

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

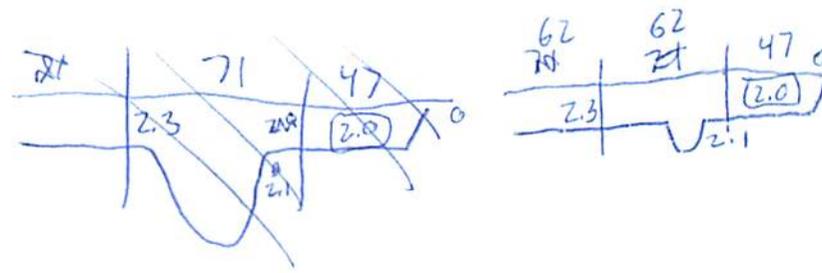
Bridge Structure No. 02040063 Date 6/12/12 Initials RAT Region (A B C D) D  
 Site \_\_\_\_\_ Location 7.7 miles North of White Lake on 374 Ave - Aurora Co.  
 $Q_{100} =$  1320 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1320 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 62 ft. Flow angle at bridge = 35.0° Abut. Skew = 30° Effective Skew = 10°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 61.00 ft\*  $q_2 = Q_2/W_2 =$  21.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.3 ft/s Final  $y_2 = q_2/V_2 =$  6.6 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.8 ft  
 \* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

See last page

Water Surface Elev. = 2.7 ft  
 Low Steel Elev. = 6.6 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.2 ft  
 Pier Length = 1.2 ft  
 # Piers for 100 yr = 3



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  62 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  62 ft Average left overbank flow depth,  $y_{lob} =$  2.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  47 ft Average right overbank flow depth,  $y_{rob} =$  2.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.86 From Figure 9  $W_2$  (effective) = 57.5 ft  $y_{cs} =$  3.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} V_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.23 Using pier width  $a$  on Figure 11,  $\xi =$  5.5 Pier scour  $y_{ps} =$  4.4 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.3 ft right abutment,  $y_{aRT} =$  2.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  9.4 and  $\psi_{RT} =$  8.2  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  14 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  12.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

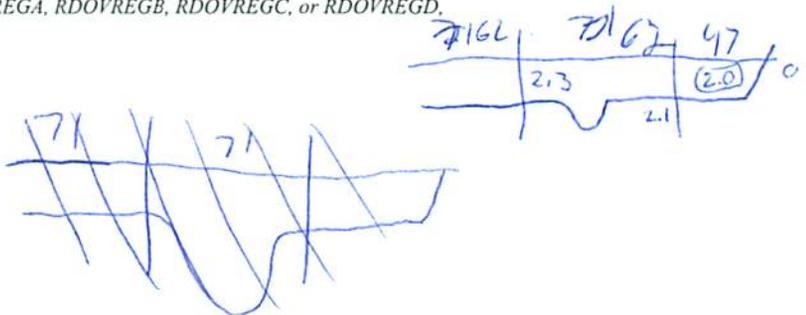
Bridge Structure No. 02040063 Date 6/12/17 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location 7.7 mi N of White Lake on 374 Ave  
 $Q_{500} =$  2520 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1334 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = 40 ° Abut. Skew = 30 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 61.06 ft\*  $q_2 = Q_2/W_2 =$  21.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.3 ft/s Final  $y_2 = q_2/V_2 =$  6.6 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.7 ft  
 Low Steel Elev. = 6.6 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.030  
 Pier Width = 1.2 ft  
 Pier Length = 1.2 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  62 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  62 ft Average left overbank flow depth,  $y_{lob} =$  2.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  47 ft Average right overbank flow depth,  $y_{rob} =$  2.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.60 From Figure 9  $W_2$  (effective) = ~~58.7~~ 57.5 ft  $y_{cs} =$  ~~3.7~~ 3.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.23 Using pier width  $a$  on Figure 11,  $\xi =$  5.5 Pier scour  $y_{ps} =$  4.4 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.3 ft right abutment,  $y_{aRT} =$  2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  9.4 and  $\psi_{RT} =$  8.2  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  14 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  12.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

ps 58  
lott mid

98.71425  
43.8448

430 50' 41.28"  
99° 42' 51.3"  
"

