

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 03110132 Date 7/24/12 Initials RT Region (A B C D) D  
 Site \_\_\_\_\_ Location 1.8 mi N of Wolsey - Beadle Co. on 387 Ave  
 $Q_{100} = Q_{10}$  1560 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1560 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 89 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 71.09 ft\*  $q_2 = Q_2/W_2 = \underline{20.2}$  ft<sup>2</sup>/s

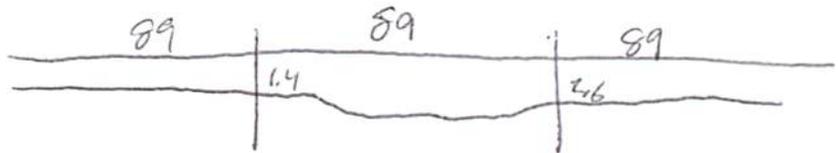
Bridge Vel,  $V_2 = \underline{3.2}$  ft/s Final  $y_2 = q_2/V_2 = \underline{6.4}$  ft  $\Delta h = \underline{0.2}$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{6.6}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{89}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{89}$  ft Average left overbank flow depth,  $y_{lob} = \underline{1.4}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{89}$  ft Average right overbank flow depth,  $y_{rob} = \underline{2.6}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{5.12}$  From Figure 9  $W_2$  (effective) = 71.7 ft  $y_{cs} = \underline{5.9}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = \underline{\quad}$  ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) = \underline{\quad}$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = \underline{\quad}$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$  From Figure 10,  $y_{cs} = \underline{\quad}$  ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.22 Using pier width a on Figure 11,  $\xi = \underline{6}$  Pier scour  $y_{ps} = \underline{4.4}$  ft  
4.8

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{1.4}$  ft right abutment,  $y_{aRT} = \underline{2.6}$  ft  
 Shape coefficient  $K_1 = \underline{1.00}$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{5.9}$  and  $\psi_{RT} = \underline{10.6}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{10.6}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{19.3}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

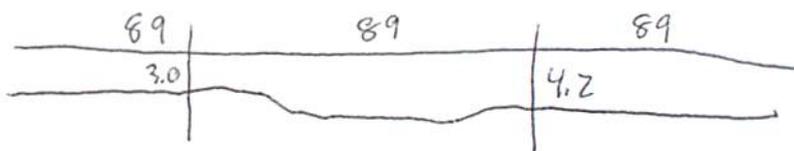
Bridge Structure No. 03110132 Date 7/24/12 Initials ROT Region (A B C D)  
 Site \_\_\_\_\_ Location 1.8 mi. N of Wolsey on 387 Ave  
 $Q_{500} = Q_{25}$  3290 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2415 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 89 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 77.06 ft\*  $q_2 = Q_2/W_2 =$  31.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4 ft/s Final  $y_2 = q_2/V_2 =$  7.9 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 7.9 ft  
 n (Channel) = 0.015  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  89 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  6.9 ft Average left overbank flow depth,  $y_{lob} =$  3.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  8.9 ft Average right overbank flow depth,  $y_{rob} =$  4.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  9.85 From Figure 9  $W_2$  (effective) = 71.7 ft  $y_{cs} =$  10.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.25 Using pier width a on Figure 11,  $\xi =$  6 Pier scour  $y_{ps} =$  4.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.0 ft right abutment,  $y_{aRT} =$  4.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.5 and  $\psi_{RT} =$  13.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  20.9 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  24.7 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 387 Ave Stream Can CK MRM \_\_\_\_\_ Date 7/24/12 Initials Ant  
 Bridge Structure No. 03110132 Location 1.8 mi N of Walsey on 387 Ave  
 GPS coordinates: N 44° 26' 25.8" W 98° 28' 43.6" taken from: USL abutment centerline of ↑ MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84 NAD27 \_\_\_\_\_

Drainage area = 234.77 sq. mi.  
 The average bottom of the main channel was 12.4 ft below top of guardrail at a point 58 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio X regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_p$ 1560			$Q_{500} = Q_{25}$ 3290		
Estimated flow passing through bridge	1560			2415		
Estimated road overflow & overtopping	0			875		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X		X		
Chance of Pressure flow		X		X		
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

Riprap at abutments? \_\_\_ Yes X No \_\_\_ Marginal  
 Evidence of past Scour? X Yes \_\_\_ No \_\_\_ Don't know *near pier/contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med X Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay X Sand X Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left ab  
 2) main channel  
 3) right ab  
 4) pier  
 5) pier scour  
 6-7) left abutment  
 8-9) right abutment  
 10) main channel

Summary of Results

	$Q_{100} Q_p$	$Q_{500} Q_{25}$
Bridge flow evaluated	1560	2415
Flow depth at left abutment (yaLT), in feet	1.4	3.0
Flow depth at right abutment (yaRT), in feet	2.6	4.2
Contraction scour depth (y <sub>cs</sub> ), in feet	5.8	10.8
Pier scour depth (y <sub>ps</sub> ), in feet	<del>4.9</del> 4.8	4.8
Left abutment scour depth (y <sub>as</sub> ), in feet	10.6	20.9
Right abutment scour depth (y <sub>as</sub> ), in feet	19.3	24.7
Flow angle of attack	30	30

See Comments/Diagram for justification where required

8/22

2	166
5	749
10	1560
25	3290
50	5170
100	7640
500	16100

5/14

2	164
5	740
10	1550
25	3280
50	5110
100	7550
500	15900