Prepared in cooperation with the Bureau of Land Management, Wyoming State Office Reservoir Management Group

## Megascopic Lithologic Studies of Coals in the Powder River Basin in Wyoming and in Adjacent Basins in Wyoming and North Dakota



Cover. Photographs showing coal and core-drilling activities. (All photographs by Michael H. Trippi, except as noted.)
Top, Coalbed-methane drill site in the Powder River Basin in Montana.
Left middle, Drilling crew removing coal core from core barrel.
Right middle, Coal core segment being placed in gas desorption canister. (Photograph by Margaret S. Ellis.)
Bottom, Section of coal core split open for lithologic examination, showing alternating vitrain (shiny) and attrital (dull) bands.

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By Michael H. Trippi, Gary D. Stricker, Romeo M. Flores, Ronald W. Stanton, Lora A. Chiehowsky, and Timothy A. Moore

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## Conversion Factors

|  | Multiply | By |
| :--- | :---: | :--- |
|  | To obtain |  |
| inch (in.) | Length |  |
| inch (in.) | 2.54 | centimeter (cm) |
| foot (ft) | 25.4 | millimeter $(\mathrm{mm})$ |
|  | 0.3048 | meter $(\mathrm{m})$ |
| cubic foot per ton $\left(\mathrm{ft}^{3} / \mathrm{ton}\right)$ | 0.0312 | Volume |

# Megascopic Lithologic Studies of Coals in the Powder River Basin in Wyoming and in Adjacent Basins in Wyoming and North Dakota 

By Michael H. Trippi, ${ }^{1}$ Gary D. Stricker, ${ }^{2}$ Romeo M. Flores, ${ }^{2}$ Ronald W. Stanton, ${ }^{3}$ Lora A. Chiehowsky, ${ }^{1}$ and Timothy A. Moore ${ }^{4}$

## Introduction

Between 1999 and 2007, the U.S. Geological Survey (USGS) investigated coalbed methane (CBM) resources in the Wyoming portion of the Powder River Basin (PRB) (fig. 1). The study also included the CBM resources in the North Dakota portion of the Williston Basin (WB) of North Dakota and the Wyoming portion of the Green River Basin (GRB) of Wyoming (fig. 1). This project involved the cooperation of the State Office, Reservoir Management Group (RMG) of the Bureau of Land Management (BLM) in Casper, Wyo., and 16 independent gas operators in the Powder River, Williston, and Green River Basins. The USGS and BLM entered into agreements with these CBM operators to supply samples for the USGS to analyze and provide the RMG with rapid, timely results of total gas desorbed, coal quality, and high-pressure methane adsorption isotherm data (Stricker and others, 2006, 2007). This program resulted in the collection of 963 cored coal samples (also called canister samples, or simply canisters, in this report) from 37 core holes (also called wells in this report; fig. 1, table 1). This report presents megascopic lithologic descriptive data collected from canister samples extracted from the 37 wells cored for this project.

## Objectives

The purpose of this study was to determine if there was any relationship between the parameters studied and the volumes of gas generated by the coals sampled. This report contains data, summary tables, histograms, and charts of coal analyses for the megascopic petrologic characteristics of the coal in the region. For each unit (a lithologically distinct subdivision of a canister sample) described, the following characteristics were recorded: cumulative fusain thickness; lithotype

[^1]code; cleat spacing; cleat frequency; the percentages of vitrain, attritus, and fusain; and the average attrital band thickness and vitrain band thickness.

Included in this report are data and summaries, as needed, from the two previous reports on gas desorption and coal quality for these 37 core holes (Stricker and others, 2006; and Stricker and others, 2007, respectively).

## General Geology

## Powder River Basin

The coal beds that were sampled from the Powder River Basin are in the Tongue River Member of the Paleocene Fort Union Formation (fig. 2) and include, in ascending order, the Roberts, Cache, Pawnee, Wall, and Cook coal beds and beds in the Wyodak-Anderson coal zone (including the Werner, Canyon-Wyodak, Anderson-Big George, School, and Smith coal beds). The Tongue River Member contains the thick coal beds and coal zones that are targets for coal mining and coalbed-methane production. The names of the sampled coal beds are those given by gas operators and do not necessarily follow USGS names and correlations as established in earlier studies by Mapel (1973), Culbertson and others (1979), Kent (1986), Flores, Ochs, and others (1999), and Luppens and others (2008). See Stricker and others (2007) for explanations of some of these inconsistencies. Flores and others (2005) show the confusion that has arisen in the naming and correlation of the Cook, Canyon, and Anderson coal beds by gas operators in two different adjacent lease areas of the PRB. The stratigraphic positions and correlations of the Wyodak-Anderson coal zone are considered to be less problematic than those involving coal beds lower in the stratigraphic section (see Flores, Ochs, and others, 1999; McGarry and Flores, 2004). Thirty-four core holes penetrated several different coal beds in the Powder River basin, as follows (in ascending order): Roberts coal bed, core hole 29; Cache coal bed, core hole 27; Pawnee coal bed, core holes 25, 27, 36, and 37; Wall coal bed, core holes 4 and 6; Cook coal


Figure 1. Map showing the location of the 37 core holes that were sampled for this study of the coalbed methane resources in the Wyoming part of the Powder River and Green River Basins, and the North Dakota part of the Williston Basin.


Figure 2. Stratigraphic column for the Fort Union Formation in the Powder River Basin, Wyoming and Montana, showing location of sampled coal beds.

Table 1. Core holes used in coal studies, Wyoming part of the Powder River and Green River Basins, and the North Dakota part of the Williston Basin.
[Abbreviations are as follows: GRB, Green River Basin; N., north; NA, no API number; n.d., no data recorded; NE, northeast; NW, northwest; SE, southeast; SW, southwest; N.D., North Dakota; PRB, Powder River Basin; R., range; sec., section; T., township; W., west; WB, Williston Basin; Wyo., Wyoming]

| Core hole number | Gas operator | Core hole name | American Petroleum Institute (API) well number | State |
| :---: | :---: | :---: | :---: | :---: |
| 1 | MichiWest Energy, Inc. | Pilot State 16-14 | 049-019-21068 | Wyo. |
| 2 | MichiWest Energy, Inc. | Pilot State 16-32 | 049-019-21071 | Wyo. |
| 3 | Ocean Energy, Inc. | Schlautmann 9-10-45-74WY (Ocean 43-10C) | 049-005-34173 | Wyo. |
| 4 | Pennaco Energy, Inc. | Sorenson 2-33-54-74W | 049-005-35137 | Wyo. |
| 5 | Barrett Resources Corp. | Haas 32-31 | 049-005-35287 | Wyo. |
| 6 | CMS Oil and Gas Co. | West 6-19W | 049-005-35339 | Wyo. |
| 7 | Gregory Water and Energy, Inc. | Leroy Gregory 1 | NA | N.D. |
| 8 | CMS Oil and Gas Co. | Laramore 11-6C | 049-005-37516 | Wyo. |
| 9 | Kennecott Energy | Kennecott CBM-1 | NA | Wyo. |
| 10 | Kennecott Energy | Kennecott CBM-2 | NA | Wyo. |
| 11 | Barrett Resources Corp. | CARU State 22-16-5075W | 049-005-38103 | Wyo. |
| 12 | Barrett Resources Corp. | Schoonover Road Unit (SRU) State 12-16-4876 | 049-005-36110 | Wyo. |
| 13 | Rim Operating, Inc. | CBM H-11-04 | 049-005-37359 | Wyo. |
| 14 | Rim Operating, Inc. | CBM C-33-1R | 049-005-37386 | Wyo. |
| 15 | Peabody Natural Gas, LLC | PNG 34-1 | NA | Wyo. |
| 16 | Peabody Natural Gas, LLC | PNG 33-1 | NA | Wyo. |
| 17 | Peabody Natural Gas, LLC | PNG 31-1 | NA | Wyo. |
| 18 | Peabody Natural Gas, LLC | PNG 35-1 | NA | Wyo. |
| 19 | Barrett Resources Corp. | All Night Creek (ANCU) Iberlin 21-33-4374 | 049-005-37965 | Wyo. |
| 20 | Peabody Natural Gas, LLC | PNG 16-2 | NA | Wyo. |
| 21 | The Coteau Properties Co. | Coteau MC00250C | NA | N.D. |
| 22 | The Coteau Properties Co. | Coteau MC00251 | NA | N.D. |
| 23 | Ammonite Energy Texas, Inc. | Thomas Jefferson State 36-3 | 049-009-22996 | Wyo. |
| 24 | Bridger Coal Co. | BCX-9 | NA | Wyo. |
| 25 | Peabody Natural Gas, LLC | PNG Duvall 13J-D | 049-005-44594 | Wyo. |
| 26 | Barrett Resources Corp. | KU Harriett 41-34-4777 | 049-019-21774 | Wyo. |
| 27 | Peabody Natural Gas, LLC | PNG Carter-Federal 18F-D | 049-005-37063 | Wyo. |
| 28 | Nance Petroleum Corp. | Remington 58-79-30-07A | 049-033-23127 | Wyo. |
| 29 | Nance Petroleum Corp. | Remington 57-79-18-03R | 049-033-23136 | Wyo. |
| 30 | Nance Petroleum Corp. | Remington 58-79-30-01C | 049-033-23131 | Wyo. |
| 31 | Williams Production RMT Co. | Bullwacker Creek Unit (BCU) 32-9-4277 | 049-019-21969 | Wyo. |
| 32 | Lance Oil and Gas Company, Inc. | Whiskey Draw Unit 12-12-4778 | 049-019-22873 | Wyo. |
| 33 | Lance Oil and Gas Company, Inc. | McBeth 12-30-4673-BG | 049-005-50378 | Wyo. |
| 34 | Williams Production RMT Co. | State 23-16-4171 | 049-005-50711 | Wyo. |
| 35 | Williams Production RMT Co. | Groves 12-19-4574 | 049-005-51276 | Wyo. |
| 36 | Peabody Natural Gas, LLC | PNG 24-1 | NA | Wyo. |
| 37 | Peabody Natural Gas, LLC | PNG 26-1 | NA | Wyo. |

Table 1. Core holes used in coal studies, Wyoming part of the Powder River and Green River Basins, and the North Dakota part of the Williston Basin.-Continued
[Abbreviations are as follows: GRB, Green River Basin; N., north; NA, no API number; n.d., no data recorded; NE, northeast; NW, northwest; SE, southeast; SW, southwest; N.D., North Dakota; PRB, Powder River Basin; R., range; sec., section; T., township; W., west; WB, Williston Basin; Wyo., Wyoming]

| Core hole number | Basin | Latitude (in decimal degrees) | Longitude (in decimal degrees) | Section, township, and range | Date cored | Lithologic description method (table 3) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | PRB | 44.12838 N . | 106.12824W. | SW1/4SW1/4 sec. 16, T. 48 N., R. 77 W. | 01/27/1999 | A |
| 2 | PRB | 44.13568 N . | 106.11822W. | SW1/4NE1/4 sec. 16, T. 48 N., R. 77 W. | 04/07/1999 | A |
| 3 | PRB | 43.88730 N . | 105.73104W. | NE1/4SE1/4 sec. 10, T. 45 N., R. 74 W. | 06/25/1999 | A |
| 4 | PRB | 44.62333 N . | 105.76500 W . | NW1/4NE1/4 sec. 33, T. 54 N., R. 74 W. | 08/13/1999 | n.d. |
| 5 | PRB | 44.00851 N . | 105.67651W. | SW1/4NE1/4 sec. 31, T. 47 N., R. 73 W. | 09/24/1999 | n.d. |
| 6 | PRB | 44.81796 N . | 105.93621 W . | SE1/4NW1/4 sec. 19, T. 56 N., R. 75 W. | 09/27/1999 | n.d. |
| 7 | WB | 47.23228 N . | 103.14541W. | SE1/4SE1/4 sec. 6, T. 143 N., R. 98 W. | 10/13/1999 | n.d. |
| 8 | PRB | 44.51333 N . | 105.93560 W . | NE1/4SW1/4 sec. 6, T. 52 N., R. 75 W. | 12/10/1999 | A |
| 9 | PRB | 43.71728 N . | 105.27447W. | SW1/4NW1/4 sec. 9, T. 43 N., R. 70 W. | 01/05/2000 | C |
| 10 | PRB | 43.72136 N . | 105.27680 W . | SW1/4NW1/4 sec. 9, T. 43 N., R. 70 W. | 01/06/2000 | A |
| 11 | PRB | 44.31003 N . | 105.88602W. | SE1/4NW1/4 sec. 16, T. 50 N., R. 75 W. | 02/20/2000 | A |
| 12 | PRB | 44.13523 N . | 106.00883 W . | SW1/4NW1/4 sec. 16, T. 48 N., R. 76 W. | 02/29/2000 | A |
| 13 | PRB | 43.73564 N . | 105.27828W. | NW1/4NW1/4 sec. 4, T. 43 N., R. 70 W. | 03/22/2000 | A |
| 14 | PRB | 43.72872 N . | 105.32945 W . | NW1/4SE1/4 sec. 1, T. 43 N., R. 71 W. | 04/27/2000 | A |
| 15 | PRB | 43.57330 N . | 105.26031W. | NE1/4NW1/4 sec. 34, T. 42 N., R. 70 W. | 06/02/2000 | A |
| 16 | PRB | 43.57583 N . | 105.28145 W . | NE1/4NW1/4 sec. 33, T. 42 N., R. 70 W. | 06/02/2000 | A |
| 17 | PRB | 43.57895 N . | 105.32843 W . | NE1/4NW1/4 sec. 31, T. 42 N., R. 70 W. | 06/03/2000 | D |
| 18 | PRB | 43.57624 N . | 105.35947W. | SW1/4NE1/4 sec. 35, T. 42 N., R. 71 W. | 07/12/2000 | D |
| 19 | PRB | 43.66122 N . | 105.75760W. | NE1/4NW1/4 sec. 33, T. 43 N., R. 74 W. | 07/14/2000 | B |
| 20 | PRB | 44.14510 N . | 105.40291W. | NW1/4NW1/4 sec. 9, T. 48 N., R. 71 W. | 07/31/2000 | B |
| 21 | WB | 47.33781 N . | 101.82531W. | C SE1/4NE1/4 sec. 36, T. 145 N., R. 88 W. | 08/22/2000 | B |
| 22 | WB | 47.38478 N . | 101.88874W. | C NE1/4NE1/4 sec. 16, T. 145 N., R. 88 W. | 08/24/2000 | B |
| 23 | PRB | 43.05322 N . | 105.79355 W . | NE1/4NE1/4 sec. 36, T. 36 N., R. 75 W. | 09/07/2000 | A |
| 24 | GRB | 41.80364 N . | 108.70250 W . | SW1/4NW1/4 sec. 11, T. 21 N., R. 100 W. | 10/24/2000 | A |
| 25 | PRB | 44.04874 N . | 105.45364 W . | NW1/4SE1/4 sec. 13, T. 47 N., R. 72 W . | 06/10/2001 | E |
| 26 | PRB | 44.00798 N . | 106.09271 W . | NE1/4NE1/4 sec. 34, T. 47 N., R. 77 W. | 07/13/2001 | E |
| 27 | PRB | 44.05166 N . | 105.56000 W . | SE1/4NW1/4 sec. 18, T. 47 N., R. 72 W . | 07/21/2001 | E |
| 28 | PRB | 44.97265 N . | 106.42874W. | SW1/4NE1/4 sec. 30, T. 58 N., R. 79 W. | 12/05/2001 | E |
| 29 | PRB | 44.91805 N . | 106.43215 W . | NE1/4NW1/4 sec. 18, T. 57 N., R. 79 W. | 12/08/2001 | n.d. |
| 30 | PRB | 44.97623 N . | 106.42377W. | NE1/4NE1/4 sec. 30, T. 58 N., R. 79 W. | 12/08/2001 | E |
| 31 | PRB | 43.62830 N . | 106.11680W. | SW1/4NE1/4 sec. 9, T. 42 N., R. 77 W. | 01/18/2002 | E |
| 32 | PRB | 44.06227 N . | 106.18863W. | SW1/4NW1/4 sec. 12, T. 47 N., R. 77 W. | 01/08/2003 | E |
| 33 | PRB | 43.93458 N . | 105.68611 W . | SW1/4NW1/4 sec. 30, T. 46 N., R. 73 W. | 04/22/2003 | E |
| 34 | PRB | 43.52525 N . | 105.39694W. | NE1/4SW1/4 sec. 16, T. 41 N., R. 71 W. | 07/09/2003 | C |
| 35 | PRB | 43.86103 N . | 105.80693 W . | SW1/4NW1/4 sec. 19, T. 45 N., R. 74 W. | 10/22/2003 | C |
| 36 | PRB | 43.51627 N . | 105.33530W. | SE1/4SW1/4 sec. 24, T. 41 N., R. 71 W. | 10/25/2003 | C |
| 37 | PRB | 43.57958 N . | 105.34513W. | SE1/4SE1/4 sec. 26, T. 42 N., R. 71 W. | 10/28/2003 | C |

bed, core holes 4 and 6; Werner coal bed, core hole 11; Canyon coal bed, core holes $6,8,30$, and 34 ; Wyodak coal bed (including upper, middle, and lower Wyodak coal beds), core holes 5, 9, 10, 13-18, and 20; Anderson coal bed, core holes 3, 5, 8, 28, and 34 ; Big George coal bed, core holes $1,2,5,11,12,19,26$, 31-33, and 35; School coal bed, core hole 23; and Smith coal bed, core hole 8 (see figure 2).

## Williston Basin

The Williston Basin contains three main coal-bearing intervals: the Harmon-Hansen coal zone, the Hagel coal zone, and the Beulah-Zap coal zone, which are in the lower, middle, and upper parts of the Paleocene Fort Union Formation, respectively (Flores, Keighin, and others, 1999) (fig. 3). One sampled coal bed (unnamed coal bed 1, probably from the Harmon-Hansen coal zone) in the Leroy Gregory 1 well (core hole 7; table 1) is up to 14 feet ( ft ) thick. Four coal beds sampled at the Coteau Coal Mines (the Beulah coal bed and unnamed 2 coal bed from core hole 21 (Coteau MC00250C) and the unnamed 3 and unnamed 4 coal beds from core hole 22 (Coteau MC00251); table 1) came from the Beulah-Zap coal zone (fig. 3).

## Green River Basin

The Green River Basin contains two coal zones: the Deadman coal zone in the lower part of the Paleocene Fort Union Formation and the Cherokee coal zone in the upper part. These two zones contain more than eight coal beds (fig. 4) that are separated by a fluvial-channel-sandstone-dominated interval (Hettinger and Kirschbaum, 1991). Samples from core hole 24 (BCX-9) came from the Bridger Coal Company mine (table 1) from the Deadman coal zone (fig. 4) (Flores, Ochs, and Bader, 1999), which is up to 20 ft thick.

## Collection and Analyses of New Data

## Non-Lithotype Data

Analyses performed on coal samples extracted from the 37 core holes include methane desorption and adsorption, gas composition (Stricker and others, 2006), and coal chemistry (Stricker and others, 2007). At the drill site, cored coal samples were cut into sections (usually about 2 ft long) and immediately placed into desorption canisters. After the coal samples were desorbed, they were shipped to the USGS in Reston, Va. In the USGS laboratory in Reston, the sealed samples were unwrapped and split lengthwise.

After splitting, the coal was examined and, where deemed appropriate, subdivided into units on the basis of observed megascopic lithologic features, as shown in figure 5. The thicknesses of these units were measured to the nearest centimeter (occasionally to the nearest half centimeter) and recorded (see


Figure 3. Stratigraphic column for the Fort Union Formation in the Williston Basin, North Dakota.


## EXPLANATION

## Coal

Sandstone
Mudstone, siltstone, and sandstone
Unconformity
the unit thickness (UT) column in appendix 1 ; see table 2 for a list of all acronyms used in the lithologic descriptions and calculations of this report). The sum of the UT values for all units in each canister sample is the total thickness of coal in each canister, or the canister total measured thickness (CaToMT) (appendix 1). The unit proportion of the canister thickness (UPrCaT) for each unit is determined by dividing each UT by CaToMT (appendix 1). Finally, the core cumulative measured thickness (CoCuMT) is the cumulative sum of UT values from the top of the cored section of the well (note that it is not the surface elevation of the well) to the base of each unit (appendix 1). Canister 39 of core hole 2 (MichiWest Energy, Inc., Pilot State 16-32) is a common example of a canister sample that was divided into three units, with a UT of 5 centimeters (cm) for the top unit, 9 cm for the middle unit, and 39 cm for the bottom unit (appendix 1 , table 1-2). The CaToMT is therefore $53 \mathrm{~cm}(5+9+39)$, and UPrCaT values are 0.09 (5/53), 0.17 (9/53), and 0.74 (39/53) for the top, middle, and bottom units, respectively (values are reported to two decimal places). The CoCuMT values for the three units in canister 39 are $61.01,61.30$, and 62.58 ft for the top, middle, and bottom units, respectively (all UT values in the well were divided by 2.54 to convert from centimeters to inches, then divided by twelve to obtain feet, then summed from the top of the cored section of the well to the unit concerned). For the vertical axes of the charts in appendix 2 , the CoCuMT was used instead of the approximate depth values determined at the drill site because the sum of UT values for each canister was rarely equal to the canister thickness recorded in the field (usually 2 ft ).

Several other characteristics were determined in the laboratory (appendix 1): (1) the cleat spacing (CS), which is the distance between adjacent (vertical) cleat surfaces measured to the nearest millimeter; (2) the cleat frequency (CFr), which is the number of cleats per meter (cleats/m, equal to $1000 / \mathrm{CS}$ ); and (3) the canister average cleat frequency $(\mathrm{CaAvCFr}$, which is the average of all CFr values for all units within the entire canister (determined by multiplying the CFr by the UPrCaT for each unit within a canister, and summing the results).

For the three units in canister 39 of core hole 2, the CS values are 4 millimeters (mm) (top), 4 mm (middle), and 10 mm (bottom) (appendix 1, table 1-2). The CFr values for these three units are therefore 250 (1000/4), 250 (1000/4), and $100(1000 / 10)$ cleats $/ \mathrm{m}$, for the top, middle, and bottom units, respectively. The CaAvCFr for canister 39 is 139.62 cleats $/ \mathrm{m}$, which is the result of the following calculation: $(250 \times 0.09)$ $+(250 \times 0.17)+(100 \times 0.74)$. Units with no CFr values (for example, non-coal partings or gaps in the section with no data) were excluded from the CaAvCFr calculations.

The total gas (in standard cubic feet per ton (SCF/ton), which is standard industry usage) and apparent rank data were obtained from Stricker and others (2007) (appendix 1). For some canisters, we do not report total gas and (or) apparent rank data. No canisters have more than one value for either total gas or apparent rank. Finally, miscellaneous interesting or unusual features (such as the presence of pyrite, kaolinite, or calcite on cleat surfaces) were recorded in the laboratory and appear in appendix 1.

Figure 4. Stratigraphic column for the Fort Union Formation in the Green River Basin, Wyoming.

Figure 5. Photograph of canister coal sample split open for examination of megascopic lithologic features. Notice alternating vitrain (V, shiny) and attritus (A, dull) bands. Thicknesses of vitrain and attritus bands were measured in millimeters with the ruler.

Table 2. Acronyms used frequently throughout the report, listed in alphabetical order.

| Acronym | Attribute represented by acronym |  | Description of attribute |
| :--- | :--- | :--- | :--- |

## Lithotype Data

Coal lithology described in this report follows the classification scheme and definitions presented by American Society for Testing and Materials (1994), which is a modification of a classification scheme originally developed by Schopf (1960). This method involves the description of coal using three lithotypes: attritus (also called attrital coal), vitrain, and fusain. Attritus is derived from a variety of materials of vegetal origin and occurs as a fine-grained, tightly compacted mass (Theissen, 1920). Attritus makes up the groundmass in which vitrain and fusain are embedded. The luster of attritus can vary, but is generally duller than vitrain and not as dull as fusain. Stopes (1919) prefers to use the terms "clarain" for the brighter varieties of attritus and "durain" for the duller varieties. Vitrain is composed of shiny bands embedded in attrital groundmass and generally is considered to be the coalified remains of the woody portions of plants. Fusain is silky to dull, fibrous, and so soft and friable that it makes one's hands dirty when handled (Taylor and others, 1998). Fusain is generally considered to be the charcoal remains of burnt woody material (Taylor and others, 1998); however, Moore and others (1996) report that fungal activity during the peat accumulation stage has produced "inertinite"-like material (that is, fusain) in modern peat swamps.

Vitrain and fusain form bands of varying thickness, parallel or subparallel to bedding, separated by attrital groundmass (fig. 5). For most coal samples, vitrain bands alternate with attrital "bands" (which actually are areas of attrital groundmass separating vitrain bands), with occasional bands of fusain interspersed. Measurements (or visual estimates) of band thicknesses are made approximately perpendicular to the plane of bedding. These thickness measurements form the basis of the various methods used to describe the coal in this report. The methodologies used for describing the megascopic lithologic features of the coals evolved over the course of the project based on decisions made by several different researchers involved with the project. In general, we believe that point-counting methods (methods D and E, below) result in more accurate data than methods that depend on visual estimation alone (methods $\mathrm{A}, \mathrm{B}$, and C , below); however, there is no objective way for us to compare the accuracy of data created using these different methods because the coal samples are no longer available for reexamination in their original form (after the lithotype descriptions were completed, the samples were sent out for grinding and chemical analyses). The methods used to describe the lithology of the coal are presented in detail below. Table 3 also summarizes these different methods.

## Methods

Five methods were used to describe the coal samples in this project. Method A, developed by Ronald W. Stanton, employed a visual estimation of the average vitrain
band thickness (AvVBT), the average attrital band thickness (AvABT), and the cumulative fusain thickness (CuFT) in each unit. This method was useful and quick, but the possibility of inaccuracy of the visually estimated values was a major drawback. Also, in its original form, this method did not include a determination of the cumulative vitrain thickness $(\mathrm{CuVT})$ or cumulative attritus thickness (CuAT); therefore, the percentages of vitrain and attritus (VP and AP, respectively) also were not determined. Later, when it was decided that the VP and AP were needed, we assumed that the ratio of vitrain to attritus in each unit was equal to the ratio of the AvVBT to AvABT in order to calculate the $\mathrm{CuVT}, \mathrm{CuAT}, \mathrm{VP}$, and AP (see formulas in table 3). This assumption may not be accurate, but we had no other means to determine these values.

As a way of improving on method A , method B also included visual estimation of the VP and AP. These visually estimated percentages also may have had some inaccuracy, but were probably more reliable than the calculated percentages of method A.

Method C improved upon method B by visually estimating only the AvVBT, CuFT, VP, and AP. The CuVT and CuAT were still determined using VP and AP, but AvABT was determined by dividing CuAT by the number of vitrain bands ( $\mathrm{CuVT} / \mathrm{AvVBT}$ ) (the number of vitrain bands was assumed to be equal to the number of attrital bands, which was reasonable because the bands alternated from vitrain to attritus and back). Once again, the visual estimations were a possible source of inaccuracy, but with the AvABT calculated instead of estimated, this method may have been even more accurate than the previous two.

Method D, developed by Timothy A. Moore, attempted to remove even more inaccuracy by using a point-count method instead of visual estimation to determine VP and AP (see table 3 for formulas); however, the AvVBT, AvABT, and CuFT were still visually estimated, and may have been a source of inaccuracy as described above for methods A and B. This method was more time consuming due to the use of point counting, but the VP and AP values were probably more accurate than the visually estimated values of methods $B$ and $C$ and the calculated values of method A.

Finally, method E attempted to eliminate almost all visually estimated values (except CuFT) by using point-count values to determine the $\mathrm{CuVT}, \mathrm{CuAT}, \mathrm{VP}, \mathrm{AP}, \mathrm{AvVBT}$, and AvABT. Although method E was more time consuming than any of the previous methods, it was considered to be the most accurate method.

Because of the evolving nature of the methodology as described above, the values determined by different methods may be of different accuracies and, therefore, perhaps not always compatible with each other. Unfortunately, the samples (which were all sent to the laboratory for chemical analyses) are no longer available to check the accuracy of this assumption; however, we believe that the inaccuracies mentioned above are small enough that the results are still comparable from the beginning of the project to the end.

Table 3. Summary of methods used for determining the average vitrain band thickness (AvVBT), average attrital band thickness (AvABT), cumulative fusain thickness (CuFT), cumulative vitrain thickness (CuVT), and cumulative attritus thickness (CuAT) for coal units, grouped by methodology
[Abbreviations are as follows: AP, percent of attritus; UT, unit thickness (measured in the laboratory); VP, percent of vitrain]

| Core hole number | Average vitrain band thickness (AvVBT) | Average attrital band thickness (AvABT) | Cumulative fusain thickness (CuFT) | Vitrain percentage (VP) | Attrital percentage (AP) | Fusain percentage (AP) | Cumulative vitrain thickness (CuVT) | Cumulative <br> attritus thickness (CuAT) | Method used |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 1-3,8 \\ 10-16, \\ 23-24 \end{gathered}$ | Visually estimated | Visually estimated | Visually estimated | $\begin{aligned} & \hline(\mathrm{AvVBT} / \\ & {[\operatorname{AvVBT}+} \\ & \operatorname{AvABT}]) \\ & \times 100 \end{aligned}$ | $\begin{aligned} & (\mathrm{AvABT} / \\ & {[\mathrm{AvVBT}+} \\ & \text { AvABT] }) \times \\ & 100 \end{aligned}$ | $\begin{gathered} (\mathrm{CuFT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | $\begin{aligned} & (\mathrm{VP} / 100) \times \\ & (\mathrm{UT}-\mathrm{CuFT}) \end{aligned}$ | $\begin{aligned} & (\mathrm{AP} / 100) \times \\ & (\mathrm{UT}-\mathrm{CuFT}) \end{aligned}$ | A (the original method by Ronald W. Stanton, unpub. data, 1999). |
| 19-22 | Visually estimated | Visually estimated | Visually estimated | $\begin{gathered} (\mathrm{CuVT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | $\begin{aligned} & (\mathrm{CuAT} / \mathrm{UT}) \times \\ & \quad 100 \end{aligned}$ | $\begin{gathered} (\mathrm{CuFT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | (visually estimated VP / 100) $\times$ (UT - CuFT) | (visually estimated $\mathrm{AP} / 100) \times$ <br> (UT - CuFT) | B (method A with visually estimated VP and AP). |
| 9, 34-37 | Visually estimated | CuAT / (CuVT / AvVBT) | Visually estimated | $\begin{aligned} & (\mathrm{CuVT} / \mathrm{UT}) \\ & \times 100 \end{aligned}$ | $\begin{aligned} & (\mathrm{CuAT} / \mathrm{UT}) \times \\ & 100 \end{aligned}$ | $\begin{gathered} (\mathrm{CuFT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | (visually estimated VP / 100) $\times$ (UT - CuFT) | (visually estimated $\mathrm{AP} / 100) \times$ (UT - CuFT) | C (method A with visually estimated VP and AP and corrected AvABT). |
| 17-18 | Visually estimated | Visually estimated | Visually estimated | $\begin{gathered} (\mathrm{CuVT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | $\begin{aligned} & (\mathrm{CuAT} / \mathrm{UT}) \times \\ & \quad 100 \end{aligned}$ | $\begin{gathered} (\mathrm{CuFT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | (vitrain bands counted/ [vitrain bands counted +attritus bands counted]) $\times$ (UT - CuFT) | (attritus bands counted / [vitrain bands counted + attritus bands counted]) $\times$ (UT - CuFT) | D (method A with point-count method modified from Moore and others (1993)). |
| $\begin{aligned} & 25-28, \\ & 30-33 \end{aligned}$ | $\mathrm{CuVT} /$ vitrain bands counted | $\mathrm{CuAT} /$ attritus bands counted (= vitrain bands counted) | Visually estimated | $\begin{gathered} (\mathrm{CuVT} / \mathrm{UT}) \\ \mathrm{x} 100 \end{gathered}$ | $\begin{aligned} & (\mathrm{CuAT} / \mathrm{UT}) \mathrm{x} \\ & 100 \end{aligned}$ | $\begin{gathered} (\mathrm{CuFT} / \mathrm{UT}) \\ \times 100 \end{gathered}$ | Sum of vitrain band thicknesses (measured in the lab) | $\begin{gathered} \mathrm{UT}-(\mathrm{CuFT}+ \\ \mathrm{CuVT}) \end{gathered}$ | E (method A with point-count method modified from Moore and others (1993) and corrected AvVBT and AvABT). |

## Method A

A coal lithotype descriptive system, first developed by Ronald W. Stanton (unpub. data, 1999), was followed for coal samples from core holes $1-3,8,10$ through 16,23 , and 24. (Lithologic descriptions of coal samples from core holes 4 through 7 were never performed. Coal samples from core holes 17 through 22 were described in the laboratory at a later time (using methods B and D, described below) even though these core holes were drilled in the field before core holes 23 and 24. Samples from core hole 9 were placed in storage for more than three years before we decided to describe their lithology in the lab (using method C, described below).) For each unit in a canister the AvVBT, AvABT, and CuFT were visually estimated and recorded for each unit (table 3; appendix 1). The AvVBT and AvABT values were divided into five categories each. These categories were used to construct a coal lithotype matrix (fig. 6, developed by Ronald W. Stanton, unpub. data, 1999) that produced a lithotype code that was then assigned to each unit. Non-coal material (such as that found in partings) is labeled as "clay" (lithotype code 0 ) regardless of grain size and (or) mineralogy. Coal units are classified as follows, on the basis AvVBT and AvABT values and the presence or absence of fusain (fig. 6): attritus (nearly all attritus with little or no vitrain; lithotype code 1), finely laminated attritus and vitrain (code 2), medium to coarsely laminated attritus and vitrain (code 3), very coarsely laminated attritus and vitrain (code 4), woody material (nearly all vitrain with little or no attritus; code 5 ), and fusain ( 100 percent fusain; code 8). Note that from the late 1980s, Stanton used coal "facies" descriptions without actually assigning numerical lithotype codes or using a lithotype matrix (Stanton and others, 1989; Roberts and Stanton, 1994, Roberts and others, 1994; and Stanton and others, 2005).

As an example, the top and bottom units of canister 39, core hole 2, had an AvVBT value of 5 mm and an AvABT value of 10 mm , which indicated a lithotype code of 3 (medium to coarsely laminated attritus and vitrain) at the intersection of the third row (with AvVBT values between 5 and 20 mm ) and the third column (with AvABT values between 5 and 20 mm ) on the lithotype matrix (fig. 6). The middle unit had both AvVBT and AvABT values equal to zero mm and a CuFT equal to 90 mm ; therefore, the lithotype matrix indicated a code of 8 (fusain) at the intersection of the first row (AvVBT equal to zero) and the first column (AvABT equal to zero) (fig. 6).

In this method, the CuFT was visually estimated in the laboratory, but similar cumulative thicknesses of vitrain and attritus (CuVT and CuAT, respectively) were not. Later, when we decided to graph canister average percentages of vitrain (CaAvVP) and attritus (CaAvAP) against total gas (appendix 3 ), it became apparent that we needed CuVT and CuAT values to calculate the percentages of vitrain and attritus (VP and AP, respectively) in each unit. For this reason, we needed to derive values for the CuVT and CuAT using the AvVBT and AvABT values collected in the laboratory. Because all coal units are a
combination of vitrain, attritus, and fusain, the UT value minus the CuFT value had to equal the thickness of the non-fusain portion of the unit, or the sum of the CuVT and CuAT (that is, UT $-\mathrm{CuFT}=\mathrm{CuVT}+\mathrm{CuAT})(\mathrm{UT}$, recorded in centimeters, had to be converted to millimeters before subtracting the CuFT). Then, assuming an equal number of vitrain and attritus bands in each unit (which was reasonable because vitrain bands alternated with attritus bands), the ratios (AvVBT / (AvVBT +AvABT$)$ ) and (AvABT / (AvVBT + AvABT)) gave us the proportions of vitrain and attritus, respectively, in the non-fusain portion of the unit. Therefore, if we multiplied (UT - CuFT) by (AvVBT / (AvVBT $+\operatorname{AvABT})$ ), the result was the CuVT. Likewise, the product of (UT - CuFT) and (AvABT / (AvVBT + AvABT)) was the CuAT. For example, in the top unit of canister 39, core hole 2, UT $\mathrm{CuFT}=50 \mathrm{~mm}-0 \mathrm{~mm}$, or 50 mm . The CuVT was therefore 50 $\mathrm{mm} \times(5 \mathrm{~mm} /(5 \mathrm{~mm}+10 \mathrm{~mm}))$ or 16.67 mm , and the CuAT was $50 \times(10 /(5+10))$, or 33.33 mm (appendix 1, table 1-2).

At this point, the percentages of vitrain (VP), attritus (AP), and fusain (FP) in each unit were calculated by using the following formulas: $\mathrm{VP}=100 \times \mathrm{CuVT} / \mathrm{UT} ; \mathrm{AP}=100 \times$ $\mathrm{CuAT} / \mathrm{UT}$; and $\mathrm{FP}=100 \times \mathrm{CuFT} / \mathrm{UT}$. For example, for the top unit of canister 39 , core hole $2, \mathrm{VP}=100 \times 16.67 \mathrm{~mm} / 50$ $\mathrm{mm}=33.33$ percent, $\mathrm{AP}=100 \times 33.33 \mathrm{~mm} / 50 \mathrm{~mm}=66.67$ percent, and FP $=100 \times 0 \mathrm{~mm} / 50 \mathrm{~mm}=0$ percent (appendix 1, table 1-2).

The coal in most of the canisters was subdivided into several units. The total gas values and coal chemistry values (from Stricker and others (2006) and Stricker and others (2007), respectively), however, represented an average value for all of the coal in a canister. Therefore, whenever the canister was subdivided, it was necessary to determine the canister average percentages of vitrain (CaAvVP), attritus (CaAvAP), fusain ( CaAvFP ), and cleat frequency ( CaAvCFr ) in order to match the total gas and coal chemistry values. The canister average percentages for each of the three lithotypes were calculated in a manner similar to the canister average cleat frequency (CaAvCFr) described above. The CaAvVP was calculated by dividing the sum of the CuVT values for all units within the canister by the CaToMT, and multiplying by 100 . For example, in canister 39 of core hole 2 , the sum of the CuVT values for the three units was $16.67 \mathrm{~mm}+0.00 \mathrm{~mm}+126.67 \mathrm{~mm}=143.34$ mm . Next, 143.43 was divided by the CaToMT (first converted from 53 cm to 530 mm ), and multiplied by 100 to yield the CaAvVP value of 27.04 percent (appendix 1, table 1-2). Calculating the canister average attrital percentage (CaAvAP) and canister average fusain percentage ( CaAvFP ) was done in the same manner, but by using the sums of the CuAT and CuFT values, respectively, instead of the CuVT. Non-coal (sand, clay, ash, and so on) layers were included because they were included in the canister when the gas was desorbed and in the chemical analysis. Intervals that were not described or were missing (because of isotherm analysis sample removal, loss during drilling, or other reasons) were not included in these calculations.

| Coal <br> lithotype <br> matrix | Average attrital band thickness (AvABT) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 mm | Less than <br> 5 mm | $5-20 \mathrm{~mm}$ | Greater than <br> $20-40 \mathrm{~mm}$ | Greater than <br> 40 mm |  |
| Average <br> vitrain <br> band <br> thickness <br> (AvVBT) | 0 mm | 8 | 1 | 1 | 1 | 1 |
|  | Less than <br> 5 mm | 2 | 2 | 2 | 1 | 1 |
|  | Greater than <br> $20-40 \mathrm{~mm}$ | 5 | 4 | 4 | 4 | 3 |

Figure 6. Chart showing coal lithotype matrix developed by Ronald W. Stanton (unpub. data, 1999). The average attrital band thickness (AvABT, columns) and average vitrain band thickness (AvVBT, rows) determine the lithotype code at the cell of intersection. Lithotype codes are as follows: 0 , "clay" (non-coal lithotype, not found on matrix); 1, attritus (nearly all attritus with little or no vitrain); 2, finely laminated attritus and vitrain; 3 , medium to coarsely laminated attritus and vitrain; 4, very coarsely laminated attritus and vitrain; 5 , woody material (nearly all vitrain with little or no attritus); 8 , fusain (100 percent fusain). mm, millimeter.

## Method B

As mentioned above, the original procedure followed in method A only recorded visual estimates of the AvVBT, AvABT, and CuFT values in the laboratory. Two years into the project we decided to add visual estimation of vitrain percent (VP) and attrital percent (AP) during laboratory examination of the coal samples (table 3). Beginning with core hole 19 and continuing through core hole 22 , we visually estimated and recorded the VP and AP for each unit (with the exception of canisters C5 and C6 of core hole 19, method A was used for these two canisters). However, these percentages ignored the amount contributed by fusain (when present), so we corrected them (when fusain was present) in the following manner: (1) the thickness of non-fusain material (equal to $\mathrm{CuVT}+\mathrm{CuAT}$ ) was determined by subtracting the CuFT from the UT (that is, $\mathrm{CuVT}+\mathrm{CuAT}=\mathrm{UT}-\mathrm{CuFT}$ ); (2) the result was multiplied by the uncorrected VP (divided by 100) to obtain the CuVT , and by the uncorrected AP to get the CuAT; (3) the corrected VP was determined by dividing the CuVT by the UT and multiplying by 100 ; the corrected AP was determined by dividing the CuAT by the UT and multiplying by 100 . For example, canister C2 of core hole 19 (All Night Creek (ANCU) Iberlin 21-33-4374, table 1) had a VP of 30 percent and an AP of 70 percent recorded in the laboratory; however, these percentages ignored the presence of fusain in the unit (the CuFT was 8 mm , appendix 1 , table $1-15$ ). Correcting for the 8 mm of fusain yielded a VP of 29.58 percent, which was determined by the following calculation: $([(570 \mathrm{~mm}-8 \mathrm{~mm}) \times(30 / 100)]$
$/ 570 \mathrm{~mm}) \times 100$ (appendix 1, table 1-15). Appendix 1 lists only the corrected VP and AP values.

## Method C

For samples from core holes 9 and 34 through 37, we originally followed the same procedure as method B. Unfortunately, our visually estimated AvABT values for these samples were later determined to be erroneous, so we recalculated the AvABT in the following manner: (1) the average number of vitrain bands was determined by dividing the CuVT by the AvVBT; (2) assuming an equal number of attrital and vitrain bands, the CuAT was divided by the average number of vitrain bands to find the AvABT. For example, for the top unit of canister A-5 in core hole 9 (Kennecott CBM-1), the AvABT was calculated in the following manner: $(90 \mathrm{~mm} /[10 \mathrm{~mm}$ $/ 1 \mathrm{~mm}])=9 \mathrm{~mm}($ appendix 1, table $1-5)$. The recalculated AvABT values are reported in appendix 1 for samples from core holes 9 and 34 through 37.

## Method D

For samples from core holes 17 and 18, a point-counting method to calculate percentages of attritus and vitrain was developed by Timothy A. Moore. This method was a simplified version of the procedure described in Moore and others (1993) and was performed in addition to method A (described above). As in method A, the AvVBT, AvABT, and CuFT were visually estimated and recorded in the laboratory. In addition,
the coal lithotype (vitrain or attritus) was determined at 2-cm intervals and recorded (fig. 7). The VP (or AP) was then calculated by dividing the number of vitrain (or attrital) bands counted by the total number of bands (vitrain and attritus) counted and multiplying by 100 (point-count data was not included in appendix 1). As in method B above, the VP and AP were corrected for the presence of fusain by (1) subtracting the CuFT from the UT, (2) multiplying by the uncorrected VP (or AP) (divided by 100) to obtain the CuVT (or CuAT), and (3) dividing the CuVT (or CuAT) by UT and multiplying by 100 to obtain the corrected VP (or AP). For example, in canister A12 of core hole 17 (PNG 31-1), there were 10 vitrain bands counted out of a total of 20 vitrain and attritus bands, which yielded an uncorrected VP of 50 percent in the non-fusain portion of the canister (not shown in appendix 1); however, with a CuFT of 2 mm and a UT of 590 mm , the VP is corrected as follows: $([(590 \mathrm{~mm}-2 \mathrm{~mm}) \times(50 / 100)] / 590 \mathrm{~mm}) \times 100=$ 49.83 percent (appendix 1, table 1-13). Note that the same raw data (UT, AvVBT, AvABT, CuFT, vitrain and attrital band count values, and CFr) that were previously summarized by Moore and others (2001) correspond to the raw data used for samples from core holes 17 and 18 in this report.

## Method E

For samples from core holes 25 through 28 and 30 through 33 (samples from core hole 29 were not described), we used a procedure similar to method D (see above), but which employed the point-counting procedure described by Moore and others (1993). As in method D, the coal lithotype (attritus or vitrain) was determined at $2-\mathrm{cm}$ intervals and recorded. In addition to the number of attrital and vitrain bands, the thicknesses of individual vitrain bands encountered at the $2-\mathrm{cm}$ intervals also were recorded (these data are not included in appendix 1). In cases where vitrain bands spanned more than one $2-\mathrm{cm}$ interval, the vitrain band was counted only once. The AvVBT was calculated by dividing the sum of the recorded vitrain band thicknesses (that is, the CuVT ) by the number of vitrain bands. The CuAT was determined by subtracting the sum of the CuVT and the CuFT from the UT ( or CuAT $=\mathrm{UT}-(\mathrm{CuVT}+\mathrm{CuFT})$ ). Assuming an equal number of attrital and vitrain bands (a significant difference from method D), the AvABT was determined by dividing the CuAT by the number of vitrain bands. The VP (or AP) was then determined by dividing the CuVT (or CuAT) by the UT. For example, in canister D31 of core hole 25 (PNG Duvall 13J-D) we counted 7 vitrain bands with thicknesses of $18 \mathrm{~mm}, 1 \mathrm{~mm}, 2 \mathrm{~mm}, 2 \mathrm{~mm}, 30 \mathrm{~mm}, 1 \mathrm{~mm}$, and 60 mm (not shown in appendix 1). The sum of these vitrain band thicknesses, or the CuVT, was 114 mm (appendix 1, table 1-21). The AvVBT was determined by dividing 114 mm by 7 to yield 16.29 mm (appendix 1, page table 1-21). The CuAT was determined by subtracting the sum of the CuFT and the CuVT from the UT $(600 \mathrm{~mm}-[114 \mathrm{~mm}+7 \mathrm{~mm}]=479 \mathrm{~mm})$ (appendix 1, page table 1-21). Finally, the AvABT was determined by dividing the CuAT by the number of attrital bands (assumed to be equal
to the number of vitrain bands) as follows: $479 \mathrm{~mm} / 7=68.43$ mm (appendix 1, table 1-21). Note that point counting was not done on 12 units in core hole 26 (all units in canisters D12, D15, D17, and D18), one unit in core hole 32 (canister C17), three units in core hole 32 (canisters 36 (the middle and bottom units) and canister 47 (the fifth unit from the top)), and one unit in core hole 33 (canister D2). For these 17 units, method A had to be used to determine the AvVBT, AvABT, CuVT, and CuAT.

## Discussion of Data and Results

The thicknesses of coal samples measured in the laboratory commonly were found to differ from the thicknesses indicated by the approximate top and bottom depths recorded in the field (usually 2 -ft-thick segments). There are several possible explanations for the discrepancies. First, the total length of the original coal sample placed in the canister may have been slightly shorter or longer than the thickness indicated by the top and bottom field depths. Second, movement of the coal samples during desorption and shipment often resulted in the breakage of the coal into smaller, more loosely packed fragments. It was often very difficult in the laboratory to reassemble these fragments into a reasonable facsimile of the original coal sample; thus, the thickness measurements may have been erroneous for some samples. Finally, it is possible that the coal may have expanded slightly after absorbing water in the desorption canister. As a result, the base depths calculated from unit thickness measurements in the laboratory often differed from the canister base depths recorded in the field. To avoid confusion, the total measured thickness from the top of the highest canister sample in the core hole (the core cumulative measured thickness (CoCuMT) in appendix 1) was used rather than drilling depth (from the surface) to the unit base for the vertical axes of the graphs in appendix 2 . The thicknesses of the unsampled portions of the core hole were included to graphically represent the locations of gaps in the stratigraphic column.

Graphs showing the total measured thickness plotted against total gas and five other variables (average attrital band thickness, cleat frequency, cumulative fusain thickness, lithotype code, and average vitrain band thickness) are presented in appendix 2 . In a few cases, a relationship between total gas and one or more of these variables may be evident. For example, in core holes 1,8 (in the Cook coal bed section), 20, and 34 (in the Anderson coal bed section) (appendix 2, figs. $2-1,2-7,2-20$, and $2-36$, respectively), the total gas values on the cleat frequency graphs seem to partially mimic the variations in cleat frequency. Similarly, the total gas values may exhibit a trend slightly parallel to the average vitrain band thickness in core holes 8 (in the Cook coal bed section), 10, and 23 (appendix 2, figs. $2-7,2-9$, and $2-25$, respectively). In most cases, however, it was difficult or impossible to recognize any positive relationship between the total gas and these variables. In some cases, the amount of measured gas was very


Figure 7. Photograph of canister coal sample with a string that is marked at $2-\mathrm{cm}$ intervals and was used for the point-counting procedure. At this location, 11 bands of vitrain with a total thickness of 218 mm were recorded, resulting in an average vitrain band thickness of $19.8 \mathrm{~mm}(218 / 11)$. Assuming an equal number of attrital and vitrain bands, an average attrital thickness of 33.8 mm was calculated ( $[590-218] / 11$, where 590 mm is the total canister thickness). Using these values for average vitrain and attrital band thicknesses a lithotype code of 3 (medium to coarsely laminated attritus and vitrain) was determined from the lithotype matrix (fig. 6).
small (less than 10 standard cubic feet per ton), so the likelihood of obtaining measurable variations of gas content would be low (for example, core holes $9,10,13,15,16,21$ through 27 , and 34 through 37 ; appendix 2, figs. $2-8,2-9,2-13,2-15$, $2-16,2-21$ through $2-29$, and $2-36$ through $2-40$, respectively). Also, some core holes had such a small number of gas samples (fewer than 6 per bed) that the likelihood of noticing variation within the canister was very small (for example, core holes $3,8,21,22,25$, and 36 ; appendix 2 , figs. $2-3$ through $2-7,2-21$ through $2-24,2-27$, and $2-39$, respectively).

In general, we found no obvious positive correlation between the total gas and the average vitrain band thickness, canister average attrital band thickness, and canister average cleat frequency (appendix 3). The samples in core hole 32 appear to form a cluster of points that may show a slightly positive correlation between the canister average vitrain band thickness and the total gas (appendix 3, fig. 3-1D), but the trend line passing through these points (not shown) has a very low R-squared value of 0.18 . Similarly, a slight negative correlation may be present between canister average attrital percentage and total depth based on an R-squared value of -0.18 for samples from core hole 32 (appendix 3, fig. 3-3D).

## Interpretations

Previous studies using data from some of the same samples (core holes 2, 17, and 18) from this study have noted a possible relationship between the percent of vitrain in the sample and the amount of gas desorbed (Moore and others, 2001; Chiehowsky and others, 2003. As noted above, there were a few instances where a positive relationship between the percentage of vitrain and total gas may exist (core holes 8 (Cook coal bed), 10, and 23 in appendix 2 (figs. $2-7,2-9$, and $2-25$; core hole 32 in appendix 3 , figs. $3-1 D$ and $3-3 D$ ), but in general, a good relation between vitrain thickness and total gas values was not observable in this study. The reason for the weak relationship is unknown, but may be due to one or more of the following: (1) gas may have migrated out of the source areas along cleat or porous fusain channels; (2) low levels of gas may be a result of high ash content in coals; (3) canisterlevel total gas values may not reflect variations in gas content that correlate with lithotype variations at the millimeter scale; or (4) variation in hydrostatic pressure may be a greater influence on gas content than the lithology of the coal.

As already mentioned above, we observed no apparent relationship between average (vertical) cleat frequency and total gas or heating value. Note that cleat spacing was often very difficult to determine with certainty for a number of reasons, including the following: (1) highly fractured coal samples often were difficult to reassemble and, consequently, cleat measurements may have been difficult to determine; (2) cleat spacing varied from unit to unit in the coal sample, and sometimes even varied within the unit; (3) some units had very wide spacing of cleats that was greater than the diameter of
the core hole; and (4) some units (usually those with high ash content) had a massive "uncleated" appearance. Also, the total gas values of the canisters may not have correlated well with average cleat frequencies calculated for each canister.

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## Appendix 1. Tables of Lithologic Data for Samples From 32 Cores

The following tables are arranged according to core hole number (see figure 1 and table 1 in report). They show canister number, approximate depth (top and bottom), coal bed name, unit thickness (UT), canister total measured thickness (CaToMT), unit proportion of canister thickness (UPrCaT), core cumulative measured thickness (CoCuMT), average vitrain band thickness (AvVBT), average attrital band thickness (AvABT), cumulative fusain thickness (CuFT), lithotype code (see table 3), cumulative vitrain thickness (CuVT), cumulative attritus thickness (CuAT), percentages of vitrain (VP), attritus (AP), and fusain (FP), canister average percentages of vitrain (CaAvVP), attritus (CaAvAP), and fusain (CaAvFP), cleat
spacing (CS), cleat frequency (CFr), canister average cleat frequency ( CaAvCFr ), total gas per canister, apparent rank, and comments. In cases where no sample was available, the coal was too fragmented to describe, and (or) no descriptions were made, the following abbreviations are either appended to the canister number or used alone in the first column for further description: ns, no sample available; fr, highly fractured sample; nr, data not recorded. In these cases, the unit concerned was not included in determination of vitrain, attritus, fusain, and cleat frequency canister averages. The total gas and apparent rank data are from Stricker and others (2007).

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approxim (ft) | te depth | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| 1 | 1,213.00 | --- | Big George | 4.00 | --- | 0.04 | 0.13 | 0.0 | 0.0 |
| 1 | --- | 1,215.00 | Big George | 56.60 | 60.60 | 0.51 | 1.99 | 6.0 | 6.0 |
| 2 | 1,215.00 | --- | Big George | 38.10 | --- | 0.58 | 3.24 | 2.0 | 20.0 |
| 2 | --- | 1,217.00 | Big George | 27.90 | 66.00 | 0.42 | 4.15 | 30.0 | 0.0 |
| 3 | 1,217.00 | 1,219.00 | Big George | 60.10 | 60.10 | 1.00 | 6.13 | 30.0 | 0.0 |
| 4 | 1,219.00 | --- | Big George | 40.00 | --- | 0.67 | 7.44 | 2.0 | 20.0 |
| 4 | --- | 1,221.00 | Big George | 20.00 | 60.00 | 0.33 | 8.09 | 30.0 | 0.0 |
| 5 | 1,221.00 | --- | Big George | 40.90 | --- | 0.68 | 9.44 | 2.0 | 20.0 |
| 5 | --- | 1,223.00 | Big George | 19.60 | 60.50 | 0.32 | 10.08 | 20.0 | 0.0 |
| 6 | 1,223.00 | --- | Big George | 52.00 | --- | 0.85 | 11.78 | 30.0 | 0.0 |
| 6 | --- | 1,225.00 | Big George | 9.00 | 61.00 | 0.15 | 12.08 | 20.0 | 0.0 |
| 7 | 1,225.00 | --- | Big George | 15.00 | --- | 0.25 | 12.57 | 30.0 | 0.0 |
| 7 | --- | --- | Big George | 7.00 | --- | 0.11 | 12.80 | 3.0 | 10.0 |
| 7 | --- | 1,227.00 | Big George | 39.00 | 61.00 | 0.64 | 14.08 | 20.0 | 1.0 |
| 8 | 1,227.00 | 1,229.00 | Big George | 50.80 | 111.40 | 0.46 | 15.75 | 0.0 | 0.0 |
| 9 | 1,229.00 | --- | Big George | 2.54 | --- | 0.04 | 15.83 | 0.0 | 0.0 |
| 9 | --- | 1,231.00 | Big George | 58.50 | 61.04 | 0.96 | 17.75 | 20.0 | 2.0 |
| 10 | 1,231.00 | --- | Big George | 30.50 | --- | 0.50 | 18.75 | 20.0 | 2.0 |
| 10 | --- | --- | Big George | 7.00 | --- | 0.11 | 18.98 | 2.0 | 4.0 |
| 10 | --- | 1,233.00 | Big George | 23.50 | 61.00 | 0.39 | 19.75 | 4.0 | 4.0 |
| 11 | 1,233.00 | --- | Big George | 35.00 | --- | 0.57 | 20.90 | 10.0 | 20.0 |
| 11 | --- | --- | Big George | 21.00 | --- | 0.34 | 21.59 | 10.0 | 20.0 |
| 11 | --- | 1,235.00 | Big George | 5.00 | 61.00 | 0.08 | 21.75 | 4.0 | 4.0 |
| 12 | 1,235.00 | --- | Big George | 24.50 | --- | 0.42 | 22.56 | 3.0 | 5.0 |
| 12 | --- | 1,237.00 | Big George | 34.50 | 59.00 | 0.58 | 23.69 | 20.0 | 0.0 |
| 13 | 1,237.00 | --- | Big George | 30.00 | --- | 0.49 | 24.67 | 20.0 | 0.0 |
| 13 | --- | -- | Big George | 15.00 | --- | 0.25 | 25.17 | 40.0 | 0.0 |
| 13 | --- | 1,239.00 | Big George | 16.00 | 61.00 | 0.26 | 25.69 | 0.0 | 50.0 |
| 14 | 1,239.00 | --- | Big George | 40.00 | --- | 0.66 | 27.00 | 10.0 | 1.0 |
| 14 | --- | 1,241.00 | Big George | 21.00 | 61.00 | 0.34 | 27.69 | 5.0 | 5.0 |
| ns1 | 1,241.00 | 1,242.50 | ns1 | 46.00 | 46.00 | 1.00 | 29.20 | --- | --- |
| 15 | 1,242.50 | --- | Big George | 38.00 | --- | 0.62 | 30.45 | 20.0 | 10.0 |
| 15 | --- | 1,244.50 | Big George | 23.00 | 61.00 | 0.38 | 31.20 | 2.0 | 4.0 |
| 16 | 1,244.50 |  | Big George | 39.62 | --- | 0.91 | 32.50 | 5.0 | 2.0 |
| 16 | --- | 1,246.70 | Big George | 3.81 | 43.43 | 0.09 | 32.63 | 0.0 | 0.0 |
| 17 | 1,246.70 | --- | Big George | 15.24 | --- | 0.20 | 33.13 | 10.0 | 40.0 |
| 17 | --- | --- | Big George | 15.00 | --- | 0.20 | 33.62 | 10.0 | 10.0 |
| 17 | --- | --- | Big George | 37.00 | --- | 0.49 | 34.83 | 4.0 | 4.0 |
| 17 | --- | 1,248.80 | Big George | 9.00 | 76.24 | 0.12 | 35.13 | 2.0 | 2.0 |
| 18 | 1,248.80 | --- | Big George | 7.60 | --- | 0.12 | 35.38 | 2.0 | 20.0 |
| 18 | --- | 1,250.80 | Big George | 54.00 | 61.60 | 0.88 | 37.15 | 2.0 | 20.0 |
| 19 | 1,250.80 | --- | Big George | 4.00 | --- | 0.07 | 37.28 | 20.0 | 0.0 |
| 19 | --- | --- | Big George | 1.00 | --- | 0.02 | 37.31 | 0.0 | 0.0 |
| 19 | --- | 1,252.80 | Big George | 56.00 | 61.00 | 0.92 | 39.15 | 20.0 | 0.0 |
| 20 | 1,252.80 | 1,254.90 | Big George | 61.00 | 61.00 | 1.00 | 41.15 | 5.0 | 20.0 |
| 21 | 1,254.90 | --- | Big George | 35.00 | --- | 0.57 | 42.30 | 20.0 | 1.0 |
| 21 | --- | 1,257.00 | Big George | 26.00 | 61.00 | 0.43 | 43.15 | 30.0 | 0.0 |
| 22 | 1,257.00 | 1,259.00 | Big George | 61.00 | 61.00 | 1.00 | 45.15 | 8.0 | 2.0 |
| 23 | 1,259.00 | 1,261.00 | Big George | 61.00 | 61.00 | 1.00 | 47.16 | 30.0 | 0.0 |
| 24 | 1,261.00 | 1,263.00 | Big George | 61.00 | 61.00 | 1.00 | 49.16 | 10.0 | 40.0 |
| ns2 | 1,263.00 | 1,272.00 | ns2 | 274.00 | 274.00 | 1.00 | 58.15 | --- | --- |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- |
| 1 | 1.0 | 3 | 282.50 | 282.50 | 49.91 | 49.91 | 0.18 | --- |
| 2 | 1.0 | 2 | 34.55 | 345.45 | 9.07 | 90.67 | 0.26 | --- |
| 2 | 0.0 | 5 | 279.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 3 | 1.0 | 5 | 600.00 | 0.00 | 99.83 | 0.00 | 0.17 | --- |
| 4 | 0.0 | 2 | 36.36 | 363.64 | 9.09 | 90.91 | 0.00 | --- |
| 4 | 0.0 | 5 | 200.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 5 | 0.0 | 2 | 37.18 | 371.82 | 9.09 | 90.91 | 0.00 | --- |
| 5 | 0.0 | 3 | 196.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 6 | 0.0 | 5 | 520.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 6 | 1.0 | 3 | 89.00 | 0.00 | 98.89 | 0.00 | 1.11 | --- |
| 7 | 0.0 | 5 | 150.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 7 | 0.0 | 2 | 16.15 | 53.85 | 23.08 | 76.92 | 0.00 | --- |
| 7 | 0.0 | 3 | 371.43 | 18.57 | 95.24 | 4.76 | 0.00 | --- |
| 8 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- |
| 9 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- |
| 9 | 0.0 | 3 | 531.82 | 53.18 | 90.91 | 9.09 | 0.00 | 87.13 |
| 10 | 0.0 | 3 | 277.27 | 27.73 | 90.91 | 9.09 | 0.00 | -- |
| 10 | 0.0 | 2 | 23.33 | 46.67 | 33.33 | 66.67 | 0.00 | --- |
| 10 | 0.0 | 2 | 117.50 | 117.50 | 50.00 | 50.00 | 0.00 | 68.54 |
| 11 | 10.0 | 3 | 113.33 | 226.67 | 32.38 | 64.76 | 2.86 | --- |
| 11 | 0.0 | 3 | 70.00 | 140.00 | 33.33 | 66.67 | 0.00 | --- |
| 11 | 0.0 | 2 | 25.00 | 25.00 | 50.00 | 50.00 | 0.00 | --- |
| 12 | 1.0 | 2 | 91.50 | 152.50 | 37.35 | 62.24 | 0.41 | --- |
| 12 | 0.0 | 3 | 345.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 13 | 0.0 | 3 | 300.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 13 | 0.0 | 5 | 150.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 13 | 0.0 | 1 | 0.00 | 160.00 | 0.00 | 100.00 | 0.00 | 73.77 |
| 14 | 0.0 | 3 | 363.64 | 36.36 | 90.91 | 9.09 | 0.00 | --- |
| 14 | 0.0 | 3 | 105.00 | 105.00 | 50.00 | 50.00 | 0.00 | --- |
| ns1 | --- | -- | --- | --- | --- | --- | --- | --- |
| 15 | 0.0 | 3 | 253.33 | 126.67 | 66.67 | 33.33 | 0.00 | --- |
| 15 | 1.0 | 2 | 76.33 | 152.67 | 33.19 | 66.38 | 0.43 | --- |
| 16 | 0.0 | 3 | 283.03 | 113.21 | 71.43 | 28.57 | 0.00 | --- |
| 16 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- |
| 17 | 0.0 | 3 | 30.48 | 121.92 | 20.00 | 80.00 | 0.00 | --- |
| 17 | 0.0 | 3 | 75.00 | 75.00 | 50.00 | 50.00 | 0.00 | --- |
| 17 | 0.0 | 2 | 185.00 | 185.00 | 50.00 | 50.00 | 0.00 | --- |
| 17 | 0.0 | 2 | 45.00 | 45.00 | 50.00 | 50.00 | 0.00 | --- |
| 18 | 0.0 | 2 | 6.91 | 69.09 | 9.09 | 90.91 | 0.00 | --- |
| 18 | 0.0 | 2 | 49.09 | 490.91 | 9.09 | 90.91 | 0.00 | --- |
| 19 | 0.0 | 3 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 19 | 10.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- |
| 19 | 0.0 | 3 | 560.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 20 | 1.0 | 3 | 121.80 | 487.20 | 19.97 | 79.87 | 0.16 | --- |
| 21 | 0.0 | 3 | 333.33 | 16.67 | 95.24 | 4.76 | 0.00 | --- |
| 21 | 0.0 | 5 | 260.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 22 | 0.0 | 3 | 488.00 | 122.00 | 80.00 | 20.00 | 0.00 | --- |
| 23 | 0.0 | 5 | 610.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 24 | 0.0 | 3 | 122.00 | 488.00 | 20.00 | 80.00 | 0.00 | 20.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | --- | --- | 40 | 25.00 | --- | --- | --- | Parting. |
| 1 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 2 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 2 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 3 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 4 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 4 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 5 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 5 | --- | --- | 4 | 250.00 | --- | --- | SubA | --- |
| 6 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 6 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 7 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 7 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 7 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 8 | --- | --- | 20 | 50.00 | --- | --- | --- | Parting. |
| 9 | --- | --- | 20 | 50.00 | --- | --- | --- | Parting. |
| 9 | 8.71 | 0.00 | 20 | 50.00 | 50.00 | 16.82 | --- | --- |
| 10 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 10 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 10 | 31.46 | 0.00 | 10 | 100.00 | 100.00 | 62.02 | SubA | --- |
| 11 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 11 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 11 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 12 | --- | --- | 4 | 250.00 | --- | --- | --- | --- |
| 12 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 13 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 13 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 13 | 26.23 | 0.00 | 100 | 10.00 | 26.21 | 23.86 | --- | --- |
| 14 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 14 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 15 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 15 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 16 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 16 | --- | --- | 10 | 100.00 | --- | --- | --- | Parting. |
| 17 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 17 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 17 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 17 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 18 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 18 | --- | --- | 10 | 100.00 | --- | --- | SubA | --- |
| 19 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 19 | --- | --- | 100 | 10.00 | --- | --- | --- | Fusain layer. |
| 19 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 20 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 21 | --- | --- | 8 | 125.00 | --- | --- | --- | --- |
| 21 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 22 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 23 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 24 | 80.00 | 0.00 | 10 | 100.00 | 100.00 | 22.92 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | -- | --- | No sample. |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approxim (ft) | ate depth | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| 25 | 1,272.00 | --- | Big George | 30.00 | --- | 0.50 | 59.13 | 20.0 | 0.0 |
| 25 | - | 1,274.00 | Big George | 30.00 | 60.00 | 0.50 | 60.12 | 4.0 | 20.0 |
| 26 | 1,274.00 | --- | Big George | 15.00 | --- | 0.25 | 60.61 | 1.0 | 20.0 |
| 26 | --- | --- | Big George | 20.00 | --- | 0.33 | 61.26 | 30.0 | 0.0 |
| 26 | --- | 1,276.00 | Big George | 26.00 | 61.00 | 0.43 | 62.12 | 10.0 | 10.0 |
| 27 | 1,276.00 | --- | Big George | 27.00 | --- | 0.53 | 63.00 | 3.0 | 30.0 |
| 27 | --- | --- | Big George | 13.00 | --- | 0.25 | 63.43 | 30.0 | 0.0 |
| 27 | --- | 1,278.00 | Big George | 11.00 | 51.00 | 0.22 | 63.79 | 2.0 | 20.0 |
| 28 | 1,278.00 | --- | Big George | 10.00 | --- | 0.16 | 64.12 | 1.0 | 10.0 |
| 28 | --- | 1,280.00 | Big George | 51.00 | 61.00 | 0.84 | 65.79 | 30.0 | 0.0 |
| 29 | 1,280.00 | 1,282.00 | Big George | 61.00 | 61.00 | 1.00 | 67.79 | 30.0 | 0.0 |
| 30 | 1,282.00 | 1,284.00 | Big George | 61.00 | 61.00 | 1.00 | 69.79 | 30.0 | 0.0 |
| 31 | 1,284.00 | --- | Big George | 17.78 | --- | 0.37 | 70.38 | 30.0 | 0.0 |
| 31 | --- | --- | Big George | 2.54 | --- | 0.05 | 70.46 | 0.0 | 0.0 |
| ns3 | --- | --- | ns3 | 12.70 | --- | 1.00 | 70.88 | --- | --- |
| 31 | --- | --- | Big George | 25.40 | --- | 0.53 | 71.71 | 30.0 | 4.0 |
| 31 | --- | 1,286.00 | Big George | 2.54 | 48.26 | 0.05 | 71.79 | 0.0 | 0.0 |
| ns4 | 1,286.00 | 1,287.00 | ns4 | 30.50 | 30.50 | 1.00 | 72.79 | --- | --- |
| 35 | 1,287.00 | 1,289.00 | Big George | 61.00 | 61.00 | 1.00 | 74.80 | 3.0 | 20.0 |
| 36 | 1,289.00 | --- | Big George | 2.00 | --- | 0.03 | 74.86 | 20.0 | 0.0 |
| 36 | --- | --- | Big George | 18.32 | --- | 0.30 | 75.46 | 5.0 | 1.0 |
| 36 | --- | 1,291.00 | Big George | 40.68 | 61.00 | 0.67 | 76.80 | 5.0 | 1.0 |
| 37 | 1,291.00 | 1,293.00 | Big George | 61.00 | 61.00 | 1.00 | 78.80 | 3.0 | 20.0 |
| 38 | 1,293.00 | 1,295.00 | Big George | 61.00 | 61.00 | 1.00 | 80.80 | 20.0 | 0.0 |
| ns5 | 1,295.00 | 1,303.00 | ns5 | 244.00 | 244.00 | 1.00 | 88.80 | --- | --- |
| 32 | 1,303.00 | --- | Big George | 55.00 | --- | 0.90 | 90.61 | 1.0 | 10.0 |
| 32 | --- | 1,305.00 | Big George | 6.00 | 61.00 | 0.10 | 90.81 | 30.0 | 0.0 |
| 33 | 1,305.00 | --- | Big George | 20.32 | --- | 0.50 | 91.47 | 10.0 | 30.0 |
| 33 | --- | --- | Big George | 20.32 | 40.64 | 0.50 | 92.14 | 10.0 | 20.0 |
| ns6 | --- | 1,307.00 | ns6 | 20.32 | --- | 1.00 | 92.81 | --- | --- |
| 34 | 1,307.00 | --- | Big George | 22.86 | --- | 0.47 | 93.56 | 20.0 | 4.0 |
| 34 | --- | --- | Big George | 12.70 | --- | 0.26 | 93.97 | 20.0 | 2.0 |
| 34 | --- | --- | Big George | 12.70 | 48.26 | 0.26 | 94.39 | 5.0 | 5.0 |
| ns7 | --- | 1,309.00 | ns7 | 12.74 | --- | 1.00 | 94.81 | --- | --- |
| 39 | 1,309.00 | --- | Big George | 0.50 | --- | 0.01 | 94.82 | 0.0 | 0.0 |
| 39 | --- | --- | Big George | 14.00 | --- | 0.23 | 95.28 | 20.0 | 10.0 |
| 39 | --- | --- | Big George | 11.00 | --- | 0.18 | 95.64 | 20.0 | 0.0 |
| 39 | --- | 1,311.00 | Big George | 35.00 | 60.50 | 0.58 | 96.79 | 1.0 | 20.0 |
| 40 | 1,311.00 | 1,313.00 | Big George | 61.00 | 61.00 | 1.00 | 98.79 | 50.0 | 30.0 |
| 41 | 1,313.00 | --- | Big George | 20.32 | --- | 0.33 | 99.46 | 40.0 | 0.0 |
| 41 | --- | --- | Big George | 16.51 | --- | 0.27 | 100.00 | 20.0 | 0.0 |
| 41 | --- | 1,315.00 | Big George | 25.40 | 62.23 | 0.41 | 100.84 | 10.0 | 2.0 |
| 42 | 1,315.00 | 1,317.00 | Big George | 61.00 | 61.00 | 1.00 | 102.84 | 5.0 | 5.0 |
| 43 | 1,317.00 | --- | Big George | 38.10 | --- | 0.65 | 104.09 | 15.0 | 0.0 |
| 43 | --- | 1,319.00 | Big George | 20.32 | 58.42 | 0.35 | 104.75 | 50.0 | 0.0 |
| 44 | 1,319.00 | 1,321.00 | Big George | 61.00 | 61.00 | 1.00 | 106.75 | 20.0 | 0.0 |
| 45 | 1,321.00 |  | Big George | 7.62 | --- | 0.13 | 107.00 | 10.0 | 2.0 |
| 45 | --- | --- | Big George | 20.32 | --- | 0.33 | 107.67 | 40.0 | 0.0 |
| 45 | --- | 1,323.00 | Big George | 33.02 | 60.96 | 0.54 | 108.75 | 5.0 | 0.0 |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 0.0 | 3 | 300.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 25 | 0.0 | 2 | 50.00 | 250.00 | 16.67 | 83.33 | 0.00 | --- |
| 26 | 0.0 | 2 | 7.14 | 142.86 | 4.76 | 95.24 | 0.00 | --- |
| 26 | 0.0 | 5 | 200.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 26 | 0.0 | 3 | 130.00 | 130.00 | 50.00 | 50.00 | 0.00 | --- |
| 27 | 0.0 | 1 | 24.55 | 245.45 | 9.09 | 90.91 | 0.00 | --- |
| 27 | 0.0 | 5 | 130.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 27 | 0.0 | 2 | 10.00 | 100.00 | 9.09 | 90.91 | 0.00 | --- |
| 28 | 0.0 | 2 | 9.09 | 90.91 | 9.09 | 90.91 | 0.00 | --- |
| 28 | 3.0 | 5 | 507.00 | 0.00 | 99.41 | 0.00 | 0.59 | --- |
| 29 | 0.0 | 5 | 610.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 30 | 0.0 | 5 | 610.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 31 | 0.0 | 5 | 177.80 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 31 | 25.4 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- |
| ns3 | --- | --- | --- | --- | --- | ---- | ---- | --- |
| 31 | 0.0 | 4 | 224.12 | 29.88 | 88.24 | 11.76 | 0.00 | --- |
| 31 | 25.4 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | 83.28 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- |
| 35 | 0.0 | 2 | 79.57 | 530.43 | 13.04 | 86.96 | 0.00 | 13.04 |
| 36 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 36 | 0.0 | 3 | 152.67 | 30.53 | 83.33 | 16.67 | 0.00 | --- |
| 36 | 0.0 | 3 | 339.00 | 67.80 | 83.33 | 16.67 | 0.00 | --- |
| 37 | 0.0 | 2 | 79.57 | 530.43 | 13.04 | 86.96 | 0.00 | --- |
| 38 | 0.0 | 3 | 610.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- |
| 32 | 0.5 | 2 | 49.95 | 499.55 | 9.08 | 90.83 | 0.09 | --- |
| 32 | 0.0 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 33 | 0.0 | 3 | 50.80 | 152.40 | 25.00 | 75.00 | 0.00 | --- |
| 33 | 0.0 | 3 | 67.73 | 135.47 | 33.33 | 66.67 | 0.00 | 29.17 |
| ns6 | --- | --- | --- | --- | --- | --- | --- | --- |
| 34 | 0.0 | 3 | 190.50 | 38.10 | 83.33 | 16.67 | 0.00 | --- |
| 34 | 0.0 | 3 | 115.45 | 11.55 | 90.91 | 9.09 | 0.00 | --- |
| 34 | 5.0 | 3 | 61.00 | 61.00 | 48.03 | 48.03 | 3.94 | 76.04 |
| ns7 | --- | --- | --- | --- | --- | --- | --- | --- |
| 39 | 0.5 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 10.00 | --- |
| 39 | 1.0 | 3 | 92.67 | 46.33 | 66.19 | 33.10 | 0.71 | --- |
| 39 | 0.0 | 3 | 110.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 39 | 0.0 | 2 | 16.67 | 333.33 | 4.76 | 95.24 | 0.00 | --- |
| 40 | 1.0 | 4 | 380.63 | 228.38 | 62.40 | 37.44 | 0.16 | --- |
| 41 | 1.0 | 5 | 202.20 | 0.00 | 99.51 | 0.00 | 0.49 | --- |
| 41 | 3.0 | 3 | 162.10 | 0.00 | 98.18 | 0.00 | 1.82 | --- |
| 41 | 4.0 | 3 | 208.33 | 41.67 | 82.02 | 16.40 | 1.57 | --- |
| 42 | 10.0 | 3 | 300.00 | 300.00 | 49.18 | 49.18 | 1.64 | --- |
| 43 | 30.0 | 3 | 351.00 | 0.00 | 92.13 | 0.00 | 7.87 | --- |
| 43 | 0.0 | 5 | 203.20 | 0.00 | 100.00 | 0.00 | 0.00 | 94.86 |
| 44 | 10.0 |  | 600.00 | 0.00 | 98.36 | 0.00 | 1.64 | --- |
| 45 | 10.0 |  | 55.17 | 11.03 | 72.40 | 14.48 | 13.12 | --- |
| 45 | 20.0 | 5 | 183.20 | 0.00 | 90.16 | 0.00 | 9.84 | --- |
| 45 | 5.0 | 3 | 325.20 | 0.00 | 98.49 | 0.00 | 1.51 | --- |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 25 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 26 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 26 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 26 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 27 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 27 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 27 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 28 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 28 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 29 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 30 | --- | --- | 80 | 12.50 | --- | --- | --- | --- |
| 31 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 31 | --- | --- | 10 | 100.00 | --- | --- | SubA | Fusain layer. |
| ns3 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 31 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 31 | 6.19 | 10.53 | 5 | 200.00 | 105.26 | 69.21 | --- | Fusain layer. |
| ns4 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 35 | 86.96 | 0.00 | 20 | 50.00 | 50.00 | 68.12 | --- | --- |
| 36 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 36 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 36 | --- | --- | 100 | 10.00 | --- | --- | --- | --- |
| 37 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 38 | 0.00 | 0.00 | 50 | 20.00 | 20.00 | 25.97 | --- | --- |
| ns5 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 32 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 32 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 33 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 33 | 70.83 | 0.00 | 10 | 100.00 | 75.00 | 26.46 | --- | -- |
| ns6 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 34 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 34 | --- | --- | 10 | 100.00 | --- | - | --- | --- |
| 34 | 22.93 | 1.04 | 10 | 100.00 | 100.00 | 46.68 | --- | --- |
| ns7 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 39 | --- | --- | 10 | 100.00 | --- | --- | --- | Fusain layer. |
| 39 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 39 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 39 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 40 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 41 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 41 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 41 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 42 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 43 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 43 | 0.00 | 5.14 | 20 | 50.00 | 50.00 | 33.42 | --- | --- |
| 44 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 45 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 45 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 45 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approxima (ft) | te depth | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| 46 | 1,323.00 | --- | Big George | 20.32 | --- | 0.33 | 109.42 | 40.0 | 0.0 |
| 46 | --- | --- | Big George | 10.16 | --- | 0.17 | 109.75 | 4.0 | 0.0 |
| 46 | --- | 1,325.00 | Big George | 30.48 | 60.96 | 0.50 | 110.75 | 5.0 | 0.0 |
| 47 | 1,325.00 | 1,327.00 | Big George | 61.00 | 61.00 | 1.00 | 112.76 | 4.0 | 15.0 |
| ns8 | 1,327.00 | 1,332.00 | ns8 | 152.00 | 152.00 | 1.00 | 117.74 | --- | --- |
| 48 | 1,332.00 | --- | Big George | 7.62 | --- | 0.13 | 117.99 | 1.0 | 5.0 |
| 48 | --- | --- | Big George | 10.16 | --- | 0.17 | 118.33 | 20.0 | 10.0 |
| 48 | --- | --- | Big George | 13.97 | --- | 0.24 | 118.78 | 0.0 | 5.0 |
| 48 | --- | --- | Big George | 21.59 | --- | 0.37 | 119.49 | 20.0 | 10.0 |
| 48 | --- | 1,334.00 | Big George | 5.08 | 58.42 | 0.09 | 119.66 | 1.0 | 2.0 |
| ns9 | 1,334.00 | 1,335.00 | ns9 | 30.50 | 30.50 | 1.00 | 120.66 | --- | --- |
| 49 | 1,335.00 | --- | Big George | 25.40 | --- | 0.42 | 121.49 | 4.0 | 10.0 |
| 49 | --- | 1,337.00 | Big George | 35.60 | 61.00 | 0.58 | 122.66 | 5.0 | 5.0 |
| 50 | 1,337.00 | --- | Big George | 57.00 | --- | 0.93 | 124.53 | 2.0 | 40.0 |
| 50 | --- | 1,339.00 | Big George | 4.00 | 61.00 | 0.07 | 124.66 | 0.0 | 0.0 |
| 51 | 1,339.00 | --- | Big George | 45.76 | --- | 0.75 | 126.16 | 60.0 | 0.0 |
| 51 | --- | 1,341.00 | Big George | 15.24 | 61.00 | 0.25 | 126.66 | 10.0 | 100.0 |
| 52 | 1,341.00 | 1,343.00 | Big George | 61.00 | 61.00 | 1.00 | 128.67 | 50.0 | 0.0 |
| 53 | 1,343.00 | 1,345.00 | Big George | 61.00 | 61.00 | 1.00 | 130.67 | 10.0 | 40.0 |
| 54 | 1,345.00 | 1,347.00 | Big George | 61.00 | 61.00 | 1.00 | 132.67 | 50.0 | 0.0 |
| 55 | 1,347.00 | --- | Big George | 20.32 | --- | 0.33 | 133.33 | 50.0 | 0.0 |
| 55 | --- | --- | Big George | 30.48 | --- | 0.50 | 134.33 | 20.0 | 0.0 |
| 55 | --- | 1,349.00 | Big George | 10.16 | 60.96 | 0.17 | 134.67 | 20.0 | 0.0 |
| 56 | 1,349.00 | 1,351.00 | Big George | 61.00 | 61.00 | 1.00 | 136.67 | 30.0 | 0.0 |
| 57 | 1,351.00 | --- | Big George | 27.94 | --- | 0.46 | 137.59 | 20.0 | 10.0 |
| 57 | --- | --- | Big George | 20.32 | --- | 0.33 | 138.25 | 12.0 | 5.0 |
| 57 | --- | 1,353.00 | Big George | 12.70 | 60.96 | 0.21 | 138.67 | 3.0 | 0.0 |
| 58 | 1,353.00 | --- | Big George | 38.10 | --- | 0.63 | 139.92 | 10.0 | 0.0 |
| 58 | --- | --- | Big George | 12.70 | --- | 0.21 | 140.34 | 20.0 | 10.0 |
| 58 | --- | 1,355.00 | Big George | 10.16 | 60.96 | 0.17 | 140.67 | 4.0 | 0.0 |
| 59 | 1,355.00 | 1,357.00 | Big George | 61.00 | 61.00 | 1.00 | 142.67 | 20.0 | 0.0 |
| 61 | 1,357.00 | 1,359.00 | Big George | 61.00 | 61.00 | 1.00 | 144.67 | 20.0 | 30.0 |
| 64 | 1,359.00 | --- | Big George | 17.78 | --- | 0.29 | 145.26 | 3.0 | 0.0 |
| 64 | --- | --- | Big George | 2.50 | --- | 0.04 | 145.34 | 0.0 | 0.0 |
| 64 | --- | --- | Big George | 7.62 | --- | 0.13 | 145.59 | 5.0 | 0.0 |
| 64 | --- | 1,361.00 | Big George | 33.02 | 60.92 | 0.54 | 146.67 | 0.0 | 20.0 |

