 | 14.470 | 1.3 | 463 | 28.6 | 9.2 | 0.42 | 170 | -- |
| 05 | 38.622 | 14.695 | 0.3 | 463 | 29.2 | 9.3 | 0.21 | 180 | -- |
| 0813 | 38.615 | 14.747 | 1.4 | 464 | 28.5 | 9.2 | 0.35 | 190 | sand |
| 0814 | 38.544 | 15.032 | 1.1 | 471 | 28.1 | 9.9 | 0.14 | 140 | mud, sand |
| 0815 | 38.466 | 15.395 | 1.2 | 478 | 29.6 | 10.2 | 0.10 | 170 | sand |
| 0816 | 38.377 | 15.743 | 3.5 | 484 | 27.4 | 9.5 | 0.31 | 150 | sand |
| 0817 | $43^{\circ}38.300$ | $091^{\circ}16.101$ | 1.3 | 485 | 26.9 | 10.1 | 0.06 | 350 | mud |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 8, Transect 2--UMR mile 683.3

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 7 TW: 632.86 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Brownsville, Minn.-Wis.; Stoddard, Wis.; Genoa, Wis.; and Reno, Minn.

DATE: June 19, 1994

GAGE HEIGHT at Dam 8: 630.14 ft

RIVER SLOPE: 21.5×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on a dogleg of the earth dam next to a dirt road with an elevation of 640 ft (43°36.040 N, 091°15.470 W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was 900 m³/s, and the discharge at Dam 8 (provided by the U.S. Army Corps of Engineers) was 1,190 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 078° magnetic

| Site | NAD27 | | Depth (m) | Surface | | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | Dissolved oxygen (mg/L) | | | |
| LEW | | | 0.0 | | | | | | |
| 10 | 43°37.608 | 091°13.312 | 4.2 | 462 | 29.5 | 9.8 | 0.15 | 150 | -- |
| 11 | 37.600 | 13.366 | 7.4 | 458 | 29.7 | 10.0 | 0.33 | 150 | -- |
| 12 | 37.589 | 13.408 | 3.6 | 461 | 28.3 | 9.3 | 0.31 | 140 | -- |
| 13 | 37.550 | 13.628 | 1.4 | 460 | 29.0 | 10.0 | 0.38 | 150 | -- |
| 0821 | 37.555 | 13.799 | 1.0 | 466 | 29.1 | 10.4 | 0.11 | 160 | sand |
| 0822 | 37.527 | 14.105 | 1.7 | 460 | 30.3 | 11.0 | 0.15 | 160 | sand |
| 0823 | 37.499 | 14.447 | 0.9 | 444 | 31.3 | 11.5 | 0.14 | 150 | sand |
| 0824 | 37.467 | 14.787 | 1.0 | 464 | 30.6 | 12.0 | 0.13 | 150 | sand |
| 0825 | 37.432 | 15.122 | 2.0 | 462 | 30.3 | 12.4 | 0.14 | 130 | mud, shells |
| 0826 | 37.410 | 15.461 | 1.5 | 460 | 31.2 | 14.0 | 0.13 | 140 | mud |
| 0827 | 43°37.379 | 091°15.798 | 0.8 | 475 | 29.5 | 12.8 | 0.11 | 110 | mud |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 8, Transect 3--UMR mile 682.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 7 TW: 632.86 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Genoa, Wis., and Reno, Minn.

DATE: June 19, 1994

GAGE HEIGHT at Dam 8: 630.14 ft

RIVER SLOPE: 21.5×10^{-6}

DATE RATED: 06-25-92

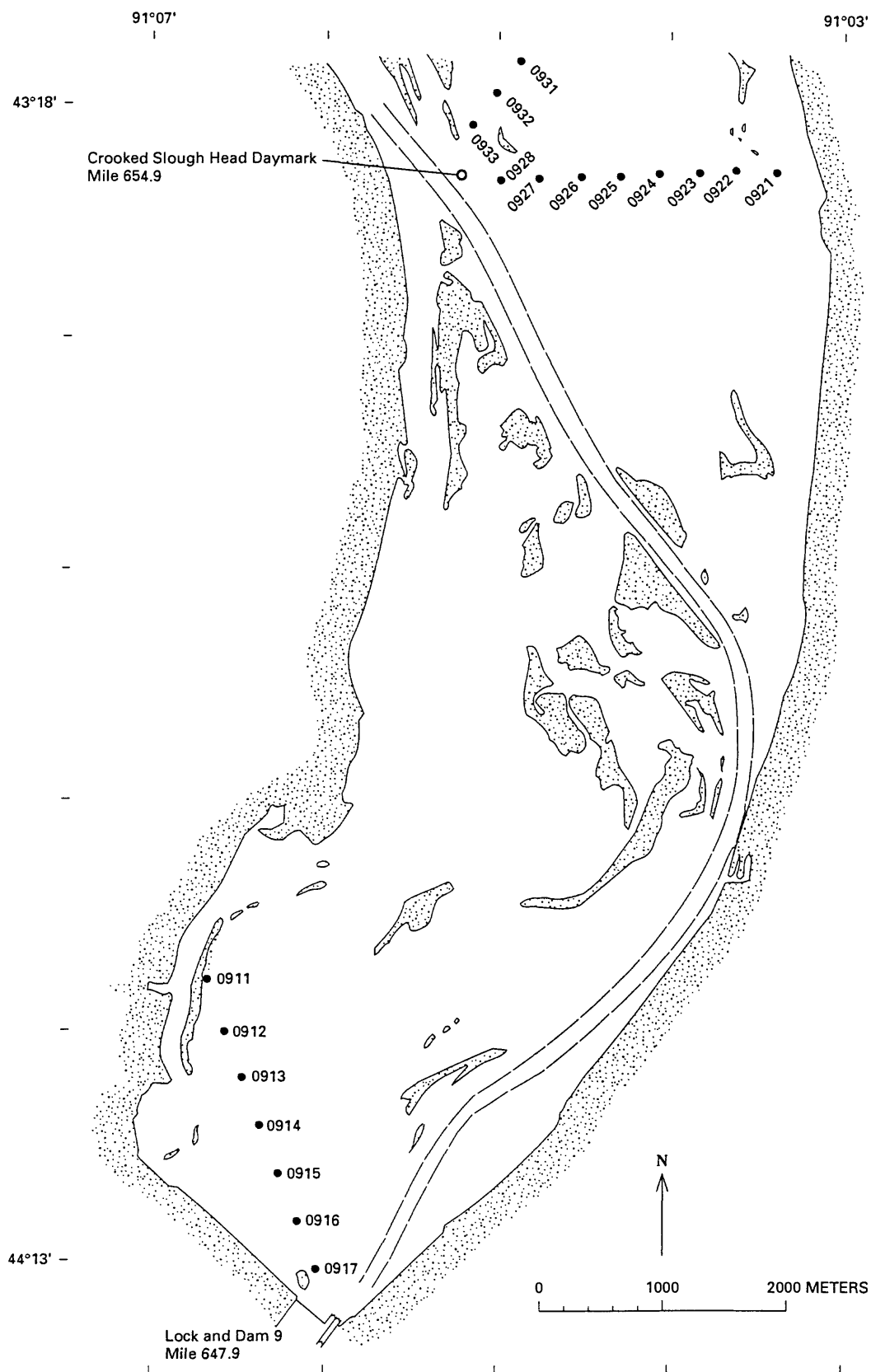
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on a dogleg of the earth dam next to a dirt road with an elevation of 640 ft ($43^{\circ}36.040$ N, $091^{\circ}15.470$ W, NAD27, accuracy ± 25 m). No grab sample was collected from site 0834. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $940 \text{ m}^3/\text{s}$ and the discharge at Dam 8 (provided by the U.S. Army Corps of Engineers) was about $1,190 \text{ m}^3/\text{s}$.

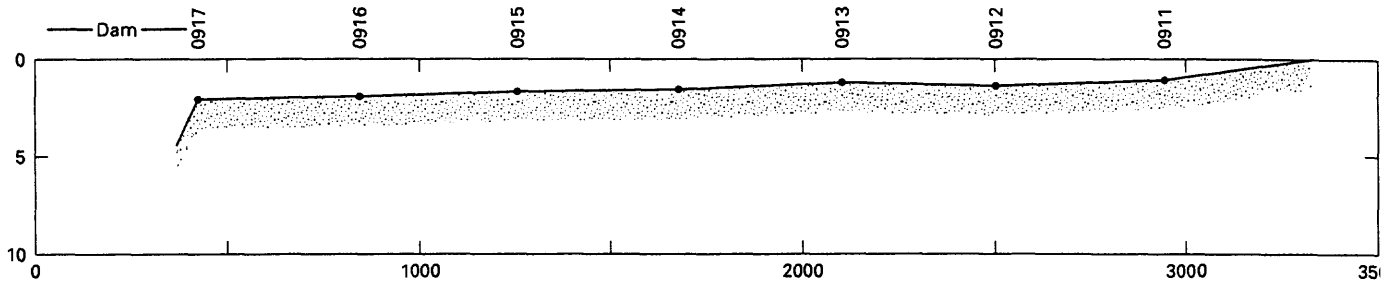
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 064° magnetic

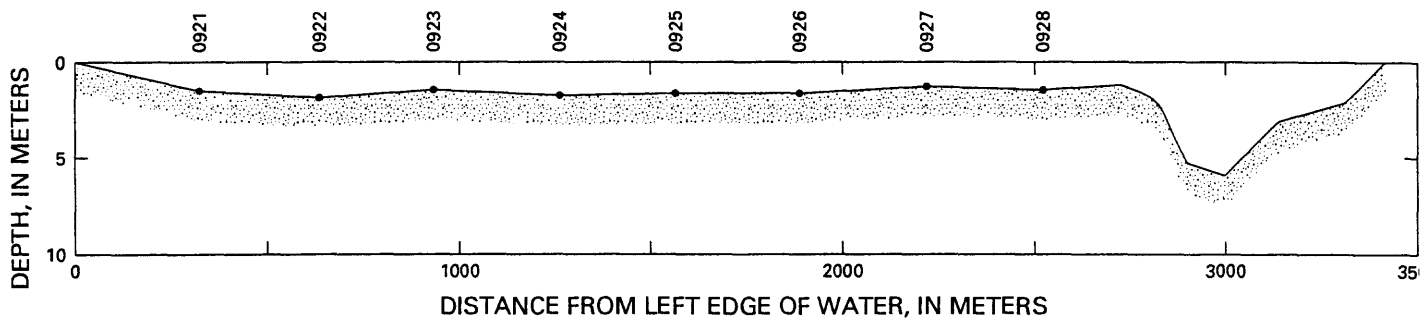
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 04 | $43^{\circ}36.741$ | $091^{\circ}13.383$ | 4.1 | 469 | 26.9 | 8.0 | 0.30 | 140 | -- |
| 03 | 36.729 | 13.431 | 4.8 | 471 | 26.8 | 8.1 | 0.32 | 150 | -- |
| 02 | 36.705 | 13.517 | 4.0 | 472 | 26.6 | 8.4 | 0.25 | 140 | -- |
| 01 | 36.660 | 13.655 | 1.7 | 474 | 26.7 | 9.5 | 0.13 | 140 | -- |
| 0831 | 36.623 | 13.787 | 3.4 | 473 | 26.6 | 8.9 | 0.14 | 120 | mud |
| 0832 | 36.528 | 14.068 | 1.6 | 473 | 26.5 | 8.8 | 0.21 | 140 | mud, sand |
| 0833 | 36.425 | 14.362 | 1.5 | 478 | 26.4 | 8.9 | 0.17 | 120 | clay |
| 0834 | 36.329 | 14.627 | 1.2 | 475 | 26.7 | 8.8 | 0.14 | 120 | clay |
| 0835 | 36.245 | 14.879 | 1.4 | 474 | 26.5 | 9.0 | 0.13 | 120 | mud, sand |
| 0836 | $43^{\circ}36.146$ | $091^{\circ}15.163$ | 1.0 | 486 | 26.2 | 8.5 | 0.13 | 150 | sand |
| REW | | | 0.0 | | | | | | |



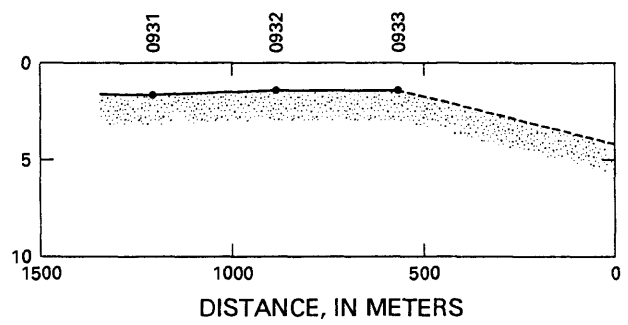
Transect 1 - UMR mile 648.0



Transect 2 - UMR mile 655.0



Transect 3 - UMR mile 655.0



STATION: Mississippi River in Pool 9, Transect 1--UMR mile 648.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 8 TW: 623.59 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Eastman, Wis.-Iowa

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock (43°12.740 N, 091°05.955 W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample from site 0915. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 9 (provided by the U.S. Army Corps of Engineers) was about 1,070 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 159° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| REW | | | 0.0 | | | | | | |
| 0911 | 43°14.203 | 091°06.665 | 0.7 | 485 | 26.5 | 2.8 | <0.05 | -- | mud |
| 0912 | 13.988 | 06.547 | 1.1 | 484 | 26.8 | 4.0 | 0.05 | 150 | mud |
| 0913 | 13.795 | 06.452 | 1.0 | 480 | 27.1 | 4.2 | 0.09 | 120 | mud |
| 0914 | 13.583 | 06.350 | 1.2 | 483 | 26.8 | 3.7 | 0.12 | 130 | mud |
| 0915 | 13.367 | 06.242 | 1.3 | 483 | 27.0 | 3.5 | 0.14 | 130 | mud |
| 0916 | 13.154 | 06.133 | 1.7 | 484 | 27.0 | 3.6 | 0.20 | 140 | mud, clay |
| 0917 | 43°12.938 | 091°06.031 | 1.8 | 484 | 27.1 | 3.4 | 0.40 | 130 | clay |

STATION: Mississippi River in Pool 9, Transect 2--UMR mile 655.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 8 TW: 623.59 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Ferryville, Iowa-Wis.

DATE: June 20, 1994

GAGE HEIGHT at Dam 9: 619.19 ft

RIVER SLOPE: 26.9×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock ($43^{\circ}12.740$ N, $091^{\circ}05.955$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $860 \text{ m}^3/\text{s}$, and the discharge at Dam 9 (provided by the U.S. Army Corps of Engineers) was $1,070 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 089° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0921 | $43^{\circ}17.761$ | $091^{\circ}03.322$ | 1.2 | 459 | 27.4 | 4.5 | 0.18 | 150 | mud |
| 0922 | 17.758 | 03.564 | 1.8 | 456 | 27.7 | 4.9 | 0.17 | 140 | mud |
| 0923 | 17.747 | 03.792 | 1.3 | 455 | 27.9 | 5.2 | 0.17 | 150 | mud |
| 0924 | 17.735 | 04.033 | 1.4 | 455 | 27.4 | 5.2 | 0.23 | 140 | mud |
| 0925 | 17.730 | 04.248 | 1.4 | 455 | 27.3 | 5.1 | 0.16 | 140 | mud |
| 0926 | 17.724 | 04.487 | 1.2 | 455 | 27.1 | 4.9 | 0.06 | 130 | mud |
| 0927 | 17.713 | 04.728 | 1.0 | 469 | 27.3 | 4.8 | 0.14 | 150 | mud |
| 0928 | 17.705 | 04.964 | 1.3 | 464 | 27.1 | 4.9 | 0.14 | 160 | mud |
| 01 | 17.694 | 05.106 | 0.9 | 469 | 27.2 | 5.4 | 0.17 | 090 | -- |
| 02 | 17.691 | 05.187 | 1.9 | 473 | 27.6 | 7.0 | 0.18 | 150 | -- |
| 03 | 17.689 | 05.245 | 5.3 | 472 | 27.6 | 7.5 | 0.39 | 130 | -- |
| 04 | 17.688 | 05.310 | 6.0 | 470 | 27.6 | 7.1 | 0.33 | 120 | -- |
| 05 | 17.687 | 05.408 | 2.8 | 472 | 27.6 | 6.8 | 0.39 | 120 | -- |
| 06 | $43^{\circ}17.682$ | $091^{\circ}05.541$ | 2.1 | 470 | 27.8 | 6.5 | 0.30 | 170 | -- |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 9, Transect 3--UMR mile 655.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 8 TW: 623.59 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Ferryville, Iowa-Wis.

DATE: June 20, 1994

GAGE HEIGHT at Dam 9: 619.19 ft

RIVER SLOPE: 26.9×10^{-6}

DATE RATED: 06-25-92

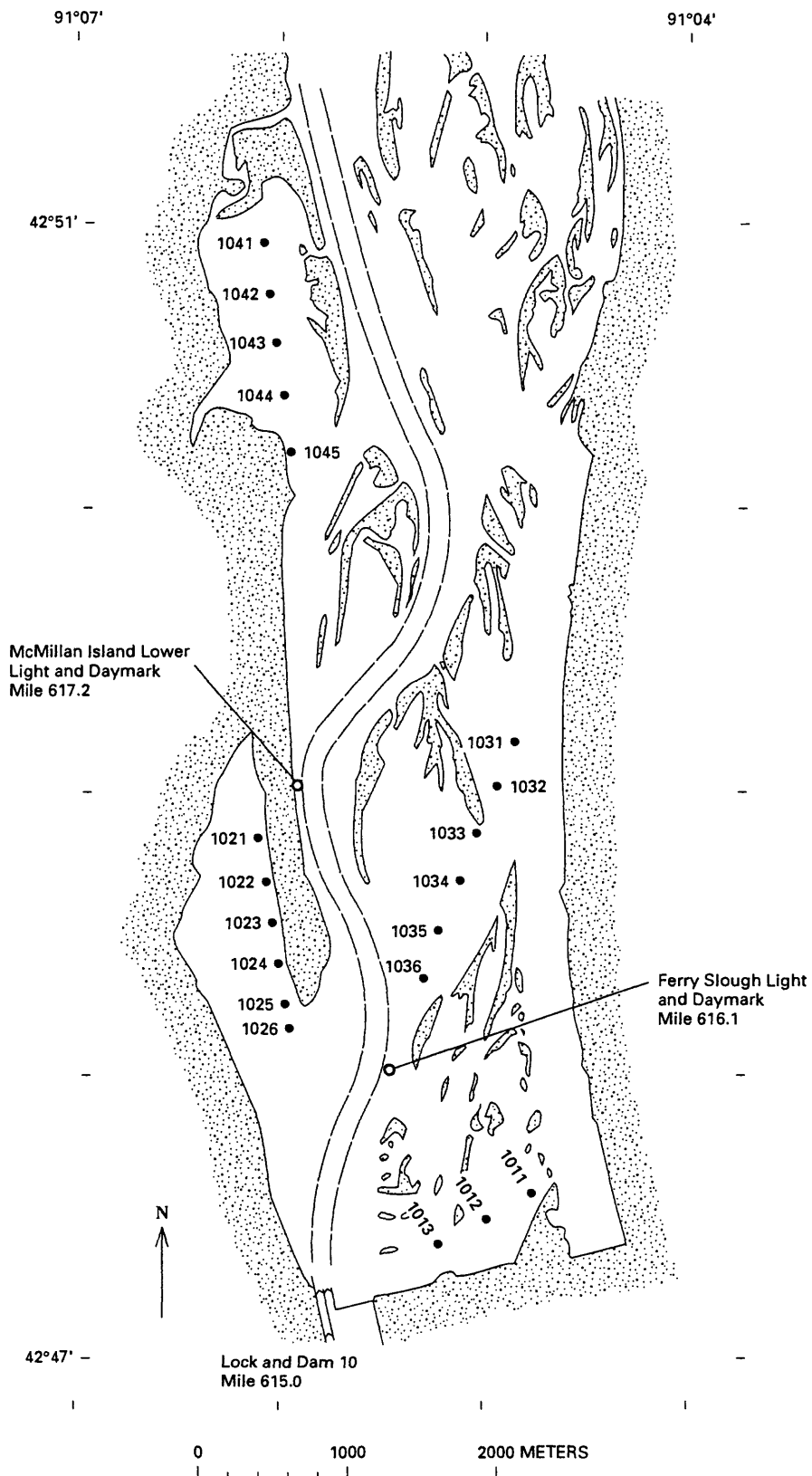
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock ($43^{\circ}12.740$ N, $091^{\circ}05.955$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 9 (provided by the U.S. Army Corps of Engineers) was about $1,070 \text{ m}^3/\text{s}$.

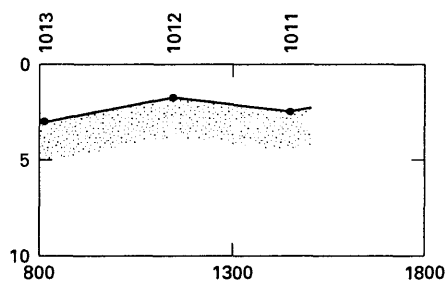
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 037° magnetic

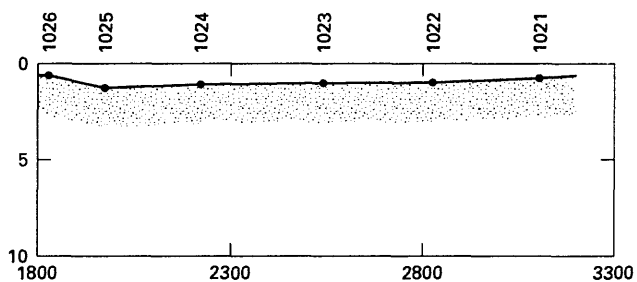
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| LEW | | | 0.0 | | | | | | |
| 0931 | $43^{\circ}18.223$ | $091^{\circ}04.850$ | 1.3 | 474 | 26.8 | 5.6 | 0.13 | 150 | mud |
| 0932 | 18.074 | 04.993 | 1.0 | 473 | 27.0 | 5.2 | 0.11 | 140 | mud |
| 0933 | $43^{\circ}17.941$ | 05.135 | 1.1 | 471 | 27.0 | 5.9 | 0.11 | 110 | mud |



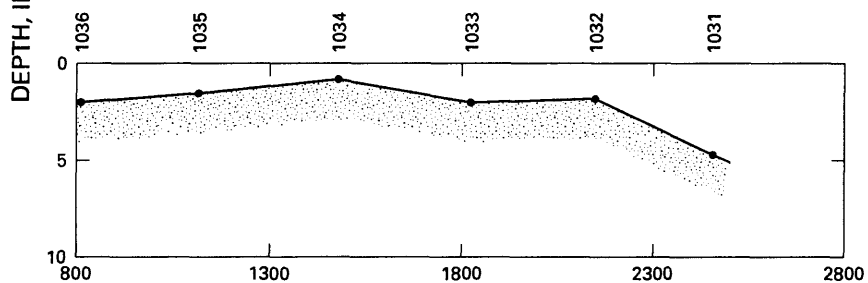
Transect 1 - UMR mile 615.0



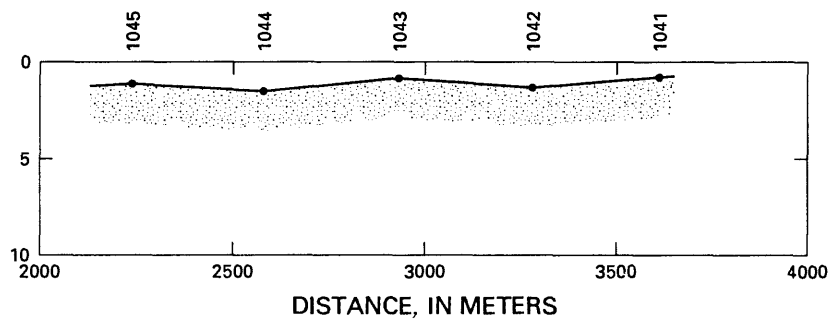
Transect 2 - UMR mile 615.0 - Bussey Lake



Transect 3 - UMR mile 616.1



Transect 4 - UMR mile 617.2 - Frenchtown Lake



STATION: Mississippi River in Pool 10, Transect 1--UMR mile 615.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 9 TW: 615.62 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Guttenberg, Iowa-Wis.

