

# Modified Level II Streambed-Scour Analysis for Structure I-69-64-4767 Crossing Tippey Ditch in Grant County, Indiana

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Prepared in cooperation with the  
INDIANA DEPARTMENT OF TRANSPORTATION

U.S. GEOLOGICAL SURVEY  
Open-File Report 97-318



Indianapolis, Indiana

1997

U.S. DEPARTMENT OF THE INTERIOR  
BRUCE BABBITT, Secretary

U.S. GEOLOGICAL SURVEY  
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## CONVERSION FACTORS AND ABBREVIATIONS

<b>Multiply</b>	<b>By</b>	<b>To obtain</b>
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft <sup>2</sup> )	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft <sup>3</sup> /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi <sup>2</sup> )	2.590	square kilometer

### Abbreviations used in this report:

D <sub>50</sub>	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	U. S. Geological Survey
WSPRO	Water Surface PROfile model

# Modified Level II Streambed-Scour Analysis for Structure I-69-64-4767 Crossing Tippey Ditch in Grant County, Indiana

By Bret A. Robinson, David C. Voelker, *and* Robert L. Miller

## ABSTRACT

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-69-64-4767 on Interstate 69 crossing Tippey Ditch in Grant County, Indiana, are presented. The site is near the town of Van Buren in the northeastern part of Grant County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 11.9 feet for the modeled discharge of 2,000 cubic feet per second and approximately 19.8 feet for the modeled discharge of 3,400 cubic feet per second.

## INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-69-64-4767.

### Background and Scope

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the “Evaluation Methods” section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

### **Site Description**

The study site is located near the town of Van Buren in the northeastern part of Grant County. The drainage area for the site is approximately 5.2 mi<sup>2</sup> (estimated using Hoggatt, 1975, and USGS 7.5-minute topographic data). The predominant land use in the basin is agricultural; in the immediate vicinity of the bridge, the land is predominantly agricultural.

Within the immediate vicinity of the bridge, Tippey Ditch has a channel-bed slope of approximately 0.00125 ft/ft. The channel-bed material is gravelly sand, and the channel banks consist of sandy gravelly silt-clay. At the time of the Level I site visit on June 16, 1993, the banks were observed to have 0 to 25 percent woody vegetative cover; the field report noted that the banks were experiencing fluvial erosion.

The Interstate 69 crossing of Tippey Ditch is a 60-ft-long, multi-lane bridge consisting of three spans supported by concrete and steel piers and sloping concrete spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

## EVALUATION METHODS

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

To determine drainage area, either published values found in Hoggatt (1975) or 7.5-minute topographic maps with Hoggatt's original drainage-area delineations were used. Where there are no published data, drainage-area segments measured from the maps produced by Hoggatt were either subtracted from downstream sites or added to upstream sites published by Hoggatt (1975).

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a Q100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated Q100 and 2) a discharge equal to 1.7 times the approximated Q100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1962) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting water-surface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.

**Table 1.** Cumulative scour depths for the modeled discharges at structure I-69-64-4767 crossing Tippey Ditch in Grant County, Indiana  
 [--, no value]

Pier number <sup>1</sup>	Stationing from bridge plans <sup>2</sup>	Initial bed-elevation at pier (feet)	Main-channel contraction scour depth (feet)	Local scour depth (feet)	Worst-case total-scour depth <sup>3</sup> (feet)	Bottom elevation of pier (feet)	Worst-case bed elevation after scour <sup>4</sup> (feet)
<b>Modeled discharge<sup>5</sup> is 2,000 cubic feet per second</b>							
1	298+34	837	7.1	4.8	11.9	827	819.8
2	298+60	837	7.1	4.8	11.9	827	819.8
<b>Modeled discharge is 3,400 cubic feet per second</b>							
1	298+34	837	14.0	5.8	19.8	827	811.9
2	298+60	837	14.0	5.8	19.8	827	811.9

<sup>1</sup>Pier numbers were assigned from left to right as shown on the bridge plans.

<sup>2</sup>Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 298+34, represents a point 29,834 feet from an arbitrary starting location referenced on the bridge plans.

<sup>3</sup>Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

<sup>4</sup>Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (831.7 feet).

<sup>5</sup>Not a coordinated discharge.

