

QUALITY ASSURANCE OF U.S. GEOLOGICAL SURVEY STREAM CURRENT METERS: THE METER- EXCHANGE PROGRAM 1988-98

by E.F. Hubbard, K.G. Thibodeaux, and Mai N. Duong

U.S. GEOLOGICAL SURVEY
Open-file Report 99-221

Reston, Virginia
1999

U.S. DEPARTMENT OF THE INTERIOR
BRUCE BABBITT, *Secretary*

U.S. GEOLOGICAL SURVEY
Charles G. Groat, *Director*

For additional information write to:

Chief, Office of Surface Water
U.S. Geological Survey, WRD
415 National Center
Reston, VA 20192

Copies of this report can be purchased from:

U.S. Geological Survey
Books and Open-File Reports Section
Federal Center
Box 25425
Denver, CO 80225

TABLE OF CONTENTS

Abstract	1
Introduction	2
Rating of Current Meters.....	3
Contribution of Instrument Error to Discharge-Measurement Error.....	5
Meter-Exchange Program.....	6
Failure Rate	6
Statistical Analysis	8
Effect of Discharge Measurement Error.....	11
Calculation of Effect	12
Conclusions and Actions	13
Conclusions	13
Actions	14
References	15

FIGURES

1. Assembly drawing of Price type AA current meter	2
2. Calibration results for AA meters in the Meter-Exchange Program	10
3. Calibration results for pygmy meters in the Meter-Exchange Program.....	11

TABLES

1. Accuracy criteria for Price type AA and pygmy current meters	4
2. Results of the Meter-Exchange Program through 1998	7
3. Calibration data for 128 Price AA meters, expressed in difference of standard rating velocity estimates from true velocities.....	9
4. Calibration data for 125 Price pygmy meters, expressed in difference of standard rating velocity estimates from true velocities.....	9

Quality Assurance of U.S. Geological Survey Stream Current Meters: The Meter-Exchange Program 1988-98

by E.F. Hubbard, K.G. Thibodeaux, and Mai N. Duong

Abstract

The U.S. Geological Survey principally uses two types of current meters for measurements of streamflow velocity, the Price AA meter and the Price pygmy meter. Through the Meter-Exchange Program, the U.S. Geological Survey has calibrated 128 AA current meters and 125 pygmy current meters selected from the field since the program began in 1988. The standard current-meter ratings developed for these meters failed to predict the true velocity for 36 percent of the AA meters and 59 percent of the pygmy meters to within the limits of long-standing accuracy criteria. Subsequent analysis of the calibration data showed that the standard ratings are no longer accurate estimators of the mean responsiveness of current meters used in the field and that calibration data from these meters tend to deviate farther from the mean than was previously thought. The amount, however, that velocity estimates from the standard rating tables deviated from true velocities measured during calibration of the meters was small. About 95 percent of all data points for AA meters at calibration velocities of 0.75 feet per second and faster were within -2.6 to +1.6 percent of the true velocity; for pygmy meters, 95 percent of the data points ranged from -2.6 to +4.6 percent at calibration velocities this fast and faster. At about 2.2 fps, the velocity estimated by the standard rating for AA meters averaged 0.5 percent less than the true velocity. The pygmy meters, in contrast, had velocities from the standard rating that averaged 1.2 percent more than the true velocities at this calibration point. A meter that responds differently than predicted by the standard rating has the potential for introducing error in a stage-discharge relation, and consequently, the gaging station streamflow record. These errors could be reduced or eliminated by developing new standard rating tables or by using individual meter ratings. Enhanced by an expansion of the Meter-Exchange Program to better monitor current-meter accuracy and an improved training program for hydrographers in the care and maintenance of current meters, either of these changes in current-meter ratings will improve the accuracy of streamflow records.

Introduction

The U.S. Geological Survey (USGS) principally uses two types of current meters for measurements of streamflow velocity, the Price AA meter and the Price pygmy meter. Through the Meter-Exchange Program, the USGS has calibrated 128 AA current meters and 125 pygmy current meters selected from the field since the program began in 1988. AA and pygmy current meters are vertical-axis current meters, having conical cups (or buckets) mounted on a bucket wheel that rotates in moving water. The speed of rotation is a precise indicator of the velocity of the water that impinges on the cups. Figure 1 is an assembly drawing of a AA current meter. A pygmy meter, which is similar but smaller, does not have a tail piece and has no penta-count mechanism (which allows aggregating the bucket-wheel revolutions into groups of five).