DATE: June 20, 1994

GAGE HEIGHT at Dam 10: 611.13 ft

RIVER SLOPE: 25.8×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock ($42^{\circ}47.165$ N, $091^{\circ}05.675$ W, NAD27, accuracy ± 25 m). John Sullivan got a navigation beacon fix at this location of $42^{\circ}47.1705$ N, $091^{\circ}05.6856$ W, NAD27, the average of 100 fixes over 4 minutes. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 10 (provided by the U.S. Army Corps of Engineers) was about $1,360 \text{ m}^3/\text{s}$. The discharge, gage heights, and river slopes are for June 21, 1994.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 057° magnetic

| Site | NAD27 | | Depth (m) | Surface | | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | Dissolved oxygen (mg/L) | | | |
| LEW | | | 0.0 | | | | | | |
| 1011 | $42^{\circ}47.553$ | $091^{\circ}04.725$ | 2.2 | 429 | 28.1 | 5.6 | 0.24 | 200 | sand |
| 1012 | 47.458 | 04.946 | 1.4 | 423 | 28.3 | 5.9 | 0.18 | 220 | sand |
| 1013 | $42^{\circ}47.372$ | 05.154 | 2.9 | 424 | 28.1 | 5.8 | 0.35 | 200 | sand |

STATION: Mississippi River in Pool 10, Transect 2--UMR mile 615.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 9 TW: 615.62 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Guttenberg, Iowa-Wis.

DATE: June 20, 1994

GAGE HEIGHT at Dam 10: 611.13 ft

RIVER SLOPE: 25.8×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock ($42^{\circ}47.165$ N, $091^{\circ}05.675$ W, NAD27, accuracy ± 25 m). John Sullivan got a navigation beacon fix at this location of $42^{\circ}47.1705$ N, $091^{\circ}05.6856$ W, NAD27, the average of 100 fixes over 4 minutes. Biological Resources Division collected a sample at site 1023. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 10 (provided by the U.S. Army Corps of Engineers) was about $1,360 \text{ m}^3/\text{s}$. The discharge, gage heights, and river slopes are for June 21, 1994.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 164° magnetic

| Site | NAD27 | | Depth (m) | Surface | | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | Dissolved oxygen (mg/L) | | | |
| 1021 | $42^{\circ}48.839$ | $091^{\circ}06.079$ | 0.6 | 362 | 24.8 | 2.9 | <0.05 | -- | mud, roots |
| 1022 | 48.674 | 06.041 | 0.9 | 383 | 24.9 | 2.4 | <0.05 | -- | mud |
| 1023 | 48.518 | 05.999 | 1.1 | 450 | 25.9 | 5.2 | <0.05 | -- | mud |
| 1024 | 48.373 | 05.968 | 1.0 | 462 | 26.3 | 3.8 | 0.07 | 150 | mud |
| 1025 | 48.212 | 05.920 | 1.1 | 476 | 26.7 | 3.7 | 0.09 | 240 | mud |
| 1026 | $42^{\circ}48.135$ | $091^{\circ}05.901$ | 0.7 | 477 | 27.0 | 3.8 | 0.25 | 210 | sand, clay |

STATION: Mississippi River in Pool 10, Transect 3--UMR mile 616.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 9 TW: 615.62 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Guttenberg, Iowa--Wis.

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock (42°47.165 N, 091°05.675 W, NAD27, accuracy ± 25 m). John Sullivan got a navigation beacon fix at this location of 42°47.1705 N, 091°05.6856 W, NAD27, the average of 100 fixes over 4 minutes. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 10 (provided by the U.S. Army Corps of Engineers) was about 1,360 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 015° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 1031 | 42°49.156 | 091°04.854 | 4.7 | 439 | 27.5 | 4.9 | 0.36 | 170 | mud |
| 1032 | 48.999 | 04.929 | 1.8 | 454 | 27.5 | 4.9 | 0.41 | 210 | sand |
| 1033 | 48.788 | 05.031 | 2.0 | 451 | 27.6 | 4.9 | 0.28 | 190 | sand |
| 1034 | 48.650 | 05.095 | 0.6 | 449 | 27.3 | 5.0 | 0.37 | 190 | sand |
| 1035 | 48.471 | 05.175 | 1.2 | 447 | 27.7 | 5.2 | 0.22 | 190 | mud, sand |
| 1036 | 42°48.310 | 091°05.252 | 1.8 | 442 | 28.1 | 5.3 | 0.16 | 190 | mud |

STATION: Mississippi River in Pool 10, Transect 4--UMR mile 617.2

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 9 TW: 615.62 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Guttenberg, Iowa-Wis.

DATE: June 21, 1994

GAGE HEIGHT at Dam 10: 611.13 ft

RIVER SLOPE: 25.8×10^{-6}

DATE RATED: 06-25-92

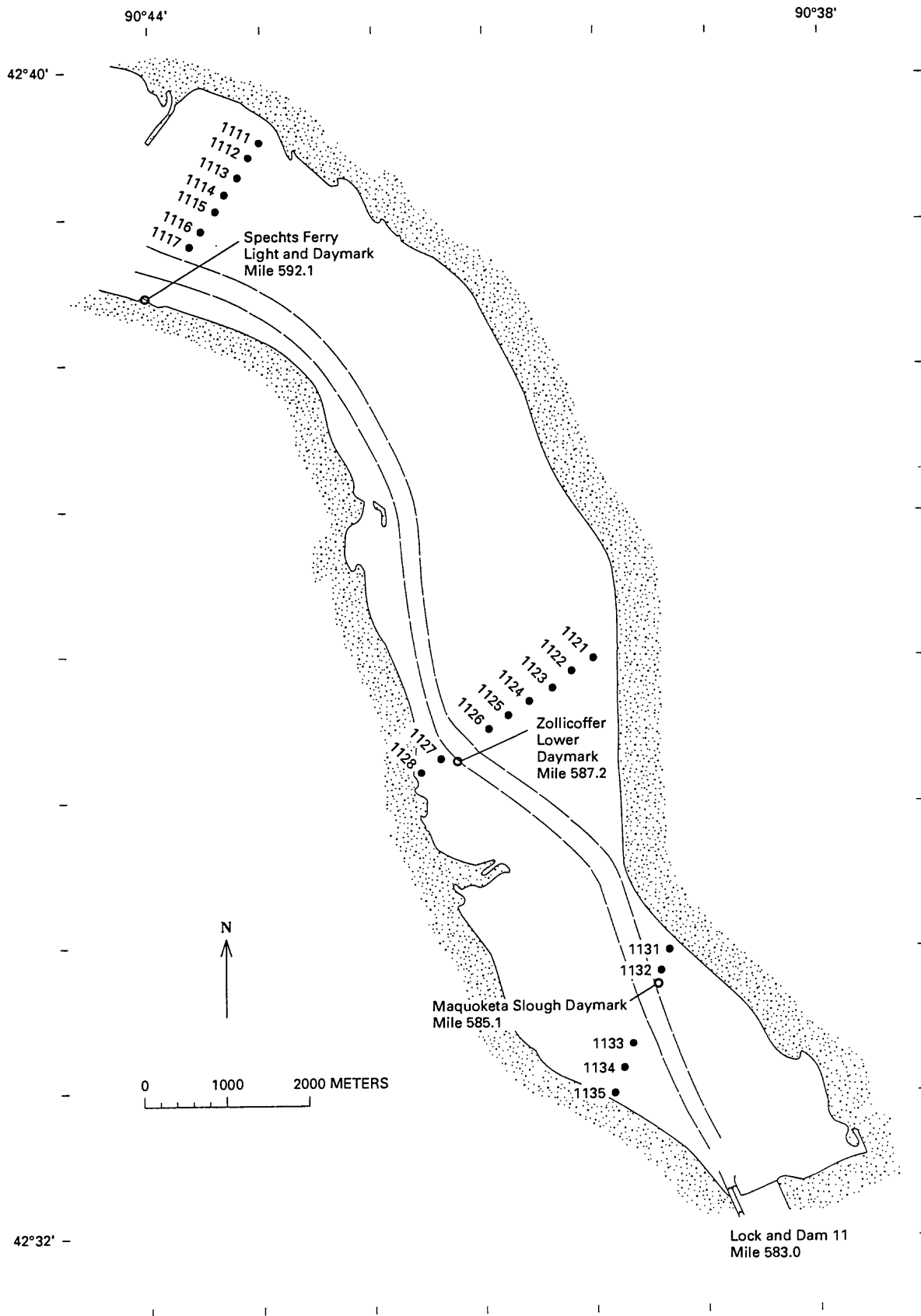
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the dam side wall of the auxiliary lock ($42^{\circ}47.165$ N, $091^{\circ}05.675$ W, NAD27, accuracy ± 25 m). John Sullivan got a navigation beacon fix at this location of $42^{\circ}47.1705$ N, $091^{\circ}05.6856$ W, NAD27, the average of 100 fixes over 4 minutes. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Discharge at Dam 10 (provided by the U.S. Army Corps of Engineers) was about $1,360 \text{ m}^3/\text{s}$.

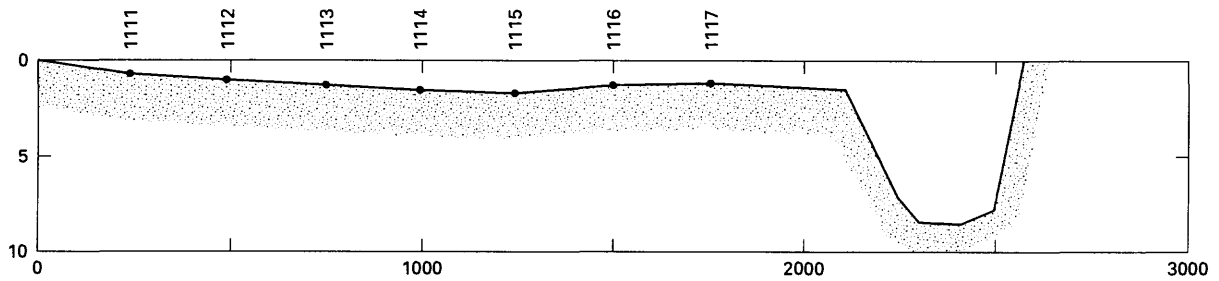
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 168° magnetic

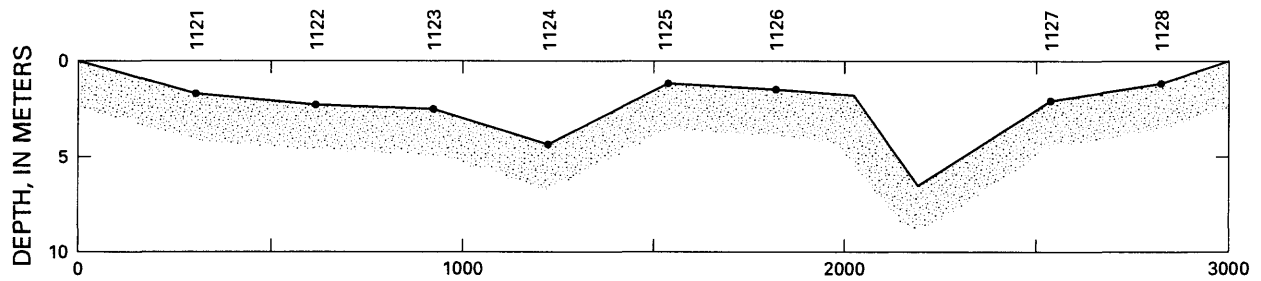
| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------------------|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | | |
| 1041 | $42^{\circ}50.940$ | $091^{\circ}06.101$ | 0.8 | 477 | 26.2 | 3.5 | <0.05 | -- | mud |
| 1042 | 50.770 | 06.062 | 1.2 | 476 | 27.3 | 4.2 | 0.17 | 170 | sand |
| 1043 | 50.582 | 06.021 | 0.8 | 476 | 27.2 | 4.1 | 0.10 | 160 | mud |
| 1044 | 50.394 | 05.975 | 1.1 | 476 | 27.2 | 4.1 | 0.17 | -- | mud |
| 1045 | $42^{\circ}50.211$ | $091^{\circ}05.956$ | 0.9 | 483 | 25.5 | 3.6 | 0.20 | 130 | mud |



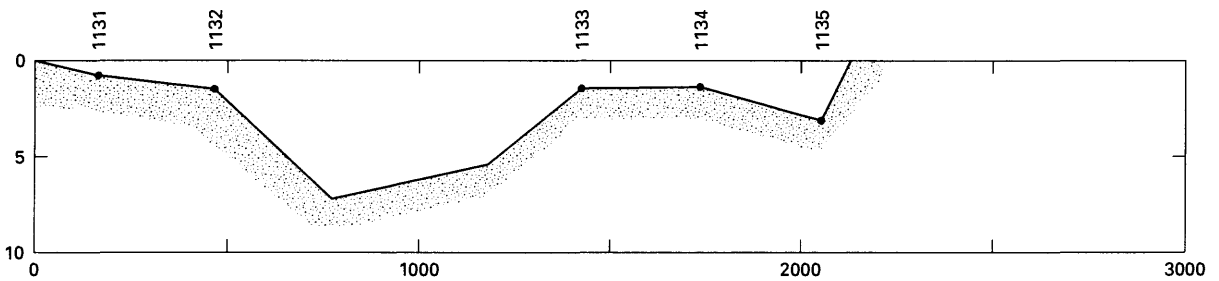
Transect 1 - UMR mile 591.9



Transect 2 - UMR mile 587.4



Transect 3 - UMR mile 585.1



DISTANCE FROM LEFT EDGE OF WATER, IN METERS

STATION: Mississippi River in Pool 11, Transect 1--UMR mile 591.9

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 10 TW: 606.82 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Potosi, Wis.-Iowa

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of a small delta at Spechts Ferry, Iowa ($42^{\circ}38.510$ N, $090^{\circ}44.000$ W, NAD27, accuracy ± 25 m). Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was $1,540 \text{ m}^3/\text{s}$.

DATE: June 21, 1994

GAGE HEIGHT at Dam 11: 603.11 ft

RIVER SLOPE: 22.0×10^{-6}

DATE RATED: 06-25-92

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 034° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissoived oxygen (mg/L) | Veelocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------------------|--------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 1111 | 42°39.522 | 090°42.999 | 0.4 | 540 | 30.3 | 8.5 | 0.05 | 090 | mud |
| 1112 | 39.430 | 43.098 | 0.6 | 431 | 30.8 | 8.8 | 0.12 | 090 | mud |
| 1113 | 39.300 | 43.197 | 1.2 | 423 | 30.2 | 7.7 | 0.13 | 100 | mud, shells |
| 1114 | 39.177 | 43.308 | 1.5 | 421 | 30.1 | 6.8 | 0.15 | 090 | mud |
| 1115 | 39.062 | 43.404 | 1.7 | 422 | 29.9 | 6.2 | 0.17 | 090 | mud, shells |
| 1116 | 38.946 | 43.502 | 1.2 | 424 | 30.1 | 7.4 | 0.08 | 070 | mud, sand |
| 1117 | 38.832 | 43.602 | 1.1 | 428 | 29.8 | 7.2 | 0.16 | 090 | sand |
| 05 | 38.709 | 43.830 | 1.8 | 433 | 29.9 | 5.8 | 0.20 | 100 | -- |
| 04 | 38.630 | 43.863 | 6.7 | 443 | 29.0 | 6.1 | 0.41 | 080 | -- |
| 03 | 38.575 | 43.871 | 8.0 | 444 | 28.8 | 6.0 | 0.52 | 100 | -- |
| 02 | 38.541 | 43.900 | 8.3 | 447 | 28.7 | 5.5 | 0.60 | 100 | -- |
| 01 | 42°38.507 | 090°43.928 | 7.8 | 441 | 29.2 | 5.1 | 0.28 | 110 | -- |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 11, Transect 2--UMR mile 587.4

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 10 TW: 606.82 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Dubuque, Iowa-Wis.-Ill.

DATE: June 22, 1994

GAGE HEIGHT at Dam 11: 603.11 ft

RIVER SLOPE: 22.0×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the outer auxiliary lockwall (42°32.435 N, 090°38.705 W, NAD27, accuracy ± 25 m) at the dam side corner where the wall is widest (upstream from the auxiliary lock gate and downstream from the opening in the lockwall at water level). Biological Resources Division collected a sample at site 1122. Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Tailwater (TW) measured at Dam 10 is for June 21, 1994, so that river slope is not for June 22, but is approximate. Measured discharge was $1,510 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 057° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 1121 | 42°36.013 | 090°40.020 | 1.4 | 435 | 27.3 | 6.7 | 0.19 | 160 | mud, clay |
| 1122 | 35.922 | 40.207 | 2.0 | 443 | 26.7 | 6.2 | 0.17 | 170 | mud, shells |
| 1123 | 35.831 | 40.388 | 2.1 | 449 | 27.3 | 5.3 | 0.22 | 150 | mud, shells |
| 1124 | 35.735 | 40.581 | 4.5 | 449 | 27.3 | 5.2 | 0.28 | 150 | sand |
| 1125 | 35.639 | 40.772 | 0.9 | 453 | 27.6 | 5.5 | 0.10 | 150 | mud, sand |
| 1126 | 35.559 | 40.932 | 1.2 | 455 | 27.2 | 5.8 | 0.12 | 140 | mud |
| 08 | 35.485 | 41.060 | 1.5 | 458 | 27.0 | 5.2 | 0.22 | 160 | -- |
| 09 | 35.435 | 41.149 | 6.5 | 464 | 27.2 | 5.1 | 0.44 | 170 | -- |
| 10 | 35.397 | 41.253 | 4.1 | 470 | 26.8 | 5.0 | 0.26 | 140 | -- |
| 1127 | 35.338 | 41.364 | 1.9 | 459 | 26.8 | 4.4 | 0.23 | 130 | mud |
| 1128 | 42°35.275 | 090°41.529 | 0.9 | 457 | 25.7 | 4.1 | 0.07 | 150 | mud |
| REW | | | 0.0 | | | | | | |

STATION: Mississippi River in Pool 11, Transect 3--UMR mile 585.1

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 10 TW: 606.82 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Dubuque, Iowa-Wis.-Ill.

REMARKS:

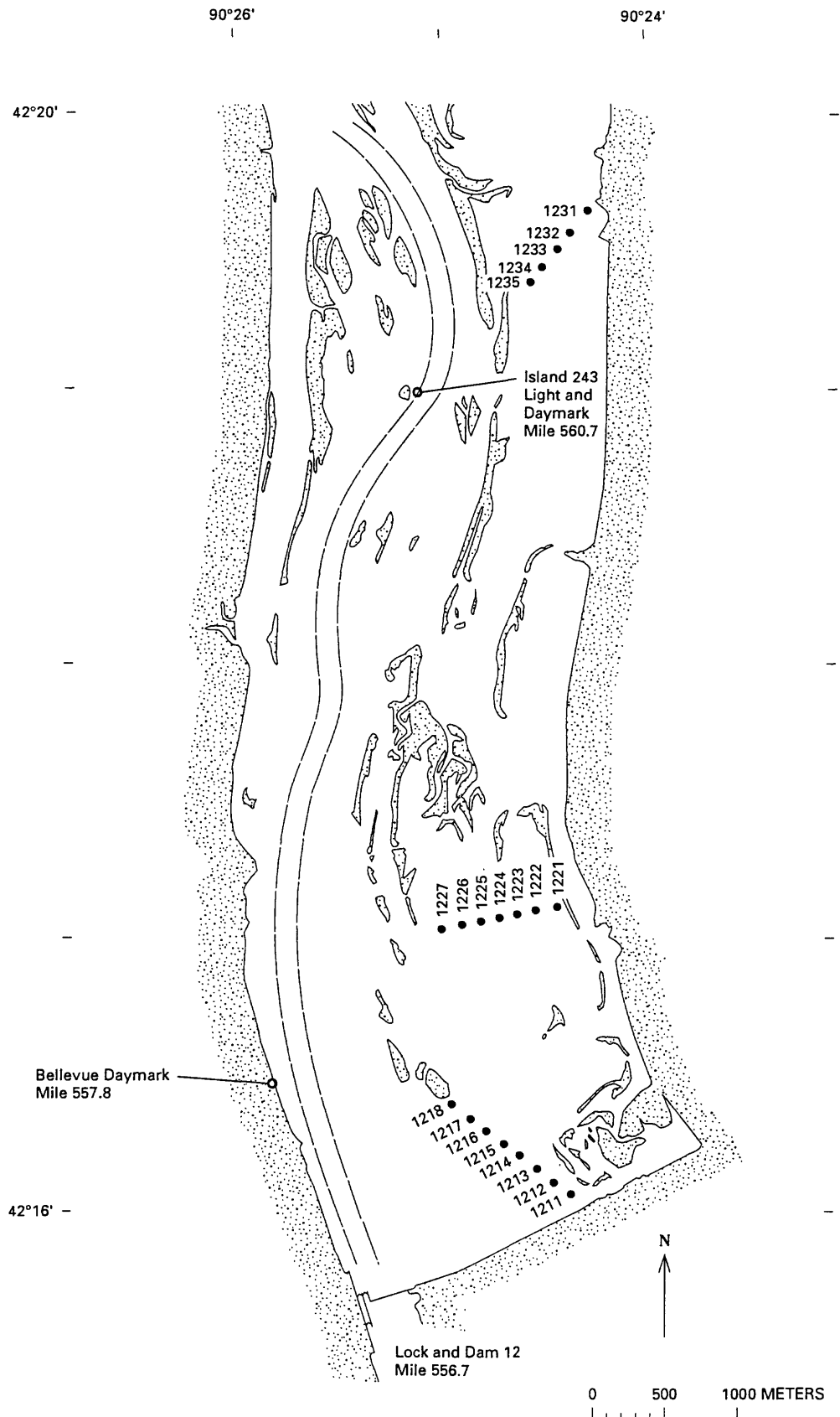
Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located on the outer auxiliary lockwall (42°32.435 N, 090°38.705 W, NAD27, accuracy ± 25 m) at the dam side corner where the wall is widest (upstream from the auxiliary lock gate and downstream from the opening in the lockwall at water level).