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | 40.0 | 5 | 163.20 | 0.00 | 80.31 | 0.00 | 19.69 | --- |
| 46 | 1.0 | 2 | 100.60 | 0.00 | 99.02 | 0.00 | 0.98 | --- |
| 46 | 1.0 | 3 | 303.80 | 0.00 | 99.67 | 0.00 | 0.33 | --- |
| 47 | 0.0 | 2 | 128.42 | 481.58 | 21.05 | 78.95 | 0.00 | --- |
| ns8 | --- | --- | --- | --- | --- | --- | --- | --- |
| 48 | 3.0 | 2 | 12.20 | 61.00 | 16.01 | 80.05 | 3.94 | --- |
| 48 | 2.0 | 3 | 66.40 | 33.20 | 65.35 | 32.68 | 1.97 | --- |
| 48 | 2.0 | 1 | 0.00 | 137.70 | 0.00 | 98.57 | 1.43 | --- |
| 48 | 5.0 | 3 | 140.60 | 70.30 | 65.12 | 32.56 | 2.32 | --- |
| 48 | 0.0 | 2 | 16.93 | 33.87 | 33.33 | 66.67 | 0.00 | 40.42 |
| ns9 | --- | --- | --- | --- | --- | --- | --- | --- |
| 49 | 10.0 | 2 | 69.71 | 174.29 | 27.45 | 68.62 | 3.94 | --- |
| 49 | 1.0 | 3 | 177.50 | 177.50 | 49.86 | 49.86 | 0.28 | 40.53 |
| 50 | 0.0 | 1 | 27.14 | 542.86 | 4.76 | 95.24 | 0.00 | --- |
| 50 | 40.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- |
| 51 | 0.0 | 5 | 457.60 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 51 | 0.0 | 3 | 13.85 | 138.55 | 9.09 | 90.91 | 0.00 | --- |
| 52 | 10.0 | 5 | 600.00 | 0.00 | 98.36 | 0.00 | 1.64 | --- |
| 53 | 0.0 | 3 | 122.00 | 488.00 | 20.00 | 80.00 | 0.00 | --- |
| 54 | 10.0 | 5 | 600.00 | 0.00 | 98.36 | 0.00 | 1.64 | --- |
| 55 | 20.0 | 5 | 183.20 | 0.00 | 90.16 | 0.00 | 9.84 | --- |
| 55 | 30.0 | 3 | 274.80 | 0.00 | 90.16 | 0.00 | 9.84 | --- |
| 55 | 10.0 | 3 | 91.60 | 0.00 | 90.16 | 0.00 | 9.84 | 90.16 |
| 56 | 10.0 | 5 | 600.00 | 0.00 | 98.36 | 0.00 | 1.64 | 98.36 |
| 57 | 10.0 | 3 | 179.60 | 89.80 | 64.28 | 32.14 | 3.58 | --- |
| 57 | 1.0 | 3 | 142.73 | 59.47 | 70.24 | 29.27 | 0.49 | --- |
| 57 | 40.0 | 2 | 87.00 | 0.00 | 68.50 | 0.00 | 31.50 | 67.15 |
| 58 | 15.0 | 3 | 366.00 | 0.00 | 96.06 | 0.00 | 3.94 | --- |
| 58 | 4.0 | 3 | 82.00 | 41.00 | 64.57 | 32.28 | 3.15 | --- |
| 58 | 10.0 | 2 | 91.60 | 0.00 | 90.16 | 0.00 | 9.84 | 88.52 |
| 59 | 20.0 | 3 | 590.00 | 0.00 | 96.72 | 0.00 | 3.28 | 96.72 |
| 61 | 4.0 | 3 | 242.40 | 363.60 | 39.74 | 59.61 | 0.66 | 39.74 |
| 64 | 5.0 | 2 | 172.80 | 0.00 | 97.19 | 0.00 | 2.81 | --- |
| 64 | 25.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- |
| 64 | 5.0 | 3 | 71.20 | 0.00 | 93.44 | 0.00 | 6.56 | --- |
| 64 | 10.0 | 1 | 0.00 | 320.20 | 0.00 | 96.97 | 3.03 | 40.05 |

## 28 Megascopic Lithologic Studies of Coals, Wyoming and North Dakota

Table 1-1. Data for samples from core hole 1, MichiWest Energy Inc., Pilot State 16-14.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 46 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 46 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 47 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| ns8 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 48 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 48 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 48 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 48 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 48 | 57.53 | 2.05 | 20 | 50.00 | 50.00 | 77.45 | SubA | --- |
| ns9 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 49 | --- | --- | 40 | 25.00 | --- | --- | --- | --- |
| 49 | 57.67 | 1.80 | 40 | 25.00 | 25.00 | 21.98 | --- | --- |
| 50 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 50 | --- | --- | 25 | 40.00 | --- | --- | --- | Fusain layer. |
| 51 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 51 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 52 | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| 53 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| 54 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 55 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 55 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 55 | 0.00 | 9.84 | 10 | 100.00 | 100.00 | 63.82 | --- | --- |
| 56 | 0.00 | 1.64 | 5 | 200.00 | 200.00 | 46.98 | --- | --- |
| 57 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 57 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 57 | 24.49 | 8.37 | 5 | 200.00 | 200.00 | 64.15 | SubB | --- |
| 58 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 58 | --- | --- | 10 | 100.00 | --- | --- | --- | --- |
| 58 | 6.73 | 4.76 | 10 | 100.00 | 100.00 | 53.23 | --- | --- |
| 59 | 0.00 | 3.28 | 10 | 100.00 | 100.00 | 55.36 | --- | --- |
| 61 | 59.61 | 0.66 | 20 | 50.00 | 50.00 | 76.09 | --- | --- |
| 64 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 64 | --- | --- | 5 | 200.00 | --- | --- | --- | Fusain layer. |
| 64 | --- | --- | 5 | 200.00 | --- | --- | --- | --- |
| 64 | 52.56 | 7.39 | 5 | 200.00 | 200.00 | 70.87 | SubA | --- |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approx dept | $\begin{aligned} & \text { ximate } \\ & \text { h (ft) } \end{aligned}$ | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 1 | 1,077.00 | --- | Big George | 28.00 | --- | 0.52 | 0.92 | 50.0 | 0.0 | 0.0 |
| 1 | --- | 1,079.00 | Big George | 26.00 | 54.00 | 0.48 | 1.77 | 10.0 | 2.0 | 26.0 |
| MC-1 | 1,079.00 | --- | Big George | 10.00 | --- | 0.16 | 2.10 | 50.0 | 0.0 | 0.0 |
| MC-1 | --- | --- | Big George | 20.00 | --- | 0.31 | 2.76 | 10.0 | 10.0 | 0.0 |
| MC-1 | --- | 1,081.00 | Big George | 34.00 | 64.00 | 0.53 | 3.87 | 50.0 | 0.0 | 5.0 |
| 2 | 1,081.00 | --- | Big George | 27.00 | --- | 0.45 | 4.76 | 20.0 | 4.0 | 0.0 |
| 2 | --- | 1,083.00 | Big George | 33.00 | 60.00 | 0.55 | 5.84 | 10.0 | 30.0 | 2.0 |
| 3 | 1,083.00 | 1,085.00 | Big George | 60.00 | 60.00 | 1.00 | 7.81 | 2.0 | 20.0 | 0.0 |
| 4 | 1,085.00 | --- | Big George | 38.00 | --- | 0.63 | 9.06 | 2.0 | 10.0 | 5.0 |
| 4 | --- | 1,087.00 | Big George | 22.00 | 60.00 | 0.37 | 9.78 | 50.0 | 0.0 | 0.0 |
| 5 | 1,087.00 | --- | Big George | 16.00 | --- | 0.25 | 10.30 | 20.0 | 5.0 | 0.0 |
| 5 | --- | 1,089.00 | Big George | 47.00 | 63.00 | 0.75 | 11.84 | 2.0 | 50.0 | 15.0 |
| 6 | 1,089.00 | --- | Big George | 8.00 | --- | 0.13 | 12.11 | 2.0 | 50.0 | 2.0 |
| 6 | --- | 1,091.00 | Big George | 52.00 | 60.00 | 0.87 | 13.81 | 50.0 | 2.0 | 1.0 |
| ns1 | 1,091.00 | 1,092.00 | ns1 | 30.50 | 30.50 | 1.00 | 14.81 | --- | --- | -- |
| 7 | 1,092.00 | --- | Big George | 45.00 | --- | 0.70 | 16.29 | 50.0 | 30.0 | 0.0 |
| 7 | --- | 1,094.00 | Big George | 19.00 | 64.00 | 0.30 | 16.91 | 5.0 | 2.0 | 5.0 |
| 8 | 1,094.00 | --- | Big George | 10.00 | --- | 0.15 | 17.24 | 5.0 | 2.0 | 2.0 |
| 8 | --- | --- | Big George | 33.00 | --- | 0.49 | 18.32 | 5.0 | 8.0 | 10.0 |
| 8 | --- | --- | Big George | 20.00 | --- | 0.30 | 18.98 | 20.0 | 4.0 | 0.0 |
| 8 | --- | 1,096.00 | Big George | 4.00 | 67.00 | 0.06 | 19.11 | 10.0 | 2.0 | 5.0 |
| 11 | 1,096.00 | 1,098.00 | Big George | 59.00 | 59.00 | 1.00 | 21.05 | 5.0 | 8.0 | 10.0 |
| 12 | 1,098.00 | --- | Big George | 15.00 | --- | 0.24 | 21.54 | 5.0 | 8.0 | 0.0 |
| 12 | --- | 1,100.00 | Big George | 47.00 | 62.00 | 0.76 | 23.08 | 10.0 | 10.0 | 20.0 |
| 13 | 1,100.00 | --- | Big George | 30.00 | --- | 0.52 | 24.06 | 20.0 | 30.0 | 20.0 |
| 13 | --- | 1,102.00 | Big George | 28.00 | 58.00 | 0.48 | 24.98 | 2.0 | 10.0 | 10.0 |
| 14 | 1,102.00 | 1,104.00 | Big George | 65.00 | 65.00 | 1.00 | 27.12 | 5.0 | 10.0 | 5.0 |
| MC-3 | 1,104.00 | 1,106.00 | Big George | 60.00 | 60.00 | 1.00 | 29.08 | 50.0 | 0.0 | 0.0 |
| 15 | 1,106.00 | --- | Big George | 11.00 | --- | 0.20 | 29.45 | 50.0 | 5.0 | 20.0 |
| 15 | --- | --- | Big George | 15.00 | --- | 0.28 | 29.94 | 5.0 | 5.0 | 0.0 |
| 15 | --- | 1,108.00 | Big George | 28.00 | 54.00 | 0.52 | 30.86 | 50.0 | 0.0 | 0.0 |
| 16 | 1,108.00 | --- | Big George | 30.00 | --- | 0.49 | 31.84 | 3.0 | 10.0 | 10.0 |
| 16 | --- | 1,110.00 | Big George | 31.00 | 61.00 | 0.51 | 32.86 | 10.0 | 3.0 | 5.0 |
| 18 | 1,110.00 | --- | Big George | 24.00 | --- | 0.38 | 33.65 | 10.0 | 3.0 | 5.0 |
| 18 | --- | --- | Big George | 19.00 | --- | 0.30 | 34.27 | 3.0 | 3.0 | 0.0 |
| 18 | --- | 1,112.00 | Big George | 20.00 | 63.00 | 0.32 | 34.92 | 30.0 | 40.0 | 5.0 |
| 19 | 1,112.00 | --- | Big George | 8.00 | --- | 0.13 | 35.19 | 5.0 | 5.0 | 0.0 |
| 19 | --- | --- | Big George | 47.00 | --- | 0.78 | 36.73 | 50.0 | 0.0 | 0.0 |
| 19 | --- | 1,114.00 | Big George | 5.00 | 60.00 | 0.08 | 36.89 | 49.0 | 1.0 | 0.0 |
| 20 | 1,114.00 | 1,116.00 | Big George | 59.00 | 59.00 | 1.00 | 38.83 | 50.0 | 0.0 | 0.0 |
| 21 | 1,116.00 | 1,118.00 | Big George | 61.00 | 61.00 | 1.00 | 40.83 | 70.0 | 0.0 | 5.0 |
| ns2 | 1,118.00 | 1,119.00 | ns2 | 30.50 | 30.50 | 1.00 | 41.83 | --- | --- | --- |
| MC-4ns | 1,119.00 | --- | Big George | 19.00 | --- | 1.00 | 42.45 | --- | --- | --- |
| MC-4 | --- | --- | Big George | 18.00 | --- | 0.44 | 43.04 | 50.0 | 0.0 | 0.0 |
| MC-4 | --- | 1,121.00 | Big George | 23.00 | 41.00 | 0.56 | 43.80 | 5.0 | 30.0 | 0.0 |
| 25 | 1,121.00 | --- | Big George | 16.00 | --- | 0.26 | 44.32 | 70.0 | 0.0 | 0.0 |
| 25 | --- | 1,123.00 | Big George | 45.00 | 61.00 | 0.74 | 45.80 | 30.0 | 5.0 | 0.0 |
| 26 | 1,123.00 | 1,125.00 | Big George | 61.00 | 61.00 | 1.00 | 47.80 | 2.0 | 10.0 | 0.0 |
| 27 | 1,125.00 | --- | Big George | 14.00 | --- | 0.24 | 48.26 | 2.0 | 10.0 | 0.0 |
| 27 | --- | 1,127.00 | Big George | 45.00 | 59.00 | 0.76 | 49.74 | 50.0 | 0.0 | 0.0 |
| 28 | 1,127.00 | 1,129.00 | Big George | 64.00 | 64.00 | 1.00 | 51.84 | 70.0 | 0.0 | 5.0 |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 5 | 280.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 1 | 3 | 195.00 | 39.00 | 75.00 | 15.00 | 10.00 | 87.96 | 7.22 | 4.81 |
| MC-1 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| MC-1 | 3 | 100.00 | 100.00 | 50.00 | 50.00 | 0.00 | --- | - --- | --- |
| MC-1 | 5 | 335.00 | 0.00 | 98.53 | 0.00 | 1.47 | --- | --- | --- |
| 2 | 3 | 225.00 | 45.00 | 83.33 | 16.67 | 0.00 | --- | --- | --- |
| 2 | 3 | 82.00 | 246.00 | 24.85 | 74.55 | 0.61 | 51.17 | 48.50 | 0.33 |
| 3 | 2 | 54.55 | 545.45 | 9.09 | 90.91 | 0.00 | 9.09 | 90.91 | 0.00 |
| 4 | 2 | 62.50 | 312.50 | 16.45 | 82.24 | 1.32 | --- | --- | --- |
| 4 | 5 | 220.00 | 0.00 | 100.00 | 0.00 | 0.00 | 47.08 | 52.08 | 0.83 |
| 5 | 3 | 128.00 | 32.00 | 80.00 | 20.00 | 0.00 | --- | --- | --- |
| 5 | 1 | 17.50 | 437.50 | 3.72 | 93.09 | 3.19 | 23.10 | 74.52 | 2.38 |
| 6 | 1 | 3.00 | 75.00 | 3.75 | 93.75 | 2.50 | --- | --- | -- |
| 6 | 5 | 499.04 | 19.96 | 95.97 | 3.84 | 0.19 | 83.67 | 15.83 | 0.50 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 7 | 4 | 281.25 | 168.75 | 62.50 | 37.50 | 0.00 | --- | --- | --- |
| 7 | 3 | 132.14 | 52.86 | 69.55 | 27.82 | 2.63 | 64.59 | 34.63 | 0.78 |
| 8 | 3 | 70.00 | 28.00 | 70.00 | 28.00 | 2.00 | --- | --- | --- |
| 8 | 3 | 123.08 | 196.92 | 37.30 | 59.67 | 3.03 | --- | --- | --- |
| 8 | 3 | 166.67 | 33.33 | 83.33 | 16.67 | 0.00 | --- | --- | --- |
| 8 | 3 | 29.17 | 5.83 | 72.92 | 14.58 | 12.50 | 58.05 | 39.42 | 2.54 |
| 11 | 3 | 223.08 | 356.92 | 37.81 | 60.50 | 1.69 | 37.81 | 60.50 | 1.69 |
| 12 | 3 | 57.69 | 92.31 | 38.46 | 61.54 | 0.00 | --- | --- | -- |
| 12 | 3 | 225.00 | 225.00 | 47.87 | 47.87 | 4.26 | 45.60 | 51.18 | 3.23 |
| 13 | 3 | 112.00 | 168.00 | 37.33 | 56.00 | 6.67 | -- | --- | -- |
| 13 | 2 | 45.00 | 225.00 | 16.07 | 80.36 | 3.57 | 27.07 | 67.76 | 5.17 |
| 14 | 3 | 215.00 | 430.00 | 33.08 | 66.15 | 0.77 | 33.08 | 66.15 | 0.77 |
| MC-3 | 5 | 600.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 15 | 4 | 81.82 | 8.18 | 74.38 | 7.44 | 18.18 | --- | --- | --- |
| 15 | 3 | 75.00 | 75.00 | 50.00 | 50.00 | 0.00 | --- | --- | -- |
| 15 | 5 | 280.00 | 0.00 | 100.00 | 0.00 | 0.00 | 80.89 | 15.40 | 3.70 |
| 16 | 2 | 66.92 | 223.08 | 22.31 | 74.36 | 3.33 | --- | --- | --- |
| 16 | 3 | 234.62 | 70.38 | 75.68 | 22.70 | 1.61 | 49.43 | 48.11 | 2.46 |
| 18 | 3 | 180.77 | 54.23 | 75.32 | 22.60 | 2.08 | --- | --- | --- |
| 18 | 2 | 95.00 | 95.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| 18 | 4 | 83.57 | 111.43 | 41.79 | 55.71 | 2.50 | 57.04 | 41.37 | 1.59 |
| 19 | 3 | 40.00 | 40.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| 19 | 5 | 470.00 | 0.00 | 100.00 | 0.00 | 0.00 | -- | --- | --- |
| 19 | 5 | 49.00 | 1.00 | 98.00 | 2.00 | 0.00 | 93.17 | 6.83 | 0.00 |
| 20 | 5 | 590.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| 21 | 5 | 605.00 | 0.00 | 99.18 | 0.00 | 0.82 | 99.18 | 0.00 | 0.82 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| MC-4ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| MC-4 | 5 | 180.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| MC-4 | 3 | 32.86 | 197.14 | 14.29 | 85.71 | 0.00 | --- | --- | --- |
| 25 | 5 | 160.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 25 | 4 | 385.71 | 64.29 | 85.71 | 14.29 | 0.00 | 89.46 | 10.54 | 0.00 |
| 26 | 2 | 101.67 | 508.33 | 16.67 | 83.33 | 0.00 | 16.67 | 83.33 | 0.00 |
| 27 | 2 | 23.33 | 116.67 | 16.67 | 83.33 | 0.00 | --- | --- | --- |
| 27 | 5 | 450.00 | 0.00 | 100.00 | 0.00 | 0.00 | 80.23 | 19.77 | 0.00 |
| 28 | 5 | 635.00 | 0.00 | 99.22 | 0.00 | 0.78 | 99.22 | 0.00 | 0.78 |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | $\begin{gathered} \text { Cleat } \\ \text { spacing } \\ \text { (CS) }(\mathrm{mm}) \end{gathered}$ | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 10 | 100.00 | --- | --- | --- | --- |
| 1 | 10 | 100.00 | 100.00 | 62.03 | --- | Kaolinite on cleat. |
| MC-1 | --- | --- | --- | --- | --- | --- |
| MC-1 | --- | --- | --- | --- | --- | --- |
| MC-1 | --- | --- | --- | --- | --- | --- |
| 2 | 5 | 200.00 | --- | --- | --- | --- |
| 2 | 2 | 500.00 | 365.00 | 68.17 | SubA | --- |
| 3 | 20 | 50.00 | 50.00 | 78.09 | --- | --- |
| 4 | 5 | 200.00 | --- | --- | --- | --- |
| 4 | 10 | 100.00 | 163.33 | 70.29 | --- | --- |
| 5 | 30 | 33.33 | --- | --- | --- | Curvilinear fractures, bright vitrain. |
| 5 | 30 | 33.33 | 33.33 | 74.09 | --- | --- |
| 6 | 10 | 100.00 | --- | --- | --- | Curvilinear fractures and microfractures. |
| 6 | 10 | 100.00 | 100.00 | 90.52 | SubA | --- |
| ns1 | --- | --- | --- | --- | --- | Adsorption analysis sample removed. |
| 7 | 10 | 100.00 | --- | --- | --- | --- |
| 7 | 20 | 50.00 | 85.16 | 73.59 | --- | Bright. |
| 8 | 70 | 14.29 | --- | --- | --- | Tight. |
| 8 | 70 | 14.29 | --- | --- | --- | --- |
| 8 | 50 | 20.00 | --- | --- | --- | Resin. |
| 8 | 50 | 20.00 | 16.33 | 72.68 | --- | Horizontal fractures. |
| 11 | 40 | 25.00 | 25.00 | 72.68 | --- | Inert attritus. |
| 12 | 40 | 25.00 | --- | --- | --- | --- |
| 12 | 10 | 100.00 | 81.85 | 75.16 | --- |  |
| 13 | 15 | 66.67 | --- | --- | --- | Minor cleat. |
| 13 | 5 | 200.00 | 131.03 | 76.02 | --- | --- |
| 14 | 30 | 33.33 | 33.33 | 74.06 | SubA | More fractured at basal 10 cm . |
| MC-3 | 10 | 100.00 | --- | --- | --- | Highly fractured sample. |
| 15 | 30 | 33.33 | --- | --- | --- | 1 cm thick fusain bands at 9 and 11 cm . |
| 15 | 50 | 20.00 | --- | --- | --- | Closed cleat, hard. |
| 15 | 40 | 25.00 | 25.31 | 72.07 | --- | Bright, brittle. |
| 16 | 10 | 100.00 | --- | --- | --- | --- |
| 16 | 70 | 14.29 | 56.44 | 73.39 | --- | Hard, mineralization along tight cleat. |
| 18 | 30 | 33.33 | --- | --- | --- | --- |
| 18 | 70 | 14.29 | --- | --- | --- | Hard, cleat mineralization at base. |
| 18 | 40 | 25.00 | 24.94 | 75.96 | --- | Cleat mineralization. |
| 19 | 40 | 25.00 | --- | --- | --- | --- |
| 19 | 70 | 14.29 | --- | --- | --- | Hard to break, bright. |
| 19 | 10 | 100.00 | 22.86 | 72.88 | --- | --- |
| 20 | 50 | 20.00 | 20.00 | 72.17 | --- | Hard to find cleat. |
| 21 | 50 | 20.00 | 20.00 | 79.51 | SubA | Brittle, bright, cleat mineralization at 8 and 50 cm . |
| ns2 | --- | --- | --- | --- | --- | No sample. |
| MC-4ns | --- | --- | --- | --- | --- | Adsorption analysis sample removed. |
| MC-4 | 30 | 33.33 | --- | --- | --- | --- |
| MC-4 | 30 | 33.33 | --- | --- | --- | --- |
| 25 | 20 | 50.00 | --- | --- | --- | --- |
| 25 | 20 | 50.00 | 50.00 | 73.29 | --- | --- |
| 26 | 40 | 25.00 | 25.00 | 74.18 | --- | Kaolinite(?). |
| 27 | 40 | 25.00 | --- | --- | --- | Curvilinear cleat, tight, kaolinite on surface. |
| 27 | 70 | 14.29 | 16.83 | 77.46 | --- | --- |
| 28 | 70 | 14.29 | 14.29 | 75.35 | --- | --- |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 30 | 1,129.00 | 1,131.00 | Big George | 64.00 | 64.00 | 1.00 | 53.94 | 70.0 | 0.0 | 60.0 |
| 32 | 1,131.00 | --- | Big George | 6.00 | --- | 0.10 | 54.13 | 50.0 | 0.0 | 0.0 |
| 32 |  | 1,133.00 | Big George | 54.00 | 60.00 | 0.90 | 55.91 | 5.0 | 10.0 | 35.0 |
| MC-6ns | 1,133.00 | 1,134.00 | Big George | 30.50 | 30.50 | 1.00 | 56.91 | --- | --- | --- |
| MC-5 | 1,134.00 | 1,136.00 | Big George | 60.00 | 60.00 | 1.00 | 58.87 | 5.0 | 20.0 | 10.0 |
| 38 | 1,136.00 | 1,138.00 | Big George | 60.00 | 60.00 | 1.00 | 60.84 | 5.0 | 10.0 | 10.0 |
| 39 | 1,138.00 | ---- | Big George | 5.00 | --- | 0.09 | 61.01 | 5.0 | 10.0 | 0.0 |
| 39 | --- | --- | Big George | 9.00 | --- | 0.17 | 61.30 | 0.0 | 0.0 | 90.0 |
| 39 | --- | 1,140.00 | Big George | 39.00 | 53.00 | 0.74 | 62.58 | 5.0 | 10.0 | 10.0 |
| 40 | 1,140.00 | --- | Big George | 9.00 | --- | 0.16 | 62.88 | 5.0 | 10.0 | 2.0 |
| 40 | --- | --- | Big George | 29.00 | --- | 0.50 | 63.83 | 50.0 | 0.0 | 6.0 |
| 40 | --- | 1,142.00 | Big George | 20.00 | 58.00 | 0.34 | 64.48 | 10.0 | 30.0 | 0.0 |
| 42 | 1,142.00 | --- | Big George | 51.00 | --- | 0.91 | 66.16 | 50.0 | 10.0 | 0.0 |
| 42 | --- | 1,144.00 | Big George | 5.00 | 56.00 | 0.09 | 66.32 | 50.0 | 0.0 | 0.0 |
| 47 | 1,144.00 | 1,146.00 | Big George | 58.00 | 58.00 | 1.00 | 68.23 | 70.0 | 0.0 | 0.0 |
| MC-7fr | 1,146.00 | 1,148.00 | Big George | 60.00 | 60.00 | 1.00 | 70.19 | --- | --- | --- |
| ns3 | 1,148.00 | 1,149.00 | ns3 | 30.50 | 30.50 | 1.00 | 71.19 | --- | --- | --- |
| 50 | 1,149.00 | 1,151.00 | Big George | 58.00 | 58.00 | 1.00 | 73.10 | 20.0 | 5.0 | 10.0 |
| 51 | 1,151.00 | 1,153.00 | Big George | 60.00 | 60.00 | 1.00 | 75.07 | 5.0 | 20.0 | 25.0 |
| 53 | 1,153.00 | 1,155.00 | Big George | 60.00 | 60.00 | 1.00 | 77.03 | 10.0 | 30.0 | 10.0 |
| 60 | 1,155.00 | --- | Big George | 17.00 | --- | 0.28 | 77.59 | 5.0 | 10.0 | 0.0 |
| 60 | --- | 1,157.00 | Big George | 43.00 | 60.00 | 0.72 | 79.00 | 70.0 | 0.0 | 10.0 |
| 62 | 1,157.00 | --- | Big George | 41.00 | --- | 0.68 | 80.35 | 2.0 | 10.0 | 14.0 |
| 62 | --- | 1,159.00 | Big George | 19.00 | 60.00 | 0.32 | 80.97 | 70.0 | 5.0 | 10.0 |
| 63 | 1,159.00 | --- | Big George | 7.00 | --- | 0.14 | 81.20 | 65.0 | 5.0 | 0.0 |
| 63 | --- | --- | Big George | 20.00 | --- | 0.41 | 81.86 | 2.0 | 20.0 | 10.0 |
| 63 | --- | --- | Big George | 10.00 | --- | 0.20 | 82.19 | 10.0 | 10.0 | 10.0 |
| 63 | --- | --- | Big George | 6.00 | --- | 0.12 | 82.38 | 30.0 | 5.0 | 0.0 |
| 63 | --- | 1,161.00 | Big George | 6.00 | 49.00 | 0.12 | 82.58 | 10.0 | 40.0 | 0.0 |
| ns4 | 1,161.00 | 1,162.00 | ns4 | 30.50 | 30.50 | 1.00 | 83.58 | --- | --- | -- |
| MC-8 | 1,162.00 | 1,164.00 | Big George | 60.00 | 60.00 | 1.00 | 85.55 | 10.0 | 20.0 | 20.0 |
| 65 | 1,164.00 | --- | Big George | 14.00 | --- | 0.23 | 86.01 | 3.0 | 1.0 | 10.0 |
| 65 | --- | --- | Big George | 12.00 | --- | 0.20 | 86.40 | 20.0 | 0.0 | 0.0 |
| 65 | --- | 1,166.00 | Big George | 34.00 | 60.00 | 0.57 | 87.52 | 5.0 | 3.0 | 30.0 |
| 66 | 1,166.00 | --- | Big George | 42.00 | --- | 0.70 | 88.89 | 5.0 | 3.0 | 30.0 |
| 66 | --- | 1,168.00 | Big George | 18.00 | 60.00 | 0.30 | 89.48 | 3.0 | 5.0 | 0.0 |
| 67 | 1,168.00 | 1,170.00 | Big George | 63.00 | 63.00 | 1.00 | 91.55 | 10.0 | 5.0 | 50.0 |
| 68 | 1,170.00 | 1,172.00 | Big George | 64.00 | 64.00 | 1.00 | 93.65 | 10.0 | 5.0 | 100.0 |
| 69 | 1,172.00 | --- | Big George | 9.00 | --- | 0.15 | 93.95 | 10.0 | 5.0 | 10.0 |
| 69 | --- | --- | Big George | 20.00 | --- | 0.33 | 94.60 | 30.0 | 0.0 | 0.0 |
| 69 | --- | 1,174.00 | Big George | 31.00 | 60.00 | 0.52 | 95.62 | 10.0 | 2.0 | 15.0 |
| 70 | 1,174.00 | --- | Big George | 15.00 | --- | 0.23 | 96.11 | 10.0 | 2.0 | 15.0 |
| 70 | --- | 1,176.00 | Big George | 50.00 | 65.00 | 0.77 | 97.75 | 10.0 | 20.0 | 0.0 |
| ns5 | 1,176.00 | 1,177.00 | ns5 | 30.50 | 30.50 | 1.00 | 98.75 | --- | --- | --- |
| MC-9 | 1,177.00 | , | Big George | 16.00 | --- | 0.27 | 99.28 | 5.0 | 5.0 | 0.0 |
| MC-9 | --- | --- | Big George | 16.00 | --- | 0.27 | 99.80 | 20.0 | 30.0 | 5.0 |
| MC-9 | --- | 1,179.00 | Big George | 27.00 | 59.00 | 0.46 | 100.69 | 20.0 | 50.0 | 10.0 |
| ns6 | 1,179.00 | 1,180.50 | ns6 | 45.70 | 45.70 | 1.00 | 102.19 | --- | --- | --- |
| MC-10 | 1,180.50 | 1,182.50 | Big George | 60.00 | 60.00 | 1.00 | 104.16 | 30.0 | 30.0 | 0.0 |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 5 | 580.00 | 0.00 | 90.63 | 0.00 | 9.38 | 90.63 | 0.00 | 9.38 |
| 32 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 32 | 3 | 168.33 | 336.67 | 31.17 | 62.35 | 6.48 | 38.06 | 56.11 | 5.83 |
| MC-6ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| MC-5 | 3 | 118.00 | 472.00 | 19.67 | 78.67 | 1.67 | --- | --- | --- |
| 38 | 3 | 196.67 | 393.33 | 32.78 | 65.56 | 1.67 | 32.78 | 65.56 | 1.67 |
| 39 | 3 | 16.67 | 33.33 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| 39 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- | --- |
| 39 | 3 | 126.67 | 253.33 | 32.48 | 64.96 | 2.56 | 27.04 | 54.09 | 18.87 |
| 40 | 3 | 29.33 | 58.67 | 32.59 | 65.19 | 2.22 | --- | --- | --- |
| 40 | 5 | 284.00 | 0.00 | 97.93 | 0.00 | 2.07 | --- | --- | --- |
| 40 | 3 | 50.00 | 150.00 | 25.00 | 75.00 | 0.00 | 62.64 | 35.98 | 1.38 |
| 42 | 4 | 425.00 | 85.00 | 83.33 | 16.67 | 0.00 | --- | --- | --- |
| 42 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | 84.82 | 15.18 | 0.00 |
| 47 | 5 | 580.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| MC-7fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 50 | 3 | 456.00 | 114.00 | 78.62 | 19.66 | 1.72 | 78.62 | 19.66 | 1.72 |
| 51 | 3 | 115.00 | 460.00 | 19.17 | 76.67 | 4.17 | 19.17 | 76.67 | 4.17 |
| 53 | 3 | 147.50 | 442.50 | 24.58 | 73.75 | 1.67 | 24.58 | 73.75 | 1.67 |
| 60 | 3 | 56.67 | 113.33 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| 60 | 5 | 420.00 | 0.00 | 97.67 | 0.00 | 2.33 | 79.44 | 18.89 | 1.67 |
| 62 | 2 | 66.00 | 330.00 | 16.10 | 80.49 | 3.41 | --- | --- | --- |
| 62 | 4 | 168.00 | 12.00 | 88.42 | 6.32 | 5.26 | 39.00 | 57.00 | 4.00 |
| 63 | 4 | 65.00 | 5.00 | 92.86 | 7.14 | 0.00 | --- | --- | --- |
| 63 | 2 | 17.27 | 172.73 | 8.64 | 86.36 | 5.00 | --- | --- | --- |
| 63 | 3 | 45.00 | 45.00 | 45.00 | 45.00 | 10.00 | --- | --- | --- |
| 63 | 4 | 51.43 | 8.57 | 85.71 | 14.29 | 0.00 | --- | --- | --- |
| 63 | 3 | 12.00 | 48.00 | 20.00 | 80.00 | 0.00 | 38.92 | 57.00 | 4.08 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| MC-8 | 3 | 193.33 | 386.67 | 32.22 | 64.44 | 3.33 | --- | --- | --- |
| 65 | 2 | 97.50 | 32.50 | 69.64 | 23.21 | 7.14 | --- | --- | --- |
| 65 | 3 | 120.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 65 | 3 | 193.75 | 116.25 | 56.99 | 34.19 | 8.82 | 68.54 | 24.79 | 6.67 |
| 66 | 3 | 243.75 | 146.25 | 58.04 | 34.82 | 7.14 | --- | --- | --- |
| 66 | 2 | 67.50 | 112.50 | 37.50 | 62.50 | 0.00 | 51.88 | 43.13 | 5.00 |
| 67 | 3 | 386.67 | 193.33 | 61.38 | 30.69 | 7.94 | 61.38 | 30.69 | 7.94 |
| 68 | 3 | 360.00 | 180.00 | 56.25 | 28.13 | 15.63 | 56.25 | 28.13 | 15.63 |
| 69 | 3 | 53.33 | 26.67 | 59.26 | 29.63 | 11.11 | --- | --- | --- |
| 69 | 5 | 200.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 69 | 3 | 245.83 | 49.17 | 79.30 | 15.86 | 4.84 | 83.19 | 12.64 | 4.17 |
| 70 | 3 | 112.50 | 22.50 | 75.00 | 15.00 | 10.00 | --- | --- | --- |
| 70 | 3 | 166.67 | 333.33 | 33.33 | 66.67 | 0.00 | 42.95 | 54.74 | 2.31 |
| ns5 | --- | --- | --- | --- | --- | ---- | --- | --- | --- |
| MC-9 | 3 | 80.00 | 80.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| MC-9 | 3 | 62.00 | 93.00 | 38.75 | 58.13 | 3.13 | --- | --- | --- |
| MC-9 | 3 | 74.29 | 185.71 | 27.51 | 68.78 | 3.70 | --- | --- | --- |
| ns6 | -- | --- | --- | --- | --- | --- | --- | --- | --- |
| MC-10 | 4 | 300.00 | 300.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |

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Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 40 | 25.00 | 25.00 | 74.33 | --- | 2 thick fusain attrital layers, kaolinite on cleat. |
| 32 | 40 | 25.00 | --- | --- | --- | --- |
| 32 | 30 | 33.33 | 32.50 | 79.57 | --- | --- |
| MC-6ns | --- | --- | --- | --- | --- | Adsorption analysis sample removed. |
| MC-5 | 10 | 100.00 | --- | --- | --- | Adsorption analysis sample removed. |
| 38 | 4 | 250.00 | 250.00 | 79.05 | SubA | Highly fractured sample, 50 mm of vitrain at 49 cm , calcite. |
| 39 | 4 | 250.00 | --- | --- | --- | Highly fractured sample, calcite on cleat. |
| 39 | 4 | 250.00 | --- | --- | --- | Fusain layer, no calcite. |
| 39 | 10 | 100.00 | 139.62 | 77.32 | --- | Thick calcite on cleat. |
| 40 | 4 | 250.00 | --- | --- | --- | Calcite. |
| 40 | 4 | 250.00 | --- | --- | --- | Calcite. |
| 40 | 4 | 250.00 | 250.00 | 79.82 | --- | Calcite. |
| 42 | 4 | 250.00 | --- | --- | --- | No obvious high ash layers (unless parting was removed). |
| 42 | 40 | 25.00 | 229.91 | 78.94 | --- | No cleat mineralization. |
| 47 | 50 | 20.00 | 20.00 | 67.92 | SubB | Less cleat in basal 20 cm . |
| MC-7fr | --- | --- | --- | --- | --- | Highly fractured sample, not described. |
| ns3 | --- | --- | --- | --- | --- | No sample. |
| 50 | 10 | 100.00 | 100.00 | 75.34 | --- | Top 15 cm is highly fractured, fusain at 18 and 20 cm , kaolinite on cleat. |
| 51 | 20 | 50.00 | 50.00 | 78.80 | --- | Fusain at 34 and 55 cm , bright vitrain at 24 cm . |
| 53 | 20 | 50.00 | 50.00 | 74.97 | --- | Fusain at 24 and 43 cm , cleat kaolinite at base, bright vitrain. |
| 60 | 20 | 50.00 | --- | --- | --- | --- |
| 60 | 30 | 33.33 | 38.06 | 73.83 | --- | Fusain at 19 and 60 cm , kaolinite on cleat. |
| 62 | 10 | 100.00 | --- | --- | --- | Minor calcite at 38 cm . |
| 62 | 10 | 100.00 | 100.00 | 77.18 | SubA | Hard parting at 59 cm , calcite at base. |
| 63 | 20 | 50.00 | --- | --- | --- | --- |
| 63 | 20 | 50.00 | --- | --- | --- | --- |
| 63 | 20 | 50.00 | --- | --- | --- | Kaolinite on cleat. |
| 63 | 20 | 50.00 | --- | --- | --- | --- |
| 63 | 20 | 50.00 | 50.00 | 72.53 | SubA | Parting at base. |
| ns4 | --- | --- | --- | --- | --- | Sample removed for MichiWest geologist. |
| MC-8 | 5 | 200.00 | --- | --- | --- | Highly fractured sample, not described. |
| 65 | 10 | 100.00 | --- | --- | --- | --- |
| 65 | 20 | 50.00 | --- | --- | --- | --- |
| 65 | 20 | 50.00 | 61.67 | 71.38 | --- | Fusain-rich attritus. |
| 66 | 10 | 100.00 | --- | --- | --- | Resin bleb. |
| 66 | 20 | 50.00 | 85.00 | 74.00 | --- | --- |
| 67 | 30 | 33.33 | 33.33 | 69.13 | --- | --- |
| 68 | 20 | 50.00 | 50.00 | 69.73 | --- | --- |
| 69 | 10 | 100.00 | --- | --- | --- | --- |
| 69 | 20 | 50.00 | --- | --- | --- | --- |
| 69 | 10 | 100.00 | 83.33 | 71.43 | --- | --- |
| 70 | 5 | 200.00 | --- | --- | --- | --- |
| 70 | 10 | 100.00 | 123.08 | 72.64 | --- | Inert attritus, no true fusain. |
| ns5 | --- | --- | --- | ---- | --- | Sample removed for adsorption analysis. |
| MC-9 | 10 | 100.00 | --- | --- | --- | --- |
| MC-9 | 10 | 100.00 | --- | --- | --- | --- |
| MC-9 | 5 | 200.00 | --- | --- | --- | --- |
| ns6 | --- | --- | --- | --- | --- | No sample. |
| MC-10 | 20 | 50.00 | --- | --- | --- | Sheared, minor kaolinite. |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 71 | 1,182.50 | --- | Big George | 30.00 | --- | 0.50 | 105.14 | 10.0 | 20.0 | 5.0 |
| 71 | --- | --- | Big George | 6.00 | --- | 0.10 | 105.34 | 0.0 | 0.0 | 0.0 |
| 71 | --- | 1,184.50 | Big George | 24.00 | 60.00 | 0.40 | 106.13 | 30.0 | 30.0 | 2.0 |
| 72 | 1,184.50 | --- | Big George | 28.00 | --- | 0.45 | 107.04 | 20.0 | 2.0 | 20.0 |
| 72 | --- | --- | Big George | 6.00 | --- | 0.10 | 107.24 | 0.0 | 0.0 | 0.0 |
| 72 | --- | 1,186.50 | Big George | 28.00 | 62.00 | 0.45 | 108.16 | 10.0 | 5.0 | 15.0 |
| 73 | 1,186.50 | --- | Big George | 44.00 | --- | 0.79 | 109.60 | 10.0 | 10.0 | 20.0 |
| 73 | --- | 1,188.50 | Big George | 12.00 | 56.00 | 0.21 | 110.00 | 2.0 | 5.0 | 10.0 |
| ns7 | 1,188.50 | 1,189.50 | ns7 | 30.50 | 30.50 | 1.00 | 111.00 | --- | --- | --- |
| 74 | 1,189.50 | ---- | Big George | 17.50 | --- | 0.28 | 111.57 | 10.0 | 3.0 | 10.0 |
| 74 | --- | --- | Big George | 2.00 | --- | 0.03 | 111.64 | 0.0 | 0.0 | 0.0 |
| 74 | --- | --- | Big George | 8.00 | --- | 0.13 | 111.90 | 10.0 | 2.0 | 10.0 |
| 74 | --- | --- | Big George | 12.00 | --- | 0.20 | 112.29 | 0.0 | 0.0 | 0.0 |
| 74 | --- | --- | Big George | 9.00 | --- | 0.15 | 112.59 | 10.0 | 1.0 | 0.0 |
| 74 | --- | 1,191.50 | Big George | 13.00 | 61.50 | 0.21 | 113.02 | 0.0 | 0.0 | 0.0 |
| 75 | 1,191.50 | 1,193.50 | Big George | 40.00 | 40.00 | 1.00 | 114.33 | 10.0 | 3.0 | 30.0 |
| ns8 | 1,193.50 | 1,196.50 | ns8 | 91.00 | 91.00 | 1.00 | 117.31 | - | --- | --- |
| 76 | 1,196.50 | 1,199.00 | Big George | 64.00 | 64.00 | 1.00 | 119.41 | 60.0 | 40.0 | 0.0 |
| A1 | 1,199.00 | 1,199.50 | Big George | 15.00 | 15.00 | 0.23 | 119.90 | 10.0 | 5.0 | 20.0 |
| ns9 | 1,199.50 | 1,201.50 | ns9 | 60.00 | 60.00 | 1.00 | 121.87 | --- | --- | --- |
| A1 | 1,201.50 | 1,203.00 | Big George | 49.00 | 64.00 | 0.77 | 123.48 | 10.0 | 5.0 | 20.0 |
| MC-11 | 1,203.00 | 1,205.00 | Big George | 49.00 | 49.00 | 1.00 | 125.09 | 5.0 | 30.0 | 10.0 |
| ns10 | 1,205.00 | 1,209.00 | ns10 | 122.00 | 122.00 | 1.00 | 129.09 | --- | -- | --- |
| A2 | 1,209.00 | 1,211.00 | Big George | 59.00 | 59.00 | 1.00 | 131.03 | 40.0 | 10.0 | 30.0 |
| MC-12 | 1,211.00 | --- | Big George | 32.00 | --- | 0.62 | 132.08 | 50.0 | 0.0 | 0.0 |
| MC-12 | --- | 1,213.00 | Big George | 20.00 | 52.00 | 0.38 | 132.73 | 10.0 | 0.0 | 20.0 |
| A3 | 1,213.00 | 1,215.00 | Big George | 48.00 | 48.00 | 1.00 | 134.31 | 20.0 | 2.0 | 10.0 |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 71 | 3 | 98.33 | 196.67 | 32.78 | 65.56 | 1.67 | --- | --- | --- |
| 71 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 71 | 4 | 119.00 | 119.00 | 49.58 | 49.58 | 0.83 | 36.22 | 52.61 | 1.17 |
| 72 | 3 | 236.36 | 23.64 | 84.42 | 8.44 | 7.14 | --- | --- | --- |
| 72 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 72 | 3 | 176.67 | 88.33 | 63.10 | 31.55 | 5.36 | 66.62 | 18.06 | 5.65 |
| 73 | 3 | 210.00 | 210.00 | 47.73 | 47.73 | 4.55 | --- | --- | --- |
| 73 | 2 | 31.43 | 78.57 | 26.19 | 65.48 | 8.33 | 43.11 | 51.53 | 5.36 |
| ns7 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 74 | 3 | 126.92 | 38.08 | 72.53 | 21.76 | 5.71 | --- | --- | --- |
| 74 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 74 | 3 | 58.33 | 11.67 | 72.92 | 14.58 | 12.50 | --- | --- | --- |
| 74 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 74 | 3 | 81.82 | 8.18 | 90.91 | 9.09 | 0.00 | --- | --- | --- |
| 74 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 75 | 3 | 284.62 | 85.38 | 71.15 | 21.35 | 7.50 | 71.15 | 21.35 | 7.50 |
| ns8 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 76 | 4 | 384.00 | 256.00 | 60.00 | 40.00 | 0.00 | 60.00 | 40.00 | 0.00 |
| A1 | 3 | 86.67 | 43.33 | 57.78 | 28.89 | 13.33 | --- | --- | --- |
| ns9 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| A1 | 3 | 313.33 | 156.67 | 63.95 | 31.97 | 4.08 | 62.50 | 31.25 | 6.25 |
| MC-11 | 3 | 68.57 | 411.43 | 13.99 | 83.97 | 2.04 | --- | --- | --- |
| ns 10 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| A2 | 4 | 448.00 | 112.00 | 75.93 | 18.98 | 5.08 | 75.93 | 18.98 | 5.08 |
| MC-12 | 5 | 320.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| MC-12 | 3 | 180.00 | 0.00 | 90.00 | 0.00 | 10.00 | --- | --- | --- |
| A3 | 3 | 427.27 | 42.73 | 89.02 | 8.90 | 2.08 | 89.02 | 8.90 | 2.08 |

Table 1-2. Data for samples from core hole 2, MichiWest Energy Inc., Pilot State 16-32.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 71 | 10 | 100.00 | --- | --- | --- | Kaolinite on cleat. |
| 71 | --- | --- | --- | --- | --- | Sand dike(?), kaolinite on cleat. |
| 71 | 20 | 50.00 | 77.78 | 63.17 | --- | Slickensides below sand, no loss around sand. |
| 72 | 20 | 50.00 | --- | --- | --- | Sand at top. |
| 72 | --- | --- | --- | --- | --- | Sand dike. |
| 72 | 30 | 33.33 | 41.67 | 63.13 | --- | Sand at 16-18 cm. |
| 73 | 10 | 100.00 | --- | --- | --- | Curvilinear. |
| 73 | 40 | 25.00 | 83.93 | 75.52 | SubA | Tight. |
| ns7 | --- | --- | --- | --- | --- | No sample. |
| 74 | 20 | 50.00 | --- | --- | --- | --- |
| 74 | --- | --- | --- | --- | --- | Sand. |
| 74 | 10 | 100.00 | --- | --- | --- | --- |
| 74 | --- | --- | --- | --- | --- | Sand. |
| 74 | 10 | 100.00 | --- | --- | --- | --- |
| 74 | --- | --- | --- | --- | SubA | Sand with coal stringers at basal 9 cm . |
| 75 | 20 | 50.00 | 50.00 | 58.78 | --- | Permeable, mostly fusain and vitrain, sulfate. |
| ns8 | --- | --- | --- | --- | --- | No sample. |
| 76 | 10 | 100.00 | 100.00 | 62.67 | --- | Bedding dips 25 degrees, sand blebs at 24 cm . |
| A1 | 10 | 100.00 | --- | --- | --- | Bedding dips 25 degrees, tight cleat. |
| ns9 | --- | --- | --- | --- | --- | Sand excluded from canister. |
| A1 | 10 | 100.00 | 100.00 | 62.67 | --- | Bedding dips 25 degrees, tight cleat. |
| MC-11 | 30 | 33.33 | --- | --- | --- | --- |
| ns10 | --- | --- | --- | --- | --- | No sample. |
| A2 | 30 | 33.33 | 33.33 | 75.68 | --- | Horizontal bedding. |
| $\mathrm{MC}-12$ | 30 | 33.33 | --- | --- | --- | Kaolinite on cleat at 29-32 cm. |
| $\mathrm{MC}-12$ | 30 | 33.33 | --- | --- | --- | --- |
| A3 | 10 | 100.00 | 100.00 | 72.12 | --- | Horizontal bedding. |

Table 1-3. Data for samples from core hole 3, Ocean Energy, Inc., Schlautmann 9-10-45-74WY (Ocean 43-10C).
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Appro dep | $\begin{aligned} & \text { ximate } \\ & \text { h (ft) } \end{aligned}$ | Coal bed name | Unit <br> thickness <br> (UT) (cm) | Canister total <br> measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| 14 | 1,190.00 | --- | Anderson | 40.00 | --- | 0.69 | 1.31 | 50.0 | 0.0 |
| 14 |  | 1,192.00 | Anderson | 18.00 | 58.00 | 0.31 | 1.90 | 20.0 | 5.0 |

Table 1-3. Data for samples from core hole 3, Ocean Energy, Inc., Schlautmann 9-10-45-74WY (Ocean 43-10C).—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative <br> fusain <br> thickness <br> (CuFT) (mm) | Lithotype code | Canister number | Cumulative vitrain thickness (CuVT) (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | 0.0 | 5 | 14 | 400.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| 14 | 0.0 | 3 | 14 | 144.00 | 36.00 | 80.00 | 20.00 | 0.00 | 93.79 |