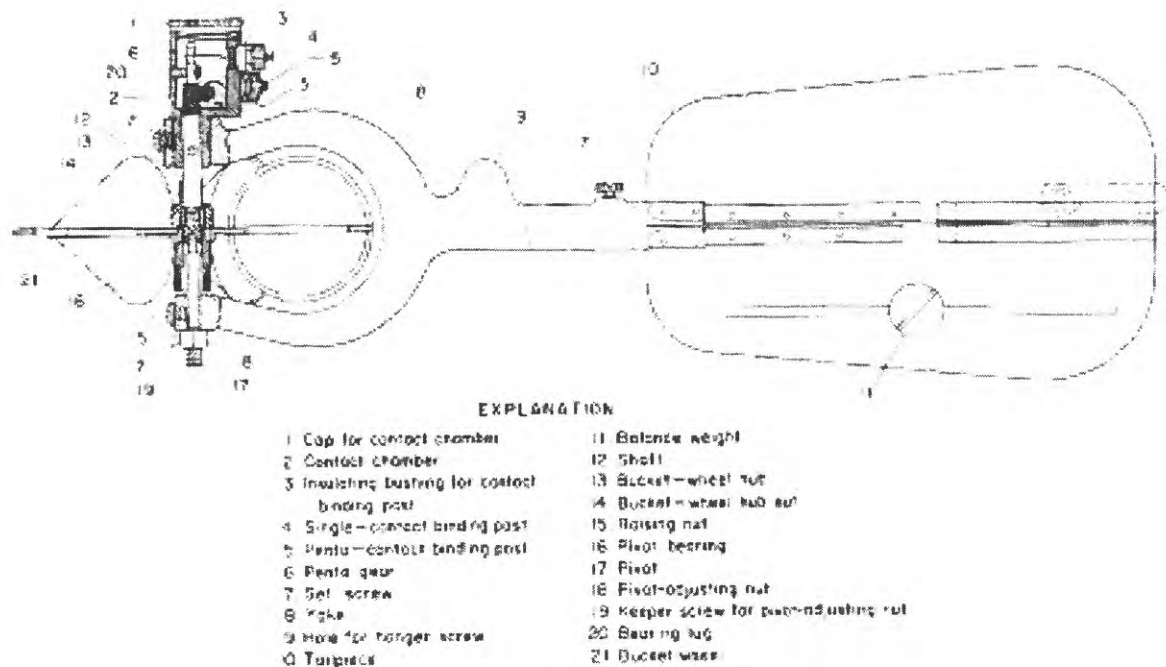


Figure 1: Assembly drawing of Price type AA current meter.

The AA meter is capable of accurately measuring a larger range of velocity, both slower and faster, than the pygmy meter. The pygmy meter was developed for use in shallower water depths than was the AA meter. An experienced hydrographer can obtain accurate measurements of discharge by using the velocities obtained with the appropriate meter in open-channel conditions where flows range from a flood in a river to a virtual trickle of water in a ditch.

Water velocities measured with current meters are used to compute the discharge data that the USGS publishes through various media. These discharges, which are used for flood warning and prediction; design of bridges, dams, and levees; legal agreements and compacts; planning; regulation; and research, should be based on the most accurate streamflow records that can be reasonably obtained.

This report describes the results of current-meter calibrations done for the Meter-Exchange Program in which meters are selected from the field for calibration. The purpose of this program is to learn how accurately the current meters, when used with standard rating tables, measure water velocities.

Rating of Current Meters

The USGS uses, with few exceptions, a standard rating for each type of current meter. These ratings are based on equations that relate the rotational velocity of the current-meter bucket wheel to the velocity of the water. Two equations define the range of velocities in which AA meters are used. These equations yield the same water velocity at 2.2 feet per second (fps), which is 1 revolution per second of the bucket wheel. Below 2.2 fps one equation is used; above that velocity, the other is used. For pygmy meters the entire range of velocity is defined by a single equation. The equations for each type of meter are converted to look-up tables (rating tables) for use in the field. Using a current-meter rating table, a hydrographer can convert observations of the number of revolutions of the meter bucket wheel in a given number of seconds directly into water velocities.

Before 1980 for pygmy meters and before 1970 for AA meters, each USGS current meter was rated separately and was issued with an individual rating table. Smoot and Carter (1968) showed that, within groups of meters from each of three manufacturers, an average (standard) rating gave nearly as accurate results as individual ratings. Subsequently, Schneider and Smoot (1976) demonstrated for pygmy meters that little additional error (generally a fraction of 1 percent) resulted from using a standard rating rather than individual meter ratings.

These and other similar investigations provided an opportunity for cost savings. If meters have nearly identical physical dimensions and responsiveness, then random samples can be tested, and thus avoid calibrating every meter in a batch of new meters. Use of standard ratings also permits replacement in the field of a principal component of a current meter, such as a bucket wheel, without having to have the meter recalibrated.

To determine if the responsiveness of a meter (in an “as-received” condition from the field or new from a manufacturer) is accurately described by an appropriate standard-rating equation, it is necessary to calibrate the meter in a tow tank or similar device. In a tow tank, a meter is towed horizontally through a long tank of still water where the number of bucket-wheel revolutions is recorded over very precisely measured distances and times. The meter is towed in both directions through the tank at each of several nominal calibration velocities to cover much of the range of velocities to be measured with the meter type. Averaging the calibration data in both directions ensures that they are not affected by any currents that may exist in the tank. These procedures are specified in more detail in the international standard, “Liquid flow measurement in open channels--Calibration of rotating-element current-meters in straight open tanks”, (International Organization for Standardization, 1976).

The USGS calibrates about 10 percent of the meters that are received in a batch from a manufacturer by using a tow tank in the Office of Surface Water Hydraulic Laboratory at Stennis Space Center, Mississippi. If one meter from the sample fails to meet the criteria established for

meter accuracy, another 10 percent of meters from the batch is calibrated. If any more meters fail to meet the criteria, then the entire batch of meters is calibrated, and only those that meet the accuracy criteria are accepted. (E. C. Hayes and D. R. Meyers, USGS Hydrologic Instrumentation Facility, written commun., 1998).