## **SPECIAL CONSIDERATIONS**

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled.

The piers supporting this bridge are set on the sloping concrete spill-through abutments. Therefore, even though the results shown in table 1 indicate that scour could undermine the piers, scour could only take place after the concrete abutments were removed or by erosion of bed sediment from under the protective abutments.

## **RESULTS**

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

## **REFERENCES**

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1962, Bridge plans Interstate Route 69: Bridge File I-69-64-4767.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

# APPENDIX

# WSPRO INPUT FILE

```
T1          I-69 Over Tippey Ditch          I69-64-4767
T2          County: Grant                   Quad: Van Buren 74D
T3          11-21-96                       Bret A. Robinson
SI          0
Q           2000 3400
SK          .00125 .00125
XS          EXIT 0 0
GR          29255 850 29767 842 29813 842 29820 840 29830 835 29841 831.5
GR          29851 831.5 29860 841 29926 842 30228 850
N           .035 .034 .035
SA          29815 29860
XS          FULLV 61 0
GR          29255 850 29767 842 29813 842 29820 840 29830 835 29841 831.5
GR          29851 831.5 29860 841 29926 842 30228 850
N           .035 .034 .035
SA          29815 29860
BR          BRDGE 61 844.2 0
GR          29821 0844.1 29846 0831.6 29851 0831.7 29876 0843.9 29821 0844.1
N           .034
PD          837 3 1
CD          3 130 2 843
*           LXBr RXBr * * * TPierW
DC 0 BRDGE 29825 29871 29820 29870 * 3
*           LPierEdge RPierEdge PierWdth * * K1 K2 K3(1.1)
DP          29821 29876 1.5 * * 1 1 1.1
DP          29821 29876 1.5 * * 1 1 1.1
XS          APPR 252 0
GR          29166 850 29309 850 29759 840 29808 841 29822 841 29828 840
GR          29838 835 29841 833 29846 833 29855 835 29867 840 29887 840
GR          29894 840 30453 850
N           .045 .034 .045
SA          29820 29870
EX
ER
```

# WSPRO OUTPUT

```
***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Run Date & Time: 8/ 6/97 6:45 am Version V050196
Input File: 4767.dat Output File: 4767.LST
```

```
-----*
T1      I-69 OVER TIPPEY DITCH          I69-64-4767
T2      COUNTY: GRANT                  QUAD: VAN BUREN 74D
T3      11-21-96                       BRET A. ROBINSON
SI      0
Q       2000 3400
```

\*\*\* Processing Flow Data; Placing Information into Sequence 1 \*\*\*

SK .00125 .00125

```
***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English
```

```
-----*
I-69 OVER TIPPEY DITCH          I69-64-4767
COUNTY: GRANT                  QUAD: VAN BUREN 74D
11-21-96                       BRET A. ROBINSON
```

```
-----*
* Starting To Process Header Record EXIT *
-----*
```

```
XS EXIT 0 0
GR      29255 850 29767 842 29813 842 29820 840 29830 835 29841
831.5
GR      29851 831.5 29860 841 29926 842 30228 850
N       .035 .034 .035
SA      29815 29860
```

\*\*\* Completed Reading Data Associated With Header Record EXIT \*\*\*  
 \*\*\* Storing X-Section Data In Temporary File As Record Number 1 \*\*\*

```
*** Data Summary For Header Record EXIT ***
SRD Location: 0. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
```

X,Y-coordinates (10 pairs)					
X	Y	X	Y	X	Y
29255.000	850.000	29767.000	842.000	29813.000	842.000
29820.000	840.000	29830.000	835.000	29841.000	831.500
29851.000	831.500	29860.000	841.000	29926.000	842.000
30228.000	850.000				