Table 1-3. Data for samples from core hole 3, Ocean Energy, Inc., Schlautmann 9-10-45-74WY (Ocean 43-10C).—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | $\begin{gathered} \text { Cleat } \\ \text { spacing } \\ \text { (CS) }(\mathrm{mm}) \end{gathered}$ | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| 14 | 6.21 | 0.00 | 20 | 50.00 | 38.51 | 27.12 | SubC | --- |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| A-7 | 343.00 | --- | Smith | 29.00 | --- | 0.47 | 0.95 | 0.0 | 50.0 | 0.0 |
| A-7 | --- | 345.00 | Smith | 33.00 | 62.00 | 0.53 | 2.03 | 20.0 | 0.0 | 80.0 |
| A-10 | 345.00 | --- | Smith | 6.00 | --- | 0.10 | 2.23 | 10.0 | 5.0 | 0.0 |
| A-10 | --- | --- | Smith | 16.00 | --- | 0.25 | 2.76 | 5.0 | 10.0 | 0.0 |
| A-10 | --- | --- | Smith | 35.00 | --- | 0.56 | 3.90 | 20.0 | 5.0 | 5.0 |
| A-10 | --- | 347.00 | Smith | 6.00 | 63.00 | 0.10 | 4.10 | 20.0 | 5.0 | 0.0 |
| A-11 | 347.00 | --- | Smith | 24.00 | --- | 0.39 | 4.89 | 2.0 | 10.0 | 0.0 |
| A-11 | --- | --- | Smith | 33.00 | --- | 0.53 | 5.97 | 50.0 | 5.0 | 0.0 |
| A-11 | --- | 349.00 | Smith | 5.00 | 62.00 | 0.08 | 6.14 | 2.0 | 5.0 | 10.0 |
| A-12 | 349.00 | 351.00 | Smith | 64.00 | 64.00 | 1.00 | 8.23 | 10.0 | 2.0 | 5.0 |
| A-13 | 351.00 | --- | Smith | 53.00 | --- | 0.87 | 9.97 | 10.0 | 2.0 | 22.0 |
| A-13 | --- | 353.00 | Smith | 8.00 | 61.00 | 0.13 | 10.24 | 5.0 | 30.0 | 0.0 |
| A-14 | 353.00 | --- | Smith | 47.00 | --- | 0.81 | 11.78 | 5.0 | 20.0 | 5.0 |
| A-14 | --- | 355.00 | Smith | 11.00 | 58.00 | 0.19 | 12.14 | 20.0 | 2.0 | 0.0 |
| A-15 | 355.00 | --- | Smith | 15.00 | --- | 0.24 | 12.63 | 50.0 | 0.0 | 0.0 |
| A-15 | --- | --- | Smith | 33.00 | --- | 0.52 | 13.71 | 3.0 | 10.0 | 25.0 |
| A-15 | --- | 357.00 | Smith | 15.00 | 63.00 | 0.24 | 14.21 | 20.0 | 1.0 | 0.0 |
| A-16 | 357.00 | --- | Smith | 11.00 | --- | 0.32 | 14.57 | 5.0 | 10.0 | 0.0 |
| A-16 | --- | --- | Smith | 11.00 | --- | 0.32 | 14.93 | 2.0 | 3.0 | 60.0 |
| A-16 | --- | 358.00 | Smith | 12.00 | 34.00 | 0.35 | 15.32 | 2.0 | 5.0 | 0.0 |
| ns1 | 358.00 | 358.50 | ns 1 | 15.00 | 15.00 | 1.00 | 15.81 | --- | --- | --- |
| A-16 | 358.50 | 359.50 | Smith | 19.00 | 19.00 | 1.00 | 16.44 | 40.0 | 10.0 | 0.0 |
| A-17 | 359.50 | --- | Smith | 49.00 | --- | 0.74 | 18.04 | 40.0 | 10.0 | 0.0 |
| A-17 | --- | 361.50 | Smith | 17.00 | 66.00 | 0.26 | 18.60 | 2.0 | 10.0 | 0.0 |
| ns2 | 361.50 | 374.00 | ns2 | 381.00 | 381.00 | 1.00 | 31.10 | --- | --- | --- |
| A-18 | 374.00 | --- | Smith | 33.00 | --- | 0.56 | 32.19 | 3.0 | 10.0 | 10.0 |
| A-18 | --- | --- | Smith | 19.00 | --- | 0.32 | 32.81 | 0.0 | 20.0 | 0.0 |
| A-18 | --- | 376.00 | Smith | 7.00 | 59.00 | 0.12 | 33.04 | 5.0 | 5.0 | 10.0 |
| A-19 | 376.00 | 378.00 | Smith | 59.00 | 59.00 | 1.00 | 34.97 | 50.0 | 0.0 | 10.0 |
| A-20 | 378.00 | --- | Smith | 34.00 | --- | 0.54 | 36.09 | 50.0 | 0.0 | 0.0 |
| A-20 | --- | --- | Smith | 12.00 | --- | 0.19 | 36.48 | 0.0 | 0.0 | 0.0 |
| A-20 | --- | --- | Smith | 9.00 | --- | 0.14 | 36.78 | 10.0 | 2.0 | 20.0 |
| A-20 | --- | 380.00 | Smith | 8.00 | 63.00 | 0.13 | 37.04 | 0.0 | 0.0 | 80.0 |
| A-23 | 380.00 | --- | Smith | 27.00 | --- | 0.44 | 37.93 | 8.0 | 10.0 | 12.0 |
| A-23 | --- | 382.00 | Smith | 35.00 | 62.00 | 0.56 | 39.07 | 50.0 | 0.0 | 0.0 |
| A-24 | 382.00 | --- | Smith | 30.00 | --- | 0.47 | 40.06 | 8.0 | 3.0 | 0.0 |
| A-24 | --- | 384.00 | Smith | 34.00 | 64.00 | 0.53 | 41.17 | 50.0 | 0.0 | 0.0 |
| A-25 | 384.00 | 386.00 | Smith | 59.00 | 59.00 | 1.00 | 43.11 | 50.0 | 0.0 | 2.0 |
| ns3 | 386.00 | 779.20 | ns3 | 11,985.00 | 11,985.00 | 1.00 | 436.32 | --- | - | --- |
| C-1 | 779.20 | --- | Anderson | 43.00 | --- | 0.68 | 437.73 | 50.0 | 10.0 | 0.0 |
| C-1 | --- | 781.20 | Anderson | 20.00 | 63.00 | 0.32 | 438.39 | 3.0 | 5.0 | 0.0 |
| C-4 | 781.20 | --- | Anderson | 7.00 | --- | 0.12 | 438.62 | 3.0 | 0.0 | 30.0 |
| C-4 | --- | --- | Anderson | 31.00 | --- | 0.52 | 439.63 | 50.0 | 20.0 | 5.0 |
| C-4 | --- | 783.20 | Anderson | 22.00 | 60.00 | 0.37 | 440.35 | 5.0 | 2.0 | 10.0 |
| C-5 | 783.20 | --- | Anderson | 24.00 | --- | 0.44 | 441.14 | 50.0 | 5.0 | 0.0 |
| C-5 | --- | 785.20 | Anderson | 30.00 | 54.00 | 0.56 | 442.13 | 3.0 | 2.0 | 10.0 |
| C-6 | 785.20 | --- | Anderson | 10.00 | --- | 0.16 | 442.45 | 50.0 | 0.0 | 0.0 |
| C-6 | --- | 787.20 | Anderson | 54.00 | 64.00 | 0.84 | 444.23 | 5.0 | 5.0 | 0.0 |
| C-7 | 787.20 | --- | Anderson | 58.00 | --- | 0.91 | 446.13 | 2.0 | 1.0 | 40.0 |
| C-7 | --- | 789.20 | Anderson | 6.00 | 64.00 | 0.09 | 446.33 | 50.0 | 0.0 | 0.0 |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain thickness (CuVT) (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) <br> (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-7 | 1 | 0.00 | 290.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| A-7 | 3 | 250.00 | 0.00 | 75.76 | 0.00 | 24.24 | 40.32 | 46.77 | 12.90 |
| A-10 | 3 | 40.00 | 20.00 | 66.67 | 33.33 | 0.00 | --- | --- | --- |
| A-10 | 3 | 53.33 | 106.67 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| A-10 | 3 | 276.00 | 69.00 | 78.86 | 19.71 | 1.43 | --- | --- |  |
| A-10 | 3 | 48.00 | 12.00 | 80.00 | 20.00 | 0.00 | 66.24 | 32.96 | 0.79 |
| A-11 | 2 | 40.00 | 200.00 | 16.67 | 83.33 | 0.00 | --- | --- | --- |
| A-11 | 4 | 300.00 | 30.00 | 90.91 | 9.09 | 0.00 | --- | --- | --- |
| A-11 | 2 | 11.43 | 28.57 | 22.86 | 57.14 | 20.00 | 56.68 | 41.71 | 1.61 |
| A-12 | 3 | 529.17 | 105.83 | 82.68 | 16.54 | 0.78 | 82.68 | 16.54 | 0.78 |
| A-13 | 3 | 423.33 | 84.67 | 79.87 | 15.97 | 4.15 | --- | --- | --- |
| A-13 | 3 | 11.43 | 68.57 | 14.29 | 85.71 | 0.00 | 71.27 | 25.12 | 3.61 |
| A-14 | 3 | 93.00 | 372.00 | 19.79 | 79.15 | 1.06 | --- | --- | --- |
| A-14 | 3 | 100.00 | 10.00 | 90.91 | 9.09 | 0.00 | 33.28 | 65.86 | 0.86 |
| A-15 | 5 | 150.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| A-15 | 2 | 70.38 | 234.62 | 21.33 | 71.10 | 7.58 | --- | --- | --- |
| A-15 |  | 142.86 | 7.14 | 95.24 | 4.76 | 0.00 | 57.66 | 38.37 | 3.97 |
| A-16 | 3 | 36.67 | 73.33 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| A-16 | 2 | 20.00 | 30.00 | 18.18 | 27.27 | 54.55 | --- | --- | --- |
| A-16 | 2 | 34.29 | 85.71 | 28.57 | 71.43 | 0.00 | 26.75 | 55.60 | 17.65 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| A-16 |  | 152.00 | 38.00 | 80.00 | 20.00 | 0.00 | 80.00 | 20.00 | 0.00 |
| A-17 | 4 | 392.00 | 98.00 | 80.00 | 20.00 | 0.00 | --- | --- | --- |
| A-17 | 2 | 28.33 | 141.67 | 16.67 | 83.33 | 0.00 | 63.69 | 36.31 | 0.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| A-18 |  | 73.85 | 246.15 | 22.38 | 74.59 | 3.03 | --- | --- | --- |
| A-18 | 1 | 0.00 | 190.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| A-18 |  | 30.00 | 30.00 | 42.86 | 42.86 | 14.29 | 17.60 | 79.01 | 3.39 |
| A-19 | 5 | 580.00 | 0.00 | 98.31 | 0.00 | 1.69 | 98.31 | 0.00 | 1.69 |
| A-20 |  | 340.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| A-20 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| A-20 | 3 | 58.33 | 11.67 | 64.81 | 12.96 | 22.22 | --- | --- | -- |
| A-20 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | 63.23 | 1.85 | 15.87 |
| A-23 |  | 114.67 | 143.33 | 42.47 | 53.09 | 4.44 | --- | --- | --- |
| A-23 | 5 | 350.00 | 0.00 | 100.00 | 0.00 | 0.00 | 74.95 | 23.12 | 1.94 |
| A-24 | 3 | 218.18 | 81.82 | 72.73 | 27.27 | 0.00 | --- | --- | --- |
| A-24 | 5 | 340.00 | 0.00 | 100.00 | 0.00 | 0.00 | 87.22 | 12.78 | 0.00 |
| A-25 | 5 | 588.00 | 0.00 | 99.66 | 0.00 | 0.34 | --- | --- | --- |
| ns3 | --- | --- | . | --- | --- | --- | --- | --- | --- |
| C-1 | 4 | 358.33 | 71.67 | 83.33 | 16.67 | 0.00 | --- | --- | --- |
| C-1 | 2 | 75.00 | 125.00 | 37.50 | 62.50 | 0.00 | 68.78 | 31.22 | 0.00 |
| C-4 | , | 40.00 | 0.00 | 57.14 | 0.00 | 42.86 | --- | ---- | ---- |
| C-4 | 4 | 217.86 | 87.14 | 70.28 | 28.11 | 1.61 | --- | --- | --- |
| C-4 | , | 150.00 | 60.00 | 68.18 | 27.27 | 4.55 | 67.98 | 24.52 | 7.50 |
| C-5 | 4 | 218.18 | 21.82 | 90.91 | 9.09 | 0.00 | --- | --- | --- |
| C-5 | , | 174.00 | 116.00 | 58.00 | 38.67 | 3.33 | 72.63 | 25.52 | 1.85 |
| C-6 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C-6 |  | 270.00 | 270.00 | 50.00 | 50.00 | 0.00 | 57.81 | 42.19 | 0.00 |
| C-7 |  | 360.00 | 180.00 | 62.07 | 31.03 | 6.90 | --- | --- | --- |
| C-7 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | 65.63 | 28.13 | 6.25 |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A-7 | 10.00 | 100.00 | --- | --- | --- | --- |
| A-7 | 10.00 | 100.00 | 100.00 | 16.99 | --- | Hard. |
| A-10 | 10.00 | 100.00 | --- | --- | --- | --- |
| A-10 | --- | --- | --- | --- | --- | --- |
| A-10 | --- | --- | --- | --- | --- | --- |
| A-10 | 10.00 | 100.00 | 100.00 | 22.28 | --- | --- |
| A-11 | 5.00 | 200.00 | --- | --- | --- | --- |
| A-11 | 10.00 | 100.00 | --- | --- | --- | --- |
| A-11 | 20.00 | 50.00 | 134.68 | 22.75 | --- | --- |
| A-12 | 30.00 | 33.33 | 33.33 | 23.52 | SubC | Hard, resin at 54 cm . |
| A-13 | --- | --- | --- | --- | --- | --- |
| A-13 | --- | --- | --- | 26.7 | --- | --- |
| A-14 | 30.00 | 33.33 | --- | --- | --- | --- |
| A-14 | 10.00 | 100.00 | 45.98 | 22.03 | --- | --- |
| A-15 | --- | --- | --- | --- | --- | --- |
| A-15 | 10.00 | 100.00 | --- | --- | --- | --- |
| A-15 | 5.00 | 200.00 | 131.25 | 19.26 | --- | --- |
| A-16 | 20.00 | 50.00 | --- | --- | --- | --- |
| A-16 | 40.00 | 25.00 | --- | --- | --- | --- |
| A-16 | 30.00 | 33.33 | 36.03 | 20.68 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | 6 inches of shale, excluded from canister A16. |
| A-16 | 20.00 | 50.00 | 50.00 | 22.35 | --- | --- |
| A-17 | 10.00 | 100.00 | --- | --- | --- | --- |
| A-17 | 30.00 | 33.33 | 82.83 | 25.51 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | No sample. |
| A-18 | 30.00 | 33.33 | --- | --- | --- | Resin at 4 cm . |
| A-18 | --- | --- | --- | --- | --- | --- |
| A-18 | 20.00 | 50.00 | 36.25 | 23.55 | --- | --- |
| A-19 | 10.00 | 100.00 | 100.00 | 22.37 | SubC | Kaolinite at $50-55 \mathrm{~cm}$. |
| A-20 | 10.00 | 100.00 | --- | --- | --- | Kaolinite at 12 cm . |
| A-20 | --- | --- | --- | --- | --- | Parting. |
| A-20 | 20.00 | 50.00 | --- | --- | --- | --- |
| A-20 | 20.00 | 50.00 | 83.33 | 24.78 | --- | Fusain layer. |
| A-23 | 20.00 | 50.00 | --- | --- | --- | --- |
| A-23 | 10.00 | 100.00 | 78.23 | 22.48 | --- | --- |
| A-24 | 5.00 | 200.00 | --- | --- | --- | --- |
| A-24 | 40.00 | 25.00 | 107.03 | 18.97 | --- | --- |
| A-25 | 50.00 | 20.00 | --- | --- | SubB | --- |
| ns3 | --- | --- | --- | --- | --- | No sample. |
| C-1 | 40.00 | 25.00 | --- | --- | --- | Kaolinite at 15-25 cm. |
| C-1 | 50.00 | 20.00 | 23.41 | 32.14 | --- | --- |
| C-4 | 50 | 20.00 | --- | --- | --- | --- |
| C-4 | 5 | 200.00 | --- | --- | --- | --- |
| C-4 | 10 | 100.00 | 142.33 | 28.73 | --- | --- |
| C-5 | 2 | 500.00 | --- | --- | --- | Highly fractured sample. |
| C-5 | 2 | 500.00 | 500.00 | 30.17 | --- | Highly fractured sample. |
| C-6 | 10 | 100.00 | --- | --- | --- | --- |
| C-6 | 5 | 200.00 | 184.38 | 28.80 | --- | --- |
| C-7 | 5 | 200.00 | --- | --- | --- | --- |
| C-7 | 10 | 100.00 | 190.63 | 32.42 | --- | Kaolinite at top. |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Appro dept | ximate <br> h (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| C-8 | 789.20 | --- | Anderson | 47.00 | --- | 0.82 | 447.87 | 10.0 | 20.0 | 25.0 |
| C-8 | --- | 791.20 | Anderson | 10.00 | 57.00 | 0.18 | 448.20 | 50.0 | 0.0 | 0.0 |
| ns4 | 791.20 | 986.00 | ns4 | 5937.50 | 5,937.50 | 1.00 | 643.00 | --- | --- | --- |
| C-9 | 986.00 | 988.00 | Canyon | 63.00 | 63.00 | 1.00 | 645.06 | 10.0 | 30.0 | 18.0 |
| C-10 | 988.00 | --- | Canyon | 50.00 | --- | 0.81 | 646.70 | 20.0 | 10.0 | 20.0 |
| C-10 | --- | 990.00 | Canyon | 12.00 | 62.00 | 0.19 | 647.10 | 10.0 | 2.0 | 0.0 |
| C-11 | 990.00 | 992.00 | Canyon | 60.00 | 60.00 | 1.00 | 649.06 | 5.0 | 2.0 | 5.0 |
| C-12 | 992.00 | 994.00 | Canyon | 56.00 | 56.00 | 1.00 | 650.90 | 10.0 | 2.0 | 10.0 |
| ns5 | 994.00 | 1,340.00 | ns5 | 10,546.00 | 10,546.00 | 1.00 | 996.90 | --- | --- | --- |
| C-13 | 1,340.00 | --- | Cook | 2.00 | --- | 0.03 | 996.97 | 0.0 | 20.0 | 0.0 |
| C-13 | --- | --- | Cook | 8.00 | --- | 0.13 | 997.23 | 0.0 | 0.0 | 0.0 |
| C-13 | --- | --- | Cook | 13.00 | --- | 0.22 | 997.65 | 5.0 | 20.0 | 0.0 |
| C-13 | --- | 1,342.00 | Cook | 37.00 | 60.00 | 0.62 | 998.87 | 5.0 | 0.0 | 0.0 |
| C-14 | 1,342.00 | --- | Cook | 14.00 | --- | 0.22 | 999.33 | 10.0 | 0.0 | 0.0 |
| C-14 | --- | --- | Cook | 42.00 | --- | 0.67 | 1,000.71 | 50.0 | 2.0 | 0.0 |
| C-14 | --- | --- | Cook | 1.00 | --- | 0.02 | 1,000.74 | 0.0 | 0.0 | 0.0 |
| C-14 | --- | 1,344.00 | Cook | 6.00 | 63.00 | 0.10 | 1,000.94 | 50.0 | 0.0 | 0.0 |
| C-15 | 1,344.00 | --- | Cook | 32.00 | --- | 0.51 | 1,001.98 | 1.0 | 0.0 | 0.0 |
| C-15 | --- | 1,346.00 | Cook | 31.00 | 63.00 | 0.49 | 1,003.00 | 5.0 | 30.0 | 0.0 |
| C-16 | 1,346.00 | --- | Cook | 22.00 | --- | 0.37 | 1,003.72 | 1.0 | 20.0 | 2.0 |
| C-16 | --- | 1,348.00 | Cook | 38.00 | 60.00 | 0.63 | 1,004.97 | 50.0 | 5.0 | 0.0 |
| C-17 | 1,348.00 | --- | Cook | 37.00 | --- | 0.61 | 1,006.18 | 20.0 | 10.0 | 5.0 |
| C-17 | --- | --- | Cook | 6.00 | --- | 0.10 | 1,006.38 | 0.0 | 0.0 | 0.0 |
| C-17 | --- | --- | Cook | 12.00 | --- | 0.20 | 1,006.77 | 2.0 | 5.0 | 5.0 |
| C-17 | --- | 1,350.00 | Cook | 6.00 | 61.00 | 0.10 | 1,006.97 | 50.0 | 0.0 | 0.0 |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-8 | 3 | 148.33 | 296.67 | 31.56 | 63.12 | 5.32 | --- | --- | --- |
| C-8 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | 43.57 | 52.05 | 4.39 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C-9 | 3 | 153.00 | 459.00 | 24.29 | 72.86 | 2.86 | 24.29 | 72.86 | 2.86 |
| C-10 | 3 | 320.00 | 160.00 | 64.00 | 32.00 | 4.00 | --- | --- | --- |
| C-10 | 3 | 100.00 | 20.00 | 83.33 | 16.67 | 0.00 | 67.74 | 29.03 | 3.23 |
| C-11 | 3 | 425.00 | 170.00 | 70.83 | 28.33 | 0.83 | 70.83 | 28.33 | 0.83 |
| C-12 | 3 | 458.33 | 91.67 | 81.85 | 16.37 | 1.79 | 81.85 | 16.37 | 1.79 |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C-13 | 1 | 0.00 | 20.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C-13 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | ---- | --- |
| C-13 | 3 | 26.00 | 104.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| C-13 | 3 | 370.00 | 0.00 | 100.00 | 0.00 | 0.00 | 66.00 | 20.67 | 0.00 |
| C-14 | 3 | 140.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C-14 | 5 | 403.85 | 16.15 | 96.15 | 3.85 | 0.00 | --- | --- | --- |
| C-14 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| C-14 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | 95.85 | 2.56 | 0.00 |
| C-15 | 2 | 320.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C-15 | 3 | 44.29 | 265.71 | 14.29 | 85.71 | 0.00 | 57.82 | 42.18 | 0.00 |
| C-16 | 2 | 10.38 | 207.62 | 4.72 | 94.37 | 0.91 | --- | --- | --- |
| C-16 | 4 | 345.45 | 34.55 | 90.91 | 9.09 | 0.00 | 59.31 | 40.36 | 0.33 |
| C-17 | 3 | 243.33 | 121.67 | 65.77 | 32.88 | 1.35 | --- | --- | --- |
| C-17 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| C-17 | 2 | 32.86 | 82.14 | 27.38 | 68.45 | 4.17 | --- | --- | --- |
| C-17 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | 55.11 | 33.41 | 1.64 |

Table 1-4. Data for samples from core hole 8, CMS Oil and Gas Company, Laramore 11-6C.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) <br> (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-8 | 10 | 100.00 | --- | --- | --- | --- |
| C-8 | 40 | 25.00 | 86.84 | 28.95 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | No sample. |
| C-9 | 20 | 50.00 | 50.00 | 37.78 | SubB | --- |
| C-10 | 5 | 200.00 | --- | --- | --- | --- |
| C-10 | 5 | 200.00 | 200.00 | 38.77 | --- | --- |
| C-11 | 5 | 200.00 | 200.00 | 36.80 | --- | Highly fractured sample. |
| C-12 | 10 | 100.00 | 100.00 | 38.46 | SubB | Pyrite at 54 cm along cleat. |
| ns5 | --- | --- | --- | --- | --- | No sample. |
| C-13 | 40 | 25.00 | --- | --- | --- | --- |
| C-13 | --- | --- | --- | --- | --- | Parting. |
| C-13 | 50 | 20.00 | --- | --- | --- | --- |
| C-13 | --- | --- | 20.67 | 51.56 | --- | --- |
| C-14 | 30 | 33.33 | --- | --- | --- | --- |
| C-14 | 20 | 50.00 | --- | --- | --- | --- |
| C-14 | --- | --- | --- | --- | --- | Parting. |
| C-14 | 20 | 50.00 | 46.24 | 60.74 | --- | Kaolinite on cleat. |
| C-15 | --- | --- | --- | --- | --- | --- |
| C-15 | 20 | 50.00 | 50.00 | 33.83 | --- | --- |
| C-16 | 30 | 33.33 | --- | --- | --- | --- |
| C-16 | 10 | 100.00 | 75.56 | 68.87 | --- | Kaolinite at 55 mm . |
| C-17 | 40 | 25.00 | --- | --- | --- | --- |
| C-17 | --- | --- | --- | --- | --- | Parting. |
| C-17 | 10 | 100.00 | --- | --- | --- | --- |
| C-17 | 10 | 100.00 | 49.55 | 61.99 | --- | --- |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | imate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| A5 | 134.00 | --- | upper Wyodak | 10.00 | --- | 0.24 | 0.33 | 1.0 |
| ns1 | --- | --- | ns 1 | 25.00 | --- | 1.00 | 1.15 | --- |
| A5 | --- | --- | upper Wyodak | 15.00 | --- | 0.37 | 1.64 | 2.0 |
| A5 | --- | 136.00 | upper Wyodak | 16.00 | 41.00 | 0.39 | 2.17 | 4.0 |
| A6 | 136.00 | --- | upper Wyodak | 7.50 | --- | 0.12 | 2.41 | 4.0 |
| A6 | --- | --- | upper Wyodak | 21.00 | --- | 0.33 | 3.10 | 2.0 |
| A6 | --- | --- | upper Wyodak | 7.00 | --- | 0.11 | 3.33 | 4.0 |
| A6 | --- | --- | upper Wyodak | 10.50 | --- | 0.16 | 3.67 | 105.0 |
| A6 | --- | --- | upper Wyodak | 6.50 | --- | 0.10 | 3.89 | 4.0 |
| A6 | --- | --- | upper Wyodak | 3.50 | --- | 0.05 | 4.00 | 1.0 |
| A6 | --- | 138.00 | upper Wyodak | 8.50 | 64.50 | 0.13 | 4.28 | 85.0 |
| A8 | 138.00 | --- | upper Wyodak | 1.50 | --- | 0.03 | 4.33 | 2.0 |
| A8 | --- | --- | upper Wyodak | 4.00 | --- | 0.07 | 4.46 | 40.0 |
| A8 | --- | --- | upper Wyodak | 4.00 | --- | 0.07 | 4.59 | 1.0 |
| A8 | --- | --- | upper Wyodak | 3.00 | --- | 0.05 | 4.69 | 2.0 |
| A8 | --- | --- | upper Wyodak | 2.00 | --- | 0.04 | 4.76 | 0.0 |
| A8 | --- | --- | upper Wyodak | 5.00 | --- | 0.09 | 4.92 | 2.0 |
| A8 | --- | --- | upper Wyodak | 6.50 | --- | 0.11 | 5.13 | 2.0 |
| A8 | --- | --- | upper Wyodak | 17.50 | --- | 0.31 | 5.71 | 1.0 |
| A8 | --- | --- | upper Wyodak | 8.00 | --- | 0.14 | 5.97 | 80.0 |
| A8 | --- | 140.00 | upper Wyodak | 5.50 | 57.00 | 0.10 | 6.15 | 2.0 |
| A9 | 140.00 | --- | upper Wyodak | 1.50 | --- | 0.03 | 6.20 | 2.0 |
| A9 | --- | --- | upper Wyodak | 9.50 | --- | 0.16 | 6.51 | 2.0 |
| A9 | --- | --- | upper Wyodak | 34.00 | --- | 0.59 | 7.63 | 1.0 |
| A9 | --- | 142.00 | upper Wyodak | 13.00 | 58.00 | 0.22 | 8.05 | 0.0 |
| A21 | 142.00 | --- | upper Wyodak | 8.00 | --- | 0.14 | 8.32 | 1.0 |
| A21 | --- | 143.00 | upper Wyodak | 6.00 | --- | 0.11 | 8.51 | 0.0 |
| ns2 | 143.00 | 145.50 | ns2 | 76.00 | 76.00 | 1.00 | 11.01 | --- |
| A21 | 145.50 | --- | upper Wyodak | 2.00 | --- | 0.04 | 11.07 | 1.0 |
| A21 | --- | --- | upper Wyodak | 17.50 | --- | 0.31 | 11.65 | 1.0 |
| A21 | --- | --- | upper Wyodak | 4.50 | --- | 0.08 | 11.79 | 0.0 |
| A21 | --- | 146.50 | upper Wyodak | 19.00 | 43.00 | 0.33 | 12.42 | 1.0 |
| ns3 | 146.50 | 150.00 | ns3 | 107.00 | 107.00 | 1.00 | 15.93 | --- |
| B1 | 150.00 | --- | middle and lower Wyodak | 9.00 | --- | 0.14 | 16.22 | 1.0 |
| B1 | --- | --- | middle and lower Wyodak | 16.00 | --- | 0.25 | 16.75 | 2.0 |
| B1 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 16.81 | 20.0 |
| B1 | --- | --- | middle and lower Wyodak | 5.50 | --- | 0.09 | 16.99 | 2.0 |
| B1 | --- | --- | middle and lower Wyodak | 8.50 | --- | 0.13 | 17.27 | 85.0 |
| B1 | --- | --- | middle and lower Wyodak | 5.00 | --- | 0.08 | 17.44 | 2.0 |
| B1 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 17.50 | 20.0 |
| B1 | --- | --- | middle and lower Wyodak | 8.50 | --- | 0.13 | 17.78 | 2.0 |
| B1 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.02 | 17.83 | 15.0 |
| B1 | --- | 152.00 | middle and lower Wyodak | 5.50 | 63.50 | 0.09 | 18.01 | 1.0 |
| B2 | 152.00 | --- | middle and lower Wyodak | 4.50 | --- | 0.08 | 18.16 | 1.0 |
| B2 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 18.19 | 10.0 |
| B2 | --- | --- | middle and lower Wyodak | 33.00 | --- | 0.56 | 19.27 | 1.0 |
| B2 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.03 | 19.32 | 15.0 |
| B2 | --- | -- | middle and lower Wyodak | 13.50 | --- | 0.23 | 19.77 | 1.0 |
| B2 | --- | 154.00 | middle and lower Wyodak | 5.00 | 58.50 | 0.09 | 19.93 | 3.0 |
| B3 | 154.00 | 156.00 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 21.93 | 1.0 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A5 | 9.0 | 0.0 | 2 | 10.00 | 90.00 | 10.00 | 90.00 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- |
| A5 | 18.0 | 0.0 | 2 | 15.00 | 135.00 | 10.00 | 90.00 | 0.00 |
| A5 | 6.0 | 0.0 | 2 | 64.00 | 96.00 | 40.00 | 60.00 | 0.00 |
| A6 | 6.0 | 0.0 | 2 | 30.00 | 45.00 | 40.00 | 60.00 | 0.00 |
| A6 | 18.0 | 0.0 | 2 | 21.00 | 189.00 | 10.00 | 90.00 | 0.00 |
| A6 | 6.0 | 0.0 | 2 | 28.00 | 42.00 | 40.00 | 60.00 | 0.00 |
| A6 | 0.0 | 0.0 | 5 | 105.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| A6 | 6.0 | 0.0 | 2 | 26.00 | 39.00 | 40.00 | 60.00 | 0.00 |
| A6 | 19.0 | 0.0 | 2 | 1.75 | 33.25 | 5.00 | 95.00 | 0.00 |
| A6 | 0.0 | 0.0 | 5 | 85.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| A8 | 3.0 | 0.0 | 2 | 6.00 | 9.00 | 40.00 | 60.00 | 0.00 |
| A8 | 0.0 | 0.0 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| A8 | 19.0 | 0.0 | 2 | 2.00 | 38.00 | 5.00 | 95.00 | 0.00 |
| A8 | 3.0 | 0.0 | 2 | 12.00 | 18.00 | 40.00 | 60.00 | 0.00 |
| A8 | 20.0 | 0.0 | 1 | 0.00 | 20.00 | 0.00 | 100.00 | 0.00 |
| A8 | 3.0 | 0.0 | 2 | 20.00 | 30.00 | 40.00 | 60.00 | 0.00 |
| A8 | 18.0 | 0.0 | 2 | 6.50 | 58.50 | 10.00 | 90.00 | 0.00 |
| A8 | 19.0 | 0.0 | 2 | 8.75 | 166.25 | 5.00 | 95.00 | 0.00 |
| A8 | 0.0 | 0.0 | 5 | 80.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| A8 | 3.0 | 0.0 | 2 | 22.00 | 33.00 | 40.00 | 60.00 | 0.00 |
| A9 | 18.0 | 0.0 | 2 | 1.50 | 13.50 | 10.00 | 90.00 | 0.00 |
| A9 | 3.0 | 0.0 | 2 | 38.00 | 57.00 | 40.00 | 60.00 | 0.00 |
| A9 | 19.0 | 0.0 | 2 | 17.00 | 323.00 | 5.00 | 95.00 | 0.00 |
| A9 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| A21 | 9.0 | 0.0 | 2 | 8.00 | 72.00 | 10.00 | 90.00 | 0.00 |
| A21 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| ns 2 | --- | --- | --- | --- | --- | --- | --- | --- |
| A21 | 9.0 | 5.0 | 2 | 1.50 | 13.50 | 7.50 | 67.50 | 25.00 |
| A21 | 19.0 | 0.0 | 2 | 8.75 | 166.25 | 5.00 | 95.00 | 0.00 |
| A21 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| A21 | 19.0 | 0.0 | 2 | 9.50 | 180.50 | 5.00 | 95.00 | 0.00 |
| ns3 | --- | --- | --- | --- |  | --- | --- | --- |
| B1 | 19.0 | 0.0 | 2 | 4.50 | 85.50 | 5.00 | 95.00 | 0.00 |
| B1 | 3.0 | 0.0 | 2 | 64.00 | 96.00 | 40.00 | 60.00 | 0.00 |
| B1 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B1 | 3.0 | 0.0 | 2 | 22.00 | 33.00 | 40.00 | 60.00 | 0.00 |
| B1 | 0.0 | 0.0 | 5 | 85.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B1 | 18.0 | 0.0 | 2 | 5.00 | 45.00 | 10.00 | 90.00 | 0.00 |
| B1 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B1 | 18.0 | 0.0 | 2 | 8.50 | 76.50 | 10.00 | 90.00 | 0.00 |
| B1 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B1 | 19.0 | 0.0 | 2 | 2.75 | 52.25 | 5.00 | 95.00 | 0.00 |
| B2 | 19.0 | 0.0 | 2 | 2.25 | 42.75 | 5.00 | 95.00 | 0.00 |
| B2 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B2 | 19.0 | 0.0 | 2 | 16.50 | 313.50 | 5.00 | 95.00 | 0.00 |
| B2 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B2 | 19.0 | 0.0 | 2 | 6.75 | 128.25 | 5.00 | 95.00 | 0.00 |
| B2 | 12.0 | 0.0 | 2 | 10.00 | 40.00 | 20.00 | 80.00 | 0.00 |
| B3 | 19.0 | 0.0 | 2 | 30.50 | 579.50 | 5.00 | 95.00 | 0.00 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A5 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | No sample. |
| A5 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| A5 | 21.71 | 78.29 | 0.00 | 60 | 16.67 | 36.99 | 3.39 | --- | --- |
| A6 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A6 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| A6 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A6 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| A6 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A6 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| A6 | 46.01 | 53.99 | 0.00 | 20 | 50.00 | 31.55 | 3.19 | -- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A8 | 34.61 | 65.39 | 0.00 | 60 | 16.67 | 19.01 | 3.12 | --- | --- |
| A9 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A9 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A9 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| A9 | 9.74 | 67.84 | 0.00 | 60 | 16.67 | 16.67 | 1.90 | SubB | Parting. |
| A21 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| A21 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | Parting. |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | No sample. |
| A21 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| A21 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| A21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | Parting. |
| A21 | 4.87 | 75.83 | 0.88 | 25 | 40.00 | 38.02 | 2.72 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | No sample. |
| B1 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B1 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B1 | 38.86 | 61.14 | 0.00 | 25 | 40.00 | 27.82 | 2.59 | --- | --- |
| B2 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B2 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B2 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B2 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B2 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B2 | 10.34 | 89.66 | 0.00 | 20 | 50.00 | 50.00 | 1.95 | --- | --- |
| B3 | 5.00 | 95.00 | 0.00 | 20 | 50.00 | 50.00 | 2.61 | --- | --- |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | imate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| B4 | 156.00 | --- | middle and lower Wyodak | 5.00 | --- | 0.08 | 22.10 | 1.0 |
| B4 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 22.13 | 10.0 |
| B4 | --- |  | middle and lower Wyodak | 2.00 | --- | 0.03 | 22.19 | 1.0 |
| B4 | --- | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 22.28 | 2.0 |
| B4 | --- | --- | middle and lower Wyodak | 21.00 | --- | 0.33 | 22.97 | 1.0 |
| B4 | --- | --- | middle and lower Wyodak | 13.50 | --- | 0.21 | 23.41 | 135.0 |
| B4 | --- | 158.00 | middle and lower Wyodak | 18.00 | 63.00 | 0.29 | 24.00 | 10.0 |
| B14 | 158.00 | --- | middle and lower Wyodak | 17.00 | --- | 0.27 | 24.56 | 1.0 |
| B14 | --- | --- | middle and lower Wyodak | 13.00 | --- | 0.20 | 24.98 | 130.0 |
| B14 | --- | --- | middle and lower Wyodak | 13.00 | --- | 0.20 | 25.41 | 1.0 |
| B14 | --- | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 25.49 | 25.0 |
| B14 | --- | 160.00 | middle and lower Wyodak | 18.00 | 63.50 | 0.28 | 26.08 | 1.0 |
| ns4 | 160.00 | 161.50 | ns4 | 46.00 | 46.00 | 1.00 | 27.59 | --- |
| B15 | 161.50 | --- | middle and lower Wyodak | 20.00 | --- | 0.38 | 28.25 | 1.0 |
| B15 | --- | --- | middle and lower Wyodak | 5.50 | --- | 0.10 | 28.43 | 55.0 |
| B15 | --- | 163.50 | middle and lower Wyodak | 27.00 | 52.50 | 0.51 | 29.31 | 3.0 |
| B16 | 163.50 | --- | middle and lower Wyodak | 40.50 | --- | 0.64 | 30.64 | 2.0 |
| B16 | --- | --- | middle and lower Wyodak | 20.50 | --- | 0.33 | 31.32 | 3.0 |
| B16 | --- | 165.50 | middle and lower Wyodak | 2.00 | 63.00 | 0.03 | 31.38 | 20.0 |
| B17 | 165.50 | --- | middle and lower Wyodak | 3.00 | --- | 0.05 | 31.48 | 3.0 |
| B17 | --- | --- | middle and lower Wyodak | 29.00 | --- | 0.48 | 32.43 | 1.0 |
| B17 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 32.50 | 20.0 |
| B17 | --- | 167.50 | middle and lower Wyodak | 26.00 | 60.00 | 0.43 | 33.35 | 3.0 |
| B18 | 167.50 | --- | middle and lower Wyodak | 32.50 | --- | 0.46 | 34.42 | 3.0 |
| B18 | --- | --- | middle and lower Wyodak | 25.00 | --- | 0.35 | 35.24 | 1.0 |
| B18 | --- | 169.50 | middle and lower Wyodak | 13.00 | 70.50 | 0.18 | 35.66 | 130.0 |
| B19 | 169.50 | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 35.74 | 25.0 |
| B19 | --- | --- | middle and lower Wyodak | 23.00 | --- | 0.37 | 36.50 | 3.0 |
| B19 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 36.53 | 0.0 |
| B19 | --- | --- | middle and lower Wyodak | 24.00 | --- | 0.39 | 37.32 | 3.0 |
| B19 | --- | --- | middle and lower Wyodak | 5.50 | --- | 0.09 | 37.50 | 55.0 |
| B19 | --- | --- | middle and lower Wyodak | 3.50 | --- | 0.06 | 37.61 | 1.0 |
| B19 | --- | 171.50 | middle and lower Wyodak | 2.50 | 62.00 | 0.04 | 37.70 | 25.0 |
| B20 | 171.50 | --- | middle and lower Wyodak | 38.00 | --- | 0.54 | 38.94 | 3.0 |
| B20 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.02 | 38.99 | 15.0 |
| B20 | --- | --- | middle and lower Wyodak | 8.50 | --- | 0.12 | 39.27 | 1.0 |
| B20 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 39.34 | 20.0 |
| B20 | --- | --- | middle and lower Wyodak | 3.50 | --- | 0.05 | 39.45 | 1.0 |
| B20 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.02 | 39.50 | 15.0 |
| B20 | --- | --- | middle and lower Wyodak | 11.50 | --- | 0.16 | 39.88 | 1.0 |
| B20 | --- | 173.50 | middle and lower Wyodak | 4.50 | 71.00 | 0.06 | 40.03 | 45.0 |
| B21 | 173.50 | --- | middle and lower Wyodak | 9.00 | --- | 0.15 | 40.32 | 90.0 |
| B21 | ---- | --- | middle and lower Wyodak | 18.00 | --- | 0.30 | 40.91 | 3.0 |
| B21 | --- | --- | middle and lower Wyodak | 5.00 | --- | 0.08 | 41.08 | 50.0 |
| B21 | --- | --- | middle and lower Wyodak | 8.00 | --- | 0.13 | 41.34 | 1.0 |
| B21 | --- | --- | middle and lower Wyodak | 7.50 | --- | 0.13 | 41.58 | 5.0 |
| B21 | --- | --- | middle and lower Wyodak | 6.50 | --- | 0.11 | 41.80 | 65.0 |
| B21 | --- | 175.50 | middle and lower Wyodak | 5.50 | 59.50 | 0.09 | 41.98 | 1.0 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B4 | 19.0 | 0.0 | 2 | 2.50 | 47.50 | 5.00 | 95.00 | 0.00 |
| B4 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B4 | 19.0 | 0.0 | 2 | 1.00 | 19.00 | 5.00 | 95.00 | 0.00 |
| B4 | 3.0 | 0.0 | 2 | 10.00 | 15.00 | 40.00 | 60.00 | 0.00 |
| B4 | 19.0 | 0.0 | 2 | 10.50 | 199.50 | 5.00 | 95.00 | 0.00 |
| B4 | 0.0 | 0.0 | 5 | 135.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B4 | 10.0 | 0.0 | 3 | 90.00 | 90.00 | 50.00 | 50.00 | 0.00 |
| B14 | 19.0 | 0.0 | 2 | 8.50 | 161.50 | 5.00 | 95.00 | 0.00 |
| B14 | 0.0 | 0.0 | 5 | 130.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B14 | 19.0 | 0.0 | 2 | 6.50 | 123.50 | 5.00 | 95.00 | 0.00 |
| B14 | 0.0 | 0.0 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B14 | 19.0 | 0.0 | 2 | 9.00 | 171.00 | 5.00 | 95.00 | 0.00 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- |
| B15 | 19.0 | 0.0 | 2 | 10.00 | 190.00 | 5.00 | 95.00 | 0.00 |
| B15 | 0.0 | 0.0 | 5 | 55.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B15 | 27.0 | 0.0 | 2 | 27.00 | 243.00 | 10.00 | 90.00 | 0.00 |
| B16 | 38.0 | 0.0 | 2 | 20.25 | 384.75 | 5.00 | 95.00 | 0.00 |
| B16 | 12.0 | 0.0 | 2 | 41.00 | 164.00 | 20.00 | 80.00 | 0.00 |
| B16 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B17 | 12.0 | 0.0 | 2 | 6.00 | 24.00 | 20.00 | 80.00 | 0.00 |
| B17 | 19.0 | 0.0 | 2 | 14.50 | 275.50 | 5.00 | 95.00 | 0.00 |
| B17 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B17 | 27.0 | 0.0 | 2 | 26.00 | 234.00 | 10.00 | 90.00 | 0.00 |
| B18 | 12.0 | 0.0 | 2 | 65.00 | 260.00 | 20.00 | 80.00 | 0.00 |
| B18 | 19.0 | 0.0 | 2 | 12.50 | 237.50 | 5.00 | 95.00 | 0.00 |
| B18 | 0.0 | 0.0 | 5 | 130.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B19 | 0.0 | 0.0 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B19 | 12.0 | 0.0 | 2 | 46.00 | 184.00 | 20.00 | 80.00 | 0.00 |
| B19 | 0.0 | 10.0 | 1 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 |
| B19 | 12.0 | 0.0 | 2 | 48.00 | 192.00 | 20.00 | 80.00 | 0.00 |
| B19 | 0.0 | 0.0 | 5 | 55.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B19 | 19.0 | 0.0 | 2 | 1.75 | 33.25 | 5.00 | 95.00 | 0.00 |
| B19 | 0.0 | 0.0 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B20 | 27.0 | 0.0 | 2 | 38.00 | 342.00 | 10.00 | 90.00 | 0.00 |
| B20 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B20 | 19.0 | 0.0 | 2 | 4.25 | 80.75 | 5.00 | 95.00 | 0.00 |
| B20 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B20 | 19.0 | 0.0 | 2 | 1.75 | 33.25 | 5.00 | 95.00 | 0.00 |
| B20 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B20 | 19.0 | 0.0 | 2 | 5.75 | 109.25 | 5.00 | 95.00 | 0.00 |
| B20 | 0.0 | 0.0 | 5 | 45.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B21 | 0.0 | 0.0 | 5 | 90.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B21 | 12.0 | 0.0 | 2 | 36.00 | 144.00 | 20.00 | 80.00 | 0.00 |
| B21 | 0.0 | 0.0 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B21 | 19.0 | 0.0 | 2 | 4.00 | 76.00 | 5.00 | 95.00 | 0.00 |
| B21 | 5.0 | 0.0 | 3 | 37.50 | 37.50 | 50.00 | 50.00 | 0.00 |
| B21 | 0.0 | 0.0 | 5 | 65.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B21 | 19.0 | 0.0 | 2 | 2.75 | 52.25 | 5.00 | 95.00 | 0.00 |

## 50 Megascopic Lithologic Studies of Coals, Wyoming and North Dakota

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | $\begin{gathered} \text { Cleat } \\ \text { spacing } \\ \text { (CS) (mm) } \end{gathered}$ | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B4 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| B4 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B4 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B4 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B4 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B4 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B4 | 41.11 | 58.89 | 0.00 | 20 | 50.00 | 45.77 | 2.92 | --- | --- |
| B14 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B14 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B14 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| B14 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| B14 | 28.19 | 71.81 | 0.00 | 30 | 33.33 | 25.46 | 3.39 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | No sample. |
| B15 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B15 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B15 | 17.52 | 82.48 | 0.00 | 25 | 40.00 | 41.37 | 4.79 | --- | --- |
| B16 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B16 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B16 | 12.90 | 87.10 | 0.00 | 60 | 16.67 | 38.10 | 3.38 | --- | --- |
| B17 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B17 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B17 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B17 | 11.08 | 88.92 | 0.00 | 25 | 40.00 | 38.83 | 3.52 | SubC | --- |
| B18 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B18 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B18 | 29.43 | 70.57 | 0.00 | 25 | 40.00 | 40.00 | 2.92 | --- | --- |
| B19 | --- | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| B19 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B19 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B19 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B19 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B19 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B19 | 32.38 | 66.01 | 1.61 | 60 | 16.67 | 29.97 | 2.21 | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B20 | 20.39 | 79.61 | 0.00 | 60 | 16.67 | 16.67 | 3.18 | --- | --- |
| B21 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B21 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B21 | 47.94 | 52.06 | 0.00 | 60 | 16.67 | 31.79 | 2.53 | --- | --- |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| B23 | 175.50 | --- | middle and lower Wyodak | 6.50 | --- | 0.14 | 42.19 | 1.0 |
| B23 | --- | --- | middle and lower Wyodak | 21.50 | --- | 0.46 | 42.90 | 2.0 |
| B23 | --- | --- | middle and lower Wyodak | 4.00 | --- | 0.09 | 43.03 | 40.0 |
| B23 | --- | --- | middle and lower Wyodak | 11.00 | --- | 0.23 | 43.39 | 2.0 |
| B23 | --- | 177.50 | middle and lower Wyodak | 4.00 | 47.00 | 0.09 | 43.52 | 4.0 |
| B24 | 177.50 | --- | middle and lower Wyodak | 21.50 | --- | 0.33 | 44.23 | 1.0 |
| B24 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.02 | 44.27 | 15.0 |
| B24 | --- | --- | middle and lower Wyodak | 3.00 | --- | 0.05 | 44.37 | 1.0 |
| B24 | --- | --- | middle and lower Wyodak | 3.00 | --- | 0.05 | 44.47 | 30.0 |
| B24 | --- | --- | middle and lower Wyodak | 3.00 | --- | 0.05 | 44.57 | 1.0 |
| B24 | --- | --- | middle and lower Wyodak | 5.00 | --- | 0.08 | 44.73 | 50.0 |
| B24 | --- | --- | middle and lower Wyodak | 5.50 | --- | 0.08 | 44.91 | 5.0 |
| B24 | --- | --- | middle and lower Wyodak | 10.50 | --- | 0.16 | 45.26 | 1.0 |
| B24 | --- | 179.50 | middle and lower Wyodak | 12.00 | 65.00 | 0.18 | 45.65 | 5.0 |
| C2 | 179.50 | --- | middle and lower Wyodak | 1.50 | --- | 0.03 | 45.70 | 1.0 |
| C2 | --- | --- | middle and lower Wyodak | 8.00 | --- | 0.13 | 45.96 | 2.0 |
| C2 | --- | 181.50 | middle and lower Wyodak | 50.50 | 60.00 | 0.84 | 47.62 | 1.0 |
| C18 | 181.50 | --- | middle and lower Wyodak | 3.50 | --- | 0.07 | 47.74 | 1.0 |
| C18 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 47.77 | 10.0 |
| C18 | --- | --- | middle and lower Wyodak | 19.00 | --- | 0.36 | 48.39 | 1.0 |
| C18 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 48.43 | 10.0 |
| C18 | --- | 183.50 | middle and lower Wyodak | 29.00 | 53.50 | 0.54 | 49.38 | 3.0 |
| B22 | 183.50 | --- | middle and lower Wyodak | 6.50 | --- | 0.10 | 49.59 | 1.0 |
| B22 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 49.66 | 20.0 |
| B22 | --- | --- | middle and lower Wyodak | 22.50 | --- | 0.35 | 50.39 | 1.0 |
| B22 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 50.43 | 10.0 |
| B22 | --- | --- | middle and lower Wyodak | 14.00 | --- | 0.22 | 50.89 | 1.0 |
| B22 | --- | --- | middle and lower Wyodak | 9.00 | --- | 0.14 | 51.18 | 90.0 |
| B22 | --- | 185.50 | middle and lower Wyodak | 9.50 | 64.50 | 0.15 | 51.49 | 1.0 |
| C19 | 185.50 | 187.50 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 53.26 | 1.0 |
| ns5 | 187.50 | 188.50 | ns5 | 30.50 | 30.50 | 1.00 | 54.27 | --- |
| C20 | 188.50 | --- | middle and lower Wyodak | 56.00 | --- | 0.93 | 56.10 | 1.0 |
| C20 | --- | --- | middle and lower Wyodak | 1.50 | --- | 0.03 | 56.15 | 15.0 |
| C20 | --- | 190.50 | middle and lower Wyodak | 2.50 | 60.00 | 0.04 | 56.23 | 1.0 |
| C21 | 190.50 | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 56.32 | 1.0 |
| C21 | --- | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 56.40 | 5.0 |
| C21 | --- | --- | middle and lower Wyodak | 47.00 | --- | 0.80 | 57.94 | 1.0 |
| C21 | --- | 192.50 | middle and lower Wyodak | 6.50 | 58.50 | 0.11 | 58.15 | 3.0 |
| C22 | 192.50 | --- | middle and lower Wyodak | 25.50 | --- | 0.41 | 58.99 | 1.0 |
| C22 | --- | --- | middle and lower Wyodak | 4.00 | --- | 0.07 | 59.12 | 10.0 |
| C22 | --- | --- | middle and lower Wyodak | 5.50 | --- | 0.09 | 59.30 | 0.0 |
| C22 | --- | 194.50 | middle and lower Wyodak | 26.50 | 61.50 | 0.43 | 60.17 | 3.0 |
| C23 | 194.50 | --- | middle and lower Wyodak | 8.00 | --- | 0.14 | 60.43 | 1.0 |
| C23 | --- | --- | middle and lower Wyodak | 13.00 | --- | 0.23 | 60.86 | 3.0 |
| C23 | --- | --- | middle and lower Wyodak | 12.00 | --- | 0.21 | 61.25 | 1.0 |
| C23 | --- | 196.50 | middle and lower Wyodak | 24.00 | 57.00 | 0.42 | 62.04 | 2.0 |
| C24 | 196.50 | --- | middle and lower Wyodak | 12.00 | --- | 0.28 | 62.43 | 1.0 |
| C24 | --- | --- | middle and lower Wyodak | 5.00 | --- | 0.12 | 62.60 | 50.0 |
| C24 | --- | --- | middle and lower Wyodak | 15.00 | --- | 0.35 | 63.09 | 1.0 |
| C24 | --- | 198.50 | middle and lower Wyodak | 11.00 | 43.00 | 0.26 | 63.45 | 5.0 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B23 | 19.0 | 0.0 | 2 | 3.25 | 61.75 | 5.00 | 95.00 | 0.00 |
| B23 | 8.0 | 0.0 | 2 | 43.00 | 172.00 | 20.00 | 80.00 | 0.00 |
| B23 | 0.0 | 0.0 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B23 | 3.0 | 1.0 | 2 | 43.60 | 65.40 | 39.64 | 59.45 | 0.91 |
| B23 | 4.0 | 0.0 | 2 | 20.00 | 20.00 | 50.00 | 50.00 | 0.00 |
| B24 | 19.0 | 1.0 | 2 | 10.70 | 203.30 | 4.98 | 94.56 | 0.47 |
| B24 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B24 | 19.0 | 0.0 | 2 | 1.50 | 28.50 | 5.00 | 95.00 | 0.00 |
| B24 | 0.0 | 0.0 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B24 | 19.0 | 0.0 | 2 | 1.50 | 28.50 | 5.00 | 95.00 | 0.00 |
| B24 | 0.0 | 0.0 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B24 | 5.0 | 0.0 | 3 | 27.50 | 27.50 | 50.00 | 50.00 | 0.00 |
| B24 | 19.0 | 0.0 | 2 | 5.25 | 99.75 | 5.00 | 95.00 | 0.00 |
| B24 | 5.0 | 0.0 | 3 | 60.00 | 60.00 | 50.00 | 50.00 | 0.00 |
| C2 | 19.0 | 0.0 | 2 | 0.75 | 14.25 | 5.00 | 95.00 | 0.00 |
| C2 | 2.0 | 0.0 | 2 | 40.00 | 40.00 | 50.00 | 50.00 | 0.00 |
| C2 | 19.0 | 0.0 | 2 | 25.25 | 479.75 | 5.00 | 95.00 | 0.00 |
| C18 | 19.0 | 0.0 | 2 | 1.75 | 33.25 | 5.00 | 95.00 | 0.00 |
| C18 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C18 | 19.0 | 0.0 | 2 | 9.50 | 180.50 | 5.00 | 95.00 | 0.00 |
| C18 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C18 | 17.0 | 0.0 | 2 | 43.50 | 246.50 | 15.00 | 85.00 | 0.00 |
| B22 | 19.0 | 0.0 | 2 | 3.25 | 61.75 | 5.00 | 95.00 | 0.00 |
| B22 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B22 | 19.0 | 0.0 | 2 | 11.25 | 213.75 | 5.00 | 95.00 | 0.00 |
| B22 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B22 | 19.0 | 0.0 | 2 | 7.00 | 133.00 | 5.00 | 95.00 | 0.00 |
| B22 | 0.0 | 0.0 | 5 | 90.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| B22 | 19.0 | 0.0 | 2 | 4.75 | 90.25 | 5.00 | 95.00 | 0.00 |
| C19 | 9.0 | 0.0 | 2 | 54.00 | 486.00 | 10.00 | 90.00 | 0.00 |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- |
| C20 | 19.0 | 0.0 | 2 | 28.00 | 532.00 | 5.00 | 95.00 | 0.00 |
| C20 | 0.0 | 0.0 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C20 | 19.0 | 0.0 | 2 | 1.25 | 23.75 | 5.00 | 95.00 | 0.00 |
| C21 | 19.0 | 0.0 | 2 | 1.25 | 23.75 | 5.00 | 95.00 | 0.00 |
| C21 | 5.0 | 0.0 | 3 | 12.50 | 12.50 | 50.00 | 50.00 | 0.00 |
| C21 | 19.0 | 0.0 | 2 | 23.50 | 446.50 | 5.00 | 95.00 | 0.00 |
| C21 | 12.0 | 0.0 | 2 | 13.00 | 52.00 | 20.00 | 80.00 | 0.00 |
| C22 | 19.0 | 0.0 | 2 | 12.75 | 242.25 | 5.00 | 95.00 | 0.00 |
| C22 | 6.7 | 0.0 | 3 | 24.00 | 16.00 | 60.00 | 40.00 | 0.00 |
| C22 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| C22 | 7.0 | 0.0 | 2 | 79.50 | 185.50 | 30.00 | 70.00 | 0.00 |
| C23 | 19.0 | 0.0 | 2 | 4.00 | 76.00 | 5.00 | 95.00 | 0.00 |
| C23 | 3.0 | 0.0 | 2 | 65.00 | 65.00 | 50.00 | 50.00 | 0.00 |
| C23 | 19.0 | 0.0 | 2 | 6.00 | 114.00 | 5.00 | 95.00 | 0.00 |
| C23 | 3.0 | 0.0 | 2 | 96.00 | 144.00 | 40.00 | 60.00 | 0.00 |
| C24 | 9.0 | 0.0 | 2 | 12.00 | 108.00 | 10.00 | 90.00 | 0.00 |
| C24 | 0.0 | 0.0 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C24 | 19.0 | 0.0 | 2 | 7.50 | 142.50 | 5.00 | 95.00 | 0.00 |
| C24 | 7.5 | 0.0 | 3 | 44.00 | 66.00 | 40.00 | 60.00 | 0.00 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas <br> (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B23 | 31.88 | 67.90 | 0.21 | 60 | 16.67 | 16.67 | 3.75 | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B24 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| B24 | 30.99 | 68.85 | 0.15 | 60 | 16.67 | 19.36 | 1.89 | --- | --- |
| C2 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C2 | -- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C2 | 11.00 | 89.00 | 0.00 | 60 | 16.67 | 16.67 | 1.59 | --- | --- |
| C18 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C18 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C18 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C18 | --- | --- | --- | 60 | 16.67 | --- | -- | --- | --- |
| C18 | 13.97 | 86.03 | 0.00 | 60 | 16.67 | 16.67 | 1.24 | --- | --- |
| B22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B22 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B22 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| B22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| B22 | 22.67 | 77.33 | 0.00 | 60 | 16.67 | 28.81 | 2.61 | --- | --- |
| C19 | 10.00 | 90.00 | 0.00 | 60 | 16.67 | 16.67 | 2.23 | --- | --- |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- | No sample. |
| C20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C20 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C20 | 7.38 | 92.63 | 0.00 | 60 | 16.67 | 16.67 | 2.78 | --- | --- |
| C21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C21 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C21 | 8.59 | 91.41 | 0.00 | 60 | 16.67 | 16.67 | 2.44 | --- | --- |
| C22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C22 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | Parting. |
| C22 | 18.90 | 72.15 | 0.00 | 15 | 66.67 | 38.21 | 2.15 | SubB | --- |
| C23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C23 | --- | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| C23 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C23 | 30.00 | 70.00 | 0.00 | 20 | 50.00 | 34.50 | 1.34 | --- | --- |
| C24 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| C24 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| C24 | --- | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| C24 | 26.40 | 73.60 | 0.00 | 20 | 50.00 | 50.00 | 1.48 | --- | --- |

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Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | imate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| C25 | 198.50 | --- | middle and lower Wyodak | 7.50 | --- | 0.14 | 63.70 | 3.0 |
| C25 | --- | --- | middle and lower Wyodak | 4.50 | --- | 0.08 | 63.85 | 45.0 |
| C25 | --- | --- | middle and lower Wyodak | 20.00 | --- | 0.36 | 64.50 | 2.0 |
| C25 | --- | --- | middle and lower Wyodak | 13.00 | --- | 0.24 | 64.93 | 5.0 |
| C25 | --- | --- | middle and lower Wyodak | 7.00 | --- | 0.13 | 65.16 | 70.0 |
| C25 | --- | 200.50 | middle and lower Wyodak | 3.00 | 55.00 | 0.05 | 65.26 | 5.0 |
| C26 | 200.50 | --- | middle and lower Wyodak | 46.00 | --- | 0.78 | 66.77 | 2.0 |
| C26 | --- | 202.50 | middle and lower Wyodak | 13.00 | 59.00 | 0.22 | 67.19 | 130.0 |
| C27 | 202.50 | --- | middle and lower Wyodak | 2.50 | --- | 0.04 | 67.27 | 25.0 |
| C27 | --- | --- | middle and lower Wyodak | 18.50 | --- | 0.30 | 67.88 | 3.0 |
| C27 | --- | --- | middle and lower Wyodak | 2.00 | --- | 0.03 | 67.95 | 20.0 |
| C27 | --- | --- | middle and lower Wyodak | 14.00 | --- | 0.23 | 68.41 | 1.0 |
| C27 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 68.44 | 10.0 |
| C27 | --- | 204.50 | middle and lower Wyodak | 23.00 | 61.00 | 0.38 | 69.19 | 3.0 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C25 | 4.5 | 0.0 | 2 | 30.00 | 45.00 | 40.00 | 60.00 | 0.00 |
| C25 | 0.0 | 0.0 | 5 | 45.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C25 | 8.0 | 0.0 | 2 | 40.00 | 160.00 | 20.00 | 80.00 | 0.00 |
| C25 | 11.7 | 0.0 | 3 | 39.00 | 91.00 | 30.00 | 70.00 | 0.00 |
| C25 | 0.0 | 0.0 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C25 | 11.7 | 0.0 | 3 | 9.00 | 21.00 | 30.00 | 70.00 | 0.00 |
| C26 | 18.0 | 0.0 | 2 | 46.00 | 414.00 | 10.00 | 90.00 | 0.00 |
| C26 | 0.0 | 0.0 | 5 | 130.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C27 | 0.0 | 0.0 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C27 | 12.0 | 0.0 | 2 | 37.00 | 148.00 | 20.00 | 80.00 | 0.00 |
| C27 | 0.0 | 0.0 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C27 | 19.0 | 0.0 | 2 | 7.00 | 133.00 | 5.00 | 95.00 | 0.00 |
| C27 | 0.0 | 0.0 | 3 | 10.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| C 27 | 27.0 | 0.0 | 2 | 23.00 | 207.00 | 10.00 | 90.00 | 0.00 |

Table 1-5. Data for samples from core hole 9, Kennecott Energy, Kennecott CBM-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C25 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C25 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C25 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C25 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C25 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C25 | 42.36 | 57.64 | 0.00 | 60 | 16.67 | 16.67 | 1.72 | --- | --- |
| C26 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C26 | 29.83 | 70.17 | 0.00 | 60 | 16.67 | 16.67 | 1.52 | --- | --- |
| C27 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C27 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C27 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C27 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C27 | --- | --- | --- | 60 | 16.67 | --- | --- | --- | --- |
| C27 | 20.00 | 80.00 | 0.00 | 60 | 16.67 | 16.67 | 1.70 | --- | --- |

Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Appro dep | ximate <br> th (ft) | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` |  | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 10 | 165.00 | --- | upper Wyodak | 33.00 | --- | 0.49 | 1.08 | 50.0 | 0.0 | 0.0 |
| 10 | --- | --- | upper Wyodak | 1.00 | --- | 0.01 | 1.12 | 0.0 | 0.0 | 10.0 |
| 10 | --- | --- | upper Wyodak | 33.50 | --- | 0.49 | 2.21 | 50.0 | 0.0 | 0.0 |
| 10 | --- | 167.00 | upper Wyodak | 0.50 | 68.00 | 0.01 | 2.23 | 0.0 | 0.0 | 5.0 |
| 22 | 167.00 | --- | upper Wyodak | 46.00 | --- | 0.68 | 3.74 | 50.0 | 0.0 | 0.0 |
| 22 | --- | --- | upper Wyodak | 17.00 | --- | 0.25 | 4.30 | 4.0 | 15.0 | 0.0 |
| 22 | --- | 169.00 | upper Wyodak | 5.00 | 68.00 | 0.07 | 4.46 | 0.0 | 2.0 | 0.0 |
| ns1 | 169.00 | 180.50 | ns 1 | 350.50 | 350.50 | 1.00 | 15.96 | --- | --- | --- |
| 23 | 180.50 | 182.50 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 18.03 | 50.0 | 0.0 | 10.0 |
| 24 | 182.50 | --- | middle and lower Wyodak | 19.00 | --- | 0.31 | 18.65 | 50.0 | 0.0 | 20.0 |
| 24 | --- | 184.50 | middle and lower Wyodak | 43.00 | 62.00 | 0.69 | 20.06 | 40.0 | 50.0 | 10.0 |
| 29 | 184.50 | 186.50 | middle and lower Wyodak | 65.50 | 65.50 | 1.00 | 22.21 | 40.0 | 50.0 | 10.0 |
| 31 | 186.50 | 188.50 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 24.28 | 10.0 | 40.0 | 5.0 |
| 33 | 188.50 | --- | middle and lower Wyodak | 32.00 | --- | 0.52 | 25.33 | 10.0 | 40.0 | 5.0 |
| 33 | --- | 190.50 | middle and lower Wyodak | 30.00 | 62.00 | 0.48 | 26.31 | 30.0 | 0.0 | 5.0 |
| ns2 | 190.50 | 191.50 | ns2 | 30.50 | 30.50 | 1.00 | 27.31 | --- | --- | --- |
| 34 | 191.50 | --- | middle and lower Wyodak | 8.00 | --- | 0.14 | 27.58 | 30.0 | 0.0 | 2.0 |
| 34 | --- | 193.50 | middle and lower Wyodak | 50.00 | 58.00 | 0.86 | 29.22 | 50.0 | 0.0 | 2.0 |
| 35 | 193.50 | 195.50 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 31.28 | 40.0 | 10.0 | 2.0 |
| 36 | 195.50 | 197.50 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 33.28 | 50.0 | 40.0 | 5.0 |
| 37 | 197.50 | --- | middle and lower Wyodak | 37.00 | --- | 0.64 | 34.50 | 2.0 | 100.0 | 0.0 |
| 37 | --- | 199.50 | middle and lower Wyodak | 21.00 | 58.00 | 0.36 | 35.19 | 20.0 | 20.0 | 0.0 |
| 41 | 199.50 | --- | middle and lower Wyodak | 26.00 | --- | 0.43 | 36.04 | 10.0 | 40.0 | 2.0 |
| 41 | --- | 201.46 | middle and lower Wyodak | 34.00 | 60.00 | 0.57 | 37.16 | 50.0 | 0.0 | 0.0 |
| 41-nr | 201.46 | 201.50 | middle and lower Wyodak | 7.00 | 7.00 | 1.00 | 37.39 | --- | --- | --- |
| 43 | 201.50 | 203.50 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 39.45 | 40.0 | 40.0 | 4.0 |
| 44 | 203.50 | --- | middle and lower Wyodak | 13.00 | --- | 0.22 | 39.88 | 2.0 | 20.0 | 0.0 |
| 44 | --- | --- | middle and lower Wyodak | 10.00 | --- | 0.17 | 40.21 | 2.0 | 30.0 | 0.0 |
| 44 | --- | 205.50 | middle and lower Wyodak | 36.00 | 59.00 | 0.61 | 41.39 | 2.0 | 30.0 | 5.0 |
| ns3 | 205.50 | 206.50 | ns3 | 30.50 | 30.50 | 1.00 | 42.39 | --- | --- | --- |
| 45 | 206.50 | --- | middle and lower Wyodak | 33.00 | --- | 0.52 | 43.47 | 40.0 | 0.0 | 10.0 |
| 45 | --- | 208.50 | middle and lower Wyodak | 30.00 | 63.00 | 0.48 | 44.46 | 3.0 | 40.0 | 0.0 |
| 46 | 208.50 | 210.50 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 46.42 | 5.0 | 0.0 | 200.0 |
| 48 | 210.50 | --- | middle and lower Wyodak | 8.00 | --- | 0.13 | 46.69 | 5.0 | 0.0 | 20.0 |
| 48 | --- | 212.50 | middle and lower Wyodak | 56.00 | 64.00 | 0.88 | 48.52 | 2.0 | 40.0 | 20.0 |
| 49 | 212.50 | --- | middle and lower Wyodak | 60.00 | --- | 0.87 | 50.49 | 5.0 | 30.0 | 20.0 |
| 49 | --- | 214.50 | middle and lower Wyodak | 9.00 | 69.00 | 0.13 | 50.79 | 1.0 | 3.0 | 0.0 |
| 54 | 214.50 | --- | middle and lower Wyodak | 14.00 | --- | 0.21 | 51.25 | 20.0 | 0.0 | 2.0 |
| 54 | --- | 216.50 | middle and lower Wyodak | 52.00 | 66.00 | 0.79 | 52.95 | 2.0 | 40.0 | 5.0 |
| 56 | 216.50 | --- | middle and lower Wyodak | 9.00 | --- | 0.13 | 53.25 | 2.0 | 40.0 | 0.0 |
| 56 | --- | 218.50 | middle and lower Wyodak | 58.00 | 67.00 | 0.87 | 55.15 | 40.0 | 40.0 | 0.0 |
| 57 | 218.50 | --- | middle and lower Wyodak | 18.00 | --- | 0.45 | 55.74 | 20.0 | 60.0 | 0.0 |
| 57 | --- | 219.80 | middle and lower Wyodak | 22.00 | 40.00 | 0.55 | 56.46 | 5.0 | 0.0 | 50.0 |
| 57-nr | 219.80 | 220.50 | middle and lower Wyodak | 20.00 | 20.00 | 1.00 | 57.12 | --- | --- | --- |
| ns4 | 220.50 | 221.50 | ns4 | 30.50 | 30.50 | 1.00 | 58.12 | --- | --- | --- |
| 58 | 221.50 | --- | middle and lower Wyodak | 30.00 | --- | 0.53 | 59.10 | 2.0 | 6.0 | 250.0 |
| 58 | --- | 223.50 | middle and lower Wyodak | 27.00 | 57.00 | 0.47 | 59.99 | 40.0 | 20.0 | 15.0 |
| 59 | 223.50 | --- | middle and lower Wyodak | 6.00 | --- | 0.09 | 60.19 | 35.0 | 15.0 | 10.0 |
| 59 | --- | --- | middle and lower Wyodak | 34.00 | --- | 0.52 | 61.30 | 2.0 | 2.0 | 10.0 |
| 59 | --- | --- | middle and lower Wyodak | 23.00 | --- | 0.35 | 62.06 | 1.0 | 40.0 | 5.0 |
| 59 | --- | 225.50 | middle and lower Wyodak | 2.00 | 65.00 | 0.03 | 62.12 | 2.0 | 2.0 | 5.0 |

Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) <br> (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| 10 | 5 | 330.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- | 50 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- | --- | --- |
| 10 | 5 | 335.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- | 50 |
| 10 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | 97.79 | 0.00 | 2.21 | --- |
| 22 | 5 | 460.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- | 50 |
| 22 | 2 | 35.79 | 134.21 | 21.05 | 78.95 | 0.00 | --- | --- | --- | 50 |
| 22 | 1 | 0.00 | 50.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- | 50 |
| ns 1 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 23 | 5 | 620.00 | 0.00 | 98.41 | 0.00 | 1.59 | 98.41 | 0.00 | 1.59 | 20 |
| 24 | 5 | 170.00 | 0.00 | 89.47 | 0.00 | 10.53 | --- | --- | --- | 30 |
| 24 | 4 | 186.67 | 233.33 | 43.41 | 54.26 | 2.33 | 57.53 | 37.63 | 4.84 | 30 |
| 29 | 4 | 286.67 | 358.33 | 43.77 | 54.71 | 1.53 | 43.77 | 54.71 | 1.53 | 10 |
| 31 | 3 | 125.00 | 500.00 | 19.84 | 79.37 | 0.79 | 19.84 | 79.37 | 0.79 | 10 |
| 33 | 3 | 63.00 | 252.00 | 19.69 | 78.75 | 1.56 | --- | --- | --- | 10 |
| 33 | 5 | 295.00 | 0.00 | 98.33 | 0.00 | 1.67 | 57.74 | 40.65 | 1.61 | 10 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 34 | 5 | 78.00 | 0.00 | 97.50 | 0.00 | 2.50 | --- | --- | --- | 50 |
| 34 | 5 | 498.00 | 0.00 | 99.60 | 0.00 | 0.40 | 99.31 | 0.00 | 0.69 | 5 |
| 35 | 4 | 502.40 | 125.60 | 79.75 | 19.94 | 0.32 | 79.75 | 19.94 | 0.32 | 30 |
| 36 | 4 | 336.11 | 268.89 | 55.10 | 44.08 | 0.82 | 55.10 | 44.08 | 0.82 | 50 |
| 37 | 1 | 7.25 | 362.75 | 1.96 | 98.04 | 0.00 | --- | --- | --- | 50 |
| 37 | 3 | 105.00 | 105.00 | 50.00 | 50.00 | 0.00 | 19.35 | 80.65 | 0.00 | 30 |
| 41 | 3 | 51.60 | 206.40 | 19.85 | 79.38 | 0.77 | --- | --- | --- | 30 |
| 41 | 5 | 340.00 | 0.00 | 100.00 | 0.00 | 0.00 | 65.27 | 34.40 | 0.33 | 50 |
| 41-nr | --- | --- | --- | --- | --- | --- | --- | --- | --- | 50 |
| 43 | 4 | 313.00 | 313.00 | 49.68 | 49.68 | 0.63 | 49.68 | 49.68 | 0.63 | 50 |
| 44 | 2 | 11.82 | 118.18 | 9.09 | 90.91 | 0.00 | --- | --- | --- | 50 |
| 44 | 1 | 6.25 | 93.75 | 6.25 | 93.75 | 0.00 | --- | --- | --- | 5 |
| 44 | 1 | 22.19 | 332.81 | 6.16 | 92.45 | 1.39 | 6.82 | 92.33 | 0.85 | 50 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 45 | 5 | 320.00 | 0.00 | 96.97 | 0.00 | 3.03 | --- | --- | --- | 5 |
| 45 | 1 | 20.93 | 279.07 | 6.98 | 93.02 | 0.00 | 54.12 | 44.30 | 1.59 | 20 |
| 46 | 3 | 400.00 | 0.00 | 66.67 | 0.00 | 33.33 | 66.67 | 0.00 | 33.33 | 50 |
| 48 | 3 | 60.00 | 0.00 | 75.00 | 0.00 | 25.00 | --- | --- | --- | 50 |
| 48 | 1 | 25.71 | 514.29 | 4.59 | 91.84 | 3.57 | 13.39 | 80.36 | 6.25 | 50 |
| 49 | 3 | 82.86 | 497.14 | 13.81 | 82.86 | 3.33 | --- | --- | --- | 30 |
| 49 | 2 | 22.50 | 67.50 | 25.00 | 75.00 | 0.00 | 15.27 | 81.83 | 2.90 | 50 |
| 54 | 3 | 138.00 | 0.00 | 98.57 | 0.00 | 1.43 | -- | --- | --- | 30 |
| 54 | 1 | 24.52 | 490.48 | 4.72 | 94.32 | 0.96 | 24.62 | 74.31 | 1.06 | 20 |
| 56 | 1 | 4.29 | 85.71 | 4.76 | 95.24 | 0.00 | --- | --- | --- | 30 |
| 56 | 4 | 290.00 | 290.00 | 50.00 | 50.00 | 0.00 | 43.92 | 56.08 | 0.00 | 10 |
| 57 | 3 | 45.00 | 135.00 | 25.00 | 75.00 | 0.00 | --- | --- | --- | 10 |
| 57 | 3 | 170.00 | 0.00 | 77.27 | 0.00 | 22.73 | 53.75 | 33.75 | 12.50 | 5 |
| 57-nr | --- | --- | --- | --- | --- | --- | --- | --- | --- | 2 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 58 | 2 | 12.50 | 37.50 | 4.17 | 12.50 | 83.33 | -- | - | --- | 10 |
| 58 | 4 | 170.00 | 85.00 | 62.96 | 31.48 | 5.56 | 32.02 | 21.49 | 46.49 | 20 |
| 59 | 4 | 35.00 | 15.00 | 58.33 | 25.00 | 16.67 | --- | --- | --- | 20 |
| 59 | 2 | 165.00 | 165.00 | 48.53 | 48.53 | 2.94 | --- | --- | --- | 30 |
| 59 | 1 | 5.49 | 219.51 | 2.39 | 95.44 | 2.17 | --- | --- | --- | 20 |
| 59 | 2 | 7.50 | 7.50 | 37.50 | 37.50 | 25.00 | 32.77 | 62.62 | 4.62 | 20 |

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Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]


| 10 | 20.00 | --- | --- --- | Hard, solid. |
| :---: | :---: | :---: | :---: | :---: |
| 10 | --- | --- | --- --- | Hard, solid. |
| 10 | 20.00 | --- | --- | Hard, solid. |
| 10 | --- | 20.00 | 3.62 SubC | Hard, solid. |
| 22 | 20.00 | --- | --- --- | Hard, solid. |
| 22 | 20.00 | --- | --- | Hard, solid. |
| 22 | 20.00 | --- | --- --- | Hard, solid. |
| ns 1 | --- | --- | --- --- | No sample. |
| 23 | 50.00 | 50.00 | 3.61 --- | --- |
| 24 | 33.33 | --- | -- | Clay blebs at base. |
| 24 | 33.33 | 33.33 | 3.30 SubC | --- |
| 29 | 100.00 | 100.00 | 3.74 --- | --- |
| 31 | 100.00 | 100.00 | 3.02 --- | --- |
| 33 | 100.00 | --- | --- --- | --- |
| 33 | 100.00 | 100.00 | 1.23 SubC | --- |
| ns2 | -- | --- | --- | No sample. |
| 34 | 20.00 | --- | --- --- |  |
| 34 | 200.00 | 175.17 | 0.83 --- | --- |
| 35 | 33.33 | 33.33 | 1.64 --- | --- |
| 36 | 20.00 | 20.00 | 1.12 --- | --- |
| 37 | 20.00 | --- | --- --- | --- |
| 37 | 33.33 | 24.83 | 1.29 --- | --- |
| 41 | 33.33 | --- | -- | --- |
| 41 | 20.00 | 25.78 | 1.10 --- | --- |
| $41-\mathrm{nr}$ | 20.00 | -- | --- --- | Vitrain, attritus, and fusain not recorded. |
| 43 | 20.00 | 20.00 | 1.02 SubC | Vitair |
| 44 | 20.00 | --- | --- | --- |
| 44 | 200.00 | --- | --- --- | --- |
| 44 | 20.00 | 50.51 | 0.94 --- | One large 30-mm-thick vitrain band with 5 mm of fusain (cumulative thickness) |
| ns3 | -- | --- | -- | No sample. |
| 45 | 200.00 | -- | --- --- | --- |
| 45 | 50.00 | 128.57 | 0.05 SubC | --- |
| 46 | 20.00 | 20.00 | 1.44 --- | Hard. |
| 48 | 20.00 | --- | --- --- | ---- |
| 48 | 20.00 | 20.00 | 1.85 --- | ---- |
| 49 | 33.33 | --- | ---- | Papery fusain at 40 cm with small amount of pyrite. |
| 49 | 20.00 | 31.59 | 1.77 --- | ---- |
| 54 | 33.33 | --- | --- --- | Highly fractured sample. |
| 54 | 50.00 | 46.46 | 1.51 --- | ---- |
| 56 | 33.33 | --- | --- --- | --- |
| 56 | 100.00 | 91.04 | 1.07 --- | --- |
| 57 | 100.00 | --- | --- SubB | ---- |
| 57 | 200.00 | 155.00 | 1.50 --- | ---- |
| 57-nr | 500.00 | --- | ------ | Vitrain, attritus, and fusain not recorded, resin. |
| ns4 | --- | --- | --- --- | No sample. |
| 58 | 100.00 | --- | --- --- | ---- |
| 58 | 50.00 | 76.32 | 1.37 SubC | ---- |
| 59 | 50.00 | --- | --- --- | ---- |
| 59 | 33.33 | --- | --- --- | ---- |
| 59 | 50.00 | --- | --- --- | ---- |
| 59 | 50.00 | 41.28 | 0.85 --- | ---- |

Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Appro dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative <br> fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 61 | 225.50 | 227.50 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 63.99 | 5.0 | 10.0 | 50.0 |
| C28 | 227.50 | --- | middle and lower Wyodak | 34.00 | --- | 0.53 | 65.11 | 10.0 | 0.0 | 35.0 |
| C28 | --- | 229.50 | middle and lower Wyodak | 30.00 | 64.00 | 0.47 | 66.09 | 1.0 | 5.0 | 40.0 |
| C29 | 229.50 | 231.50 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 68.00 | 10.0 | 20.0 | 7.0 |
| C30 | 231.50 | 233.50 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 70.00 | 10.0 | 20.0 | 30.0 |
| C31 | 233.50 | --- | middle and lower Wyodak | 34.00 | --- | 0.57 | 71.11 | 5.0 | 0.0 | 150.0 |
| C31 | --- | 235.50 | middle and lower Wyodak | 26.00 | 60.00 | 0.43 | 71.97 | 5.0 | 10.0 | 5.0 |
| C32 | 235.50 | --- | middle and lower Wyodak | 10.00 | --- | 0.15 | 72.29 | 5.0 | 40.0 | 5.0 |
| C32 | --- | 237.00 | middle and lower Wyodak | 25.00 | 35.00 | 0.38 | 73.11 | 30.0 | 0.0 | 0.0 |
| ns5 | 237.00 | 239.70 | ns5 | 82.00 | 82.00 | 1.00 | 75.80 | --- | --- | --- |
| C32 | 239.70 | 240.40 | middle and lower Wyodak | 31.00 | 66.00 | 0.47 | 76.82 | 5.0 | 5.0 | 5.0 |

Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 3 | 173.33 | 346.67 | 30.41 | 60.82 | 8.77 | 30.41 | 60.82 | 8.77 | 10 |
| C28 | 3 | 305.00 | 0.00 | 89.71 | 0.00 | 10.29 | --- | --- | --- | 10 |
| C28 | 2 | 43.33 | 216.67 | 14.44 | 72.22 | 13.33 | 54.43 | 33.85 | 11.72 | 10 |
| C29 | 3 | 191.00 | 382.00 | 32.93 | 65.86 | 1.21 | 32.93 | 65.86 | 1.21 | 10 |
| C30 | 3 | 193.33 | 386.67 | 31.69 | 63.39 | 4.92 | 31.69 | 63.39 | 4.92 | 5 |
| C31 | 3 | 190.00 | 0.00 | 55.88 | 0.00 | 44.12 | --- | --- | --- | 5 |
| C31 | 3 | 85.00 | 170.00 | 32.69 | 65.38 | 1.92 | 45.83 | 28.33 | 25.83 | 20 |
| C32 | 3 | 10.56 | 84.44 | 10.56 | 84.44 | 5.00 | --- | --- | - | 30 |
| C32 | 5 | 250.00 | 0.00 | 100.00 | 0.00 | 0.00 | 74.44 | 24.13 | 1.43 | 30 |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C32 | 3 | 152.50 | 152.50 | 49.19 | 49.19 | 1.61 | 62.58 | 35.90 | 1.52 | 20 |

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Table 1-6. Data for samples from core hole 10, Kennecott Energy, Kennecott CBM-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; nr, data not recorded; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas Apparent (SCF/ton) rank | Comments |
| :---: | :---: | :---: | :---: | :---: |
| 61 | 100.00 | 100.00 | 0.78 --- | ---- |
| C28 | 100.00 | --- | --- --- | ---- |
| C28 | 100.00 | 100.00 | 2.05 SubC | 5 mm of fusain at 28,42 , and 45 cm . |
| C29 | 100.00 | 100.00 | 0.31 --- | ---- |
| C30 | 200.00 | 200.00 | 1.29 --- | Highly fractured sample. |
| C31 | 200.00 | --- | --- --- | ---- |
| C31 | 50.00 | 135.00 | 0.93 --- | ---- |
| C32 | 33.33 | --- | --- | Slickensides. |
| C32 | 33.33 | 17.68 | 0.89 --- | ---- |
| ns5 | --- | --- | --- --- | Rock excluded from canister. |
| C32 | 50.00 | 41.16 | 3.50 SubB | --- |

Table 1-7. Data for samples from core hole 11, Barrett Resources Corporation, CARU State 22-16-5075W.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D1 | 1,352.80 | 1,354.80 | Big George | 60.00 | 60.00 | 1.00 | 1.97 | 2.0 | 5.0 | 0.0 |
| D2 | 1,354.80 | 1,356.80 | Big George | 58.00 | 58.00 | 1.00 | 3.87 | 5.0 | 20.0 | 3.0 |
| D3 | 1,356.80 | 1,358.80 | Big George | 60.00 | 60.00 | 1.00 | 5.84 | 5.0 | 30.0 | 0.0 |
| D4 | 1,358.80 | 1,360.80 | Big George | 60.00 | 60.00 | 1.00 | 7.81 | 5.0 | 30.0 | 0.0 |
| D5 | 1,360.80 | --- | Big George | 20.00 | --- | 0.33 | 8.46 | 5.0 | 30.0 | 0.0 |
| D5 | --- | 1,362.80 | Big George | 40.00 | 60.00 | 0.67 | 9.78 | 2.0 | 5.0 | 2.0 |
| D6 | 1,362.80 | 1,364.80 | Big George | 58.00 | 58.00 | 1.00 | 11.68 | 3.0 | 10.0 | 0.0 |
| ns1 | 1,364.80 | 1,365.80 | ns 1 | 30.50 | 30.50 | 1.00 | 12.68 | --- | --- | --- |
| ns2 | 1,365.80 | 1,368.00 | ns2 | 67.00 | 67.00 | 1.00 | 14.88 | --- | --- | --- |
| D7 | 1,368.00 | 1,370.00 | Big George | 60.00 | 60.00 | 1.00 | 16.85 | 10.0 | 30.0 | 0.0 |
| D8 | 1,370.00 | 1,372.00 | Big George | 60.00 | 60.00 | 1.00 | 18.82 | 2.0 | 20.0 | 0.0 |
| D9 | 1,372.00 | --- | Big George | 35.00 | --- | 0.58 | 19.96 | 5.0 | 2.0 | 0.0 |
| D9 | --- | 1,374.00 | Big George | 25.00 | 60.00 | 0.42 | 20.78 | 2.0 | 1.0 | 5.0 |
| D10 | 1,374.00 | 1,376.00 | Big George | 63.00 | 63.00 | 1.00 | 22.85 | 10.0 | 10.0 | 0.0 |
| D11 | 1,376.00 | 1,378.00 | Big George | 58.00 | 58.00 | 1.00 | 24.75 | 3.0 | 10.0 | 2.0 |
| D12 | 1,378.00 | 1,380.00 | Big George | 58.00 | 58.00 | 1.00 | 26.66 | 2.0 | 10.0 | 0.0 |
| ns3 | 1,380.00 | 1,381.00 | ns3 | 30.50 | 30.50 | 1.00 | 27.66 | 66 --- | --- | --- |
| ns4 | 1,381.00 | 1,382.00 | ns4 | 30.50 | 30.50 | 1.00 | 28.66 | --- | --- | --- |
| ns5 | 1,382.00 | 1,384.00 | ns5 | 61.00 | 61.00 | 1.00 | 30.66 | ---- | --- | --- |
| ns6 | 1,384.00 | 1,751.00 | ns6 | 11,187.00 | 11,187.00 | 1.00 | 397.69 | --- | --- | --- |
| D14 | 1,751.00 | 1,752.00 | Werner | 30.00 | 30.00 | 1.00 | 398.67 | 3.0 | 3.0 | 0.0 |
| D13 | 1,752.00 | 1,754.00 | Werner | 61.00 | 61.00 | 1.00 | 400.67 | 10.0 | 30.0 | 25.0 |
| ns7 | 1,754.00 | 1,755.00 | ns7 | 30.50 | 30.50 | 1.00 | 401.67 | --- | --- | --- |
| ns8 | 1,755.00 | 1,759.00 | ns8 | 122.00 | 122.00 | 1.00 | 405.68 | --- | --- | --- |
| ns9 | 1,759.00 | 1,761.00 | ns9 | 61.00 | 61.00 | 1.00 | 407.68 | --- | --- | --- |
| D25 | 1,761.00 | --- | Werner | 20.00 | --- | 0.36 | 408.33 | 50.0 | 20.0 | 10.0 |
| D25 | --- | 1,763.00 | Werner | 36.00 | 56.00 | 0.64 | 409.51 | 5.0 | 5.0 | 10.0 |
| D15 | 1,763.00 | 1,765.00 | Werner | 60.00 | 60.00 | 1.00 | 411.48 | 5.0 | 10.0 | 25.0 |
| D16 | 1,765.00 | --- | Werner | 30.00 | --- | 0.50 | 412.47 | 5.0 | 10.0 | 25.0 |
| D16 |  | 1,767.00 | Werner | 30.00 | 60.00 | 0.50 | 413.45 | 10.0 | 5.0 | 0.0 |
| D17 | 1,767.00 | 1,769.00 | Werner | 60.00 | 60.00 | 1.00 | 415.42 | 10.0 | 5.0 | 85.0 |
| D18 | 1,769.00 | 1,771.00 | Werner | 60.00 | 60.00 | 1.00 | 417.39 | 10.0 | 10.0 | 110.0 |
| D19 | 1,771.00 | --- | Werner | 26.00 | --- | 0.46 | 418.24 | 10.0 | 5.0 | 30.0 |
| D19 | --- | 1,773.00 | Werner | 30.00 | 56.00 | 0.54 | 419.23 | 30.0 | 2.0 | 5.0 |
| D20 | 1,773.00 | 1,775.00 | Werner | 60.00 | 60.00 | 1.00 | 421.19 | 5.0 | 3.0 | 60.0 |
| D21 | 1,775.00 | 1,777.00 | Werner | 60.00 | 60.00 | 1.00 | 423.16 | 5.0 | 3.0 | 60.0 |
| D22 | 1,777.00 | 1,779.00 | Werner | 49.00 | 49.00 | 1.00 | 424.77 | 10.0 | 5.0 | 35.0 |
| D23 | 1,779.00 | 1,781.00 | Werner | 60.00 | 60.00 | 1.00 | 426.74 | 10.0 | 5.0 | 50.0 |
| D24 | 1,781.00 | --- | Werner | 24.00 | --- | 0.40 | 427.53 | 20.0 | 30.0 | 20.0 |
| D24 |  | 1,783.00 | Werner | 36.00 | 60.00 | 0.60 | 428.71 | 10.0 | 5.0 | 10.0 |

Table 1-7. Data for samples from core hole 11, Barrett Resources Corporation, CARU State 22-16-5075W.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) <br> (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2 | 171.43 | 428.57 | 28.57 | 71.43 | 0.00 | 28.57 | 71.43 | 0.00 |
| D2 | 3 | 115.40 | 461.60 | 19.90 | 79.59 | 0.52 | 19.90 | 79.59 | 0.52 |
| D3 | 3 | 85.71 | 514.29 | 14.29 | 85.71 | 0.00 | 14.29 | 85.71 | 0.00 |
| D4 | 3 | 85.71 | 514.29 | 14.29 | 85.71 | 0.00 | 14.29 | 85.71 | 0.00 |
| D5 | 3 | 28.57 | 171.43 | 14.29 | 85.71 | 0.00 | --- | --- | --- |
| D5 | 2 | 113.71 | 284.29 | 28.43 | 71.07 | 0.50 | 23.71 | 75.95 | 0.33 |
| D6 | 2 | 133.85 | 446.15 | 23.08 | 76.92 | 0.00 | 23.08 | 76.92 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | - | -- |
| ns2 | --- | --- | --- | --- | ---- | --- | --- | --- | --- |
| D7 | 3 | 150.00 | 450.00 | 25.00 | 75.00 | 0.00 | 25.00 | 75.00 | 0.00 |
| D8 | 2 | 54.55 | 545.45 | 9.09 | 90.91 | 0.00 | 9.09 | 90.91 | 0.00 |
| D9 | 3 | 250.00 | 100.00 | 71.43 | 28.57 | 0.00 | --- | --- | --- |
| D9 | 2 | 163.33 | 81.67 | 65.33 | 32.67 | 2.00 | 68.89 | 30.28 | 0.83 |
| D10 | 3 | 315.00 | 315.00 | 50.00 | 50.00 | 0.00 | 50.00 | 50.00 | 0.00 |
| D11 | 2 | 133.38 | 444.62 | 23.00 | 76.66 | 0.34 | 23.00 | 76.66 | 0.34 |
| D12 | 2 | 96.67 | 483.33 | 16.67 | 83.33 | 0.00 | 16.67 | 83.33 | 0.00 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns6 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D14 | 2 | 150.00 | 150.00 | 50.00 | 50.00 | 0.00 | 50.00 | 50.00 | 0.00 |
| D13 | 3 | 146.25 | 438.75 | 23.98 | 71.93 | 4.10 | 23.98 | 71.93 | 4.10 |
| ns7 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns8 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns9 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D25 | 4 | 135.71 | 54.29 | 67.86 | 27.14 | 5.00 | --- | --- | --- |
| D25 | 3 | 175.00 | 175.00 | 48.61 | 48.61 | 2.78 | 55.48 | 40.94 | 3.57 |
| D15 | 3 | 191.67 | 383.33 | 31.94 | 63.89 | 4.17 | 31.94 | 63.89 | 4.17 |
| D16 | 3 | 91.67 | 183.33 | 30.56 | 61.11 | 8.33 | --- | --- | --- |
| D16 | 3 | 200.00 | 100.00 | 66.67 | 33.33 | 0.00 | 48.61 | 47.22 | 4.17 |
| D17 | 3 | 343.33 | 171.67 | 57.22 | 28.61 | 14.17 | 57.22 | 28.61 | 14.17 |
| D18 | 3 | 245.00 | 245.00 | 40.83 | 40.83 | 18.33 | 40.83 | 40.83 | 18.33 |
| D19 | 3 | 153.33 | 76.67 | 58.97 | 29.49 | 11.54 | --- | --- | --- |
| D19 | 4 | 276.56 | 18.44 | 92.19 | 6.15 | 1.67 | 76.77 | 16.98 | 6.25 |
| D20 | 3 | 337.50 | 202.50 | 56.25 | 33.75 | 10.00 | 56.25 | 33.75 | 10.00 |
| D21 | 3 | 337.50 | 202.50 | 56.25 | 33.75 | 10.00 | 56.25 | 33.75 | 10.00 |
| D22 | 3 | 303.33 | 151.67 | 61.90 | 30.95 | 7.14 | 61.90 | 30.95 | 7.14 |
| D23 | 3 | 366.67 | 183.33 | 61.11 | 30.56 | 8.33 | 61.11 | 30.56 | 8.33 |
| D24 | 3 | 88.00 | 132.00 | 36.67 | 55.00 | 8.33 | --- | --- | --- |
| D24 | 3 | 233.33 | 116.67 | 64.81 | 32.41 | 2.78 | 53.56 | 41.44 | 5.00 |

Table 1-7. Data for samples from core hole 11, Barrett Resources Corporation, CARU State 22-16-5075W.Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 20 | 50.00 | 50.00 | 28.46 | SubB | Highly fragmented sample. |
| D2 | 20 | 50.00 | 50.00 | 29.49 | --- | --- |
| D3 | 10 | 100.00 | 100.00 | 32.00 | --- | Highly fragmented sample/slickensides. |
| D4 | 10 | 100.00 | 100.00 | 33.14 | --- | Solid. |
| D5 | 30 | 33.33 | --- | --- | --- | --- |
| D5 | 10 | 100.00 | 77.78 | 31.20 | --- | --- |
| D6 | 30 | 33.33 | 33.33 | 34.10 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | Sample taken for adsorption analysis. |
| ns2 | --- | --- | --- | --- | --- | No sample, lost in core hole. |
| D7 | 20 | 50.00 | 50.00 | 31.11 | --- | --- |
| D8 | 30 | 33.33 | 33.33 | 31.27 | --- | Tight. |
| D9 | 30 | 33.33 | --- | --- | --- | --- |
| D9 | 30 | 33.33 | 33.33 | 34.81 | --- | Fusain in attritus. |
| D10 | 30 | 33.33 | 33.33 | 35.02 | --- | Resin at 10 cm . |
| D11 | 20 | 50.00 | 50.00 | 32.95 | --- | Kaolinite. |
| D12 | 10 | 100.00 | 100.00 | 30.81 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | Bagged sample. |
| ns4 | --- | --- | --- | --- | --- | Bagged sample. |
| ns5 | --- | --- | --- | --- | --- | No sample, lost in core hole. |
| ns6 | --- | --- | --- | --- | --- | No sample. |
| D14 | 5 | 200.00 | 200.00 | 32.62 | --- | --- |
| D13 | 20 | 50.00 | 50.00 | 38.16 | --- | --- |
| ns7 | --- | --- | --- | --- | --- | Bagged sample for adsorption analysis. |
| ns8 | --- | --- | --- | --- | --- | No sample. |
| ns9 | --- | --- | --- | --- | --- | Bagged sample. |
| D25 | 20 | 50.00 | --- | --- | --- | --- |
| D25 | 20 | 50.00 | 50.00 | 37.45 | --- | Some kaolinite. |
| D15 | 5 | 200.00 | 200.00 | 39.09 | --- | Highly fragmented sample, kaolinite on cleat. |
| D16 | 5 | 200.00 | --- | --- | --- | --- |
| D16 | 10 | 100.00 | 150.00 | 42.27 | --- | Highly fragmented sample. |
| D17 | 30 | 33.33 | 33.33 | 40.85 | SubB | Fusain rich. |
| D18 | 30 | 33.33 | 33.33 | 43.47 | --- | Fusain rich. |
| D19 | 10 | 100.00 | --- | --- | --- | Highly fragmented sample. |
| D19 | 10 | 100.00 | 100.00 | 38.39 | --- | --- |
| D20 | 5 | 200.00 | 200.00 | 41.39 | --- | Fusain rich. |
| D21 | 5 | 200.00 | 200.00 | 41.96 | --- | --- |
| D22 | 5 | 200.00 | 200.00 | 37.38 | --- | Highly fragmented sample. |
| D23 | 5 | 200.00 | 200.00 | 44.70 | --- | --- |
| D24 | 10 | 100.00 | --- | --- | --- | --- |
| D24 | 10 | 100.00 | 100.00 | 39.65 | SubB | --- |

Table 1-8. Data for samples from core hole 12, Barrett Resources Corporation, Schoonover Road Unit (SRU) State 12-16-4876.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D30fr | 1,360.00 | 1,362.00 | Big George | 40.00 | 40.00 | 1.00 | 1.31 | --- | --- | --- |
| D31 | 1,362.00 | 1,364.00 | Big George | 47.00 | 47.00 | 1.00 | 2.85 | 50.0 | 1.0 | 0.0 |
| ns1 | 1,364.00 | 1,371.00 | ns1 | 213.50 | 213.50 | 1.00 | 9.86 | --- | --- | --- |
| D38 | 1,371.00 | 1,372.00 | Big George | 30.00 | 30.00 | 1.00 | 10.84 | 10.0 | 1.0 | 10.0 |
| D37 | 1,372.00 | 1,374.00 | Big George | 67.00 | 67.00 | 1.00 | 13.04 | 50.0 | 0.0 | 0.0 |
| D36 | 1,374.00 | 1,376.00 | Big George | 67.00 | 67.00 | 1.00 | 15.24 | 50.0 | 0.0 | 0.0 |
| D32 | 1,376.00 | --- | Big George | 24.00 | --- | 0.35 | 16.03 | 50.0 | 0.0 | 0.0 |
| D32 | --- | 1,378.00 | Big George | 44.00 | 68.00 | 0.65 | 17.47 | 10.0 | 2.0 | 5.0 |
| D33 | 1,378.00 | --- | Big George | 27.00 | --- | 0.44 | 18.36 | 20.0 | 2.0 | 5.0 |
| D33 | --- | 1,380.00 | Big George | 35.00 | 62.00 | 0.56 | 19.50 | 5.0 | 2.0 | 10.0 |
| D34 | 1,380.00 | 1,382.00 | Big George | 64.00 | 64.00 | 1.00 | 21.60 | 20.0 | 2.0 | 10.0 |
| ns2 | 1,382.00 | 1,383.00 | ns2 | 30.50 | 30.50 | 1.00 | 22.60 | --- | --- | --- |
| D35 | 1,383.00 | 1,384.00 | Big George | 30.00 | 30.00 | 1.00 | 23.59 | 30.0 | 2.0 | 5.0 |
| D39 | 1,384.00 | 1,385.00 | Big George | 30.00 | 30.00 | 1.00 | 24.57 | 40.0 | 1.0 | 0.0 |
| ns3 | 1,385.00 | 1,390.00 | ns3 | 152.50 | 152.50 | 1.00 | 29.58 | --- | --- | --- |
| D43 | 1,390.00 | 1,394.00 | Big George | 54.00 | 54.00 | 1.00 | 31.35 | 20.0 | 5.0 | 0.0 |
| D42 | 1,392.00 | 1,394.00 | Big George | 59.00 | 59.00 | 1.00 | 33.28 | 20.0 | 2.0 | 0.0 |
| D41 | 1,394.00 | 1,396.00 | Big George | 54.00 | 54.00 | 1.00 | 35.06 | 10.0 | 5.0 | 5.0 |
| D40 | 1,396.00 | 1,398.00 | Big George | 52.00 | 52.00 | 1.00 | 36.76 | 10.0 | 2.0 | 10.0 |
| ns4 | 1,398.00 | 1,399.00 | ns4 | 30.50 | 30.50 | 1.00 | 37.76 | --- | --- | --- |
| D50 | 1,399.00 | 1,400.00 | Big George | 30.00 | 30.00 | 1.00 | 38.75 | 5.0 | 1.0 | 0.0 |
| D44 | 1,400.00 | 1,402.00 | Big George | 58.00 | 58.00 | 1.00 | 40.65 | 30.0 | 3.0 | 10.0 |
| D45 | 1,402.00 | 1,404.00 | Big George | 58.00 | 58.00 | 1.00 | 42.55 | 50.0 | 2.0 | 0.0 |
| D46 | 1,404.00 | 1,406.00 | Big George | 60.00 | 60.00 | 1.00 | 44.52 | 50.0 | 5.0 | 0.0 |
| D47 | 1,406.00 | 1,408.00 | Big George | 63.00 | 63.00 | 1.00 | 46.59 | 30.0 | 10.0 | 0.0 |
| D48fr | 1,408.00 | 1,410.00 | Big George | 40.00 | 40.00 | 1.00 | 47.90 | --- | --- | --- |
| D49 | 1,410.00 | 1,412.00 | Big George | 65.00 | 65.00 | 1.00 | 50.03 | 10.0 | 2.0 | 0.0 |
| ns5 | 1,412.00 | 1,415.00 | ns5 | 91.50 | 91.50 | 1.00 | 53.03 | --- | --- | --- |
| D29 | 1,415.00 | 1,417.00 | Big George | 63.00 | 63.00 | 1.00 | 55.10 | 10.0 | 5.0 | 5.0 |
| D51 | 1,417.00 | 1,419.00 | Big George | 64.00 | 64.00 | 1.00 | 57.20 | 5.0 | 10.0 | 0.0 |
| D52 | 1,419.00 | --- | Big George | 40.00 | --- | 0.60 | 58.51 | 50.0 | 20.0 | 20.0 |
| D52 | --- | 1,421.00 | Big George | 27.00 | 67.00 | 0.40 | 59.40 | 50.0 | 0.0 | 0.0 |
| D53 | 1,421.00 | 1,423.00 | Big George | 64.00 | 64.00 | 1.00 | 61.50 | 10.0 | 2.0 | 5.0 |
| D54 | 1,423.00 | --- | Big George | 16.00 | --- | 0.27 | 62.02 | 30.0 | 2.0 | 10.0 |
| D54 | --- | 1,425.00 | Big George | 44.00 | 60.00 | 0.73 | 63.47 | 3.0 | 5.0 | 40.0 |
| D55 | 1,425.00 | 1,427.00 | Big George | 60.00 | 60.00 | 1.00 | 65.44 | 10.0 | 2.0 | 120.0 |
| D56 | 1,427.00 | --- | Big George | 46.00 | --- | 0.70 | 66.95 | 10.0 | 2.0 | 90.0 |
| D56 | --- | 1,429.00 | Big George | 20.00 | 66.00 | 0.30 | 67.60 | 10.0 | 2.0 | 5.0 |
| D57fr | 1,429.00 | 1,430.30 | Big George | 40.00 | 40.00 | 1.00 | 68.91 | --- | --- | --- |
| D57 | 1,430.30 | 1,431.00 | Big George | 30.00 | 30.00 | 1.00 | 69.90 | 5.0 | 2.0 | 95.0 |
| ns6 | 1,431.00 | 1,432.00 | ns6 | 30.50 | 30.50 | 1.00 | 70.90 | --- | --- | --- |
| D26 | 1,432.00 | 1,432.40 | Big George | 13.00 | 13.00 | 1.00 | 71.33 | 2.0 | 50.0 | 0.0 |
| D26fr | 1,432.40 | 1,433.00 | Big George | 17.50 | 17.50 | 1.00 | 71.90 | --- | --- | --- |
| D28 | 1,433.00 | --- | Big George | 31.00 | --- | 0.56 | 72.92 | 10.0 | 2.0 | 15.0 |
| D28 | --- | --- | Big George | 17.00 | --- | 0.31 | 73.47 | 50.0 | 2.0 | 10.0 |
| D28 | --- | 1,435.00 | Big George | 7.00 | 55.00 | 0.13 | 73.70 | 0.0 | 0.0 | 0.0 |
| D27 | 1,435.00 | 1437.00 | Big George | 64.00 | 64.00 | 1.00 | 75.80 | 2.0 | 5.0 | 10.0 |

Table 1-8. Data for samples from core hole 12, Barrett Resources Corporation, Schoonover Road Unit (SRU) State 12-16-4876.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D30fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D31 | 5 | 460.78 | 9.22 | 98.04 | 1.96 | 0.00 | 98.04 | 1.96 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D38 | 3 | 263.64 | 26.36 | 87.88 | 8.79 | 3.33 | 87.88 | 8.79 | 3.33 |
| D37 | 5 | 670.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| D36 | 5 | 670.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 |
| D32 | 5 | 240.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | ---- | --- |
| D32 | 3 | 362.50 | 72.50 | 82.39 | 16.48 | 1.14 | 88.60 | 10.66 | 0.74 |
| D33 | 3 | 240.91 | 24.09 | 89.23 | 8.92 | 1.85 | --- | --- | --- |
| D33 | 3 | 242.86 | 97.14 | 69.39 | 27.76 | 2.86 | 78.03 | 19.55 | 2.42 |
| D34 | 3 | 572.73 | 57.27 | 89.49 | 8.95 | 1.56 | 89.49 | 8.95 | 1.56 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D35 | 4 | 276.56 | 18.44 | 92.19 | 6.15 | 1.67 | 92.19 | 6.15 | 1.67 |
| D39 | 4 | 292.68 | 7.32 | 97.56 | 2.44 | 0.00 | 97.56 | 2.44 | 0.00 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D43 | 3 | 432.00 | 108.00 | 80.00 | 20.00 | 0.00 | 80.00 | 20.00 | 0.00 |
| D42 | 3 | 536.36 | 53.64 | 90.91 | 9.09 | 0.00 | 90.91 | 9.09 | 0.00 |
| D41 | 3 | 356.67 | 178.33 | 66.05 | 33.02 | 0.93 | 66.05 | 33.02 | 0.93 |
| D40 | 3 | 425.00 | 85.00 | 81.73 | 16.35 | 1.92 | 81.73 | 16.35 | 1.92 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D50 | 3 | 250.00 | 50.00 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 | 0.00 |
| D44 | 4 | 518.18 | 51.82 | 89.34 | 8.93 | 1.72 | 89.34 | 8.93 | 1.72 |
| D45 | 5 | 557.69 | 22.31 | 96.15 | 3.85 | 0.00 | 96.15 | 3.85 | 0.00 |
| D46 | 4 | 545.45 | 54.55 | 90.91 | 9.09 | 0.00 | 90.91 | 9.09 | 0.00 |
| D47 | 4 | 472.50 | 157.50 | 75.00 | 25.00 | 0.00 | 75.00 | 25.00 | 0.00 |
| D48fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D49 | 3 | 541.67 | 108.33 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 | 0.00 |
| ns5 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D29 | 3 | 416.67 | 208.33 | 66.14 | 33.07 | 0.79 | 66.14 | 33.07 | 0.79 |
| D51 | 3 | 213.33 | 426.67 | 33.33 | 66.67 | 0.00 | 33.33 | 66.67 | 0.00 |
| D52 | 4 | 271.43 | 108.57 | 67.86 | 27.14 | 5.00 | --- | --- | --- |
| D52 | 5 | 270.00 | 0.00 | 100.00 | 0.00 | 0.00 | 80.81 | 16.20 | 2.99 |
| D53 | 3 | 529.17 | 105.83 | 82.68 | 16.54 | 0.78 | 82.68 | 16.54 | 0.78 |
| D54 | 4 | 140.63 | 9.38 | 87.89 | 5.86 | 6.25 | --- | --- | --- |
| D54 | 2 | 150.00 | 250.00 | 34.09 | 56.82 | 9.09 | 48.44 | 43.23 | 8.33 |
| D55 | 3 | 400.00 | 80.00 | 66.67 | 13.33 | 20.00 | 66.67 | 13.33 | 20.00 |
| D56 | 3 | 308.33 | 61.67 | 67.03 | 13.41 | 19.57 | --- | --- | --- |
| D56 | 3 | 162.50 | 32.50 | 81.25 | 16.25 | 2.50 | 71.34 | 14.27 | 14.39 |
| D57fr | - | --- | --- | --- | --- | --- | --- | --- | --- |
| D57 | 3 | 146.43 | 58.57 | 48.81 | 19.52 | 31.67 | 48.81 | 19.52 | 31.67 |
| ns6 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D26 | 1 | 5.00 | 125.00 | 3.85 | 96.15 | 0.00 | 3.85 | 96.15 | 0.00 |
| D26fr | - | --- | --- | --- | --- | --- | --- | --- | --- |
| D28 | 3 | 245.83 | 49.17 | 79.30 | 15.86 | 4.84 | --- | --- | --- |
| D28 | 5 | 153.85 | 6.15 | 90.50 | 3.62 | 5.88 | --- | --- | --- |
| D28 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 72.67 | 10.06 | 4.55 |
| D27 | 2 | 180.00 | 450.00 | 28.13 | 70.31 | 1.56 | 28.13 | 70.31 | 1.56 |

Table 1-8. Data for samples from core hole 12, Barrett Resources Corporation, Schoonover Road Unit (SRU) State 12-16-4876.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) <br> (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D30fr | --- | --- | --- | 25.33 | --- | Sample too highly fractured to describe. |
| D31 | 20 | 50.00 | 50.00 | 24.24 | --- | Highly fractured sample. |
| ns1 | --- | --- | --- | --- | --- | No sample, top 1 ft is sample for adsorption analysis. |
| D38 | 40 | 25.00 | 25.00 | 32.06 | --- | Resin at 3 cm . |
| D37 | 20 | 50.00 | 50.00 | 28.33 | --- | --- |
| D36 | 20 | 50.00 | 50.00 | 31.93 | SubB | --- |
| D32 | 20 | 50.00 | --- | --- | --- | --- |
| D32 | 30 | 33.33 | 39.22 | 32.39 | --- | --- |
| D33 | 30 | 33.33 | --- | --- | --- | --- |
| D33 | 40 | 25.00 | 28.63 | 34.36 | --- | --- |
| D34 | 30 | 33.33 | 33.33 | 36.00 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | No sample, lost during drilling. |
| D35 | 30 | 33.33 | 33.33 | 30.95 | --- | --- |
| D39 | 10 | 100.00 | 100.00 | 27.06 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | No sample, top 1 ft is sample taken for adsorption analysis. |
| D43 | 30 | 33.33 | 33.33 | 30.95 | SubB | --- |
| D42 | 20 | 50.00 | 50.00 | 34.46 | --- | --- |
| D41 | 20 | 50.00 | 50.00 | 33.38 | --- | --- |
| D40 | 20 | 50.00 | 50.00 | 30.09 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | Sample taken for adsorption analysis. |
| D50 | 10 | 100.00 | 100.00 | 26.02 | --- | Highly fractured sample. |
| D44 | 5 | 200.00 | 200.00 | 31.74 | --- | Kaolinite on cleat. |
| D45 | 10 | 100.00 | 100.00 | 31.30 | --- | --- |
| D46 | 10 | 100.00 | 100.00 | 34.39 | --- | --- |
| D47 | 10 | 100.00 | 100.00 | 30.06 | --- | Highly fractured sample. |
| D48fr | --- | --- | --- | 30.52 | --- | Sample too highly fractured to describe. |
| D49 | 5 | 200.00 | 200.00 | 30.72 | SubB | --- |
| ns5 | --- | --- | --- | --- | --- | Sample taken for adsorption analysis. |
| D29 | 30 | 33.33 | 33.33 | 32.00 | --- | --- |
| D51 | 20 | 50.00 | 50.00 | 28.38 | --- | --- |
| D52 | 10 | 100.00 | --- | --- | --- | --- |
| D52 | 10 | 100.00 | 100.00 | 30.41 | --- | --- |
| D53 | 10 | 100.00 | 100.00 | 30.58 | --- | Dark band is fusain. |
| D54 | 40 | 25.00 | --- | --- | --- | --- |
| D54 | 20 | 50.00 | 43.33 | 29.62 | --- | --- |
| D55 | 30 | 33.33 | 33.33 | 33.70 | --- | Fusain-rich attritus at 54 cm . |
| D56 | 10 | 100.00 | --- | --- | --- | Fusain-rich 5 mm fractures at $0-5 \mathrm{~cm}$. |
| D56 | 30 | 33.33 | 79.80 | 23.98 | --- | --- |
| D57fr | --- | --- | --- | --- | --- | Sample too highly fractured to describe. |
| D57 | 10 | 100.00 | 100.00 | 24.32 | --- | --- |
| ns6 | --- | --- | --- | --- | --- | No sample, lost during drilling. |
| D26 | 10 | 100.00 | 100.00 | 16.97 | SubB | --- |
| D26fr | --- | --- | --- | --- | --- | Sample too highly fractured to describe. |
| D28 | 50 | 20.00 | --- | --- | --- | --- |
| D28 | 50 | 20.00 | --- | --- | --- | --- |
| D28 | 50 | 20.00 | 20.00 | 15.00 | --- | Clay parting included. |
| D27 | 50 | 20.00 | 20.00 | 19.02 | SubB | Calcite on cleat, very bright pyrite bleb at 35 cm . |

Table 1-9. Data for samples from core hole 13, Rim Operating Inc., CBM H -11-04.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| C-2 | 204.00 | --- | Upper Wyodak | 5.00 | --- | 0.08 | 0.16 | 0.0 |
| C-2 | --- | 206.00 | Upper Wyodak | 55.00 | 60.00 | 0.92 | 1.97 | 50.0 |
| C-3 | 206.00 | --- | Upper Wyodak | 13.00 | --- | 0.25 | 2.40 | 0.0 |
| C-3 | --- | --- | Upper Wyodak | 35.00 | --- | 0.69 | 3.54 | 2.0 |
| C-3 | --- | 208.00 | Upper Wyodak | 3.00 | 51.00 | 0.06 | 3.64 | 0.0 |
| C-18 | 208.00 | --- | Upper Wyodak | 4.00 | --- | 0.07 | 3.77 | 0.0 |
| C-18 | --- | 210.00 | Upper Wyodak | 51.00 | 55.00 | 0.93 | 5.45 | 50.0 |
| C-19 | 210.00 | --- | Upper Wyodak | 30.00 | --- | 0.54 | 6.43 | 2.0 |
| C-19 | --- | 212.00 | Upper Wyodak | 26.00 | 56.00 | 0.46 | 7.28 | 50.0 |
| C-20 | 212.00 | --- | Upper Wyodak | 34.00 | --- | 0.56 | 8.40 | 50.0 |
| C-20 | --- | 214.00 | Upper Wyodak | 27.00 | 61.00 | 0.44 | 9.28 | 5.0 |
| C-21 | 214.00 | 216.00 | Upper Wyodak | 60.00 | 60.00 | 1.00 | 11.25 | 5.0 |
| C-22 | 216.00 | --- | Upper Wyodak | 7.00 | --- | 0.12 | 11.48 | 5.0 |
| C-22 | --- | 218.00 | Upper Wyodak | 53.00 | 60.00 | 0.88 | 13.22 | 50.0 |
| C-23 | 218.00 | --- | Upper Wyodak | 33.00 | --- | 0.56 | 14.30 | 1.0 |
| C-23 | --- | 220.00 | Upper Wyodak | 26.00 | 59.00 | 0.44 | 15.16 | 50.0 |
| ns1 | 220.00 | 222.00 | ns1 | 61.00 | 61.00 | 1.00 | 17.16 | --- |
| 43 | 222.00 | 224.00 | Mid-Lower Wyodak | 42.00 | 42.00 | 1.00 | 18.54 | 0.0 |
| C-24 | 224.00 | 226.00 | Mid-Lower Wyodak | 59.00 | 59.00 | 1.00 | 20.47 | 50.0 |
| C-27 | 226.00 | 228.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 22.44 | 10.0 |
| C-26 | 228.00 | 230.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 24.41 | 50.0 |
| C-28 | 230.00 | 232.00 | Mid-Lower Wyodak | 55.00 | 55.00 | 1.00 | 26.21 | 50.0 |
| C-29A | 232.00 | 234.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 28.18 | 50.0 |
| C-30 | 234.00 | 236.00 | Mid-Lower Wyodak | 59.00 | 59.00 | 1.00 | 30.12 | 50.0 |
| C-31 | 236.00 | 238.00 | Mid-Lower Wyodak | 52.00 | 52.00 | 1.00 | 31.82 | 50.0 |
| C-32 | 238.00 | 240.00 | Mid-Lower Wyodak | 57.00 | 57.00 | 1.00 | 33.69 | 50.0 |
| C-33 | 240.00 | 242.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 35.66 | 2.0 |
| ns2 | 242.00 | 244.00 | ns2 | 61.00 | 61.00 | 1.00 | 37.66 | --- |
| C-35 | 244.00 | 246.00 | Mid-Lower Wyodak | 58.00 | 58.00 | 1.00 | 39.57 | 50.0 |
| C-36 | 246.00 | 248.00 | Mid-Lower Wyodak | 62.00 | 62.00 | 1.00 | 41.60 | 2.0 |
| C-37 | 248.00 | --- | Mid-Lower Wyodak | 8.00 | --- | 0.13 | 41.86 | 2.0 |
| C-37 | --- | 250.00 | Mid-Lower Wyodak | 56.00 | 64.00 | 0.88 | 43.70 | 50.0 |
| C-38 | 250.00 | --- | Mid-Lower Wyodak | 24.00 | --- | 0.40 | 44.49 | 10.0 |
| C-38 | --- | 252.00 | Mid-Lower Wyodak | 36.00 | 60.00 | 0.60 | 45.67 | 2.0 |
| C-39 | 252.00 | --- | Mid-Lower Wyodak | 20.00 | --- | 0.33 | 46.33 | 5.0 |
| C-39 | --- | --- | Mid-Lower Wyodak | 3.00 | --- | 0.05 | 46.42 | 0.0 |
| C-39 | --- | 254.00 | Mid-Lower Wyodak | 37.00 | 60.00 | 0.62 | 47.64 | 10.0 |
| C-40 | 254.00 | --- | Mid-Lower Wyodak | 44.00 | --- | 0.71 | 49.08 | 2.0 |
| C-40 | --- | 256.00 | Mid-Lower Wyodak | 18.00 | 62.00 | 0.29 | 49.67 | 50.0 |
| C-41 | 256.00 | --- | Mid-Lower Wyodak | 17.00 | --- | 0.27 | 50.23 | 50.0 |
| C-41 | --- | --- | Mid-Lower Wyodak | 2.00 | --- | 0.03 | 50.30 | 0.0 |
| C-41 | --- | --- | Mid-Lower Wyodak | 27.00 | --- | 0.42 | 51.18 | 1.0 |
| C-41 | --- | 258.00 | Mid-Lower Wyodak | 18.00 | 64.00 | 0.28 | 51.77 | 50.0 |
| C-42 | 258.00 | 260.00 | Mid-Lower Wyodak | 56.00 | 56.00 | 1.00 | 53.61 | 50.0 |
| C-43 | 260.00 | 262.00 | Mid-Lower Wyodak | 52.00 | 52.00 | 1.00 | 55.31 | 50.0 |
| 6 | 262.00 | 264.00 | Mid-Lower Wyodak | 43.00 | 43.00 | 1.00 | 56.73 | 30.0 |
| 10 | 264.00 | 266.00 | Mid-Lower Wyodak | 62.00 | 62.00 | 1.00 | 58.76 | 10.0 |
| 56 | 266.00 | 268.00 | Mid-Lower Wyodak | 58.00 | 58.00 | 1.00 | 60.66 | 50.0 |
| 65 | 268.00 | 270.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 62.63 | 5.0 |
| A3fr | 270.00 | 272.00 | Mid-Lower Wyodak | 54.00 | 54.00 | 1.00 | 64.40 | --- |
| A5fr | 272.00 | 274.00 | Mid-Lower Wyodak | 59.00 | 59.00 | 1.00 | 66.34 | --- |
| A6fr | 274.00 | 276.00 | Mid-Lower Wyodak | 60.00 | 60.00 | 1.00 | 68.31 | --- |
| A8fr | 276.00 | --- | Mid-Lower Wyodak | 21.00 | --- | 1.00 | 69.00 | --- |
| A8 | --- | 278.00 | Mid-Lower Wyodak | 33.00 | 33.00 | 1.00 | 70.08 | 50.0 |
| A21 | 278.00 | 280.00 | Mid-Lower Wyodak | 43.00 | 43.00 | 1.00 | 71.49 | --- |

Table 1-9. Data for samples from core hole 13, Rim Operating Inc., CBM H -11-04.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-2 | 10.0 | 0.0 | 1 | 0.00 | 50.00 | 0.00 | 100.00 |
| C-2 | 0.0 | 0.0 | 5 | 550.00 | 0.00 | 100.00 | 0.00 |
| C-3 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-3 | 50.0 | 0.0 | 1 | 13.46 | 336.54 | 3.85 | 96.15 |
| C-3 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-18 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-18 | 0.0 | 0.0 | 5 | 510.00 | 0.00 | 100.00 | 0.00 |
| C-19 | 50.0 | 0.0 | 1 | 11.54 | 288.46 | 3.85 | 96.15 |
| C-19 | 0.0 | 0.0 | 5 | 260.00 | 0.00 | 100.00 | 0.00 |
| C-20 | 0.0 | 0.0 | 5 | 340.00 | 0.00 | 100.00 | 0.00 |
| C-20 | 20.0 | 10.0 | 3 | 52.00 | 208.00 | 19.26 | 77.04 |
| C-21 | 10.0 | 10.0 | 3 | 196.67 | 393.33 | 32.78 | 65.56 |
| C-22 | 10.0 | 0.0 | 3 | 23.33 | 46.67 | 33.33 | 66.67 |
| C-22 | 5.0 | 0.0 | 4 | 481.82 | 48.18 | 90.91 | 9.09 |
| C-23 | 50.0 | 0.0 | 1 | 6.47 | 323.53 | 1.96 | 98.04 |
| C-23 | 0.0 | 0.0 | 5 | 260.00 | 0.00 | 100.00 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | - |
| 43 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-24 | 0.0 | 0.0 | 5 | 590.00 | 0.00 | 100.00 | 0.00 |
| C-27 | 20.0 | 0.0 | 3 | 200.00 | 400.00 | 33.33 | 66.67 |
| C-26 | 50.0 | 0.0 | 4 | 300.00 | 300.00 | 50.00 | 50.00 |
| C-28 | 0.0 | 10.0 | 5 | 540.00 | 0.00 | 98.18 | 0.00 |
| C-29A | 50.0 | 8.0 | 4 | 296.00 | 296.00 | 49.33 | 49.33 |
| C-30 | 50.0 | 0.0 | 4 | 295.00 | 295.00 | 50.00 | 50.00 |
| C-31 | 0.0 | 0.0 | 5 | 520.00 | 0.00 | 100.00 | 0.00 |
| C-32 | 0.0 | 0.0 | 5 | 570.00 | 0.00 | 100.00 | 0.00 |
| C-33 | 50.0 | 0.0 | 1 | 23.08 | 576.92 | 3.85 | 96.15 |
| ns2 | --- | --- | -- | --- | --- | --- | --- |
| C-35 | 0.0 | 0.0 | 5 | 580.00 | 0.00 | 100.00 | 0.00 |
| C-36 | 10.0 | 0.0 | 2 | 103.33 | 516.67 | 16.67 | 83.33 |
| C-37 | 10.0 | 0.0 | 2 | 13.33 | 66.67 | 16.67 | 83.33 |
| C-37 | 0.0 | 5.0 | 5 | 555.00 | 0.00 | 99.11 | 0.00 |
| C-38 | 5.0 | 0.0 | 3 | 160.00 | 80.00 | 66.67 | 33.33 |
| C-38 | 50.0 | 0.0 | 1 | 13.85 | 346.15 | 3.85 | 96.15 |
| C-39 | 5.0 | 0.0 | 3 | 100.00 | 100.00 | 50.00 | 50.00 |
| C-39 | 0.0 | 30.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-39 | 20.0 | 0.0 | 3 | 123.33 | 246.67 | 33.33 | 66.67 |
| C-40 | 10.0 | 0.0 | 2 | 73.33 | 366.67 | 16.67 | 83.33 |
| C-40 | 30.0 | 0.0 | 4 | 112.50 | 67.50 | 62.50 | 37.50 |
| C-41 | 0.0 | 0.0 | 5 | 170.00 | 0.00 | 100.00 | 0.00 |
| C-41 | 0.0 | 20.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 |
| C-41 | 40.0 | 0.0 | 1 | 6.59 | 263.41 | 2.44 | 97.56 |
| C-41 | 0.0 | 0.0 | 5 | 180.00 | 0.00 | 100.00 | 0.00 |
| C-42 | 0.0 | 0.0 | 5 | 560.00 | 0.00 | 100.00 | 0.00 |
| C-43 | 40.0 | 0.0 | 4 | 288.89 | 231.11 | 55.56 | 44.44 |
| 6 | 10.0 | 10.0 | 4 | 315.00 | 105.00 | 73.26 | 24.42 |
| 10 | 20.0 | 5.0 | 3 | 205.00 | 410.00 | 33.06 | 66.13 |
| 56 | 10.0 | 0.0 | 4 | 483.33 | 96.67 | 83.33 | 16.67 |
| 65 | 10.0 | 10.0 | 3 | 196.67 | 393.33 | 32.78 | 65.56 |
| A3fr | --- | --- | --- | --- | --- | --- | --- |
| A5fr | --- | --- | --- | --- | --- | --- | --- |
| A6fr | --- | --- | --- | --- | --- | --- | --- |
| A8fr | --- | --- | --- | --- | --- | --- | --- |
| A8 | 40.0 | 10.0 | 4 | 177.78 | 142.22 | 53.87 | 43.10 |
| A21 | --- | --- | --- | --- | --- | --- | --- |

Table 1-9. Data for samples from core hole 13, Rim Operating Inc., CBM H -11-04.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat requency (CFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-2 | 0.00 | --- | --- | --- | --- | - |
| C-2 | 0.00 | 91.67 | 8.33 | 0.00 | 10 | 100.00 |
| C-3 | 0.00 | --- | --- | --- | --- | --- |
| C-3 | 0.00 | --- | --- | --- | 20 | 50.00 |
| C-3 | 0.00 | 2.64 | 65.99 | 0.00 | --- | --- |
| C-18 | 0.00 | --- | --- | --- | --- | --- |
| C-18 | 0.00 | 92.73 | 0.00 | 0.00 | 5 | 200.00 |
| C-19 | 0.00 | --- | --- | --- | 20 | 50.00 |
| C-19 | 0.00 | 48.49 | 51.51 | 0.00 | 5 | 200.00 |
| C-20 | 0.00 | --- | --- | --- | 5 | 200.00 |
| C-20 | 3.70 | 64.26 | 34.10 | 1.64 | 10 | 100.00 |
| C-21 | 1.67 | 32.78 | 65.56 | 1.67 | 20 | 50.00 |
| C-22 | 0.00 | --- | --- | --- | 10 | 100.00 |
| C-22 | 0.00 | 84.19 | 15.81 | 0.00 | 5 | 200.00 |
| C-23 | 0.00 | --- | --- | --- | --- | --- |
| C-23 | 0.00 | 45.16 | 54.84 | 0.00 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- |
| 43 | 0.00 | --- | --- | --- | --- | --- |
| C-24 | 0.00 | 100.00 | 0.00 | 0.00 | 10 | 100.00 |
| C-27 | 0.00 | 33.33 | 66.67 | 0.00 | 5 | 200.00 |
| C-26 | 0.00 | 50.00 | 50.00 | 0.00 | 10 | 100.00 |
| C-28 | 1.82 | 98.18 | 0.00 | 1.82 | 5 | 200.00 |
| C-29A | 1.33 | 49.33 | 49.33 | 1.33 | 5 | 200.00 |
| C-30 | 0.00 | 50.00 | 50.00 | 0.00 | 5 | 200.00 |
| C-31 | 0.00 | 100.00 | 0.00 | 0.00 | 5 | 200.00 |
| C-32 | 0.00 | 100.00 | 0.00 | 0.00 | 10 | 100.00 |
| C-33 | 0.00 | 3.85 | 96.15 | 0.00 | 30 | 33.33 |
| ns2 | --- | --- | --- | --- | --- | --- |
| C-35 | 0.00 | 100.00 | 0.00 | 0.00 | 10 | 100.00 |
| C-36 | 0.00 | 16.67 | 83.33 | 0.00 | 10 | 100.00 |
| C-37 | 0.00 | --- | --- | --- | 5 | 200.00 |
| C-37 | 0.89 | 88.80 | 10.42 | 0.78 | 5 | 200.00 |
| C-38 | 0.00 | --- | --- | --- | 30 | 33.33 |
| C-38 | 0.00 | 28.97 | 71.03 | 0.00 | 40 | 25.00 |
| C-39 | 0.00 | --- | --- | --- | 5 | 200.00 |
| C-39 | 100.00 | --- | --- | --- | --- | --- |
| C-39 | 0.00 | 37.22 | 57.78 | 5.00 | 30 | 33.33 |
| C-40 | 0.00 | --- | --- | --- | 5 | 200.00 |
| C-40 | 0.00 | 29.97 | 70.03 | 0.00 | 10 | 100.00 |
| C-41 | 0.00 | --- | --- | --- | 5 | 200.00 |
| C-41 | 100.00 | --- | --- | --- | --- | --- |
| C-41 | 0.00 | --- | --- | --- | 20 | 50.00 |
| C-41 | 0.00 | 55.72 | 41.16 | 3.13 | 5 | 200.00 |
| C-42 | 0.00 | 100.00 | 0.00 | 0.00 | 5 | 200.00 |
| C-43 | 0.00 | 55.56 | 44.44 | 0.00 | 5 | 200.00 |
| 6 | 2.33 | 73.26 | 24.42 | 2.33 | 5 | 200.00 |
| 10 | 0.81 | 33.06 | 66.13 | 0.81 | 5 | 200.00 |
| 56 | 0.00 | 83.33 | 16.67 | 0.00 | 5 | 200.00 |
| 65 | 1.67 | 32.78 | 65.56 | 1.67 | 5 | 200.00 |
| A3fr | --- | --- | --- | --- | --- | --- |
| A5fr | --- | --- | --- | --- | --- | --- |
| A6fr | --- | --- | --- | --- | --- | --- |
| A8fr | --- | --- | --- | --- | --- | --- |
| A8 | 3.03 | 53.87 | 43.10 | 3.03 | 10 | 100.00 |
| A21 | --- | --- | --- | --- | --- | --- |

Table 1-9. Data for samples from core hole 13, Rim Operating Inc., CBM H -11-04.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: |
| C-2 | --- | --- | --- | --- |
| C-2 | 100.00 | 4.46 | --- | --- |
| C-3 | --- | --- | --- | Clay. |
| C-3 | --- | --- | --- | --- |
| C-3 | 50.00 | 2.10 | --- | Clay. |
| C-18 | --- | --- | --- | Highly fractured sample, clay. |
| C-18 | 200.00 | 3.21 | --- | Highly fractured sample. |
| C-19 | --- | --- | --- | Highly fractured sample. |
| C-19 | 119.64 | 2.09 | --- | Pyrite at 15 cm . |
| C-20 | --- | --- | --- | Highly fractured sample. |
| C-20 | 155.74 | 2.61 | --- | --- |
| C-21 | 50.00 | 1.94 | SubC | --- |
| C-22 | --- | --- | --- | --- |
| C-22 | 188.33 | 4.59 | --- | Highly fractured sample. |
| C-23 | --- | --- | --- | Kaolinite at 16 cm . |
| C-23 | --- | 1.96 | --- | --- |
| ns1 | --- | --- | --- | No sample, top 1 ft is coal, bottom 1 ft is rock. |
| 43 | --- | --- | --- | Dark-gray siltstone. |
| C-24 | 100.00 | 2.80 | --- | Woody. |
| C-27 | 200.00 | 2.10 | --- | Pyrite at $41-42 \mathrm{~cm}, 1 \mathrm{~cm}$ thick, pyrite blebs throughout bed. |
| C-26 | 100.00 | 1.32 | --- | Woody. |
| C-28 | 200.00 | 1.79 | --- | Highly fractured sample. |
| C-29A | 200.00 | 1.75 | SubC | --- |
| C-30 | 200.00 | 1.59 | --- | Highly fractured sample. |
| C-31 | 200.00 | 1.83 | --- | Highly fractured sample. |
| C-32 | 100.00 | 2.28 | --- | Highly fractured sample. |
| C-33 | 33.33 | 2.45 | --- | Highly fractured sample. |
| ns2 | --- | --- | --- | No sample, lost during drilling. |
| C-35 | 100.00 | 2.40 | SubB | Highly fractured sample. |
| C-36 | 100.00 | 1.27 | --- | --- |
| C-37 | --- | --- | --- | --- |
| C-37 | 200.00 | 1.60 | --- | --- |
| C-38 | --- | --- | --- | --- |
| C-38 | 28.33 | 1.94 | --- | --- |
| C-39 | --- | --- | --- | Highly fractured sample. |
| C-39 | --- | --- | --- | Bed of fusain. |
| C-39 | 91.81 | 1.20 | --- | --- |
| C-40 | --- | --- | --- | Highly fractured sample. |
| C-40 | 170.97 | 3.41 | --- | --- |
| C-41 | --- | --- | --- | Highly fractured sample. |
| C-41 | --- | --- | --- | Bed of fusain. |
| C-41 | --- | --- | --- | --- |
| C-41 | 134.68 | 2.15 | --- | Highly fractured sample. |
| C-42 | 200.00 | 2.37 | --- | Highly fractured sample. |
| C-43 | 200.00 | 1.52 | --- | Highly fractured sample. |
| 6 | 200.00 | 2.44 | --- | Highly fractured sample. |
| 10 | 200.00 | 1.47 | --- | Highly fractured sample. |
| 56 | 200.00 | 1.23 | SubC | Highly fractured sample. |
| 65 | 200.00 | 2.01 | --- | Highly fractured sample. |
| A3fr | --- | 1.32 | --- | Sample too fractured to describe. |
| A5fr | --- | 14.59 | --- | Sample too fractured to describe. |
| A6fr | --- | 2.17 | --- | Sample too fractured to describe. |
| A8fr | --- | --- | --- | Sample too fractured to describe. |
| A8 | 100.00 | 2.77 | --- | --- |
| A21 | --- | 37.10 | --- | Sample too fractured to describe. |

Table 1-10. Data for samples from core hole 14, Rim Operating Inc., CBM C 33-1R.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit <br> thickness <br> (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| 8 | 259.00 | 261.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 1.71 | 50.0 |
| 9 fr | 261.00 | 263.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 3.67 | --- |
| 11 | 263.00 | --- | middle and lower Wyodak | 30.00 | --- | 0.56 | 4.66 | 10.0 |
| 11 | --- | 264.80 | middle and lower Wyodak | 24.00 | 54.00 | 0.44 | 5.45 | 2.0 |
| ns1 | 264.80 | 265.00 | ns1 | 6.00 | 6.00 | 1.00 | 5.64 | --- |
| 12fr | 265.00 | 267.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 7.61 | --- |
| 13 fr | 267.00 | 269.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 9.58 | --- |
| 14 | 269.00 | 271.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 11.55 | 20.0 |
| 15 | 271.00 | 273.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 13.52 | 2.0 |
| 16 | 273.00 | 274.80 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 15.35 | 20.0 |
| ns2 | 274.80 | 275.00 | ns2 | 6.00 | 6.00 | 1.00 | 15.55 | --- |
| 18 | 275.00 | 277.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 17.52 | 5.0 |
| 19 | 277.00 | 279.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 19.46 | 10.0 |
| 20 fr | 279.00 | 281.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 21.42 | --- |
| 21 | 281.00 | 283.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 23.39 | 5.0 |
| 22 | 283.00 | 285.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 25.16 | 10.0 |
| 23 fr | 285.00 | 287.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 26.87 | --- |
| 24fr | 287.00 | 289.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 28.64 | --- |
| 25 | 289.00 | 291.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 30.41 | 2.0 |
| 26 fr | 291.00 | 293.00 | middle and lower Wyodak | 53.00 | 53.00 | 1.00 | 32.15 | --- |
| 27 | 293.00 | 295.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 33.99 | 5.0 |
| 28 fr | 295.00 | 297.00 | middle and lower Wyodak | 49.00 | 49.00 | 1.00 | 35.60 | --- |
| 29fr | 297.00 | 299.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 37.57 | --- |
| 30 fr | 299.00 | 301.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 39.53 | --- |
| 31 fr | 301.00 | 303.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 41.50 | --- |
| 32 | 303.00 | 305.00 | middle and lower Wyodak | 50.00 | 50.00 | 1.00 | 43.14 | 3.0 |
| 33 fr | 305.00 | 307.00 | middle and lower Wyodak | 48.00 | 48.00 | 1.00 | 44.72 | --- |
| 34fr | 307.00 | 309.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 46.49 | --- |
| 35 | 309.00 | 311.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 48.39 | 5.0 |
| 36 | 311.00 | 313.00 | middle and lower Wyodak | 40.00 | 40.00 | 1.00 | 49.70 | 30.0 |
| 37 | 313.00 | 315.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 51.54 | 10.0 |
| 38 | 315.00 | 317.00 | middle and lower Wyodak | 40.00 | 40.00 | 1.00 | 52.85 | 2.0 |
| 39 | 317.00 | 319.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 54.82 | 5.0 |

Table 1-10. Data for samples from core hole 14, Rim Operating Inc., CBM C 33-1R.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 0.0 | 0.0 | 5 | 520.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 |
| 9 fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 11 | 5.0 | 0.0 | 3 | 200.00 | 100.00 | 66.67 | 33.33 | 0.00 | --- |
| 11 | 10.0 | 0.0 | 2 | 40.00 | 200.00 | 16.67 | 83.33 | 0.00 | 44.44 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 12fr | --- | --- | --- | --- | --- | --- | ---- | --- | --- |
| 13fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 14 | 2.0 | 25.0 | 3 | 522.73 | 52.27 | 87.12 | 8.71 | 4.17 | 87.12 |
| 15 | 5.0 | 10.0 | 2 | 168.57 | 421.43 | 28.10 | 70.24 | 1.67 | 28.10 |
| 16 | 20.0 | 0.0 | 3 | 280.00 | 280.00 | 50.00 | 50.00 | 0.00 | 50.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 18 | 5.0 | 0.0 | 3 | 300.00 | 300.00 | 50.00 | 50.00 | 0.00 | 50.00 |
| 19 | 20.0 | 0.0 | 3 | 196.67 | 393.33 | 33.33 | 66.67 | 0.00 | 33.33 |
| 20 fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 21 | 5.0 | 0.0 | 3 | 300.00 | 300.00 | 50.00 | 50.00 | 0.00 | 50.00 |
| 22 | 20.0 | 30.0 | 3 | 170.00 | 340.00 | 31.48 | 62.96 | 5.56 | 31.48 |
| 23fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 24fr | --- | --- | --- | --- | --- | --- | --- | --- | - |
| 25 | 20.0 | 0.0 | 2 | 49.09 | 490.91 | 9.09 | 90.91 | 0.00 | 9.09 |
| 26 fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 27 | 20.0 | 0.0 | 3 | 112.00 | 448.00 | 20.00 | 80.00 | 0.00 | 20.00 |
| 28fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 29 fr | --- | --- | --- | --- | --- | --- | ---- | --- | --- |
| 30 fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 31 fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 32 | 5.0 | 30.0 | 2 | 176.25 | 293.75 | 35.25 | 58.75 | 6.00 | 35.25 |
| 33fr | --- | --- | --- | ---- | --- | --- | - --- | --- | --- |
| 34fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 35 | 5.0 | 40.0 | 3 | 270.00 | 270.00 | 46.55 | 46.55 | 6.90 | 46.55 |
| 36 | 30.0 | 20.0 | 4 | 190.00 | 190.00 | 47.50 | 47.50 | 5.00 | 47.50 |
| 37 | 10.0 | 20.0 | , | 270.00 | 270.00 | 48.21 | 48.21 | 3.57 | 48.21 |
| 38 | 40.0 | 0.0 | 1 | 19.05 | 380.95 | 4.76 | 95.24 | 0.00 | 4.76 |
| 39 | 40.0 | 5.0 | 3 | 66.11 | 528.89 | 11.02 | 88.15 | 0.83 | 11.02 |

Table 1-10. Data for samples from core hole 14, Rim Operating Inc., CBM C 33-1R.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | 0.00 | 0.00 | 10 | 100.00 | 100.00 | 9.54 | SubC | Highly fragmented sample. |
| 9fr | --- | --- | --- | --- | --- | 10.51 | --- | Sample too fragmented to describe. |
| 11 | --- | --- | 20 | 50.00 | --- | --- | --- | --- |
| 11 | 55.56 | 0.00 | 10 | 100.00 | 72.22 | 10.43 | --- | Highly fragmented sample. |
| ns1 | --- | --- | --- | --- | --- | --- | --- | No sample, lost during drilling. |
| 12 fr | --- | --- | --- | --- | --- | 8.22 | --- | Sample too fragmented to describe. |
| 13 fr | --- | --- | --- | --- | --- | 11.41 | --- | Sample too fragmented to describe. |
| 14 | 8.71 | 4.17 | 20 | 50.00 | 50.00 | 12.83 | --- | Highly fragmented sample. |
| 15 | 70.24 | 1.67 | 20 | 50.00 | 50.00 | 12.73 | --- | --- |
| 16 | 50.00 | 0.00 | 20 | 50.00 | 50.00 | 14.32 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | --- | --- | No sample, lost during drilling. |
| 18 | 50.00 | 0.00 | 20 | 50.00 | 50.00 | 11.57 | --- | Highly fragmented sample. |
| 19 | 66.67 | 0.00 | 10 | 100.00 | 100.00 | 11.81 | --- | --- |
| 20 fr | --- | --- | --- | --- | --- | 11.37 | --- | Sample too fragmented to describe. |
| 21 | 50.00 | 0.00 | 10 | 100.00 | 100.00 | 15.44 | SubC | 边 |
| 22 | 62.96 | 5.56 | 20 | 50.00 | 50.00 | 12.22 | --- | --- |
| 23 fr | --- | --- | --- | --- | --- | 12.19 | --- | Sample too fragmented to describe. |
| 24 fr | --- | --- | --- | --- | --- | 12.21 | --- | Sample too fragmented to describe. |
| 25 | 90.91 | 0.00 | 10 | 100.00 | 100.00 | 12.07 | --- | Highly fragmented sample. |
| 26 fr | --- | --- | --- | ---- | --- | 12.33 | --- | Sample too fragmented to describe. |
| 27 | 80.00 | 0.00 | 5 | 200.00 | 200.00 | 13.50 | --- | Highly fragmented sample. |
| 28 fr | --- | --- | --- | --- | --- | 10.81 | --- | Sample too fragmented to describe. |
| 29 fr | --- | --- | --- | ---- | --- | 10.36 | --- | Sample too fragmented to describe. |
| 30 fr | --- | --- | --- | --- | --- | 11.58 | --- | Sample too fragmented to describe. |
| 31 fr | --- | --- | --- | ---- | --- | 11.78 | --- | Sample too fragmented to describe. |
| 32 | 58.75 | 6.00 | 5 | 200.00 | 200.00 | 12.34 | --- | Highly fragmented sample. |
| 33 fr | --- | --- | --- | --- | --- | 11.35 | --- | Sample too fragmented to describe. |
| 34 fr | --- | --- | --- | --- | --- | 12.40 | --- | Sample too fragmented to describe. |
| 35 | 46.55 | 6.90 | 5 | 200.00 | 200.00 | 12.74 | SubC | Highly fragmented, kaolinite on cleats. |
| 36 | 47.50 | 5.00 | 10 | 100.00 | 100.00 | 13.03 | SubC | Highly fragmented sample. |
| 37 | 48.21 | 3.57 | 10 | 100.00 | 100.00 | 13.36 | --- | Highly fragmented sample. |
| 38 | 95.24 | 0.00 | 5 | 200.00 | 200.00 | 12.01 | --- | Highly fragmented sample. |
| 39 | 88.15 | 0.83 | 10 | 100.00 | 100.00 | 11.68 | --- | Highly fragmented sample. |

Table 1-11. Data for samples from core hole 15, Peabody Natural Gas LLC, PNG 34-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| B-1 | 258.30 | 260.30 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 2.10 | 5.0 | 40.0 |
| B-2 | 260.30 | --- | middle and lower Wyodak | 47.00 | --- | 0.73 | 3.64 | 20.0 | 40.0 |
| B-2 | --- | 262.30 | middle and lower Wyodak | 17.00 | 64.00 | 0.27 | 4.20 | 2.0 | 20.0 |
| B-3 | 262.30 | --- | middle and lower Wyodak | 15.00 | --- | 0.22 | 4.69 | 50.0 | 0.0 |
| B-3 | --- | --- | middle and lower Wyodak | 32.00 | --- | 0.48 | 5.74 | 2.0 | 10.0 |
| B-3 | --- | 264.30 | middle and lower Wyodak | 20.00 | 67.00 | 0.30 | 6.40 | 50.0 | 0.0 |
| ns1 | 264.30 | 266.00 | ns1 | 52.00 | 52.00 | 1.00 | 8.10 | --- | --- |
| B-4fr | 266.00 | 268.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 10.01 | --- | --- |
| B-5fr | 268.00 | 270.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 11.91 | --- | --- |
| B-6fr | 270.00 | 272.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 13.68 | --- | --- |
| B-7fr | 272.00 | 274.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 15.65 | --- | --- |
| B-8 | 274.00 | --- | middle and lower Wyodak | 26.00 | --- | 0.46 | 16.50 | 50.0 | 50.0 |
| B-8 | --- | --- | middle and lower Wyodak | 19.00 | --- | 0.33 | 17.13 | 5.0 | 50.0 |
| B-8 | --- | 276.00 | middle and lower Wyodak | 12.00 | 57.00 | 0.21 | 17.52 | 5.0 | 20.0 |
| B-9fr | 276.00 | 278.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 19.49 | --- | --- |
| B10 | 278.00 | 280.00 | middle and lower Wyodak | 48.00 | 48.00 | 1.00 | 21.06 | 20.0 | 20.0 |
| B-11 fr | 280.00 | 282.00 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 23.13 | --- | --- |
| B-12fr | 282.00 | 284.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 25.10 | --- | --- |
| B-13 | 284.00 | --- | middle and lower Wyodak | 20.00 | --- | 0.33 | 25.75 | 5.0 | 5.0 |
| B-13 | --- | --- | middle and lower Wyodak | 30.00 | --- | 0.50 | 26.74 | 50.0 | 50.0 |
| B-13 | --- | 286.00 | middle and lower Wyodak | 10.00 | 60.00 | 0.17 | 27.07 | 5.0 | 30.0 |
| B-14fr | 286.00 | --- | middle and lower Wyodak | 18.00 | --- | 1.00 | 27.66 | --- | --- |
| B-14 | --- | 288.00 | middle and lower Wyodak | 45.00 | 45.00 | 1.00 | 29.13 | 10.0 | 20.0 |
| B-15 | 288.00 | --- | middle and lower Wyodak | 17.00 | --- | 0.27 | 29.69 | 5.0 | 30.0 |
| B-15 | --- | 290.00 | middle and lower Wyodak | 46.00 | 63.00 | 0.73 | 31.20 | 50.0 | 50.0 |
| ns2 | 290.00 | 291.00 | ns2 | 30.50 | 30.50 | 1.00 | 32.20 | --- | - |
| B16 | 291.00 | 293.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 34.17 | 5.0 | 20.0 |
| B18 | 293.00 | 295.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 36.14 | 5.0 | 15.0 |
| B19 | 295.00 | 297.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 38.11 | 10.0 | 10.0 |
| B17 | 297.00 | --- | middle and lower Wyodak | 39.00 | --- | 0.62 | 39.39 | 10.0 | 10.0 |
| B17 | --- | 299.00 | middle and lower Wyodak | 24.00 | 63.00 | 0.38 | 40.17 | 30.0 | 70.0 |
| B20 | 299.00 | --- | middle and lower Wyodak | 35.00 | --- | 0.56 | 41.32 | 30.0 | 70.0 |
| B20 | --- | 301.00 | middle and lower Wyodak | 28.00 | 63.00 | 0.44 | 42.24 | 2.0 | 10.0 |
| B21 | 301.00 | --- | middle and lower Wyodak | 24.00 | --- | 0.33 | 43.03 | 2.0 | 10.0 |
| B21 | --- | --- | middle and lower Wyodak | 24.00 | --- | 0.33 | 43.82 | 5.0 | 10.0 |
| B21 | --- | --- | middle and lower Wyodak | 10.00 | --- | 0.14 | 44.14 | 50.0 | 50.0 |
| B21 | --- | 303.00 | middle and lower Wyodak | 14.00 | 72.00 | 0.19 | 44.60 | 3.0 | 5.0 |
| B22 | 303.00 | 305.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 46.31 | 1.0 | 5.0 |
| ns3 | 305.00 | 307.00 | ns3 | 61.00 | 61.00 | 1.00 | 48.31 | --- | --- |
| B23fr | 307.00 | 309.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 50.02 | --- | --- |
| B24 | 309.00 | 311.00 | middle and lower Wyodak | 50.00 | 50.00 | 1.00 | 51.66 | 5.0 | 20.0 |
| 40 | 311.00 | 313.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 53.56 | 10.0 | 40.0 |
| 41 | 313.00 | 315.00 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 55.63 | 2.0 | 50.0 |
| 42 | 315.00 | 317.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 57.60 | 10.0 | 50.0 |
| 43 | 317.00 | --- | middle and lower Wyodak | 45.00 | --- | 0.70 | 59.07 | 1.0 | 5.0 |
| 43 | --- | 319.00 | middle and lower Wyodak | 19.00 | 64.00 | 0.30 | 59.69 | 20.0 | 20.0 |
| 44 | 319.00 | --- | middle and lower Wyodak | 14.00 | --- | 0.23 | 60.15 | 20.0 | 20.0 |
| 44 | --- | 321.00 | middle and lower Wyodak | 46.00 | 60.00 | 0.77 | 61.66 | 5.0 | 5.0 |
| ns4 | 321.00 | 322.00 | ns4 | 30.50 | 30.50 | 1.00 | 62.66 | --- | --- |
| 45 | 322.00 | 324.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 64.50 | 2.0 | 20.0 |
| 46fr | 324.00 | 326.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 66.47 | --- | --- |
| 47fr | 326.00 | 328.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 68.44 | --- | --- |