The accuracy criteria relative to the true velocity that is measured in the calibration process, are as follows:

Table 1: Accuracy criteria for Price type AA and pygmy current meters

Price AA current meter		Price pygmy current meter	
Velocity, in feet per second	Accuracy criterion, in percent	Velocity, in feet per second	Accuracy criterion, in percent
0.25	+/- 6.0	0.25	+/- 6.0
0.50	+/- 3.4	0.50	+/- 3.4
0.75	+/- 2.5	0.75	+/- 2.5
1.10	+/- 2.0	1.50	+/- 1.8
1.50	+/- 1.5	2.20	+/- 1.5
2.20	+/- 1.0	3.00	+/- 1.5
5.00	+/- 1.0		
8.00	+/- 1.0		

These accuracy criteria are based on much experimental data and have a statistical basis. The criteria are set at about 2 standard deviations of published current-meter calibration data (Smoot and Carter, 1968; Schneider and Smoot, 1976; and W.H. Kirby, written commun., 1998). Current meters that are subsequently calibrated meet the criteria if their velocities predicted from the appropriate standard rating falls within the plus or minus limits of the true velocity, which is measured during the calibration process. About 95 percent of current meters are expected to meet the criteria shown in table 1, if the calibration data are normally distributed and the standard rating is an accurate measure of the average responsiveness of the meters tested. International standard "Assessment of uncertainty in the calibration and use of flow measurement devices-Part 1: Linear calibration relationships," which was issued by The International Organization for Standardization (1989), also establishes the 2-standard-deviation criteria as being appropriate for calibration of current meters.

The accuracy criteria for whether a meter passes or fails in regard to the true velocity are applied with considerable judgement and latitude. If the standard rating does not predict (based on the rotational velocity of the bucket wheel) the actual velocity within the criteria at one calibration-data point, the possibility of a laboratory error is explored. If miscounting by the instrument that counts the bucket-wheels rotations is detected when inspecting the data, that data point is deleted or corrected to permit the meter to pass. If there are still one or more calibration-data points that are not within the criteria but are close (within about one tenth of a percent), the relationship between rotational velocity and water velocity that is defined by the individual meter's calibration data is generated. If this resulting equation (or equations in the case of the AA meters) plots within the accuracy criteria, the meter is judged to have passed, even if a calibration-data point or two is outside the limits. Finally, the rounding of the accuracy criteria as used in the

laboratory software is such that the limits are slightly larger than those shown in table 1. For example, the working criteria for the three faster velocities for the AA meter effectively has been 1.1 percent, instead of 1.0 percent (table 1).

The USGS counterparts in Environment Canada do not use standard ratings. Although they principally use the AA and pygmy meters, the Canadians feel it necessary to rate each meter individually. The meters that the Canadians use are periodically recalled to their hydraulic laboratory in Burlington, Ontario, to be rebuilt and re-rated (DeZeeuw and Bil, 1975). The laboratory also performs this function for meters owned by Canadian provinces, hydro-power companies, and others.

Contribution of Instrument Error to Discharge-Measurement Error

Instrument error is only one of several significant errors that may contribute to the overall error of a discharge measurement. Sauer and Meyer (1992) found that most measurements of discharge by current meters will have standard errors ranging from 3 to 6 percent. Poor measuring conditions (such as very slow water velocities or shallow depths) or improper procedures of meter use, however, can result in much larger errors. They cited important sources of error--other than the error contributed by the current meter--such as the measurement of depth, the pulsation of flow, the vertical distribution of velocities, the measurement of horizontal angles, and the computations involving the horizontal distribution of velocity and depth (insufficient number of or inadequate measuring subsections).

Sauer and Meyer estimated the total error of discharge measurements by taking the square root of the sum of the squares of the individual errors contributed by the various sources of error. The error associated with the current meter, which Sauer and Meyer termed "instrument error", was relatively small (0.3 percent) for AA meters used under ideal measuring conditions and following the recommended field procedures. For pygmy meters, the instrument error they used was still relatively small at 0.8 percent for a wading measurement with good field conditions. Their analysis properly used the standard error of estimate, which is 1 standard deviation of the calibration data used to develop the standard rating. Sauer and Meyer did not consider the case of a meter whose difference from the standard rating is near to or falls outside of the accuracy criteria, which is 2 standard deviations. Such a meter could contribute an instrument error up to about twice as large as they used.

In poorer field conditions where the velocity is slow, Sauer and Meyer found meter error to be a large source of error with respect to the other sources. Here again, they used the standard error of 1, not 2, standard deviations as the instrument error.

The errors associated with individual discharge measurements contribute to the error of the rating curve, which is the graphical relationship between stage and discharge for a streamflow gaging station. The rating-curve error is incorporated directly in the discharges that are computed and published for a station.

If several meters were employed in the development of the rating curve, instrument errors might off-set each other. This does not always happen in practice, however. Sometimes long periods go

by when one meter is predominately used to define the rating curve. Thus, any error in velocity data that is introduced by a current meter would be of concern.

Meter-Exchange Program

In 1988, the Office of Surface Water began the Meter-Exchange Program. One of the purposes of the program was to select meters being used in the field for calibration in the hydraulic laboratory tow tank. The reason for the calibration was to determine the accuracy of current meters as they are actually used in the field. The meters were selected by USGS technical review teams as they periodically reviewed the surface-water programs in field offices. The team members were asked to either select the meters at random or, if a meter in particularly poor physical condition was discovered, on the basis of appearance.

Current meters received in the hydraulic laboratory under this program were first calibrated without instrument adjustments or repairs. These calibration data of the “as-received” meters were retained as representative of the accuracy of meters being used in the field. Afterwards, the meters were repaired, adjusted, and recalibrated to ensure they fit within the accuracy criteria of the standard rating (table 1). The recalibrated meters were exchanged for other current meters selected during subsequent reviews. This program has continued until the present (1999).