Minimum and Maximum X,Y-coordinates

# WSPRO OUTPUT

```

Minimum X-Station: 29255.000 ( associated Y-Elevation: 850.000 )
Maximum X-Station: 30228.000 ( associated Y-Elevation: 850.000 )
Minimum Y-Elevation: 831.500 ( associated X-Station: 29851.000 )
Maximum Y-Elevation: 850.000 ( associated X-Station: 29255.000 )
    
```

```

          Roughness Data ( 3 SubAreas )
                Roughness  Horizontal
          SubArea Coefficient Breakpoint
          -----
            1      .035      ---
            ---      *****
            2      .034      ---
            ---      *****
            3      .035      ---
          -----
    
```

```

*-----*
*      Finished Processing Header Record EXIT      *
*-----*
    
```

```

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English
    
```

```

-----*
I-69 OVER TIPPEY DITCH          I69-64-4767
COUNTY: GRANT                 QUAD: VAN BUREN 74D
11-21-96                       BRET A. ROBINSON
    
```

```

*-----*
*      Starting To Process Header Record FULLV      *
*-----*
    
```

```

XS  FULLV 61 0
GR  29255 850 29767 842 29813 842 29820 840 29830 835 29841
831.5
GR  29851 831.5 29860 841 29926 842 30228 850
N   .035 .034 .035
SA  29815 29860
    
```

```

*** Completed Reading Data Associated With Header Record FULLV ***
*** Storing X-Section Data In Temporary File As Record Number 2 ***
    
```

```

*** Data Summary For Header Record FULLV ***
SRD Location: 61. Cross-Section Skew: .0 Error Code 0
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
    
```

```

          X,Y-coordinates (10 pairs)
                X          Y          X          Y          X          Y
          -----
29255.000    850.000    29767.000    842.000    29813.000    842.000
29820.000    840.000    29830.000    835.000    29841.000    831.500
29851.000    831.500    29860.000    841.000    29926.000    842.000
    
```



# WSPRO OUTPUT

-----	-----	-----	-----	-----	-----
29821.000	844.100	29846.000	831.600	29851.000	831.700
29876.000	843.900	29821.000	844.100		
-----	-----	-----	-----	-----	-----

Minimum and Maximum X,Y-coordinates

```

Minimum X-Station: 29821.000 ( associated Y-Elevation: 844.100 )
Maximum X-Station: 29876.000 ( associated Y-Elevation: 843.900 )
Minimum Y-Elevation: 831.600 ( associated X-Station: 29846.000 )
Maximum Y-Elevation: 844.100 ( associated X-Station: 29821.000 )
    
```

Roughness Data ( 1 SubAreas )

SubArea	Roughness Coefficient	Horizontal Breakpoint
-----	-----	-----
1	.034	---
-----	-----	-----

Discharge coefficient parameters

BRType	BRWidth	EMBSS	EMBElv	UserCD
3	130.000	2.00	843.000	*****

Pressure flow elevations

AVBCEL	PFElev
*****	844.200

Abutment Parameters

ABSLPL	ABSLPR	XTOELT	YTOELT	XTOERT	YTOERT
*****	*****	*****	*****	*****	*****

Pier/Pile Data ( 1 Group(s) )

Code Indicates Bridge Uses Piers

Group	Elevation	Gross Width	Number
-----	-----	-----	-----
1	837.000	3.000	1
-----	-----	-----	-----

```

*-----*
* Finished Processing Header Record BRDGE *
*-----*
    
```

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
 Model for Water-Surface Profile Computations.  
 Input Units: English / Output Units: English

\*-----\*

I-69 OVER TIPPEY DITCH COUNTY: GRANT 11-21-96	I69-64-4767 QUAD: VAN BUREN 74D BRET A. ROBINSON
DC 0 BRDGE 29825 29871 29820 29870 * 3	
DP        29821 29876 1.5 * * 1 1 1.1	
DP        29821 29876 1.5 * * 1 1 1.1	

# WSPRO OUTPUT

```

*-----*
*           Starting To Process Header Record APPR           *
*-----*
  
```

```

XS  APPR 252 0
GR   29166 850 29309 850 29759 840 29808 841 29822 841 29828 840
GR   29838 835 29841 833 29846 833 29855 835 29867 840 29887 840
GR   29894 840 30453 850
N    .045 .034 .045
SA   29820 29870
  
```

```

*** Completed Reading Data Associated With Header Record APPR ***
*** Storing X-Section Data In Temporary File As Record Number 4 ***
  
```

```

*** Data Summary For Header Record APPR ***
SRD Location:      252. Cross-Section Skew: .0 Error Code 0
Valley Slope:     .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
  
```

X,Y-coordinates (14 pairs)