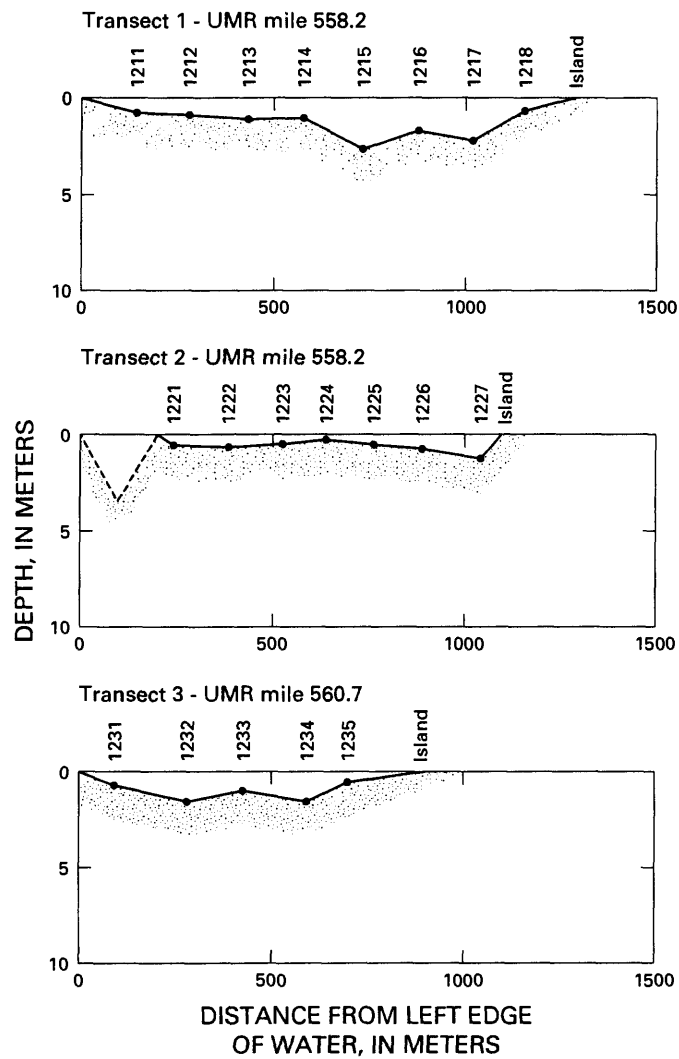
Oxygen was measured by using the Yellow Springs Instrument (Model 57), and the surface specific conductance and temperature were measured by using a LabComp meter. Measured discharge was 1,580 m³/s.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 021° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Dissolved oxygen (mg/L) | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | | |
| LEW | | | 0.0 | | | | | | |
| 1131 | 42°34.059 | 090°39.343 | 0.7 | 452 | 28.5 | 8.0 | 0.14 | 130 | sand |
| 1132 | 33.907 | 39.416 | 1.4 | 453 | 28.4 | 7.6 | 0.19 | 130 | mud, sand |
| 06 | 33.754 | 39.473 | 7.0 | 441 | 28.4 | -- | 0.38 | 140 | -- |
| 07 | 33.542 | 39.518 | 5.0 | 443 | 28.5 | -- | 0.44 | 160 | -- |
| 1133 | 33.421 | 39.660 | 1.4 | 446 | 28.5 | 6.0 | 0.27 | 150 | sand |
| 1134 | 33.267 | 39.734 | 1.2 | 444 | 28.4 | 6.2 | 0.16 | 140 | mud |
| 1135 | 42°33.102 | 090°39.815 | 3.0 | 445 | 28.4 | 6.4 | 0.20 | 120 | mud |
| REW | | | 0.0 | | | | | | |





STATION: Mississippi River in Pool 12, Transect 1--UMR mile 558.2

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 11 TW: 595.10 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Bellevue, Iowa-Ill.

DATE: June 22, 1994

GAGE HEIGHT at Dam 12: 592.08 ft

RIVER SLOPE: 21.8×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the outer auxiliary lockwall ($42^{\circ}15.695$ N, $090^{\circ}25.350$ W, NAD27, accuracy ± 25 m). Autonomous GPS was used to navigate to sites 1211, 1212, and 1213 and used to determine the latitude and longitude at sites 1211 and 1212. Differential/fixed height mode was used to determine the latitude and longitude at site 1213. The surface specific conductance and temperature were measured by using a LabComp meter. Biological Resources Division collected a sample at site 1215.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 126° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| LEW | | | 0.0 | | | | | |
| 1211 | 42°16.07 | 090°24.33 | 0.9 | 450 | 31.7 | <0.05 | -- | mud |
| 1212 | 16.10 | 24.10 | 0.9 | 444 | 30.9 | 0.07 | 130 | mud |
| 1213 | 16.126 | 24.486 | 1.1 | 447 | 30.3 | -- | -- | mud |
| 1214 | 16.201 | 24.578 | 1.0 | 455 | 29.3 | 0.08 | 210 | mud |
| 1215 | 16.239 | 24.667 | 2.1 | 457 | 30.5 | 0.10 | 210 | mud |
| 1216 | 16.288 | 24.754 | 1.7 | 435 | 31.4 | 0.10 | 170 | mud |
| 1217 | 16.329 | 24.822 | 2.0 | 443 | 31.6 | 0.15 | 180 | mud |
| 1218 | 42°16.381 | 090°24.914 | 0.6 | 430 | 33.5 | 0.10 | 190 | mud |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 12, Transect 2--UMR mile 558.2

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 11 TW: 595.10 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Bellevue, Iowa-III.

DATE: June 22, 1994

GAGE HEIGHT at Dam 12: 592.08 ft

RIVER SLOPE: 21.8×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the outer auxiliary lockwall ($42^{\circ}15.695$ N, $090^{\circ}25.350$ W, NAD27, accuracy ± 25 m). The surface specific conductance and temperature were measured by using a LabComp meter. No measurements were made of the velocity at sites 1223 through 1227 because of the shallow water and lack of time.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 079° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|---|--|-------------------|-------------------------------------|---------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| LEW | | | 0.0 | | | | | |
| 1221 | $42^{\circ}17.112$ | $090^{\circ}24.399$ | 0.6 | 425 | 33.4 | 0.09 | 180 | mud |
| 1222 | 17.089 | 24.506 | 0.6 | 424 | 32.2 | 0.12 | 220 | mud |
| 1223 | 17.079 | 24.591 | 0.3 | 427 | 32.7 | -- | -- | mud |
| 1224 | 17.069 | 24.681 | 0.3 | 420 | 33.8 | -- | -- | mud |
| 1225 | 17.054 | 24.770 | 0.4 | 437 | 30.4 | -- | -- | mud, lily pads |
| 1226 | 17.044 | 24.868 | 0.5 | 438 | 29.5 | -- | -- | -- |
| 1227 | $42^{\circ}17.032$ | $090^{\circ}24.966$ | 1.3 | 438 | 30.8 | -- | -- | -- |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 12, Transect 3--UMR mile 560.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 11 TW: 595.10 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Bellevue, Iowa-III.

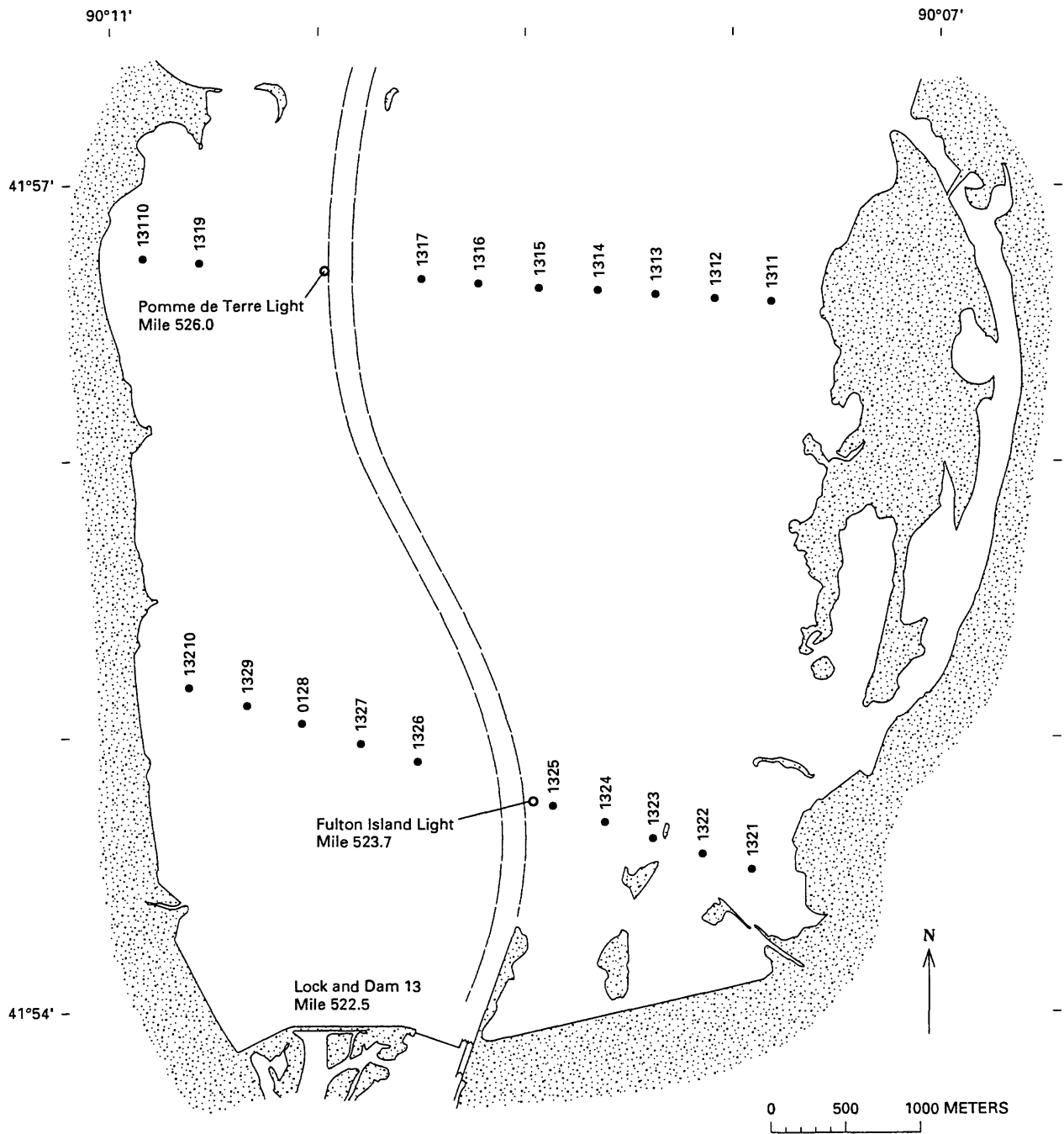
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the tip of the outer auxiliary lockwall ($42^{\circ}15.695$ N, $090^{\circ}25.350$ W, NAD 27, accuracy ± 25 m). The surface specific conductance and temperature were measured by using a LabComp meter.

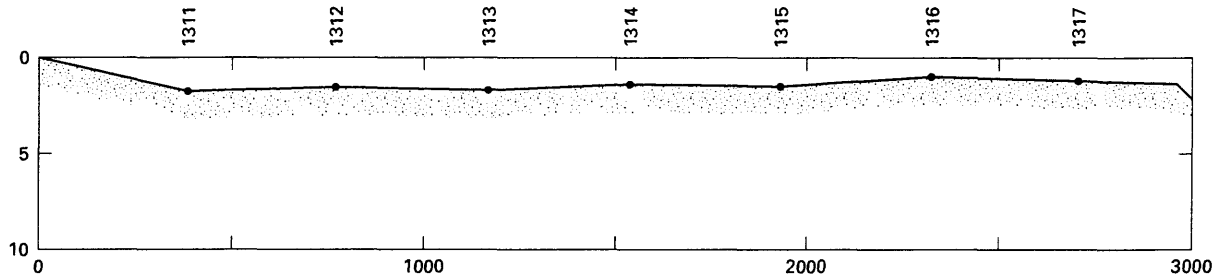
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 039° magnetic

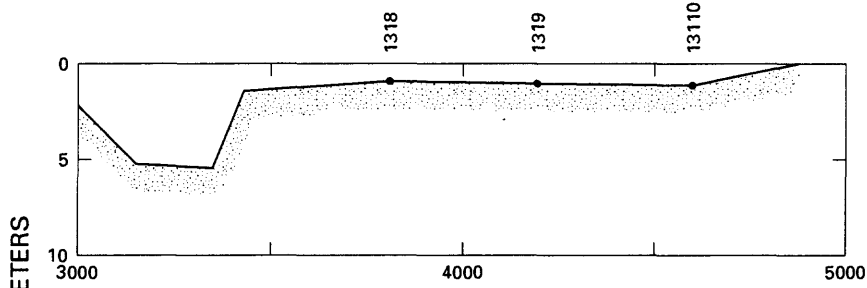
| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|-------------------|--------------------|--------------|--|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| LEW | | | 0.0 | | | | | |
| 1231 | $42^{\circ}19.64$ | $090^{\circ}24.25$ | 0.6 | 496 | 30.5 | <0.05 | -- | mud |
| 1232 | 19.58 | 24.36 | 1.3 | 473 | 29.2 | 0.07 | 150 | mud |
| 1233 | 19.52 | 24.42 | 1.0 | 456 | 30.4 | 0.08 | 170 | mud |
| 1234 | 19.44 | 24.49 | 1.2 | 458 | 31.4 | 0.06 | 170 | mud |
| 1235 | $42^{\circ}19.45$ | $090^{\circ}24.55$ | 0.2 | 435 | 32.9 | <0.05 | -- | mud |
| REW | | | 0.0 | | | | | |



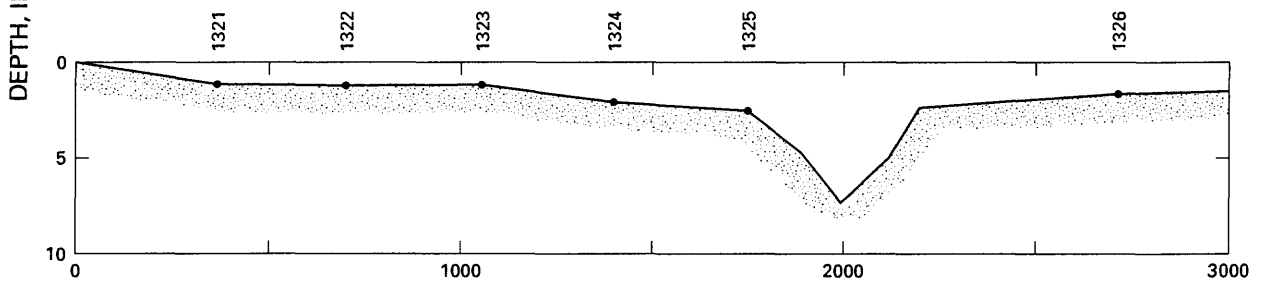
Transect 1 - UMR mile 526.0



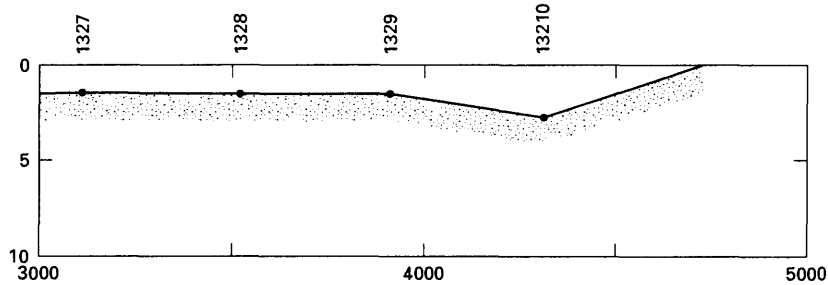
Transect 1 (continued) - UMR mile 526.0



Transect 2 - UMR mile 523.7



Transect 2 (continued) - UMR mile 523.7



DISTANCE FROM LEFT EDGE OF WATER, IN METERS

STATION: Mississippi River in Pool 13, Transect 1--UMR mile 526.0

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 12 TW: 587.42 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Clinton NW, Iowa-III.

DATE: June 23, 1994

GAGE HEIGHT at Dam 13: 583.40 ft

RIVER SLOPE: 22.4×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 10 m because of wind and waves. The GPS reference station was located at the tip of the center lockwall at Lock 13 ($41^{\circ}53.910$ N, $090^{\circ}09.265$ W, NAD27, accuracy ± 25 m). The surface specific conductance and temperature were measured by using a LabComp meter. Wind was from the southeast at 2-7 m/s. Measured discharge was $1,250 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 095° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|-------|--------------------|---------------------|--------------|---|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| LEW | | | 0.0 | | | | | |
| 1311 | $41^{\circ}56.575$ | $090^{\circ}07.808$ | 1.7 | 447 | 25.1 | 0.23 | 230 | mud |
| 1312 | 56.589 | 08.073 | 1.3 | 436 | 24.6 | 0.13 | 230 | mud |
| 1313 | 56.599 | 08.363 | 1.5 | 443 | 25.4 | 0.18 | 220 | mud |
| 1314 | 56.615 | 08.650 | 1.3 | 434 | 24.8 | 0.18 | 240 | mud |
| 1315 | 56.624 | 08.930 | 1.1 | 435 | 25.1 | 0.17 | 200 | sand |
| 1316 | 56.641 | 09.223 | 0.9 | 442 | 26.2 | 0.14 | 260 | sand |
| 1317 | 56.656 | 09.504 | 1.0 | 451 | 25.4 | 0.20 | 210 | sand, mud |
| 09 | 56.660 | 09.701 | 1.9 | 438 | 26.7 | 0.34 | 160 | -- |
| 08 | 56.660 | 09.843 | 5.0 | 448 | 25.8 | 0.42 | 170 | -- |
| 07 | 56.676 | 09.955 | 5.2 | 449 | 25.6 | 0.42 | 170 | -- |
| 06 | 56.687 | 10.044 | 1.2 | 450 | 25.4 | 0.22 | 210 | -- |
| 1318 | 56.708 | 10.291 | 0.8 | 453 | 24.0 | 0.14 | 250 | mud |
| 1319 | 56.723 | 10.576 | 0.8 | 437 | 25.2 | 0.10 | 240 | mud |
| 13110 | $41^{\circ}56.729$ | $090^{\circ}10.857$ | 0.8 | 430 | 24.2 | 0.12 | 240 | mud |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 13, Transect 2--UMR mile 523.7

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 12 TW: 587.42 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Clinton NW, Iowa-III.

DATE: June 23, 1994

GAGE HEIGHT at Dam 13: 583.40 ft

RIVER SLOPE: 22.4×10^{-6}

DATE RATED: 06-25-92

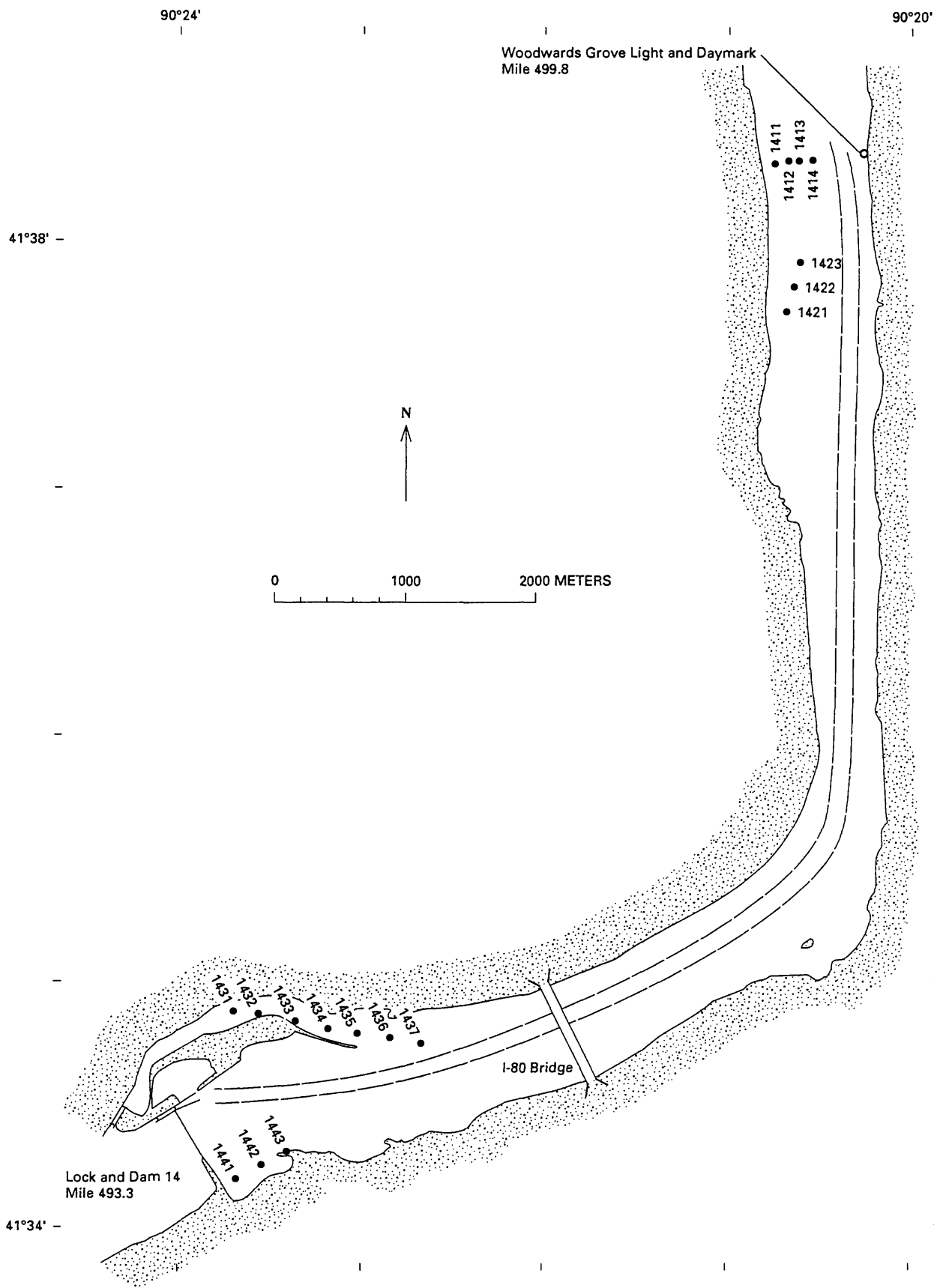
REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 10 m because of wind and waves. The GPS reference station was located at the tip of the center lockwall at Lock 13 ($41^{\circ}53.910$ N, $090^{\circ}09.265$ W, NAD27, accuracy ± 25 m). Biological Resources Division collected a sample at site 1322. The surface specific conductance and temperature were measured by using a LabComp meter. Wind was from the southeast at 2-7 m/s. At sites 1324 and 1325 the boat drifted about 10 to 20 m (probably to the west) after the van Veen grab was collected and before the location was recorded. Measured discharge was $1,290 \text{ m}^3/\text{s}$.