Failure Rate

Through the Meter-Exchange Program, 128 AA and 125 pygmy meters have been calibrated (table 2). The results of the calibrations indicated that 46 AA and 74 pygmy meters failed to meet the accuracy criteria. Assuming that the calibration data average the same as predicted by the standard rating equations and are distributed normally, then only about 5 percent of the current meters should fall outside the 2-standard-deviation accuracy criterion. The actual failure rates, which are 36 percent for AA meters and 59 percent for pygmy meters, are unacceptably high.

Although the term, “failure rate”, is used to describe the percentage of current meters that did not fall with the accuracy criteria of the true velocities measured at calibration, it does not imply that the meters that failed were faulty or operated improperly. Almost all of the meters, in fact, operated satisfactorily. The standard ratings, however, did not predict the responsiveness to water velocity of the meters that failed within the established accuracy criteria. In other words, the bucket wheels of these meters turned unacceptably slower or faster for a given water velocity, causing the velocities estimated by the standard ratings to be outside of the accuracy limits around the true velocity.

The high failure rates gave rise to a concern that the meters selected because of poor physical condition were biasing the calibration results. To investigate this concern, the calibration data were divided into three groups: meters selected at random, meters selected non-randomly because of poor appearance, and meters for which there is no information concerning the basis for selection. These data are summarized in table 2.

Table 2: Results of the Meter-Exchange Program through 1998

ALL METERS			
Meter Type	No. of Meters Meeting Accuracy Criteria	No. of Meters Failing to Meet Accuracy Criteria	Percent Failing
AA	82	46	36
Pygmy	51	74	59

METERS SELECTED AT RANDOM			
Meter Type	No. of Meters Meeting Accuracy Criteria	No. of Meters Failing to Meet Accuracy Criteria	Percent Failing
AA	65	35	35
Pygmy	40	62	61

METERS HAVING NON-RANDOM SELECTION (Poor Physical Condition)			
Meter Type	No. of Meters Meeting Accuracy Criteria	No. of Meters Failing to Meet Accuracy Criteria	Percent Failing
AA	9	8	47
Pygmy	8	4	33

METERS HAVING UNKNOWN SELECTION CRITERIA			
Meter Type	No. of Meters Meeting Accuracy Criteria	No. of Meters Failing to Meet Accuracy Criteria	Percent Failing
AA	8	3	27
Pygmy	3	8	73

There appears to be little difference in the failure rate among the meters in the three categories shown in table 2. The exceptions are that the non-randomly selected AA meters had a somewhat higher rate of failure than that of other AA-meter categories, and the non-randomly selected pygmy meters had a lower rate of failure than that of other pygmy-meter categories. Perhaps technical reviewers were better able to visually discern problems with the AA meters than with the pygmy meters. The physical appearance of a meter, however, is not necessarily a good indicator of whether the meter will fail or meet the accuracy criteria. Even a spin test of a meter is not a good indicator of whether a meter will pass or fail (K.G. Thibodeaux, oral commun., U.S. Geological Survey, 1999). Thibodeaux cites instances of AA meters that had timed spin tests of about 1 minute that met the accuracy criteria, even though this time is well below the minimum spin-test standard of 2 minutes (Hubbard and Barker, 1995).

Because the failure rates of meters chosen at random were virtually the same as that for all three groups combined, those meters chosen on non-random and unknown bases are deemed representative of the entire group and, probably, of the population of current meters used by the USGS. Thus, all the calibration data, regardless of the selection criteria, are used in this analysis.

The apparent causes of meters failing to meet the accuracy criteria were diverse. The physical conditions noted for the meters that failed and the corrective action taken was recorded for each meter that failed. Based on experiences in rebuilding and calibrating current meters in the laboratory, the following general observations are provided:

Conditions that do not usually affect meter responsiveness:

- Cups slightly bent,
- Dull pivot,
- Pivot adjustment too loose, and
- Yoke out of alignment (AA meter).

Conditions that may adversely affect meter responsiveness:

- Pivot burred,
- Penta gear out of adjustment,
- Pivot adjustment too tight,
- Yoke out of alignment (pygmy meter), and
- Non-standard bucket wheel.

Statistical Analysis

Tables 3 and 4 summarize the results of the calibration of meters in an “as-received” condition. These statistics represent all meters from the Meter-Exchange Program, although a few individual calibration runs were deleted from the data as spurious outliers. (Calibration data from forward and reverse directions at each nominal velocity were averaged for individual meters to minimize the effects of currents in the tow tank. Thus, the term “calibration run” represents both forward and reverse directions at one of the calibration velocities.)

The average differences and prediction intervals in tables 3 and 4 are calculated to compare with the established accuracy tolerances (table 1) and with the instrument errors that are assumed when estimating overall discharge-measurement error. The statistics are based on the difference, for an individual meter, between the velocity estimated by the standard rating, using the rotational velocity of the bucket wheel, and the measured (true) velocity for each calibration run (forward and reverse averaged). Thus, for all AA meters at a calibration velocity of 0.25 fps (table 3, first row, col. 1), the average difference of the velocities estimated using the standard rating from the actual velocities is -1.06 percent (col. 2). In column 3, the standard deviation of all the individual meter differences is listed for each calibration velocity. Prediction intervals at 1 standard deviation are shown in column 4. The standard deviation used to define the prediction interval corresponds to the standard deviation of the difference between a non-sampled meter’s standard- rating velocity estimate and the true velocity. The prediction interval is equal to the square root of the sum of the variance of the individual differences and the variance of the average difference. The prediction intervals listed in column 5 correspond to 2 standard deviations.