Table 1-11. Data for samples from core hole 15, Peabody Natural Gas LLC, PNG 34-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B-1 | 0.0 | 3 | 71.11 | 568.89 | 11.11 | 88.89 | 0.00 | 11.11 | 88.89 |
| B-2 | 5.0 | 3 | 155.00 | 310.00 | 32.98 | 65.96 | 1.06 | --- | --- |
| B-2 | 0.0 | 2 | 15.45 | 154.55 | 9.09 | 90.91 | 0.00 | 26.63 | 72.59 |
| B-3 | 5.0 | 5 | 145.00 | 0.00 | 96.67 | 0.00 | 3.33 | --- | --- |
| B-3 | 0.0 | 2 | 53.33 | 266.67 | 16.67 | 83.33 | 0.00 | --- | --- |
| B-3 | 0.0 | 5 | 200.00 | 0.00 | 100.00 | 0.00 | 0.00 | 59.45 | 39.80 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-4fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-5fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-6fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-7fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-8 | 0.0 | 4 | 130.00 | 130.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| B-8 | 0.0 | 3 | 17.27 | 172.73 | 9.09 | 90.91 | 0.00 | --- | --- |
| B-8 | 0.0 | 3 | 24.00 | 96.00 | 20.00 | 80.00 | 0.00 | 30.05 | 69.95 |
| B-9fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B10 | 0.0 | 3 | 240.00 | 240.00 | 50.00 | 50.00 | 0.00 | 50.00 | 50.00 |
| B-11fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-12fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-13 | 0.0 | 3 | 100.00 | 100.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| B-13 | 0.0 | 4 | 150.00 | 150.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| B-13 | 5.0 | 3 | 13.57 | 81.43 | 13.57 | 81.43 | 5.00 | 43.93 | 55.24 |
| B-14fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B-14 | 15.0 | 3 | 145.00 | 290.00 | 32.22 | 64.44 | 3.33 | 32.22 | 64.44 |
| B-15 | 10.0 | 3 | 22.86 | 137.14 | 13.45 | 80.67 | 5.88 | --- | --- |
| B-15 | 0.0 | 4 | 230.00 | 230.00 | 50.00 | 50.00 | 0.00 | 40.14 | 58.28 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B16 | 0.0 | 3 | 120.00 | 480.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 |
| B18 | 5.0 | 3 | 148.75 | 446.25 | 24.79 | 74.38 | 0.83 | 24.79 | 74.38 |
| B19 | 15.0 | 3 | 292.50 | 292.50 | 48.75 | 48.75 | 2.50 | 48.75 | 48.75 |
| B17 | 10.0 | 3 | 190.00 | 190.00 | 48.72 | 48.72 | 2.56 | --- | --- |
| B17 | 0.0 | 4 | 72.00 | 168.00 | 30.00 | 70.00 | 0.00 | 41.59 | 56.83 |
| B20 | 0.0 | 4 | 105.00 | 245.00 | 30.00 | 70.00 | 0.00 | --- | --- |
| B20 | 10.0 | 2 | 45.00 | 225.00 | 16.07 | 80.36 | 3.57 | 23.81 | 74.60 |
| B21 | 5.0 | 2 | 39.17 | 195.83 | 16.32 | 81.60 | 2.08 | --- | --- |
| B21 | 0.0 | 3 | 80.00 | 160.00 | 33.33 | 66.67 | 0.00 | --- | --- |
| B21 | 0.0 | 4 | 50.00 | 50.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| B21 | 10.0 | 2 | 48.75 | 81.25 | 34.82 | 58.04 | 7.14 | 30.27 | 67.65 |
| B22 | 15.0 | 2 | 84.17 | 420.83 | 16.19 | 80.93 | 2.88 | 16.19 | 80.93 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B23fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B24 | 5.0 | 3 | 99.00 | 396.00 | 19.80 | 79.20 | 1.00 | 19.80 | 79.20 |
| 40 | 0.0 | 3 | 116.00 | 464.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 |
| 41 | 0.0 | 1 | 24.23 | 605.77 | 3.85 | 96.15 | 0.00 | 3.85 | 96.15 |
| 42 | 0.0 | 3 | 100.00 | 500.00 | 16.67 | 83.33 | 0.00 | 16.67 | 83.33 |
| 43 | 10.0 | 2 | 73.33 | 366.67 | 16.30 | 81.48 | 2.22 | --- | --- |
| 43 | 0.0 | 3 | 95.00 | 95.00 | 50.00 | 50.00 | 0.00 | 26.30 | 72.14 |
| 44 | 0.0 | 3 | 70.00 | 70.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| 44 | 10.0 | 3 | 225.00 | 225.00 | 48.91 | 48.91 | 2.17 | 49.17 | 49.17 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 45 | 0.0 | 2 | 50.91 | 509.09 | 9.09 | 90.91 | 0.00 | 9.09 | 90.91 |
| 46fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 47fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |

Table 1-11. Data for samples from core hole 15, Peabody Natural Gas LLC, PNG 34-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) <br> (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B-1 | 0.00 | 40 | 25.00 | 25.00 | 1.26 | SubC | --- |
| B-2 | --- | 10 | 100.00 | --- | --- | --- | --- |
| B-2 | 0.78 | 40 | 25.00 | 80.08 | 0.48 | --- | --- |
| B-3 | --- | 30 | 33.33 | --- | --- | --- | --- |
| B-3 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B-3 | 0.75 | 10 | 100.00 | 61.19 | 0.82 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | Bag sample taken. |
| B-4fr | --- | --- | --- | --- | 1.55 | --- | Sample too fragmented to describe. |
| B-5fr | --- | --- | --- | --- | 1.15 | --- | Sample too fragmented to describe. |
| B-6fr | --- | --- | --- | --- | 0.56 | --- | Sample too fragmented to describe. |
| B-7fr | --- | --- | --- | --- | 0.59 | SubC | Sample too fragmented to describe. |
| B-8 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B-8 | --- | 30 | 33.33 | --- | --- | --- | --- |
| B-8 | 0.00 | 20 | 50.00 | 44.44 | 0.69 | --- | --- |
| B-9fr | --- | --- | --- | --- | 0.58 | --- | Sample too fragmented to describe. |
| B10 | 0.00 | 10 | 100.00 | 100.00 | 1.30 | --- | Highly fragmented sample. |
| B-11 fr | --- | --- | --- | --- | 0.77 | --- | Sample too fragmented to describe. |
| B-12fr | --- | --- | --- | --- | 1.00 | --- | Sample too fragmented to describe. |
| B-13 | --- | 5 | 200.00 | --- | --- | --- | --- |
| B-13 | --- | 30 | 33.33 | --- | --- | --- | --- |
| B-13 | 0.83 | 20 | 50.00 | 91.67 | 0.64 | SubC | --- |
| B-14fr | --- | --- | --- | --- | --- | --- | Sample taken for adsorption analysis. |
| B-14 | 3.33 | 10 | 100.00 | 100.00 | 0.92 | --- | --- |
| B-15 | --- | 30 | 33.33 | --- | --- | --- | --- |
| B-15 | 1.59 | 50 | 20.00 | 23.60 | 0.78 | --- | --- |
| ns2 | --- | --- | --- | --- | - | --- | Bag sample taken. |
| B16 | 0.00 | 10 | 100.00 | 100.00 | 1.93 | --- | Highly fragmented sample. |
| B18 | 0.83 | 10 | 100.00 | 100.00 | 0.89 | --- | Highly fragmented sample. |
| B19 | 2.50 | 10 | 100.00 | 100.00 | 0.96 | --- | Highly fragmented sample. |
| B17 | --- | 5 | 200.00 | --- | --- | --- | --- |
| B17 | 1.59 | 10 | 100.00 | 161.90 | 0.95 | --- | --- |
| B20 | --- | 10 | 100.00 | --- | --- | --- | --- |
| B20 | 1.59 | 30 | 33.33 | 70.37 | 1.10 | SubC | Fusain-rich attritus. |
| B21 | --- | 10 | 100.00 | --- | --- | --- | --- |
| B21 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B21 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B21 | 2.08 | 20 | 50.00 | 66.67 | 0.89 | --- | --- |
| B22 | 2.88 | 20 | 50.00 | 50.00 | 1.27 | --- | Fusain-rich attritus. |
| ns3 | --- | --- | --- | --- | --- | --- | Bag sample taken. |
| B23fr | --- | - | --- | --- | 1.04 | --- | Sample too fragmented to describe. |
| B24 | 1.00 | 5 | 200.00 | 200.00 | 1.54 | --- | Highly fragmented sample. |
| 40 | 0.00 | 5 | 200.00 | 200.00 | 1.53 | --- | Highly fragmented sample. |
| 41 | 0.00 | 5 | 200.00 | 200.00 | 1.28 | SubC | Highly fragmented sample. |
| 42 | 0.00 | 5 | 200.00 | 200.00 | 0.86 | --- | --- |
| 43 | --- | 30 | 33.33 | --- | --- | --- | --- |
| 43 | 1.56 | 20 | 50.00 | 38.28 | 1.32 | --- | --- |
| 44 | --- | 20 | 50.00 | --- | --- | --- | --- |
| 44 | 1.67 | 30 | 33.33 | 37.22 | 1.67 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | No sample. |
| 45 | 0.00 | 20 | 50.00 | 50.00 | 1.77 | --- | Highly fragmented sample. |
| 46fr | --- | --- | --- | --- | 1.72 | --- | Sample too fragmented to describe. |
| 47 fr | --- | --- | --- | --- | 1.55 | --- | Sample too fragmented to describe. |

Table 1-12. Data for samples from core hole 16, Peabody Natural Gas LLC, PNG 33-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| C1 | 286.00 | 288.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 1.97 | 10.0 | 10.0 |
| C2 | 288.00 | --- | middle and lower Wyodak | 20.00 | --- | 0.31 | 2.62 | 5.0 | 50.0 |
| C2 | --- | 290.00 | middle and lower Wyodak | 44.00 | 64.00 | 0.69 | 4.07 | 30.0 | 30.0 |
| C3 | 290.00 | --- | middle and lower Wyodak | 24.00 | --- | 0.37 | 4.86 | 5.0 | 50.0 |
| C3 | --- | 292.00 | middle and lower Wyodak | 41.00 | 65.00 | 0.63 | 6.20 | 10.0 | 40.0 |
| C4 | 292.00 | 294.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 8.07 | 10.0 | 50.0 |
| C5fr | 294.20 | 296.40 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 10.10 | --- | --- |
| C6fr | 296.40 | 298.60 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 12.01 | --- | --- |
| C7 | 298.60 | 300.80 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 14.07 | 50.0 | 10.0 |
| C8 | 300.80 | 303.00 | middle and lower Wyodak | 67.00 | 67.00 | 1.00 | 16.27 | 50.0 | 0.0 |
| ns1 | 303.00 | 303.50 | ns1 | 15.00 | 15.00 | 1.00 | 16.77 | --- | --- |
| C9 | 303.50 | 305.50 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 18.64 | 50.0 | 10.0 |
| C10fr | 305.50 | 307.50 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 20.64 | --- | --- |
| C11 | 307.50 | 309.50 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 22.57 | 50.0 | 5.0 |
| C12 | 309.50 | 311.50 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 24.51 | 50.0 | 20.0 |
| ns2 | 311.50 | 314.30 | ns2 | 85.00 | 85.00 | 1.00 | 27.30 | --- | --- |
| C13 | 314.30 | 316.30 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 29.36 | 30.0 | 10.0 |
| C14fr | 316.30 | 318.30 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 31.33 | --- | --- |
| C15 | 318.30 | 320.30 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 33.37 | 2.0 | 10.0 |
| C16fr | 320.30 | 322.30 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 35.40 | --- | --- |
| ns3 | 322.30 | 328.00 | ns3 | 174.00 | 174.00 | 1.00 | 41.11 | --- | --- |
| C17 | 328.00 | 330.00 | middle and lower Wyodak | 47.00 | 47.00 | 1.00 | 42.65 | 5.0 | 20.0 |
| C18 | 330.00 | --- | middle and lower Wyodak | 32.00 | --- | 0.53 | 43.70 | 20.0 | 5.0 |
| C18 | --- | 332.00 | middle and lower Wyodak | 28.00 | 60.00 | 0.47 | 44.62 | 5.0 | 50.0 |
| C19 | 332.00 | 334.00 | middle and lower Wyodak | 66.00 | 66.00 | 1.00 | 46.78 | 5.0 | 30.0 |
| C20 | 334.00 | 336.00 | middle and lower Wyodak | 65.00 | 65.00 | 1.00 | 48.92 | 5.0 | 20.0 |
| C21 | 336.00 | 338.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 50.95 | 20.0 | 50.0 |
| C22 | 338.00 | 340.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 52.92 | 2.0 | 20.0 |
| C23 | 340.00 | 342.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 54.89 | 50.0 | 10.0 |
| ns4 | 342.00 | 343.30 | ns4 | 40.00 | 40.00 | 1.00 | 56.20 | - | --- |
| C24 | 343.30 | 345.30 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 58.30 | 50.0 | 10.0 |
| C26 | 345.30 | 347.30 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 60.33 | 10.0 | 30.0 |
| C27fr | 347.30 | 349.30 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 62.30 | --- | --- |
| C28fr | 349.30 | 351.30 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 64.27 | --- | --- |
| C29fr | 351.30 | 353.30 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 66.24 | --- | --- |

Table 1-12. Data for samples from core hole 16, Peabody Natural Gas LLC, PNG 33-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 5.0 | 3 | 297.50 | 297.50 | 49.58 | 49.58 | 0.83 | 49.58 | 49.58 |
| C2 | 2.0 | 3 | 18.00 | 180.00 | 9.00 | 90.00 | 1.00 | --- | --- |
| C2 | 2.0 | 4 | 219.00 | 219.00 | 49.77 | 49.77 | 0.45 | 37.03 | 62.34 |
| C3 | 0.0 | 3 | 21.82 | 218.18 | 9.09 | 90.91 | 0.00 | --- | --- |
| C3 | 0.0 | 3 | 82.00 | 328.00 | 20.00 | 80.00 | 0.00 | 15.97 | 84.03 |
| C4 | 0.0 | 3 | 95.00 | 475.00 | 16.67 | 83.33 | 0.00 | 16.67 | 83.33 |
| C5fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C6fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C7 | 0.0 | 4 | 525.00 | 105.00 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 |
| C8 | 0.0 | 5 | 670.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C9 | 0.0 | 4 | 475.00 | 95.00 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 |
| C10fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C11 | 10.0 | 4 | 527.27 | 52.73 | 89.37 | 8.94 | 1.69 | 89.37 | 8.94 |
| C12 | 0.0 | 4 | 421.43 | 168.57 | 71.43 | 28.57 | 0.00 | 71.43 | 28.57 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C13 | 0.0 | 4 | 472.50 | 157.50 | 75.00 | 25.00 | 0.00 | 75.00 | 25.00 |
| C14fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C15 | 0.0 | 2 | 103.33 | 516.67 | 16.67 | 83.33 | 0.00 | 16.67 | 83.33 |
| C16fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C17 | 10.0 | 3 | 92.00 | 368.00 | 19.57 | 78.30 | 2.13 | 19.57 | 78.30 |
| C18 | 0.0 | 3 | 256.00 | 64.00 | 80.00 | 20.00 | 0.00 | --- | --- |
| C18 | 0.0 | 3 | 25.45 | 254.55 | 9.09 | 90.91 | 0.00 | 46.91 | 53.09 |
| C19 | 10.0 | 3 | 92.86 | 557.14 | 14.07 | 84.42 | 1.52 | 14.07 | 84.42 |
| C20 | 5.0 | 3 | 129.00 | 516.00 | 19.85 | 79.38 | 0.77 | 19.85 | 79.38 |
| C21 | 0.0 | 3 | 177.14 | 442.86 | 28.57 | 71.43 | 0.00 | 28.57 | 71.43 |
| C22 | 0.0 | 2 | 54.55 | 545.45 | 9.09 | 90.91 | 0.00 | 9.09 | 90.91 |
| C23 | 0.0 | 4 | 500.00 | 100.00 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C24 | 0.0 | 4 | 533.33 | 106.67 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 |
| C26 | 0.0 | 3 | 155.00 | 465.00 | 25.00 | 75.00 | 0.00 | 25.00 | 75.00 |
| C27fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C28fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C29fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |

Table 1-12. Data for samples from core hole 16, Peabody Natural Gas LLC, PNG 33-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparen t rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 0.83 | 30 | 33.33 | 33.33 | 3.19 | SubC | --- |
| C2 | --- | 50 | 20.00 | --- | --- | --- | --- |
| C2 | 0.63 | 20 | 50.00 | 40.63 | 2.26 | --- | --- |
| C3 | --- | 30 | 33.33 | --- | --- | --- | --- |
| C3 | 0.00 | 30 | 33.33 | 33.33 | 2.10 | --- | --- |
| C4 | 0.00 | 30 | 33.33 | 33.33 | 3.34 | --- | Highly fragmented sample. |
| C5fr | --- | --- | --- | --- | 2.07 | --- | Sample too fragmented to describe. |
| C6fr | --- | --- | --- | --- | 2.27 | --- | Sample too fragmented to describe. |
| C7 | 0.00 | 10 | 100.00 | 100.00 | 2.45 | --- | Highly fragmented sample. |
| C8 | 0.00 | 10 | 100.00 | 100.00 | 2.83 | SubC | --- |
| ns1 | --- | --- | --- | --- | --- | --- | Bag sample taken. |
| C9 | 0.00 | 10 | 100.00 | 100.00 | 1.84 | --- | Highly fragmented sample. |
| C10fr | --- | --- | --- | --- | 3.84 | --- | Sample too fragmented to describe. |
| C11 | 1.69 | 10 | 100.00 | 100.00 | 1.37 | --- | --- |
| C12 | 0.00 | 10 | 100.00 | 100.00 | 1.22 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | --- | Top 2.5 ft lost during coring, bottom 0.3 ft is bag sample. |
| C13 | 0.00 | 10 | 100.00 | 100.00 | 2.99 | SubC | Highly fragmented sample. |
| C14fr | --- | --- | --- | --- | 3.00 | --- | Sample too fragmented to describe. |
| C15 | 0.00 | 20 | 50.00 | 50.00 | 2.94 | --- | Highly fragmented sample. |
| C16fr | --- | --- | --- | --- | 2.40 | --- | Sample too fragmented to describe. |
| ns3 | --- | --- | --- | --- | --- | --- | Top 4.7 ft lost during coring, bottom $1 \mathrm{ft} \mathrm{is} \mathrm{bag} \mathrm{sample}$. |
| C17 | 2.13 | 10 | 100.00 | 100.00 | 1.98 | SubC | Highly fragmented sample. |
| C18 | --- | 30 | 33.33 | --- | --- | --- | --- |
| C18 | 0.00 | 30 | 33.33 | 33.33 | 2.33 | --- | --- |
| C19 | 1.52 | 20 | 50.00 | 50.00 | 2.59 | --- | --- |
| C20 | 0.77 | 5 | 200.00 | 200.00 | 2.98 | --- | --- |
| C21 | 0.00 | 10 | 100.00 | 100.00 | 2.84 | --- | --- |
| C22 | 0.00 | 30 | 33.33 | 33.33 | 2.96 | --- | --- |
| C23 | 0.00 | 30 | 33.33 | 33.33 | 3.04 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | Bag sample taken. |
| C24 | 0.00 | --- | --- | --- | 2.68 | SubC | Highly fragmented sample. |
| C26 | 0.00 | 10 | 100.00 | 100.00 | 2.36 | --- | --- |
| C27fr | --- | --- | --- | --- | 1.64 | --- | Sample too fragmented to describe. |
| C28fr | --- | --- | --- | --- | 1.57 | --- | Sample too fragmented to describe. |
| C29fr | --- | --- | --- | --- | 2.40 | --- | Sample too fragmented to describe. |

Table 1-13. Data for samples from core hole 17, Peabody Natural Gas LLC, PNG 31-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| A1 | 252.00 | 254.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 1.94 | 1.0 |
| A2 | 254.00 | 256.00 | middle and lower Wyodak | 55.00 | 55.00 | 1.00 | 3.74 | 4.0 |
| A7 | 256.00 | 258.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 5.64 | 4.0 |
| A9 | 258.00 | 260.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 7.35 | 10.0 |
| A10 | 260.00 | 262.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 9.32 | 4.0 |
| A11 | 262.00 | 264.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 11.29 | 5.0 |
| A12 | 264.00 | 266.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 13.22 | 10.0 |
| ns1 | 266.00 | 267.00 | ns1 | 30.50 | 30.50 | 1.00 | 14.22 | --- |
| A13 | 267.00 | 269.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 16.06 | 2.0 |
| A14 | 269.00 | 271.00 | middle and lower Wyodak | 55.00 | 55.00 | 1.00 | 17.86 | 2.0 |
| A15 | 271.00 | 273.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 19.70 | 3.0 |
| A16 | 273.00 | 275.00 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 21.80 | 3.0 |
| A17 | 275.00 | --- | middle and lower Wyodak | 50 | --- | 0.84 | 23.44 | 3.0 |
| A17 | --- | 277.00 | middle and lower Wyodak | 9.50 | 59.50 | 0.16 | 23.75 | 20.0 |
| A18 | 277.00 | 279.00 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 25.85 | 20.0 |
| A19 | 279.00 | 281.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 27.82 | 8.0 |
| ns2 | 281.00 | 282.00 | ns2 | 30.50 | 30.50 | 1.00 | 28.82 | --- |
| A20 | 282.00 | 284.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 30.69 | 4.0 |
| A21 | 284.00 | 286.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 32.66 | 3.0 |
| A22 | 286.00 | 288.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 34.56 | 5.0 |
| A23 | 288.00 | --- | middle and lower Wyodak | 39 | --- | 0.63 | 35.84 | 15.0 |
| A23 | --- | 290.00 | middle and lower Wyodak | 23.00 | 62.00 | 0.37 | 36.60 | 2.0 |
| A24 | 290.00 | 292.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 38.44 | 20.0 |
| A25 | 292.00 | 294.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 40.31 | 8.0 |
| A26 | 294.00 | 296.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 42.24 | 8.0 |
| ns3 | 296.00 | 297.00 | ns3 | 30.50 | 30.50 | 1.00 | 43.24 | --- |
| 48 | 297.00 | --- | middle and lower Wyodak | 25 | --- | 0.45 | 44.06 | 10.0 |
| 48 | --- | --- | middle and lower Wyodak | 3 | --- | 0.05 | 44.16 | 0.0 |
| 48 | --- | 299.00 | middle and lower Wyodak | 28.00 | 56.00 | 0.50 | 45.08 | 10.0 |
| 49 | 299.00 | 301.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 46.95 | 5.0 |
| 50 | 301.00 | 303.00 | middle and lower Wyodak | 65.00 | 65.00 | 1.00 | 49.08 | 8.0 |
| 51 | 303.00 | 305.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 50.95 | 15.0 |
| 52 | 305.00 | --- | middle and lower Wyodak | 23 | --- | 0.37 | 51.71 | 2.0 |
| 52 | --- | 307.00 | middle and lower Wyodak | 39.00 | 62.00 | 0.63 | 52.99 | 10.0 |
| 53 | 307.00 | 309.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 54.92 | 20.0 |
| 54 | 309.00 | 311.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 56.86 | 10.0 |
| 55 | 311.00 | 313.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 58.76 | 8.0 |
| 57 | 313.00 | 315.00 | middle and lower Wyodak | 52.00 | 52.00 | 1.00 | 60.47 | 3.0 |
| 58 | 315.00 | 317.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 62.34 | 15.0 |
| 59 | 317.00 | 319.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 64.30 | 8.0 |
| 61 | 319.00 | --- | middle and lower Wyodak | 47 | --- | 0.78 | 65.85 | 10.0 |
| 61 | --- | 321.00 | middle and lower Wyodak | 13.00 | 60.00 | 0.22 | 66.27 | 130.0 |
| 62 | 321.00 | 323.00 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 68.34 | 20.0 |
| 63 | 323.00 | 325.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 70.31 | 10.0 |
| ns4 | 325.00 | 326.30 | ns4 | 40.00 | 40.00 | 1.00 | 71.62 | --- |
| 64 | 326.30 | 328.30 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 73.72 | 5.0 |
| 66 | 328.30 | --- | middle and lower Wyodak | 44 | --- | 0.73 | 75.16 | 7.0 |
| 66 | --- | 330.30 | middle and lower Wyodak | 16.00 | 60.00 | 0.27 | 75.69 | 2.0 |
| 67 | 330.30 | --- | middle and lower Wyodak | 50 | --- | 0.83 | 77.33 | 7.0 |
| 67 | --- | 332.30 | middle and lower Wyodak | 10.00 | 60.00 | 0.17 | 77.66 | 100.0 |
| 68 | 332.30 | --- | middle and lower Wyodak | 39 | --- | 0.64 | 78.94 | 10.0 |
| 68 | --- | --- | middle and lower Wyodak | 1 | --- | 0.02 | 78.97 | 0.0 |
| 68 | --- | 334.30 | middle and lower Wyodak | 21.00 | 61.00 | 0.34 | 79.66 | 3.0 |

Table 1-13. Data for samples from core hole 17, Peabody Natural Gas LLC, PNG 31-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain thickness (CuVT) (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 50.0 | 1.0 | 1 | 53.55 | 535.45 | 9.08 | 90.76 | 0.17 | 9.08 |
| A2 | 20.0 | 0.0 | 2 | 150.00 | 400.00 | 27.27 | 72.73 | 0.00 | 27.27 |
| A7 | 15.0 | 0.0 | 2 | 136.47 | 443.53 | 23.53 | 76.47 | 0.00 | 23.53 |
| A9 | 20.0 | 0.0 | 3 | 185.71 | 334.29 | 35.71 | 64.29 | 0.00 | 35.71 |
| A10 | 15.0 | 10.0 | 2 | 173.53 | 416.47 | 28.92 | 69.41 | 1.67 | 28.92 |
| A11 | 25.0 | 5.0 | 3 | 148.75 | 446.25 | 24.79 | 74.38 | 0.83 | 24.79 |
| A12 | 10.0 | 2.0 | 3 | 294.00 | 294.00 | 49.83 | 49.83 | 0.34 | 49.83 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | -- |
| A13 | 20.0 | 4.0 | 2 | 69.50 | 486.50 | 12.41 | 86.88 | 0.71 | 12.41 |
| A14 | 30.0 | 1.0 | 1 | 219.60 | 329.40 | 39.93 | 59.89 | 0.18 | 39.93 |
| A15 | 30.0 | 2.0 | 1 | 223.20 | 334.80 | 39.86 | 59.79 | 0.36 | 39.86 |
| A16 | 10.0 | 5.0 | 2 | 282.22 | 352.78 | 44.10 | 55.12 | 0.78 | 44.10 |
| A17 | 15.0 | 3.0 | 2 | 94.67 | 402.33 | 18.93 | 80.47 | 0.60 | --- |
| A17 | 5.0 | 3.0 | 3 | 73.60 | 18.40 | 77.47 | 19.37 | 3.16 | 28.28 |
| A18 | 5.0 | 2.0 | 3 | 261.00 | 377.00 | 40.78 | 58.91 | 0.31 | 40.78 |
| A19 | 20.0 | 1.0 | 3 | 119.80 | 479.20 | 19.97 | 79.87 | 0.17 | 19.97 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | -- |
| A20 | 10.0 | 3.0 | 2 | 236.25 | 330.75 | 41.45 | 58.03 | 0.53 | 41.45 |
| A21 | 8.0 | 10.0 | 2 | 295.00 | 295.00 | 49.17 | 49.17 | 1.67 | 49.17 |
| A22 | 10.0 | 8.0 | 3 | 254.22 | 317.78 | 43.83 | 54.79 | 1.38 | 43.83 |
| A23 | 15.0 | 5.0 | 3 | 192.50 | 192.50 | 49.36 | 49.36 | 1.28 | -- |
| A23 | 20.0 | 2.0 | 2 | 32.57 | 195.43 | 14.16 | 84.97 | 0.87 | 36.30 |
| A24 | 15.0 | 10.0 | 3 | 305.56 | 244.44 | 54.56 | 43.65 | 1.79 | 54.56 |
| A25 | 10.0 | 5.0 | 3 | 188.33 | 376.67 | 33.04 | 66.08 | 0.88 | 33.04 |
| A26 | 5.0 | 8.0 | 3 | 304.86 | 277.14 | 51.67 | 46.97 | 1.36 | 51.67 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 48 | 8.0 | 5.0 | 3 | 142.92 | 102.08 | 57.17 | 40.83 | 2.00 | --- |
| 48 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -- |
| 48 | 8.0 | 5.0 | 3 | 160.42 | 114.58 | 57.29 | 40.92 | 1.79 | 54.17 |
| 49 | 15.0 | 30.0 | 3 | 216.00 | 324.00 | 37.89 | 56.84 | 5.26 | 37.89 |
| 50 | 8.0 | 20.0 | 3 | 288.75 | 341.25 | 44.42 | 52.50 | 3.08 | 44.42 |
| 51 | 5.0 | 20.0 | 3 | 412.50 | 137.50 | 72.37 | 24.12 | 3.51 | 72.37 |
| 52 | 20.0 | 10.0 | 2 | 27.50 | 192.50 | 11.96 | 83.70 | 4.35 | --- |
| 52 | 5.0 | 25.0 | 3 | 219.00 | 146.00 | 56.15 | 37.44 | 6.41 | 39.76 |
| 53 | 5.0 | 40.0 | 3 | 246.55 | 303.45 | 41.79 | 51.43 | 6.78 | 41.79 |
| 54 | 5.0 | 20.0 | 3 | 332.50 | 237.50 | 56.36 | 40.25 | 3.39 | 56.36 |
| 55 | 10.0 | 5.0 | 3 | 191.67 | 383.33 | 33.05 | 66.09 | 0.86 | 33.05 |
| 57 | 10.0 | 5.0 | 2 | 206.00 | 309.00 | 39.62 | 59.42 | 0.96 | 39.62 |
| 58 | 10.0 | 10.0 | 3 | 263.53 | 296.47 | 46.23 | 52.01 | 1.75 | 46.23 |
| 59 | 15.0 | 15.0 | 3 | 265.91 | 319.09 | 44.32 | 53.18 | 2.50 | 44.32 |
| 61 | 10.0 | 50.0 | 3 | 224.00 | 196.00 | 47.66 | 41.70 | 10.64 | --- |
| 61 | 0.0 | 0.0 | 5 | 130.00 | 0.00 | 100.00 | 0.00 | 0.00 | 59.00 |
| 62 | 5.0 | 5.0 | 3 | 343.75 | 281.25 | 54.56 | 44.64 | 0.79 | 54.56 |
| 63 | 10.0 | 0.0 | 3 | 300.00 | 300.00 | 50.00 | 50.00 | 0.00 | 50.00 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 64 | 8.0 | 0.0 | 3 | 247.74 | 392.26 | 38.71 | 61.29 | 0.00 | 38.71 |
| 66 | 8.0 | 0.0 | 3 | 165.00 | 275.00 | 37.50 | 62.50 | 0.00 | --- |
| 66 | 15.0 | 0.0 | 2 | 35.56 | 124.44 | 22.22 | 77.78 | 0.00 | 33.43 |
| 67 | 10.0 | 0.0 | 3 | 147.06 | 352.94 | 29.41 | 70.59 | 0.00 | --- |
| 67 | 0.0 | 0.0 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | 41.18 |
| 68 | 8.0 | 30.0 | 3 | 180.00 | 180.00 | 46.15 | 46.15 | 7.69 | --- |
| 68 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- |
| 68 | 5.0 | 0.0 | 2 | 105.00 | 105.00 | 50.00 | 50.00 | 0.00 | 46.72 |

Table 1-13. Data for samples from core hole 17, Peabody Natural Gas LLC, PNG 31-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparen t rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 90.76 | 0.17 | 40 | 25.00 | 25.00 | 5.27 | SubC | --- |
| A2 | 72.73 | 0.00 | 30 | 33.33 | 33.33 | 7.92 | --- | --- |
| A7 | 76.47 | 0.00 | 9 | 111.11 | 111.11 | 10.10 | --- | --- |
| A9 | 64.29 | 0.00 | 25 | 40.00 | 40.00 | 10.04 | --- | --- |
| A10 | 69.41 | 1.67 | 28 | 35.71 | 35.71 | 8.85 | --- | --- |
| A11 | 74.38 | 0.83 | 25 | 40.00 | 40.00 | 9.40 | --- | --- |
| A12 | 49.83 | 0.34 | 30 | 33.33 | 33.33 | 7.62 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| A13 | 86.88 | 0.71 | 32 | 31.25 | 31.25 | 8.49 | --- | --- |
| A14 | 59.89 | 0.18 | 23 | 43.48 | 43.48 | 8.74 | --- | --- |
| A15 | 59.79 | 0.36 | 35 | 28.57 | 28.57 | 10.66 | SubC | --- |
| A16 | 55.12 | 0.78 | 40 | 25.00 | 25.00 | 10.00 | --- | --- |
| A17 | --- | --- | 25 | 40.00 | --- | --- | --- | White clay on cleat. |
| A17 | 70.71 | 1.01 | 25 | 40.00 | 40.00 | 9.98 | --- | White clay on cleat. |
| A18 | 58.91 | 0.31 | 21 | 47.62 | 47.62 | 9.55 | --- | --- |
| A19 | 79.87 | 0.17 | 40 | 25.00 | 25.00 | 7.82 | --- | White clay on cleat. |
| ns2 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| A20 | 58.03 | 0.53 | 15 | 66.67 | 66.67 | 11.11 | --- | --- |
| A21 | 49.17 | 1.67 | 25 | 40.00 | 40.00 | 9.99 | --- | --- |
| A22 | 54.79 | 1.38 | 25 | 40.00 | 40.00 | 11.64 | --- | --- |
| A23 | --- | --- | 34 | 29.41 | --- | --- | --- | --- |
| A23 | 62.57 | 1.13 | 34 | 29.41 | 29.41 | 10.35 | --- | --- |
| A24 | 43.65 | 1.79 | 9 | 111.11 | 111.11 | 10.15 | --- | --- |
| A25 | 66.08 | 0.88 | 25 | 40.00 | 40.00 | 12.35 | SubB | --- |
| A26 | 46.97 | 1.36 | 25 | 40.00 | 40.00 | 11.35 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 48 | --- | --- | 50 | 20.00 | --- | --- | --- | --- |
| 48 | --- | --- | 50 | 20.00 | --- | --- | --- | High ash. |
| 48 | 38.69 | 1.79 | 50 | 20.00 | 20.00 | 10.83 | --- | --- |
| 49 | 56.84 | 5.26 | 25 | 40.00 | 40.00 | 10.94 | --- | --- |
| 50 | 52.50 | 3.08 | 55 | 18.18 | 18.18 | 6.32 | --- | --- |
| 51 | 24.12 | 3.51 | 20 | 50.00 | 50.00 | 10.49 | --- | --- |
| 52 | --- | --- | 35 | 28.57 | --- | --- | --- | --- |
| 52 | 54.60 | 5.65 | 35 | 28.57 | 28.57 | 11.54 | --- | --- |
| 53 | 51.43 | 6.78 | 30 | 33.33 | 33.33 | 12.03 | --- | Fusain band 35 mm thick. |
| 54 | 40.25 | 3.39 | 18 | 55.56 | 55.56 | 11.11 | --- | --- |
| 55 | 66.09 | 0.86 | 32 | 31.25 | 31.25 | 12.96 | --- | --- |
| 57 | 59.42 | 0.96 | 25 | 40.00 | 40.00 | 9.42 | SubC | Highly fractured sample. |
| 58 | 52.01 | 1.75 | 35 | 28.57 | 28.57 | 11.67 | --- | --- |
| 59 | 53.18 | 2.50 | 32 | 31.25 | 31.25 | 12.01 | --- | --- |
| 61 | --- | --- | 30 | 33.33 | --- | --- | --- | Fusain band 50 mm thick. |
| 61 | 32.67 | 8.33 | 30 | 33.33 | 33.33 | 10.51 | --- | --- |
| 62 | 44.64 | 0.79 | 25 | 40.00 | 40.00 | 11.17 | --- | --- |
| 63 | 50.00 | 0.00 | 40 | 25.00 | 25.00 | 12.45 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | --- | No sample. |
| 64 | 61.29 | 0.00 | 50 | 20.00 | 20.00 | 13.08 | --- | Sooty appearance. |
| 66 | --- | --- | 20 | 50.00 | --- | --- | --- | Sooty appearance. |
| 66 | 66.57 | 0.00 | 20 | 50.00 | 50.00 | 13.01 | --- | --- |
| 67 | --- | --- | 40 | 25.00 | --- | --- | --- | Slightly sooty appearance. |
| 67 | 58.82 | 0.00 | 40 | 25.00 | 25.00 | 12.02 | --- | --- |
| 68 | --- | --- | 40 | 25.00 | --- | --- | --- | Fusain band 30 mm thick. |
| 68 | --- | --- | 40 | 25.00 | --- | --- | --- | High ash content. |
| 68 | 46.72 | 4.92 | 40 | 25.00 | 25.00 | 12.03 | --- | White clay on cleat. |

Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| B8 | 322.00 | 324.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 2.03 | 10.0 | 10.0 |
| B9 | 324.00 | 326.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 4.07 | 5.0 | 10.0 |
| ns1 | 326.00 | 327.00 | ns 1 | 30.50 | 30.50 | 1.00 | 5.07 | --- | --- |
| B10 | 327.00 | 329.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 7.04 | 4.0 | 15.0 |
| B11 | 329.00 | 331.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 9.01 | 15.0 | 5.0 |
| B12 | 331.00 | 333.00 | middle and lower Wyodak | 66.00 | 66.00 | 1.00 | 11.17 | 15.0 | 10.0 |
| B13 | 333.00 | --- | middle and lower Wyodak | 52.00 | --- | 0.85 | 12.88 | 10.0 | 20.0 |
| B13 | --- | 335.00 | middle and lower Wyodak | 9.00 | 61.00 | 0.15 | 13.17 | 20.0 | 5.0 |
| B14 | 335.00 | 337.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 15.11 | 25.0 | 5.0 |
| B15 | 337.00 | --- | middle and lower Wyodak | 12.00 | --- | 0.20 | 15.50 | 20.0 | 5.0 |
| B15 | --- | 339.00 | middle and lower Wyodak | 47.00 | 59.00 | 0.80 | 17.04 | 5.0 | 20.0 |
| B16 | 339.00 | 341.00 | middle and lower Wyodak | 59.00 | 59.00 | 1.00 | 18.98 | 30.0 | 5.0 |
| ns2 | 341.00 | 342.00 | ns2 | 30.50 | 30.50 | 1.00 | 19.98 | --- | --- |
| B17 | 342.00 | --- | middle and lower Wyodak | 15.00 | --- | 0.26 | 20.47 | 140.0 | 0.0 |
| B17 | --- | --- | middle and lower Wyodak | 10.00 | --- | 0.18 | 20.80 | 1.0 | 20.0 |
| B17 | --- | 344.00 | middle and lower Wyodak | 32.00 | 57.00 | 0.56 | 21.85 | 310.0 | 0.0 |
| B18 | 344.00 | 346.00 | middle and lower Wyodak | 56.00 | 56.00 | 1.00 | 23.69 | 10.0 | 15.0 |
| B19 | 346.00 | --- | middle and lower Wyodak | 22.00 | --- | 0.38 | 24.41 | 215.0 | 0.0 |
| B19 | --- | 348.00 | middle and lower Wyodak | 36.00 | 58.00 | 0.62 | 25.59 | 50.0 | 5.0 |
| B20 | 348.00 | --- | middle and lower Wyodak | 36.00 | --- | 0.55 | 26.77 | 12.0 | 5.0 |
| B20 | --- | 350.00 | middle and lower Wyodak | 30.00 | 66.00 | 0.45 | 27.76 | 2.0 | 15.0 |
| B21 | 350.00 | --- | middle and lower Wyodak | 47.00 | --- | 0.84 | 29.30 | 10.0 | 20.0 |
| B21 | --- | 352.00 | middle and lower Wyodak | 9.00 | 56.00 | 0.16 | 29.59 | 90.0 | 0.0 |
| B22 | 352.00 | --- | middle and lower Wyodak | 10.00 | --- | 0.17 | 29.92 | 100.0 | 0.0 |
| B22 | --- | 354.00 | middle and lower Wyodak | 49.00 | 59.00 | 0.83 | 31.53 | 3.0 | 20.0 |
| B23 | 354.00 | --- | middle and lower Wyodak | 41.00 | --- | 0.69 | 32.87 | 20.0 | 10.0 |
| B23 | --- | 356.00 | middle and lower Wyodak | 18.00 | 59.00 | 0.31 | 33.46 | 15.0 | 5.0 |
| ns3 | 356.00 | 357.00 | ns3 | 30.50 | 30.50 | 1.00 | 34.47 | --- | -- |
| B24 | 357.00 | 359.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 36.37 | 3.0 | 20.0 |
| A3 | 359.00 | 361.00 | middle and lower Wyodak | 57.00 | 57.00 | 1.00 | 38.24 | 5.0 | 25.0 |
| A5 | 361.00 | 363.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 40.14 | 8.0 | 15.0 |
| A6 | 363.00 | 365.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 42.11 | 5.0 | 10.0 |
| A8 | 365.00 | --- | middle and lower Wyodak | 54.00 | --- | 0.83 | 43.88 | 15.0 | 10.0 |
| A8 | --- | 367.00 | middle and lower Wyodak | 11.00 | 65.00 | 0.17 | 44.24 | 110.0 | 0.0 |
| 6 | 367.00 | 368.35 | middle and lower Wyodak | 41.00 | 41.00 | 0.62 | 45.59 | 2.0 | 20.0 |
| 6 | 368.35 | 369.00 | middle and lower Wyodak | 25.00 | 66.00 | 0.38 | 46.41 | 8.0 | 10.0 |
| 10 | 369.00 | 371.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 48.31 | 10.0 | 10.0 |
| ns4 | 371.00 | 372.00 | ns4 | 30.50 | 30.50 | 1.00 | 49.31 | --- | - |
| 40 | 372.00 | 374.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 51.35 | 15.0 | 5.0 |
| 41 | 374.00 | 376.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 53.38 | 10.0 | 5.0 |
| 42 | 376.00 | 378.00 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 55.38 | 5.0 | 10.0 |
| 43 | 378.00 | 380.00 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 57.45 | 3.0 | 20.0 |
| 44 | 380.00 | --- | middle and lower Wyodak | 10.00 | --- | 0.16 | 57.78 | 2.0 | 20.0 |
| 44 | --- | --- | middle and lower Wyodak | 28.00 | --- | 0.45 | 58.69 | 280.0 | 0.0 |
| 44 | --- | 382.00 | middle and lower Wyodak | 24.00 | 62.00 | 0.39 | 59.48 | 2.0 | 20.0 |
| 45 | 382.00 | --- | middle and lower Wyodak | 20.00 | --- | 0.31 | 60.14 | 5.0 | 10.0 |
| 45 | --- | --- | middle and lower Wyodak | 17.00 | --- | 0.27 | 60.70 | 170.0 | 0.0 |
| 45 | --- | 384.00 | middle and lower Wyodak | 27.00 | 64.00 | 0.42 | 61.58 | 5.0 | 10.0 |
| 46 | 384.00 | --- | middle and lower Wyodak | 28.00 | --- | 0.49 | 62.50 | 5.0 | 15.0 |
| 46 | --- | 386.00 | middle and lower Wyodak | 29.00 | 57.00 | 0.51 | 63.45 | 15.0 | 5.0 |
| ns5 | 386.00 | 387.00 | ns5 | 30.50 | 30.50 | 1.00 | 64.45 | --- | --- |

Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| B8 | 0.0 | 3 | 284.17 | 335.83 | 45.83 | 54.17 | 0.00 | 45.83 | 54.17 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B9 | 8.0 | 3 | 226.67 | 385.33 | 36.56 | 62.15 | 1.29 | 36.56 | 62.15 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B10 | 5.0 | 2 | 247.92 | 347.08 | 41.32 | 57.85 | 0.83 | 41.32 | 57.85 |
| B11 | 4.0 | 3 | 255.43 | 340.57 | 42.57 | 56.76 | 0.67 | 42.57 | 56.76 |
| B12 | 2.0 | 3 | 329.00 | 329.00 | 49.85 | 49.85 | 0.30 | 49.85 | 49.85 |
| B13 | 0.0 | 3 | 113.04 | 406.96 | 21.74 | 78.26 | 0.00 | --- | --- |
| B13 | 0.0 | 3 | 67.50 | 22.50 | 75.00 | 25.00 | 0.00 | 29.60 | 70.40 |
| B14 | 2.0 | 4 | 261.33 | 326.67 | 44.29 | 55.37 | 0.34 | 44.29 | 55.37 |
| B15 | 0.0 | 3 | 60.00 | 60.00 | 50.00 | 50.00 | 0.00 | --- | --- |
| B15 | 20.0 | 3 | 120.00 | 330.00 | 25.53 | 70.21 | 4.26 | 30.51 | 66.10 |
| B16 | 50.0 | 4 | 180.00 | 360.00 | 30.51 | 61.02 | 8.47 | 30.51 | 61.02 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B17 | 10.0 | 5 | 140.00 | 0.00 | 93.33 | 0.00 | 6.67 | --- | --- |
| B17 | 0.0 | 2 | 0.00 | 100.00 | 0.00 | 100.00 | 0.00 | --- | --- |
| B17 | 10.0 | 5 | 310.00 | 0.00 | 96.88 | 0.00 | 3.13 | 78.95 | 17.54 |
| B18 | 5.0 | 3 | 194.25 | 360.75 | 34.69 | 64.42 | 0.89 | 34.69 | 64.42 |
| B19 | 5.0 | 5 | 215.00 | 0.00 | 97.73 | 0.00 | 2.27 | --- | --- |
| B19 | 2.0 | 4 | 223.75 | 134.25 | 62.15 | 37.29 | 0.56 | 75.65 | 23.15 |
| B20 | 5.0 | 3 | 126.79 | 228.21 | 35.22 | 63.39 | 1.39 | --- | --- |
| B20 | 0.0 | 2 | 60.00 | 240.00 | 20.00 | 80.00 | 0.00 | 28.30 | 70.94 |
| B21 | 0.0 | 3 | 128.18 | 341.82 | 27.27 | 72.73 | 0.00 | --- | --- |
| B21 | 0.0 | 5 | 90.00 | 0.00 | 100.00 | 0.00 | 0.00 | 38.96 | 61.04 |
| B22 | 0.0 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- |
| B22 | 2.0 | 2 | 102.74 | 385.26 | 20.97 | 78.63 | 0.41 | 34.36 | 65.30 |
| B23 | 1.0 | 3 | 204.50 | 204.50 | 49.88 | 49.88 | 0.24 | --- | --- |
| B23 | 20.0 | 3 | 120.00 | 40.00 | 66.67 | 22.22 | 11.11 | 55.00 | 41.44 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| B24 | 2.0 | 2 | 236.45 | 341.55 | 40.77 | 58.89 | 0.34 | 40.77 | 58.89 |
| A3 | 0.0 | 3 | 147.78 | 422.22 | 25.93 | 74.07 | 0.00 | 25.93 | 74.07 |
| A5 | 0.0 | 3 | 204.71 | 375.29 | 35.29 | 64.71 | 0.00 | 35.29 | 64.71 |
| A6 | 2.0 | 3 | 208.00 | 390.00 | 34.67 | 65.00 | 0.33 | 34.67 | 65.00 |
| A8 | 5.0 | 3 | 197.11 | 337.89 | 36.50 | 62.57 | 0.93 | --- | --- |
| A8 | 0.0 | 5 | 110.00 | 0.00 | 100.00 | 0.00 | 0.00 | 47.25 | 51.98 |
| 6 | 2.0 | 2 | 45.33 | 362.67 | 11.06 | 88.46 | 0.49 | --- | --- |
| 6 | 10.0 | 3 | 120.00 | 120.00 | 48.00 | 48.00 | 4.00 | 25.05 | 73.13 |
| 10 | 5.0 | 3 | 265.38 | 309.62 | 45.76 | 53.38 | 0.86 | 45.76 | 53.38 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 40 | 5.0 | 3 | 294.13 | 320.87 | 47.44 | 51.75 | 0.81 | 47.44 | 51.75 |
| 41 | 3.0 | 3 | 359.92 | 257.08 | 58.05 | 41.47 | 0.48 | 58.05 | 41.47 |
| 42 | 5.0 | 3 | 277.29 | 327.71 | 45.46 | 53.72 | 0.82 | 45.46 | 53.72 |
| 43 | 2.0 | 2 | 171.27 | 456.73 | 27.19 | 72.50 | 0.32 | 27.19 | 72.50 |
| 44 | 0.0 | 2 | 40.00 | 60.00 | 40.00 | 60.00 | 0.00 | --- | --- |
| 44 | 0.0 | 5 | 280.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- |
| 44 | 0.0 | 2 | 80.00 | 160.00 | 33.33 | 66.67 | 0.00 | 64.52 | 35.48 |
| 45 | 0.0 | 3 | 111.11 | 88.89 | 55.56 | 44.44 | 0.00 | --- | --- |
| 45 | 0.0 | 5 | 170.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- |
| 45 | 0.0 | 3 | 81.00 | 189.00 | 30.00 | 70.00 | 0.00 | 56.58 | 43.42 |
| 46 | 5.0 | 3 | 84.62 | 190.38 | 30.22 | 67.99 | 1.79 | --- | --- |
| 46 | 5.0 | 3 | 178.13 | 106.88 | 61.42 | 36.85 | 1.72 | 46.09 | 52.15 |
| ns5 | --- | --- | --- | --- | --- | --- | - | --- | --- |

Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B8 | 0.00 | 35 | 28.57 | 28.57 | 11.65 | --- | --- |
| B9 | 1.29 | 55 | 18.18 | 18.18 | 12.74 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | No sample. |
| B10 | 0.83 | 40 | 25.00 | 25.00 | 15.18 | --- | , |
| B11 | 0.67 | 25 | 40.00 | 40.00 | 14.24 | --- | --- |
| B12 | 0.30 | 44 | 22.73 | 22.73 | 13.30 | --- | --- |
| B13 | --- | 25 | 40.00 | --- | --- | --- | Pyrite bleb, 1 cm thick. |
| B13 | 0.00 | 25 | 40.00 | 40.00 | 13.34 | --- | --- |
| B14 | 0.34 | 35 | 28.57 | 28.57 | 14.77 | --- | --- |
| B15 | --- | 19 | 52.63 | --- | --- | --- | --- |
| B15 | 3.39 | 19 | 52.63 | 52.63 | 13.50 | --- | Sooty with fusain. |
| B16 | 8.47 | 30 | 33.33 | 33.33 | 12.81 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | --- | No sample. |
| B17 | --- | 50 | 20.00 | --- | --- | --- | --- |
| B17 | --- | 50 | 20.00 | --- | --- | --- | --- |
| B17 | 3.51 | 50 | 20.00 | 20.00 | 15.07 | --- | Sooty . |
| B18 | 0.89 | 25 | 40.00 | 40.00 | 15.50 | SubC | --- |
| B19 | --- | 45 | 22.22 | --- | --- | --- | --- |
| B19 | 1.21 | 40 | 25.00 | 23.95 | 15.52 | --- | --- |
| B20 | --- | 50 | 20.00 | --- | --- | --- | --- |
| B20 | 0.76 | 50 | 20.00 | 20.00 | 13.53 | --- | --- |
| B21 | --- | 35 | 28.57 | --- | --- | --- | --- |
| B21 | 0.00 | 35 | 28.57 | 28.57 | 13.80 | --- | --- |
| B22 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B22 | 0.34 | 20 | 50.00 | 50.00 | 14.82 | --- | --- |
| B23 | --- | 30 | 33.33 | --- | --- | --- | --- |
| B23 | 3.56 | 30 | 33.33 | 33.33 | 15.02 | --- | Sooty. |
| ns3 | --- | --- | --- | --- | --- | --- | No sample. |
| B24 | 0.34 | 22 | 45.45 | 45.45 | 16.69 | --- | --- |
| A3 | 0.00 | 28 | 35.71 | 35.71 | 16.30 | --- | --- |
| A5 | 0.00 | 35 | 28.57 | 28.57 | 10.59 | --- | White clay on cleat. |
| A6 | 0.33 | 22 | 45.45 | 45.45 | 17.15 | --- | Wood at base, 70 mm thick. |
| A8 | --- | 70 | 14.29 | --- | --- | --- | --- |
| A8 | 0.77 | 70 | 14.29 | 14.29 | 13.84 | --- | --- |
| 6 | --- | 38 | 26.32 | --- | --- | --- | Dull, hard. |
| 6 | 1.82 | 38 | 26.32 | 26.32 | 15.49 | --- | Sooty. |
| 10 | 0.86 | 40 | 25.00 | 25.00 | 15.71 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | --- | No sample. |
| 40 | 0.81 | 15 | 66.67 | 66.67 | 15.99 | --- | --- |
| 41 | 0.48 | 35 | 28.57 | 28.57 | 15.59 | SubC | --- |
| 42 | 0.82 | 20 | 50.00 | 50.00 | 16.57 | --- | --- |
| 43 | 0.32 | 25 | 40.00 | 40.00 | 14.41 | --- | --- |
| 44 | --- | 40 | 25.00 | --- | --- | --- | --- |
| 44 | --- | 40 | 25.00 | --- | --- | --- | --- |
| 44 | 0.00 | 40 | 25.00 | 25.00 | 15.57 | --- | --- |
| 45 | --- | 40 | 25.00 | --- | --- | --- | --- |
| 45 | --- | 40 | 25.00 | --- | --- | --- | --- |
| 45 | 0.00 | 40 | 25.00 | 25.00 | 14.00 | --- | --- |
| 46 | --- | 22 | 45.45 | --- | --- | --- | --- |
| 46 | 1.75 | 22 | 45.45 | 45.45 | 13.22 | --- | --- |
| ns5 | --- | --- | --- | --- | --- | --- | No sample. |

Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Appro dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| 47 | 387.00 | 389.00 | middle and lower Wyodak | 64.00 | 64.00 | 1.00 | 66.55 | 3.0 | 20.0 |
| 56 | 389.00 | 391.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 68.59 | 3.0 | 10.0 |
| 65 | 391.00 | 393.00 | middle and lower Wyodak | 62.00 | 62.00 | 1.00 | 70.62 | 8.0 | 10.0 |
| 69 | 393.00 | --- | middle and lower Wyodak | 38.00 | --- | 0.63 | 71.87 | 1.0 | 30.0 |
| 69 | --- | --- | middle and lower Wyodak | 1.00 | --- | 0.02 | 71.90 | 0.0 | 0.0 |
| 69 | --- | 395.00 | middle and lower Wyodak | 21.00 | 60.00 | 0.35 | 72.59 | 5.0 | 10.0 |
| 70 | 395.00 | --- | middle and lower Wyodak | 9.00 | --- | 0.16 | 72.88 | 20.0 | 5.0 |
| 70 | --- | --- | middle and lower Wyodak | 16.00 | --- | 0.28 | 73.41 | 0.0 | 0.0 |
| 70 | --- | 397.00 | middle and lower Wyodak | 32.00 | 57.00 | 0.56 | 74.46 | 15.0 | 5.0 |
| 71 | 397.00 | 399.00 | middle and lower Wyodak | 33.00 | 33.00 | 1.00 | 75.54 | 8.0 | 8.0 |
| 72 | 399.00 | 401.00 | middle and lower Wyodak | 61.00 | 61.00 | 1.00 | 77.54 | 3.0 | 15.0 |
| 73 | 401.00 | --- | middle and lower Wyodak | 15.00 | --- | 0.33 | 78.03 | 2.0 | 15.0 |
| 73 | --- | 403.00 | middle and lower Wyodak | 31.00 | 46.00 | 0.67 | 79.05 | 10.0 | 5.0 |
| 74 | 403.00 | --- | middle and lower Wyodak | 42.00 | --- | 0.69 | 80.43 | 5.0 | 10.0 |
| 74 | --- | --- | middle and lower Wyodak | 5.00 | --- | 0.08 | 80.59 | 0.0 | 0.0 |
| 74 | --- | 405.00 | middle and lower Wyodak | 14.00 | 61.00 | 0.23 | 81.05 | 5.0 | 10.0 |
| 75 | 405.00 | --- | middle and lower Wyodak | 40.00 | --- | 0.71 | 82.37 | 20.0 | 5.0 |
| 75 | --- | --- | middle and lower Wyodak | 6.00 | --- | 0.11 | 82.56 | 0.0 | 0.0 |
| 75 | --- | 407.00 | middle and lower Wyodak | 10.00 | 56.00 | 0.18 | 82.89 | 20.0 | 5.0 |

Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 5.0 | 2 | 79.38 | 555.63 | 12.40 | 86.82 | 0.78 | 12.40 | 86.82 |
| 56 | 5.0 | 2 | 223.64 | 391.36 | 36.07 | 63.12 | 0.81 | 36.07 | 63.12 |
| 65 | 10.0 | 3 | 244.00 | 366.00 | 39.35 | 59.03 | 1.61 | 39.35 | 59.03 |
| 69 | 5.0 | 1 | 26.79 | 348.21 | 7.05 | 91.64 | 1.32 | --- | --- |
| 69 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| 69 | 5.0 | 3 | 93.18 | 111.82 | 44.37 | 53.25 | 2.38 | 19.99 | 76.67 |
| 70 | 5.0 | 3 | 28.33 | 56.67 | 31.48 | 62.96 | 5.56 | --- | --- |
| 70 | 160.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- |
| 70 | 3.0 | 3 | 176.11 | 140.89 | 55.03 | 44.03 | 0.94 | 35.87 | 34.66 |
| 71 | 2.0 | 3 | 178.91 | 149.09 | 54.21 | 45.18 | 0.61 | 54.21 | 45.18 |
| 72 | 0.0 | 2 | 213.50 | 396.50 | 35.00 | 65.00 | 0.00 | 35.00 | 65.00 |
| 73 | 0.0 | 2 | 60.00 | 90.00 | 40.00 | 60.00 | 0.00 | --- | --- |
| 73 | 0.0 | 3 | 186.00 | 124.00 | 60.00 | 40.00 | 0.00 | 53.48 | 46.52 |
| 74 | 2.0 | 3 | 185.78 | 232.22 | 44.23 | 55.29 | 0.48 | --- | --- |
| 74 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| 74 | 2.0 | 3 | 61.33 | 76.67 | 43.81 | 54.76 | 1.43 | 40.51 | 50.64 |
| 75 | 5.0 | 3 | 131.67 | 263.33 | 32.92 | 65.83 | 1.25 | --- | --- |
| 75 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| 75 | 0.0 | 3 | 33.33 | 66.67 | 33.33 | 66.67 | 0.00 | 29.46 | 58.93 |

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Table 1-14. Data for samples from core hole 18, Peabody Natural Gas LLC, PNG 35-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 0.78 | 50 | 20.00 | 20.00 | 14.70 | --- | Dull. |
| 56 | 0.81 | 55 | 18.18 | 18.18 | 13.86 | --- | --- |
| 65 | 1.61 | 70 | 14.29 | 14.29 | 14.90 | --- | --- |
| 69 | --- | 30 | 33.33 | --- | --- | --- | --- |
| 69 | --- | 30 | 33.33 | --- | --- | --- | --- |
| 69 | 1.67 | 30 | 33.33 | 33.33 | 14.12 | --- | --- |
| 70 | --- | 35 | 28.57 | --- | --- | --- | --- |
| 70 | --- | 35 | 28.57 | --- | --- | --- | Very minor amounts of vitrain and attritus. |
| 70 | 29.47 | 35 | 28.57 | 28.57 | 15.16 | --- | --- |
| 71 | 0.61 | 45 | 22.22 | 22.22 | 15.87 | --- | --- |
| 72 | 0.00 | 50 | 20.00 | 20.00 | 14.85 | SubC | --- |
| 73 | --- | 35 | 28.57 | --- | --- | --- | Pyrite. |
| 73 | 0.00 | 35 | 28.57 | 28.57 | 15.90 | --- | -- |
| 74 | --- | 40 | 25.00 | --- | --- | --- | --- |
| 74 | --- | 40 | 25.00 | --- | --- | --- | Very minor amount of vitrain. |
| 74 | 0.66 | 40 | 25.00 | 25.00 | 16.28 | --- | , |
| 75 | --- | 35 | 28.57 | --- | --- | --- | --- |
| 75 | --- | 35 | 28.57 | --- | --- | --- | Very minor amount of vitrain. |
| 75 | 0.89 | 35 | 28.57 | 28.57 | 12.68 | --- | --- |

Table 1-15. Data for samples from core hole 19, Barrett Resources Corporation, All Night Creek Unit (ANCU) Iberlin 21-33-4374.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |
| C1 | 1,300.00 | 1,302.00 | Big George | 55.00 | 55.00 | 1.00 | 1.80 |
| C2 | 1,302.00 | 1,304.00 | Big George | 57.00 | 57.00 | 1.00 | 3.67 |
| C3 | 1,304.00 | 1,306.00 | Big George | 37.00 | 37.00 | 1.00 | 4.89 |
| ns1 | 1,306.00 | 1,309.00 | ns1 | 91.00 | 91.00 | 1.00 | 7.87 |
| C5 | 1,309.00 | 1,311.00 | Big George | 49.00 | 49.00 | 1.00 | 9.48 |
| C4 | 1,311.00 | 1,313.00 | Big George | 69.00 | 69.00 | 1.00 | 11.75 |
| ns2 | 1,313.00 | 1,316.00 | ns2 | 91.00 | 91.00 | 1.00 | 14.73 |
| C6 | 1,316.00 | 1,318.00 | Big George | 60.00 | 60.00 | 1.00 | 16.70 |

Table 1-15. Data for samples from core hole 19, Barrett Resources Corporation, All Night Creek Unit (ANCU) Iberlin 21-33-4374.— Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 10.0 | 15.0 | 0.0 | 3 | 275.00 | 275.00 | 50.00 |
| C2 | 8.0 | 25.0 | 8.0 | 3 | 168.60 | 393.40 | 29.58 |
| C3 | 5.0 | 8.0 | 0.0 | 3 | 148.00 | 222.00 | 40.00 |
| ns1 | --- | --- | --- | --- | --- | ---- | --- |
| C5 | 70.0 | 2.0 | 0.0 | 5 | 476.39 | 13.61 | 97.22 |
| C4 | 5.0 | 3.0 | 0.0 | 3 | 483.00 | 207.00 | 70.00 |
| ns2 | --- | --- | --- | --- | --- | ---- | --- |
| C6 | 70.0 | 15.0 | 0.0 | 4 | 494.12 | 105.88 | 82.35 |

Table 1-15. Data for samples from core hole 19, Barrett Resources Corporation, All Night Creek Unit (ANCU) Iberlin 21-33-4374.Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 50.00 | 0.00 | 50.00 | 50.00 | 0.00 | 30 | 33.33 |
| C2 | 69.02 | 1.40 | 29.58 | 69.02 | 1.40 | 10 | 100.00 |
| C3 | 60.00 | 0.00 | 40.00 | 60.00 | 0.00 | 60 | 16.67 |
| ns1 | --- | --- | --- | --- | --- | --- | --- |
| C5 | 2.78 | 0.00 | 97.22 | 2.78 | 0.00 | 30 | 33.33 |
| C4 | 30.00 | 0.00 | 70.00 | 30.00 | 0.00 | 40 | 25.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- |
| C6 | 17.65 | 0.00 | 82.35 | 17.65 | 0.00 | 30 | 33.33 |