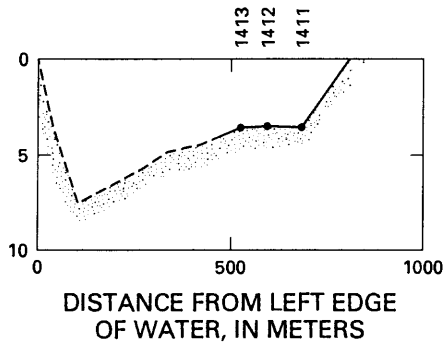
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 107° magnetic

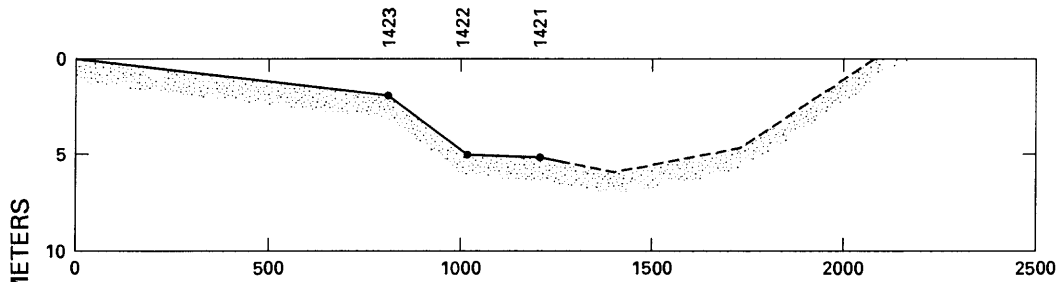
| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|-------|--------------------|---------------------|--------------|---|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| LEW | | | 0.0 | | | | | |
| 1321 | $41^{\circ}54.512$ | $090^{\circ}07.897$ | 1.0 | 339 | 24.8 | <0.05 | -- | mud |
| 1322 | 54.577 | 08.134 | 1.0 | 427 | 23.2 | 0.05 | 150 | mud |
| 1323 | 54.636 | 08.385 | 1.1 | 448 | 24.6 | 0.10 | 200 | sand |
| 1324 | 54.700 | 08.622 | 1.8 | 460 | 25.0 | 0.13 | 200 | mud |
| 1325 | 54.758 | 08.879 | 2.1 | 448 | 24.2 | 0.13 | 180 | mud |
| 04 | 54.774 | 08.908 | 1.9 | 443 | 24.8 | 0.16 | 220 | -- |
| 05 | 54.754 | 08.967 | 4.2 | 445 | 24.4 | 0.22 | 180 | -- |
| 03 | 54.763 | 09.031 | 7.7 | 450 | 25.6 | 0.29 | 150 | -- |
| 02 | 54.794 | 09.112 | 5.1 | 446 | 26.2 | 0.31 | 170 | -- |
| 01 | 54.825 | 09.178 | 2.1 | 451 | 25.7 | 0.28 | 160 | -- |
| 1326 | 54.918 | 09.524 | 1.6 | 459 | 24.8 | 0.16 | 170 | mud |
| 1327 | 54.990 | 09.807 | 1.5 | 452 | 24.5 | 0.19 | 170 | mud, shells |
| 1328 | 55.059 | 10.084 | 1.3 | 448 | 24.8 | 0.22 | 150 | mud |
| 1329 | 55.129 | 10.346 | 1.3 | 448 | 25.0 | 0.21 | 150 | mud |
| 13210 | $41^{\circ}55.201$ | $090^{\circ}10.637$ | 2.3 | 437 | 25.3 | 0.23 | 160 | mud |
| REW | | | 0.0 | | | | | |



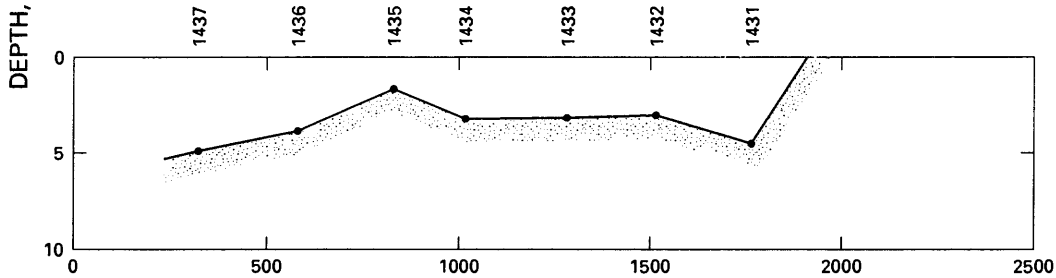
Transect 1 - UMR mile 499.8



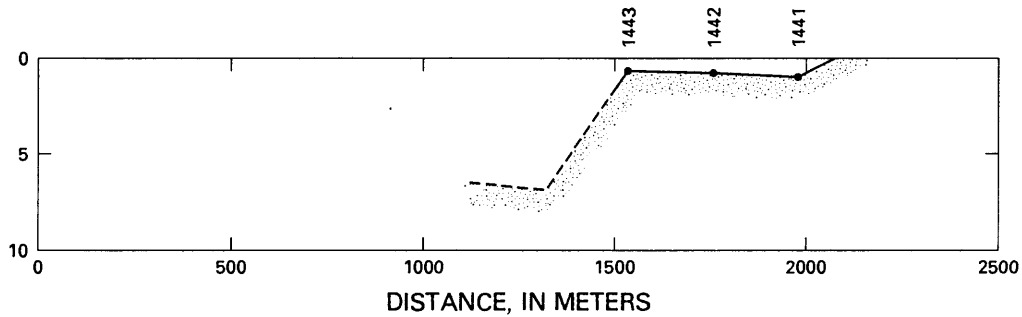
Transect 2 - UMR mile 499.8



Transect 3 - UMR mile 494.8 - LeClaire Canal



Transect 4 - UMR mile 494.8



STATION: Mississippi River in Pool 14, Transect 1 and 2--UMR mile 499.8

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 13 TW: 575.80 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Cordova, Ill.-Iowa

DATE: June 23, 1994

GAGE HEIGHT at Dam 14: 572.24 ft

RIVER SLOPE: 22.5×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS. The error is estimated to be about ± 50 m because of wind and waves. The surface specific conductance and temperature were measured by using a LabComp meter.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT 1: 088° magnetic

BEARING OF TRANSECT 2: 191° magnetic

| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| REW | | | 0.0 | | | | | |
| 1411 | 41°38.30 | 090°20.78 | 3.6 | 462 | 25.8 | 0.29 | 160 | mud |
| 1412 | 38.31 | 20.70 | 3.5 | 440 | 27.5 | 0.34 | 150 | sand |
| 1413 | 38.31 | 20.65 | 3.2 | 443 | 27.6 | 0.27 | 160 | sand |
| 1421 | 37.71 | 20.71 | 5.0 | 457 | 26.2 | 0.38 | 190 | sand |
| 1422 | 37.79 | 20.68 | 5.0 | 446 | 27.3 | 0.36 | 180 | mud, sand |
| 1423 | 41°37.91 | 090°20.64 | 1.9 | 453 | 26.5 | 0.29 | 180 | mud, sand |

STATION: Mississippi River in Pool 14, Transect 3 and 4--UMR mile 494.8

PARTY: Moody, Sullivan, and Writer

GAGE HEIGHT at Dam 13 TW: 576.41 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Silvis, Iowa-III.

DATE: June 24, 1994

GAGE HEIGHT at Dam 14: 572.45 ft

RIVER SLOPE: 25.0×10^{-6}

DATE RATED: 06-25-92

REMARKS:

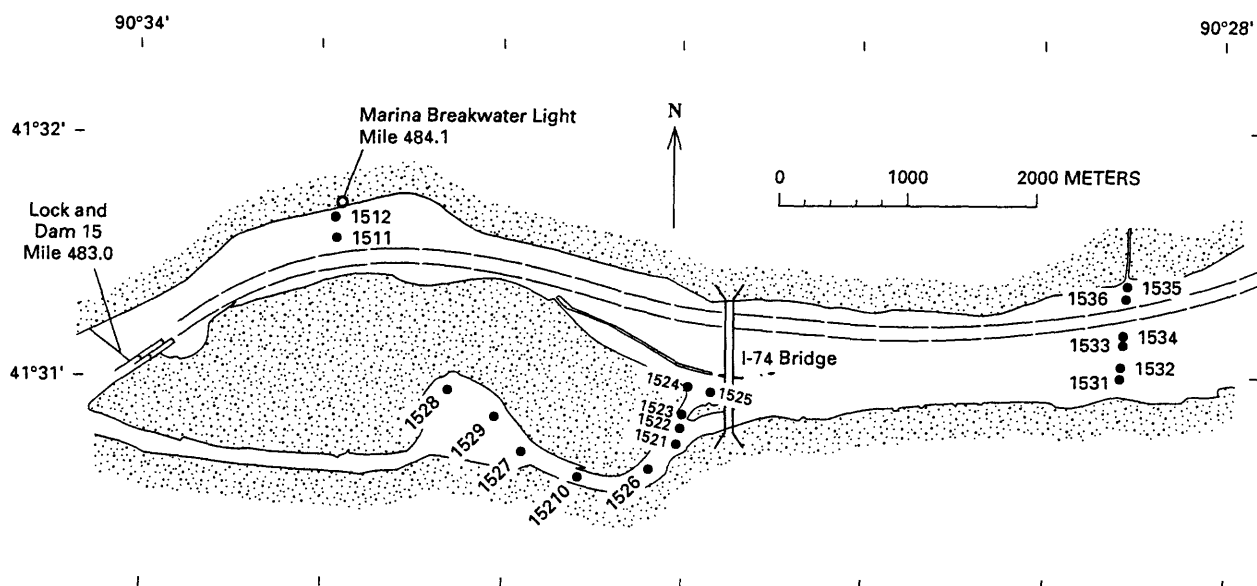
Resampled sites using differential GPS. The error is estimated to be about ± 5 m. The GPS reference station was located at the upstream tip of the dam-side lockwall where the narrower guidewall begins ($41^{\circ}34.480$ N, $090^{\circ}23.955$ W, NAD27, accuracy ± 25 m). The surface specific conductance and temperature were measured by using a LabComp meter. Biological Resources Division collected a sample from site 1433.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

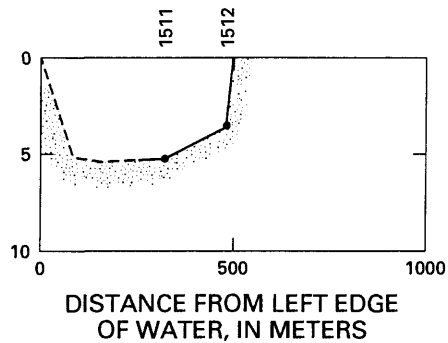
BEARING OF TRANSECT 1: 096° magnetic

BEARING OF TRANSECT 2: 056° magnetic

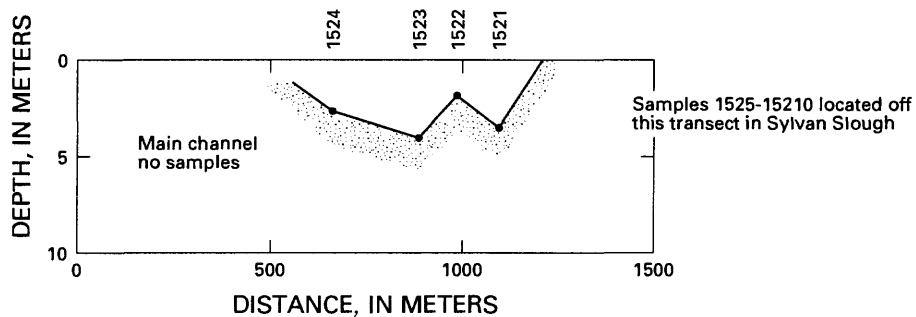
| Site | NAD27 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|--|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| 1431 | $41^{\circ}34.871$ | $090^{\circ}23.681$ | 4.3 | 466 | 24.6 | 0.10 | 130 | mud |
| 1432 | 34.849 | 23.534 | 2.9 | 460 | 26.5 | 0.07 | 110 | sand |
| 1433 | 34.821 | 23.339 | 3.2 | 457 | 26.5 | 0.06 | 140 | mud |
| 1434 | 34.797 | 23.147 | 2.9 | 457 | 25.7 | 0.07 | 120 | mud |
| 1435 | 34.777 | 23.002 | 1.8 | 470 | 25.5 | 0.16 | 260 | mud |
| 1436 | 34.752 | 22.841 | 3.5 | 463 | 25.2 | 0.38 | 240 | sand |
| 1437 | 34.729 | 22.670 | 4.7 | 453 | 25.1 | 0.47 | 260 | sand |
| 1441 | 34.177 | 23.665 | 0.9 | 450 | 23.4 | 0.06 | 120 | mud |
| 1442 | 34.229 | 23.524 | 0.8 | 475 | 24.1 | -- | -- | mud |
| 1443 | $41^{\circ}34.298$ | $090^{\circ}23.395$ | 0.5 | 482 | 24.3 | -- | -- | |



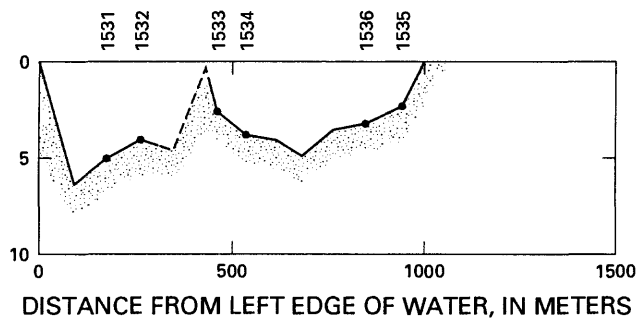
Transect 1 - UMR mile 484.0



Transect 2 - UMR mile 485.8



Transect 3 - UMR mile 487.8



STATION: Mississippi River in Pool 15, Transect 1--UMR mile 484.0

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 14 TW: 563.72 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Davenport East, Iowa-Ill.

DATE: June 26, 1994

GAGE HEIGHT at Dam 15: 561.20 ft

RIVER SLOPE: 47.8×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT 1: 174° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| 1511 | 41°31.570 | 090°32.877 | 5.0 | 444 | 24.7 | 0.71 | 270 | sand |
| 1512 | 41°31.664 | 090°32.863 | 3.5 | 434 | 23.6 | <0.05 | -- | mud |

STATION: Mississippi River in Pool 15, Transect 2--UMR mile 485.8

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 14 TW: 563.72 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Davenport East, Iowa-Ill.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. No grab sample was collected from sites 1522 and 1525. Biological Resources Division collected a sample from site 1529.

DATE: June 26, 1994

GAGE HEIGHT at Dam 15: 561.20 ft

RIVER SLOPE: 47.8×10^{-6}

DATE RATED: 06-25-92

CURRENT METER EQUATION: $V(m/s) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 003° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|---|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| 1521 | 41°30.738 | 090°30.982 | 3.2 | 452 | 24.7 | 0.42 | 210 | mud |
| 1522 | 30.798 | 30.964 | 1.6 | 445 | 25.1 | 0.27 | 230 | shells |
| 1523 | 30.853 | 30.949 | 3.9 | 445 | 25.1 | 0.29 | 200 | mud |
| 1524 | 30.977 | 30.920 | 2.7 | 446 | 25.0 | 0.31 | 280 | mud |
| The following sites were not on the transect, but in the backwater area of Sylvan Slough upstream from Sylvan Island. | | | | | | | | |
| 1525 | 30.948 | 30.790 | 2.3 | 441 | 25.3 | 0.36 | 290 | shells, sand |
| 1526 | 30.633 | 31.112 | 3.5 | 453 | 24.8 | 0.20 | 180 | mud |
| 1527 | 30.702 | 31.837 | 0.8 | 450 | 24.4 | 0.13 | 310 | mud |
| 1528 | 30.946 | 32.249 | 1.1 | 447 | 24.5 | 0.11 | 250 | mud |
| 1529 | 30.837 | 31.989 | 0.5 | 443 | 23.7 | -- | -- | mud |
| 15210 | 41°30.595 | 090°31.526 | 2.0 | 451 | 24.7 | 0.31 | 300 | mud |

STATION: Mississippi River in Pool 15, Transect 3--UMR mile 487.8

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 14 TW: 563.72 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Silvis, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. No grab sample was collected from sites 1532 and 1535.

DATE: June 26, 1994

GAGE HEIGHT at Dam 15: 561.20 ft

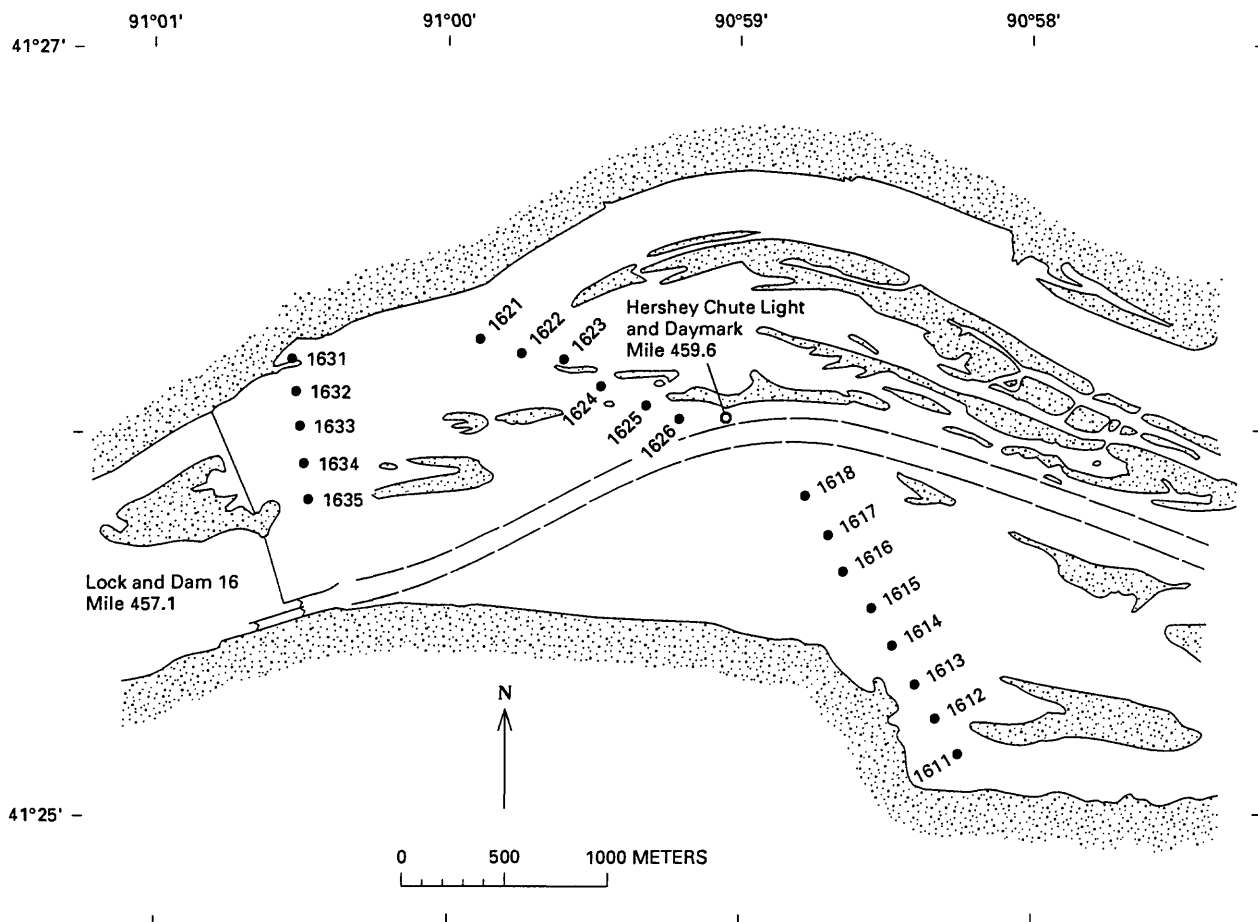
RIVER SLOPE: 47.8×10^{-6}

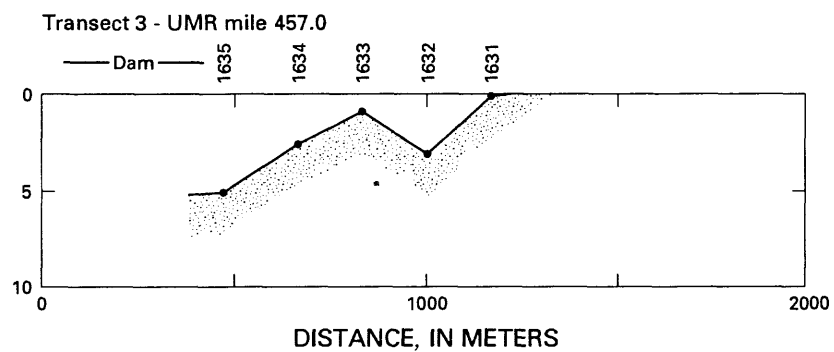
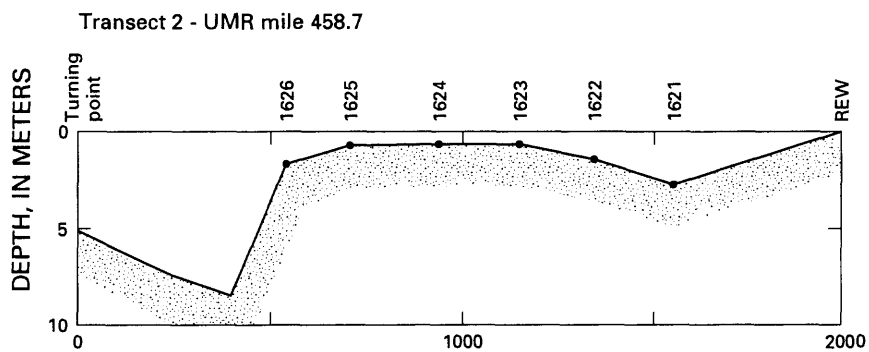
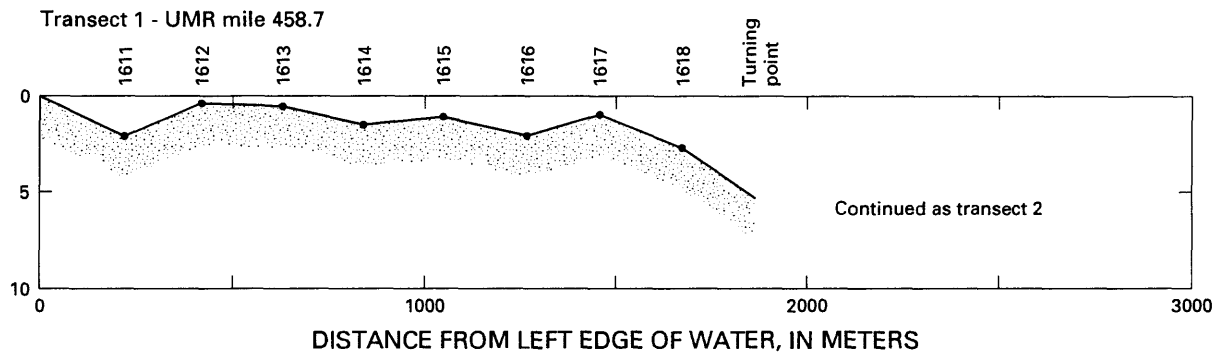
DATE RATED: 06-25-92

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 003° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| 1531 | 41°31.010 | 090°28.537 | 4.7 | 446 | 25.2 | 0.52 | 290 | mud, sand |
| 1532 | 31.062 | 28.527 | 3.5 | 447 | 25.3 | 0.66 | 270 | sand, rocks |
| 1533 | 31.157 | 28.518 | 2.6 | 428 | 26.9 | 0.47 | 270 | mud, sand |
| 1534 | 31.145 | 28.516 | 3.5 | 443 | 25.5 | 0.71 | 260 | sand |
| 1535 | 31.392 | 28.499 | 2.3 | 429 | 27.0 | 0.55 | 240 | sand, rocks |
| 1536 | 41°31.339 | 090°28.496 | 3.3 | 430 | 26.6 | 0.65 | 270 | sand |





STATION: Mississippi River in Pool 16, Transect 1--UMR mile 458.7

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 15 TW: 551.02 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Illinois City, Iowa-Ill.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. Differential GPS was checked by comparing the GPS-derived coordinates for the tip of the guidewall closest to the dam (41°25.588 N, 091°00.456 W, NAD27) with coordinates taken from the Muscatine, Iowa-Ill., quadrangle (41°25.580 N, 091°00.460 W, NAD27). The difference is about 14 m in latitude and 6 m in longitude. The surface specific conductance and temperature were measured by using a LabComp meter. Some stratification was observed in the core samples, with coarser silt on top of finer silt and mud. Biological Resources Division collected a sample at site 1613.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 149° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 1611 | 41°25.151 | 090°58.279 | 1.8 | 508 | 23.9 | 0.51 | 300 | sand |
| 1612 | 25.233 | 58.377 | 0.2 | 507 | 23.8 | 0.16 | 270 | mud |
| 1613 | 25.350 | 58.397 | 0.4 | 496 | 24.5 | 0.45 | 220 | mud, sand |
| 1614 | 25.450 | 58.432 | 1.3 | 497 | 24.3 | 0.60 | 280 | sand |
| 1615 | 25.545 | 58.552 | 1.0 | 500 | 24.2 | 0.28 | 290 | sand |
| 1616 | 25.634 | 58.651 | 2.2 | 489 | 24.5 | 0.78 | 250 | sand, peloids |
| 1617 | 25.731 | 58.703 | 0.5 | 492 | 24.5 | 0.25 | 300 | mud |
| 1618 | 41°25.832 | 090°58.788 | 2.5 | 463 | 24.9 | 0.65 | 290 | mud |

STATION: Mississippi River in Pool 16, Transect 2--UMR mile 458.7

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 15 TW: 551.02 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Illinois City, Iowa-III.