Table 3: Calibration data for 128 Price AA meters, expressed in difference of standard rating velocity estimates from true velocities

Average calibration velocity, in feet per second (1)	Average difference, in percent (2)	Standard deviation, in percent (3)	Predictions interval at 1 standard deviation, in percent (4)		Prediction interval at 2 standard deviations, in percent (5)	
0.25	-1.06	2.56	-3.63	1.51	-6.20	4.08
0.50	-0.18	1.05	-1.23	0.87	-2.29	1.93
0.75	-0.10	0.84	-0.94	0.74	-1.79	1.59
1.10	-0.41	0.84	-1.25	0.43	-2.10	1.28
1.51	-0.51	0.88	-1.39	0.37	-2.28	1.26
2.22	-0.50	0.92	-1.42	0.42	-2.35	1.35
5.01	-0.51	0.95	-1.46	0.44	-2.42	1.40
8.01	-0.66	0.94	-1.60	0.28	-2.55	1.23

At calibration velocities faster than 1 fps, the AA-meter bucket wheels turned 0.41 to 0.66 percent slower than estimated using the standard rating (table 3, col. 2). That is, the meters turned more slowly than expected for a given true velocity and, thus, would yield a velocity from the standard rating table that is slower than the true velocity. On the other hand, the pygmy meters, generally turned faster than predicted by the standard rating, yielding velocities as much as 1.32 percent faster than the true velocity (table 4, col. 2).

Table 4: Calibration data for 125 Price pygmy meters, expressed in difference of standard rating velocity estimates from true velocities

Average calibration velocity, in feet per second (1)	Average difference, in percent (2)	Standard deviation, in percent (3)	Predictions interval at 1 standard deviation, in percent (4)		Prediction interval at 2 standard deviations, in percent (5)	
0.25	-1.40	4.07	-5.49	2.69	-9.57	6.77
0.50	0.22	1.72	-1.51	1.95	-3.23	3.67
0.75	0.81	1.43	-0.63	2.25	-2.06	3.68
1.51	0.72	1.68	-0.97	2.41	-2.65	4.09
2.21	1.17	1.61	-0.45	2.79	-2.06	4.40
3.01	1.32	1.63	-0.32	2.96	-1.95	4.59

At calibration velocities of 0.75 fps and faster, the standard deviations of the differences from the true velocity are 0.84 to 0.95 percent for the AA meter (table 3, col. 3). Assuming a normal distribution of the average-difference data, about two-thirds of calibration-run results for untested meters are expected to fall within the prediction interval (col. 4).

About 95 percent of the AA-meter calibration data are expected to be within the prediction interval at 2 standard deviations of the mean. (The mean is shown as the average difference in table 3 col. 2.) For a calibration velocity of 2.22 fps the prediction interval at 2 standard

deviations goes from -2.35 to +1.35 percent (col. 5). The range of this prediction interval is more than that of the established accuracy tolerance interval of plus or minus 1.0 percent shown in table 1. For AA meters from the Meter-Exchange Program at calibration velocities of 0.75 fps and faster, the prediction intervals at 2 standard deviations for the standard rating range from -2.55 to +1.59 percent (table 3, col. 5) of the true velocities. This variability in calibration data and the differences from the true velocity for AA meters can be seen in figure 2.