Table 1-15. Data for samples from core hole 19, Barrett Resources Corporation, All Night Creek Unit (ANCU) Iberlin 21-33-4374.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister <br> number | Canister average cleat <br> frequency (CaAvCFr) <br> (cleats/m) | Total gas <br> (SCF/ton) | Apparent <br> rank | Comments |
| :--- | ---: | ---: | :--- | :--- |
| C1 | 33.33 | 16.97 | SubB | Bedding at 70 degrees to horizontal. |
| C2 | 100.00 | 14.04 | --- | Fusain band at 44 cm , bedding at 60 degrees to horizontal, kaolinite on cleat. |
| C3 | 16.67 | 16.36 | --- | Bedding at 45 degrees to horizontal. |
| ns1 | --- | --- | --- | Top 2 ft is bag sample, bottom 1 ft was lost during drilling. |
| C5 | 33.33 | 12.92 | --- | Highly fragmented sample. |
| C4 | 25.00 | 15.38 | --- | Vertical wood grain at top, bedding 90 degrees to horizontal. |
| ns2 | --- | -- | --- | Top 1 ft is bag sample, bottom 2 ft was lost during drilling. |
| C6 | 33.33 | 12.95 | --- | High-angle bedding. |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| C-7 | 213.00 | --- | middle and lower Wyodak | 14.00 | ---- | 0.23 | 0.46 | 40.0 |
| C-7 | --- | 215.00 | middle and lower Wyodak | 46.00 | 60.00 | 0.77 | 1.97 | 2.0 |
| C-8 | 215.00 | 217.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 3.94 | 8.0 |
| C-9 | 217.00 | 219.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 5.91 | 10.0 |
| C-10 | 219.00 | 221.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 7.87 | 10.0 |
| C-11 | 221.00 | --- | middle and lower Wyodak | 23.00 | --- | 0.37 | 8.63 | 5.0 |
| C-11 | --- | --- | middle and lower Wyodak | 22.00 | --- | 0.35 | 9.35 | 40.0 |
| C-11 | --- | 223.00 | middle and lower Wyodak | 18.00 | 63.00 | 0.29 | 9.94 | 3.0 |
| C-12 | 223.00 | 225.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 11.91 | 30.0 |
| C-13 | 225.00 | 227.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 13.88 | 4.0 |
| ns1 | 227.00 | 228.00 | ns1 | 30.50 | 30.50 | 1.00 | 14.88 | --- |
| C-14 | 228.00 | 230.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 16.85 | 4.0 |
| C-15 | 230.00 | --- | middle and lower Wyodak | 54.00 | --- | 0.84 | 18.62 | 40.0 |
| C-15 | --- | 232.00 | middle and lower Wyodak | 10.00 | 64.00 | 0.16 | 18.95 | 4.0 |
| C-16 | 232.00 | 234.00 | middle and lower Wyodak | 65.00 | 65.00 | 1.00 | 21.08 | 50.0 |
| C-17 | 234.00 | 236.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 23.05 | 25.0 |
| C-18 | 236.00 | 238.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 25.02 | 2.0 |
| C-19 | 238.00 | 240.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 26.98 | 10.0 |
| C-20 | 240.00 | --- | middle and lower Wyodak | 45.00 | --- | 0.75 | 28.46 | 2.0 |
| C-20 | --- | 242.00 | middle and lower Wyodak | 15.00 | 60.00 | 0.25 | 28.95 | 50.0 |
| ns2 | 242.00 | 243.00 | ns2 | 30.50 | 30.50 | 1.00 | 29.95 | --- |
| C-21 | 243.00 | --- | middle and lower Wyodak | 46.00 | --- | 0.77 | 31.46 | 6.0 |
| C-21 | --- | 245.00 | middle and lower Wyodak | 14.00 | 60.00 | 0.23 | 31.92 | 50.0 |
| C-22 | 245.00 | 247.00 | middle and lower Wyodak | 58.00 | 58.00 | 1.00 | 33.83 | 4.0 |
| C-23 | 247.00 | --- | middle and lower Wyodak | 12.00 | --- | 0.20 | 34.22 | 1.0 |
| C-23 | --- | 249.00 | middle and lower Wyodak | 48.00 | 60.00 | 0.80 | 35.79 | 30.0 |
| C-24 | 249.00 | 251.00 | middle and lower Wyodak | 63.00 | 63.00 | 1.00 | 37.86 | 5.0 |
| C-26 | 251.00 | --- | middle and lower Wyodak | 20.00 | --- | 0.42 | 38.52 | 5.0 |
| C-26 | --- | --- | middle and lower Wyodak | 10.00 | --- | 0.21 | 38.85 | 6.0 |
| C-26 | --- | 253.00 | middle and lower Wyodak | 18.00 | 48.00 | 0.38 | 39.44 | 35.0 |
| C-27 | 253.00 | 255.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 41.40 | 6.0 |
| C-28 | 255.00 | --- | middle and lower Wyodak | 30.00 | --- | 0.50 | 42.39 | 6.0 |
| C-28 | --- | 257.00 | middle and lower Wyodak | 30.00 | 60.00 | 0.50 | 43.37 | 4.0 |
| ns3 | 257.00 | 258.00 | ns3 | 30.50 | 30.50 | 1.00 | 44.37 | --- |
| C-29 | 258.00 | 260.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 46.34 | 3.0 |
| C-30 | 260.00 | --- | middle and lower Wyodak | 8.00 | --- | 0.13 | 46.60 | 3.0 |
| C-30 | --- | --- | middle and lower Wyodak | 24.00 | --- | 0.40 | 47.39 | 4.0 |
| C-30 | --- | --- | middle and lower Wyodak | 6.00 | --- | 0.10 | 47.59 | 2.0 |
| C-30 | --- | --- | middle and lower Wyodak | 16.00 | --- | 0.27 | 48.11 | 1.0 |
| C-30 | --- | 262.00 | middle and lower Wyodak | 6.00 | 60.00 | 0.10 | 48.31 | 40.0 |
| C-31 | 262.00 | --- | middle and lower Wyodak | 20.00 | --- | 0.33 | 48.97 | 4.0 |
| C-31 | --- | --- | middle and lower Wyodak | 20.00 | --- | 0.33 | 49.62 | 1.0 |
| C-31 | --- | 264.00 | middle and lower Wyodak | 20.00 | 60.00 | 0.33 | 50.28 | 3.0 |
| C-32 | 264.00 | --- | middle and lower Wyodak | 22.00 | --- | 0.37 | 51.00 | 7.0 |
| C-32 | --- | --- | middle and lower Wyodak | 28.00 | --- | 0.47 | 51.92 | 30.0 |
| C-32 | --- | 266.00 | middle and lower Wyodak | 10.00 | 60.00 | 0.17 | 52.25 | 4.0 |
| C-33 | 266.00 | --- | middle and lower Wyodak | 50.00 | --- | 0.83 | 53.89 | 7.0 |
| C-33 | --- | 268.00 | middle and lower Wyodak | 10.00 | 60.00 | 0.17 | 54.22 | 1.0 |
| C-35 | 268.00 | --- | middle and lower Wyodak | 19.00 | --- | 0.30 | 54.84 | 6.0 |
| C-35 | --- | --- | middle and lower Wyodak | 12.00 | --- | 0.19 | 55.23 | 2.0 |
| C-35 | --- | --- | middle and lower Wyodak | 12.00 | --- | 0.19 | 55.63 | 1.0 |
| C-35 | --- | 270.00 | middle and lower Wyodak | 21.00 | 64.00 | 0.33 | 56.32 | 30.0 |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | $\begin{aligned} & \text { Cumulative } \\ & \text { attritus } \\ & \text { thickness } \\ & \text { (CuAT) (mm) } \end{aligned}$ | Vitrain percentage (VP) | Attritus percentage (AP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-7 | 1.0 | 0.0 | 5 | 126.00 | 14.00 | 90.00 | 10.00 |
| C-7 | 10.0 | 0.0 | 2 | 138.00 | 322.00 | 30.00 | 70.00 |
| C-8 | 4.0 | 0.0 | 3 | 240.00 | 360.00 | 40.00 | 60.00 |
| C-9 | 8.0 | 0.0 | 3 | 360.00 | 240.00 | 60.00 | 40.00 |
| C-10 | 25.0 | 0.0 | 3 | 240.00 | 360.00 | 40.00 | 60.00 |
| C-11 | 20.0 | 1.0 | 3 | 91.60 | 137.40 | 39.83 | 59.74 |
| C-11 | 1.0 | 0.0 | 5 | 198.00 | 22.00 | 90.00 | 10.00 |
| C-11 | 40.0 | 0.0 | 1 | 108.00 | 72.00 | 60.00 | 40.00 |
| C-12 | 4.0 | 1.0 | 4 | 419.30 | 179.70 | 69.88 | 29.95 |
| C-13 | 10.0 | 4.0 | 2 | 298.00 | 298.00 | 49.67 | 49.67 |
| ns1 | --- | --- | --- | --- | --- | --- | --- |
| C-14 | 10.0 | 2.0 | 2 | 239.20 | 358.80 | 39.87 | 59.80 |
| C-15 | 4.0 | 0.0 | , | 486.00 | 54.00 | 90.00 | 10.00 |
| C-15 | 10.0 | 0.0 | 2 | 30.00 | 70.00 | 30.00 | 70.00 |
| C-16 | 4.0 | 1.0 | 5 | 584.10 | 64.90 | 89.86 | 9.98 |
| C-17 | 0.0 | 2.0 | 5 | 538.20 | 0.00 | 89.70 | 0.00 |
| C-18 | 20.0 | 0.0 | 2 | 120.00 | 480.00 | 20.00 | 80.00 |
| C-19 | 50.0 | 0.0 | 3 | 120.00 | 480.00 | 20.00 | 80.00 |
| C-20 | 4.0 | 0.0 | 2 | 247.50 | 202.50 | 55.00 | 45.00 |
| C-20 | 2.0 | 3.0 | 5 | 132.30 | 14.70 | 88.20 | 9.80 |
| ns2 | --- | --- | --- | --- | --- | --- | --- |
| C-21 | 9.0 | 0.0 | 3 | 184.00 | 276.00 | 40.00 | 60.00 |
| C-21 | 2.0 | 0.0 | 5 | 126.00 | 14.00 | 90.00 | 10.00 |
| C-22 | 8.0 | 0.0 | 2 | 290.00 | 290.00 | 50.00 | 50.00 |
| C-23 | 20.0 | 0.0 | 2 | 12.00 | 108.00 | 10.00 | 90.00 |
| C-23 | 2.0 | 0.0 | 4 | 432.00 | 48.00 | 90.00 | 10.00 |
| C-24 | 20.0 | 0.0 | 3 | 189.00 | 441.00 | 30.00 | 70.00 |
| C-26 | 2.0 | 0.0 | 3 | 160.00 | 40.00 | 80.00 | 20.00 |
| C-26 | 1.0 | 0.0 | 3 | 80.00 | 20.00 | 80.00 | 20.00 |
| C-26 | 1.0 | 2.0 | 4 | 160.20 | 17.80 | 89.00 | 9.89 |
| C-27 | 4.0 | 0.0 | 3 | 240.00 | 360.00 | 40.00 | 60.00 |
| C-28 | 10.0 | 0.0 | 3 | 60.00 | 240.00 | 20.00 | 80.00 |
| C-28 | 3.0 | 0.0 | 2 | 180.00 | 120.00 | 60.00 | 40.00 |
| ns3 | --- | --- | --- | --- | --- | --- | --- |
| C-29 | 30.0 | 0.0 | 1 | 120.00 | 480.00 | 20.00 | 80.00 |
| C-30 | 2.0 | 0.0 | 2 | 48.00 | 32.00 | 60.00 | 40.00 |
| C-30 | 1.0 | 0.0 | 2 | 192.00 | 48.00 | 80.00 | 20.00 |
| C-30 | 5.0 | 0.0 | 2 | 30.00 | 30.00 | 50.00 | 50.00 |
| C-30 | 20.0 | 0.0 | 1 | 16.00 | 144.00 | 10.00 | 90.00 |
| C-30 | 1.0 | 0.0 | 5 | 54.00 | 6.00 | 90.00 | 10.00 |
| C-31 | 15.0 | 0.0 | 2 | 60.00 | 140.00 | 30.00 | 70.00 |
| C-31 | 45.0 | 0.0 | 1 | 20.00 | 180.00 | 10.00 | 90.00 |
| C-31 | 15.0 | 2.0 | , | 59.40 | 138.60 | 29.70 | 69.30 |
| C-32 | 15.0 | 0.0 | 3 | 154.00 | 66.00 | 70.00 | 30.00 |
| C-32 | 30.0 | 0.0 | 4 | 112.00 | 168.00 | 40.00 | 60.00 |
| C-32 | 15.0 | 0.0 | 2 | 40.00 | 60.00 | 40.00 | 60.00 |
| C-33 | 5.0 | 2.0 | 3 | 298.80 | 199.20 | 59.76 | 39.84 |
| C-33 | 1.0 | 0.0 | 2 | 70.00 | 30.00 | 70.00 | 30.00 |
| C-35 | 6.0 | 0.0 | 3 | 95.00 | 95.00 | 50.00 | 50.00 |
| C-35 | 25.0 | 0.0 | 1 | 12.00 | 108.00 | 10.00 | 90.00 |
| C-35 | 1.0 | 20.0 | 2 | 60.00 | 40.00 | 50.00 | 33.33 |
| C-35 | 20.0 | 2.0 | 4 | 145.60 | 62.40 | 69.33 | 29.71 |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-7 | 0.00 | -- | - | --- | 35 | 28.57 | --- |
| C-7 | 0.00 | 44.00 | 56.00 | 0.00 | 10 | 100.00 | 83.33 |
| C-8 | 0.00 | 40.00 | 60.00 | 0.00 | 25 | 40.00 | 40.00 |
| C-9 | 0.00 | 60.00 | 40.00 | 0.00 | 40 | 25.00 | 25.00 |
| C-10 | 0.00 | 40.00 | 60.00 | 0.00 | 60 | 16.67 | 16.67 |
| C-11 | 0.43 | --- | --- | --- | 65 | 15.38 | --- |
| C-11 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-11 | 0.00 | 63.11 | 36.73 | 0.16 | 50 | 20.00 | 22.97 |
| C-12 | 0.17 | 69.88 | 29.95 | 0.17 | 50 | 20.00 | 20.00 |
| C-13 | 0.67 | 49.67 | 49.67 | 0.67 | 30 | 33.33 | 33.33 |
| ns1 | --- | - | --- | --- | --- | --- | --- |
| C-14 | 0.33 | 39.87 | 59.80 | 0.33 | 40 | 25.00 | 25.00 |
| C-15 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-15 | 0.00 | 80.63 | 19.38 | 0.00 | 50 | 20.00 | 31.25 |
| C-16 | 0.15 | 89.86 | 9.98 | 0.15 | 20 | 50.00 | 50.00 |
| C-17 | 0.33 | 89.70 | 0.00 | 0.33 | 30 | 33.33 | 33.33 |
| C-18 | 0.00 | 20.00 | 80.00 | 0.00 | 50 | 20.00 | 20.00 |
| C-19 | 0.00 | 20.00 | 80.00 | 0.00 | 20 | 50.00 | 50.00 |
| C-20 | 0.00 | --- | --- | --- | 20 | 50.00 | --- |
| C-20 | 2.00 | 63.30 | 36.20 | 0.50 | 30 | 33.33 | 45.83 |
| ns2 | --- | --- | --- | --- | --- | --- | --- |
| C-21 | 0.00 | --- | --- | --- | 20 | 50.00 | --- |
| C-21 | 0.00 | 51.67 | 48.33 | 0.00 | 40 | 25.00 | 44.17 |
| C-22 | 0.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| C-23 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-23 | 0.00 | 74.00 | 26.00 | 0.00 | 20 | 50.00 | 46.67 |
| C-24 | 0.00 | 30.00 | 70.00 | 0.00 | 20 | 50.00 | 50.00 |
| C-26 | 0.00 | --- | --- | --- | --- | --- | --- |
| C-26 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-26 | 1.11 | 83.38 | 16.21 | 0.42 | 20 | 50.00 | 44.05 |
| C-27 | 0.00 | 40.00 | 60.00 | 0.00 | 65 | 15.38 | 15.38 |
| C-28 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-28 | 0.00 | 40.00 | 60.00 | 0.00 | 20 | 50.00 | 41.67 |
| ns3 | --- | --- | --- | --- | --- | --- | --- |
| C-29 | 0.00 | 20.00 | 80.00 | 0.00 | 20 | 50.00 | 50.00 |
| C-30 | 0.00 | --- | --- | --- | 40 | 25.00 | --- |
| C-30 | 0.00 | --- | --- | --- | 40 | 25.00 | --- |
| C-30 | 0.00 | --- | --- | --- | --- | --- | --- |
| C-30 | 0.00 | --- | --- | --- | 40 | 25.00 | --- |
| C-30 | 0.00 | 56.67 | 43.33 | 0.00 | 30 | 33.33 | 25.93 |
| C-31 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-31 | 0.00 | --- | --- | --- | 55 | 18.18 | --- |
| C-31 | 1.00 | 23.23 | 76.43 | 0.33 | 40 | 25.00 | 25.51 |
| C-32 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-32 | 0.00 | --- | --- | --- | 15 | 66.67 | --- |
| C-32 | 0.00 | 51.00 | 49.00 | 0.00 | 30 | 33.33 | 48.89 |
| C-33 | 0.40 | --- | --- | --- | 20 | 50.00 | --- |
| C-33 | 0.00 | 61.47 | 38.20 | 0.33 | 10 | 100.00 | 58.33 |
| C-35 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-35 | 0.00 | --- | --- | --- | 50 | 20.00 | --- |
| C-35 | 16.67 | --- | --- | --- | 40 | 25.00 | --- |
| C-35 | 0.95 | 48.84 | 47.72 | 3.44 | 15 | 66.67 | 40.21 |

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Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: |
| C-7 | --- | --- | --- |
| C-7 | 3.67 | SubB | Gypsum on cleat. |
| C-8 | 4.71 | --- | Slickensides at top. |
| C-9 | 10.60 | --- | --- |
| C-10 | 7.01 | --- | --- |
| C-11 | --- | --- | --- |
| C-11 | --- | --- | --- |
| C-11 | 6.06 | --- | Hard. |
| C-12 | 5.64 | --- | Numerous wood structures visible, kaolinite at $50-60 \mathrm{~cm}$. |
| C-13 | 6.59 | --- | Kaolinite at 58-63 cm. |
| ns1 | --- | --- | No sample. |
| C-14 | 5.82 | --- | Dull. |
| C-15 | --- | --- | A lot of wood grain visible, kaolinite on cleat. |
| C-15 | 5.27 | --- | --- |
| C-16 | 8.08 | --- | A lot of wood grain visible, kaolinite on cleat. |
| C-17 | 5.18 | --- | Numerous wood structures visible, kaolinite on cleat. |
| C-18 | 7.40 | SubB | Fewer wood structures visible, kaolinite on cleat. |
| C-19 | 7.37 | --- | --- |
| C-20 | --- | --- | --- |
| C-20 | 6.97 | --- | Fusain layer at 45 cm . |
| ns2 | --- | --- | No sample. |
| C-21 | --- | --- | Top half is very fractured. |
| C-21 | 9.06 | --- | Almost all vitrain. |
| C-22 | 8.40 | --- | Highly fractured sample. |
| C-23 | --- | --- | --- |
| C-23 | 9.45 | --- | Very woody. |
| C-24 | 9.56 | --- | Highly fractured sample. |
| C-26 | --- | --- | Banding thickness increases downward. |
| C-26 | --- | --- | Banding thickness increases downward. |
| C-26 | 9.33 | --- | Banding thickness increases downward. |
| C-27 | 7.86 | --- | --- |
| C-28 | --- | --- | --- |
| C-28 | 9.99 | --- | --- |
| ns3 | --- | --- | No sample. |
| C-29 | 8.31 | -- | Hard. |
| C-30 | -- | --- | Compressed banding at 5 cm , very disturbed banding from 8 to 28 cm . |
| C-30 | --- | --- | --- |
| C-30 | -- | --- | --- |
| C-30 | --- | --- | --- |
| C-30 | 8.81 | SubC | Conchoidally fractured. |
| C-31 | --- | --- | --- |
| C-31 | --- | --- | --- |
| C-31 | 7.27 | --- | --- - - - - |
| C-32 | --- | --- | --- |
| C-32 | --- | --- | --- |
| C-32 | 8.85 | --- | --- |
| C-33 | --- | --- | --- |
| C-33 | 12.28 | --- | Very hard, shiny. |
| C-35 | --- | --- | --- |
| C-35 | --- | --- | Small amount of resin present. |
| C-35 | --- | --- | Numerous gypsum crystals on bedding and cleat surfaces, highly fractured sample, large amount of fusain present. |
| C-35 | 9.06 | --- | Large woody structures present. |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |
| C-36 | 270.00 | --- | middle and lower Wyodak | 46.00 | --- | 0.75 | 57.82 | 3.0 |
| C-36 | --- | --- | middle and lower Wyodak | 9.00 | --- | 0.15 | 58.12 | 50.0 |
| C-36 | --- | 272.00 | middle and lower Wyodak | 6.00 | 61.00 | 0.10 | 58.32 | 20.0 |
| ns4 | 272.00 | 273.00 | ns4 | 30.50 | 30.50 | 1.00 | 59.32 | --- |
| C-37 | 273.00 | 275.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 61.29 | 1.0 |
| C-38 | 275.00 | 277.00 | middle and lower Wyodak | 55.00 | 55.00 | 1.00 | 63.09 | 3.0 |
| C-39 | 277.00 | 279.00 | middle and lower Wyodak | 54.00 | 54.00 | 1.00 | 64.86 | 4.0 |
| C-40 | 279.00 | --- | middle and lower Wyodak | 27.00 | --- | 0.45 | 65.75 | 4.0 |
| C-40 | --- | 281.00 | middle and lower Wyodak | 33.00 | 60.00 | 0.55 | 66.83 | 8.0 |
| C-41 | 281.00 | 283.00 | middle and lower Wyodak | 60.00 | 60.00 | 1.00 | 68.80 | 5.0 |
| C-42 | 283.00 | --- | middle and lower Wyodak | 15.00 | --- | 0.25 | 69.29 | 2.0 |
| C-42 | --- | --- | middle and lower Wyodak | 30.00 | --- | 0.50 | 70.28 | 25.0 |
| C-42 | --- | 285.00 | middle and lower Wyodak | 15.00 | 60.00 | 0.25 | 70.77 | 2.0 |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-36 | 2.0 | 0.0 | 2 | 276.00 | 184.00 | 60.00 | 40.00 |
| C-36 | 0.0 | 0.0 | 5 | 90.00 | 0.00 | 100.00 | 0.00 |
| C-36 | 2.0 | 4.0 | 3 | 39.20 | 16.80 | 65.33 | 28.00 |
| ns4 | --- | --- | --- | --- | --- | --- | --- |
| C-37 | 4.0 | 0.0 | 2 | 240.00 | 360.00 | 40.00 | 60.00 |
| C-38 | 2.0 | 3.0 | 2 | 328.20 | 218.80 | 59.67 | 39.78 |
| C-39 | 1.0 | 1.0 | 2 | 377.30 | 161.70 | 69.87 | 29.94 |
| C-40 | 1.0 | 0.0 | 2 | 189.00 | 81.00 | 70.00 | 30.00 |
| C-40 | 30.0 | 0.0 | 3 | 99.00 | 231.00 | 30.00 | 70.00 |
| C-41 | 4.0 | 1.0 | 3 | 359.40 | 239.60 | 59.90 | 39.93 |
| C-42 | 10.0 | 1.0 | 2 | 74.50 | 74.50 | 49.67 | 49.67 |
| C-42 | 1.0 | 0.0 | 4 | 240.00 | 60.00 | 80.00 | 20.00 |
| C-42 | 5.0 | 3.0 | 2 | 102.90 | 44.10 | 68.60 | 29.40 |

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Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-36 | 0.00 | --- | --- | --- | 20 | 50.00 | --- |
| C-36 | 0.00 | --- | --- | --- | 35 | 28.57 | --- |
| C-36 | 6.67 | 66.43 | 32.92 | 0.66 | 30 | 33.33 | 45.20 |
| ns4 | --- | --- | --- | --- | --- | --- | --- |
| C-37 | 0.00 | 40.00 | 60.00 | 0.00 | 50 | 20.00 | 20.00 |
| C-38 | 0.55 | 59.67 | 39.78 | 0.55 | 30 | 33.33 | 33.33 |
| C-39 | 0.19 | 69.87 | 29.94 | 0.19 | 30 | 33.33 | 33.33 |
| C-40 | 0.00 | --- | --- | --- | 30 | 33.33 | --- |
| C-40 | 0.00 | 48.00 | 52.00 | 0.00 | 40 | 25.00 | 28.75 |
| C-41 | 0.17 | 59.90 | 39.93 | 0.17 | 25 | 40.00 | 40.00 |
| C-42 | 0.67 | --- | --- | --- | 70 | 14.29 | --- |
| C-42 | 0.00 | --- | --- | --- | 20 | 50.00 | --- |
| C-42 | 2.00 | 69.57 | 29.77 | 0.67 | 30 | 33.33 | 36.90 |

Table 1-16. Data for samples from core hole 20, Peabody Natural Gas LLC, PNG 16-2.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister <br> number | Total gas <br> (SCF/ton) | Apparent <br> rank |  |
| :--- | ---: | :--- | :--- |
|  |  |  | Comments |
| C-36 | --- | --- | --- |
| C-36 | --- | --- | -- |
| C-36 | 10.39 | --- | Fusian layers at 55 and 61 cm. |
| ns4 | --- | --- | No sample. |
| C-37 | 12.10 | --- | Highly fractured sample. |
| C-38 | 8.47 | --- | --- |
| C-39 | 11.36 | --- | --- |
| C-40 | --- | --- | Highly fractured sample. |
| C-40 | 7.56 | --- | Highly fractured sample. |
| C-41 | 11.19 | --- | --- |
| C-42 | --- | -- | --- |
| C-42 | --- | --- | -- |
| C-42 | 12.52 | SubC | Fusain layer at 47 cm. |

Table 1-17. Data for samples from core hole 21, The Coteau Properties Co., Coteau MC00250C.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; LigA, lignite A; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D20 | 167.00 | 169.00 | Beulah | 56.00 | 56.00 | 1.00 | 1.84 | 4.0 | 25.0 | 1.0 |
| ns1 | 169.00 | 173.00 | ns1 | 122.00 | 122.00 | 1.00 | 5.84 | --- | --- | --- |
| D21 | 173.00 | - | Beulah | 25.00 | --- | 0.51 | 6.66 | 4.0 | 25.0 | 0.0 |
| D21 | --- | 175.00 | Beulah | 24.00 | 49.00 | 0.49 | 7.45 | 7.0 | 25.0 | 0.0 |
| ns2 | 175.00 | 438.20 | ns2 | 8022.00 | 8,022.00 | 1.00 | 270.64 | --- | --- | --- |
| D22 | 438.20 | 440.20 | unnamed 2 | 60.00 | 60.00 | 1.00 | 272.60 | 10.0 | 13.0 | 3.0 |
| D23 | 440.20 | 442.20 | unnamed 2 | 60.00 | 60.00 | 1.00 | 274.57 | 10.0 | 15.0 | 2.0 |
| ns3 | 442.20 | 443.00 | ns3 | 24.00 | 24.00 | 1.00 | 275.36 | --- | --- | --- |
| D24 | 443.00 | 445.00 | unnamed 2 | 59.00 | 59.00 | 1.00 | 277.30 | 10.0 | 10.0 | 1.0 |
| D25 | 445.00 | 447.00 | unnamed 2 | 55.00 | 55.00 | 1.00 | 279.10 | 5.0 | 7.0 | 2.0 |
| ns4 | 447.00 | 571.00 | ns4 | 3779.50 | 3,779.50 | 1.00 | 403.10 | --- | --- | --- |
| D26 | 571.00 | 573.40 | unnamed 3 | 66.00 | 66.00 | 1.00 | 405.27 | 4.0 | 5.0 | 0.0 |

Table 1-17. Data for samples from core hole 21, The Coteau Properties Co., Coteau MC00250C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; LigA, lignite A; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D20 | 1 | 111.80 | 447.20 | 19.96 | 79.86 | 0.18 | 19.96 | 79.86 | 0.18 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D21 | 1 | 50.00 | 200.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| D21 | 3 | 72.00 | 168.00 | 30.00 | 70.00 | 0.00 | 24.90 | 75.10 | 0.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D22 | 3 | 358.20 | 238.80 | 59.70 | 39.80 | 0.50 | 59.70 | 39.80 | 0.50 |
| D23 | 3 | 299.00 | 299.00 | 49.83 | 49.83 | 0.33 | 49.83 | 49.83 | 0.33 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D24 | 3 | 235.60 | 353.40 | 39.93 | 59.90 | 0.17 | 39.93 | 59.90 | 0.17 |
| D25 | 3 | 219.20 | 328.80 | 39.85 | 59.78 | 0.36 | 39.85 | 59.78 | 0.36 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D26 | 2 | 198.00 | 462.00 | 30.00 | 70.00 | 0.00 | 30.00 | 70.00 | 0.00 |

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Table 1-17. Data for samples from core hole 21, The Coteau Properties Co., Coteau MC00250C.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; LigA, lignite A; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D20 | 50 | 20.00 | 20.00 | 0.57 | --- | Fusain on bedding. |
| ns1 | --- | --- | --- | --- | --- | Sample taken by Coteau mine engineer. |
| D21 | 75 | 13.33 | --- | --- | --- | Blebs of resin at 4 mm . |
| D21 | 75 | 13.33 | 13.33 | 0.88 | --- | Woody material near base. |
| ns2 | --- | --- | --- | --- | --- | No sample. |
| D22 | 75 | 13.33 | 13.33 | 2.55 | --- | --- |
| D23 | 75 | 13.33 | 13.33 | 2.18 | LigA | --- |
| ns3 | --- | --- | --- | --- | --- | Shale, no sample. |
| D24 | 30 | 33.33 | 33.33 | 2.51 | --- | --- |
| D25 | 40 | 25.00 | 25.00 | 2.16 | --- | --- |
| ns4 | --- | --- | --- | --- | --- | No sample. |
| D26 | 30 | 33.33 | 33.33 | 0.96 | --- | --- |

Table 1-18. Data for samples from core hole 22, The Coteau Properties Co., Coteau MC00251.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; LigA, lignite A; ---, no data]

| Canister number | Approximate | depth (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| D28 | 791.00 | --- | unnamed 4 | 17.00 | --- | 0.24 | 0.56 | 2.0 | 6.0 |
| D28 | --- | 793.00 | unnamed 4 | 53.00 | 70.00 | 0.76 | 2.30 | 20.0 | 10.0 |
| D27 | 793.00 | --- | unnamed 4 | 17.00 | --- | 0.35 | 2.85 | 1.0 | 0.0 |
| D27 | --- | 795.00 | unnamed 4 | 32.00 | 49.00 | 0.65 | 3.90 | 7.0 | 4.0 |
| D29 | 795.00 | --- | unnamed 4 | 10.50 | --- | 0.20 | 4.25 | 0.0 | 0.0 |
| D29 | --- | 797.00 | unnamed 4 | 41.50 | 52.00 | 0.80 | 5.61 | 7.0 | 10.0 |

Table 1-18. Data for samples from core hole 22, The Coteau Properties Co., Coteau MCO0251.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; LigA, lignite A; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) <br> (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D28 | 0.0 | 2 | 51.00 | 119.00 | 30.00 | 70.00 | 0.00 | --- | --- |
| D28 | 4.0 | 3 | 315.60 | 210.40 | 59.55 | 39.70 | 0.75 | 52.37 | 47.06 |
| D27 | 0.0 | 2 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| D27 | 0.0 | 3 | 288.00 | 32.00 | 90.00 | 10.00 | 0.00 | 58.78 | 6.53 |
| D29 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| D29 | 0.0 | 3 | 124.50 | 290.50 | 30.00 | 70.00 | 0.00 | 23.94 | 55.87 |

Table 1-18. Data for samples from core hole 22, The Coteau Properties Co., Coteau MC00251.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; LigA, lignite A; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat <br> spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D28 | --- | --- | --- | --- | --- | --- | $16-\mathrm{mm}$-thick clay band at 9 cm . |
| D28 | 0.57 | --- | --- | --- | 0.40 | LigA | 4 mm of fusain at 44 cm . |
| D27 | --- | --- | --- | --- | --- | --- | --- |
| D27 | 0.00 | 25 | 40.00 | 40.00 | 0.67 | --- | --- |
| D29 | --- | --- | --- | --- | --- | --- | Rooted clay, dark brown. |
| D29 | 0.00 | --- | --- | --- | 0.86 | --- | --- |

Table 1-19. Data for samples from core hole 23, Ammonite Energy Texas, Inc., Thomas Jefferson State 36-3.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Approxima | te depth | Coal bed name | Unit <br> thickness <br> (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| D1 | 337.00 | --- | School | 53.00 | --- | 0.88 | 1.74 | 50.0 | 0.0 |
| D1 | --- | 339.00 | School | 7.00 | 60.00 | 0.12 | 1.97 | 5.0 | 20.0 |
| D2 | 339.00 | --- | School | 42.00 | --- | 0.70 | 3.35 | 2.0 | 10.0 |
| D2 | --- | 341.00 | School | 18.00 | 60.00 | 0.30 | 3.94 | 10.0 | 5.0 |
| D3 | 341.00 | --- | School | 7.00 | --- | 0.12 | 4.17 | 2.0 | 10.0 |
| D3 | --- | --- | School | 19.00 | --- | 0.32 | 4.79 | 0.0 | 0.0 |
| D3 | --- | --- | School | 21.00 | --- | 0.35 | 5.48 | 1.0 | 10.0 |
| D3 | --- | 343.00 | School | 13.00 | 60.00 | 0.22 | 5.91 | 2.0 | 5.0 |
| D4 | 343.00 | --- | School | 23.00 | --- | 0.43 | 6.66 | 1.0 | 40.0 |
| D4 | --- | --- | School | 19.00 | --- | 0.36 | 7.28 | 10.0 | 2.0 |
| D4 | --- | 345.00 | School | 11.00 | 53.00 | 0.21 | 7.64 | 3.0 | 5.0 |
| D5 | 345.00 | --- | School | 2.00 | --- | 0.04 | 7.71 | 0.0 | 0.0 |
| D5 | --- | --- | School | 17.00 | --- | 0.30 | 8.27 | 30.0 | 2.0 |
| D5 | --- | 347.00 | School | 38.00 | 57.00 | 0.67 | 9.51 | 1.0 | 20.0 |
| D6 | 347.00 | 349.00 | School | 54.00 | 54.00 | 1.00 | 11.29 | 5.0 | 2.0 |
| D7 | 349.00 | --- | School | 19.00 | --- | 0.32 | 11.91 | 2.0 | 3.0 |
| D7 | --- | --- | School | 15.00 | --- | 0.25 | 12.40 | 10.0 | 15.0 |
| D7 | --- | 351.00 | School | 26.00 | 60.00 | 0.43 | 13.25 | 20.0 | 10.0 |
| D8 | 351.00 | --- | School | 55.00 | --- | 0.87 | 15.06 | 20.0 | 10.0 |
| D8 | --- | 353.00 | School | 8.00 | 63.00 | 0.13 | 15.32 | 2.0 | 8.0 |
| D9 | 353.00 | --- | School | 23.00 | --- | 0.38 | 16.08 | 2.0 | 8.0 |
| D9 | --- | 355.00 | School | 37.00 | 60.00 | 0.62 | 17.29 | 40.0 | 0.0 |

Table 1-19. Data for samples from core hole 23, Ammonite Energy Texas, Inc., Thomas Jefferson State 36-3.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 3.0 | 5 | 527.00 | 0.00 | 99.43 | 0.00 | 0.57 | --- | --- |
| D1 | 0.0 | 3 | 14.00 | 56.00 | 20.00 | 80.00 | 0.00 | 90.17 | 9.33 |
| D2 | 0.0 | 2 | 70.00 | 350.00 | 16.67 | 83.33 | 0.00 | --- | --- |
| D2 | 2.0 | 3 | 118.67 | 59.33 | 65.93 | 32.96 | 1.11 | 31.44 | 68.22 |
| D3 | 0.0 | 2 | 11.67 | 58.33 | 16.67 | 83.33 | 0.00 | --- | --- |
| D3 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| D3 | 0.0 | 2 | 19.09 | 190.91 | 9.09 | 90.91 | 0.00 | --- | --- |
| D3 | 0.0 | 2 | 37.14 | 92.86 | 28.57 | 71.43 | 0.00 | 11.32 | 57.02 |
| D4 | 2.0 | 1 | 5.56 | 222.44 | 2.42 | 96.71 | 0.87 | --- | --- |
| D4 | 2.0 | 3 | 156.67 | 31.33 | 82.46 | 16.49 | 1.05 | --- | --- |
| D4 | 0.0 | 2 | 41.25 | 68.75 | 37.50 | 62.50 | 0.00 | 38.39 | 60.85 |
| D5 | 20.0 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- |
| D5 | 0.0 | 4 | 159.38 | 10.63 | 93.75 | 6.25 | 0.00 | --- | --- |
| D5 | 0.0 | 2 | 18.10 | 361.90 | 4.76 | 95.24 | 0.00 | 31.14 | 65.36 |
| D6 | 6.0 | 3 | 381.43 | 152.57 | 70.63 | 28.25 | 1.11 | 70.63 | 28.25 |
| D7 | 0.0 | 2 | 76.00 | 114.00 | 40.00 | 60.00 | 0.00 | --- | --- |
| D7 | 0.0 | 3 | 60.00 | 90.00 | 40.00 | 60.00 | 0.00 | --- | --- |
| D7 | 0.0 | 3 | 173.33 | 86.67 | 66.67 | 33.33 | 0.00 | 51.56 | 48.44 |
| D8 | 0.0 | 3 | 366.67 | 183.33 | 66.67 | 33.33 | 0.00 | --- | -- |
| D8 | 1.0 | 2 | 15.80 | 63.20 | 19.75 | 79.00 | 1.25 | 60.71 | 39.13 |
| D9 | 1.0 | 2 | 45.80 | 183.20 | 19.91 | 79.65 | 0.43 | --- | --- |
| D9 | 0.0 | 5 | 370.00 | 0.00 | 100.00 | 0.00 | 0.00 | 69.30 | 30.53 |

Table 1-19. Data for samples from core hole 23, Ammonite Energy Texas, Inc., Thomas Jefferson State 36-3.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | --- | 30 | 33.33 | --- | --- | --- | --- |
| D1 | 0.50 | 20 | 50.00 | 35.28 | 1.33 | SubC | --- |
| D2 | --- | 50 | 20.00 | --- | --- | --- | --- |
| D2 | 0.33 | 50 | 20.00 | 20.00 | 0.57 | --- | --- |
| D3 | --- | 2 | 500.00 | --- | --- | --- | --- |
| D3 | --- | --- | --- | --- | --- | --- | Clay included in sample. |
| D3 | --- | 40 | 25.00 | --- | --- | --- | Light-gray. |
| D3 | 0.00 | 40 | 25.00 | 106.10 | 1.21 | --- | --- - - - - |
| D4 | --- | 40 | 25.00 | --- | --- | --- | --- |
| D4 | --- | 30 | 33.33 | --- | --- | --- | --- |
| D4 | 0.75 | 40 | 25.00 | 27.99 | 1.48 | --- | Hard and dense. |
| D5 | --- | --- | --- | --- | --- | --- | --- |
| D5 | --- | 30 | 33.33 | --- | --- | --- | --- |
| D5 | 3.51 | 40 | 25.00 | 27.58 | 2.01 | --- | --- |
| D6 | 1.11 | 10 | 100.00 | 100.00 | 2.47 | --- | --- |
| D7 | --- | 10 | 100.00 | --- | --- | --- | --- |
| D7 | --- | 10 | 100.00 | --- | --- | --- | --- |
| D7 | 0.00 | 5 | 200.00 | 143.33 | 1.18 | --- | --- |
| D8 | --- | 10 | 100.00 | --- | --- | --- | --- |
| D8 | 0.16 | 40 | 25.00 | 90.48 | 1.05 | --- | Hard and dense. |
| D9 | --- | 30 | 33.33 | --- | --- | --- | --- |
| D9 | 0.17 | 5 | 200.00 | 136.11 | 0.94 | SubC | --- |

Table 1-20. Data for samples from core hole 24, Bridger Coal Company, BCX-9.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; m, meter; SCF, standard cubic feet; SubA, subbituminous A; HvolC, high-volatile C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D-10 | 943.20 | 945.00 | Deadman | 45.00 | 45.00 | 1.00 | 1.48 | 30.0 | 2.0 | 0.0 |
| D-11 | 945.00 | --- | Deadman | 25.00 | --- | 0.41 | 2.30 | 15.0 | 2.0 | 1.0 |
| D-11 | --- | --- | Deadman | 7.00 | --- | 0.11 | 2.53 | 0.0 | 0.0 | 0.0 |
| D-11 | --- | 947.00 | Deadman | 29.00 | 61.00 | 0.48 | 3.48 | 5.0 | 7.0 | 2.0 |
| D-12 | 947.00 | 949.00 | Deadman | 59.00 | 59.00 | 1.00 | 5.41 | 5.0 | 20.0 | 3.0 |
| D-13 | 949.00 | --- | Deadman | 40.00 | --- | 0.68 | 6.73 | 15.0 | 5.0 | 1.0 |
| D-13 | --- | 951.00 | Deadman | 19.00 | 59.00 | 0.32 | 7.35 | 5.0 | 30.0 | 1.0 |
| D-14 | 951.00 | 953.00 | Deadman | 60.00 | 60.00 | 1.00 | 9.32 | 5.0 | 7.0 | 2.0 |
| D-15 | 953.00 | --- | Deadman | 45.00 | --- | 0.75 | 10.79 | 2.0 | 10.0 | 1.0 |
| D-15 | --- | 955.00 | Deadman | 15.00 | 60.00 | 0.25 | 11.29 | 5.0 | 2.0 | 1.0 |

Table 1-20. Data for samples from core hole 24, Bridger Coal Company, BCX-9.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; m, meter; SCF, standard cubic feet; SubA, subbituminous A; HvolC, high-volatile C; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D-10 | 4 | 421.88 | 28.13 | 93.75 | 6.25 | 0.00 | 93.75 | 6.25 | 0.00 |
| D-11 | 3 | 219.71 | 29.29 | 87.88 | 11.72 | 0.40 | --- | --- | --- |
| D-11 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| D-11 | 3 | 120.00 | 168.00 | 41.38 | 57.93 | 0.69 | 55.69 | 32.34 | 0.49 |
| D-12 | 3 | 117.40 | 469.60 | 19.90 | 79.59 | 0.51 | 19.90 | 79.59 | 0.51 |
| D-13 | 3 | 299.25 | 99.75 | 74.81 | 24.94 | 0.25 | --- | --- | --- |
| D-13 | 3 | 27.00 | 162.00 | 14.21 | 85.26 | 0.53 | 55.30 | 44.36 | 0.34 |
| D-14 | 3 | 249.17 | 348.83 | 41.53 | 58.14 | 0.33 | 41.53 | 58.14 | 0.33 |
| D-15 | 2 | 74.83 | 374.17 | 16.63 | 83.15 | 0.22 | --- | --- | --- |
| D-15 | 3 | 106.43 | 42.57 | 70.95 | 28.38 | 0.67 | 30.21 | 69.46 | 0.33 |

Table 1-20. Data for samples from core hole 24, Bridger Coal Company, BCX-9.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; m, meter; SCF, standard cubic feet; SubA, subbituminous A; HvolC, high-volatile C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D-10 | 40 | 25.00 | 25.00 | 0.77 | SubA | Highly fragmented sample. |
| D-11 | 30 | 33.33 | --- | --- | --- | Pyrite and kaolinite on cleats. |
| D-11 | --- | --- | --- | --- | --- | Parting. |
| D-11 | 25 | 40.00 | 36.91 | 0.69 | --- | Pyrite and kaolinite on cleats. |
| D-12 | 25 | 40.00 | 40.00 | 0.60 | --- | Pyrite, kaolinite, and calcite on cleats. |
| D-13 | 15 | 66.67 | --- | --- | --- | Pyrite on cleats, 5-mm-thick clastic dike in lower part of core. |
| D-13 | 60 | 16.67 | 50.56 | 0.98 | --- | 5-mm-thick clastic dike in upper part of core. |
| D-14 | 20 | 50.00 | 50.00 | 1.31 | --- | Pyrite on cleats, finely laminated to coarsely laminated at base. |
| D-15 | 25 | 40.00 | --- | --- | --- | Pyrite and kaolin on cleats. |
| D-15 | 25 | 40.00 | 40.00 | 0.33 | HvolC | --- |

Table 1-21. Data for samples from core hole 25, Peabody Natural Gas LLC, Duvall 13J-D.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D30 | 1,238.00 | 1,240.00 | Pawnee | 27.00 | 27.00 | 1.00 | 0.89 | 3.5 | 130.5 | 2.0 |
| D31 | 1,240.00 | 1,242.00 | Pawnee | 60.00 | 60.00 | 1.00 | 2.85 | 16.3 | 68.4 | 7.0 |
| D32 | 1,242.00 | 1,244.00 | Pawnee | 57.00 | 57.00 | 1.00 | 4.72 | 3.8 | 90.7 | 3.0 |
| D33 | 1,244.00 | 1,246.00 | Pawnee | 59.00 | 59.00 | 1.00 | 6.66 | 5.3 | 189.7 | 5.0 |
| D34 | 1,246.00 | 1,248.00 | Pawnee | 35.00 | 35.00 | 1.00 | 7.81 | 8.6 | 61.4 | 0.0 |

Table 1-21. Data for samples from core hole 25, Peabody Natural Gas LLC, Duvall 13J-D.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D30 | 1 | 7.00 | 261.00 | 2.59 | 96.67 | 0.74 | 2.59 | 96.67 | 0.74 |
| D31 | 3 | 114.00 | 479.00 | 19.00 | 79.83 | 1.17 | 19.00 | 79.83 | 1.17 |
| D32 | 1 | 23.00 | 544.00 | 4.04 | 95.44 | 0.53 | 4.04 | 95.44 | 0.53 |
| D33 | 3 | 16.00 | 569.00 | 2.71 | 96.44 | 0.85 | 2.71 | 96.44 | 0.85 |
| D34 | 3 | 43.00 | 307.00 | 12.29 | 87.71 | 0.00 | 12.29 | 87.71 | 0.00 |

Table 1-21. Data for samples from core hole 25, Peabody Natural Gas LLC, Duvall 13J-D.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D30 | 25 | 40.00 | 40.00 | 4.65 | SubB | Clay on cleat surfaces. |
| D31 | 18 | 55.56 | 55.56 | 2.40 | --- | Clay on cleat surfaces, more than 60 mm of vitrain at base. |
| D32 | 22 | 45.45 | 45.45 | 2.89 | --- | Clay on cleats. |
| D33 | 30 | 33.33 | 33.33 | 2.54 | --- | Clay on cleats, broken. |
| D34 | 22 | 45.45 | 45.45 | 1.70 | SubC | Clay on cleats, broken. |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness <br> (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |
| D35 | 1,313.00 | 1,315.00 | Big George | 61.00 | 61.00 | 1.00 | 2.00 |
| D36 | 1,315.00 | 1,317.00 | Big George | 66.00 | 66.00 | 1.00 | 4.17 |
| D37 | 1,317.00 | 1,319.00 | Big George | 71.00 | 71.00 | 1.00 | 6.50 |
| D38 | 1,319.00 | 1,321.00 | Big George | 66.00 | 66.00 | 1.00 | 8.66 |
| D39 | 1,321.00 | 1,323.00 | Big George | 69.00 | 69.00 | 1.00 | 10.93 |
| D40 | 1,323.00 | 1,325.00 | Big George | 69.00 | 69.00 | 1.00 | 13.19 |
| D41 | 1,325.00 | 1,327.00 | Big George | 69.00 | 69.00 | 1.00 | 15.45 |
| D42 | 1,327.00 | 1,329.00 | Big George | 64.00 | 64.00 | 1.00 | 17.55 |
| D43 | 1,329.00 | 1,331.00 | Big George | 64.00 | 64.00 | 1.00 | 19.65 |
| D44 | 1,331.00 | --- | Big George | 45.00 | --- | 0.83 | 21.13 |
| D44 | --- | 1,331.00 | Big George | 9.00 | 54.00 | 0.17 | 21.42 |
| D45 | 1,333.00 | 1,335.00 | Big George | 60.00 | 60.00 | 1.00 | 23.39 |
| D46 | 1,335.00 | 1,337.00 | Big George | 67.00 | 67.00 | 1.00 | 25.59 |
| ns1 | 1,337.00 | 1,338.00 | ns1 | 30.50 | 30.50 | 1.00 | 26.59 |
| D47 | 1,338.00 | 1,340.00 | Big George | 64.00 | 64.00 | 1.00 | 28.69 |
| D48 | 1,340.00 | 1,342.00 | Big George | 62.00 | 62.00 | 1.00 | 30.73 |
| D49 | 1,342.00 | 1,344.00 | Big George | 66.00 | 66.00 | 1.00 | 32.89 |
| D50 | 1,344.00 | --- | Big George | 50.00 | --- | 0.83 | 34.53 |
| D50 | --- | 1,346.00 | Big George | 10.00 | 60.00 | 0.17 | 34.86 |
| D51 | 1,346.00 | 1,348.00 | Big George | 66.00 | 66.00 | 1.00 | 37.02 |
| D52 | 1,348.00 | 1,350.00 | Big George | 64.00 | 64.00 | 1.00 | 39.12 |
| D53 | 1,350.00 | 1,352.00 | Big George | 66.00 | 66.00 | 1.00 | 41.29 |
| D54 | 1,352.00 | --- | Big George | 15.00 | --- | 0.23 | 41.78 |
| D54 | --- | 1,354.00 | Big George | 49.00 | 64.00 | 0.77 | 43.39 |
| D55 | 1,354.00 | 1,356.00 | Big George | 60.00 | 60.00 | 1.00 | 45.36 |
| D56 | 1,356.00 | 1,358.00 | Big George | 62.00 | 62.00 | 1.00 | 47.39 |
| D5 | 1,358.00 | 1,360.00 | Big George | 64.00 | 64.00 | 1.00 | 49.49 |
| D8 | 1,360.00 | 1,362.00 | Big George | 73.00 | 73.00 | 1.00 | 51.89 |
| D9 | 1,362.00 | 1,364.00 | Big George | 63.00 | 63.00 | 1.00 | 53.95 |
| D10 | 1,364.00 | 1,366.00 | Big George | 74.00 | 74.00 | 1.00 | 56.38 |
| D11 | 1,366.00 | 1,368.00 | Big George | 63.00 | 63.00 | 1.00 | 58.45 |
| D12 | 1,368.00 | --- | Big George | 16.00 | --- | 0.26 | 58.97 |
| D12 | --- | --- | Big George | 29.00 | --- | 0.47 | 59.92 |
| D12 | --- | --- | Big George | 5.00 | --- | 0.08 | 60.09 |
| D12 | --- | 1,370.00 | Big George | 12.00 | 62.00 | 0.19 | 60.48 |
| D15 | 1,370.00 | --- | Big George | 15.00 | --- | 0.25 | 60.97 |
| D15 | --- | 1,372.00 | Big George | 46.00 | 61.00 | 0.75 | 62.48 |
| D16 | 1,372.00 | 1,374.00 | Big George | 64.00 | 64.00 | 1.00 | 64.58 |
| D17 | 1,374.00 | --- | Big George | 21.00 | --- | 0.38 | 65.27 |
| D17 | --- | 1,376.00 | Big George | 34.00 | 55.00 | 0.62 | 66.39 |
| D18 | 1,376.00 | --- | Big George | 4.50 | --- | 0.07 | 66.54 |
| D18 | --- | --- | Big George | 21.00 | --- | 0.32 | 67.22 |
| D18 | --- | --- | Big George | 28.00 | --- | 0.42 | 68.14 |
| D18 | --- | 1378.00 | Big George | 12.50 | 66.00 | 0.19 | 68.55 |
| D19 | 1,378.00 | 1,380.00 | Big George | 63.00 | 63.00 | 1.00 | 70.62 |
| D23 | 1,380.00 | 1,382.00 | Big George | 66.00 | 66.00 | 1.00 | 72.79 |
| D25 | 1,382.00 | 1,384.00 | Big George | 67.00 | 67.00 | 1.00 | 74.98 |
| D26 | 1,384.00 | --- | Big George | 44.00 | --- | 0.66 | 76.43 |
| D26 | --- | 1,386.00 | Big George | 23.00 | 67.00 | 0.34 | 77.18 |
| D28 | 1,386.00 | --- | Big George | 27.00 | --- | 0.44 | 78.07 |
| D28 | --- | 1,388.00 | Big George | 34.00 | 61.00 | 0.56 | 79.18 |
| ns2 | 1,388.00 | 1,389.50 | ns2 | 46.00 | 46.00 | 1.00 | 80.69 |
| 26 | 1,389.50 | 1,391.50 | Big George | 62.00 | 62.00 | 1.00 | 82.73 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D35 | 26.3 | 75.3 | 0.0 | 4 | 158.00 | 452.00 | 25.90 |
| D36 | 1.8 | 107.7 | 3.0 | 1 | 11.00 | 646.00 | 1.67 |
| D37 | 8.6 | 109.4 | 2.0 | 3 | 51.50 | 656.50 | 7.25 |
| D38 | 4.3 | 68.4 | 5.0 | 1 | 39.00 | 616.00 | 5.91 |
| D39 | 30.5 | 26.2 | 10.0 | 4 | 366.00 | 314.00 | 53.04 |
| D40 | 2.5 | 169.5 | 2.0 | 1 | 10.00 | 678.00 | 1.45 |
| D41 | 10.0 | 82.9 | 40.0 | 3 | 70.00 | 580.00 | 10.14 |
| D42 | 4.8 | 152.8 | 10.0 | 1 | 19.00 | 611.00 | 2.97 |
| D43 | 1.2 | 202.2 | 30.0 | 1 | 3.50 | 606.50 | 0.55 |
| D44 | 4.6 | 106.6 | 5.0 | 1 | 18.50 | 426.50 | 4.11 |
| D44 | 22.5 | 22.0 | 1.0 | 4 | 45.00 | 44.00 | 50.00 |
| D45 | 6.0 | 39.9 | 3.0 | 3 | 78.00 | 519.00 | 13.00 |
| D46 | 17.1 | 43.4 | 4.0 | 3 | 188.50 | 477.50 | 28.13 |
| ns1 | --- | --- | --- | --- | 0.00 | --- | --- |
| D47 | 14.4 | 37.6 | 16.0 | 3 | 173.00 | 451.00 | 27.03 |
| D48 | 18.3 | 58.0 | 10.0 | 3 | 146.00 | 464.00 | 23.55 |
| D49 | 12.9 | 51.7 | 15.0 | 3 | 128.50 | 516.50 | 19.47 |
| D50 | 7.4 | 62.6 | 10.0 | 3 | 52.00 | 438.00 | 10.40 |
| D50 | 7.4 | 8.9 | 2.0 | 3 | 44.50 | 53.50 | 44.50 |
| D51 | 13.0 | 314.5 | 5.0 | 3 | 26.00 | 629.00 | 3.94 |
| D52 | 11.6 | 78.7 | 8.0 | 3 | 81.00 | 551.00 | 12.66 |
| D53 | 7.0 | 58.6 | 5.0 | 3 | 69.50 | 585.50 | 10.53 |
| D54 | 4.3 | 44.0 | 5.0 | 1 | 13.00 | 132.00 | 8.67 |
| D54 | 8.3 | 101.8 | 50.0 | 3 | 33.00 | 407.00 | 6.73 |
| D55 | 9.4 | 49.9 | 8.0 | 3 | 93.50 | 498.50 | 15.58 |
| D56 | 19.7 | 48.7 | 5.0 | 3 | 177.00 | 438.00 | 28.55 |
| D5 | 9.4 | 52.1 | 25.0 | 3 | 94.00 | 521.00 | 14.69 |
| D8 | 3.1 | 77.2 | 8.0 | 1 | 27.50 | 694.50 | 3.77 |
| D9 | 7.9 | 35.7 | 20.0 | 3 | 110.00 | 500.00 | 17.46 |
| D10 | 38.5 | 42.6 | 10.0 | 4 | 346.50 | 383.50 | 46.82 |
| D11 | 2.8 | 66.1 | 10.0 | 1 | 25.50 | 594.50 | 4.05 |
| D12 | 7.0 | 5.0 | 5.0 | 3 | 90.42 | 64.58 | 56.51 |
| D12 | 0.0 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 |
| D12 | 0.0 | 0.0 | 50.0 | 8 | 0.00 | 0.00 | 0.00 |
| D12 | 2.0 | 8.0 | 2.0 | 2 | 23.60 | 94.40 | 19.67 |
| D15 | 2.0 | 10.0 | 5.0 | 2 | 24.17 | 120.83 | 16.11 |
| D15 | 15.0 | 5.0 | 19.0 | 3 | 330.75 | 110.25 | 71.90 |
| D16 | 37.5 | 67.5 | 10.0 | 4 | 225.00 | 405.00 | 35.16 |
| D17 | 30.0 | 5.0 | 5.0 | 5 | 175.71 | 29.29 | 83.67 |
| D17 | 7.0 | 5.0 | 0.0 | 3 | 198.33 | 141.67 | 58.33 |
| D18 | 2.0 | 2.0 | 0.0 | 2 | 22.50 | 22.50 | 50.00 |
| D18 | 7.0 | 5.0 | 0.0 | 3 | 122.50 | 87.50 | 58.33 |
| D18 | 30.0 | 5.0 | 0.0 | 5 | 240.00 | 40.00 | 85.71 |
| D18 | 3.0 | 8.0 | 0.0 | 2 | 34.09 | 90.91 | 27.27 |
| D19 | 6.4 | 37.5 | 15.0 | 3 | 90.00 | 525.00 | 14.29 |
| D23 | 7.8 | 42.6 | 5.0 | 3 | 101.00 | 554.00 | 15.30 |
| D25 | 20.0 | 35.4 | 5.0 | 4 | 240.50 | 424.50 | 35.90 |
| D26 | 14.9 | 28.6 | 5.0 | 3 | 149.00 | 286.00 | 33.86 |
| D26 | 6.0 | 36.0 | 20.0 | 3 | 30.00 | 180.00 | 13.04 |
| D28 | 6.2 | 36.3 | 15.0 | 3 | 37.00 | 218.00 | 13.70 |
| D28 | 7.0 | 163.0 | 0.0 | 3 | 14.00 | 326.00 | 4.12 |
| ns2 | --- | --- | --- | --- | --- | --- | --- |
| 26 | 13.1 | 18.6 | 50.0 | 3 | 236.00 | 334.00 | 38.06 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D35 | 74.10 | 0.00 | 25.90 | 74.10 | 0.00 | 30 | 33.33 |
| D36 | 97.88 | 0.45 | 1.67 | 97.88 | 0.45 | 25 | 40.00 |
| D37 | 92.46 | 0.28 | 7.25 | 92.46 | 0.28 | 45 | 22.22 |
| D38 | 93.33 | 0.76 | 5.91 | 93.33 | 0.76 | 40 | 25.00 |
| D39 | 45.51 | 1.45 | 53.04 | 45.51 | 1.45 | 20 | 50.00 |
| D40 | 98.26 | 0.29 | 1.45 | 98.26 | 0.29 | 30 | 33.33 |
| D41 | 84.06 | 5.80 | 10.14 | 84.06 | 5.80 | 45 | 22.22 |
| D42 | 95.47 | 1.56 | 2.97 | 95.47 | 1.56 | 15 | 66.67 |
| D43 | 94.77 | 4.69 | 0.55 | 94.77 | 4.69 | 20 | 50.00 |
| D44 | 94.78 | 1.11 | --- | --- | --- | 25 | 40.00 |
| D44 | 48.89 | 1.11 | 11.76 | 87.13 | 1.11 | 25 | 40.00 |
| D45 | 86.50 | 0.50 | 13.00 | 86.50 | 0.50 | 35 | 28.57 |
| D46 | 71.27 | 0.60 | 28.13 | 71.27 | 0.60 | 25 | 40.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- |
| D47 | 70.47 | 2.50 | 27.03 | 70.47 | 2.50 | 45 | 22.22 |
| D48 | 74.84 | 1.61 | 23.55 | 74.84 | 1.61 | 20 | 50.00 |
| D49 | 78.26 | 2.27 | 19.47 | 78.26 | 2.27 | 25 | 40.00 |
| D50 | 87.60 | 2.00 | --- | --- | --- | 25 | 40.00 |
| D50 | 53.50 | 2.00 | 16.08 | 81.92 | 2.00 | 30 | 33.33 |
| D51 | 95.30 | 0.76 | 3.94 | 95.30 | 0.76 | 30 | 33.33 |
| D52 | 86.09 | 1.25 | 12.66 | 86.09 | 1.25 | 15 | 66.67 |
| D53 | 88.71 | 0.76 | 10.53 | 88.71 | 0.76 | 22 | 45.45 |
| D54 | 88.00 | 3.33 | --- | --- | --- | 16 | 62.50 |
| D54 | 83.06 | 10.20 | 7.19 | 84.22 | 8.59 | 20 | 50.00 |
| D55 | 83.08 | 1.33 | 15.58 | 83.08 | 1.33 | 20 | 50.00 |
| D56 | 70.65 | 0.81 | 28.55 | 70.65 | 0.81 | 25 | 40.00 |
| D5 | 81.41 | 3.91 | 14.69 | 81.41 | 3.91 | 25 | 40.00 |
| D8 | 95.14 | 1.10 | 3.77 | 95.14 | 1.10 | 26 | 38.46 |
| D9 | 79.37 | 3.17 | 17.46 | 79.37 | 3.17 | 15 | 66.67 |
| D10 | 51.82 | 1.35 | 46.82 | 51.82 | 1.35 | 20 | 50.00 |
| D11 | 94.37 | 1.59 | 4.05 | 94.37 | 1.59 | 22 | 45.45 |
| D12 | 40.36 | 3.13 | --- | --- | --- | 12 | 83.33 |
| D12 | 0.00 | 0.00 | --- | --- | --- | 12 | 83.33 |
| D12 | 0.00 | 100.00 | --- | --- | --- | 12 | 83.33 |
| D12 | 78.67 | 1.67 | 18.39 | 25.64 | 9.19 | 12 | 83.33 |
| D15 | 80.56 | 3.33 | --- | --- | --- | 20 | 50.00 |
| D15 | 23.97 | 4.13 | 58.18 | 37.88 | 3.93 | 20 | 50.00 |
| D16 | 63.28 | 1.56 | 35.16 | 63.28 | 1.56 | 32 | 31.25 |
| D17 | 13.95 | 2.38 | --- | --- | --- | 30 | 33.33 |
| D17 | 41.67 | 0.00 | 68.01 | 31.08 | 0.91 | 30 | 33.33 |
| D18 | 50.00 | 0.00 | --- | --- | --- | 25 | 40.00 |
| D18 | 41.67 | 0.00 | --- | --- | --- | 25 | 40.00 |
| D18 | 14.29 | 0.00 | --- | --- | --- | 25 | 40.00 |
| D18 | 72.73 | 0.00 | 63.50 | 36.50 | 0.00 | 25 | 40.00 |
| D19 | 83.33 | 2.38 | 14.29 | 83.33 | 2.38 | 28 | 35.71 |
| D23 | 83.94 | 0.76 | 15.30 | 83.94 | 0.76 | 23 | 43.48 |
| D25 | 63.36 | 0.75 | 35.90 | 63.36 | 0.75 | 32 | 31.25 |
| D26 | 65.00 | 1.14 | --- | --- | --- | 20 | 50.00 |
| D26 | 78.26 | 8.70 | 26.72 | 69.55 | 3.73 | 20 | 50.00 |
| D28 | 80.74 | 5.56 | --- | --- | --- | 35 | 28.57 |
| D28 | 95.88 | 0.00 | 8.36 | 89.18 | 2.46 | --- | --- |
| ns2 | --- | --- | --- | --- | --- | --- | --- |
| 26 | 53.87 | 8.06 | 38.06 | 53.87 | 8.06 | 17 | 58.82 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: |
| D35 | 33.33 | 80.53 | SubA | Wood in top 10 cm . |
| D36 | 40.00 | 89.85 | --- |  |
| D37 | 22.22 | 87.03 | --- | Wood from 40 to 46 cm from top. |
| D38 | 25.00 | 89.30 | --- | Wood fracture zone from 54 to 56 cm . |
| D39 | 50.00 | 84.37 | --- | Wood from 7 to 15 cm from top. |
| D40 | 33.33 | 69.50 | --- | --- 7 |
| D41 | 22.22 | 88.29 | --- | Fusain from 56 to 59 cm , wood from 59 to 69 cm . |
| D42 | 66.67 | 85.21 | --- | Wood in top 15 cm . |
| D43 | 50.00 | 88.35 | --- | Fusain from 0 to 3 cm , wood from 3 to 15 cm . |
| D44 | --- | --- | --- | --- |
| D44 | 40.00 | 92.75 | --- | --- |
| D45 | 28.57 | 89.20 | --- | --- |
| D46 | 40.00 | 89.27 | --- | Wood from 8 to 19 cm . |
| ns1 | --- | --- | --- | No sample. |
| D47 | 22.22 | 77.96 | --- | Fusain from 40 to 42 cm , wood from 58 to 67 cm . |
| D48 | 50.00 | 98.59 | --- | Fusain |
| D49 | 40.00 | 68.27 | --- | --- |
| D50 | --- | --- | --- | --- |
| D50 | 38.89 | 98.20 | --- | --- |
| D51 | 33.33 | 98.87 | --- | --- |
| D52 | 66.67 | 63.01 | --- | - |
| D53 | 45.45 | 94.44 | --- | --- |
| D54 | --- | --- | --- | --- |
| D54 | 52.93 | 93.69 | --- | 2-cm thick-fusain at 35 and 45 cm . |
| D55 | 50.00 | 53.27 | --- | --- |
| D56 | 40.00 | 98.69 | --- | --- |
| D5 | 40.00 | 103.33 | --- | Fusain from 41 to 43 cm . |
| D8 | 38.46 | 101.98 | --- | --- |
| D9 | 66.67 | 89.69 | --- | Fusain from 18 to 19 cm . |
| D10 | 50.00 | 88.60 | --- | Wood from 1.5 to 2.3, 3.7 to 4.9 , and 52 to 62 cm , fusain at $62 \mathrm{~cm}(?)$. |
| D11 | 45.45 | 93.60 | --- | --- |
| D12 | --- | --- | --- | Attrital and vitrain band thicknesses are estimated. |
| D12 | --- | --- | --- | Clay. |
| D12 | --- | --- | --- | Fusain layer. |
| D12 | 83.33 | 59.58 | --- | Attrital and vitrain band thicknesses are estimated. |
| D15 | --- | --- | --- | Attrital and vitrain band thicknesses are estimated. |
| D15 | 50.00 | 87.63 | --- | Attrital and vitrain band thicknesses are estimated. |
| D16 | 31.25 | 87.57 | --- | --- |
| D17 | --- | --- | --- | $60-\mathrm{mm}$-thick vitrain band at 15 cm , attrital and vitrain band thicknesses are estimated. |
| D17 | 33.33 | 90.32 | --- | Attrital and vitrain band thicknesses are estimated. |
| D18 | --- | --- | --- | Attrital and vitrain band thicknesses are estimated. |
| D18 | --- | --- | --- | Attrital and vitrain band thicknesses are estimated. |
| D18 | --- | --- | --- | $75-\mathrm{mm}$-thick vitrain band at 40 cm , attrital and vitrain band thicknesses are estimated. |
| D18 | 40.00 | 93.39 | -- | Attrital and vitrain band thicknesses are estimated. |
| D19 | 35.71 | 77.29 | --- | $4-\mathrm{mm}$-thick fusain bands at 15 and 19 cm . |
| D23 | 43.48 | 100.44 | --- | --- |
| D25 | 31.25 | 97.92 | --- | --- |
| D26 | --- | --- | --- | Wood in top 70 mm . |
| D26 | 50.00 | 70.49 | --- | Fusain in top 25 mm , scattered fusain throughout(?). |
| D28 | --- | --- | --- | Fusain in top 15 cm . |
| D28 | 28.57 | 67.35 | SubB | --- |
| ns2 | --- | --- | --- | No sample. |
| 26 | 58.82 | 86.47 | --- | Fusain from 30 to 32 cm and 49 to 52 cm . |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Approximate depth (ft) |  | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |
| 27 | 1,391.50 | 1,393.50 | Big George | 63.00 | 63.00 | 1.00 | 84.79 |
| 28 | 1,393.50 | --- | Big George | 36.00 | --- | 0.60 | 85.97 |
| 28 | --- | --- | Big George | 14.50 | --- | 0.24 | 86.45 |
| 28 | --- | 1,395.50 | Big George | 9.50 | 60.00 | 0.16 | 86.76 |
| 29 | 1,395.50 | --- | Big George | 35.00 | --- | 0.53 | 87.91 |
| 29 | --- | 1,397.50 | Big George | 31.00 | 66.00 | 0.47 | 88.93 |
| 30 | 1,397.50 | --- | Big George | 6.00 | --- | 0.10 | 89.12 |
| 30 | --- | 1,399.50 | Big George | 57.00 | 63.00 | 0.90 | 90.99 |
| 31 | 1,399.50 | --- | Big George | 58.00 | --- | 0.91 | 92.90 |
| 31 | --- | 1,401.50 | Big George | 6.00 | 64.00 | 0.09 | 93.09 |
| 32 | 1,401.50 | --- | Big George | 6.00 | --- | 0.09 | 93.29 |
| 32 | --- | 1,403.50 | Big George | 60.00 | 66.00 | 0.91 | 95.26 |
| 33 | 1,403.50 | --- | Big George | 15.00 | --- | 0.23 | 95.75 |
| 33 | --- | --- | Big George | 17.00 | --- | 0.27 | 96.31 |
| 33 | --- | 1,405.50 | Big George | 32.00 | 64.00 | 0.50 | 97.36 |
| 34 | 1,405.50 | 1,407.50 | Big George | 62.00 | 62.00 | 1.00 | 99.39 |
| 35 | 1,407.50 | --- | Big George | 39.00 | --- | 0.63 | 100.67 |
| 35 | --- | --- | Big George | 5.00 | --- | 0.08 | 100.84 |
| 35 | --- | 1,409.50 | Big George | 18.00 | 62.00 | 0.29 | 101.43 |
| 36 | 1,409.50 | 1,411.50 | Big George | 65.00 | 65.00 | 1.00 | 103.56 |
| 37 | 1,411.50 | 1,413.50 | Big George | 63.00 | 63.00 | 1.00 | 105.63 |
| 38 | 1,413.50 | 1,415.50 | Big George | 63.00 | 63.00 | 1.00 | 107.69 |
| 39 | 1,415.50 | 1,417.50 | Big George | 52.00 | 52.00 | 1.00 | 109.40 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 4.5 | 36.5 | 14.0 | 1 | 68.00 | 548.00 | 10.79 |
| 28 | 1.0 | 59.0 | 0.0 | 1 | 6.00 | 354.00 | 1.67 |
| 28 | 12.7 | 8.0 | 0.0 | 3 | 89.00 | 56.00 | 61.38 |
| 28 | 0.0 | 85.5 | 9.5 | 1 | 0.00 | 85.50 | 0.00 |
| 29 | 13.6 | 35.1 | 9.0 | 3 | 95.00 | 246.00 | 27.14 |
| 29 | 6.5 | 148.5 | 0.0 | 3 | 13.00 | 297.00 | 4.19 |
| 30 | 2.4 | 12.6 | 0.0 | 2 | 9.50 | 50.50 | 15.83 |
| 30 | 7.6 | 35.5 | 10.0 | 3 | 99.00 | 461.00 | 17.37 |
| 31 | 23.4 | 39.9 | 10.0 | 4 | 211.00 | 359.00 | 36.38 |
| 31 | 0.0 | 0.0 | 60.0 | 8 | 0.00 | 0.00 | 0.00 |
| 32 | 0.0 | 0.0 | 60.0 | 8 | 0.00 | 0.00 | 0.00 |
| 32 | 11.8 | 41.8 | 10.0 | 3 | 130.00 | 460.00 | 21.67 |
| 33 | 6.8 | 65.8 | 5.0 | 3 | 13.50 | 131.50 | 9.00 |
| 33 | 0.0 | 0.0 | 170.0 | 8 | 0.00 | 0.00 | 0.00 |
| 33 | 3.0 | 75.8 | 5.0 | 1 | 12.00 | 303.00 | 3.75 |
| 34 | 8.3 | 40.8 | 30.0 | 3 | 100.00 | 490.00 | 16.13 |
| 35 | 6.8 | 57.3 | 5.0 | 3 | 41.00 | 344.00 | 10.51 |
| 35 | 0.0 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 0.00 |
| 35 | 5.7 | 53.0 | 4.0 | 3 | 17.00 | 159.00 | 9.44 |
| 36 | 7.2 | 64.8 | 2.0 | 3 | 65.00 | 583.00 | 10.00 |
| 37 | 3.6 | 74.6 | 5.0 | 1 | 28.50 | 596.50 | 4.52 |
| 38 | 5.0 | 64.4 | 5.0 | 3 | 45.00 | 580.00 | 7.14 |
| 39 | 7.7 | 95.9 | 2.0 | 3 | 38.50 | 479.50 | 7.40 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 86.98 | 2.22 | 10.79 | 86.98 | 2.22 | 35 | 28.57 |
| 28 | 98.33 | 0.00 | --- | --- | --- | 30 | 33.33 |
| 28 | 38.62 | 0.00 | --- | --- | --- | 30 | 33.33 |
| 28 | 90.00 | 10.00 | 15.83 | 82.58 | 1.58 | 30 | 33.33 |
| 29 | 70.29 | 2.57 | --- | --- | --- | 18 | 55.56 |
| 29 | 95.81 | 0.00 | 16.36 | 82.27 | 1.36 | 18 | 55.56 |
| 30 | 84.17 | 0.00 | --- | --- | --- | 25 | 40.00 |
| 30 | 80.88 | 1.75 | 17.22 | 81.19 | 1.59 | 25 | 40.00 |
| 31 | 61.90 | 1.72 | --- | --- | --- | 15 | 66.67 |
| 31 | 0.00 | 100.00 | 32.97 | 56.09 | 10.94 | 15 | 66.67 |
| 32 | 0.00 | 100.00 | --- | --- | --- | 22 | 45.45 |
| 32 | 76.67 | 1.67 | 19.70 | 69.70 | 10.61 | 22 | 45.45 |
| 33 | 87.67 | 3.33 | - | --- | --- | 27 | 37.04 |
| 33 | 0.00 | 100.00 | --- | --- | --- | 27 | 37.04 |
| 33 | 94.69 | 1.56 | 3.98 | 67.89 | 28.13 | 27 | 37.04 |
| 34 | 79.03 | 4.84 | 16.13 | 79.03 | 4.84 | 20 | 50.00 |
| 35 | 88.21 | 1.28 | --- | --- | --- | 22 | 45.45 |
| 35 | 0.00 | 0.00 | --- | --- | --- | 22 | 45.45 |
| 35 | 88.33 | 2.22 | 9.35 | 81.13 | 1.45 | 22 | 45.45 |
| 36 | 89.69 | 0.31 | 10.00 | 89.69 | 0.31 | 20 | 50.00 |
| 37 | 94.68 | 0.79 | 4.52 | 94.68 | 0.79 | 22 | 45.45 |
| 38 | 92.06 | 0.79 | 7.14 | 92.06 | 0.79 | 15 | 66.67 |
| 39 | 92.21 | 0.38 | 7.40 | 92.21 | 0.38 | 60 | 16.67 |

Table 1-22. Data for samples from core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; SubB, subbituminous B; HvolC, high-volatile C; ---, no data]

| Canister number | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: |
| 27 | 28.57 | 86.97 | --- | Fusain from 50 to 64 cm . |
| 28 | --- | --- | --- | --- |
| 28 | --- | --- | --- | --- |
| 28 | 33.33 | 87.83 | --- | Very hard fusain. |
| 29 | --- | --- | --- | --- |
| 29 | 55.56 | 94.72 | --- | Fusain(?). |
| 30 | --- | --- | --- | Dispersed fusain(?). |
| 30 | 40.00 | 93.27 | --- | Dispersed fusain(?) (a bit dull and sooty). |
| 31 | --- | --- | --- | Wood in top 7 cm . |
| 31 | 66.67 | 88.39 | --- | Hard fusain layer. |
| 32 | --- | --- | --- | Hard fusain layer. |
| 32 | 45.45 | 96.30 | --- | Wood in top 45 mm . |
| 33 | --- | --- | --- | --- |
| 33 | --- | --- | --- | Fusain layer. |
| 33 | 37.04 | 78.48 | --- | --- |
| 34 | 50.00 | 82.06 | --- | Fusain at $54-56 \mathrm{~cm}, 57-58 \mathrm{~cm}, 60-61 \mathrm{~cm}$. |
| 35 | --- | --- | --- | --- |
| 35 | --- | -- | --- | Clay. |
| 35 | 45.45 | 87.53 | --- | --- |
| 36 | 50.00 | 88.20 | --- | --- |
| 37 | 45.45 | 86.82 | --- | --- |
| 38 | 66.67 | 87.42 | --- | Clay $50.5-51 \mathrm{~cm}$ from top. |
| 39 | 16.67 | 82.91 | HvolC | Wood in top 33 cm . |