DATE: June 27, 1994

GAGE HEIGHT at Dam 16: 544.49 ft

RIVER SLOPE: 47.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. Differential GPS was checked by comparing the GPS-derived coordinates for the tip of the guidewall closest to the dam ($41^{\circ}25.588$ N, $091^{\circ}00.456$ W, NAD83) with coordinates taken from the Muscatine, Iowa-III. quadrangle ($41^{\circ}25.580$ N, $091^{\circ}00.460$ W, NAD27). The difference is about 14 m in latitude and 6 m in longitude.

Several sites could not be resampled because locations were on land, resulting from a 0.3-m lower pool elevation and perhaps deposition of sediment along the downstream edges of islands by the flood of 1993. Site 1621 was sampled 60 m south, site 1622 was sampled 39 m south and 31 m west; site 1623 was sampled 44 m south and 16 m east; and site 1624 was sampled 17 m south of the original sampling sites. In pools farther downstream, if the site was out of water, it was sampled out of water at the original location.

The surface specific conductance and temperature were measured by using a LabComp meter. A lot of mud was stirred up trying to reach site 1623, which may have affected the specific conductance. Some stratification was observed in the core samples, with coarser silt on top of finer silt and mud.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 112° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^{\circ}$ magnetic) | Surficial bed sediment |
|------|--------------------|---------------------|--------------|--|--|-------------------|-------------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^{\circ}\text{C}$) | | | |
| REW | | | 0.0 | | | | | |
| 1621 | $41^{\circ}26.202$ | $090^{\circ}59.898$ | 2.3 | 432 | 27.0 | 0.49 | 220 | mud |
| 1622 | 26.174 | 59.792 | 1.3 | 437 | 27.1 | 0.35 | 240 | mud |
| 1623 | 26.131 | 59.636 | 0.2 | 504 | 27.4 | 0.11 | 280 | mud |
| 1624 | 26.106 | 59.490 | 0.2 | 439 | 26.5 | -- | -- | mud |
| 1625 | 26.066 | 59.329 | 0.3 | 443 | 25.6 | 0.18 | 270 | mud |
| 1626 | $41^{\circ}26.048$ | $090^{\circ}59.218$ | 1.3 | 445 | 25.6 | 0.24 | 270 | mud |

STATION: Mississippi River in Pool 16, Transect 3--UMR mile 457.0

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 15 TW: 551.02 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Muscatine, Iowa-III.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. Differential GPS was checked by comparing the GPS-derived coordinates for the tip of the guidewall closest to the dam (41°25.588 N, 091°00.456 W, NAD83) with coordinates taken from the Muscatine, Iowa-III., quadrangle (41°25.588 N, 091°00.460 W, NAD 83). The difference is about 14 m in latitude and 6 m in longitude.

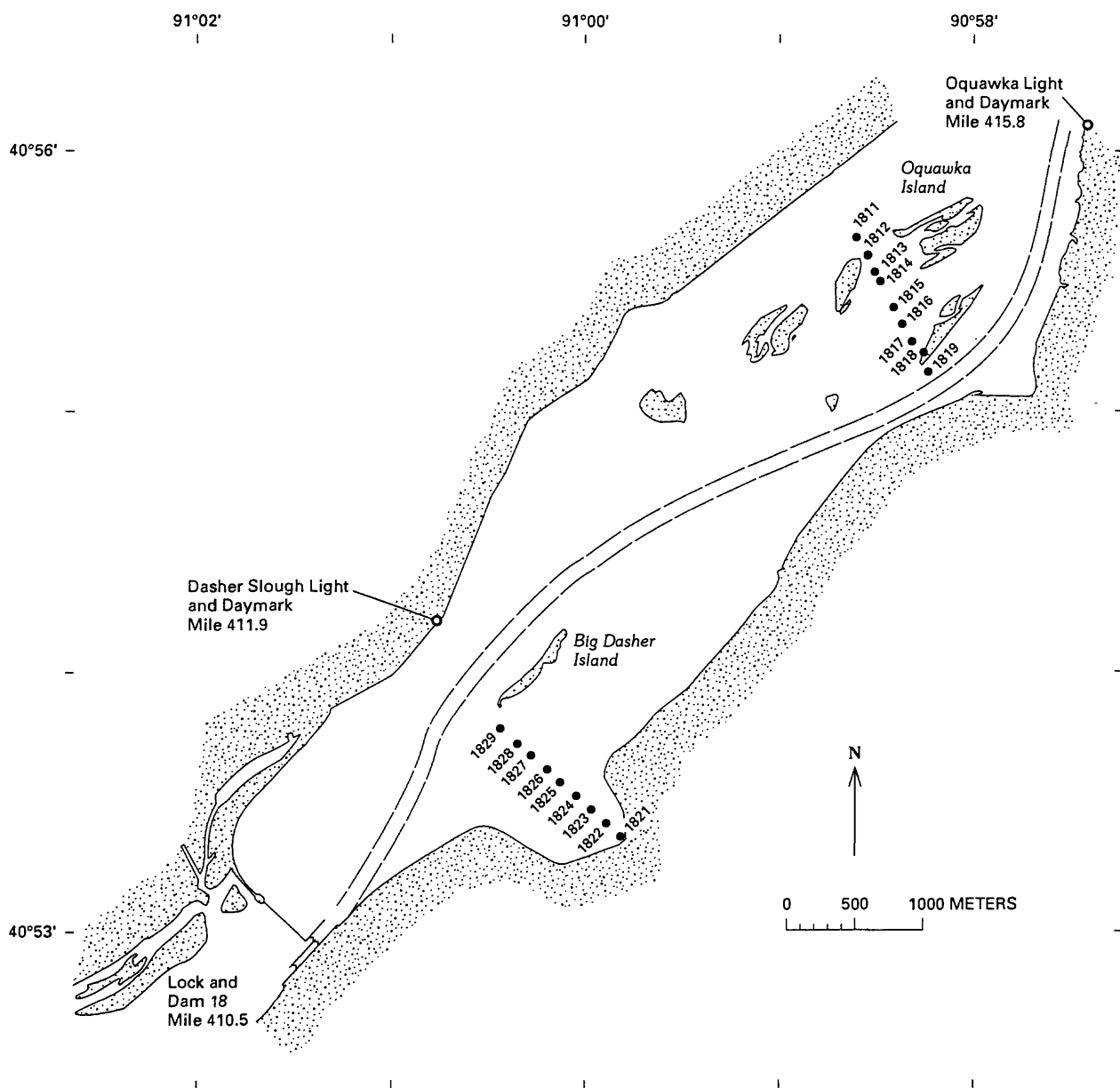
Several sites could not be resampled because locations were on land, resulting from a 0.3 m-lower pool elevation and perhaps deposition of sediment along the downstream edges of islands by the flood of 1993. Site 1631 was sampled 44 m east of original sampling site.

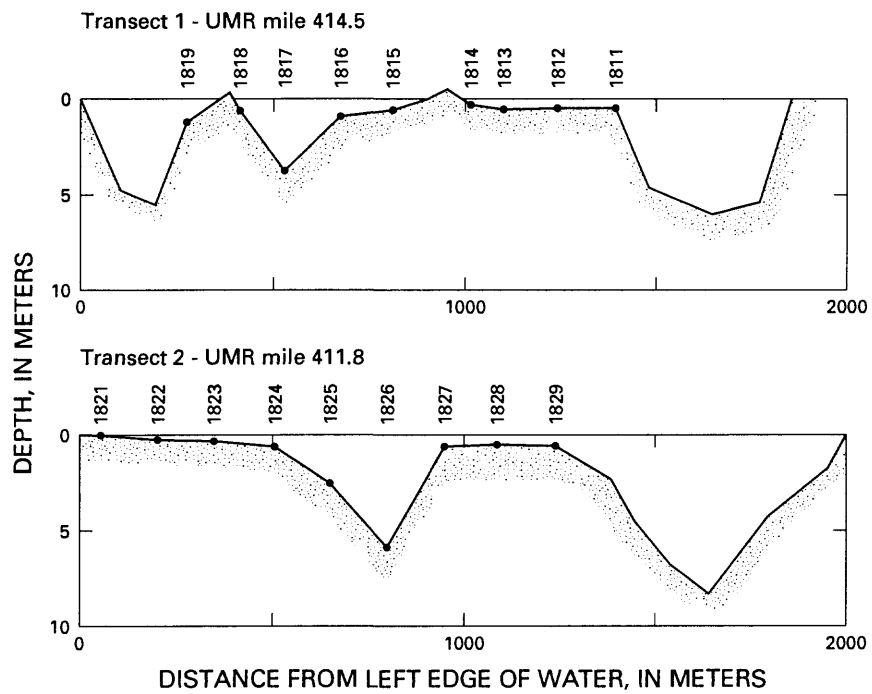
The surface specific conductance and temperature were measured by using a LabComp meter.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 173° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| REW | | | 0.0 | | | | | |
| 1631 | 41°26.182 | 091°00.538 | 0.2 | 454 | 28.4 | -- | -- | mud |
| 1632 | 26.099 | 00.553 | 3.0 | 437 | 26.4 | 0.55 | 220 | sand |
| 1633 | 26.002 | 00.534 | 0.7 | 436 | 26.8 | 0.22 | 180 | mud |
| 1634 | 25.910 | 00.526 | 2.5 | 432 | 27.2 | 0.37 | 200 | mud |
| 1635 | 41°25.817 | 090°00.513 | 5.0 | 433 | 27.2 | 0.73 | 200 | sand |





STATION: Mississippi River in Pool 18, Transect 1--UMR mile 414.5

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 17 TW: 535.19 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Oquawka, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on April 22, 1992, when the pool was first sampled, and 3.8 m lower than the maximum 1993 flood elevation. Some deposition may have occurred between sites 1811 and 1812 because there was land between the two sites in 1994 where there was water in 1992. Site 1812 was sampled 60 m south and 33 m east, site 1813 was sampled 10 m northwest, site 1814 was sampled 33 m east, and site 1818 was sampled 26 m east of the original sampling site. Measured discharge was $2,720 \text{ m}^3/\text{s}$.

DATE: June 28, 1994

GAGE HEIGHT at Dam 18: 527.75 ft

RIVER SLOPE: 54.2×10^{-6}

DATE RATED: 06-25-92

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 149° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|--------|---------------|----------------|--------------|---|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| LEW | 40°55.029 | 090°58.149 | 0.0 | 457 | 26.0 | 0.00 | -- | -- |
| 08 | 55.047 | 58.185 | 4.6 | 459 | 25.7 | 0.69 | 220 | -- |
| 09 | 55.095 | 58.212 | 5.5 | 461 | 25.6 | 0.76 | 220 | -- |
| 1819 | 55.148 | 58.240 | 2.0 | 460 | 25.9 | 0.40 | 210 | sand |
| Island | | | | | | | | |
| 1818 | 55.201 | 58.298 | 0.3 | 455 | 27.4 | 0.08 | 270 | mud |
| 1817 | 55.269 | 58.331 | 2.5 | 456 | 26.0 | 0.68 | 210 | sand |
| 1816 | 55.333 | 58.376 | 4.3 | 444 | 26.9 | 0.71 | 210 | sand |
| 1815 | 55.399 | 58.423 | 0.8 | 446 | 26.8 | 0.31 | 200 | muddy sand |
| Island | | | | | | | | |
| 1814 | 55.502 | 58.519 | 0.1 | 426 | 31.6 | <0.05 | -- | mud |
| 1813 | 55.545 | 58.527 | 0.2 | 445 | 29.6 | <0.05 | -- | mud |
| 1812 | 55.572 | 58.552 | 0.2 | 428 | 30.6 | <0.05 | -- | sandy mud |
| Island | | | | | | | | |
| 1811 | 55.666 | 58.610 | 0.7 | 439 | 28.5 | 0.25 | 210 | mud |
| 10 | 55.711 | 58.683 | 4.4 | 420 | 29.0 | 0.64 | 230 | -- |
| 11 | 55.781 | 58.750 | 6.0 | 434 | -- | 0.76 | 230 | -- |
| 12 | 40°55.843 | 090°58.799 | 5.3 | 430 | 28.5 | 0.54 | 230 | -- |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 18, Transect 2--UMR mile 411.8

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 17 TW: 535.19 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Oquawka, Ill.-Iowa

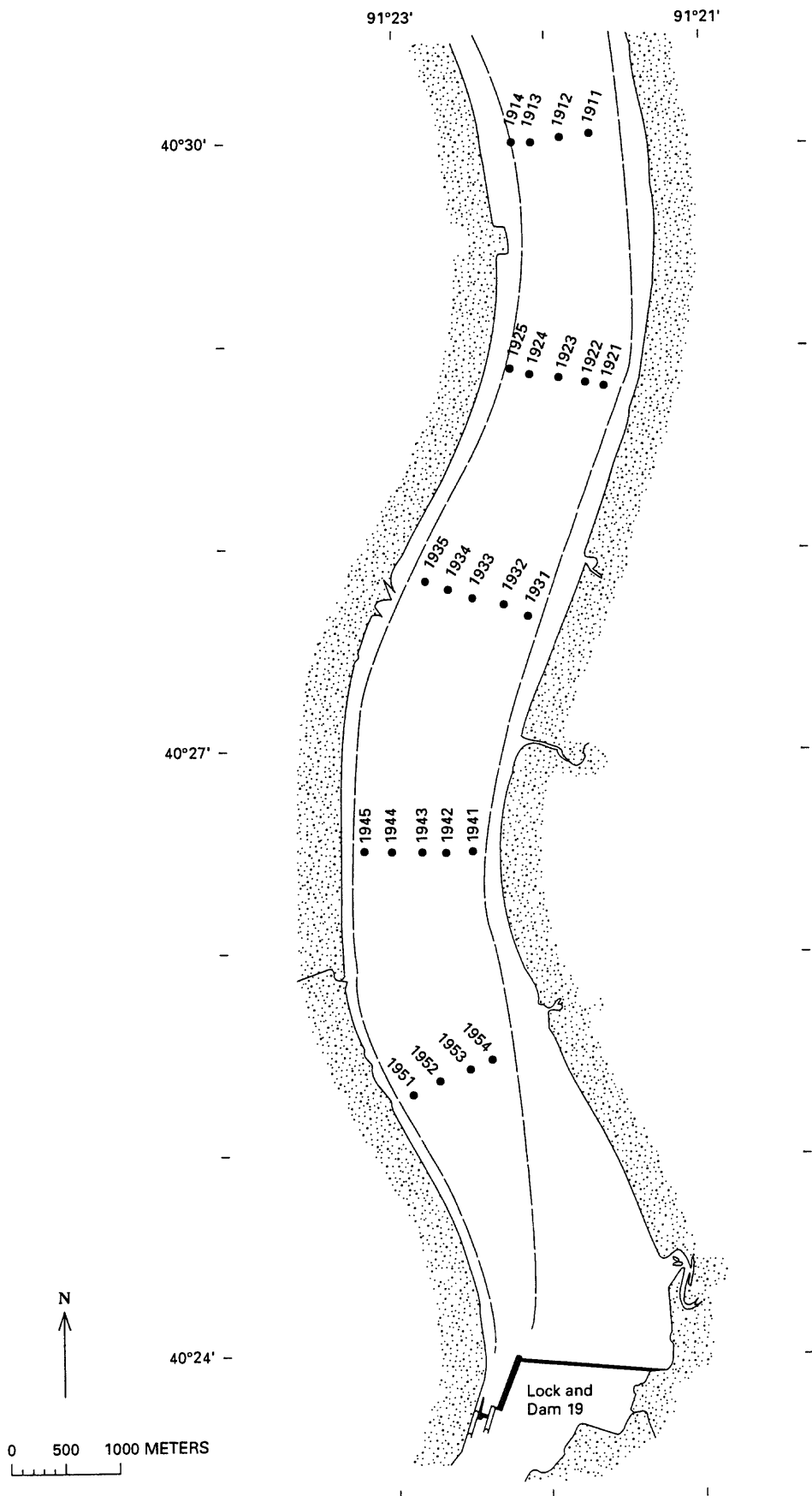
REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on April 22, 1992, when the pool was first sampled, and 3.8 m lower than the maximum 1993 flood elevation. Some deposition may have occurred between sites 1821 and 1823 because the water was too shallow to get to site 1821, and site 1822 was resampled 75 m north and 36 m west of the original site. Measured discharge was 2,720 m³/s. Biological Resources Division collected a sample from site 1823.

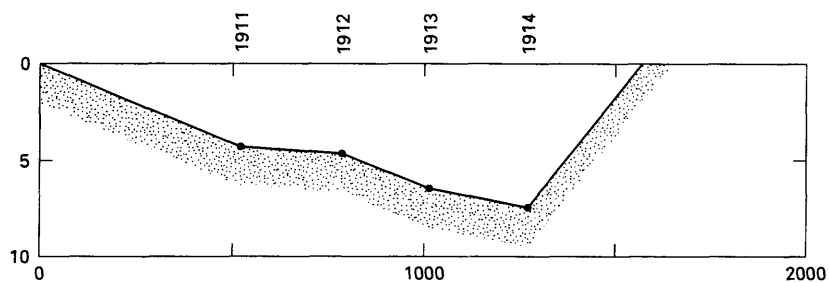
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 129° magnetic

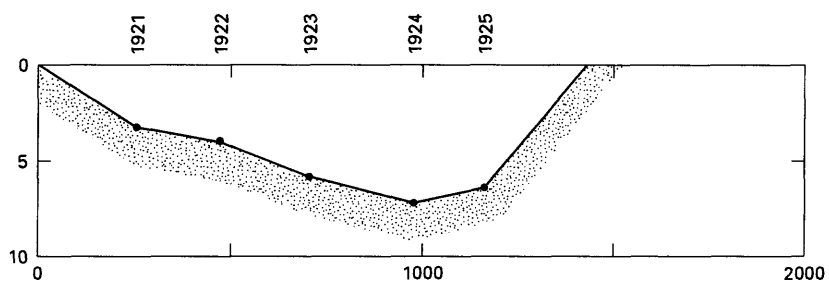
| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|--|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 1821 | Could not reach this site because the water was less than 0.1 m deep | | | | | | | |
| 1822 | 40°53.445 | 090°59.926 | 0.1 | 460 | 22.5 | <0.05 | -- | mud |
| 1823 | 53.458 | 59.972 | 0.2 | 462 | 23.7 | <0.05 | -- | mud |
| 1824 | 53.509 | 091°00.059 | 0.4 | 464 | 24.3 | 0.08 | 010 | mud |
| 1825 | 53.564 | 00.150 | 2.1 | 465 | 24.3 | 0.21 | 240 | mud |
| 1826 | 53.607 | 00.222 | 5.9 | 463 | 25.1 | 0.59 | 210 | sand |
| 1827 | 53.665 | 00.300 | 0.6 | 462 | 24.7 | 0.10 | 130 | mud |
| 1828 | 53.715 | 00.374 | 0.6 | 468 | 24.8 | 0.11 | 130 | mud |
| 1829 | 53.770 | 00.461 | 0.6 | 465 | 24.9 | 0.21 | 120 | mud |
| 01 | 53.824 | 00.535 | 1.7 | 467 | 24.8 | 0.31 | 180 | mud |
| 02 | 53.858 | 00.582 | 4.8 | 467 | 24.9 | 0.64 | 190 | -- |
| 03 | 53.894 | 00.645 | 7.2 | 461 | 25.1 | 0.71 | 210 | -- |
| 04 | 53.931 | 00.691 | 8.3 | 455 | 25.2 | 0.62 | 210 | -- |
| 05 | 53.947 | 00.721 | 6.3 | 453 | 25.2 | 0.67 | 210 | -- |
| 06 | 53.975 | 00.763 | 4.3 | 454 | 25.4 | 0.76 | 200 | -- |
| 07 | 40°54.046 | 091°00.848 | 1.3 | 454 | 25.4 | 0.35 | 200 | -- |
| REW | | | 0.0 | | | | | |



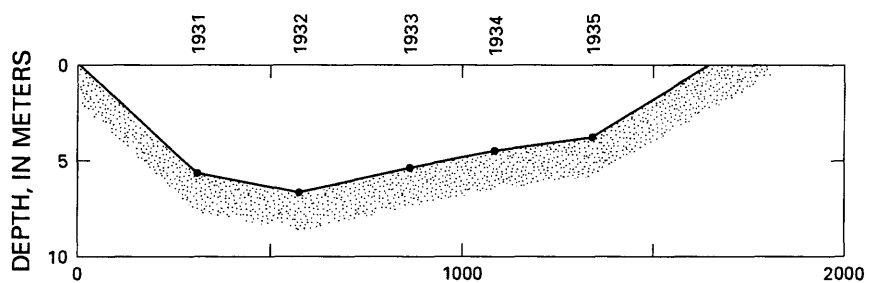
Transect 1 - UMR mile 371.6



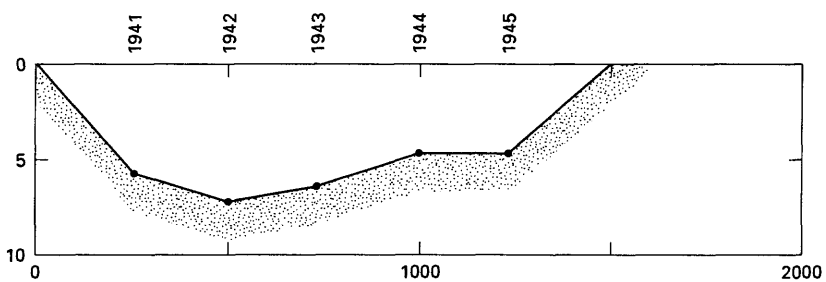
Transect 2 - UMR mile 370.2



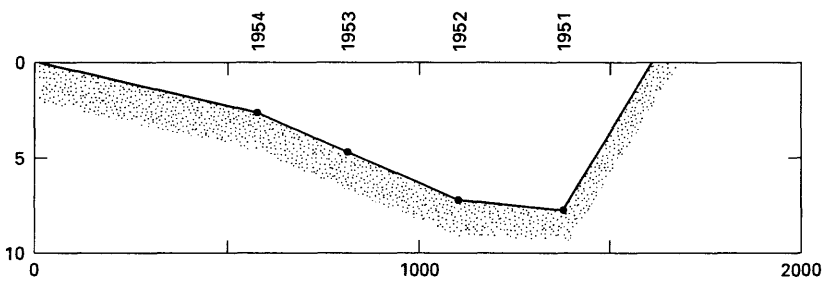
Transect 3 - UMR mile 368.9



Transect 4 - UMR mile 367.5



Transect 5 - UMR mile 366.3



DISTANCE FROM LEFT EDGE OF WATER, IN METERS

STATION: Mississippi River in Pool 19, Transect 1--UMR mile 371.6

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 18 TW: 523.52 ft

SUSPENSION: na

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Niota, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. Sites were resampled within 50 m of the original locations. The surface specific conductance and temperature were measured by using a LabComp meter. No grab sample was collected at site 1914.

