

OK RT

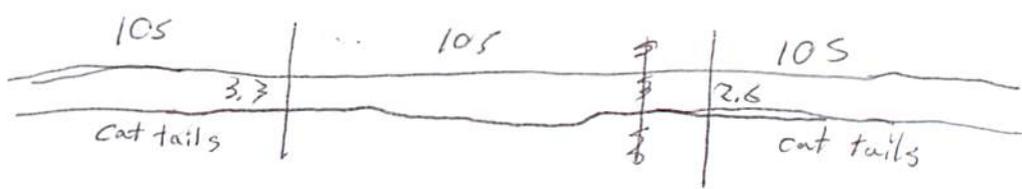
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 03155240 Date 7/24/12 Initials Root Region (A B C D) D  
 Site \_\_\_\_\_ Location 3.4 mi. E of Hwy 281 on 214 St  
 $Q_{100} = Q_2 = 923$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 923 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 105 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 90.93 ft\*  $q_2 = Q_2/W_2 = 10.2$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 2.3$  ft/s Final  $y_2 = q_2/V_2 = 4.5$  ft  $\Delta h = 0.1$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 4.6$  ft  
 \* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 5.9 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.040  
 n (ROB) = 0.040  
 Pier Width = 1.65 ft  
 Pier Length = 1.65 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 105$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 105$  ft Average left overbank flow depth,  $y_{lob} = 3.3$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 105$  ft Average right overbank flow depth,  $y_{rob} = 2.6$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 7.32$  From Figure 9  $W_2$  (effective) = 84.3 ft  $y_{cs} = 8.1$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.19 Using pier width a on Figure 11,  $\xi = 6.9$  Pier scour  $y_{ps} = 5.4$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.3$  ft right abutment,  $y_{aRT} = 2.6$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 12.0$  and  $\psi_{RT} = 10.6$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 21.9$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 19.3$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

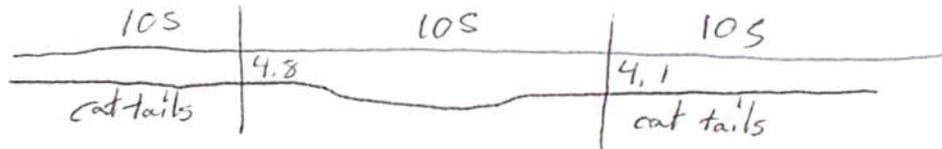
Bridge Structure No. 03155240 Date 7/24/12 Initials Rai Region (A B C D) D  
 Site \_\_\_\_\_ Location 3.4 mi E of Hwy 281 on 214 St.  
 $Q_{500} = \underline{610}$  1950 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1589 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 105 ft. Flow angle at bridge = 30° Abut. Skew = 0° Effective Skew = 30°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 90.93 ft\*  $q_2 = Q_2/W_2 = \underline{17.5}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{3}$  ft/s Final  $y_2 = q_2/V_2 = \underline{5.9}$  ft  $\Delta h = \underline{0.2}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{6.1}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 5.9 ft  
 n (Channel) = 0.015  
 n (LOB) = 0.040  
 n (ROB) = 0.040  
 Pier Width = 1.65 ft  
 Pier Length = 1.65 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{105}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{105}$  ft Average left overbank flow depth,  $y_{lob} = \underline{4.8}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{105}$  ft Average right overbank flow depth,  $y_{rob} = \underline{4.1}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{11.63}$  From Figure 9  $W_2$  (effective) = 84.3 ft  $y_{cs} = \underline{12.7}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = \underline{\quad}$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = \underline{\quad}$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \underline{\quad}$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$  From Figure 10,  $y_{cs} = \underline{\quad}$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.22 Using pier width a on Figure 11,  $\xi = \underline{6.9}$  Pier scour  $y_{ps} = \underline{5.5}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{4.8}$  ft right abutment,  $y_{aRT} = \underline{4.1}$  ft  
 Shape coefficient  $K_1 = \underline{1.00}$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{14.7}$  and  $\psi_{RT} = \underline{13.4}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{26.7}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{24.4}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

119582'11  
98.38972

440 17' 0.9996"  
960 23' 22.992"

Route 214 St. Stream Corn Creek MRM Date 7/24/12 Initials Lat  
 Bridge Structure No. 03155240 Location 3.4 mi. E of HWY 281 on 214 St  
 GPS coordinates: N 44° 17' 13" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 98° 23' 22.6" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 341 sq. mi.  
 The average bottom of the main channel was 9.7 ft below top of guardrail at a point 45 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

5/14  
 8/22  
 PK 2 | 200  
 5 | 922923  
 10 | 1950  
 25 | 4160  
 50 | 6590  
 100 | 9810  
 500 | 21000

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <del>Q<sub>100</sub></del> Q <sub>5</sub> <u>923</u>			Q <sub>500</sub> = Q <sub>10</sub> <u>1950</u>		
Estimated flow passing through bridge	<u>923</u>			<u>1584</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>362</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know minor pier/contraction/abutment  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab  
 2). main channel  
 3). right ab.  
 4-5). right abutment  
 6). pier  
 7). pier scour  
 8-9). left abutment  
 10). main channel

Summary of Results

	Q <sub>100</sub> Q <sub>5</sub>	Q <sub>500</sub> Q <sub>10</sub>
Bridge flow evaluated	<u>923</u>	<u>1950</u>
Flow depth at left abutment (yaLT), in feet	<u>3.3</u>	<u>4.8</u>
Flow depth at right abutment (yaRT), in feet	<u>2.6</u>	<u>4.1</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>8.1</u>	<u>12.7</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>5.4</u>	<u>5.5</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>21.9</u>	<u>26.7</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>19.3</u>	<u>24.4</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required