

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 02B6050 Date 6/12/12 Initials Rat Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.5 mi East of HWY 281 on 243<sup>rd</sup> St - Aurora Co.  
 $Q_{100} = Q_{92.5} = 662$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 662 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 34 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 33.48 ft\*  $q_2 = Q_2/W_2 = 20.4$  ft<sup>2</sup>/s

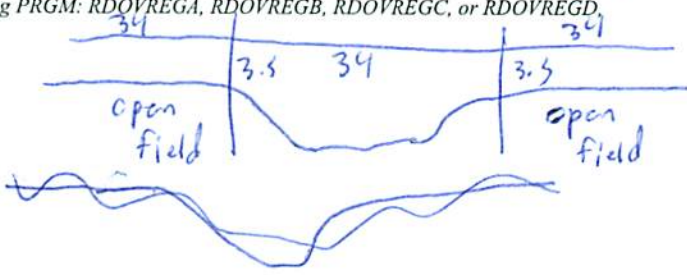
Bridge Vel,  $V_2 = 3.2$  ft/s Final  $y_2 = q_2/V_2 = 6.4$  ft  $\Delta h = 0.2$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 6.6$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.16 ft  
 Low Steel Elev. = 7.0 ft  
 $n$  (Channel) = 0.055 0.050  
 $n$  (LOB) = 0.042 0.030  
 $n$  (ROB) = 0.025 0.030  
 Pier Width = 1.05 ft  
 Pier Length = 1.05 ft  
 # Piers for 100 yr = 2



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 34$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 34$  ft Average left overbank flow depth,  $y_{lob} = 3.5$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 34$  ft Average right overbank flow depth,  $y_{rob} = 3.5$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 8.85$  From Figure 9  $W_2$  (effective) = 31.9 ft  $y_{cs} = 9.7$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.22 Using pier width  $a$  on Figure 11,  $\xi = 5$  Pier scour  $y_{ps} = 4$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.5$  ft right abutment,  $y_{aRT} = 3.5$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 12.4$  and  $\psi_{RT} = 12.4$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 18.5$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 18.5$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

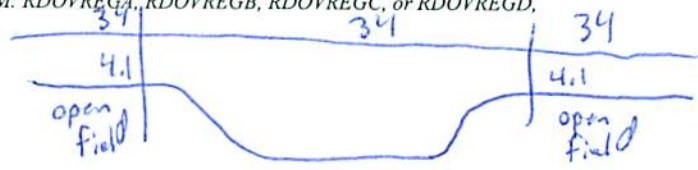
Bridge Structure No. 02186050 Date 6/12/12 Initials Rat Region (A B C D) C  
 Site \_\_\_\_\_ Location 0.5 E of HWY 281 on 243rd St  
 $Q_{500} =$   $Q_{50}$  1010 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 823 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 34 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 33.46 ft\*  $q_2 = Q_2/W_2 =$  24.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.5 ft/s Final  $y_2 = q_2/V_2 =$  7 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.



Water Surface Elev. = 2.6 ft  
 Low Steel Elev. = 7.0 ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 1.05 ft  
 Pier Length = 1.05 ft  
 # Piers for 500 yr = 2 ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  34 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  34 ft Average left overbank flow depth,  $y_{lob} =$  4.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  34 ft Average right overbank flow depth,  $y_{rob} =$  4.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  10.77 From Figure 9  $W_2$  (effective) = 31.4 ft  $y_{cs} =$  11.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.23 Using pier width  $a$  on Figure 11,  $\xi =$  5 Pier scour  $y_{ps} =$  4 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.1 ft right abutment,  $y_{aRT} =$  4.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.4 and  $\psi_{RT} =$  13.4  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  20 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  20 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment



Route 243<sup>rd</sup> St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/12/12 Initials RAT  
 Bridge Structure No. 02186050 Location 0.5 East of Hwy 281 on 243<sup>rd</sup> St  
 GPS coordinates: N 43° 51' 51.71" taken from: USL abutment  centerline of ft MRM end \_\_\_\_\_  
W 98° 26' 28.254" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 14.97 sq. mi.  
 The average bottom of the main channel was 10.6 ft below top of guardrail at a point 23 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

8/22

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> <sup>25</sup> = <u>681</u>			Q <sub>500</sub> <sup>50</sup> = <u>1010</u>		
Estimated flow passing through bridge	<u>681</u>			<u>823</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>167</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

PK2 54.2  
 5 192  
 10 360  
 25 681  
 50 1010  
 100 1410  
 500 2710

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med \_\_\_ Low

- road damage. No external abutment wall! minor abutment scour under bridge & contraction scour

5/44  
 2 54.2  
 5 192  
 10 360  
 25 682  
 50 1010  
 100 1410  
 500 2710

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4-5) left abutment  
Road damage  
(up & downstream)

- 6). right abutment
- 7). left abutment
- 8-9) piers
- 10). left abutment
- 11). right abutment
- 12). main channel

Note: No external abutment all.

Summary of Results

	Q <sub>100</sub> <sup>25</sup>	Q <sub>500</sub> <sup>50</sup>
Bridge flow evaluated	<del>681</del> <u>682</u>	<u>823</u>
Flow depth at left abutment (yaLT), in feet	<u>3.5</u>	<u>4.1</u>
Flow depth at right abutment (yaRT), in feet	<u>3.5</u>	<u>4.1</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>9.7</u>	<u>11.9</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>4</u>	<u>4</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>18.5</u>	<u>20</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>18.5</u>	<u>20</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required