DATE: June 29, 1994

GAGE HEIGHT at Dam 19: 518.14 ft

RIVER SLOPE: 21.7×10^{-6}

DATE RATED: 06-25-92

BEARING OF TRANSECT: 079° magnetic

| Site | Replicate | NAD83 | | Depth (m) | Surface | | Surficial bed sediment |
|------|-----------|-----------|------------|--------------|-----------------------------|-------------|---------------------------|
| | | Latitude | Longitude | | Conductance | Temperature | |
| | | N | W | | ($\mu\text{S}/\text{cm}$) | (°C) | |
| LEW | | | | 0.0 | | | -- |
| 1911 | 1 | 40°30.075 | 091°22.872 | 4.2 | -- | 23.4 | -- |
| | 2 | 29.889 | 22.639 | 4.1 | 453 | 23.9 | -- |
| 1912 | 1 | 30.040 | 21.931 | 4.9 | 457 | 24.8 | -- |
| | 2 | 29.950 | 22.843 | 4.0 | 455 | 25.1 | -- |
| 1913 | 1 | 30.028 | 22.105 | 7.0 | 451 | 25.1 | mud |
| | 2 | 29.843 | 21.940 | 5.9 | 453 | 25.3 | mud |
| 1914 | 1 | 30.013 | 22.219 | 7.3 | 443 | 25.1 | sand |
| | 2 | 40°29.784 | 091°22.101 | 7.3 | -- | -- | rocks |
| REW | | | | 0.0 | | | |

STATION: Mississippi River in Pool 19, Transect 2--UMR mile 370.2

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 18 TW: 523.52 ft

SUSPENSION: na

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangle is Hamilton, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. Sites were resampled within 60 m of the original locations. The surface specific conductance and temperature were measured by using a LabComp meter.

DATE: June 29, 1994

GAGE HEIGHT at Dam 19: 518.14 ft

RIVER SLOPE: 21.7×10^{-6}

DATE RATED: 06-25-92

BEARING OF TRANSECT: 094° magnetic

| Site | Replicate | NAD83 | | Depth (m) | Surface | | Surficial bed sediment |
|------|-----------|---------------|----------------|--------------|--|---------------------|---------------------------|
| | | Latitude N | Longitude W | | Conductance ($\mu\text{S}/\text{cm}$) | Temperature (°C) | |
| LEW | | | | 0.0 | | | -- |
| 1921 | 1 | 40°28.835 | 091°21.594 | 3.1 | 453 | 25.4 | -- |
| | 2 | 28.765 | 21.628 | 3.4 | 453 | 25.7 | -- |
| 1922 | 1 | 28.837 | 21.763 | 4.2 | 455 | 25.3 | -- |
| | 2 | 28.738 | 21.730 | 3.7 | 453 | 25.4 | -- |
| 1923 | 1 | 28.870 | 21.901 | 6.6 | 452 | 25.5 | -- |
| | 2 | 28.683 | 21.811 | 4.5 | 452 | 25.7 | -- |
| 1924 | 1 | 28.889 | 22.153 | 6.8 | 447 | 25.3 | -- |
| | 2 | 28.778 | 22.110 | 6.9 | 446 | 25.6 | -- |
| 1925 | 1 | 28.908 | 22.213 | 6.3 | 440 | 25.6 | mud, sand |
| | 2 | 40°28.704 | 091°22.197 | 6.4 | 445 | 25.4 | mud, sand |
| REW | | | | 0.0 | | | |

STATION: Mississippi River in Pool 19, Transect 3--UMR mile 368.9

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 18 TW: 523.52 ft

SUSPENSION: na

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangles are Keokuk, Iowa-Mo.-Ill. and Hamilton, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. Sites were resampled within 60 m of the original locations. The surface specific conductance and temperature were measured by using a LabComp meter.

DATE: June 29, 1994

GAGE HEIGHT at Dam 19: 518.14 ft

RIVER SLOPE: 21.7×10^{-6}

DATE RATED: 06-25-92

BEARING OF TRANSECT: 102° magnetic

| Site | Replicate | NAD83 | | Depth (m) | Surface | | Surficial bed sediment |
|------|-----------|---------------|----------------|--------------|--|---------------------|---------------------------|
| | | Latitude N | Longitude W | | Conductance ($\mu\text{S}/\text{cm}$) | Temperature (°C) | |
| LEW | | | | 0.0 | | | -- |
| 1931 | 1 | 40°27.719 | 091°22.108 | 5.1 | 454 | 25.9 | mud |
| | 2 | 27.706 | 22.143 | 5.5 | 454 | 25.6 | -- |
| 1932 | 1 | 27.758 | 22.285 | 7.0 | 453 | 25.7 | -- |
| | 2 | 27.598 | 22.241 | 6.3 | 454 | 25.4 | -- |
| 1933 | 1 | 27.752 | 22.476 | 5.3 | 448 | 25.5 | sand |
| | 2 | 27.650 | 22.438 | 5.9 | 451 | 25.3 | sand |
| 1934 | 1 | 27.829 | 22.656 | 4.5 | 444 | 25.1 | mud |
| | 2 | 27.745 | 22.603 | 4.9 | -- | -- | -- |
| 1935 | 1 | 27.870 | 22.794 | 3.6 | 442 | 25.3 | -- |
| | 2 | 40°27.782 | 091°22.751 | 4.3 | -- | -- | -- |
| REW | | | | 0.0 | | | |

STATION: Mississippi River in Pool 19, Transect 4--UMR mile 367.5

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 18 TW: 523.52 ft

SUSPENSION: na

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangles are Keokuk, Iowa-Mo.-Ill., and Hamilton, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. Sites were resampled within 30 m of the original locations. The surface specific conductance and temperature were measured by using a LabComp meter.

DATE: June 29, 1994

GAGE HEIGHT at Dam 19: 518.14 ft

RIVER SLOPE: 21.7×10^{-6}

DATE RATED: 06-25-92

BEARING OF TRANSECT: 086° magnetic

| Site | Replicate | NAD83 | | Depth (m) | Surface | | Surficial bed sediment |
|------|-----------|---------------|----------------|--------------|--|---------------------|---------------------------|
| | | Latitude N | Longitude W | | Conductance ($\mu\text{S}/\text{cm}$) | Temperature (°C) | |
| LEW | | | | 0.0 | | | -- |
| 1941 | 1 | 40°26.528 | 091°22.491 | 5.5 | 455 | 25.3 | -- |
| | 2 | 26.415 | 22.541 | 6.0 | 453 | 25.3 | -- |
| 1942 | 1 | 26.522 | 22.649 | 7.0 | 455 | 25.4 | -- |
| | 2 | 26.418 | 22.666 | 6.9 | 454 | 25.3 | -- |
| 1943 | 1 | 26.510 | 22.810 | 5.2 | 449 | 25.3 | -- |
| | 2 | 26.318 | 22.739 | 7.5 | 453 | 25.3 | -- |
| 1944 | 1 | 26.514 | 23.000 | 3.8 | 449 | 25.2 | -- |
| | 2 | 26.382 | 22.901 | 4.7 | -- | -- | -- |
| 1945 | 1 | 26.524 | 23.179 | 4.9 | 445 | 25.4 | -- |
| | 2 | 40°26.410 | 091°23.130 | 3.9 | -- | -- | -- |
| REW | | | | 0.0 | | | |

STATION: Mississippi River in Pool 19, Transect 5--UMR mile 366.3

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 18 TW: 523.52 ft

SUSPENSION: na

CURRENT METER No: na

MAP: USGS 7.5-minute quadrangles are Keokuk, Iowa-Mo.-Ill., and Hamilton, Ill.-Iowa

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. Sites were resampled within 30 m of the original locations. The surface specific conductance and temperature were measured by using a LabComp meter. Biological Resources Division collected a sample from site 1951.

DATE: June 29, 1994

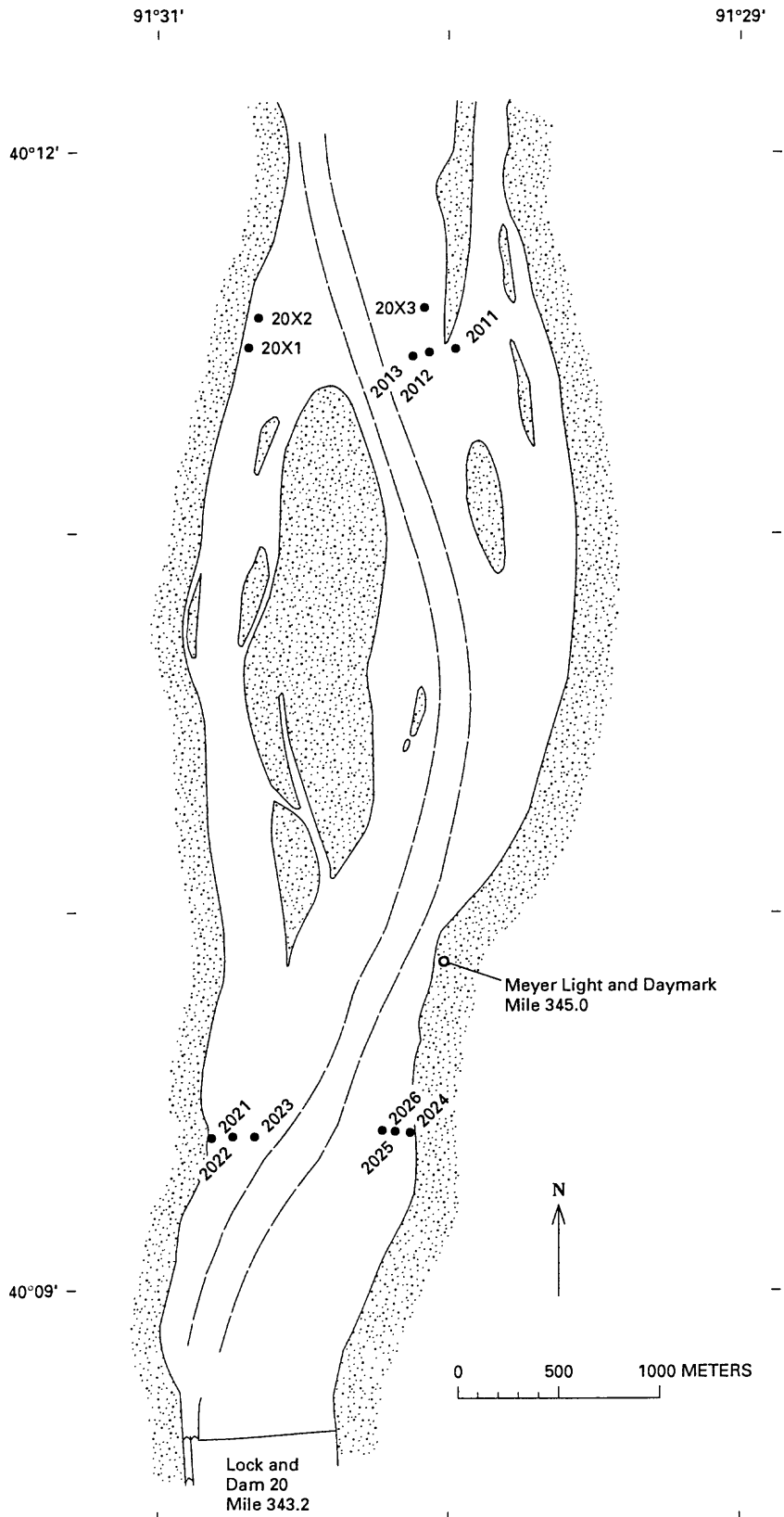
GAGE HEIGHT at Dam 19: 518.14 ft

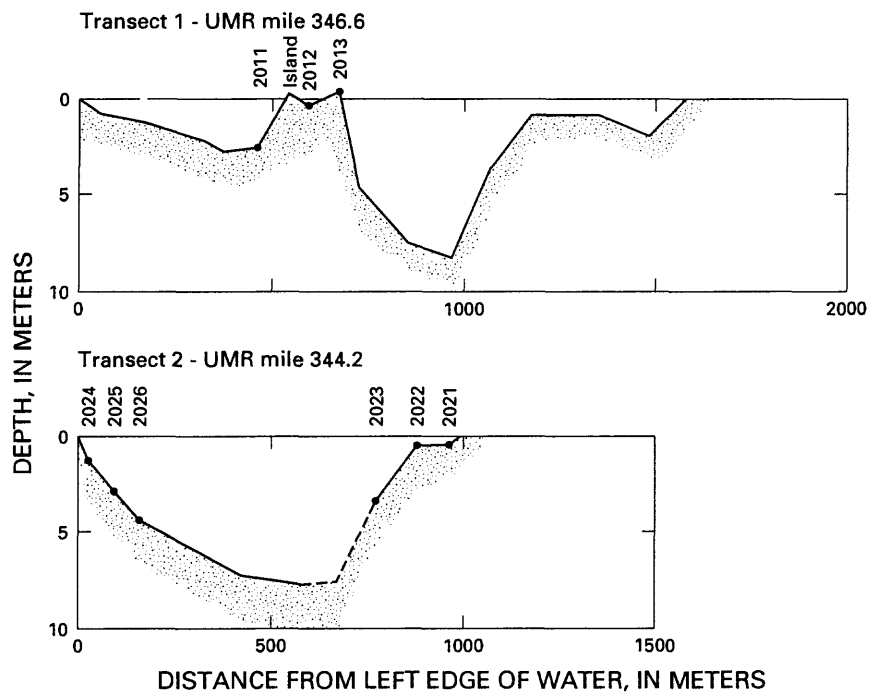
RIVER SLOPE: 21.7×10^{-6}

DATE RATED: 06-25-92

BEARING OF TRANSECT: 063° magnetic

| Site | Replicate | NAD83 | | Depth (m) | Surface | | Surficial bed sediment |
|------|-----------|-----------|------------|--------------|-----------------------------|-------------|---------------------------|
| | | Latitude | Longitude | | Conductance | Temperature | |
| | | N | W | | ($\mu\text{S}/\text{cm}$) | (°C) | |
| LEW | | | | 0.0 | | | -- |
| 1951 | 1 | 40°25.291 | 091°22.872 | 8.4 | 457 | -- | -- |
| | 2 | 24.998 | 22.517 | 8.6 | 453 | 24.3 | -- |
| 1952 | 1 | 25.310 | 22.651 | 7.8 | 453 | 24.0 | -- |
| | 2 | 25.179 | 22.495 | 6.2 | 455 | 24.5 | -- |
| 1953 | 1 | 25.412 | 22.524 | 5.1 | 451 | 24.2 | -- |
| | 2 | 25.162 | 22.361 | 4.0 | 455 | 24.5 | -- |
| 1954 | 1 | 25.429 | 22.328 | 2.0 | 457 | 24.1 | -- |
| | 2 | 40°25.385 | 091°22.324 | 2.0 | 454 | 24.3 | -- |
| REW | | | | 0.0 | | | |





STATION: Mississippi River in Pool 20, Transect 1--UMR mile 346.6

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 19 TW: 485.39 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangles are Lima, Ill.-Mo., and Canton, Mo.-Ill.

DATE: June 30, 1994

GAGE HEIGHT at Dam 20: 478.40 ft

RIVER SLOPE: 63.0×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on July 22, 1991, when the pool was first sampled, and 5.4 m lower than the maximum 1993 flood elevation. Some deposition may have occurred between sites 20X3, 2013, and 2012 because the first two sites were out of water on an apparently new sandbar to the west of Blue Goose Island. Sites with negative depths are out of the water. Sites with only hundredths of a degree are ones that could not be reached by boat but were located by measuring the remaining distance from the GPS antenna in the boat to the site using a tape measure. Measured discharge was $2,980 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 077° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^\circ$ magnetic) | Surficial bed sediment |
|---|---------------|----------------|--------------|---|--|-------------------|-----------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature ($^\circ\text{C}$) | | | |
| LEW | 40°11.552 | 091°29.676 | 0.0 | 458 | 25.6 | -- | -- | -- |
| 04 | 11.539 | 29.705 | 0.9 | 446 | 25.9 | 0.52 | 130 | -- |
| 03 | 11.530 | 29.769 | 1.1 | 452 | 25.4 | 0.57 | 130 | -- |
| 02 | 11.514 | 29.835 | 1.8 | 455 | 25.1 | 0.59 | 170 | -- |
| 01 | 11.502 | 29.909 | 2.5 | 455 | 25.0 | 0.78 | 180 | -- |
| 2011 | 11.492 | 29.980 | 2.8 | 451 | 25.6 | 0.83 | 190 | sand |
| 2012 | 11.48 | 30.07 | 0.3 | 436 | 24.7 | <0.05 | -- | sand |
| 2013 | 11.47 | 30.12 | -0.1 | -- | -- | -- | -- | sand |
| 05 | 11.463 | 30.171 | 4.3 | 445 | 26.3 | 0.65 | 150 | -- |
| 06 | 11.443 | 30.261 | 7.2 | 451 | 25.5 | 1.00 | 150 | -- |
| 07 | 11.430 | 30.346 | 8.4 | 490 | 25.6 | 0.99 | 150 | -- |
| 08 | 11.426 | 30.409 | 3.7 | 511 | 25.8 | 0.55 | 130 | -- |
| 09 | 11.416 | 30.482 | 0.8 | 513 | 25.9 | 0.64 | 160 | -- |
| 10 | 11.399 | 30.594 | 0.7 | 505 | 26.6 | 0.56 | 210 | -- |
| 11 | 11.379 | 30.717 | 1.7 | 516 | 26.1 | 0.80 | 190 | -- |
| REW | 40°11.375 | 091°30.755 | 0.0 | 511 | 26.6 | 0.00 | -- | -- |
| These sites are not on the transect but nearby. | | | | | | | | |
| 20X1 | 40°11.510 | 091°30.667 | 1.8 | 511 | 26.6 | 0.68 | 190 | sand |
| 20X2 | 11.586 | 30.640 | 2.0 | 506 | 26.8 | 0.57 | 200 | sand |
| 20X3 | 40°11.61 | 091°30.06 | -0.3 | -- | -- | -- | -- | sand |

STATION: Mississippi River in Pool 20, Transect 2--UMR mile 344.2

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 19 TW: 485.39 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Canton, Mo.-Ill.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on July 22, 1991, when the pool was first sampled, and 5.4 m lower than the maximum 1993 flood elevation. Some deposition may have occurred near site 2021 because it could not be reached by boat. This site was located by measuring the remaining distance from the GPS antenna in the boat to the site using a tape measure--location is given in hundredths of a degree. Several pictures were taken of the Lima levee break just downstream from Dam 20 on the left bank. Measured discharge was 3,080 m³/s. Biological Resources Division collected a sample at site 2024.

DATE: June 30, 1994

GAGE HEIGHT at Dam 20: 478.40 ft

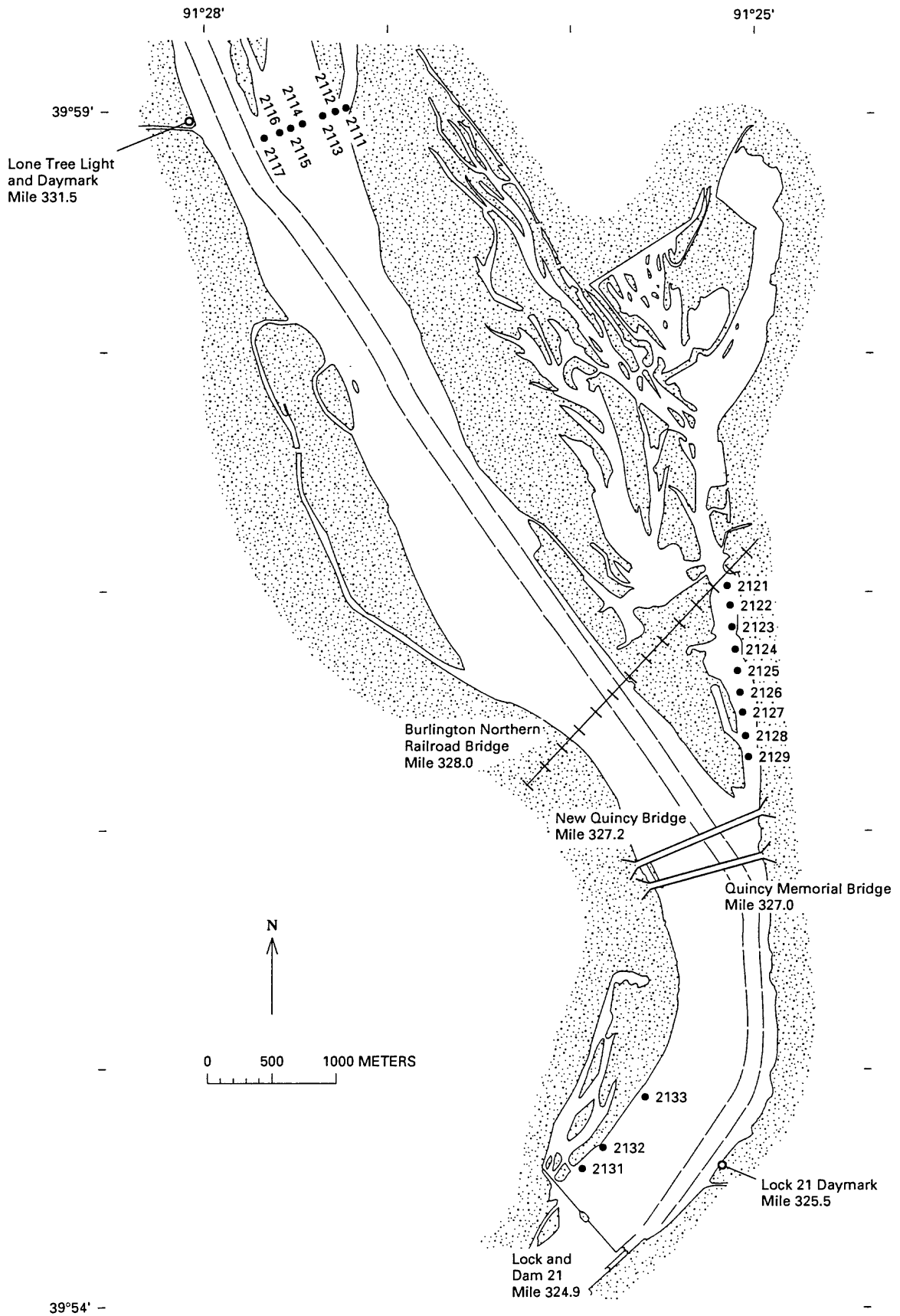
RIVER SLOPE: 63.0×10^{-6}

DATE RATED: 06-25-92

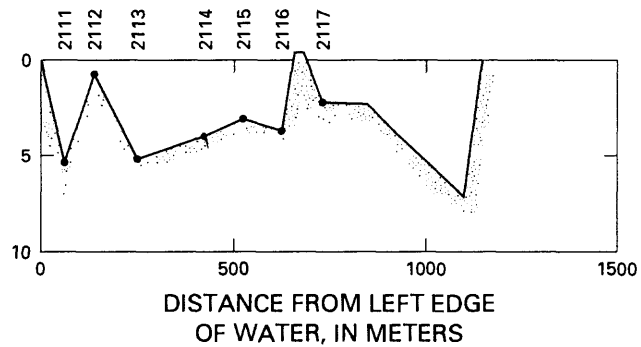
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 086° magnetic