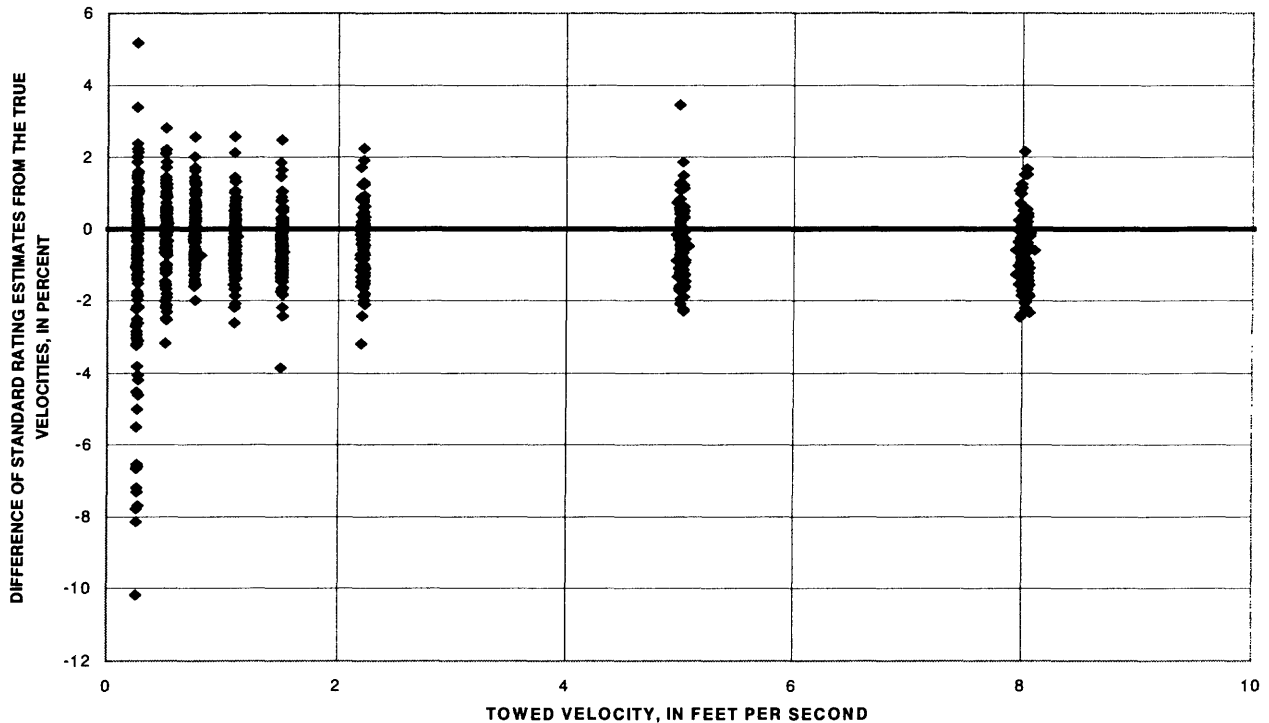


Figure 2: Calibration results for AA meters in the Meter-Exchange Program.

For pygmy meters at a calibration velocity of 2.21 fps, the prediction interval at 1 standard deviation for the standard rating is from -0.45 to +2.79 percent of true velocities and from -2.06 to +4.40 percent at 2 standard deviations (col. 5). The prediction interval at 2 standard deviations is more than the plus or minus 1.5 percent interval allowed for pygmy meters at this velocity (table 1). At calibration velocities of 0.75 fps and faster, pygmy meters from the Meter-Exchange Program have a prediction interval at 2 standard deviations that ranges from -2.65 to +4.59 percent of the true velocities (table 4, col. 5).

Similar to the AA meters, the pygmy-meter responsiveness exhibits both an average difference (shown in table 4, col. 2) and more variability (col. 5) than is permitted by the tolerances associated with the standard rating (table 1). This variability in calibration data and the differences from the true velocity for pygmy meters can be seen in figure 3.

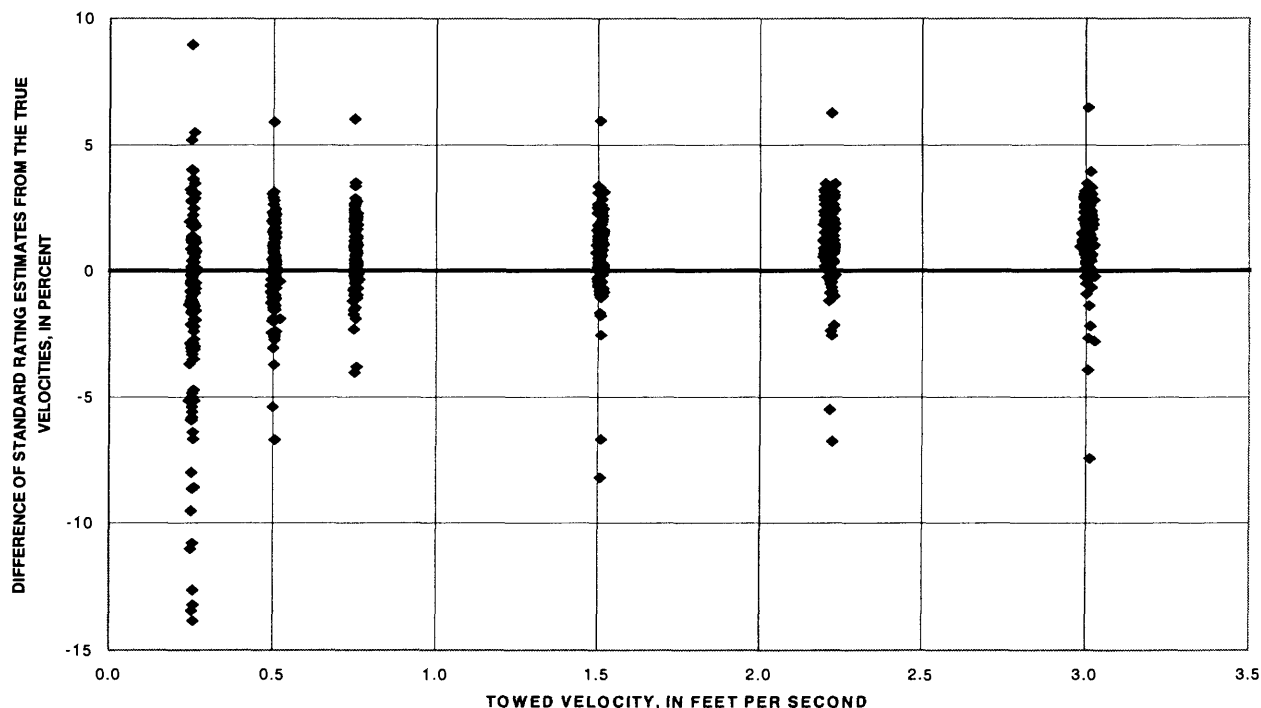


Figure 3: Calibration results for pygmy meters in the Meter-Exchange Program.