X	Y	X	Y	X	Y
29166.000	850.000	29309.000	850.000	29759.000	840.000
29808.000	841.000	29822.000	841.000	29828.000	840.000
29838.000	835.000	29841.000	833.000	29846.000	833.000
29855.000	835.000	29867.000	840.000	29887.000	840.000
29894.000	840.000	30453.000	850.000		

Minimum and Maximum X,Y-coordinates

```

Minimum X-Station: 29166.000 ( associated Y-Elevation: 850.000 )
Maximum X-Station: 30453.000 ( associated Y-Elevation: 850.000 )
Minimum Y-Elevation: 833.000 ( associated X-Station: 29846.000 )
Maximum Y-Elevation: 850.000 ( associated X-Station: 29166.000 )
  
```

Roughness Data ( 3 SubAreas )

SubArea	Roughness Coefficient	Horizontal Breakpoint
1	.045	---
	---	*****
2	.034	---
	---	*****
3	.045	---

```

Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT
***** ***** ***** *****
  
```

```

*-----*
*           Finished Processing Header Record APPR           *
*-----*
  
```

\*\*\*\*\* W S P R O \*\*\*\*\*

# WSPRO OUTPUT

Federal Highway Administration - U. S. Geological Survey  
 Model for Water-Surface Profile Computations.  
 Input Units: English / Output Units: English

```

*-----*
      I-69 OVER TIPPEY DITCH                I69-64-4767
COUNTY: GRANT                            QUAD: VAN BUREN 74D
      11-21-96                            BRET A. ROBINSON
  
```

EX

```

*====*
*      Summary of Boundary Condition Information      *
*====*
  
```

#	Reach Discharge	Water Surface Elevation	Friction Slope	Flow Regime
1	2000.00	*****	.0013	Sub-Critical
2	3400.00	*****	.0013	Sub-Critical

```

*====*
*      Beginning 2 Profile Calculation(s)          *
*====*
  
```

```

***** W S P R O *****
Federal Highway Administration - U. S. Geological Survey
Model for Water-Surface Profile Computations.
Input Units: English / Output Units: English
  
```

```

*-----*
      I-69 OVER TIPPEY DITCH                I69-64-4767
COUNTY: GRANT                            QUAD: VAN BUREN 74D
      11-21-96                            BRET A. ROBINSON
  
```

===150 WARNING: SLOPE-CONVEYANCE CONVERGENCE FAILURE.  
 Used final trial values.  
 QCOMP, WSTRY: 1992. 842.69

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: EXIT	842.686	.423	2000.000	471.107	*****	29723.070
Header Type: XS	843.109	*****	4.245	56349.36	*****	29951.910
SRD: .000	838.468	*****	.641	*****	1.509	*****
Section: FULLV	842.800	.391	2000.000	497.874	61.000	29715.770
Header Type: FV	843.192	.074	4.017	58747.60	61.000	29956.220
SRD: 61.000	838.468	.000	.615	.0012	1.559	.009

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR ".  
 KRATIO: 1.44

# WSPRO OUTPUT

```

Section: APPR      843.236   .109   2000.000   1085.475   191.000  29613.400
Header Type: AS   843.345   .154     1.843   84380.31   191.000  30074.870
SRD:      252.000   841.178   .000     .305     .0008     2.070   -.001
  
```

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>

<<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	842.462	.915	2000.000	290.735	61.000	29824.280
Header Type: BR	843.377	.117	6.879	39115.89	61.000	29873.050
SRD: 61.000	839.656	.150	.554	*****	1.243	-.001

Specific Bridge Information	C	P/A	PFELEV	BLEN	XLAB	XRAB
Bridge Type 3	Flow Type 1					
Pier/Pile Code 0	.8969	.056	844.200	*****	*****	*****

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: APPR	843.762	.070	2000.000	1342.225	61.000	29589.720
Header Type: AS	843.831	.073	1.490	107351.50	72.363	30104.280
SRD: 252.000	841.178	.381	.231	.0008	2.014	.004

Approach Section APPR Flow Contraction Information						
M( G )	M( K )	KQ	XLKQ	XRKQ	OTEL	
.891	.509	52635.8	*****	*****	843.762	

<<< End of Bridge Hydraulics Computations >>>

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
 Model for Water-Surface Profile Computations.  
 Input Units: English / Output Units: English