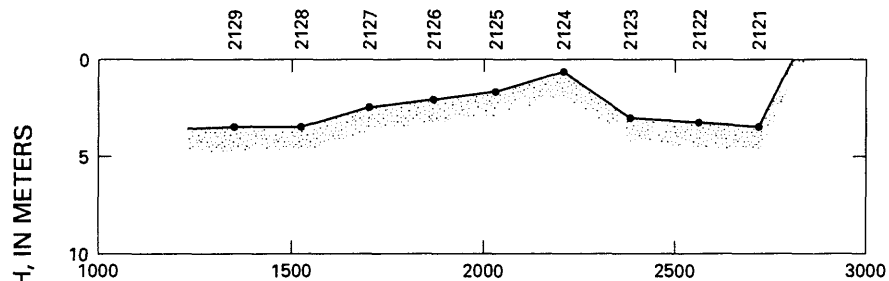
| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|---|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduc- tance ($\mu\text{S}/\text{cm}$) | Temp- erature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2024 | 40°09.436 | 091°30.131 | 0.8 | 445 | 26.8 | 0.32 | 180 | sticky mud |
| 2025 | 09.445 | 30.189 | 3.6 | 429 | 28.3 | 0.56 | 180 | sand |
| 2026 | 09.443 | 30.221 | 4.5 | 413 | 29.5 | 0.62 | 180 | sand |
| 12 | 09.434 | 30.313 | 6.0 | 427 | 28.5 | 0.80 | 180 | -- |
| 13 | 09.429 | 30.405 | 7.2 | 437 | 27.7 | 0.85 | 190 | -- |
| 14 | 09.433 | 30.489 | 7.7 | 471 | 27.2 | 0.84 | 190 | -- |
| 15 | 09.438 | 30.563 | 6.5 | 480 | 29.9 | 0.71 | 180 | -- |
| 2023 | 09.434 | 30.658 | 1.0 | 495 | 28.8 | 0.51 | 140 | sand |
| 2022 | 09.428 | 30.722 | 0.4 | 493 | 30.3 | 0.08 | 130 | sand |
| 2021 | 40°09.43 | 091°30.80 | 0.3 | 506 | 28.5 | ~0.07 | -- | sand |
| REW | | | 0.0 | | | | | |



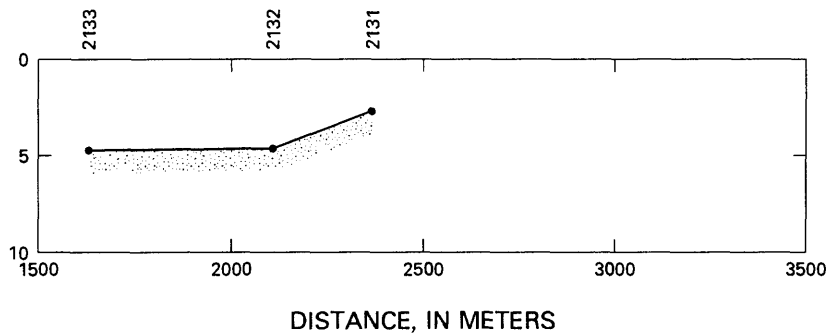
Transect 1 - UMR mile 331.4



Transect 2 - UMR mile 326.6



Transect 3 - UMR mile 326.6



STATION: Mississippi River in Pool 21, Transect 1--UMR mile 331.4

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 20 TW: 476.98 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Quincy West, Ill.-Mo.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.6 m lower than on April 24, 1992, when the pool was first sampled, and 6.0 m lower than the maximum 1993 flood elevation. Measured discharge was 2,780 m³/s. No grab sample was collected at site 2114.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 068° magnetic

DATE: July 1, 1994

GAGE HEIGHT at Dam 21: 470.30 ft

RIVER SLOPE: 70.3×10^{-6}

DATE RATED: 06-25-92

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | 39°59.013 | 091°27.200 | 0.0 | 457 | 26.0 | 0.00 | -- | |
| 2111 | 59.011 | 27.225 | 5.3 | 460 | 25.7 | 0.69 | 190 | sand |
| 2112 | 59.001 | 27.287 | 0.7 | 457 | 26.2 | 0.21 | 210 | mud |
| 2113 | 58.976 | 27.350 | 5.0 | 450 | 26.6 | 0.64 | 160 | sand |
| 2114 | 58.947 | 27.465 | 3.8 | 459 | 25.9 | 0.88 | 170 | gravel |
| 2115 | 58.930 | 27.532 | 2.9 | 454 | 26.6 | 0.80 | 180 | sand |
| 2116 | 58.909 | 27.587 | 3.5 | 455 | 26.7 | 0.71 | 160 | sand |
| 2117 | 58.885 | 27.668 | 1.9 | 454 | 27.5 | 0.64 | 190 | sand, gravel |
| 01 | 58.870 | 27.750 | 2.0 | 457 | 27.6 | 0.85 | 150 | -- |
| 02 | 58.847 | 27.806 | 3.3 | 467 | 27.5 | 0.90 | 150 | -- |
| 03 | 58.827 | 27.864 | 5.6 | 478 | 27.9 | 0.80 | 150 | -- |
| 04 | 58.806 | 27.907 | 6.5 | 490 | 27.8 | 0.99 | 150 | -- |
| 05 | 58.800 | 27.938 | 1.4 | 491 | 28.0 | 0.74 | 140 | -- |
| REW | 39°58.795 | 091°27.946 | 0.0 | 497 | 28.0 | 0.00 | -- | -- |

STATION: Mississippi River in Pool 21, Transect 2--UMR mile 326.6

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 20 TW: 476.98 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Quincy West, Ill.-Mo.

DATE: July 1, 1994

GAGE HEIGHT at Dam 21: 470.30 ft

RIVER SLOPE: 70.3×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.6 m lower than on April 24, 1992, when the pool was first sampled, and 6.0 m lower than the maximum 1993 flood elevation. No grab sample was collected at sites 2123 and 2125.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 168° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| REW | | | 0.0 | | | | | |
| 2121 | 39°57.022 | 091°25.125 | 3.2 | 465 | 25.2 | 0.22 | 100 | mud |
| 2122 | 56.934 | 25.117 | 3.0 | 466 | 25.1 | 0.37 | 150 | mud |
| 2123 | 56.846 | 25.107 | 2.9 | 463 | 25.4 | 0.39 | 160 | mud, roots |
| 2124 | 56.572 | 25.094 | 0.6 | 467 | 25.3 | 0.21 | 150 | mud |
| 2125 | 56.662 | 25.073 | 1.5 | 464 | 25.1 | 0.32 | 140 | debris |
| 2126 | 56.575 | 25.057 | 1.7 | 463 | 25.4 | 0.39 | 150 | mud |
| 2127 | 56.490 | 25.044 | 2.1 | 463 | 25.1 | 0.38 | 150 | sandy mud |
| 2128 | 56.383 | 25.030 | 3.5 | 460 | 25.3 | 0.40 | 140 | mud |
| 2129 | 39°56.299 | 091°25.027 | 3.5 | 462 | 25.2 | 0.36 | 150 | mud |

STATION: Mississippi River in Pool 21, Transect 3--UMR mile 326.6

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 20 TW: 476.98 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Quincy West, Ill.-Mo.

DATE: July 1, 1994

GAGE HEIGHT at Dam 21: 470.30 ft

RIVER SLOPE: 70.6×10^{-6}

DATE RATED: 06-25-92

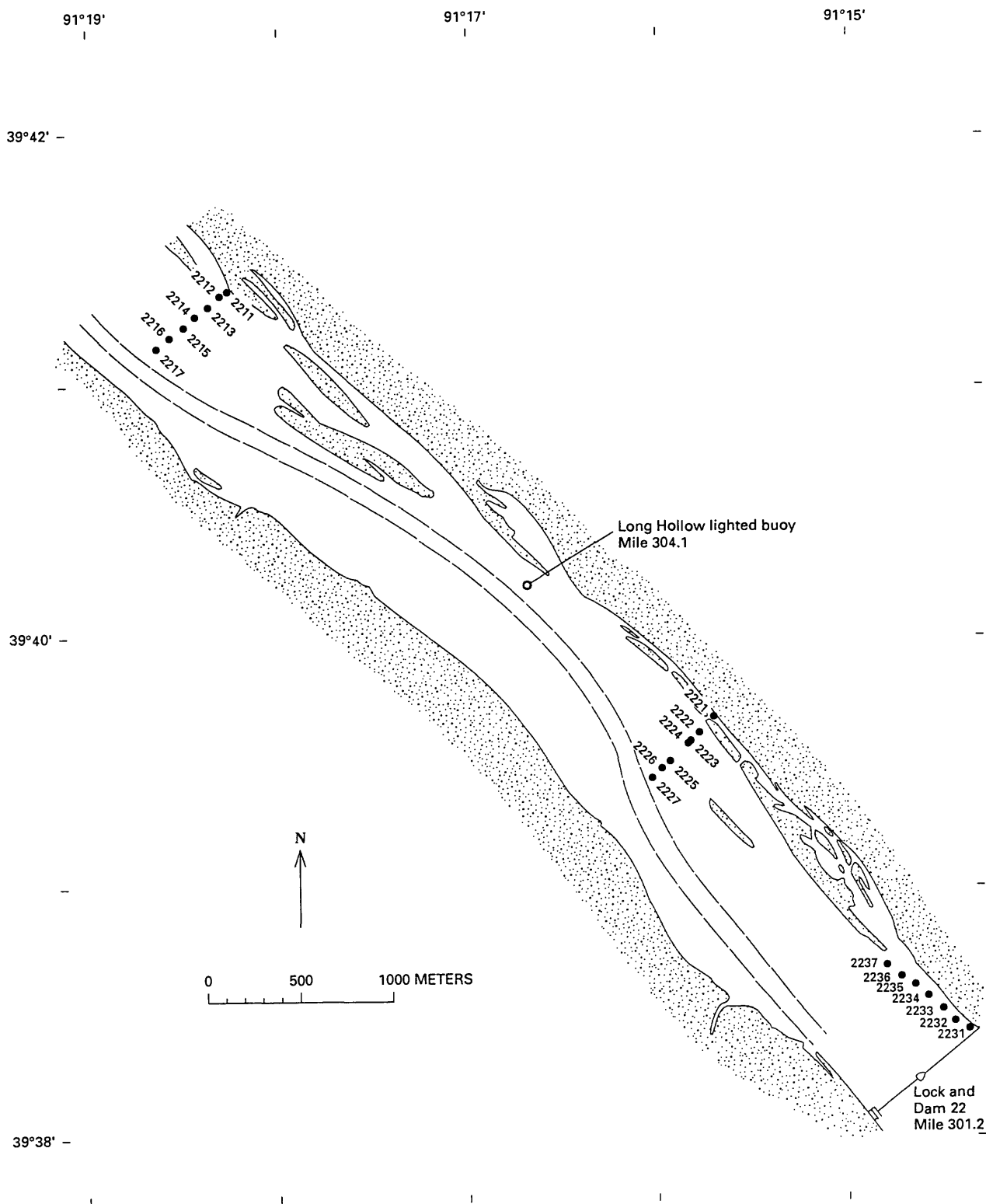
REMARKS:

Resampled sites using the differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.6 m lower than on April 24, 1992, when the pool was first sampled, and 6.0 m lower than the maximum 1993 flood elevation. Biological Resources Division collected a sample at site 2131.

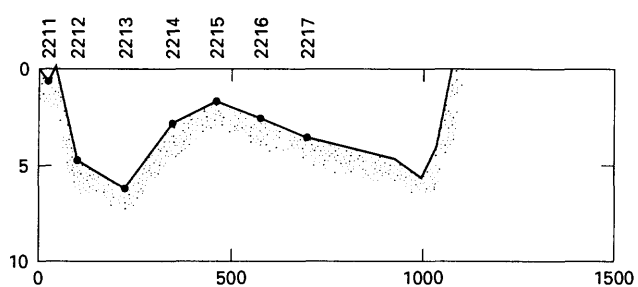
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 034° magnetic

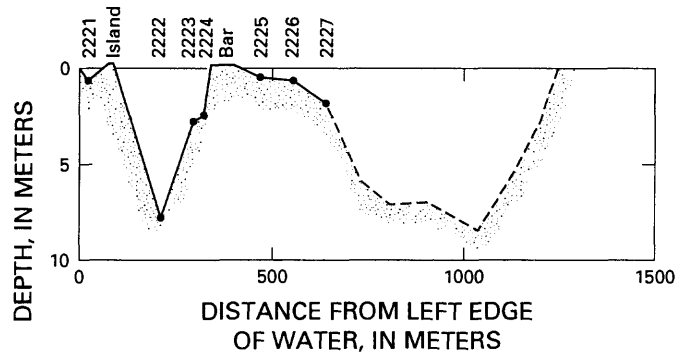
| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| REW | | | 0.0 | | | | | |
| 2131 | 39°54.585 | 091°25.927 | 2.6 | 507 | 25.7 | 0.34 | 200 | mud |
| 2132 | 54.675 | 25.823 | 4.4 | 507 | 25.7 | 0.46 | 200 | sand |
| 2133 | 39°54.885 | 091°25.574 | 4.4 | 508 | 25.6 | 0.71 | 200 | coarse sand |



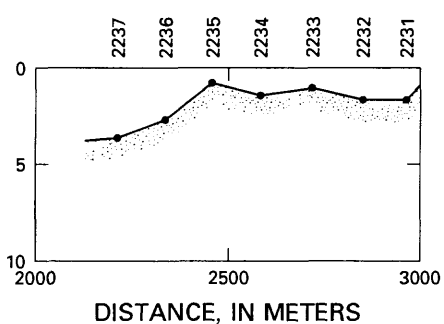
Transect 1 - UMR mile 306.0



Transect 2 - UMR mile 303.0



Transect 3 - UMR mile 303.0



STATION: Mississippi River in Pool 22, Transect 1--UMR mile 306.0

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 21 TW: 466.87 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Hannibal East, Mo.-Ill.

DATE: July 2, 1994

GAGE HEIGHT at Dam 22: 459.40 ft

RIVER SLOPE: 59.0×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on July 23, 1991, when the pool was first sampled. Measured discharge was $2,900 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 048° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|--------|---------------|----------------|--------------|---|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2211 | 39°41.353 | 091°18.189 | 0.7 | 455 | 25.8 | <0.05 | 110 | fine mud |
| 2212 | 41.321 | 18.227 | 5.0 | 462 | 26.1 | 0.93 | 120 | sand |
| 2213 | 41.285 | 18.292 | 5.7 | 466 | 26.1 | 0.78 | 130 | sand |
| 2214 | 41.223 | 18.363 | 2.7 | 470 | 26.0 | 0.76 | 120 | sand |
| Island | 41.22 | 18.40 | 0.0 | -- | -- | -- | -- | -- |
| 2215 | 41.212 | 18.421 | 1.5 | 473 | 25.9 | 0.64 | 110 | sand |
| 2216 | 41.168 | 18.443 | 2.3 | 476 | 25.9 | 0.70 | 120 | sand |
| 2217 | 41.124 | 18.556 | 3.5 | 489 | 25.6 | 0.81 | 120 | sand |
| 01 | 41.084 | 18.616 | 3.8 | 491 | 25.7 | 0.83 | 130 | -- |
| 02 | 41.056 | 18.668 | 4.5 | 497 | 25.8 | 0.87 | 120 | -- |
| 03 | 41.031 | 18.719 | 5.2 | 501 | 25.9 | 1.03 | 120 | -- |
| 04 | 41.015 | 18.750 | 3.9 | 502 | 25.8 | 0.72 | 120 | -- |
| REW | 39°41.003 | 091°18.764 | 0.0 | | | | | |

STATION: Mississippi River in Pool 22, Transect 2--UMR mile 303.0

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 21 TW: 466.87 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Hannibal East, Mo.-Ill.

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on July 23, 1991, when the pool was first sampled.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 041° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2221 | 39°39.705 | 091°15.745 | 0.8 | 469 | 24.8 | 0.14 | 140 | mud |
| 2222 | 39.635 | 15.828 | 7.4 | 474 | 25.1 | 0.56 | 130 | sand |
| 2223 | 39.602 | 15.867 | 2.7 | 478 | 25.0 | 0.47 | 130 | mud |
| 2224 | 39.592 | 15.881 | 2.4 | 475 | 25.1 | 0.26 | 120 | sand |
| 2225 | 39.530 | 15.968 | 0.3 | 468 | 24.0 | <0.05 | -- | mud, leaves |
| 2226 | 39.513 | 16.010 | 0.4 | 468 | 24.4 | 0.11 | 090 | mud |
| 2227 | 39°39.470 | 091°16.046 | 0.9 | 479 | 25.0 | 0.42 | 120 | sand |

STATION: Mississippi River in Pool 22, Transect 3--UMR mile 303.0

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 21 TW: 466.87 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Hannibal East, Mo.-Ill.

DATE: July 2, 1994

GAGE HEIGHT at Dam 22: 459.40 ft

RIVER SLOPE: 59.0×10^{-6}

DATE RATED: 06-25-92

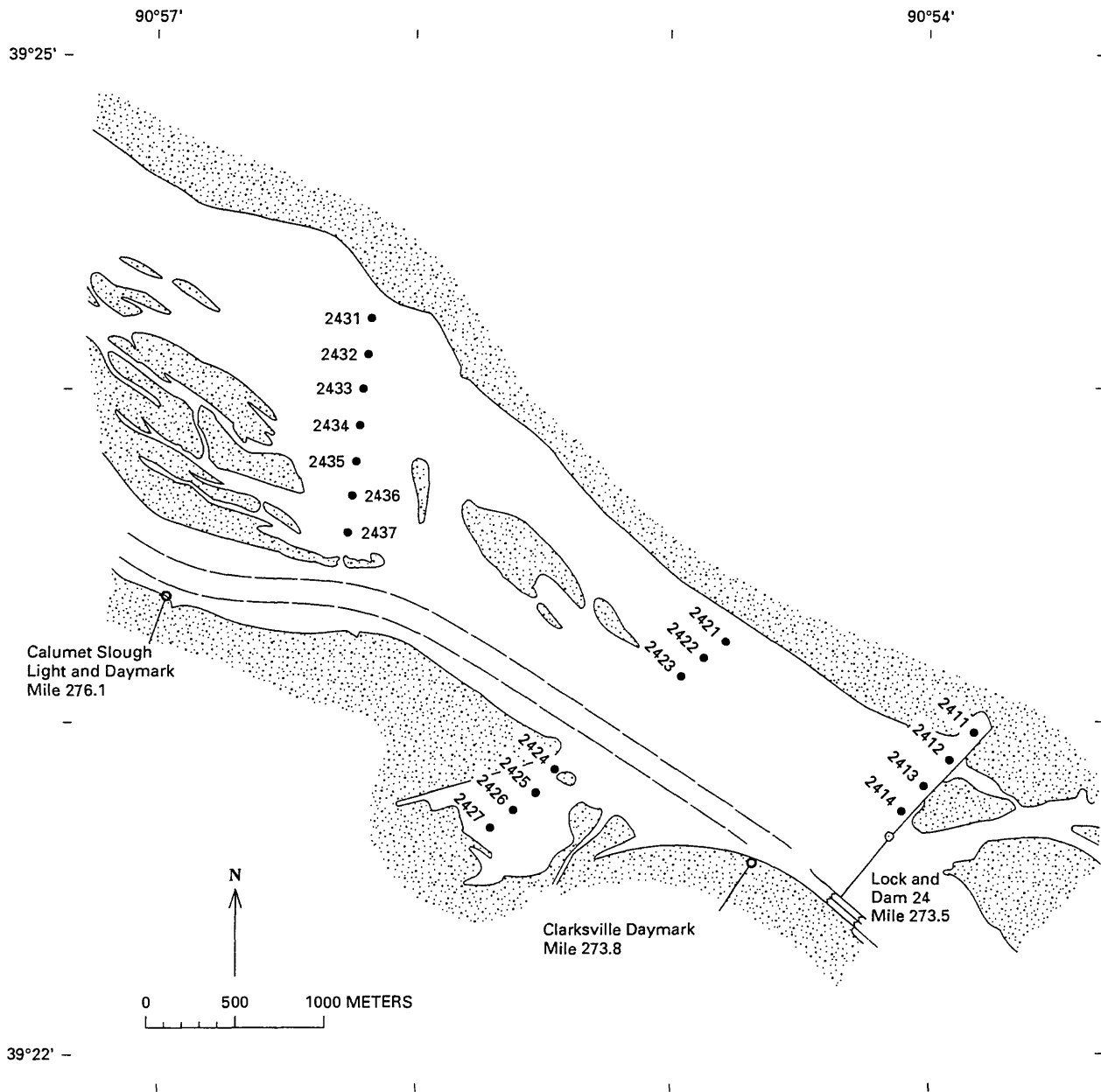
REMARKS:

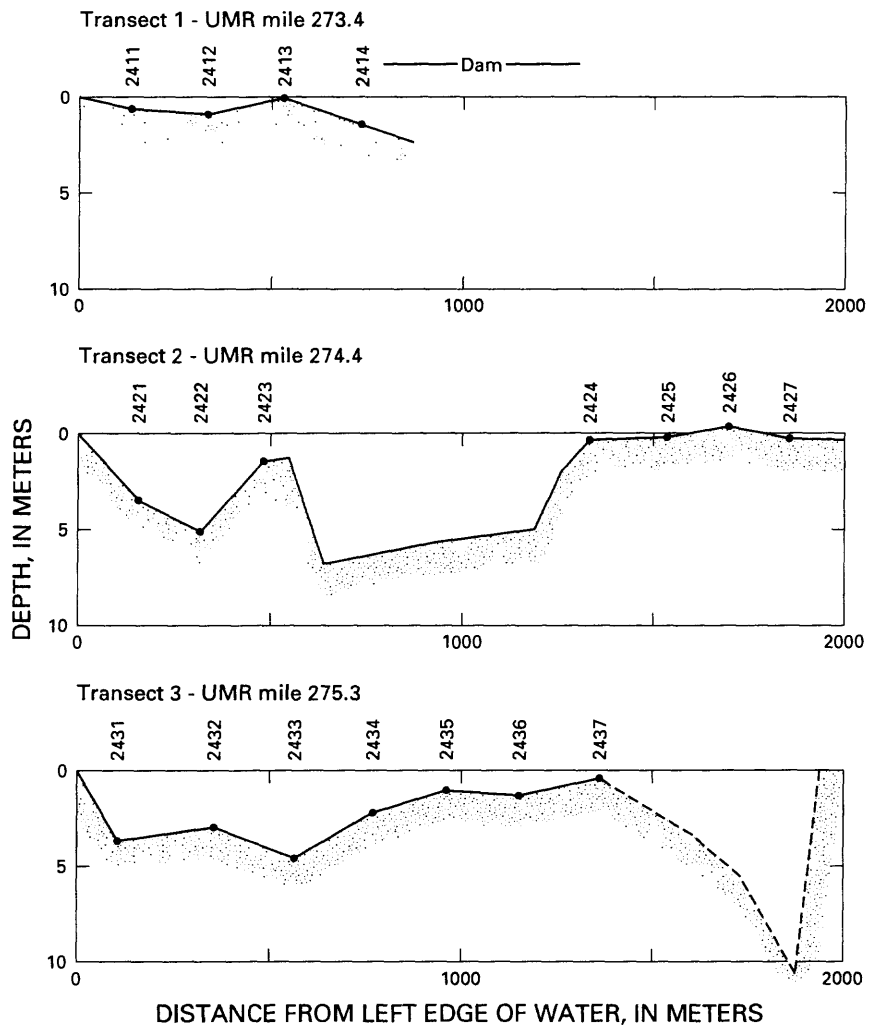
Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.1 m lower than on July 23, 1991, when the pool was first sampled. Biological Resources Division collected a sample from site 2231.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 126° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2231 | 39°38.496 | 091°14.463 | 1.5 | 461 | 24.8 | 0.05 | 170 | sticky mud |
| 2232 | 38.529 | 14.518 | 1.3 | 468 | 24.4 | <0.05 | -- | sticky mud |
| 2233 | 38.569 | 14.587 | 1.1 | 474 | 24.8 | 0.11 | 100 | mud |
| 2234 | 38.616 | 14.655 | 1.2 | 474 | 25.0 | 0.22 | 120 | mud |
| 2235 | 38.660 | 14.724 | 0.8 | 472 | 25.1 | 0.25 | 110 | mud |
| 2236 | 38.698 | 14.794 | 2.5 | 474 | 25.5 | 0.36 | 120 | mud, clay |
| 2237 | 39°38.737 | 091°14.862 | 3.4 | 468 | 25.7 | 0.69 | 110 | clay, sand |





STATION: Mississippi River in Pool 24, Transect 1--UMR mile 273.4

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 22 TW: 455.69 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Pleasant Hill, Ill.-Mo.

