

DUP ok-Kal

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 02186050 Date 9-27-12 Initials RFT Region (A B C D) (D)  
 Site \_\_\_\_\_ Location 0.5 mi E of Hwy 281 on 243<sup>rd</sup> St  
 $Q_{100}^{2.5} =$  682 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 682 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 36 ft. Flow angle at bridge = 8 ° Abut. Skew = 0 ° Effective Skew = 8 °

Width ( $W_2$ ) iteration = 36

Avg. flow depth at bridge,  $y_2$  iteration = 6.2

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 35.65 ft\*  $q_2 = Q_2/W_2 =$  19.1 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.1 ft/s Final  $y_2 = q_2/V_2 =$  6.2 ft  $\Delta h =$  0.2 ft

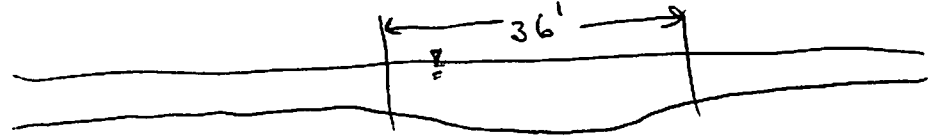
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

this site does not have a well-defined channel

Water Surface Elev. = dry ft  
 Low Steel Elev. = 6.8 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .028  
 $n$  (ROB) = .028  
 Pier Width = 1.0 ft  
 Pier Length = 1.0 ft  
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  36 ft

Width of left overbank flow at approach,  $W_{lob} =$  36 ft Average left overbank flow depth,  $y_{lob} =$  4.3 ft

Width of right overbank flow at approach,  $W_{rob} =$  36 ft Average right overbank flow depth,  $y_{rob} =$  4.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  9.27 From Figure 9  $W_2$  (effective) = 33.7 ft  $y_{cs} =$  10.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.22

Using pier width  $a$  on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  3.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.3 ft right abutment,  $y_{aRT} =$  4.3 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.8 and  $\psi_{RT} =$  13.8

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  20.5 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  20.5 ft

This bridge appears to have ~~spill-through~~ spill-through abutments that are very eroded. Although wing walls are not present, use  $K_1 = 0.82$  to reflect eroded abutments under bridge.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 02186050 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) D

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500}^{50} =$  1010 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 1010 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 36 ft. Flow angle at bridge = ~~8~~ 0° Abut. Skew = 0° Effective Skew = 8°

Width ( $W_2$ ) iteration = 36

Avg. flow depth at bridge,  $y_2$  iteration = 7.5

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 35.65 ft\*  $q_2 = Q_2/W_2 =$  28.3 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.8 ft/s Final  $y_2 = q_2/V_2 =$  7.5 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

*This bridge is probably at the verge of road overflow at  $Q_{50}$  (1010 cfs)*

Water Surface Elev. = dry ft

Low Steel Elev. = 6.8 ft

n (Channel) = .035

n (LOB) = .028

n (ROB) = .028

Pier Width = 1.0 ft

Pier Length = 1.0 ft

# Piers for 500 yr = 2 ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  36 ft

Width of left overbank flow at approach,  $W_{lob} =$  36 ft

Average left overbank flow depth,  $y_{lob} =$  5.8 ft

Width of right overbank flow at approach,  $W_{rob} =$  36 ft

Average right overbank flow depth,  $y_{rob} =$  5.8 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  13.28 From Figure 9

$W_2$  (effective) = 33.7 ft  $y_{cs} =$  14.1 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft

If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.24

Using pier width a on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  3.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.8 ft right abutment,  $y_{aRT} =$  5.8 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  16.5 and  $\psi_{RT} =$  16.5

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  24.5 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  24.5 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pic

PRGM: Abutment

Route 243<sup>rd</sup> St Stream Donegan's Draw MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 021816050 Location 0.5 E Hwy 281 on 243<sup>rd</sup> St  
 GPS coordinates: N 43° 51.869' taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 98° 26.409' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 14.97 sq. mi.  
 The average bottom of the main channel was 10.5 ft below top of guardrail at a point 9 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>25</sub> = <u>682</u>			Q <sub>50</sub> = <u>1010</u>		
Estimated flow passing through bridge	<u>682</u>			<u>1010</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low  
*Some field stone has been dumped in the up- and downstream ditch (channel) but no real riprap*  
*contraction and abutment scour evident*

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 Str. no. left abut. under bridge  
 approach from bridge rt. abut. under bridge  
 LOB from bridge field stone on upstream side of bridge  
 ROB from bridge  
 Bridge from upstream

Summary of Results

	Q <sub>100</sub> <u>25</u>	Q <sub>500</sub> <u>50</u>
Bridge flow evaluated	<u>682</u>	<u>1010</u>
Flow depth at left abutment (yaLT), in feet	<u>4.3</u>	<u>5.8</u>
Flow depth at right abutment (yaRT), in feet	<u>4.3</u>	<u>5.8</u>
Contraction scour depth (y <sub>c</sub> s), in feet	<u>10.2</u>	<u>14.1</u>
Pier scour depth (y <sub>p</sub> s), in feet	<u>3.9</u>	<u>3.9</u>
Left abutment scour depth (y <sub>a</sub> s), in feet	<u>20.5</u>	<u>24.5</u>
Right abutment scour depth (y <sub>a</sub> s), in feet	<u>20.5</u>	<u>24.5</u>
Flow angle of attack	<u>8°</u>	<u>8°</u>

See Comments/Diagram for justification where required