Effect on Discharge Measurement Error

The standard rating tables are expected to predict calibration data for current meters with a small difference from the true velocity. This expectation of a small variation of calibration data around the true velocities, which is based on the results of Smoot and Carter (1968), led Sauer and Meyer (1992) to use an instrument error for AA meters of 0.3 percent for velocities of 2.3 fps and faster. The Meter-Exchange Program calibration data show that AA meters from the field calibrated at 2.2 fps have a average difference from the standard rating of -0.50 percent (table 3, col. 2) and a standard deviation of 0.92 percent (col. 3). The prediction interval of the standard rating table at 1 standard deviation for this group of AA meters ranges from -1.42 to +0.42 percent of the true velocity at 2.22 fps (col. 4). This range in error is significantly larger than the plus or minus 0.3 percent used in Sauer and Meyer's equations for velocities of 2.3 fps and faster.

Similarly, on the basis of data from Schneider and Smoot (1976), Sauer and Meyer (1992), used instrument errors for pygmy meters that ranged from 5.14 percent at 0.25 fps to 1.42 percent at 3.0 fps. The pygmy meters, like the AA meters, that were tested in the Meter-Exchange Program had an average difference (bias) from the standard rating. These meters also had a standard deviation that was larger than expected. The prediction interval at 1 standard deviation ranges from as much as -5.49 percent of the true velocity at 0.25 fps to +2.96 percent at 3.01 fps (table 4, col. 4). The difference in velocities predicted by the standard ratings for field AA and pygmy meters from true velocities is larger than the instrument errors used by Sauer and Meyer (1992).

The changes in average responsiveness of meters that have occurred since the standard ratings were implemented probably result from small changes in the physical dimensions of bucket wheels or in other factors affecting meter responsiveness. The larger variability in responsiveness that is seen in the Meter-Exchange Program meters as contrasted to the meters on which the standard ratings are based may result from the treatment that the two groups of meters had received and from the sources of manufacture. For example, the results of calibration data cited in Smoot and Carter (1968) are from AA current meters in new or nearly new condition, and apparently, from a few manufacturing runs. The data from the Meter-Exchange Program are from a sample of meters subjected to normal wear and tear over a varying numbers of years. These meters came from many manufacturing runs. These contrasts may explain the larger variability seen in the calibration data from the Meter-Exchange Program. Nevertheless, the concept of using standard rating tables is predicated on having meters in the field that measure water velocity within accepted accuracy tolerances of the true velocity.

Calculation of Effect

For AA meters, Sauer and Meyer used a standard error of 0.3 percent to compute the overall error of a good cable-suspension as 2.4 percent¹. Had the larger value of -1.42 percent (table 3, col. 4) from the Meter-Exchange Program data at 2.22 fps been used, the error of this measurement would have increased to 2.8 percent. These calculations are made below:

$$S_f = \sqrt{\left(\frac{S_d^2 + S_v^2}{N} \right) + S_i^2 + S_s^2 + S_h^2 + S_v^2 + 0.75} \quad \text{(Equation 14, from Sauer and Meyer)}$$

where:

S_q is the standard error (se), in percent, for an individual measurement;

S_d is the se, in percent, associated with measurement of depth;

S_i is the se, in percent, associated with velocity pulsations;

N is the number of verticals;

S_i is the se, in percent, associated the instrument (current meter);

S_s is the se, in percent, associated for the vertical distribution of velocity;

S_h is the se, in percent, associated with horizontal angles;

S_v is the se, in percent, associated the horizontal distribution of velocity and depth; and the constant value 0.75 is the se, in percent, associated with the systematic errors in the measurement of width, depth and velocity.

Thus, Sauer and Meyer (1992) made the following calculation of S_q for a good cable-suspension measurement:

¹ The computations are made using equation 14, which appears on page 17 of Sauer and Meyer (1992). The procedure is basically taking the square root of the sum of squares of the errors associated with various factors, including instrument error. Sauer and Meyer's results for typical measurements are listed in their table 7 on page 19.

$$S_f = \sqrt{\left(\frac{(2.0)^2 + (3.9)^2}{28}\right) + (0.3)^2 + (1.2)^2 + (0)^2 + (1.7)^2 + 0.75} = 2.4 \text{ percent.}$$

If S_i is increased from 0.3 to 1.42 percent, then:

$$S_f = \sqrt{\left(\frac{(2.0)^2 + (3.9)^2}{28}\right) + (1.42)^2 + (1.2)^2 + (0)^2 + (1.7)^2 + 0.75} = 2.8 \text{ percent.}$$

For pygmy meters, Sauer and Meyer used an instrument error of 0.8 percent to compute an overall discharge-measurement error of 4.0 percent for a typical good wading measurement with an average velocity of 1.5 fps. At a calibration velocity of 1.5 fps, pygmy meters from the Meter-Exchange Program have a prediction interval at 1 standard deviation from the true velocity ranging up to 2.41 percent (table 4, col. 4). Using this larger percentage in the equation results in an increase in the overall error of the example pygmy meter wading measurement to 4.6 percent.

Thus, the increase in estimated error for a good cable-suspension discharge measurement made with a AA meter is only 0.4 percent (2.8 percent-2.4 percent). The increase in estimated error for a good wading measurement made with a pygmy meter is 0.6 percent. These increases in overall measurement error are inconsequential, except for the fact that both groups of meters, AA's and pygmys, have average differences from the standard ratings. These differences affect the streamflow gaging station stage-discharge ratings, which results in systematic errors in USGS records of streamflow. The errors in streamflow are small, being similar to the average differences in col. 2 of tables 3 and 4, but they could be largely eliminated. Two ways to eliminate the systematic errors are to develop new standard rating tables that more nearly reflect the average responsiveness of meters or to use individual current-meter rating tables.