Table 1-23. Data for samples from core hole 27, Peabody Natural Gas LLC, Carter-Federal 18F-D.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 5 | 1,527.00 | 1,529.00 | Pawnee | 50.00 | 50.00 | 1.00 | 1.64 | 3.9 | 49.4 | 20.0 |
| 4 | 1,529.00 | 1,531.00 | Pawnee | 52.00 | 52.00 | 1.00 | 3.35 | 12.2 | 83.8 | 40.0 |
| 3 | 1,531.00 | 1,533.00 | Pawnee | 56.00 | 56.00 | 1.00 | 5.18 | 7.2 | 35.3 | 50.0 |
| 2 | 1,533.00 | 1,535.00 | Pawnee | 58.00 | 58.00 | 1.00 | 7.09 | 11.9 | 63.9 | 50.0 |
| 1 | 1,535.00 | 1,537.00 | Pawnee | 50.00 | 50.00 | 1.00 | 8.73 | 28.4 | 51.6 | 100.0 |
| 9 | 1,537.00 | --- | Pawnee | 27.00 | --- | 0.48 | 9.61 | 7.9 | 27.9 | 20.0 |
| 9 | --- | 1,539.50 | Pawnee | 29.00 | 56.00 | 0.52 | 10.56 | 6.4 | 20.7 | 100.0 |
| 8 | 1,539.50 | 1,542.00 | Pawnee | 56.00 | 56.00 | 1.00 | 12.40 | 11.4 | 41.9 | 80.0 |
| 7 | 1,542.00 | 1,544.50 | Pawnee | 54.00 | 54.00 | 1.00 | 14.17 | 18.3 | 30.5 | 150.0 |
| 6 | 1,544.50 | 1,547.00 | Pawnee | 57.00 | 57.00 | 1.00 | 16.04 | 3.2 | 163.5 | 70.0 |
| 12 | 1,547.00 | 1,549.00 | Pawnee | 39.00 | 39.00 | 1.00 | 17.32 | 9.8 | 82.8 | 20.0 |
| 11 | 1,549.00 | --- | Pawnee | 40.00 | --- | 0.87 | 18.64 | 6.7 | 120.0 | 20.0 |
| 11 | --- | 1,551.00 | Pawnee | 6.00 | 46.00 | 0.13 | 18.83 | 0.0 | 0.0 | 0.0 |
| ns1 | 1,551.00 | 1,704.00 | ns 1 | 4667.00 | 4,667.00 | 1.00 | 171.95 | --- | --- | --- |
| 14 | 1,704.00 | 1,706.00 | Cache | 59.00 | 59.00 | 1.00 | 173.88 | 8.1 | 61.9 | 30.0 |
| 13 | 1,706.00 | 1,708.00 | Cache | 58.00 | 58.00 | 1.00 | 175.79 | 2.5 | 135.0 | 30.0 |
| 19 | 1,708.00 | 1,710.00 | Cache | 65.00 | 65.00 | 1.00 | 177.92 | 5.4 | 43.1 | 20.0 |
| 18 | 1,710.00 | 1,712.00 | Cache | 65.00 | 65.00 | 1.00 | 180.05 | 9.2 | 40.8 | 100.0 |
| 17 | 1,712.00 | 1,714.00 | Cache | 46.00 | 46.00 | 1.00 | 181.56 | 5.5 | 99.5 | 40.0 |
| 16 | 1,714.00 | 1,716.00 | Cache | 57.00 | 57.00 | 1.00 | 183.43 | 6.2 | 32.3 | 70.0 |
| 15 | 1,716.00 | 1,718.00 | Cache | 54.00 | 54.00 | 1.00 | 185.20 | 3.2 | 29.3 | 20.0 |
| 24 | 1,718.00 | 1,720.00 | Cache | 58.00 | 58.00 | 1.00 | 187.11 | 5.9 | 34.1 | 20.0 |
| 23 | 1,720.00 | 1,722.00 | Cache | 55.00 | 55.00 | 1.00 | 188.91 | 8.7 | 32.1 | 20.0 |
| 22 | 1,722.00 | --- | Cache | 40.00 | --- | 0.73 | 190.22 | 13.7 | 40.6 | 20.0 |
| 22 | --- | 1,724.00 | Cache | 15.00 | 55.00 | 0.27 | 190.72 | 1.9 | 26.1 | 10.0 |
| 21 | 1,724.00 | 1,726.00 | Cache | 54.00 | 54.00 | 1.00 | 192.49 | 3.7 | 40.9 | 50.0 |
| 20 | 1,726.00 | 1,728.00 | Cache | 55.00 | 55.00 | 1.00 | 194.29 | 12.7 | 29.0 | 50.0 |
| 43 | 1,728.00 | 1,729.00 | Cache | 46.00 | 46.00 | 1.00 | 195.80 | 6.2 | 32.9 | 30.0 |
| 42 | 1,729.00 | 1,731.00 | Cache | 52.00 | 52.00 | 1.00 | 197.51 | 9.0 | 40.0 | 30.0 |
| 40 | 1,731.00 | --- | Cache | 20.25 | --- | 0.36 | 198.17 | 4.0 | 28.1 | 10.0 |
| 40 | --- | 1,733.00 | Cache | 35.75 | 56.00 | 0.64 | 199.34 | 4.8 | 18.6 | 100.0 |
| 25 | 1,733.00 | --- | Cache | 36.00 | --- | 0.60 | 200.52 | 32.1 | 15.0 | 30.0 |
| 25 | --- | 1,735.00 | Cache | 24.00 | 60.00 | 0.40 | 201.31 | 1.9 | 58.1 | 0.0 |

Table 1-23. Data for samples from core hole 27, Peabody Natural Gas LLC, Carter-Federal 18F-D.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | $\begin{gathered} \text { Canister } \\ \text { average } \\ \text { attrital } \\ \text { percentage } \\ \text { (CaAvAP) } \end{gathered}$ | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1 | 35.00 | 445.00 | 7.00 | 89.00 | 4.00 | 7.00 | 89.00 | 4.00 |
| 4 | 3 | 61.00 | 419.00 | 11.73 | 80.58 | 7.69 | 11.73 | 80.58 | 7.69 |
| 3 | 3 | 86.00 | 424.00 | 15.36 | 75.71 | 8.93 | 15.36 | 75.71 | 8.93 |
| 2 | 3 | 83.00 | 447.00 | 14.31 | 77.07 | 8.62 | 14.31 | 77.07 | 8.62 |
| 1 | 4 | 142.00 | 258.00 | 28.40 | 51.60 | 20.00 | 28.40 | 51.60 | 20.00 |
| 9 | 3 | 55.00 | 195.00 | 20.37 | 72.22 | 7.41 | --- | --- | --- |
| 9 | 3 | 45.00 | 145.00 | 15.52 | 50.00 | 34.48 | 17.86 | 60.71 | 21.43 |
| 8 | 3 | 102.50 | 377.50 | 18.30 | 67.41 | 14.29 | 18.30 | 67.41 | 14.29 |
| 7 | 3 | 146.00 | 244.00 | 27.04 | 45.19 | 27.78 | 27.04 | 45.19 | 27.78 |
| 6 | 1 | 9.50 | 490.50 | 1.67 | 86.05 | 12.28 | 1.67 | 86.05 | 12.28 |
| 12 | 3 | 39.00 | 331.00 | 10.00 | 84.87 | 5.13 | 10.00 | 84.87 | 5.13 |
| 11 | 3 | 20.00 | 360.00 | 5.00 | 90.00 | 5.00 | 5.00 | 90.00 | 5.00 |
| 11 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 14 | 3 | 65.00 | 495.00 | 11.02 | 83.90 | 5.08 | 11.02 | 83.90 | 5.08 |
| 13 | 1 | 10.00 | 540.00 | 1.72 | 93.10 | 5.17 | 1.72 | 93.10 | 5.17 |
| 19 | 3 | 70.00 | 560.00 | 10.77 | 86.15 | 3.08 | 10.77 | 86.15 | 3.08 |
| 18 | 3 | 101.50 | 448.50 | 15.62 | 69.00 | 15.38 | 15.62 | 69.00 | 15.38 |
| 17 | 3 | 22.00 | 398.00 | 4.78 | 86.52 | 8.70 | 4.78 | 86.52 | 8.70 |
| 16 | 3 | 80.00 | 420.00 | 14.04 | 73.68 | 12.28 | 14.04 | 73.68 | 12.28 |
| 15 | 1 | 51.00 | 469.00 | 9.44 | 86.85 | 3.70 | 9.44 | 86.85 | 3.70 |
| 24 | 3 | 83.00 | 477.00 | 14.31 | 82.24 | 3.45 | 14.31 | 82.24 | 3.45 |
| 23 | 3 | 112.50 | 417.50 | 20.45 | 75.91 | 3.64 | 20.45 | 75.91 | 3.64 |
| 22 | 3 | 96.00 | 284.00 | 24.00 | 71.00 | 5.00 | --- | --- | --- |
| 22 | 1 | 9.50 | 130.50 | 6.33 | 87.00 | 6.67 | 19.18 | 75.36 | 5.45 |
| 21 | 1 | 40.50 | 449.50 | 7.50 | 83.24 | 9.26 | 7.50 | 83.24 | 9.26 |
| 20 | 3 | 152.00 | 348.00 | 27.64 | 63.27 | 9.09 | 27.64 | 63.27 | 9.09 |
| 43 | 3 | 68.00 | 362.00 | 14.78 | 78.70 | 6.52 | 14.78 | 78.70 | 6.52 |
| 42 | 3 | 90.00 | 400.00 | 17.31 | 76.92 | 5.77 | 17.31 | 76.92 | 5.77 |
| 40 | 1 | 24.00 | 168.50 | 11.85 | 83.21 | 4.94 | --- | --- | --- |
| 40 | 2 | 53.00 | 204.50 | 14.83 | 57.20 | 27.97 | 13.75 | 66.61 | 19.64 |
| 25 | 4 | 225.00 | 105.00 | 62.50 | 29.17 | 8.33 | --- | --- | --- |
| 25 | 1 | 7.50 | 232.50 | 3.13 | 96.88 | 0.00 | 38.75 | 56.25 | 5.00 |

Table 1-23. Data for samples from core hole 27, Peabody Natural Gas LLC, Carter-Federal 18F-D.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 20 | 50.00 | 50.00 | 8.51 | SubB | Clay on cleat. |
| 4 | 12 | 83.33 | 83.33 | 8.31 | --- | Clay on cleat, wood from 22 to 29 cm . |
| 3 | 20 | 50.00 | 50.00 | 7.97 | --- | Some clay on cleat. |
| 2 | 16 | 62.50 | 62.50 | 8.59 | --- | Some clay on cleat. |
| 1 | 25 | 40.00 | 40.00 | 8.97 | --- | Some clay on cleat. |
| 9 | 20 | 50.00 | --- | --- | --- | Some clay on cleat. |
| 9 | 20 | 50.00 | 50.00 | 7.58 | --- | Some clay on cleat, fusain from 30 to 30.5 cm . |
| 8 | 21 | 47.62 | 47.62 | 9.22 | --- | Some clay on cleat, highly fractured sample. |
| 7 | 20 | 50.00 | 50.00 | 8.45 | --- | Clay on cleat, fusain from 32 to 33 cm . |
| 6 | 22 | 45.45 | 45.45 | 8.61 | --- | Highly fractured sample. |
| 12 | --- | --- | --- | 5.14 | --- | Highly fractured sample. |
| 11 | 32 | 31.25 | 31.25 | 4.51 | SubB | Clay on cleat. |
| 11 | --- | --- | --- | --- | --- | Clay. |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| 14 | 26 | 38.46 | 38.46 | 2.78 | SubB | Some clay. |
| 13 | 20 | 50.00 | 50.00 | 2.77 | --- | --- |
| 19 | 27 | 37.04 | 37.04 | 1.98 | -- | --- |
| 18 | 15 | 66.67 | 66.67 | 2.53 | --- | --- |
| 17 | 18 | 55.56 | 55.56 | 1.25 | --- | --- |
| 16 | 21 | 47.62 | 47.62 | 1.76 | -- | --- |
| 15 | 24 | 41.67 | 41.67 | 1.96 | -- | --- |
| 24 | 25 | 40.00 | 40.00 | 2.55 | -- | . |
| 23 | 22 | 45.45 | 45.45 | 2.13 | -- | --- |
| 22 | 12 | 83.33 | --- | --- | --- | --- |
| 22 | 12 | 83.33 | 83.33 | 2.58 | --- | - |
| 21 | 19 | 52.63 | 52.63 | 1.98 | --- | Sample taken for adsorption analysis. |
| 20 | 30 | 33.33 | 33.33 | 2.12 | --- | --- |
| 43 | 30 | 33.33 | 33.33 | 1.75 | --- | . |
| 42 | 15 | 66.67 | 66.67 | 2.43 | --- | --- |
| 40 | 19 | 52.63 | --- | --- | --- | --- |
| 40 | 19 | 52.63 | 52.63 | 1.90 | --- | --- |
| 25 | 22 | 45.45 | --- | --- | --- | --- |
| 25 | 22 | 45.45 | 45.45 | 2.62 | SubB | High ash content(?). |

Table 1-24. Data for samples from core hole 28, Nance Petroleum Corporation, Remington 58-79-30-07A.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Appro dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| B5 | 320.00 | --- | Anderson | 14.00 | --- | 0.32 | 0.46 | 4.3 | 42.0 |
| B5 | --- | --- | Anderson | 13.00 | --- | 0.30 | 0.89 | 50.0 | 80.0 |
| B5 | --- | 322.00 | Anderson | 17.00 | 44.00 | 0.39 | 1.44 | 2.0 | 40.3 |
| B6 | 322.00 | --- | Anderson | 25.00 | --- | 0.41 | 2.26 | 14.1 | 21.6 |
| B6 | --- | 324.00 | Anderson | 36.00 | 61.00 | 0.59 | 3.44 | 5.5 | 39.5 |
| B7 | 324.00 | 326.00 | Anderson | 63.00 | 63.00 | 1.00 | 5.51 | 12.2 | 29.8 |
| B13 | 326.00 | --- | Anderson | 42.00 | --- | 0.71 | 6.89 | 5.7 | 35.6 |
| B13 | --- | 328.00 | Anderson | 17.00 | 59.00 | 0.29 | 7.45 | 42.5 | 35.0 |
| B9 | 328.00 | 330.00 | Anderson | 60.00 | 60.00 | 1.00 | 9.42 | 4.4 | 41.5 |
| B10 | 330.00 | --- | Anderson | 36.00 | --- | 0.59 | 10.60 | 1.6 | 49.9 |
| B10 | --- | --- | Anderson | 17.00 | --- | 0.28 | 11.15 | 5.8 | 22.2 |
| B10 | --- | 332.00 | Anderson | 8.00 | 61.00 | 0.13 | 11.42 | 80.0 | 0.0 |
| B15 | 332.00 | 334.00 | Anderson | 63.00 | 63.00 | 1.00 | 13.48 | 4.0 | 37.9 |
| B12 | 334.00 | 336.00 | Anderson | 43.00 | 43.00 | 1.00 | 14.90 | 4.9 | 48.8 |

Table 1-24. Data for samples from core hole 28, Nance Petroleum Corporation, Remington 58-79-30-07A.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B5 | 1.0 | 1 | 13.00 | 126.00 | 9.29 | 90.00 | 0.71 | --- | --- |
| B5 | 0.0 | 4 | 50.00 | 80.00 | 38.46 | 61.54 | 0.00 | --- | --- |
| B5 | 1.0 | 1 | 8.00 | 161.00 | 4.71 | 94.71 | 0.59 | 16.14 | 83.41 |
| B6 | 0.0 | 3 | 99.00 | 151.00 | 39.60 | 60.40 | 0.00 | --- | -- |
| B6 | 0.0 | 3 | 44.00 | 316.00 | 12.22 | 87.78 | 0.00 | 23.44 | 76.56 |
| B7 | 0.0 | 3 | 183.00 | 447.00 | 29.05 | 70.95 | 0.00 | 29.05 | 70.95 |
| B13 | 7.0 | 3 | 57.00 | 356.00 | 13.57 | 84.76 | 1.67 | --- | --- |
| B13 | 15.0 | 4 | 85.00 | 70.00 | 50.00 | 41.18 | 8.82 | 24.07 | 72.20 |
| B9 | 3.0 | 1 | 57.00 | 540.00 | 9.50 | 90.00 | 0.50 | 9.50 | 90.00 |
| B10 | 0.0 | 1 | 11.00 | 349.00 | 3.06 | 96.94 | 0.00 | --- | --- |
| B10 | 2.0 | 3 | 35.00 | 133.00 | 20.59 | 78.24 | 1.18 | --- | --- |
| B10 | 0.0 | 5 | 80.00 | 0.00 | 100.00 | 0.00 | 0.00 | 20.66 | 79.02 |
| B15 | 1.0 | 1 | 60.00 | 569.00 | 9.52 | 90.32 | 0.16 | 9.52 | 90.32 |
| B12 | 1.0 | 1 | 39.00 | 390.00 | 9.07 | 90.70 | 0.23 | 9.07 | 90.70 |

Table 1-24. Data for samples from core hole 28, Nance Petroleum Corporation, Remington 58-79-30-07A.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubC, subbituminous C; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B5 | --- | 42 | 23.81 | --- | --- | --- | Metallic grease from drill on core. |
| B5 | --- | 55 | 18.18 | --- | --- | --- | Hard. |
| B5 | 0.45 | 50 | 20.00 | 20.67 | 14.04 | --- | --- |
| B6 | --- | 20 | 50.00 | --- | --- | --- | --- |
| B6 | 0.00 | 30 | 33.33 | 40.16 | 15.54 | SubC | --- |
| B7 | 0.00 | 30 | 33.33 | 33.33 | 15.13 | --- | Broken material. |
| B13 | --- | 45 | 22.22 | --- | --- | --- | --- |
| B13 | 3.73 | 60 | 16.67 | 20.62 | 15.13 | --- | --- |
| B9 | 0.50 | 40 | 25.00 | 25.00 | 14.61 | SubC | --- |
| B10 | --- | 30 | 33.33 | --- | --- | --- | Clay on cleats. |
| B10 | --- | 35 | 28.57 | --- | --- | --- | --- |
| B10 | 0.33 | 70 | 14.29 | 29.51 | 14.61 | --- | --- |
| B15 | 0.16 | 45 | 22.22 | 22.22 | 15.13 | --- | --- |
| B12 | 0.23 | 50 | 20.00 | 20.00 | 14.61 | SubC | --- |

Table 1-25. Data for samples from core hole 30, Nance Petroleum Corporation, Remington 58-79-30-01C.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubB, subbituminous B; ---, no data]

| Canister number | Approx dept | mate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| B16 | 633.00 | 635.00 | Canyon | 54.00 | 54.00 | 1.00 | 1.77 | 6.3 | 32.9 | 30.0 |
| B17 | 635.00 | 637.00 | Canyon | 57.00 | 57.00 | 1.00 | 3.64 | 11.5 | 17.8 | 13.0 |
| B18 | 637.00 | --- | Canyon | 25.00 | --- | 0.42 | 4.46 | 42.4 | 7.2 | 2.0 |
| B18 | --- | 639.00 | Canyon | 35.00 | 60.00 | 0.58 | 5.61 | 3.3 | 27.6 | 10.0 |
| B19 | 639.00 | 641.00 | Canyon | 60.00 | 60.00 | 1.00 | 7.58 | 10.5 | 49.5 | 0.0 |
| B20 | 641.00 | --- | Canyon | 15.00 | --- | 0.25 | 8.07 | 57.5 | 17.5 | 0.0 |
| B20 | --- | 643.00 | Canyon | 45.00 | 60.00 | 0.75 | 9.55 | 7.6 | 33.1 | 2.0 |
| B21 | 643.00 | 645.00 | Canyon | 54.00 | 54.00 | 1.00 | 11.32 | 5.5 | 32.7 | 5.0 |
| B22 | 645.00 | --- | Canyon | 32.00 | --- | 0.53 | 12.37 | 28.9 | 16.6 | 2.0 |
| B22 | --- | 647.00 | Canyon | 28.00 | 60.00 | 0.47 | 13.29 | 2.2 | 28.9 | 0.0 |

Table 1-25. Data for samples from core hole 30, Nance Petroleum Corporation, Remington 58-79-30-01C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B16 | 3 | 82.00 | 428.00 | 15.19 | 79.26 | 5.56 | 15.19 | 79.26 | 5.56 |
| B17 | 3 | 218.00 | 339.00 | 38.25 | 59.47 | 2.28 | 38.25 | 59.47 | 2.28 |
| B18 | 4 | 212.00 | 36.00 | 84.80 | 14.40 | 0.80 | --- | --- | --- |
| B18 | 1 | 36.00 | 304.00 | 10.29 | 86.86 | 2.86 | 41.33 | 56.67 | 2.00 |
| B19 | 3 | 105.00 | 495.00 | 17.50 | 82.50 | 0.00 | 17.50 | 82.50 | 0.00 |
| B20 | 4 | 115.00 | 35.00 | 76.67 | 23.33 | 0.00 | --- | --- | --- |
| B20 | 3 | 84.00 | 364.00 | 18.67 | 80.89 | 0.44 | 33.17 | 66.50 | 0.33 |
| B21 | 3 | 77.00 | 458.00 | 14.26 | 84.81 | 0.93 | 14.26 | 84.81 | 0.93 |
| B22 | 4 | 202.00 | 116.00 | 63.13 | 36.25 | 0.63 | --- | --- | --- |
| B22 | 1 | 20.00 | 260.00 | 7.14 | 92.86 | 0.00 | 37.00 | 62.67 | 0.33 |

Table 1-25. Data for samples from core hole 30, Nance Petroleum Corporation, Remington 58-79-30-01C.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B16 | 35 | 28.57 | 28.57 | 19.99 | SubB | Very hard, abundant fusain. |
| B17 | 30 | 33.33 | 33.33 | 19.35 | --- | Fusain band from 39 to 40 cm . |
| B18 | 30 | 33.33 | --- | --- | --- | --- |
| B18 | 40 | 25.00 | 28.47 | 20.31 | --- | Abundant fusain in attritus bands. |
| B19 | 25 | 40.00 | 40.00 | 19.55 | SubB | Mostly laminated with 1-cm-thick woody band. |
| B20 | 25 | 40.00 | --- | --- | --- | --- |
| B20 | 70 | 14.29 | 20.71 | 18.95 | --- | --- |
| B21 | 30 | 33.33 | 33.33 | 22.47 | --- | --- |
| B22 | 30 | 33.33 | --- | --- | --- | --- |
| B22 | 13 | 76.92 | 53.68 | 17.91 | SubB | 2-cm-thick clay band at 40 cm , small number of resin blebs. |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approx <br> depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| C7 | 1,402.90 | --- | Big George | 6.00 | --- | 0.09 | 0.20 | 60.0 | 0.0 | 0.0 |
| C7 | --- | --- | Big George | 4.00 | --- | 0.06 | 0.33 | 5.0 | 35.0 | 0.0 |
| C7 | --- | --- | Big George | 6.00 | --- | 0.09 | 0.52 | 60.0 | 0.0 | 0.0 |
| C7 | --- | --- | Big George | 14.00 | --- | 0.22 | 0.98 | 10.0 | 60.0 | 0.0 |
| C7 | --- | --- | Big George | 6.00 | --- | 0.09 | 1.18 | 60.0 | 0.0 | 0.0 |
| C7 | --- | --- | Big George | 18.00 | --- | 0.28 | 1.77 | 15.0 | 45.0 | 0.0 |
| C7 | --- | --- | Big George | 5.00 | --- | 0.08 | 1.94 | 50.0 | 0.0 | 0.0 |
| C7 | --- | 1,404.90 | Big George | 5.00 | 64.00 | 0.08 | 2.10 | 5.0 | 45.0 | 0.0 |
| ns1 | 1,404.90 | 1,409.00 | ns1 | 125.00 | 125.00 | 1.00 | 6.20 | --- | --- | --- |
| C9 | 1,409.00 | --- | Big George | 22.00 | --- | 0.45 | 6.92 | 5.0 | 68.3 | 0.0 |
| C9 | --- | --- | Big George | 4.50 | --- | 0.09 | 7.07 | 45.0 | 0.0 | 0.0 |
| C9 | --- | --- | Big George | 11.50 | --- | 0.23 | 7.45 | 0.0 | 115.0 | 0.0 |
| C9 | --- | 1,410.80 | Big George | 11.00 | 49.00 | 0.22 | 7.81 | 110.0 | 0.0 | 0.0 |
| C10 | 1,410.80 | --- | Big George | 24.00 | --- | 0.48 | 8.60 | 13.8 | 46.3 | 0.0 |
| C10 | --- | --- | Big George | 22.00 | --- | 0.44 | 9.32 | 13.0 | 31.0 | 0.0 |
| C10 | --- | 1,413.00 | Big George | 4.00 | 50.00 | 0.08 | 9.45 | 40.0 | 0.0 | 0.0 |
| C11 | 1,413.00 | --- | Big George | 7.00 | --- | 0.14 | 9.68 | 10.0 | 60.0 | 0.0 |
| C11 | --- | --- | Big George | 5.00 | --- | 0.10 | 9.84 | 50.0 | 0.0 | 0.0 |
| C11 | --- | --- | Big George | 5.00 | --- | 0.10 | 10.01 | 10.0 | 40.0 | 0.0 |
| C11 | --- | --- | Big George | 5.00 | --- | 0.10 | 10.17 | 50.0 | 0.0 | 0.0 |
| C11 | --- | 1,415.30 | Big George | 27.00 | 49.00 | 0.55 | 11.06 | 15.0 | 120.0 | 0.0 |
| ns2 | 1,415.30 | 1,418.00 | ns2 | 82.00 | 82.00 | 1.00 | 13.75 | --- | --- | --- |
| C12 | 1,418.00 | --- | Big George | 22.00 | --- | 0.69 | 14.47 | 220.0 | 0.0 | 0.0 |
| C12 | --- | 1,419.40 | Big George | 10.00 | 32.00 | 0.31 | 14.80 | 5.0 | 95.0 | 0.0 |
| C13 | 1,419.40 | - | Big George | 28.00 | --- | 0.43 | 15.72 | 280.0 | 0.0 | 0.0 |
| C13 | --- | 1,421.40 | Big George | 37.00 | 65.00 | 0.57 | 16.93 | 3.0 | 182.0 | 0.0 |
| C14 | 1,421.40 | --- | Big George | 2.50 | --- | 0.05 | 17.01 | 0.0 | 25.0 | 0.0 |
| C14 | --- | --- | Big George | 18.00 | --- | 0.38 | 17.60 | 26.7 | 33.3 | 0.0 |
| C14 | --- | --- | Big George | 6.00 | --- | 0.13 | 17.80 | 1.0 | 59.0 | 0.0 |
| C14 | --- | --- | Big George | 19.00 | --- | 0.40 | 18.42 | 23.3 | 40.0 | 0.0 |
| C14 | --- | 1,423.40 | Big George | 1.50 | 47.00 | 0.03 | 18.47 | 0.0 | 12.0 | 3.0 |
| C15 | 1,423.40 | ---- | Big George | 24.00 | --- | 0.55 | 19.26 | 16.3 | 43.8 | 0.0 |
| C15 | --- | --- | Big George | 6.00 | --- | 0.14 | 19.46 | 10.0 | 50.0 | 0.0 |
| C15 | --- | --- | Big George | 12.00 | --- | 0.27 | 19.85 | 47.5 | 12.5 | 0.0 |
| C15 | --- | 1,425.40 | Big George | 2.00 | 44.00 | 0.05 | 19.91 | 0.0 | 20.0 | 0.0 |
| C16 | 1,425.40 | --- | Big George | 23.00 | --- | 0.48 | 20.67 | 8.1 | 24.7 | 0.0 |
| C16 | --- | --- | Big George | 15.00 | --- | 0.31 | 21.16 | 12.5 | 25.0 | 0.0 |
| C16 | --- | --- | Big George | 6.00 | --- | 0.13 | 21.36 | 5.0 | 55.0 | 0.0 |
| C16 | --- | 1,427.40 | Big George | 4.00 | 48.00 | 0.08 | 21.49 | 40.0 | 0.0 | 0.0 |
| ns3 | 1,427.40 | 1,428.00 | ns3 | 18.00 | 18.00 | 1.00 | 22.08 | --- | --- | --- |
| C26 | 1,428.00 | --- | Big George | 21.00 | --- | 0.55 | 22.77 | 4.8 | 47.8 | 0.0 |
| C26 | --- | --- | Big George | 3.00 | --- | 0.08 | 22.87 | 0.0 | 30.0 | 0.0 |
| C26 | --- | --- | Big George | 9.00 | --- | 0.23 | 23.16 | 6.7 | 23.3 | 0.0 |
| C26 | --- | 1429.80 | Big George | 5.50 | 38.50 | 0.14 | 23.34 | 0.0 | 55.0 | 0.0 |
| C17 | 1,429.80 | 1,431.60 | Big George | 60.00 | 60.00 | 1.00 | 25.31 | 45.0 | 1.0 | 0.0 |
| C29 | 1,431.60 | 1,433.40 | Big George | 64.00 | 64.00 | 1.00 | 27.41 | 58.0 | 6.0 | 0.0 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C7 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C7 | 3 | 5.00 | 35.00 | 12.50 | 87.50 | 0.00 | --- | --- | --- |
| C7 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C7 | 3 | 20.00 | 120.00 | 14.29 | 85.71 | 0.00 | --- | --- | --- |
| C7 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C7 | 3 | 45.00 | 135.00 | 25.00 | 75.00 | 0.00 | --- | --- | --- |
| C7 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C7 | 3 | 5.00 | 45.00 | 10.00 | 90.00 | 0.00 | 47.66 | 52.34 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C9 | 3 | 15.00 | 205.00 | 6.82 | 93.18 | 0.00 | --- | --- | --- |
| C9 | 5 | 45.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C9 | 1 | 0.00 | 115.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C9 | 5 | 110.00 | 0.00 | 100.00 | 0.00 | 0.00 | 34.69 | 65.31 | 0.00 |
| C10 | 3 | 55.00 | 185.00 | 22.92 | 77.08 | 0.00 | --- | --- | --- |
| C10 | 3 | 65.00 | 155.00 | 29.55 | 70.45 | 0.00 | --- | --- | --- |
| C10 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | 32.00 | 68.00 | 0.00 |
| C11 | 3 | 10.00 | 60.00 | 14.29 | 85.71 | 0.00 | --- | --- | --- |
| C11 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C11 | 3 | 10.00 | 40.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| C11 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C11 | 3 | 30.00 | 240.00 | 11.11 | 88.89 | 0.00 | 30.61 | 69.39 | 0.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C12 | 5 | 220.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C12 | 3 | 5.00 | 95.00 | 5.00 | 95.00 | 0.00 | 70.31 | 29.69 | 0.00 |
| C13 | 5 | 280.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C13 | 1 | 6.00 | 364.00 | 1.62 | 98.38 | 0.00 | 44.00 | 56.00 | 0.00 |
| C14 | 1 | 0.00 | 25.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C14 | 4 | 80.00 | 100.00 | 44.44 | 55.56 | 0.00 | --- | --- | --- |
| C14 | 1 | 1.00 | 59.00 | 1.67 | 98.33 | 0.00 | --- | --- | --- |
| C14 | 4 | 70.00 | 120.00 | 36.84 | 63.16 | 0.00 | --- | --- | --- |
| C14 | 1 | 0.00 | 12.00 | 0.00 | 80.00 | 20.00 | 32.13 | 67.23 | 0.64 |
| C15 | 3 | 65.00 | 175.00 | 27.08 | 72.92 | 0.00 | --- | --- | --- |
| C15 | 3 | 10.00 | 50.00 | 16.67 | 83.33 | 0.00 | --- | --- | --- |
| C15 | 4 | 95.00 | 25.00 | 79.17 | 20.83 | 0.00 | --- | --- | --- |
| C15 | 1 | 0.00 | 20.00 | 0.00 | 100.00 | 0.00 | 38.64 | 61.36 | 0.00 |
| C16 | 3 | 57.00 | 173.00 | 24.78 | 75.22 | 0.00 | --- | --- | --- |
| C16 | 3 | 50.00 | 100.00 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| C16 | 3 | 5.00 | 55.00 | 8.33 | 91.67 | 0.00 | --- | --- | --- |
| C16 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | 31.67 | 68.33 | 0.00 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C26 | 1 | 19.00 | 191.00 | 9.05 | 90.95 | 0.00 | --- | --- | --- |
| C26 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C26 | 3 | 20.00 | 70.00 | 22.22 | 77.78 | 0.00 | --- | --- | --- |
| C26 | 1 | 0.00 | 55.00 | 0.00 | 100.00 | 0.00 | 10.13 | 89.87 | 0.00 |
| C17 | 5 | 586.96 | 13.04 | 97.83 | 2.17 | 0.00 | 97.83 | 2.17 | 0.00 |
| C29 | 5 | 580.00 | 60.00 | 90.63 | 9.38 | 0.00 | 90.63 | 9.38 | 0.00 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | --- | --- | Bedding oriented 45 degrees to horizontal. |
| C7 | --- | --- | --- | 66.70 | SubA | Bedding oriented 45 degrees to horizontal. |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| C9 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C9 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C9 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C9 | --- | --- | --- | 65.37 | --- | Bedding oriented 30 degrees to horizontal. |
| C10 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C10 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C10 | --- | --- | --- | 72.41 | --- | Bedding oriented 20 degrees to horizontal. |
| C11 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C11 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C11 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C11 | --- | --- | --- | --- | --- | Bedding oriented 20 degrees to horizontal. |
| C11 | --- | --- | --- | 77.06 | --- | Bedding oriented 20 degrees to horizontal. |
| ns2 | --- | --- | --- | --- | --- | No sample. |
| C12 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C12 | --- | --- | --- | 65.42 | --- | Bedding oriented 30 degrees to horizontal. |
| C13 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C13 | --- | --- | --- | 68.74 | --- | Bedding oriented 30 degrees to horizontal. |
| C14 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C14 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C14 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C14 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C14 | --- | --- | --- | 69.90 | --- | Bedding oriented 30 degrees to horizontal. |
| C15 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C15 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C15 | --- | --- | --- | --- | --- | Bedding oriented 30 degrees to horizontal. |
| C15 | --- | --- | --- | 73.73 | --- | Bedding oriented 30 degrees to horizontal. |
| C16 | --- | --- | --- | --- | --- | --- |
| C16 | --- | --- | --- | --- | --- | --- |
| C16 | --- | --- | --- | --- | --- | --- |
| C16 | --- | --- | --- | 78.33 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | No sample. |
| C26 | --- | --- | --- | --- | --- | --- |
| C26 | --- | --- | --- | --- | --- | --- |
| C26 | --- | --- | --- | --- | --- | --- |
| C26 | --- | --- | --- | 60.54 | --- | --- |
| C17 | 15 | 66.67 | 66.67 | 84.64 | --- | Highly fractured sample, estimated attritus and vitrain band thicknesses. |
| C29 | 15 | 66.67 | 66.67 | 70.10 | SubB | Highly fractured sample. |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Appro dept | $\begin{aligned} & \text { ximate } \\ & \text { th (ft) } \end{aligned}$ | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| C19 | 1,433.40 | --- | Big George | 4.00 | ---- | 0.09 | 27.54 | 0.0 | 0.0 | 0.0 |
| C19 | --- | --- | Big George | 6.00 | --- | 0.13 | 27.74 | 3.0 | 57.0 | 0.0 |
| C19 |  | --- | Big George | 7.00 |  | 0.15 | 27.97 | 70.0 | 0.0 | 0.0 |
| C19 | --- | --- | Big George | 9.00 | --- | 0.20 | 28.26 | 10.0 | 35.0 | 0.0 |
| C19ns | --- | --- | Big George | 9.00 | --- | 1.00 | 28.56 | --- | --- | --- |
| C19 | --- | 1,435.20 | Big George | 20.00 | 46.00 | 0.43 | 29.22 | 9.3 | 24.0 | 0.0 |
| C20 | 1,435.20 | 1,437.00 | Big George | 60.00 | 60.00 | 1.00 | 31.18 | 29.4 | 45.6 | 0.0 |
| C21 | 1,437.00 | 1,438.80 | Big George | 54.00 | 54.00 | 1.00 | 32.96 | 18.2 | 23.3 | 0.0 |
| C22ns | 1,438.80 | --- | Big George | 12.50 | --- | 1.00 | 33.37 | --- | --- | --- |
| C22 | --- | 1,440.60 | Big George | 40.00 | 40.00 | 1.00 | 34.68 | 8.8 | 24.5 | 0.0 |
| C23 | 1,440.60 | --- | Big George | 24.50 | --- | 0.43 | 35.48 | 241.0 | 0.0 | 4.0 |
| C23 | --- | --- | Big George | 2.50 | --- | 0.04 | 35.56 | 0.0 | 25.0 | 0.0 |
| C23 | --- | --- | Big George | 3.00 | --- | 0.05 | 35.66 | 30.0 | 0.0 | 0.0 |
| C23 | --- | --- | Big George | 7.00 | --- | 0.12 | 35.89 | 0.0 | 70.0 | 0.0 |
| C23 | --- | --- | Big George | 7.50 | --- | 0.13 | 36.14 | 71.0 | 0.0 | 4.0 |
| C23 | --- | 1,442.40 | Big George | 12.50 | 57.00 | 0.22 | 36.55 | 2.5 | 28.8 | 0.0 |
| C24 | 1,442.40 | --- | Big George | 15.00 | --- | 0.23 | 37.04 | 14.0 | 16.0 | 0.0 |
| C24 | --- | --- | Big George | 22.00 | --- | 0.33 | 37.76 | 28.3 | 44.3 | 2.0 |
| C24 | --- | 1,444.20 | Big George | 29.00 | 66.00 | 0.44 | 38.71 | 1.8 | 56.2 | 0.0 |
| C27 | 1,444.20 | 1,446.00 | Big George | 55.00 | 55.00 | 1.00 | 40.52 | 4.3 | 70.0 | 30.0 |
| C33 | 1,446.00 | --- | Big George | 7.00 | --- | 0.14 | 40.75 | 0.0 | 70.0 | 0.0 |
| C33 | --- | --- | Big George | 2.00 | --- | 0.04 | 40.81 | 20.0 | 0.0 | 0.0 |
| C33 | --- | --- | Big George | 10.00 | --- | 0.19 | 41.14 | 10.0 | 90.0 | 0.0 |
| C33 | --- | --- | Big George | 1.50 | --- | 0.03 | 41.19 | 15.0 | 0.0 | 0.0 |
| C33 | --- | --- | Big George | 10.00 | --- | 0.19 | 41.52 | 10.0 | 90.0 | 0.0 |
| C33 | --- | --- | Big George | 10.00 | --- | 0.19 | 41.85 | 7.5 | 42.5 | 0.0 |
| C33 | --- | 1,448.00 | Big George | 11.00 | 51.50 | 0.21 | 42.21 | 1.7 | 35.0 | 0.0 |
| C28 | 1,448.00 | --- | Big George | 3.00 | --- | 0.05 | 42.31 | 0.0 | 30.0 | 0.0 |
| C28 | --- | --- | Big George | 9.00 | --- | 0.15 | 42.60 | 90.0 | 0.0 | 0.0 |
| C28 | --- | --- | Big George | 11.00 | --- | 0.18 | 42.96 | 7.5 | 47.5 | 0.0 |
| C28 | --- | --- | Big George | 7.00 | --- | 0.11 | 43.19 | 70.0 | 0.0 | 0.0 |
| C28 | --- | --- | Big George | 22.00 | --- | 0.35 | 43.91 | 45.0 | 175.0 | 0.0 |
| C28 | --- | --- | Big George | 4.00 | --- | 0.06 | 44.05 | 0.0 | 0.0 | 40.0 |
| C28 | --- | 1,450.00 | Big George | 6.00 | 62.00 | 0.10 | 44.24 | 10.0 | 50.0 | 0.0 |
| C31 | 1,450.00 | --- | Big George | 5.00 | --- | 0.09 | 44.41 | 50.0 | 0.0 | 0.0 |
| C31 | --- | --- | Big George | 22.00 | --- | 0.39 | 45.13 | 5.0 | 31.7 | 0.0 |
| C31 | --- | --- | Big George | 2.00 | --- | 0.04 | 45.19 | 20.0 | 0.0 | 0.0 |
| C31 | --- | --- | Big George | 17.00 | --- | 0.30 | 45.75 | 9.0 | 76.0 | 0.0 |
| C31 | --- | --- | Big George | 1.00 | --- | 0.02 | 45.78 | 0.0 | 0.0 | 10.0 |
| C31 | --- | --- | Big George | 4.00 | --- | 0.07 | 45.92 | 0.0 | 40.0 | 0.0 |
| C31 | --- | 1452.00 | Big George | 6.00 | 57.00 | 0.11 | 46.11 | 60.0 | 0.0 | 0.0 |
| C32 | 1,452.00 | --- | Big George | 32.00 | --- | 0.57 | 47.16 | 23.3 | 30.0 | 0.0 |
| C32 | --- | 1,454.00 | Big George | 24.00 | 56.00 | 0.43 | 47.95 | 0.0 | 240.0 | 0.0 |
| ns4 | 1,454.00 | 1,454.60 | ns4 | 18.00 | 18.00 | 1.00 | 48.54 | --- | --- | --- |
| C35 | 1,454.60 | 1,456.10 | Big George | 59.00 | 59.00 | 1.00 | 50.48 | 7.6 | 66.1 | 0.0 |
| C36 | 1,456.10 | --- | Big George | 15.00 | --- | 0.23 | 50.97 | 150.0 | 0.0 | 0.0 |
| C36 | --- | --- | Big George | 24.00 | --- | 0.36 | 51.76 | 3.3 | 56.8 | 0.0 |
| C36 | --- | --- | Big George | 5.00 | --- | 0.08 | 51.92 | 50.0 | 0.0 | 0.0 |
| C36 | --- | 1,458.10 | Big George | 22.00 | 66.00 | 0.33 | 52.64 | 10.0 | 100.0 | 0.0 |
| C37 | 1,458.10 | 1,460.00 | Big George | 54.00 | 54.00 | 1.00 | 54.41 | 10.8 | 43.2 | 0.0 |
| C38 | 1,460.00 | 1,462.00 | Big George | 60.00 | 60.00 | 1.00 | 56.38 | 71.4 | 14.3 | 0.0 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C19 | 0 | 0.00 | 40.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C19 | 1 | 3.00 | 57.00 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| C19 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C19 | 3 | 20.00 | 70.00 | 22.22 | 77.78 | 0.00 | --- | --- | --- |
| C19ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C19 | 3 | 56.00 | 144.00 | 28.00 | 72.00 | 0.00 | 32.39 | 67.61 | 0.00 |
| C20 | 4 | 235.00 | 365.00 | 39.17 | 60.83 | 0.00 | 39.17 | 60.83 | 0.00 |
| C21 | 3 | 237.00 | 303.00 | 43.89 | 56.11 | 0.00 | 43.89 | 56.11 | 0.00 |
| C22ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C22 | 3 | 106.00 | 294.00 | 26.50 | 73.50 | 0.00 | 26.50 | 73.50 | 0.00 |
| C23 | 5 | 241.00 | 0.00 | 98.37 | 0.00 | 1.63 | --- | --- | --- |
| C23 | 1 | 0.00 | 25.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C23 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C23 | 1 | 0.00 | 70.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C23 | 5 | 71.00 | 0.00 | 94.67 | 0.00 | 5.33 | --- | --- | --- |
| C23 | 1 | 10.00 | 115.00 | 8.00 | 92.00 | 0.00 | 61.75 | 36.84 | 1.40 |
| C24 | 3 | 70.00 | 80.00 | 46.67 | 53.33 | 0.00 | --- | --- | --- |
| C24 | 4 | 85.00 | 133.00 | 38.64 | 60.45 | 0.91 | --- | --- | --- |
| C24 | 1 | 9.00 | 281.00 | 3.10 | 96.90 | 0.00 | 24.85 | 74.85 | 0.30 |
| C27 | 1 | 30.00 | 490.00 | 5.45 | 89.09 | 5.45 | 5.45 | 89.09 | 5.45 |
| C33 | 1 | 0.00 | 70.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C33 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C33 | 3 | 10.00 | 90.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| C33 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C33 | 3 | 10.00 | 90.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| C33 | 3 | 15.00 | 85.00 | 15.00 | 85.00 | 0.00 | --- | --- | --- |
| C33 | 1 | 5.00 | 105.00 | 4.55 | 95.45 | 0.00 | 14.56 | 85.44 | 0.00 |
| C28 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C28 | 5 | 90.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C28 | 3 | 15.00 | 95.00 | 13.64 | 86.36 | 0.00 | --- | --- | --- |
| C28 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C28 | 4 | 45.00 | 175.00 | 20.45 | 79.55 | 0.00 | --- | --- | --- |
| C28 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- | --- |
| C28 | 3 | 10.00 | 50.00 | 16.67 | 83.33 | 0.00 | 37.10 | 56.45 | 6.45 |
| C31 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C31 | 3 | 30.00 | 190.00 | 13.64 | 86.36 | 0.00 | --- | --- | --- |
| C31 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C31 | 3 | 18.00 | 152.00 | 10.59 | 89.41 | 0.00 | --- | --- | --- |
| C31 | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | --- | --- | --- |
| C31 | 1 | 0.00 | 40.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C31 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | 31.23 | 67.02 | 1.75 |
| C32 | 4 | 140.00 | 180.00 | 43.75 | 56.25 | 0.00 | --- | --- | --- |
| C32 | 1 | 0.00 | 240.00 | 0.00 | 100.00 | 0.00 | 25.00 | 75.00 | 0.00 |
| ns4 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C35 | 3 | 61.00 | 529.00 | 10.34 | 89.66 | 0.00 | 10.34 | 89.66 | 0.00 |
| C36 | 5 | 150.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C36 | 1 | 13.00 | 227.00 | 5.42 | 94.58 | 0.00 | --- | --- | --- |
| C36 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C36 | 3 | 20.00 | 200.00 | 9.09 | 90.91 | 0.00 | 35.30 | 64.70 | 0.00 |
| C37 | 3 | 108.00 | 432.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| C38 | 4 | 500.00 | 100.00 | 83.33 | 16.67 | 0.00 | 83.33 | 16.67 | 0.00 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C19 | --- | --- | --- | --- | --- | Carbonaceous shale. |
| C19 | 25 | 40.00 | --- | --- | --- | --- |
| C19 | 10 | 100.00 | --- | --- | --- | --- |
| C19 | 35 | 28.57 | --- | --- | --- | "Roasted wood." |
| C19ns | --- | -- | --- | --- | --- | No data, adsorption analysis sample taken. |
| C19 | 40 | 25.00 | 40.41 | 89.91 | --- | --- |
| C20 | 10 | 100.00 | 100.00 | 87.92 | --- | Pyrite on cleat. |
| C21 | 25 | 40.00 | 40.00 | 85.24 | --- | Pyrite on cleat. |
| C 22 ns | --- | --- | --- | --- | --- | No data, adsorption analysis sample. |
| C22 | 20 | 50.00 | 50.00 | 88.62 | --- | Pyrite on cleat. |
| C23 | 25 | 40.00 | --- | --- | --- | --- |
| C23 | 55 | 18.18 | --- | --- | --- | --- |
| C23 | 25 | 40.00 | --- | --- | --- | --- |
| C23 | 55 | 18.18 | --- | --- | --- | --- |
| C23 | 20 | 50.00 | --- | --- | --- | --- |
| C23 | 55 | 18.18 | 32.89 | 83.45 | --- | --- |
| C24 | 25 | 40.00 | --- | --- | --- | Pyrite on cleat, laminations oriented 45 degrees to bedding. |
| C24 | 25 | 40.00 | --- | --- | --- | --- |
| C24 | 55 | 18.18 | 30.41 | 80.01 | --- | --- |
| C27 | 55 | 18.18 | 18.18 | 88.69 | --- | Dull, abundant fusain. |
| C33 | --- | --- | --- | --- | --- | Tilted bedding, "swirling" attritus. |
| C33 | --- | --- | --- | --- | --- | Tilted bedding. |
| C33 | --- | --- | --- | --- | --- | --- |
| C33 | --- | --- | --- | --- | --- | --- |
| C33 | --- | --- | --- | --- | --- | --- |
| C33 | --- | --- | --- | --- | --- | Shaly. |
| C33 | --- | --- | --- | 61.33 | -- | --- |
| C28 | --- | --- | --- | --- | --- | --- |
| C28 | --- | --- | --- | --- | -- | --- |
| C28 | --- | --- | --- | --- | --- | --- |
| C28 | --- | -- | --- | --- | --- | --- |
| C28 | --- | --- | --- | --- | --- | --- |
| C28 | --- | --- | --- | --- | --- | Thick fusain layer. |
| C28 | --- | --- | --- | 75.28 | SubA | Shaly. |
| C31 | --- | -- | --- | --- | -- | --- |
| C31 | --- | --- | --- | --- | -- | --- |
| C31 | --- | --- | --- | --- | --- | --- |
| C31 | --- | -- | --- | --- | --- | --- |
| C31 | --- | --- | --- | --- | --- | Fusain layer. |
| C31 | --- | --- | --- | --- | --- | --- |
| C31 | --- | -- | --- | 74.50 | --- | --- |
| C32 | --- | -- | --- | --- | --- | Tilted bedding, "swirling" attritus. |
| C32 | --- | --- | --- | 84.47 | -- | Tilted bedding. |
| ns4 | --- | --- | --- | --- | --- | No sample. |
| C35 | -- | -- | -- | 81.92 | --- | -- |
| C36 | --- | --- | -- | --- | --- | --- |
| C36 | - | -- | --- | --- | --- | -- |
| C36 | --- | -- | -- | . | --- | --- |
| C36 | --- | --- | --- | 78.44 | --- | --- |
| C37 | 45 | 22.22 | 22.22 | 89.50 | --- | Pyrite sampled, bedding at 35 degrees to horizontal. |
| C38 | 65 | 15.38 | 15.38 | 73.82 | --- | Bottom 2/3 at 30 degrees to horizontal, top 1/3 at 10 degrees. |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Approx dept | mate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| C39 | 1,462.00 | 1,464.00 | Big George | 50.00 | 50.00 | 1.00 | 58.02 | 16.0 | 15.1 | 3.0 |
| C40 | 1,464.00 | --- | Big George | 16.00 | --- | 0.34 | 58.55 | 160.0 | 0.0 | 0.0 |
| C40 | --- | --- | Big George | 10.00 | --- | 0.21 | 58.87 | 5.0 | 95.0 | 0.0 |
| C40 | --- | --- | Big George | 4.00 | --- | 0.09 | 59.01 | 40.0 | 0.0 | 0.0 |
| C40 | --- | --- | Big George | 8.00 | --- | 0.17 | 59.27 | 0.0 | 80.0 | 0.0 |
| C40 | --- | --- | Big George | 4.00 | --- | 0.09 | 59.40 | 40.0 | 0.0 | 0.0 |
| C40 | --- | 1,466.00 | Big George | 5.00 | 47.00 | 0.11 | 59.56 | 10.0 | 40.0 | 0.0 |
| C41 | 1,466.00 | --- | Big George | 11.00 | --- | 0.19 | 59.92 | 12.3 | 24.3 | 0.0 |
| C41 | --- | --- | Big George | 23.50 | --- | 0.41 | 60.70 | 10.0 | 68.3 | 0.0 |
| C41 | --- | --- | Big George | 4.50 | --- | 0.08 | 60.84 | 45.0 | 0.0 | 0.0 |
| C41 | --- | --- | Big George | 4.50 | --- | 0.08 | 60.99 | 0.0 | 45.0 | 0.0 |
| C41 | --- | --- | Big George | 5.00 | --- | 0.09 | 61.15 | 50.0 | 0.0 | 0.0 |
| C41 | --- | 1,468.00 | Big George | 9.50 | 58.00 | 0.16 | 61.47 | 5.0 | 42.5 | 0.0 |
| C42 | 1,468.00 | --- | Big George | 39.00 | --- | 1.00 | 62.75 | 10.0 | 68.0 | 0.0 |
| C42fr | --- | 1,470.00 | Big George | 21.00 | 21.00 | 1.00 | 63.44 | --- | --- | --- |
| C 43 | 1,470.00 | 1,471.80 | Big George | 53.00 | 53.00 | 1.00 | 65.17 | 5.5 | 127.0 | 0.0 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C39 | 3 | 256.00 | 241.00 | 51.20 | 48.20 | 0.60 | 51.20 | 48.20 | 0.60 |
| C40 | 5 | 160.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C40 | 3 | 5.00 | 95.00 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| C40 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C40 | 1 | 0.00 | 80.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C40 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C40 | 3 | 10.00 | 40.00 | 20.00 | 80.00 | 0.00 | 54.26 | 45.74 | 0.00 |
| C41 | 3 | 37.00 | 73.00 | 33.64 | 66.36 | 0.00 | --- | --- | --- |
| C41 | 3 | 30.00 | 205.00 | 12.77 | 87.23 | 0.00 | --- | --- | --- |
| C41 | 5 | 45.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| C41 | 1 | 0.00 | 45.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| C41 | 5 | 50.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | -- | --- |
| C41 | 3 | 10.00 | 85.00 | 10.53 | 89.47 | 0.00 | 29.66 | 70.34 | 0.00 |
| C42 | 3 | 50.00 | 340.00 | 12.82 | 87.18 | 0.00 | 12.82 | 87.18 | 0.00 |
| C42fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| C43 | 3 | 22.00 | 508.00 | 4.15 | 95.85 | 0.00 | 4.15 | 95.85 | 0.00 |

Table 1-26. Data for samples from core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; SubB, subbituminous B; ---, no data]

| Canister number | $\begin{gathered} \text { Cleat } \\ \text { spacing } \\ \text { (CS) }(\mathrm{mm}) \end{gathered}$ | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C39 | 40 | 25.00 | 25.00 | 76.62 | --- | --- |
| C40 | --- | --- | --- | --- | --- | --- |
| C40 | --- | --- | --- | --- | -- | --- |
| C40 | --- | --- | --- | --- | --- | --- |
| C40 | --- | --- | --- | --- | --- | --- |
| C40 | --- | --- | -- | --- | --- | --- |
| C40 | --- | --- | --- | 69.68 | --- | --- |
| C41 | -- | --- | --- | --- | --- | --- |
| C41 | --- | -- | --- | --- | --- | --- |
| C41 | --- | --- | --- | --- | --- | --- |
| C41 | --- | --- | --- | --- | --- | --- |
| C41 | --- | --- | --- | --- | --- | --- |
| C41 | --- | --- | --- | 69.11 | --- | --- |
| C42 | --- | --- | --- | 73.85 | --- | --- |
| C42fr | --- | --- | --- | --- | --- | Sample too fragmented to describe. |
| C43 | --- | --- | --- | 77.17 | SubA | --- |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 34 | 1,518.00 | --- | Big George | 5.50 | --- | 0.10 | 0.18 | 3.0 | 52.0 | 0.0 |
| 34 | --- | --- | Big George | 12.00 | --- | 0.23 | 0.57 | 2.6 | 21.4 | 0.0 |
| 34 | --- | --- | Big George | 5.00 | --- | 0.10 | 0.74 | 0.0 | 50.0 | 0.0 |
| 34 | --- | --- | Big George | 5.00 | --- | 0.10 | 0.90 | 7.5 | 17.5 | 0.0 |
| 34 | --- | --- | Big George | 3.00 | --- | 0.06 | 1.00 | 0.0 | 30.0 | 0.0 |
| 34 | --- | --- | Big George | 8.50 | --- | 0.16 | 1.28 | 4.0 | 38.5 | 0.0 |
| 34 | --- | --- | Big George | 3.00 | --- | 0.06 | 1.38 | 0.0 | 30.0 | 0.0 |
| 34 | --- | --- | Big George | 1.50 | --- | 0.03 | 1.43 | 15.0 | 0.0 | 0.0 |
| 34 | --- | --- | Big George | 3.00 | --- | 0.06 | 1.53 | 0.0 | 30.0 | 0.0 |
| 34 | --- | --- | Big George | 3.00 | --- | 0.06 | 1.62 | 30.0 | 0.0 | 0.0 |
| 34 | --- | 1,520.00 | Big George | 3.00 | 52.50 | 0.06 | 1.72 | 0.0 | 30.0 | 0.0 |
| 32 | 1,520.00 | --- | Big George | 12.00 | --- | 0.27 | 2.12 | 5.0 | 55.0 | 0.0 |
| 32 | --- | --- | Big George | 18.00 | --- | 0.41 | 2.71 | 10.6 | 25.4 | 0.0 |
| 32 | --- | --- | Big George | 2.50 | --- | 0.06 | 2.79 | 0.0 | 25.0 | 0.0 |
| 32 | --- | --- | Big George | 3.00 | --- | 0.07 | 2.89 | 30.0 | 0.0 | 0.0 |
| 32 | --- | --- | Big George | 7.00 | --- | 0.16 | 3.12 | 2.0 | 68.0 | 0.0 |
| 32 | -- | 1,522.00 | Big George | 1.50 | 44.00 | 0.03 | 3.17 | 0.0 | 15.0 | 0.0 |
| 31 | 1,522.00 | --- | Big George | 20.00 | --- | 0.35 | 3.82 | 1.3 | 65.3 | 0.0 |
| 31 | --- | --- | Big George | 6.00 | --- | 0.11 | 4.02 | 60.0 | 0.0 | 0.0 |
| 31 | --- | --- | Big George | 10.50 | --- | 0.19 | 4.36 | 3.0 | 49.5 | 0.0 |
| 31 | --- | --- | Big George | 3.00 | --- | 0.05 | 4.46 | 0.0 | 0.0 | 0.0 |
| 31 | --- | --- | Big George | 9.00 | --- | 0.16 | 4.76 | 1.0 | 29.0 | 0.0 |
| 31 | --- | --- | Big George | 6.50 | --- | 0.12 | 4.97 | 5.5 | 27.0 | 0.0 |
| 31 | --- | 1,524.00 | Big George | 1.50 | 56.50 | 0.03 | 5.02 | 0.0 | 15.0 | 0.0 |
| 30 | 1,524.00 | --- | Big George | 4.50 | --- | 0.08 | 5.17 | 12.5 | 10.0 | 0.0 |
| 30 | --- | --- | Big George | 14.50 | --- | 0.26 | 5.64 | 3.0 | 142.0 | 0.0 |
| 30 | --- | --- | Big George | 17.00 | --- | 0.30 | 6.20 | 20.0 | 36.7 | 0.0 |
| 30 | --- | 1,526.00 | Big George | 20.00 | 56.00 | 0.36 | 6.86 | 8.0 | 58.7 | 0.0 |
| ns1 | 1,526.00 | 1,534.00 | ns1 | 244.00 | 244.00 | 1.00 | 14.86 | --- | --- | --- |
| 35 | 1,534.00 | --- | Big George | 2.50 | --- | 0.05 | 14.94 | 25.0 | 0.0 | 0.0 |
| 35 |  | --- | Big George | 5.00 | --- | 0.09 | 15.11 | 0.0 | 0.0 | 0.0 |
| 35 | --- | --- | Big George | 20.00 | --- | 0.38 | 15.76 | 2.3 | 47.8 | 0.0 |
| 35 | --- | --- | Big George | 4.00 | --- | 0.08 | 15.90 | 8.5 | 11.5 | 0.0 |
| 35 | --- | 1,536.00 | Big George | 21.50 | 53.00 | 0.41 | 16.60 | 4.0 | 67.7 | 0.0 |
| 36 | 1,536.00 | --- | Big George | 15.50 | --- | 0.28 | 17.11 | 5.7 | 46.0 | 0.0 |
| 36 | --- | --- | Big George | 3.00 | --- | 0.05 | 17.21 | 30.0 | 0.0 | 0.0 |
| 36 | --- | --- | Big George | 26.00 | --- | 0.46 | 18.06 | 2.0 | 4.0 | 0.0 |
| 36 | -- | --- | Big George | 3.00 | --- | 0.05 | 18.16 | 30.0 | 0.0 | 0.0 |
| 36 | --- | 1,538.00 | Big George | 8.50 | 56.00 | 0.15 | 18.44 | 1.0 | 3.0 | 0.0 |
| ns2 | 1,538.00 | 1,538.40 | ns2 | 12.00 | 12.00 | 1.00 | 18.83 | --- | --- | --- |
| 37 | 1,538.40 | 1,588. | Big George | 22.00 | --- | 0.33 | 19.55 | 10.0 | 34.0 | 0.0 |
| 37 | --- | --- | Big George | 2.00 | --- | 0.03 | 19.62 | 20.0 | 0.0 | 0.0 |
| 37 | --- | --- | Big George | 8.00 | --- | 0.12 | 19.88 | 7.5 | 32.5 | 0.0 |
| 37 | -- | --- | Big George | 3.00 | --- | 0.05 | 19.98 | 30.0 | 0.0 | 0.0 |
| 37 | --- | --- | Big George | 22.50 | --- | 0.34 | 20.72 | 12.6 | 32.4 | 0.0 |
| 37 | --- | 1,540.40 | Big George | 8.50 | 66.00 | 0.13 | 21.00 | 7.0 | 78.0 | 0.0 |
| 38 | 1,540.40 | --- | Big George | 17.50 | --- | 0.48 | 21.57 | 3.0 | 84.5 | 0.0 |
| 38 | --- | --- | Big George | 12.00 | --- | 0.33 | 21.97 | 8.4 | 8.7 | 0.0 |
| 38 | --- | 1,542.40 | Big George | 7.00 | 36.50 | 0.19 | 22.19 | 2.0 | 68.0 | 0.0 |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 1 | 3.00 | 52.00 | 5.45 | 94.55 | 0.00 | --- | --- | --- |
| 34 | 1 | 13.00 | 107.00 | 10.83 | 89.17 | 0.00 | --- | --- | --- |
| 34 | 1 | 0.00 | 50.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 34 | 3 | 15.00 | 35.00 | 30.00 | 70.00 | 0.00 | --- | --- | --- |
| 34 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 34 | 1 | 8.00 | 77.00 | 9.41 | 90.59 | 0.00 | --- | --- | --- |
| 34 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 34 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 34 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 34 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 34 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | 16.00 | 84.00 | 0.00 |
| 32 | 3 | 10.00 | 110.00 | 8.33 | 91.67 | 0.00 | --- | - --- | --- |
| 32 | 3 | 53.00 | 127.00 | 29.44 | 70.56 | 0.00 | --- | --- | --- |
| 32 | 1 | 0.00 | 25.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 32 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 32 | 1 | 2.00 | 68.00 | 2.86 | 97.14 | 0.00 | --- | --- | --- |
| 32 | 1 | 0.00 | 15.00 | 0.00 | 100.00 | 0.00 | 21.59 | 78.41 | 0.00 |
| 31 | 1 | 4.00 | 196.00 | 2.00 | 98.00 | 0.00 | --- | - --- | --- |
| 31 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 31 | 1 | 6.00 | 99.00 | 5.71 | 94.29 | 0.00 | --- | --- | --- |
| 31 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 31 | 1 | 3.00 | 87.00 | 3.33 | 96.67 | 0.00 | --- | --- | --- |
| 31 | 3 | 11.00 | 54.00 | 16.92 | 83.08 | 0.00 | --- | --- | --- |
| 31 | 1 | 0.00 | 15.00 | 0.00 | 100.00 | 0.00 | 14.87 | 79.82 | 0.00 |
| 30 | 3 | 25.00 | 20.00 | 55.56 | 44.44 | 0.00 | --- | --- | --- |
| 30 | 1 | 3.00 | 142.00 | 2.07 | 97.93 | 0.00 | --- | --- | --- |
| 30 | 3 | 60.00 | 110.00 | 35.29 | 64.71 | 0.00 | --- | --- | --- |
| 30 | 3 | 24.00 | 176.00 | 12.00 | 88.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | ---- | --- | ---- | --- |
| 35 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 35 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- | --- |
| 35 | 1 | 9.00 | 191.00 | 4.50 | 95.50 | 0.00 | --- | --- | --- |
| 35 | 3 | 17.00 | 23.00 | 42.50 | 57.50 | 0.00 | --- | --- | --- |
| 35 | 1 | 12.00 | 203.00 | 5.58 | 94.42 | 0.00 | 11.89 | 78.68 | 0.00 |
| 36 | 3 | 17.00 | 138.00 | 10.97 | 89.03 | 0.00 | --- | - --- | --- |
| 36 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 36 | 2 | 86.67 | 173.33 | 33.33 | 66.67 | 0.00 | --- | --- | --- |
| 36 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 36 | 2 | 21.25 | 63.75 | 25.00 | 75.00 | 0.00 | 33.02 | 66.98 | 0.00 |
| ns2 | --- | --- | --- | --- | --- | --- | --- | - --- | --- |
| 37 | 3 | 50.00 | 170.00 | 22.73 | 77.27 | 0.00 | --- | --- | --- |
| 37 | 3 | 20.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 37 | 3 | 15.00 | 65.00 | 18.75 | 81.25 | 0.00 | --- | --- | --- |
| 37 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 37 | 3 | 63.00 | 162.00 | 28.00 | 72.00 | 0.00 | --- | --- | --- |
| 37 | 3 | 7.00 | 78.00 | 8.24 | 91.76 | 0.00 | 28.03 | 71.97 | 0.00 |
| 38 | 1 | 6.00 | 169.00 | 3.43 | 96.57 | 0.00 | --- | - --- | --- |
| 38 | 3 | 59.00 | 61.00 | 49.17 | 50.83 | 0.00 | --- | --- | --- |
| 38 | 1 | 2.00 | 68.00 | 2.86 | 97.14 | 0.00 | 18.36 | 81.64 | 0.00 |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | --- | --- | --- | --- |
| 34 | 20 | 50.00 | 50.00 | 85.85 | --- | --- |
| 32 | 20 | 50.00 | --- | --- | --- | --- |
| 32 | 20 | 50.00 | --- | --- | --- | --- |
| 32 | 20 | 50.00 | --- | --- | --- | --- |
| 32 | 20 | 50.00 | --- | --- | --- | --- |
| 32 | 20 | 50.00 | --- | --- | --- | --- |
| 32 | 20 | 50.00 | 50.00 | 102.39 | SubA | --- |
| 31 | 20 | 50.00 | --- | --- | --- | --- |
| 31 | 20 | 50.00 | --- | --- | --- | --- |
| 31 | 20 | 50.00 | --- | --- | --- | --- |
| 31 | --- | --- | --- | --- | --- | Shale. |
| 31 | 20 | 50.00 | --- | --- | --- | --- |
| 31 | 20 | 50.00 | --- | --- | --- | --- |
| 31 | 20 | 50.00 | 50.00 | 77.29 | --- | --- |
| 30 | 20 | 50.00 | --- | --- | --- | --- |
| 30 | 20 | 50.00 | --- | --- | --- | --- |
| 30 | 20 | 50.00 | --- | --- | --- | --- |
| 30 | 20 | 50.00 | 50.00 | 100.37 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| 35 | 20 | 50.00 | --- | --- | --- | --- |
| 35 | --- | --- | --- | --- | --- | Shale. |
| 35 | 20 | 50.00 | --- | --- | --- | --- |
| 35 | 20 | 50.00 | --- | --- | --- | --- |
| 35 | 20 | 50.00 | 50.00 | 96.49 | --- | --- |
| 36 | 30 | 33.33 | --- | --- | --- | --- |
| 36 | 30 | 33.33 | --- | --- | --- | --- |
| 36 | 30 | 33.33 | --- | --- | --- | Estimated attritus and vitrain thicknesses and percentages. |
| 36 | 30 | 33.33 | --- | --- | --- | --- |
| 36 | 30 | 33.33 | 33.33 | 91.85 | --- | Estimated attritus and vitrain thicknesses and percentages. |
| ns2 | --- | --- | --- | --- | --- | No sample. |
| 37 | 25 | 40.00 | --- | --- | --- | --- |
| 37 | 25 | 40.00 | --- | --- | --- | --- |
| 37 | 25 | 40.00 | --- | --- | --- | --- |
| 37 | 25 | 40.00 | --- | --- | --- | --- |
| 37 | 25 | 40.00 | --- | --- | --- | --- |
| 37 | 25 | 40.00 | 40.00 | 102.66 | SubA | --- |
| 38 | 20 | 50.00 | --- | --- | --- | --- |
| 38 | 20 | 50.00 | --- | --- | --- | --- |
| 38 | 20 | 50.00 | 50.00 | 102.41 | --- | --- |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit <br> thickness <br> (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 39 | 1,542.40 | --- | Big George | 10.00 | --- | 0.17 | 22.52 | 3.0 | 47.0 | 0.0 |
| 39 | --- | --- | Big George | 13.00 | --- | 0.22 | 22.95 | 15.5 | 17.0 | 0.0 |
| 39 | --- | --- | Big George | 7.50 | --- | 0.13 | 23.20 | 75.0 | 0.0 | 0.0 |
| 39 | --- | --- | Big George | 7.00 | --- | 0.12 | 23.43 | 0.0 | 70.0 | 0.0 |
| 39 | --- | 1,544.40 | Big George | 20.50 | 58.00 | 0.35 | 24.10 | 3.8 | 47.5 | 0.0 |
| 40 | 1,544.40 | --- | Big George | 21.50 | --- | 0.36 | 24.80 | 7.0 | 100.5 | 0.0 |
| 40 | --- | --- | Big George | 3.50 | --- | 0.06 | 24.92 | 35.0 | 0.0 | 0.0 |
| 40 | --- | --- | Big George | 19.50 | --- | 0.33 | 25.56 | 3.7 | 61.3 | 0.0 |
| 40 | --- | --- | Big George | 3.00 | --- | 0.05 | 25.66 | 30.0 | 0.0 | 0.0 |
| 40 | -- | 1,546.40 | Big George | 11.50 | 59.00 | 0.19 | 26.03 | 13.5 | 44.0 | 0.0 |
| 41 | 1,546.40 | ---- | Big George | 19.50 | --- | 0.32 | 26.67 | 3.0 | 62.0 | 0.0 |
| 41 | --- | --- | Big George | 6.50 | --- | 0.11 | 26.89 | 65.0 | 0.0 | 0.0 |
| 41 | --- | --- | Big George | 1.50 | --- | 0.02 | 26.94 | 1.0 | 14.0 | 0.0 |
| 41 ns | --- | --- | Big George | 12.50 | --- | 1.00 | 27.35 | --- | --- | --- |
| 41 | --- | --- | Big George | 16.50 | --- | 0.27 | 27.89 | 2.5 | 80.0 | 0.0 |
| 41 | --- | --- | Big George | 2.50 | --- | 0.04 | 27.97 | 25.0 | 0.0 | 0.0 |
| 41 | --- | 1,548.40 | Big George | 15.00 | 61.50 | 0.24 | 28.46 | 6.3 | 43.7 | 0.0 |
| 42 | 1,548.40 | --- | Big George | 23.50 | --- | 0.39 | 29.23 | 7.5 | 51.3 | 0.0 |
| 42 | --- | --- | Big George | 7.00 | --- | 0.11 | 29.46 | 70.0 | 0.0 | 0.0 |
| 42 | --- | --- | Big George | 4.50 | --- | 0.07 | 29.61 | 0.0 | 45.0 | 0.0 |
| 42 | --- | --- | Big George | 20.00 | --- | 0.33 | 30.27 | 4.3 | 45.8 | 0.0 |
| 42 | --- | --- | Big George | 3.00 | --- | 0.05 | 30.36 | 0.0 | 30.0 | 0.0 |
| 42 | --- | 1,550.40 | Big George | 3.00 | 61.00 | 0.05 | 30.46 | 30.0 | 0.0 | 0.0 |
| 43 | 1,550.40 | --- | Big George | 2.50 | --- | 0.06 | 30.54 | 25.0 | 0.0 | 0.0 |
| 43 | --- | --- | Big George | 13.50 | --- | 0.31 | 30.99 | 2.0 | 65.5 | 0.0 |
| 43 | --- | --- | Big George | 6.50 | --- | 0.15 | 31.20 | 65.0 | 0.0 | 0.0 |
| 43 | --- | 1,552.40 | Big George | 20.50 | 43.00 | 0.48 | 31.87 | 4.5 | 46.8 | 0.0 |
| ns3 | 1,552.40 | 1,554.00 | ns3 | 49.00 | 49.00 | 1.00 | 33.48 | --- | --- | --- |
| 44 | 1,554.00 | --- | Big George | 5.50 | --- | 0.10 | 33.66 | 10.0 | 45.0 | 0.0 |
| 44 | --- | --- | Big George | 6.50 | --- | 0.12 | 33.87 | 65.0 | 0.0 | 0.0 |
| 44 | --- | --- | Big George | 9.00 | --- | 0.17 | 34.17 | 1.0 | 89.0 | 0.0 |
| 44 | --- | --- | Big George | 23.00 | --- | 0.43 | 34.92 | 8.5 | 49.0 | 0.0 |
| 44 | --- | 1,556.00 | Big George | 9.00 | 53.00 | 0.17 | 35.22 | 5.5 | 37.0 | 5.0 |
| 45 | 1,556.00 | --- | Big George | 28.50 | --- | 0.48 | 36.15 | 4.6 | 52.4 | 0.0 |
| 45 | --- | --- | Big George | 16.00 | --- | 0.27 | 36.68 | 160.0 | 0.0 | 0.0 |
| 45 | --- | --- | Big George | 13.00 | --- | 0.22 | 37.11 | 5.5 | 59.5 | 0.0 |
| 45 | --- | 1,558.00 | Big George | 2.50 | 60.00 | 0.04 | 37.19 | 0.0 | 25.0 | 0.0 |
| 46 | 1,558.00 | --- | Big George | 8.50 | --- | 0.13 | 37.47 | 3.0 | 82.0 | 0.0 |
| 46 | --- | --- | Big George | 5.00 | --- | 0.08 | 37.63 | 0.0 | 50.0 | 0.0 |
| 46 | --- | --- | Big George | 11.50 | --- | 0.18 | 38.01 | 1.5 | 55.0 | 2.0 |
| 46 | --- | --- | Big George | 25.00 | --- | 0.39 | 38.83 | 3.4 | 21.4 | 2.0 |
| 46 | --- | 1,560.00 | Big George | 14.00 | 64.00 | 0.22 | 39.29 | 2.5 | 67.5 | 0.0 |
| 47 | 1,560.00 | --- | Big George | 9.00 | --- | 0.17 | 39.58 | 1.0 | 89.0 | 0.0 |
| 47 | --- | --- | Big George | 7.50 | --- | 0.14 | 39.83 | 4.0 | 33.5 | 0.0 |
| 47 | --- | --- | Big George | 4.50 | --- | 0.08 | 39.98 | 0.0 | 45.0 | 0.0 |
| 47 | --- | --- | Big George | 7.00 | --- | 0.13 | 40.21 | 2.0 | 68.0 | 0.0 |
| 47 | --- | --- | Big George | 24.00 | --- | 0.45 | 40.99 | 1.0 | 10.0 | 0.0 |
| 47 | --- | --- | Big George | 1.50 | --- | 0.03 | 41.04 | 15.0 | 0.0 | 0.0 |
| 47fr | --- | 1,562.00 | Big George | 10.50 | 10.50 | 1.00 | 41.39 | --- | --- | --- |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 1 | 6.00 | 94.00 | 6.00 | 94.00 | 0.00 | --- | --- | --- |
| 39 | 3 | 62.00 | 68.00 | 47.69 | 52.31 | 0.00 | --- | --- | --- |
| 39 | 5 | 75.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 39 | 1 | 0.00 | 70.00 | 0.00 | 100.00 | 0.00 | --- | --- | -- |
| 39 | 1 | 15.00 | 190.00 | 7.32 | 92.68 | 0.00 | 27.24 | 72.76 | 0.00 |
| 40 | 3 | 14.00 | 201.00 | 6.51 | 93.49 | 0.00 | --- | --- | --- |
| 40 | 5 | 35.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 40 | , | 11.00 | 184.00 | 5.64 | 94.36 | 0.00 | --- | --- | --- |
| 40 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 40 | 3 | 27.00 | 88.00 | 23.48 | 76.52 | 0.00 | 19.83 | 80.17 | 0.00 |
| 41 | 1 | 9.00 | 186.00 | 4.62 | 95.38 | 0.00 | --- | --- | --- |
| 41 | 5 | 65.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 41 | 2 | 1.00 | 14.00 | 6.67 | 93.33 | 0.00 | --- | --- | --- |
| 41 ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 41 | 1 | 5.00 | 160.00 | 3.03 | 96.97 | 0.00 | --- | --- | --- |
| 41 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 41 | 3 | 19.00 | 131.00 | 12.67 | 87.33 | 0.00 | 20.16 | 79.84 | 0.00 |
| 42 | 3 | 30.00 | 205.00 | 12.77 | 87.23 | 0.00 | --- | --- | --- |
| 42 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 42 | 1 | 0.00 | 45.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 42 | , | 17.00 | 183.00 | 8.50 | 91.50 | 0.00 | --- | --- | --- |
| 42 | 1 | 0.00 | 30.00 | 0.00 | 100.00 | 0.00 | --- | --- | -- |
| 42 | 5 | 30.00 | 0.00 | 100.00 | 0.00 | 0.00 | 24.10 | 75.90 | 0.00 |
| 43 | 5 | 25.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 43 | 1 | 4.00 | 131.00 | 2.96 | 97.04 | 0.00 | --- | --- | --- |
| 43 | 5 | 65.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 43 | 1 | 18.00 | 187.00 | 8.78 | 91.22 | 0.00 | 26.05 | 73.95 | 0.00 |
| ns3 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 44 | 3 | 10.00 | 45.00 | 18.18 | 81.82 | 0.00 | --- | --- | --- |
| 44 | 5 | 65.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | ---- |
| 44 | 1 | 1.00 | 89.00 | 1.11 | 98.89 | 0.00 | --- | --- | --- |
| 44 | 3 | 34.00 | 196.00 | 14.78 | 85.22 | 0.00 | --- | --- | -- |
| 44 | 3 | 11.00 | 74.00 | 12.22 | 82.22 | 5.56 | 22.83 | 76.23 | 0.94 |
| 45 | 1 | 23.00 | 262.00 | 8.07 | 91.93 | 0.00 | --- | --- | --- |
| 45 | 5 | 160.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 45 | 3 | 11.00 | 119.00 | 8.46 | 91.54 | 0.00 | --- | --- | --- |
| 45 | 1 | 0.00 | 25.00 | 0.00 | 100.00 | 0.00 | 32.33 | 67.67 | 0.00 |
| 46 | 1 | 3.00 | 82.00 | 3.53 | 96.47 | 0.00 | --- | --- | --- |
| 46 | 1 | 0.00 | 50.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 46 | , | 3.00 | 110.00 | 2.61 | 95.65 | 1.74 | --- | --- | --- |
| 46 | 1 | 34.00 | 214.00 | 13.60 | 85.60 | 0.80 | --- | --- | --- |
| 46 | 1 | 5.00 | 135.00 | 3.57 | 96.43 | 0.00 | 7.03 | 92.34 | 0.63 |
| 47 | 1 | 1.00 | 89.00 | 1.11 | 98.89 | 0.00 | --- | --- | --- |
| 47 | 1 | 8.00 | 67.00 | 10.67 | 89.33 | 0.00 | --- | --- | --- |
| 47 | , | 0.00 | 45.00 | 0.00 | 100.00 | 0.00 | --- | --- | --- |
| 47 | 1 | 2.00 | 68.00 | 2.86 | 97.14 | 0.00 | --- | --- | --- |
| 47 | 2 | 21.82 | 218.18 | 9.09 | 90.91 | 0.00 | --- | --- | --- |
| 47 | 3 | 15.00 | 0.00 | 100.00 | 0.00 | 0.00 | 8.94 | 91.06 | 0.00 |
| 47fr | --- | --- | --- | --- | --- | --- | --- | --- | --- |