DATE: July 3, 1994

GAGE HEIGHT at Dam 24: 447.32 ft

RIVER SLOPE: 56.6×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.5 m lower than on October 29, 1991, when the pool was first sampled. Site 2411 was cut off from the pool by a sandbar; we walked until the water was too deep and the mud too soft to walk farther--so location is given to the nearest hundredth of a degree. Biological Resources Division collected a sample from site 2412.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 045° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2411 | 39°22.97 | 090°53.83 | 0.6 | 470 | 24.0 | 0.00 | -- | mud |
| 2412 | 22.887 | 53.917 | 0.7 | 465 | 23.7 | <0.05 | -- | mud |
| 2413 | 22.805 | 54.025 | 0.01 | -- | -- | -- | -- | sand |
| 2414 | 39°22.735 | 090°54.107 | 1.3 | 463 | 24.3 | <0.05 | -- | mud |

STATION: Mississippi River in Pool 24, Transect 2--UMR mile 274.4

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 22 TW: 455.69 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Pleasant Hill, Ill.-Mo.

DATE: July 3, 1994

GAGE HEIGHT at Dam 24: 447.32 ft

RIVER SLOPE: 56.6×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.5 m lower than on October 29, 1991, when the pool was first sampled. Sites 2424 (within 30 m of original sample site), 2425 (out of water), 2426, and 2427 (within 30 m of original sampling site) were difficult to get to because of low water. Location of sites 2425 and 2426 are given to the nearest hundredth of a degree. Negative depth is elevation above pool level. Measured discharge was $2,880 \text{ m}^3/\text{s}$.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 053° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction ($^\circ$ magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--|-------------------|-----------------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature ($^\circ\text{C}$) | | | |
| LEW | 39°23.296 | 090°54.705 | 0.0 | 465 | 25.3 | | | |
| 01 | 23.273 | 54.725 | 2.8 | 473 | 24.6 | 0.54 | 120 | -- |
| 2421 | 23.238 | 54.791 | 3.2 | 480 | 24.5 | 0.61 | 120 | sand |
| 2422 | 23.181 | 54.879 | 5.0 | 480 | 24.7 | 0.62 | 100 | sand |
| 2423 | 23.130 | 54.967 | 1.5 | 488 | 24.5 | 0.54 | 150 | clay |
| 02 | 23.084 | 55.048 | 6.0 | 484 | 24.5 | 0.31 | 130 | -- |
| 03 | 23.035 | 55.137 | 6.0 | 481 | 25.7 | 0.65 | 110 | -- |
| 04 | 22.990 | 55.195 | 5.9 | 492 | 24.9 | 0.70 | 110 | -- |
| 05 | 22.929 | 55.325 | 5.3 | 475 | 24.8 | 0.62 | 120 | -- |
| 2424 | 22.862 | 55.447 | 0.3 | 472 | 24.2 | <0.05 | -- | mud |
| 2425 | 22.79 | 55.40 | -0.2 | -- | -- | -- | -- | mud |
| 2426 | 22.74 | 55.63 | 0.05 | -- | -- | -- | -- | mud |
| 2427 | 39°22.695 | 090°55.715 | 0.2 | 585 | 21.8 | 0.00 | -- | mud |
| REW | | | 0.0 | | | | | |

STATION: Mississippi River in Pool 24, Transect 3--UMR mile 275.3

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 22 TW: 455.69 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Pleasant Hill, Ill.-Mo.

DATE: July 3, 1994

GAGE HEIGHT at Dam 24: 447.32 ft

RIVER SLOPE: 56.6×10^{-6}

DATE RATED: 06-25-92

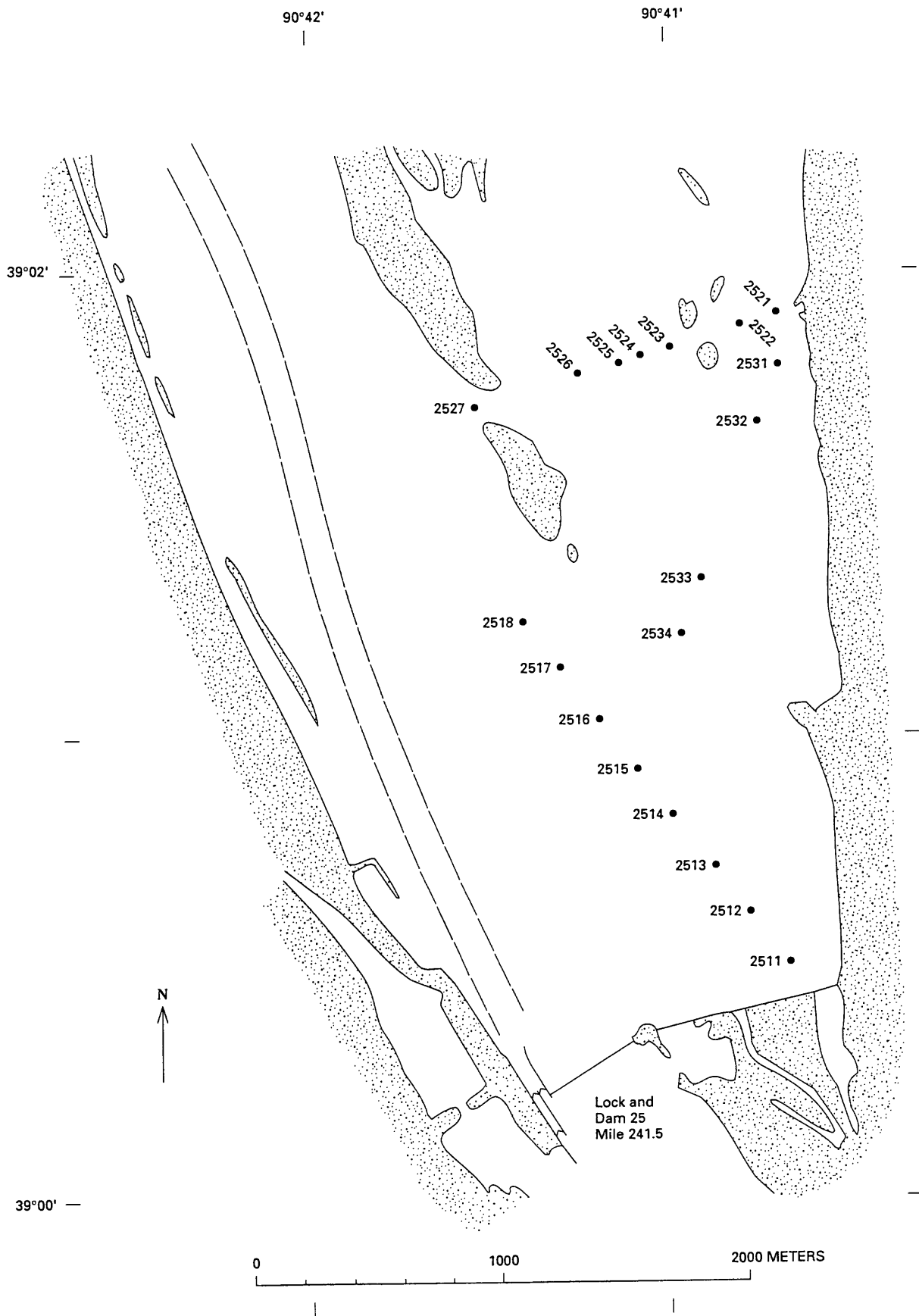
REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was 0.5 m lower than on October 29, 1991, when the pool was first sampled.

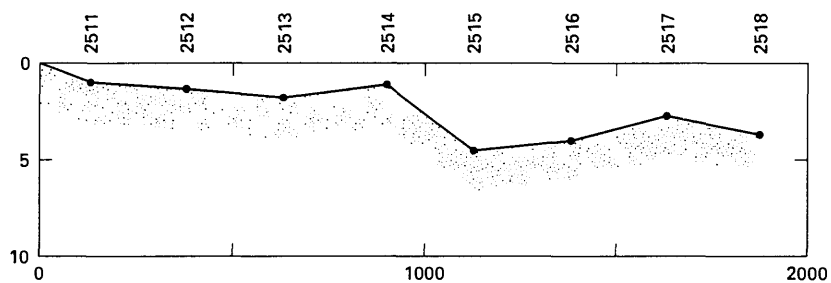
CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \times \text{rev/s} + 0.006$

BEARING OF TRANSECT: 007° magnetic

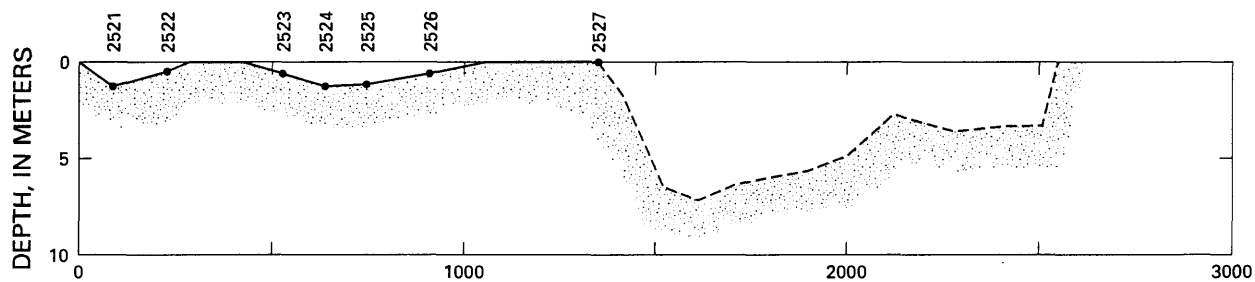
| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2431 | 39°24.208 | 090°56.171 | 3.6 | 468 | 25.8 | 0.70 | 090 | sand |
| 2432 | 24.099 | 56.192 | 2.9 | 472 | 25.6 | 0.76 | 120 | sand |
| 2433 | 23.996 | 56.207 | 4.3 | 474 | 25.5 | 0.68 | 100 | sand |
| 2434 | 23.889 | 56.231 | 2.0 | 469 | 25.5 | <0.05 | 140 | mud, sand |
| 2435 | 23.777 | 56.250 | 0.9 | 472 | 25.2 | <0.05 | 120 | mud, sand |
| 2436 | 23.682 | 56.259 | 1.2 | 479 | 25.3 | 0.14 | 140 | mud, sand |
| 2437 | 39°23.571 | 090°56.281 | 0.3 | 484 | 23.8 | 0.06 | 170 | mud |



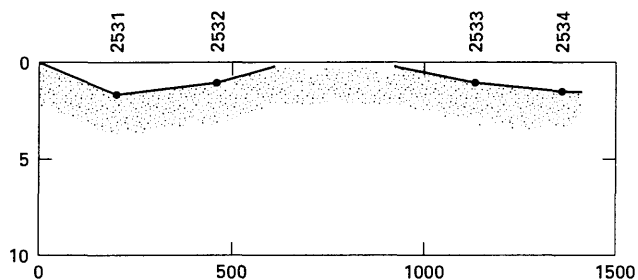
Transect 1 - UMR mile 243.1



Transect 2 - UMR mile 243.1



Transect 3 - UMR mile 241.5



DISTANCE FROM LEFT EDGE OF WATER, IN METERS

STATION: Mississippi River in Pool 25, Transect 1--UMR mile 275.3

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 24 TW: 440.76 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Foley, Mo.-Ill.

DATE: July 4, 1994

GAGE HEIGHT at Dam 25: 432.20 ft

RIVER SLOPE: 50.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was the same elevation as on April 22, 1991, when the pool was first sampled. The "R" indicates sites where a replicate sample for sediment size, total organic carbon, and total volatile solids was collected. No grab sample was collected from site 2517. Biological Resources Division collected a sample from site 2511.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 139° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|--------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2511 | 39°00.509 | 090°40.660 | 1.0 | 471 | 24.7 | 0.13 | 210 | mud |
| 2512-R | 00.621 | 40.768 | 1.0 | 472 | 25.9 | 0.23 | 210 | clay |
| 2513 | 00.721 | 40.867 | 1.5 | 474 | 25.9 | 0.32 | 170 | mud |
| 2514-R | 00.839 | 40.107 | 1.3 | 463 | 24.3 | 0.50 | 150 | mud |
| 2515 | 00.927 | 40.090 | 4.1 | 474 | 25.9 | 0.61 | 140 | sand, gravel |
| 2516-R | 01.038 | 41.197 | 3.4 | 471 | 26.0 | 0.63 | 130 | sand |
| 2517 | 01.154 | 41.303 | 2.5 | 474 | 26.0 | 0.77 | 140 | rock |
| 2518-R | 39°01.253 | 090°41.403 | 3.8 | 473 | 26.1 | 0.65 | 140 | sand |

STATION: Mississippi River in Pool 25, Transect 2--UMR mile 243.1

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 24 TW: 440.76 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Foley, Mo.-Ill.

DATE: July 4, 1994

GAGE HEIGHT at Dam 25: 432.20 ft

RIVER SLOPE: 50.7×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was the same elevation as on April 22, 1991, when the pool was first sampled. Site 2527 was in water less than 0.1 m deep. The last 41 m were measured with a tape measure while walking to the site, so the location is listed below to the nearest hundredth of a degree. The "R" indicates sites where a replicate sample for sediment size, total organic carbon, and total volatile solids was collected.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 071° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|--------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2521 | 39°01.915 | 090°40.701 | 1.1 | 447 | 30.1 | 0.14 | 210 | mud |
| 2522-R | 01.887 | 40.805 | 0.5 | 455 | 29.7 | 0.05 | 290 | mud |
| 2523 | 01.846 | 40.999 | 0.3 | 457 | 28.4 | 0.14 | 320 | mud |
| 2524-R | 01.831 | 41.077 | 1.0 | 455 | 28.2 | 0.13 | 270 | mud |
| 2525 | 01.816 | 41.144 | 1.0 | 455 | 28.1 | 0.06 | 250 | mud |
| 2526-R | 01.787 | 41.252 | 0.7 | 453 | 27.6 | <0.05 | 330 | mud |
| 2527 | 39°01.72 | 090°41.55 | 0.05 | 471 | 26.2 | -- | -- | sticky mud |

STATION: Mississippi River in Pool 25, Transect 3--UMR mile 241.5

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 24 TW: 440.76 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Foley, Mo.-Ill.

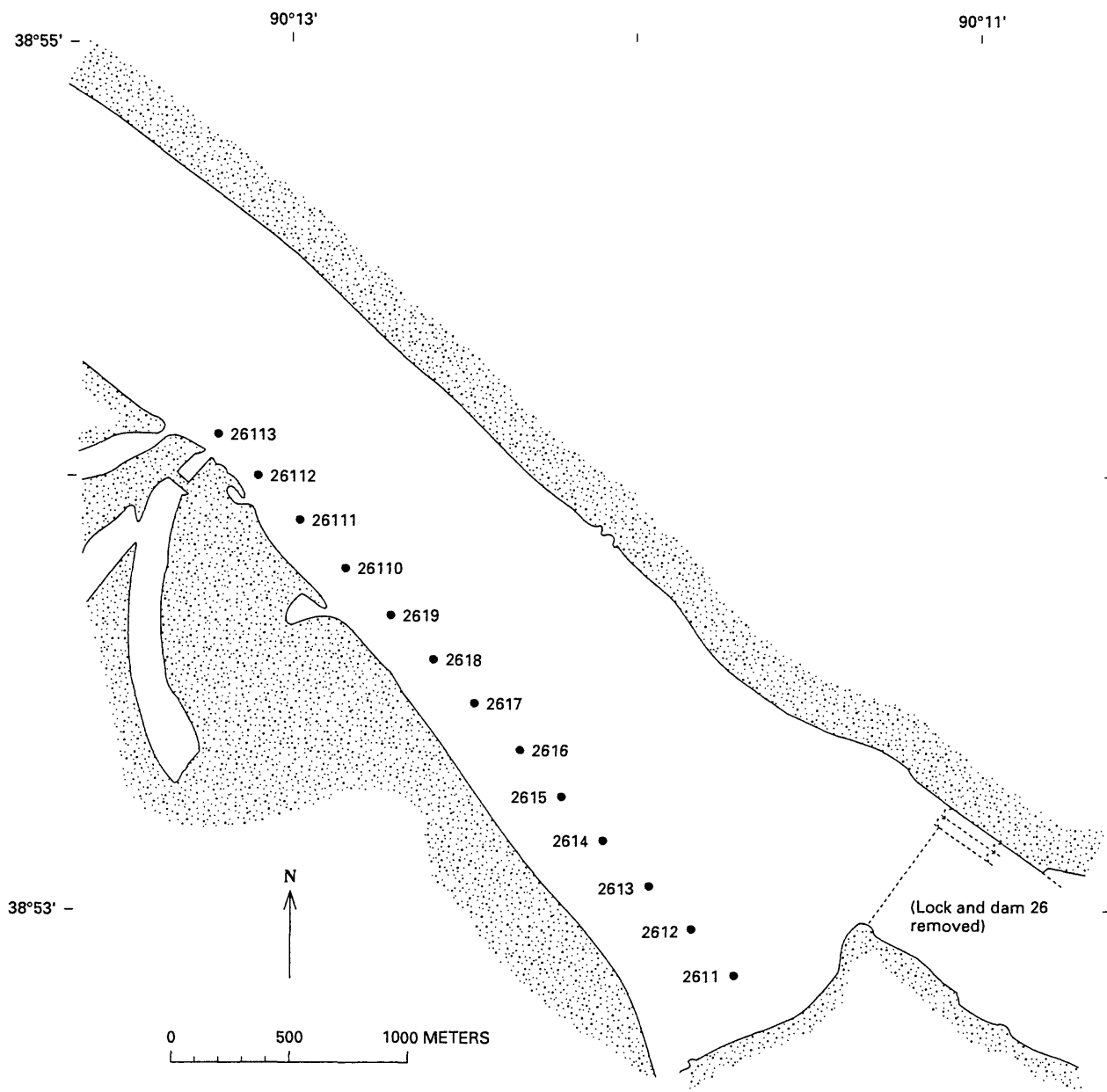
REMARKS:

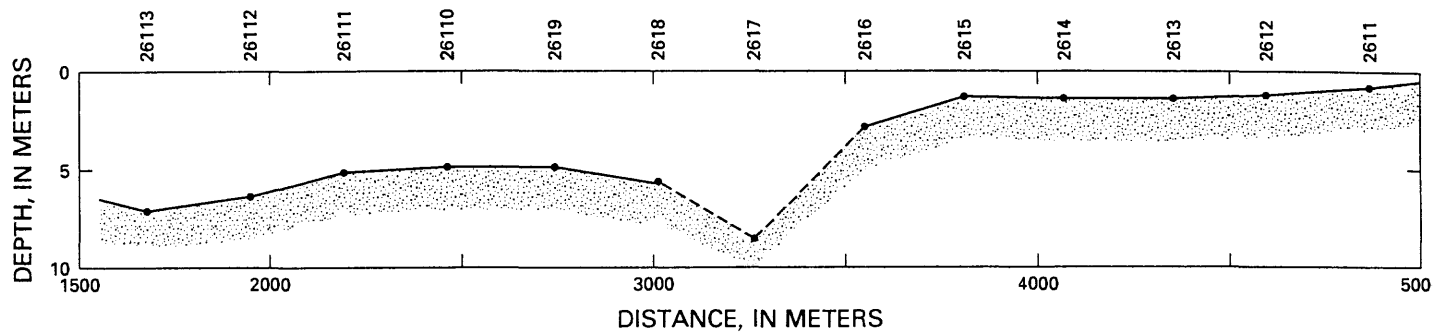
Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Pool elevation was the same elevation as on April 22, 1991, when the pool was first sampled. The "R" indicates sites where a replicate sample for sediment size, total organic carbon, and total volatile solids was collected.

CURRENT METER EQUATION: $V(m/s) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 016° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|--------|---------------|----------------|--------------|--|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S/cm}$) | Tem- perature (°C) | | | |
| LEW | | | 0.0 | | | | | |
| 2531 | 39°01.810 | 090°40.705 | 1.3 | 454 | 29.2 | 0.36 | 200 | mud |
| 2532-R | 01.679 | 40.762 | 0.9 | 457 | 28.7 | 0.08 | 230 | mud |
| 2533 | 01.341 | 40.917 | 1.0 | 466 | 26.5 | 0.11 | 260 | mud |
| 2534-R | 39°01.223 | 090°40.967 | 1.2 | 461 | 26.6 | 0.05 | 240 | mud |





STATION: Mississippi River in Pool 26, Transect 1--UMR mile 206.1

PARTY: Moody, Johnson, and Martin

GAGE HEIGHT at Dam 25 TW: 425.37 ft

SUSPENSION: 15-pound weight

CURRENT METER No: W-223906

MAP: USGS 7.5-minute quadrangle is Alton, Ill.-Mo.

DATE: July 4, 1994

GAGE HEIGHT at Dam 25: 432.20 ft

RIVER SLOPE: 42.3×10^{-6}

DATE RATED: 06-25-92

REMARKS:

Resampled sites using differential GPS navigation beacon located in East St. Louis, Ill. The estimated error in site location is about ± 5 m. The surface specific conductance and temperature were measured by using a LabComp meter. Site 2617 was 5.3 m deeper than on November 2, 1991, when it was originally sampled. It was too deep to get a van Veen grab, and when we moved toward the right bank, it only got deeper. Site 2618 was about 2 m deeper. No grab sample was collected from sites 2616. Biological Resources Division collected a sample from site 2612.

CURRENT METER EQUATION: $V(\text{m/s}) = 0.668 \cdot \text{rev/s} + 0.006$

BEARING OF TRANSECT: 137° magnetic

| Site | NAD83 | | Depth (m) | Surface | | Velocity (m/s) | Direction (°magnetic) | Surficial bed sediment |
|-------|---------------|----------------|--------------|---|--------------------------|-------------------|--------------------------|------------------------------|
| | Latitude N | Longitude W | | Conduct- ance ($\mu\text{S}/\text{cm}$) | Tem- perature (°C) | | | |
| REW | | | 0.0 | | | | | |
| 2611 | 38°52.850 | 090°11.695 | 0.4 | 472 | 26.7 | 0.08 | 270 | mud |
| 2612 | 52.948 | 11.820 | 0.9 | 476 | 26.9 | 0.25 | 060 | mud |
| 2613 | 53.050 | 11.936 | 1.0 | 474 | 27.2 | 0.09 | 080 | mud |
| 2614 | 53.162 | 12.081 | 1.0 | 476 | 27.2 | 0.14 | 080 | mud |
| 2615 | 53.266 | 12.197 | 1.0 | 476 | 27.2 | 0.26 | 100 | mud |
| 2616 | 53.364 | 12.323 | 2.3 | 474 | 27.2 | 0.37 | 100 | clay |
| 2617 | 53.475 | 12.460 | 8.8 | -- | -- | -- | -- | -- |
| 2618 | 53.583 | 12.579 | 5.2 | 474 | 27.3 | 0.43 | 120 | mud |
| 2619 | 53.677 | 12.708 | 4.8 | 475 | 27.3 | 0.40 | 110 | mud |
| 26110 | 53.784 | 12.840 | 4.7 | 475 | 27.3 | 0.45 | 120 | mud |
| 26111 | 53.898 | 12.971 | 5.1 | 473 | 27.5 | 0.46 | 120 | mud |
| 26112 | 53.994 | 13.082 | 6.1 | 473 | 27.5 | 0.47 | 120 | mud |
| 26113 | 38°54.095 | 090°13.213 | 7.0 | 473 | 27.5 | 0.42 | 100 | mud |