Conclusions and Actions

Conclusions

The Meter-Exchange Program data show that the standard-rating fails to predict the water velocities measured by 36 percent of the Price AA meters and 59 percent of the Price pygmy within the accepted accuracy criteria of about 2 standard deviations from the true velocities. Only about 5 percent of the meters would be expected to have predicted velocities that fall outside the accuracy criteria. Thus, the rate of failure is much higher than was envisioned when the standard rating tables for the meters were prepared.

Even though the failure rate is high, the resultant error in velocity measurement is small. For the AA-meter calibration data, which has less variability than the pygmy-meter data, the maximum difference from velocities predicted by the standard rating at 2 standard deviations is about -2.6 percent in the range of 0.75 to 8.00 fps. For pygmy meters, the maximum average difference from the standard rating is about +4.6 percent at calibration velocities ranging from 0.75 to 3.00 fps.

Error associated with the current meter is only one of the errors encountered in measuring discharge. For this reason, instrument error has to be relatively large to increase the overall error of a discharge measurement more than the ± 5 percent level, which is assumed to be the maximum error when “good” conditions are indicated on the front of the measurement notes sheet. For velocities of 0.75 to 8.00 fps, it is very unlikely that the size of errors in velocity seen in the Meter-Exchange Program AA-meter calibration data would result in a discharge measurement, which was made under good conditions, having an overall error exceeding 5 percent. It would be somewhat unlikely for the discharge-measurement error to exceed 5 percent when using a pygmy meter under similar measuring conditions. Under worse measuring conditions, except for low velocities, the meter error would have even less influence on the overall error of the discharge measurement.

Be that as it may, for a gaging station where a hydrographer consistently uses a meter, which has a difference in response of, say, 2 to 4 percent from that predicted by the standard rating, the stage-discharge rating for that gage will have similar error. Such an error could add up to thousands of acre-feet of water that were unaccounted for or that were over reported. An error of this size might throw off a flood forecast or otherwise mislead users of USGS data. The USGS has an obligation to reduce these errors, if it can reasonably do so.

Through the Meter-Exchange Program, 253 Price type AA and pygmy meters were calibrated in the 11-year period since its inception in 1988--about 11 or 12 meters of each type per year. This annual sample of calibrated meters is too small to evaluate whether the average responsiveness of meters used in the field is changing from year to year. The sample may also be too small over a period of a few years to identify causative factors in meters that fail to meet the accuracy criteria. Today, technical reviewers do not have the data needed to help identify causative factors of the velocity-accuracy problems in the meters they select. Such factors might include age, amount or frequency of use, environmental conditions under which the meters are used, instrument-care procedures, and so forth. Even since the inception of the program in 1988, the entire sample is too small to differentiate among selection-criteria categories, such as poor physical condition or random selection.

Meters returned to the hydraulic laboratory for calibration are almost always returned to the Meter-Exchange Program after the repairs and adjustments are made. The subsequent recalibration data has shown that these rebuilt and adjusted meters, as a group, have less variability in response than when the same group of meters were calibrated in an “as-received” condition. Thus, better procedures for current-meter maintenance in the field would prevent some of the problems found in the Meter-Exchange Program.

Actions

1. With support from other USGS division organizations, the Office of Surface Water continues to investigate ways to reduce the variability and error (with respect to standard rating tables) in current meters being used in the field. This investigation includes:
 - Development of new standard ratings,
 - Consideration of returning to the use of individually rated meters, and

- Learning the factors that cause the responsiveness of meters to depart from standard ratings.
2. The Meter-Exchange Program is being expanded to become a comprehensive quality-assurance program for current meters as they are being used in the field. Goals for the expanded program are:
 - Provide a statistically valid basis to defend the accuracy of the current meters used in the field and the resulting stage-discharge relations,
 - Identify causative factors for failure of current meters to meet the accuracy criteria,
 - Test a sufficient number of meters each year to monitor and detect trends in meter responsiveness, and
 - Provide feedback on meter accuracy to hydrographers.
 3. The USGS Office of Surface Water has increased training on the care, repair, and adjustment of current meters by sponsoring informal meter-maintenance workshops. Regional courses are also a very good means to provide training, because they can be taught at USGS regional and field offices to reach, in a timely manner, the people who most need the instruction.

REFERENCES

- DeZeeuw, C., and Bil, C., 1975, Repair and maintenance manual of the Price current meter, Canada Centre for Inland Water, National Calibration Service, Burlington, Ontario, p 5.
- Hubbard, E.F., and Barker, Allison Randolph, 1995, Selected surface-water technical memorandums of the U.S. Geological Survey: U.S. Geological Survey Open-File Report 95-354, p. 201.
- International Organization for Standardization, 1989, Assessment of uncertainty in the calibration and use of flow measurement devices-Part 1: Linear calibration relationships: ISO 7066-1: 1989 (E), 39 p.
- International Organization for Standardization, 1976, Liquid flow measurement in open channels- Calibration of rotating-element current-meters in straight open tanks: ISO 3455-1976, 8 p.
- Schneider, V. R., and Smoot, G. F., 1976, Development of a standard rating for the Price Pygmy current meter: U.S. Geological Survey Journal of Research, vol. 4, no. 3, p. 293-297.
- Smoot, G. F., and Carter, R. W., 1968, Are individual current meter ratings necessary? American Society of Civil Engineers Journal of the Hydraulics Division, 94 (HY2), p. 391-397.
- Sauer, V. B., and Meyer, R. W., 1992, Determination of error in individual discharge measurements: U.S. Geological Survey, Open-File Report 92-144, 21p.