Table 1-27. Data for samples from core hole 32, Lance Oil and Gas Company, Inc., Whiskey Draw Unit 12-12-4778.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; fr, highly fractured sample; SubA, subbituminous A; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 25 | 40.00 | --- | --- | --- | --- |
| 39 | 25 | 40.00 | --- | --- | --- | --- |
| 39 | 25 | 40.00 | --- | --- | --- | --- |
| 39 | 25 | 40.00 | --- | --- | --- | --- |
| 39 | 25 | 40.00 | 40.00 | 97.99 | --- | --- |
| 40 | 15 | 66.67 | --- | --- | --- | --- |
| 40 | 15 | 66.67 | --- | --- | --- | --- |
| 40 | 15 | 66.67 | --- | --- | --- | --- |
| 40 | 15 | 66.67 | --- | --- | --- | --- |
| 40 | 15 | 66.67 | 66.67 | 76.54 | --- | --- |
| 41 | 15 | 66.67 | --- | --- | --- | --- |
| 41 | 15 | 66.67 | --- | --- | --- | --- |
| 41 | 15 | 66.67 | --- | --- | --- | --- |
| 41 ns | 35 | 28.57 | --- | --- | --- | Sample taken for adsorption analysis. |
| 41 | 35 | 28.57 | --- | --- | --- | --- |
| 41 | 35 | 28.57 | --- | --- | --- | --- |
| 41 | 35 | 28.57 | 45.61 | 69.23 | SubA | --- |
| 42 | 25 | 40.00 | --- | --- | --- | --- |
| 42 | 25 | 40.00 | --- | --- | --- | --- |
| 42 | 25 | 40.00 | --- | --- | --- | --- |
| 42 | 25 | 40.00 | --- | --- | --- | --- |
| 42 | 25 | 40.00 | --- | --- | --- | --- |
| 42 | 25 | 40.00 | 40.00 | 94.95 | --- | --- |
| 43 | 25 | 40.00 | --- | --- | --- | --- |
| 43 | 25 | 40.00 | --- | --- | --- | --- |
| 43 | 25 | 40.00 | --- | --- | --- | --- |
| 43 | 25 | 40.00 | 40.00 | 120.73 | --- | --- |
| ns3 | --- | --- | --- | --- | --- | No sample. |
| 44 | 20 | 50.00 | --- | --- | --- | --- |
| 44 | 20 | 50.00 | --- | --- | --- | --- |
| 44 | 20 | 50.00 | --- | --- | --- | --- |
| 44 | 20 | 50.00 | --- | --- | --- | --- |
| 44 | 20 | 50.00 | 50.00 | 95.18 | --- | 5 mm of fusain at top of unit. |
| 45 | 20 | 50.00 | --- | --- | --- | --- |
| 45 | 20 | 50.00 | --- | --- | --- | --- |
| 45 | 20 | 50.00 | --- | --- | --- | --- |
| 45 | 20 | 50.00 | 50.00 | 100.27 | --- | --- |
| 46 | 20 | 50.00 | --- | --- | --- | --- |
| 46 | 20 | 50.00 | --- | --- | --- | --- |
| 46 | 20 | 50.00 | --- | --- | --- | Fusain at 16.5 cm . |
| 46 | --- | --- | --- | --- | --- | Wood grain visible. |
| 46 | 20 | 50.00 | 50.00 | 89.41 | --- | --- |
| 47 | 20 | 50.00 | --- | --- | --- | --- |
| 47 | 20 | 50.00 | --- | --- | --- | --- |
| 47 | 20 | 50.00 | --- | --- | --- | --- |
| 47 | 20 | 50.00 | --- | --- | --- | --- |
| 47 | 20 | 50.00 | --- | --- | --- | Estimated attritus and vitrain thicknesses and percentages. |
| 47 | 20 | 50.00 | 50.00 | 80.48 | SubA | --- |
| 47fr | --- | --- | --- | --- | --- | Sample too fractured to describe. |

Table 1-28. Data for samples from core hole 33, Lance Oil and Gas Company, Inc., McBeth 12-30-4673-BG.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Appro dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | ```Canister total measured thickness (CaToMT) (cm)``` | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D2 | 950.00 | 952.00 | Big George | 56.50 | 56.50 | 1.00 | 1.85 | 1.0 | 4.0 | 0.0 |
| D3 | 952.00 | --- | Big George | 40.50 | --- | 0.68 | 3.18 | 1.4 | 56.4 | 0.0 |
| D3 | --- | --- | Big George | 3.50 | --- | 0.06 | 3.30 | 35.0 | 0.0 | 0.0 |
| D3 | --- | 954.00 | Big George | 15.50 | 59.50 | 0.26 | 3.81 | 1.5 | 76.0 | 0.0 |
| D9 | 954.00 | 956.00 | Big George | 64.50 | 64.50 | 1.00 | 5.92 | 3.0 | 77.6 | 0.0 |
| D10 | 956.00 | 958.00 | Big George | 56.00 | 56.00 | 1.00 | 7.76 | 9.8 | 60.3 | 0.0 |
| D13 | 958.00 | 960.00 | Big George | 60.50 | 60.50 | 1.00 | 9.74 | 9.8 | 141.5 | 0.0 |
| D19 | 960.00 | --- | Big George | 50.00 | --- | 0.70 | 11.38 | 1.3 | 165.3 | 0.0 |
| D19 | --- | --- | Big George | 4.00 | --- | 0.06 | 11.52 | 40.0 | 0.0 | 0.0 |
| D19 | --- | 962.00 | Big George | 17.00 | 71.00 | 0.24 | 12.07 | 2.0 | 83.0 | 0.0 |
| D20 | 962.00 | 964.00 | Big George | 70.00 | 70.00 | 1.00 | 14.37 | 3.4 | 96.6 | 0.0 |
| D21 | 964.00 | --- | Big George | 18.50 | --- | 0.30 | 14.98 | 1.0 | 91.5 | 0.0 |
| D21 | --- | --- | Big George | 2.00 | --- | 0.03 | 15.04 | 20.0 | 0.0 | 0.0 |
| D21 | --- | 966.00 | Big George | 42.00 | 62.50 | 0.67 | 16.42 | 4.4 | 79.6 | 0.0 |
| ns1 | 966.00 | 967.00 | ns1 | 30.50 | 30.50 | 1.00 | 17.42 | --- | --- | --- |
| D27 | 967.00 | --- | Big George | 8.00 | --- | 0.15 | 17.68 | 80.0 | 0.0 | 0.0 |
| D27 | --- | --- | Big George | 14.00 | --- | 0.25 | 18.14 | 10.7 | 36.0 | 0.0 |
| D27 | --- | 969.00 | Big George | 33.00 | 55.00 | 0.60 | 19.23 | 4.0 | 106.0 | 0.0 |
| D30 | 969.00 | 971.00 | Big George | 56.50 | 56.50 | 1.00 | 21.08 | 1.0 | 281.5 | 0.0 |

Table 1-28. Data for samples from core hole 33, Lance Oil and Gas Company, Inc., McBeth 12-30-4673-BG.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D2 | 2 | 113.000 | 452.000 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| D3 | 1 | 10.000 | 395.000 | 2.47 | 97.53 | 0.00 | --- | - --- | - --- |
| D3 | 5 | 35.000 | 0.000 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D3 | 1 | 3.000 | 152.000 | 1.94 | 98.06 | 0.00 | 8.07 | 91.93 | 0.00 |
| D9 | 1 | 24.000 | 621.000 | 3.72 | 96.28 | 0.00 | 3.72 | 96.28 | 0.00 |
| D10 | 3 | 78.000 | 482.000 | 13.93 | 86.07 | 0.00 | 13.93 | 86.07 | 0.00 |
| D13 | 3 | 39.000 | 566.000 | 6.45 | 93.55 | 0.00 | 6.45 | 93.55 | 0.00 |
| D19 | 1 | 4.000 | 496.000 | 0.80 | 99.20 | 0.00 | --- | --- | --- |
| D19 | 5 | 40.000 | 0.000 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D19 | 1 | 4.000 | 166.000 | 2.35 | 97.65 | 0.00 | 6.76 | 93.24 | 0.00 |
| D20 | 1 | 24.000 | 676.000 | 3.43 | 96.57 | 0.00 | 3.43 | 96.57 | 0.00 |
| D21 | 1 | 2.000 | 183.000 | 1.08 | 98.92 | 0.00 | --- | --- | --- |
| D21 | 3 | 20.000 | 0.000 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D21 | 1 | 22.000 | 398.000 | 5.24 | 94.76 | 0.00 | 7.04 | 92.96 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | - --- |
| D27 | 5 | 80.000 | 0.000 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D27 | 3 | 32.000 | 108.000 | 22.86 | 77.14 | 0.00 | --- | --- | --- |
| D27 | 1 | 12.000 | 318.000 | 3.64 | 96.36 | 0.00 | 22.55 | 77.45 | 0.00 |
| D30 | 1 | 2.000 | 563.000 | 0.35 | 99.65 | 0.00 | 0.35 | 99.65 | 0.00 |

Table 1-28. Data for samples from core hole 33, Lance Oil and Gas Company, Inc., McBeth 12-30-4673-BG.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas <br> (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D2 | 20 | 50.00 | 50.00 | 12.98 | --- | Estimated attritus and vitrain thicknesses. |
| D3 | 20 | 50.00 | --- | --- | --- | --- |
| D3 | 20 | 50.00 | --- | --- | --- | --- |
| D3 | 20 | 50.00 | 50.00 | 12.58 | SubB | --- |
| D9 | 20 | 50.00 | 50.00 | 13.43 | --- | --- |
| D10 | 30 | 33.33 | 33.33 | 13.52 | SubB | --- |
| D13 | 30 | 33.33 | 33.33 | 12.15 | --- | --- |
| D19 | 20 | 50.00 | --- | --- | --- | --- |
| D19 | 20 | 50.00 | --- | --- | --- | --- |
| D19 | 20 | 50.00 | 50.00 | 13.98 | SubB | --- |
| D20 | 20 | 50.00 | 50.00 | 12.97 | --- | --- |
| D21 | 20 | 50.00 | --- | --- | --- | --- |
| D21 | 20 | 50.00 | --- | --- | --- | --- |
| D21 | 20 | 50.00 | 50.00 | 13.23 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| D27 | 25 | 40.00 | --- | --- | --- | --- |
| D27 | 25 | 40.00 | --- | --- | --- | --- |
| D27 | 25 | 40.00 | 40.00 | 14.31 | SubB | --- |
| D30 | 30 | 33.33 | 33.33 | 12.93 | --- | --- |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 48 | 328.00 | --- | Anderson | 12.00 | --- | 0.21 | 0.39 | 120.0 | 0.0 | 0.0 |
| 48 | --- | --- | Anderson | 24.00 | --- | 0.41 | 1.18 | 1.0 | 19.0 | 0.0 |
| 48 | --- | --- | Anderson | 14.00 | --- | 0.24 | 1.64 | 10.0 | 30.0 | 2.0 |
| 48 | --- | --- | Anderson | 6.00 | --- | 0.10 | 1.84 | 60.0 | 0.0 | 0.0 |
| 48 | --- | 330.00 | Anderson | 2.50 | 58.50 | 0.04 | 1.92 | 1.0 | 19.0 | 0.0 |
| 49 | 330.00 | --- | Anderson | 6.50 | --- | 0.14 | 2.13 | 65.0 | 0.0 | 0.0 |
| 49 | --- | --- | Anderson | 33.00 | --- | 0.70 | 3.22 | 2.0 | 38.0 | 0.0 |
| 49 | --- | 332.00 | Anderson | 7.50 | 47.00 | 0.16 | 3.46 | 75.0 | 0.0 | 0.0 |
| 50 | 332.00 | 334.00 | Anderson | 58.00 | 58.00 | 1.00 | 5.36 | 3.0 | 12.0 | 0.0 |
| 51 | 334.00 | --- | Anderson | 6.50 | --- | 0.14 | 5.58 | 2.0 | 18.0 | 0.0 |
| 51 | --- | --- | Anderson | 11.50 | --- | 0.25 | 5.95 | 20.0 | 13.3 | 2.0 |
| 51 | --- | 336.00 | Anderson | 28.00 | 46.00 | 0.61 | 6.87 | 10.0 | 15.0 | 0.0 |
| 52 | 336.00 | --- | Anderson | 22.50 | --- | 0.37 | 7.61 | 2.0 | 18.0 | 0.0 |
| 52 | --- | --- | Anderson | 13.50 | --- | 0.22 | 8.05 | 20.0 | 8.6 | 0.0 |
| 52 | --- | --- | Anderson | 19.50 | --- | 0.32 | 8.69 | 2.0 | 38.0 | 0.0 |
| 52 | --- | 338.00 | Anderson | 5.00 | 60.50 | 0.08 | 8.86 | 20.0 | 20.0 | 0.0 |
| 53 | 338.00 | --- | Anderson | 21.00 | --- | 0.36 | 9.55 | 2.0 | 11.3 | 0.0 |
| 53 | --- | --- | Anderson | 8.50 | --- | 0.14 | 9.83 | 85.0 | 0.0 | 0.0 |
| 53 | --- | 340.00 | Anderson | 29.50 | 59.00 | 0.50 | 10.79 | 3.0 | 27.0 | 0.0 |
| 54 | 340.00 | --- | Anderson | 9.00 | --- | 0.15 | 11.09 | 90.0 | 0.0 | 0.0 |
| 54 | --- | 342.00 | Anderson | 50.00 | 59.00 | 0.85 | 12.73 | 15.0 | 22.5 | 0.0 |
| 55 | 342.00 | 344.00 | Anderson | 59.00 | 59.00 | 1.00 | 14.67 | 1.0 | 19.0 | 0.0 |
| 56 | 344.00 | --- | Anderson | 21.00 | --- | 0.65 | 15.35 | 4.0 | 76.0 | 0.0 |
| 56 | --- | --- | Anderson | 5.50 | --- | 0.17 | 15.53 | 55.0 | 0.0 | 0.0 |
| 56 | --- | 346.00 | Anderson | 6.00 | 32.50 | 0.18 | 15.73 | 1.0 | 19.0 | 0.0 |
| 57 | 346.00 | --- | Anderson | 12.50 | --- | 0.23 | 16.14 | 3.0 | 27.0 | 0.0 |
| 57 | --- | --- | Anderson | 7.00 | --- | 0.13 | 16.37 | 70.0 | 0.0 | 0.0 |
| 57 | --- | 348.00 | Anderson | 35.00 | 54.50 | 0.64 | 17.52 | 5.0 | 20.0 | 0.0 |
| 58 | 348.00 | --- | Anderson | 21.50 | --- | 0.37 | 18.23 | 215.0 | 0.0 | 0.0 |
| 58 | --- | 350.00 | Anderson | 36.50 | 58.00 | 0.63 | 19.42 | 3.0 | 12.0 | 0.0 |
| 59 | 350.00 | 352.00 | Anderson | 58.00 | 58.00 | 1.00 | 21.33 | 1.0 | 19.0 | 0.0 |
| 61 | 352.00 | --- | Anderson | 8.00 | --- | 0.13 | 21.59 | 1.0 | 9.0 | 0.0 |
| 61 | --- | --- | Anderson | 10.50 | --- | 0.16 | 21.93 | 20.0 | 2.2 | 0.0 |
| 61 | --- | --- | Anderson | 35.00 | --- | 0.55 | 23.08 | 2.0 | 18.0 | 0.0 |
| 61 | --- | 354.00 | Anderson | 10.50 | 64.00 | 0.16 | 23.43 | 20.0 | 2.2 | 0.0 |
| 62 | 354.00 | 356.00 | Anderson | 52.50 | 52.50 | 1.00 | 25.15 | 2.0 | 11.3 | 2.0 |
| 63 | 356.00 | --- | Anderson | 30.00 | --- | 0.48 | 26.13 | 2.0 | 18.0 | 0.0 |
| 63 | --- | --- | Anderson | 7.00 | --- | 0.11 | 26.36 | 70.0 | 0.0 | 0.0 |
| 63 | --- | 358.00 | Anderson | 25.00 | 62.00 | 0.40 | 27.18 | 2.0 | 18.0 | 0.0 |
| 8 | 358.00 | 360.00 | Anderson | 58.00 | 58.00 | 1.00 | 29.08 | 2.0 | 4.7 | 0.0 |
| 7 | 360.00 | --- | Anderson | 26.00 | --- | 0.55 | 29.94 | 3.0 | 17.0 | 0.0 |
| 7 | --- | 361.80 | Anderson | 21.50 | 47.50 | 0.45 | 30.64 | 0.0 | 0.0 | 0.0 |
| ns1 | 361.80 | 507.50 | ns1 | 4440.94 | 4,440.94 | 1.00 | 176.34 | --- | --- | -- |
| 6 | 507.50 | --- | Canyon | 13.50 | --- | 0.38 | 176.79 | 2.0 | 8.0 | 0.0 |
| 6 | --- | 508.50 | Canyon | 22.00 | 35.50 | 0.62 | 177.51 | 10.0 | 10.0 | 0.0 |
| 5 | 508.50 | 510.50 | Canyon | 54.00 | 54.00 | 1.00 | 179.28 | 3.0 | 12.0 | 0.0 |
| 4 | 510.50 | 512.50 | Canyon | 67.00 | 67.00 | 1.00 | 181.48 | 3.0 | 27.0 | 0.0 |
| 3 | 512.50 | 514.50 | Canyon | 54.00 | 54.00 | 1.00 | 183.25 | 3.0 | 27.0 | 0.0 |
| 2 | 514.50 | 516.50 | Canyon | 60.50 | 60.50 | 1.00 | 185.23 | 3.0 | 57.0 | 0.0 |
| 71 | 516.50 | 518.50 | Canyon | 64.00 | 64.00 | 1.00 | 187.33 | 15.0 | 60.0 | 0.0 |
| 70 | 518.50 | 520.50 | Canyon | 56.50 | 56.50 | 1.00 | 189.19 | 3.0 | 12.0 | 0.0 |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 48 | 5 | 120.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 48 | 2 | 12.00 | 228.00 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| 48 | 3 | 34.50 | 103.50 | 24.64 | 73.93 | 1.43 | --- | --- | --- |
| 48 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 48 | 2 | 1.25 | 23.75 | 5.00 | 95.00 | 0.00 | 38.93 | 60.73 | 0.34 |
| 49 | 5 | 65.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 49 | 2 | 16.50 | 313.50 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| 49 | 5 | 75.00 | 0.00 | 100.00 | 0.00 | 0.00 | 33.30 | 66.70 | 0.00 |
| 50 | 2 | 116.00 | 464.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| 51 | 2 | 6.50 | 58.50 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 51 | 3 | 67.80 | 45.20 | 58.96 | 39.30 | 1.74 | --- | --- | --- |
| 51 | 3 | 112.00 | 168.00 | 40.00 | 60.00 | 0.00 | 40.50 | 59.07 | 0.43 |
| 52 | 2 | 22.50 | 202.50 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 52 | 3 | 94.50 | 40.50 | 70.00 | 30.00 | 0.00 | --- | --- | --- |
| 52 | 2 | 9.75 | 185.25 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| 52 | 3 | 25.00 | 25.00 | 50.00 | 50.00 | 0.00 | 25.08 | 74.92 | 0.00 |
| 53 | 2 | 31.50 | 178.50 | 15.00 | 85.00 | 0.00 | --- | --- | --- |
| 53 | 5 | 85.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 53 | 2 | 29.50 | 265.50 | 10.00 | 90.00 | 0.00 | 24.75 | 75.25 | 0.00 |
| 54 | 5 | 90.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 54 | 3 | 200.00 | 300.00 | 40.00 | 60.00 | 0.00 | 49.15 | 50.85 | 0.00 |
| 55 | 2 | 29.50 | 560.50 | 5.00 | 95.00 | 0.00 | 5.00 | 95.00 | 0.00 |
| 56 | 2 | 10.50 | 199.50 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| 56 | 5 | 55.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 56 | 2 | 3.00 | 57.00 | 5.00 | 95.00 | 0.00 | 21.08 | 78.92 | 0.00 |
| 57 | 2 | 12.50 | 112.50 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 57 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 57 | 3 | 70.00 | 280.00 | 20.00 | 80.00 | 0.00 | 27.98 | 72.02 | 0.00 |
| 58 | 5 | 215.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 58 | 2 | 73.00 | 292.00 | 20.00 | 80.00 | 0.00 | 49.66 | 50.34 | 0.00 |
| 59 | 2 | 29.00 | 551.00 | 5.00 | 95.00 | 0.00 | 5.00 | 95.00 | 0.00 |
| 61 | 2 | 8.00 | 72.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 61 | 3 | 94.50 | 10.50 | 90.00 | 10.00 | 0.00 | --- | --- | --- |
| 61 | 2 | 35.00 | 315.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 61 | 3 | 94.50 | 10.50 | 90.00 | 10.00 | 0.00 | 36.25 | 63.75 | 0.00 |
| 62 | 2 | 78.45 | 444.55 | 14.94 | 84.68 | 0.38 | 14.94 | 84.68 | 0.38 |
| 63 | 2 | 30.00 | 270.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| 63 | 5 | 70.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 63 | 2 | 25.00 | 225.00 | 10.00 | 90.00 | 0.00 | 20.16 | 79.84 | 0.00 |
| 8 | 2 | 174.00 | 406.00 | 30.00 | 70.00 | 0.00 | 30.00 | 70.00 | 0.00 |
| 7 | 2 | 39.00 | 221.00 | 15.00 | 85.00 | 0.00 | --- | --- | --- |
| 7 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.21 | 46.53 | 0.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| 6 | 2 | 27.00 | 108.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| 6 | 3 | 110.00 | 110.00 | 50.00 | 50.00 | 0.00 | 38.59 | 61.41 | 0.00 |
| 5 | 2 | 108.00 | 432.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| 4 | 2 | 67.00 | 603.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| 3 | 2 | 54.00 | 486.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| 2 | 2 | 30.25 | 574.75 | 5.00 | 95.00 | 0.00 | 5.00 | 95.00 | 0.00 |
| 71 | 3 | 128.00 | 512.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| 70 | 2 | 113.00 | 452.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 48 | 20 | 50.00 | --- | --- | --- | --- |
| 48 | 60 | 16.67 | --- | --- | --- | --- |
| 48 | 60 | 16.67 | --- | --- | --- | Fusain is at top of unit. |
| 48 | 60 | 16.67 | --- | --- | --- | --- |
| 48 | 60 | 16.67 | 23.50 | 2.44 | --- | --- |
| 49 | 60 | 16.67 | --- | --- | --- | --- |
| 49 | 60 | 16.67 | --- | --- | --- | --- |
| 49 | 60 | 16.67 | 16.67 | 0.43 | SubC | --- |
| 50 | 20 | 50.00 | 50.00 | 2.41 | --- | --- |
| 51 | 20 | 50.00 | --- | --- | --- | --- |
| 51 | 20 | 50.00 | --- | --- | --- | Fusain is at top of unit. |
| 51 | 20 | 50.00 | 50.00 | 2.33 | --- | --- |
| 52 | 20 | 50.00 | --- | --- | --- | --- |
| 52 | 20 | 50.00 | --- | --- | --- | --- |
| 52 | 20 | 50.00 | --- | --- | --- | --- |
| 52 | 20 | 50.00 | 50.00 | 1.16 | --- | --- |
| 53 | 15 | 66.67 | --- | --- | --- | --- |
| 53 | 25 | 40.00 | --- | --- | --- | --- |
| 53 | 25 | 40.00 | 49.49 | 2.20 | --- | --- |
| 54 | 25 | 40.00 | --- | --- | --- | --- |
| 54 | 25 | 40.00 | 40.00 | 2.86 | --- | --- |
| 55 | 60 | 16.67 | 16.67 | 2.34 | SubB | --- |
| 56 | 60 | 16.67 | --- | --- | --- | --- |
| 56 | 60 | 16.67 | --- | --- | --- | --- |
| 56 | 60 | 16.67 | 16.67 | 1.46 | --- | --- |
| 57 | 25 | 40.00 | --- | --- | --- | -- |
| 57 | 25 | 40.00 | --- | --- | --- | --- |
| 57 | 15 | 66.67 | 57.13 | 2.48 | --- | --- |
| 58 | 25 | 40.00 | --- | --- | --- | --- |
| 58 | 25 | 40.00 | 40.00 | 1.82 | --- | --- |
| 59 | 60 | 16.67 | 16.67 | 1.54 | --- | --- |
| 61 | 60 | 16.67 | --- | --- | --- | --- |
| 61 | 60 | 16.67 | --- | --- | --- | --- |
| 61 | 60 | 16.67 | --- | --- | --- | --- |
| 61 | 60 | 16.67 | 16.67 | 1.22 | --- | --- |
| 62 | 60 | 16.67 | 16.67 | 0.99 | --- | Fusain at 4.5 cm . |
| 63 | 60 | 16.67 | --- | --- | --- | --- |
| 63 | 60 | 16.67 | --- | --- | --- | --- |
| 63 | 60 | 16.67 | 16.67 | 2.20 | SubC | --- |
| 8 | 60 | 16.67 | 16.67 | 1.59 | --- | --- |
| 7 | 60 | 16.67 | --- | --- | --- | --- |
| 7 | 60 | 16.67 | 16.67 | 0.87 | -- | Carbonaceous shale. |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| 6 | 60 | 16.67 | --- | --- | --- | --- |
| 6 | 60 | 16.67 | 16.67 | 1.23 | --- | --- |
| 5 | 60 | 16.67 | 16.67 | 5.53 | --- | --- |
| 4 | 60 | 16.67 | 16.67 | 5.10 | --- | --- |
| 3 | 60 | 16.67 | 16.67 | 4.63 | --- | --- |
| 2 | 60 | 16.67 | 16.67 | 3.05 | --- | --- |
| 71 | 60 | 16.67 | 16.67 | 3.81 | --- | --- |
| 70 | 60 | 16.67 | 16.67 | 2.60 | --- | --- |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| 69 | 520.50 | 522.50 | Canyon | 48.00 | 48.00 | 1.00 | 190.76 | 10.0 | 90.0 | 0.0 |
| 68 | 522.50 | 524.50 | Canyon | 70.00 | 70.00 | 1.00 | 193.06 | 5.0 | 20.0 | 0.0 |
| 67 | 524.50 | --- | Canyon | 8.00 | --- | 0.13 | 193.32 | 80.0 | 0.0 | 0.0 |
| 67 | --- | --- | Canyon | 41.00 | --- | 0.65 | 194.67 | 3.0 | 12.0 | 0.0 |
| 67 | --- | --- | Canyon | 10.00 | --- | 0.16 | 194.99 | 100.0 | 0.0 | 0.0 |
| 67 | --- | 526.50 | Canyon | 4.00 | 63.00 | 0.06 | 195.13 | 2.0 | 18.0 | 0.0 |
| 66 | 526.50 | 528.50 | Canyon | 58.50 | 58.50 | 1.00 | 197.05 | 5.0 | 20.0 | 0.0 |
| 65 | 528.50 | --- | Canyon | 32.00 | --- | 0.51 | 198.10 | 15.0 | 60.0 | 4.0 |
| 65 | --- | 530.50 | Canyon | 31.00 | 63.00 | 0.49 | 199.11 | 1.0 | 19.0 | 0.0 |
| 64 | 530.50 | 532.50 | Canyon | 51.00 | 51.00 | 1.00 | 200.79 | 5.0 | 11.7 | 0.0 |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 69 | 3 | 48.00 | 432.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| 68 | 3 | 140.00 | 560.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| 67 | 5 | 80.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 67 | 2 | 82.00 | 328.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| 67 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| 67 | 2 | 4.00 | 36.00 | 10.00 | 90.00 | 0.00 | 42.22 | 57.78 | 0.00 |
| 66 | 3 | 117.00 | 468.00 | 20.00 | 80.00 | 0.00 | 20.00 | 80.00 | 0.00 |
| 65 | 3 | 63.20 | 252.80 | 19.75 | 79.00 | 1.25 | --- | --- | - |
| 65 | 2 | 15.50 | 294.50 | 5.00 | 95.00 | 0.00 | 12.49 | 86.87 | 0.63 |
| 64 | 3 | 153.00 | 357.00 | 30.00 | 70.00 | 0.00 | 30.00 | 70.00 | 0.00 |

Table 1-29. Data for samples from core hole 34, Williams Production RMT Company, State 23-16-4171.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 69 | 60 | 16.67 | 16.67 | 4.02 | SubC | --- |
| 68 | 60 | 16.67 | 16.67 | 4.71 | --- | --- |
| 67 | 60 | 16.67 | --- | --- | --- | --- |
| 67 | 60 | 16.67 | --- | --- | --- | Pyrite layer sampled at 115 mm . |
| 67 | 60 | 16.67 | --- | --- | --- | --- |
| 67 | 60 | 16.67 | 16.67 | 4.09 | --- | --- |
| 66 | 60 | 16.67 | 16.67 | 2.78 | --- | Thick vitrain at 14 cm above base. |
| 65 | 60 | 16.67 | --- | --- | --- | Fusain at 20.5 cm below top. |
| 65 | 60 | 16.67 | 16.67 | 2.64 | --- | --- |
| 64 | 60 | 16.67 | 16.67 | 1.13 | SubB | --- |

Table 1-30. Data for samples from core hole 35, Williams Production Company, Groves 12-19-4574.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Approx depth | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) | Cumulative fusain thickness (CuFT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |  |
| D1 | 1,197.00 | 1,199.00 | Big George | 59.00 | 59.00 | 1.00 | 1.94 | 2.0 | 18.0 | 0.0 |
| D2 | 1,199.00 | --- | Big George | 34.50 | --- | 0.61 | 3.07 | 3.0 | 9.0 | 3.0 |
| D2 | --- | --- | Big George | 5.00 | --- | 0.09 | 3.23 | 5.0 | 1.3 | 0.0 |
| D2 | --- | 1,201.00 | Big George | 17.00 | 56.50 | 0.30 | 3.79 | 2.0 | 11.3 | 0.0 |
| D3 | 1,201.00 | --- | Big George | 10.00 | --- | 0.16 | 4.12 | 1.0 | 19.0 | 0.0 |
| D3 | --- | --- | Big George | 17.00 | --- | 0.27 | 4.68 | 170.0 | 0.0 | 0.0 |
| D3 | --- | --- | Big George | 24.00 | --- | 0.38 | 5.46 | 2.0 | 18.0 | 0.0 |
| D3 | --- | --- | Big George | 9.00 | --- | 0.14 | 5.76 | 5.0 | 5.0 | 0.0 |
| D3 | --- | 1,203.00 | Big George | 4.00 | 64.00 | 0.06 | 5.89 | 8.0 | 1.4 | 0.0 |
| D5 | 1,203.00 | --- | Big George | 22.00 | --- | 0.45 | 6.61 | 10.0 | 1.1 | 0.0 |
| D5 | --- | --- | Big George | 23.00 | --- | 0.47 | 7.37 | 1.0 | 19.0 | 0.0 |
| D5 | --- | 1,205.00 | Big George | 4.00 | 49.00 | 0.08 | 7.50 | 40.0 | 0.0 | 0.0 |
| D6 | 1,205.00 | ---- | Big George | 18.00 | --- | 0.32 | 8.09 | 180.0 | 0.0 | 0.0 |
| D6 | --- | --- | Big George | 20.00 | --- | 0.36 | 8.74 | 1.0 | 19.0 | 0.0 |
| D6 | --- | 1,207.00 | Big George | 18.00 | 56.00 | 0.32 | 9.33 | 4.0 | 22.7 | 0.0 |
| ns1 | 1,207.00 | 1,225.00 | ns1 | 548.50 | 548.50 | 1.00 | 27.33 | --- | --- | --- |
| D7 | 1,225.00 | 1,227.00 | Big George | 61.50 | 61.50 | 1.00 | 29.35 | 1.0 | 19.0 | 0.0 |
| D8 | 1,227.00 | --- | Big George | 37.50 | --- | 0.65 | 30.58 | 2.0 | 18.0 | 0.0 |
| D8 | --- | 1,229.00 | Big George | 20.00 | 57.50 | 0.35 | 31.23 | 5.0 | 5.0 | 0.0 |
| D9 | 1,229.00 | 1,231.00 | Big George | 52.00 | 52.00 | 1.00 | 32.94 | 2.0 | 18.0 | 0.0 |
| D10 | 1,231.00 | 1,233.00 | Big George | 62.00 | 62.00 | 1.00 | 34.97 | 3.0 | 27.0 | 0.0 |
| D11 | 1,233.00 | --- | Big George | 22.50 | --- | 0.39 | 35.71 | 1.0 | 19.0 | 0.0 |
| D11 | --- | 1,235.00 | Big George | 35.00 | 57.50 | 0.61 | 36.86 | 5.0 | 5.0 | 0.0 |
| D12 | 1,235.00 | --- | Big George | 12.00 | --- | 0.21 | 37.25 | 1.0 | 9.0 | 0.0 |
| D12 | --- | --- | Big George | 10.00 | --- | 0.18 | 37.58 | 100.0 | 0.0 | 0.0 |
| D12 | --- | --- | Big George | 16.00 | --- | 0.28 | 38.11 | 5.0 | 20.0 | 0.0 |
| D12 | --- | --- | Big George | 11.00 | --- | 0.19 | 38.47 | 110.0 | 0.0 | 0.0 |
| D12 | --- | 1,237.00 | Big George | 8.00 | 57.00 | 0.14 | 38.73 | 1.0 | 19.0 | 0.0 |
| D13 | 1,237.00 | --- | Big George | 17.00 | --- | 0.28 | 39.29 | 1.0 | 19.0 | 0.0 |
| D13 | --- | --- | Big George | 22.50 | --- | 0.38 | 40.03 | 225.0 | 0.0 | 0.0 |
| D13 | --- | 1,239.00 | Big George | 20.50 | 60.00 | 0.34 | 40.70 | 1.0 | 19.0 | 0.0 |
| D14 | 1,239.00 | --- | Big George | 36.00 | --- | 0.58 | 41.88 | 5.0 | 7.5 | 0.0 |
| D14 | --- | 1,241.00 | Big George | 26.00 | 62.00 | 0.42 | 42.73 | 1.0 | 19.0 | 0.0 |
| D15 | 1,241.00 | --- | Big George | 24.50 | --- | 0.73 | 43.54 | 1.0 | 19.0 | 0.0 |
| D15ns | --- | --- | Big George | 27.00 | --- | 1.00 | 44.42 | --- | --- | --- |
| D15 | --- | 1,243.00 | Big George | 9.00 | 33.50 | 0.27 | 44.72 | 1.0 | 19.0 | 0.0 |
| D17 | 1,243.00 | --- | Big George | 15.00 | --- | 0.55 | 45.21 | 5.0 | 5.0 | 0.0 |
| D17ns | --- | --- | Big George | 30.00 | --- | 1.00 | 46.19 | --- | --- | --- |
| D17 | --- | 1,245.00 | Big George | 12.50 | 27.50 | 0.45 | 46.60 | 1.0 | 19.0 | 0.0 |
| ns2 | 1,245.00 | 1,246.50 | ns2 | 46.00 | 46.00 | 1.00 | 48.11 | --- | --- | --- |
| D18 | 1,246.50 | --- | Big George | 8.50 | --- | 0.15 | 48.39 | 5.0 | 5.0 | 0.0 |
| D18 | --- | --- | Big George | 32.00 | --- | 0.58 | 49.44 | 2.0 | 18.0 | 0.0 |
| D18 | --- | 1,248.50 | Big George | 14.50 | 55.00 | 0.26 | 49.92 | 5.0 | 5.0 | 0.0 |
| D19 | 1,248.50 | --- | Big George | 51.00 | --- | 0.87 | 51.59 | 3.0 | 12.0 | 0.0 |
| D19 | --- | 1,250.50 | Big George | 7.50 | 58.50 | 0.13 | 51.84 | 75.0 | 0.0 | 0.0 |
| D20 | 1,250.50 | --- | Big George | 15.00 | --- | 0.25 | 52.33 | 10.0 | 6.7 | 0.0 |
| D20 | --- | 1,252.50 | Big George | 46.00 | 61.00 | 0.75 | 53.84 | 2.0 | 18.0 | 0.0 |
| D21 | 1,252.50 | --- | Big George | 16.00 | --- | 0.27 | 54.36 | 3.0 | 27.0 | 0.0 |
| D21 | --- | --- | Big George | 6.00 | --- | 0.10 | 54.56 | 60.0 | 0.0 | 0.0 |
| D21 | --- | 1,254.50 | Big George | 37.00 | 59.00 | 0.63 | 55.77 | 3.0 | 12.0 | 0.0 |
| D22 | 1,254.50 | 1,256.50 | Big George | 45.00 | 45.00 | 1.00 | 57.25 | 1.0 | 9.0 | 0.0 |

Table 1-30. Data for samples from core hole 35, Williams Production Company, Groves 12-19-4574.—Cotninued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Lithotype code | Cumulative vitrain thickness (CuVT) (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | $\begin{gathered} \text { Canister } \\ \text { average } \\ \text { vitrain } \\ \text { percentage } \\ \text { (CaAvVP) } \end{gathered}$ | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2 | 59.00 | 531.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| D2 | 2 | 85.50 | 256.50 | 24.78 | 74.35 | 0.87 | --- | --- | --- |
| D2 | 3 | 40.00 | 10.00 | 80.00 | 20.00 | 0.00 | --- | --- | --- |
| D2 | 2 | 25.50 | 144.50 | 15.00 | 85.00 | 0.00 | 26.73 | 72.74 | 0.53 |
| D3 | 2 | 5.00 | 95.00 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D3 | 5 | 170.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D3 | 2 | 24.00 | 216.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| D3 | 3 | 45.00 | 45.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| D3 | 3 | 34.00 | 6.00 | 85.00 | 15.00 | 0.00 | 43.44 | 56.56 | 0.00 |
| D5 | 3 | 198.00 | 22.00 | 90.00 | 10.00 | 0.00 | --- | --- | --- |
| D5 | 2 | 11.50 | 218.50 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D5 | 5 | 40.00 | 0.00 | 100.00 | 0.00 | 0.00 | 50.92 | 49.08 | 0.00 |
| D6 | 5 | 180.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D6 | 2 | 10.00 | 190.00 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D6 | 2 | 27.00 | 153.00 | 15.00 | 85.00 | 0.00 | 38.75 | 61.25 | 0.00 |
| ns 1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D7 | 2 | 30.75 | 584.25 | 5.00 | 95.00 | 0.00 | 5.00 | 95.00 | 0.00 |
| D8 | 2 | 37.50 | 337.50 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| D8 | 3 | 100.00 | 100.00 | 50.00 | 50.00 | 0.00 | 23.91 | 76.09 | 0.00 |
| D9 | 2 | 52.00 | 468.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| D10 | 2 | 62.00 | 558.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |
| D11 | 2 | 11.25 | 213.75 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D11 | 3 | 175.00 | 175.00 | 50.00 | 50.00 | 0.00 | 32.39 | 67.61 | 0.00 |
| D12 | 2 | 12.00 | 108.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| D12 | 5 | 100.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D12 | 3 | 32.00 | 128.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| D12 | 5 | 110.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D12 | 2 | 4.00 | 76.00 | 5.00 | 95.00 | 0.00 | 45.26 | 54.74 | 0.00 |
| D13 | 2 | 8.50 | 161.50 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D13 | 5 | 225.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D13 | 2 | 10.25 | 194.75 | 5.00 | 95.00 | 0.00 | 40.63 | 59.38 | 0.00 |
| D14 | 3 | 144.00 | 216.00 | 40.00 | 60.00 | 0.00 | --- | --- | --- |
| D14 | 2 | 13.00 | 247.00 | 5.00 | 95.00 | 0.00 | 25.32 | 74.68 | 0.00 |
| D15 | 2 | 12.25 | 232.75 | 5.00 | 95.00 | 0.00 | --- | --- | --- |
| D15ns | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D15 | 2 | 4.50 | 85.50 | 5.00 | 95.00 | 0.00 | 5.00 | 95.00 | 0.00 |
| D17 | 3 | 75.00 | 75.00 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| D17ns | --- | 199.50 | 199.50 | 66.50 | 66.50 | -33.00 | --- | --- | --- |
| D17 | 2 | 6.25 | 118.75 | 5.00 | 95.00 | 0.00 | 29.55 | 70.45 | 0.00 |
| ns2 | -- | --- | --- | --- | --- | --- | --- | --- | --- |
| D18 | 3 | 42.50 | 42.50 | 50.00 | 50.00 | 0.00 | --- | --- | --- |
| D18 | 2 | 32.00 | 288.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| D18 | 3 | 72.50 | 72.50 | 50.00 | 50.00 | 0.00 | 26.73 | 73.27 | 0.00 |
| D19 | 2 | 102.00 | 408.00 | 20.00 | 80.00 | 0.00 | --- | --- | --- |
| D19 | 5 | 75.00 | 0.00 | 100.00 | 0.00 | 0.00 | 30.26 | 69.74 | 0.00 |
| D20 | 3 | 90.00 | 60.00 | 60.00 | 40.00 | 0.00 | --- | --- | --- |
| D20 | 2 | 46.00 | 414.00 | 10.00 | 90.00 | 0.00 | 22.30 | 77.70 | 0.00 |
| D21 | 2 | 16.00 | 144.00 | 10.00 | 90.00 | 0.00 | --- | --- | --- |
| D21 | 5 | 60.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- | --- | --- |
| D21 | 2 | 74.00 | 296.00 | 20.00 | 80.00 | 0.00 | 25.42 | 74.58 | 0.00 |
| D22 | 2 | 45.00 | 405.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 | 0.00 |

Table 1-30. Data for samples from core hole 35, Williams Production Company, Groves 12-19-4574.—Cotninued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; ns, no sample available; SubB, subbituminous B; SubC, subbituminous C; ---, no data]

| Canister number | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 25 | 40.00 | 40.00 | 18.01 | --- | Highly fragmented sample. |
| D2 | 25 | 40.00 | --- | --- | --- | -- |
| D2 | 25 | 40.00 | --- | --- | --- | --- |
| D2 | 25 | 40.00 | 40.00 | 16.82 | --- | --- |
| D3 | 30 | 33.33 | --- | --- | --- | --- |
| D3 | 30 | 33.33 | --- | --- | --- | --- |
| D3 | 30 | 33.33 | --- | --- | --- | --- |
| D3 | 25 | 40.00 | --- | --- | --- | --- |
| D3 | 25 | 40.00 | 34.69 | 19.81 | --- | --- |
| D5 | 30 | 33.33 | --- | --- | --- | --- |
| D5 | 30 | 33.33 | --- | --- | --- | --- |
| D5 | 35 | 28.57 | 32.94 | 17.93 | --- | --- |
| D6 | 30 | 33.33 | --- | --- | -- | --- |
| D6 | 30 | 33.33 | --- | --- | --- | --- |
| D6 | 25 | 40.00 | 35.48 | 17.31 | --- | --- |
| ns1 | --- | --- | --- | --- | --- | No sample. |
| D7 | 30 | 33.33 | 33.33 | 19.51 | SubC | --- |
| D8 | 30 | 33.33 | --- | --- | --- | --- |
| D8 | 25 | 40.00 | 35.65 | 18.61 | --- | --- |
| D9 | 25 | 40.00 | 40.00 | 17.16 | --- | Calcite(?) on cleat. |
| D10 | 25 | 40.00 | 40.00 | 18.34 | --- | Calcite( |
| D11 | 25 | 40.00 | --- | --- | --- | --- |
| D11 | 25 | 40.00 | 40.00 | 17.18 | --- | --- |
| D12 | 25 | 40.00 | --- | --- | --- | --- |
| D12 | 20 | 50.00 | --- | --- | --- | --- |
| D12 | 20 | 50.00 | --- | --- | --- | --- |
| D12 | 30 | 33.33 | --- | -- | --- | --- |
| D12 | 25 | 40.00 | 43.27 | 17.68 | -- | --- |
| D13 | 30 | 33.33 | --- | --- | --- | --- |
| D13 | 30 | 33.33 | -- | --- | --- | --- |
| D13 | 30 | 33.33 | 33.33 | 17.32 | SubC | --- |
| D14 | 20 | 50.00 | --- | --- | --- | --- |
| D14 | 20 | 50.00 | 50.00 | 17.01 | --- | --- - - - |
| D15 | 30 | 33.33 | --- | --- | --- | --- |
| D15ns | --- | --- | --- | --- | --- | Bag sample taken. |
| D15 | 30 | 33.33 | 33.33 | 15.89 | --- | --- |
| D17 | 20 | 50.00 | --- | --- | -- | Large vitrain fragment ( 30 mm thick) at 75 mm below top of canister. |
| D17ns | --- | --- | --- | --- | --- | Bag sample taken. |
| D17 | 15 | 66.67 | 57.58 | 13.91 | --- | --- |
| ns 2 | --- | --- | --- | --- | -- | No sample. |
| D18 | 30 | 33.33 | --- | --- | --- | --- |
| D18 | 30 | 33.33 | --- | --- | --- | --- |
| D18 | 30 | 33.33 | 33.33 | 18.32 | --- | --- |
| D19 | 35 | 28.57 | --- | --- | --- | -- |
| D19 | 30 | 33.33 | 29.18 | 17.19 | --- | --- |
| D20 | 20 | 50.00 | --- | --- | --- | Thick vitrain (40 mm) at 45 and 100 mm below top. |
| D20 | 25 | 40.00 | 42.46 | 19.20 | SubB | --- |
| D21 | 25 | 40.00 | --- | -- | --- | --- |
| D21 | 25 | 40.00 | --- | --- | --- | --- |
| D21 | 25 | 40.00 | 40.00 | 18.08 | --- | --- |
| D22 | 25 | 40.00 | 40.00 | 16.05 | --- | --- |

Table 1-31. Data for samples from core hole 36, Peabody Natural Gas, LLC, PNG 24-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; ---, no data]

| Canister number | Appro dept | $\begin{aligned} & \text { ximate } \\ & \text { h (ft) } \end{aligned}$ | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| D23 | 1,256.70 | --- | Pawnee | 20.30 |  | 0.36 | 0.67 | 0.0 | 0.0 |
| D23 | --- | 1,258.20 | Pawnee | 36.50 | 56.80 | 0.64 | 1.86 | 3.0 | 17.0 |
| D24 | 1,258.20 | 1,259.20 | Pawnee | 45.00 | 45.00 | 1.00 | 3.34 | 2.0 | 18.0 |
| ns1 | 1,259.20 | 1,272.10 | ns1 | 393.00 | 393.00 | 1.00 | 16.23 | --- | --- |
| D25 | 1,272.10 | --- | Pawnee | 45.50 | --- | 0.65 | 17.73 | 4.0 | 16.0 |
| D25 | --- | --- | Pawnee | 11.00 | --- | 0.16 | 18.09 | 1.0 | 19.0 |
| D25 | --- | 1,275.10 | Pawnee | 14.00 | 70.50 | 0.20 | 18.55 | 5.0 | 7.5 |
| D26 | 1,275.20 | 1,276.20 | Pawnee | 35.00 | 35.00 | 1.00 | 19.69 | 3.0 | 7.0 |

Table 1-31. Data for samples from core hole 36, Peabody Natural Gas, LLC, PNG 24-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain <br> thickness <br> (CuVT) <br> (mm) | Cumulative attritus thickness (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) | Canister average attrital percentage (CaAvAP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D23 | 0.0 | 0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | --- | --- |
| D23 | 0.0 | 2 | 54.75 | 310.25 | 15.00 | 85.00 | 0.00 | 9.64 | 54.62 |
| D24 | 0.0 | 2 | 45.00 | 405.00 | 10.00 | 90.00 | 0.00 | 10.00 | 90.00 |
| ns1 | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| D25 | 0.0 | 2 | 91.00 | 364.00 | 20.00 | 80.00 | 0.00 | --- | --- |
| D25 | 0.0 | 3 | 5.50 | 104.50 | 5.00 | 95.00 | 0.00 | --- | --- |
| D25 | 0.0 | 2 | 56.00 | 84.00 | 40.00 | 60.00 | 0.00 | 21.63 | 78.37 |
| D26 | 0.0 | 5 | 105.00 | 245.00 | 30.00 | 70.00 | 0.00 | 30.00 | 70.00 |

Table 1-31. Data for samples from core hole 36, Peabody Natural Gas, LLC, PNG 24-1.-Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; ns, no sample available; SubA, subbituminous A; ---, no data]

| Canister number | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D23 | --- | --- | --- | --- | --- | --- | Top 8 inches is carbonaceous shale. |
| D23 | 0.00 | 15 | 66.67 | 66.67 | 2.16 | --- | --- |
| D24 | 0.00 | 15 | 66.67 | 66.67 | 6.16 | --- | Pyrite sampled at 110 mm . |
| ns1 | --- | --- | --- | --- | --- | --- | No sample. |
| D25 | --- | 35 | 28.57 | --- | --- | --- | --- |
| D25 | --- | 60 | 16.67 | --- | --- | --- | --- |
| D25 | 0.00 | 35 | 28.57 | 26.71 | 2.44 | --- | --- |
| D26 | 0.00 | 30 | 33.33 | 33.33 | 5.08 | SubA | Pyrite sampled at 45 mm . |

Table 1-32. Data for samples from core hole 37, Peabody Natural Gas, LLC, PNG 26-1.
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm, centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubA, subbituminous A; ---, no data]

| Canister number | Approx dept | ximate <br> (ft) | Coal bed name | Unit thickness (UT) (cm) | Canister total measured thickness (CaToMT) (cm) | Unit proportion of canister thickness (UPrCaT) | Core cumulative measured thickness (CoCuMT) (ft) | Average vitrain band thickness (AvVBT) (mm) | Average attrital band thickness (AvABT) (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Top | Bottom |  |  |  |  |  |  |  |
| D28 | 1,156.00 | 1,158.00 | Pawnee | 52.00 | 52.00 | 1.00 | 1.71 | 3.0 | 27.0 |
| D27 | 1,158.00 | 1,160.00 | Pawnee | 55.00 | 55.00 | 1.00 | 3.51 | 3.0 | 17.0 |
| D29 | 1,160.00 | --- | Pawnee | 38.00 | --- | 0.70 | 4.76 | 3.0 | 12.0 |
| D29 | --- | 1,162.00 | Pawnee | 16.00 | 54.00 | 0.30 | 5.28 | 6.0 | 6.0 |
| D30 | 1,166.00 | 1,170.00 | Pawnee | 54.00 | 54.00 | 1.00 | 7.05 | 15.0 | 15.0 |
| D33 | 1,170.00 | --- | Pawnee | 8.00 | --- | 0.16 | 7.32 | 2.0 | 18.0 |
| D33 | --- | --- | Pawnee | 25.50 | --- | 0.53 | 8.15 | 155.0 | 0.0 |
| D33 | --- | 1,172.00 | Pawnee | 15.00 | 48.50 | 0.31 | 8.65 | 15.0 | 15.0 |
| D32 | 1,172.00 | --- | Pawnee | 11.00 | --- | 0.20 | 9.01 | 15.0 | 15.0 |
| D32 | --- | 1,174.00 | Pawnee | 45.00 | 56.00 | 0.80 | 10.48 | 2.0 | 18.0 |
| D31 | 1,174.00 | --- | Pawnee | 15.00 | --- | 0.27 | 10.97 | 15.0 | 15.0 |
| D31 | --- | --- | Pawnee | 11.00 | --- | 0.20 | 11.34 | 110.0 | 0.0 |
| D31 | --- | 1,176.00 | Pawnee | 29.00 | 55.00 | 0.53 | 12.29 | 5.0 | 11.7 |

Table 1-32. Data for samples from core hole 37, Peabody Natural Gas, LLC, PNG 26-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft, feet; cm, centimeters; mm, millimeters; m, meter; SCF, standard cubic feet; SubA, subbituminous A; ---, no data]

| Canister number | Cumulative fusain thickness (CuFT) (mm) | Lithotype code | Cumulative <br> vitrain thickness (CuVT) (mm) | Cumulative <br> attritus <br> thickness <br> (CuAT) (mm) | Vitrain percentage (VP) | Attritus percentage (AP) | Fusain percentage (FP) | Canister average vitrain percentage (CaAvVP) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D28 | 0.0 | 2 | 52.00 | 468.00 | 10.00 | 90.00 | 0.00 | 10.00 |
| D27 | 0.0 | 2 | 82.50 | 467.50 | 15.00 | 85.00 | 0.00 | 15.00 |
| D29 | 0.0 | 2 | 76.00 | 304.00 | 20.00 | 80.00 | 0.00 | --- |
| D29 | 0.0 | 3 | 80.00 | 80.00 | 50.00 | 50.00 | 0.00 | 28.89 |
| D30 | 0.0 | 3 | 270.00 | 270.00 | 50.00 | 50.00 | 0.00 | 50.00 |
| D33 | 0.0 | 2 | 8.00 | 72.00 | 10.00 | 90.00 | 0.00 | --- |
| D33 | 0.0 | 5 | 255.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| D33 | 0.0 | 3 | 75.00 | 75.00 | 50.00 | 50.00 | 0.00 | 69.69 |
| D32 | 5.0 | 3 | 52.50 | 52.50 | 47.73 | 47.73 | 4.55 | --- |
| D32 | 0.0 | 2 | 45.00 | 405.00 | 10.00 | 90.00 | 0.00 | 17.41 |
| D31 | 0.0 | 3 | 75.00 | 75.00 | 50.00 | 50.00 | 0.00 | --- |
| D31 | 0.0 | 5 | 110.00 | 0.00 | 100.00 | 0.00 | 0.00 | --- |
| D31 | 0.0 | 3 | 87.00 | 203.00 | 30.00 | 70.00 | 0.00 | 49.45 |

Table 1-32. Data for samples from core hole 37, Peabody Natural Gas, LLC, PNG 26-1.—Continued
[See figure 1 and table 1 in text for locations and other details. Abbreviations are as follows: ft , feet; cm , centimeters; mm, millimeters; m , meter; SCF, standard cubic feet; SubA, subbituminous A; ---, no data]

| Canister number | Canister average attrital percentage (CaAvAP) | Canister average fusain percentage (CaAvFP) | Cleat spacing (CS) (mm) | Cleat frequency (CFr) (cleats/m) | Canister average cleat frequency (CaAvCFr) (cleats/m) | Total gas (SCF/ton) | Apparent rank | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D28 | 90.00 | 0.00 | 30 | 33.33 | 33.33 | 2.58 | --- | --- |
| D27 | 85.00 | 0.00 | 30 | 33.33 | 33.33 | 1.67 | --- | --- |
| D29 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| D29 | 71.11 | 0.00 | 30 | 33.33 | 38.02 | 1.91 | --- | --- |
| D30 | 50.00 | 0.00 | 20 | 50.00 | 50.00 | 1.79 | --- | --- |
| D33 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| D33 | --- | --- | 25 | 40.00 | - | - | --- | --- |
| D33 | 30.31 | 0.00 | 25 | 40.00 | 40.00 | 1.99 | --- | --- |
| D32 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| D32 | 81.70 | 0.89 | 60 | 16.67 | 21.25 | 2.41 | SubA | --- |
| D31 | --- | --- | 25 | 40.00 | --- | --- | --- | --- |
| D31 | --- | --- | 30 | 33.33 | --- | --- | --- | --- |
| D31 | 50.55 | 0.00 | 30 | 33.33 | 35.15 | 1.67 | --- | --- |

# Appendix 2. Graphs of Total Gas With Average Attrital Band Thickness, Cleat Frequency, Cumulative Fusain Thickness, Lithotype Code, and Average Vitrain Band Thickness, Against Core Cumulative Measured Thickness for All Cores 

Graphs for all cores in this report showing total gas with average attrital band thickness, cleat frequency, cumulative fusain thickness, coal lithotype code (see figure 6 of report),
and average vitrain band thickness plotted against core cumulative measured thickness.


Figure 2-1. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 1, MichiWest Energy, Inc., Pilot State 16-14 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-1.


Figure 2-2. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 2, MichiWest Energy, Inc., Pilot State 16-32 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-2.


Figure 2-3. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 3, Ocean Energy, Inc., Schlautmann 9-10-45-74WY (Ocean 43-10C) (Anderson coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-3.


Figure 2-4. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 8, CMS Oil and Gas Company, Laramore 11-6C (Smith coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-4.


Figure 2-5. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 8, CMS Oil and Gas Company, Laramore 11-6C (Anderson coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-4.


Figure 2-6. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 8, CMS Oil and Gas Company, Laramore 11-6C (Canyon coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-4.


Figure 2-7. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 8, CMS Oil and Gas Company, Laramore 11-6C (Cook coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-4.


Figure 2-8. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 9, Kennecott Energy, Kennecott CBM-1 (upper, and middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-5.


Figure 2-9. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 10, Kennecott Energy, Kennecott CBM-2 (upper, and middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-6.


Figure 2-10. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 11, Barrett Resources Corporation, CARU State 22-16-5075W (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-7.


Figure 2-11. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 11, Barrett Resources Corporation, CARU State 22-16-5075W (Werner coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-7.


Figure 2-12. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 12, Barrett Resources Corporation, Schoonover Road Unit (SRU) State 12-16-4576 (Big George coal bed).Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-8.


Figure 2-13. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency ( CFr ), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 13, Rim Operating Inc., CBM H-11-04 (upper and middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-9.


Figure 2-14. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 14, Rim Operating Inc., CBM C-33-1R (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-10.


Figure 2-15. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 15, Peabody Natural Gas LLC, PNG 34-1 (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-11.


Figure 2-16. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 16, Peabody Natural Gas LLC, PNG 33-1 (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-12.


Figure 2-17. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 17, Peabody Natural Gas LLC, PNG 31-1 (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-13.


Figure 2-18. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 18, Peabody Natural Gas LLC, PNG 35-1 (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-14.


Figure 2-19. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 19, Barrett Resources Corporation, All Night Creek Unit (ANCU) Iberlin 21-33-4374 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-15.


Figure 2-20. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 20, Peabody Natural Gas LLC, PNG 16-2 (middle and lower Wyodak coal beds). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-16.


Figure 2-21. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 21, The Coteau Properties Co., Coteau MC00250C (Beulah coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-17.


Figure 2-22. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 21, The Coteau Properties Co., Coteau MC00250C (unnamed 2 coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-17.


Figure 2-23. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 21, The Coteau Properties Co., Coteau MC00250C (unnamed 3 coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-17.


Figure 2-24. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 22, The Coteau Properties Co., Coteau MC00251 (unnamed 4 coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-18.


Figure 2-25. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 23, Ammonite Energy Texas, Inc., Thomas Jefferson State 36-3 (School coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-19.


Figure 2-26. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 24, Bridger Coal Company, BCX-9 (Deadman coal zone). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-20.


Figure 2-27. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 25, Peabody Natural Gas LLC, Duvall 13J-D (Pawnee coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-21.


Figure 2-28. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 26, Barrett Resources Corporation, KU Harriett 41-34-4777 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-22.


Figure 2-29. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 27, Peabody Natural Gas LLC, Carter-Federal 18F-D (Pawnee coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-23.


Figure 2-30. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 27, Peabody Natural Gas LLC, Carter-Federal 18F-D (Cache coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-23.


Figure 2-31. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 28, Nance Petroleum Corporation, Remington 58-79-30-07A (Anderson coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-24.


Figure 2-32. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 30, Nance Petroleum Corporation, Remington 58-79-30-01C (Canyon coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-25.


Figure 2-33. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency ( CFF ), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 31, Williams Production RMT Company, Bullwacker Creek Unit (BCU) 32-9-4277 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1 , table 1-26.


Figure 2-34. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 32, Lance Oil and Gas Company, Whiskey Draw Unit 12-12-4778 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-27.


Figure 2-35. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 33, Lance Oil and Gas Company, Inc., McBeth 12-30-4673-BG (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-28.


Figure 2-36. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 34, Williams Production RMT Company, State 23-16-4171 (Anderson coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-29.


Figure 2-37. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 34, Williams Production RMT Company, State 23-16-4171 (Canyon coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-29.


Figure 2-38. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 35, Williams Production Company, Groves 12-19-4574 (Big George coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-30.


Figure 2-39. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 36, Peabody Natural Gas LLC, PNG 24-1 (Pawnee coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-31.


Figure 2-40. Graphs of total gas (standard cubic feet per ton, SCF/ton), average attrital band thickness (AvABT), cleat frequency (CFr), cumulative fusain thickness (CuFT), lithotype code, and average vitrain band thickness (AvVBT) plotted against core cumulative measured thickness (CoCuMT) for core hole 37, Peabody Natural Gas, LLC, PNG 26-1 (Pawnee coal bed). Total gas points are labeled with canister numbers. See figure 6 for lithotype codes. All variables are listed in appendix 1, table 1-32.

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## Appendix 3. Graphs of Total Gas Against Canister Average Vitrain Percentage, Canister Average Attrital Percentage, Canister Average Cleat Frequency for Data From All Cores

Graphs for all cores showing total gas (SCF/ton) plotted against canister average vitrain percentage ( CaAvVP ), canister
average attrital percentage (CaAvAP), and canister average cleat frequency ( CaAvCFr ).


Figure 3-1. Graphs showing canister average vitrain percentage (CaAvVP) plotted against total gas (in standard cubic feet per ton, SCF/ton), grouped by lithologic description method, and color coded by core hole number (see table 1 in text for well name). A, Core holes 1 through 3, 8,10 through 16, 23 , and 24 (method A). B, Core holes 19 through 22 (method B). C, Core holes 9 and 34 through 37 (method C). D, Core holes 17 and 18 (method D), 25 through 28, and 30 through 33 (method E). Trend line for points in core hole 32 (part D) has an R-squared value of 0.179 .

Big George coal bed samples


Smith, School, Anderson, Canyon, Werner, Cook, Pawnee, and Cache coal bed samples

upper Wyodak and middle and lower Wyodak coal bed samples


Beulah, unnamed 2, 3, and 4 coal bed, and Deadman coal zone samples


Figure 3-2. Graphs showing canister average vitrain percentage (CaAvVP) plotted against total gas(in standard cubic feet per ton, SCF/ton) for all core holes, color coded by coal bed. A, Big George coal bed. B, Smith, School, Anderson, Canyon, Werner, Cook, Pawnee, and Cache coal beds. C, upper Wyodak and middle and lower Wyodak coal beds. D, Beulah, unnamed 2, unnamed 3, and unnamed 4 coal beds, and Deadman coal zone.


Core holes 19 through $22($ method $B)$



Core holes 17 and $18(\operatorname{method} \mathrm{D}), 25$ through 28 , and 30 through $33(\operatorname{method} E)$


Figure 3-3. Graphs showing canister average attrital percentage (CaAvAP) plotted against total gas (in standard cubic feet per ton, SCF/ton), grouped by lithologic description method, and color coded by core hole number (see table 1 in text for well name). A, Core holes 1 through 3, 8, 10 through 16, 23, and 24 (method A). B, Core holes 19 through 22 (method B). C, Core holes 9 and 34 through 37 (method C). D, Core holes 17 and $18(\operatorname{method} D), 25$ through 28 , and 30 through 33 (method E). Trend line for points from core $32($ part D) has an $R$-squared value of 0.1775 with a negative slope.


Figure 3-4. Graphs showing canister average attrital percentage (CaAvAP) plotted against total gas (in standard cubic feet per ton, SCF/ton) for all core holes, color coded by coal bed. A, Big George coal bed. B, Smith, School, Anderson, Canyon, Werner, Cook, Pawnee, and Cache coal beds. C, upper Wyodak and middle and lower Wyodak coal beds. D, Beulah, unnamed 2, unnamed 3, and unnamed 4 coal beds, and Deadman coal zone.


Core holes 19 through 22 (method B)



Core holes 17 and 18 (method D), 25 through 28 , and 30 through 33 (method E)


Figure 3-5. Graphs showing canister average cleat frequency (CaAvCFr) (in cleats per meter, cleats/m) plotted against total gas (in standard cubic feet per ton, SCF/ton), grouped by lithologic description method, and color coded by core hole number (see table 1 in text for well name). A, Core holes 1 through $3,8,10$ through 16,23 , and 24 (method A). B, Core holes 19 through 22 (method B). C, Core holes 9 and 34 through 37 (method C). D, Core holes 17 and 18 (method D), 25 through 28 , and 30 through 33 (method E).

Big George coal bed samples
upper Wyodak and middle and lower Wyodak coal bed samples


Smith, School, Anderson, Canyon, Werner, Cook, Pawnee, and Cache coal bed samples



Canister average cleat frequency (CaAvCFr), in cleat/m
Beulah, unnamed 2, 3, and 4 coal bed, and Deadman coal zone samples


Figure 3-6. Graphs showing canister average cleat frequency (CaAvCFr) (in cleats per meter, cleats/m) plotted against total gas (in standard cubic feet per ton, SCF/ton) for all core holes, color coded by coal bed. A, Big George coal bed. B, Smith, School, Anderson, Canyon, Werner, Cook, Pawnee, and Cache coal beds. C, upper Wyodak and middle and lower Wyodak coal beds. D, Beulah, unnamed 2, unnamed 3, and unnamed 4 coal beds, and Deadman coal zone.


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[^1]:    ${ }^{1}$ U.S. Geological Survey, Reston, Va.
    ${ }^{2}$ U.S. Geological Survey, Denver, Colo.
    ${ }^{3}$ U.S. Geological Survey, Reston, Va. (deceased).
    ${ }^{4}$ Arrow Energy, Brisbane, Queensland, Australia.