Route 374 Ave Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/12/12 Initials Lat  
 Bridge Structure No. 02040063 Location 7.7 mi N of White Lake on 374 Ave - Aurora Co.  
 GPS coordinates: N 43° 50' 40.6" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 98° 42' 51.1" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 14.25 sq. mi.  
 The average bottom of the main channel was 10.5 ft below top of guardrail at a point 5 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

|                                       |                                |                                     |                                     |                                     |                                     |          |
|---------------------------------------|--------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|----------|
| Flows                                 | Q <sub>100</sub> = <u>1320</u> | Q <sub>500</sub> = <u>2520</u>      |                                     |                                     |                                     |          |
| Estimated flow passing through bridge | <u>1320</u>                    | <u>1334</u>                         |                                     |                                     |                                     |          |
| Estimated road overflow & overtopping | <u>0</u>                       | <u>1186</u>                         |                                     |                                     |                                     |          |
| Consideration                         | Yes                            | No                                  | Possibly                            | Yes                                 | No                                  | Possibly |
| Chance of overtopping                 |                                | <input checked="" type="checkbox"/> |                                     | <input checked="" type="checkbox"/> |                                     |          |
| Chance of Pressure flow               |                                |                                     | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> |                                     |          |
| Armored appearance to channel         |                                | <input checked="" type="checkbox"/> |                                     |                                     | <input checked="" type="checkbox"/> |          |
| Lateral instability of channel        |                                | <input checked="" type="checkbox"/> |                                     |                                     | <input checked="" type="checkbox"/> |          |

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes \_\_\_ No  Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA *bridge layout*

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250

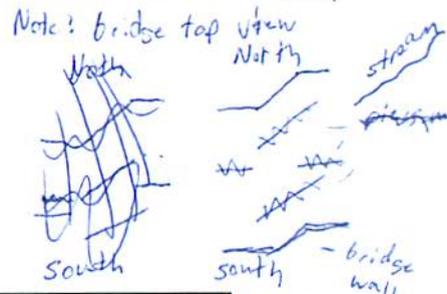
Boulders \_\_\_ >250  
*note: stream stat's shows two adjacent stream cells crossing the road*

**Comments, Diagrams & orientation of digital photos**

- 2 | 51.1
- 5 | 181
- 10 | 338
- 25 | 639
- 50 | 943
- 100 | 1326
- 500 | 2520

- 1). left ab
- 2). main channel
- 3). right ab
- 4-6). pier
- 7-10). right abutment
- 11-14). left abutment

- 15). Road Crack
- 16). main channel



**Summary of Results**

|  | Q100        | Q500           |
|--|-------------|----------------|
| Bridge flow evaluated                        | <u>1320</u> | <u>1334</u>    |
| Flow depth at left abutment (yaLT), in feet  | <u>2.3</u>  | <u>2.3</u>     |
| Flow depth at right abutment (yaRT), in feet | <u>2.0</u>  | <u>0</u>       |
| Contraction scour depth (yca), in feet       | <u>3.5</u>  | <u>3.5</u>     |
| Pier scour depth (yps), in feet              | <u>4.1</u>  | <u>4.1</u>     |
| Left abutment scour depth (yas), in feet     | <u>14</u>   | <u>12.3 14</u> |
| Right abutment scour depth (yas), in feet    | <u>12.3</u> | <u>14 12.3</u> |
| Flow angle of attack                         | <u>10</u>   | <u>10</u>      |

*There are road cracks following outlining the change from concrete to wood pier/abutment sections deep enough to see through to the water. Angled sections are concrete. Straight sections are wood.*

See Comments/Diagram for justification where required

*Pier width/length. Channel too muddy/deep to set an accurate measurement. Had to estimate.*

*6/12/12  
 PK 2 52  
 5 184  
 10 345  
 25 639  
 50 943  
 100 1350  
 500 2580*

*5/30 5/30  
 2 4.9 2 51.1  
 5 31.5 5 181  
 10 52.2 10 338  
 25 63.7 25 639  
 50 94.3 50 943  
 100 119 100 1320  
 500 156 500 2520  
 0.45 13.75*