\*-----\*

I-69 OVER TIPPEY DITCH	I69-64-4767
COUNTY: GRANT	QUAD: VAN BUREN 74D
11-21-96	BRET A. ROBINSON

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR

# WSPRO OUTPUT

```

Section: EXIT      844.079   .428   3400.000   888.451 ***** 29633.950
Header Type: XS   844.507 *****   3.827   96082.66 ***** 30004.480
SRD:      .000     840.700 *****   .597     *****   1.880     *****

Section: FULLV    844.198   .390   3400.000   933.408   61.000 29626.300
Header Type: FV   844.588   .073   3.643   100664.30 61.000 30008.990
SRD:      61.000   840.700   .000   .565     .0012   1.888     .008
  
```

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR ".  
 KRATIO: 1.53

```

Section: APPR     844.623   .103   3400.000   1822.677 191.000 29550.980
Header Type: AS   844.726   .143   1.865   153564.10 191.000 30152.410
SRD:      252.000  842.105   .000   .261     .0007   1.911   -.005
  
```

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>  
 <<< Beginning Bridge/Culvert Hydraulic Computations >>>

===220 FLOW CLASS 1 ( 4 ) SOLUTION INDICATES POSSIBLE PRESSURE FLOW.  
 WS3, WSIU, WS1, PFELV: 843.49 846.11 846.18 844.20

===245 ATTEMPTING FLOW CLASS 2 ( 5 ) SOLUTION.

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	844.100	1.467	3391.680	349.200	61.000	29821.000
Header Type: BR	845.567	*****	9.713	54041.84	*****	29876.000
SRD: 61.000	841.895	*****	.680	*****	1.000	*****

  

Specific Bridge Information	C	P/A	PFELEV	BLFN	XLAB	XRAB
Bridge Type 3	Flow Type 2					
Pier/Pile Code 0	.4924	.057	844.200	*****	*****	*****

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: APPR	847.100	.023	3400.000	3622.159	61.000	29439.500
Header Type: AS	847.123	.049	.939	355168.20	77.115	30290.890
SRD: 252.000	842.105	.709	.103	.0007	1.660	-.002

Approach Section APPR Flow Contraction Information						
M( G )	M( K )	KQ	XLKQ	XRKQ	OTEL	
*****	*****	*****	*****	*****	847.100	

# WSPRO OUTPUT

<<< End of Bridge Hydraulics Computations >>>

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

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I-69 OVER TIPPEY DITCH                      I69-64-4767  
COUNTY: GRANT                              QUAD: VAN BUREN 74D  
11-21-96                                      BRET A. ROBINSON

\*\*\* Live-Bed Contraction Scour Calculations for Header Record BRDGE \*\*\*

## Constants and Input Variables

\*-----\*

Bed Material Transport Mode Factor (k1):     .64  
Total Pier Width Value                        (Pw):    3.000

\*-----\*

#	Scour Depth	-- Flow --		-- Width --		--- X-Limits ---	
		Contract	Approach	Contract	Approach	Side	Contract Approach
1	7.063	2000.000	978.689	43.000	50.000	Left: *****	*****
	.....	Approach Channel Depth:	6.902	.....	Right: *****	*****	
2	13.969	2375.634	968.223	43.000	50.000	Left: *****	*****
	.....	Approach Channel Depth:	10.240	.....	Right: *****	*****	

\*\*\*\*\* W S P R O \*\*\*\*\*

Federal Highway Administration - U. S. Geological Survey  
Model for Water-Surface Profile Computations.  
Input Units: English / Output Units: English

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I-69 OVER TIPPEY DITCH                      I69-64-4767  
COUNTY: GRANT                              QUAD: VAN BUREN 74D  
11-21-96                                      BRET A. ROBINSON

\*\*\* Pier Scour Calculations for Header Record BRDGE \*\*\*

## Constants and Input Variables

Pier Width:     1.500

\*-----\*

Pier Shape Factor                            (K1):    1.00  
Flow Angle of Attack Factor                (K2):    1.00  
Bed Condition Factor                        (K3):    1.10  
Bed Material Factor                         (K4):    1.00  
Velocity Multiplier                         (VM):    1.00  
Depth Multiplier                            (YM):    1.00

\*-----\*

