Initials RFT Region (ABCD) Bridge Structure No. 03248185 Date 9-27-12 Site 06476000 Location James @ 3rd Stin Huron Q₁₀₀ = 18300 by: drainage area ratio flood freq. anal. regional regression eq. (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping) Bridge discharge $(Q_2) =$ Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method Bridge Width = 230 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 ° PGRM: "RegionA", "RegionB", Width (W_2) iteration = Avg. flow depth at bridge, y₂ iteration = _____ Corrected channel width at bridge Section = W_2 times cos of flow angle = ft^* $q_2 = Q_2/W_2 = ft^2/s$ Bridge Vel, $V_2 = ____ft/s$ Final $y_2 = q_2/V_2 = ____ft$ $\Delta h = ____ft$ Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ ____ft * NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, The river is impounded at this bridge due to a nock dam near 13th Street. Even though today's Water Surface Elev. = ft Low Steel Elev. = _____ ft Slow for the 3rd Street dam is approx. 32 cts, n (Channel) = _____ the depth under the bridge ranges from 3-4ft deep across most of its width. n (LOB) =n (ROB) =Approach section would also be above 3rd St dem. Pier Width = Pier Length = ft # Piers for 100 yr = _____ ft is site not suited to level 1.5 analysis. Width of main channel at approach section $W_1 =$ ____ft PGRM: Contract Width of left overbank flow at approach, $W_{lob} =$ ____ft Average left overbank flow depth, $y_{lob} =$ ____ft Width of right overbank flow at approach, $W_{rob} =$ ____ft Average right overbank flow depth, $y_{rob} = ft$ Live Bed Contraction Scour (use if bed material is small cobbles or finer) x = From Figure 9 W_2 (effective) = ft Clear Water Contraction Scour (use if bed material is larger than small cobbles) GRM: CWCSNEW Estimated bed material $D_{50} =$ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ Critical approach velocity, $Vc = 11.52y_1^{1/6}D_{50}^{1/3} = _____ft/s$ If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = _____ft$ If $D_{50} >= D_{c50}$, $\chi = 0.0$ Otherwise, $\chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ From Figure 10, $y_{cs} = ft$ PGRM: Pier PIER SCOUR CALCULATIONS L/a ratio = ____ Correction factor for flow angle of attack (from Table 1), K2 = Using pier width a on Figure 11, $\xi =$ Pier scour $y_{ps} =$ ft Froude # at bridge = ABUTMENT SCOUR CALCULATIONS Average flow depth blocked by: left abutment, $y_{aLT} = ____ft$ right abutment, $y_{aRT} = ____ft$ Shape coefficient K₁= 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ and $\psi_{RT} =$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ _____ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ _____ft

SCOUR ANALYSIS AND REPORTING FORM

	SCOUR ANALYSIS AND REPORTING FORM								
	Bridge Structure No. 03248185 Date Init Site 66476000 Location James @ 3rd	tials	Region (ABCD)						
	Site 06476000 Location James @ 5	Stin	Huron						
	Q ₅₀₀ = 32700 by: drainage area ratio flood freq. anal. regional regression eq								
	Bridge discharge $(Q_2) = $ (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)								
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method								
	Duides Width - 6 Flourengle at bridge - 9 Ab								
	Width (W ₂) iteration =								
	Avg. flow depth at bridge, y ₂ iteration =								
	Corrected channel width at bridge Section = W_2 times cos of flow angle =			ft ² /s					
	Bridge Vel, $V_2 = \underline{\hspace{1cm}}$ ft/s Final $y_2 = q_2/V_2 = \underline{\hspace{1cm}}$ ft		ft						
nC",	Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$								
PGRM "Regio	* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$								
	If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,								
	Water Surface Elev. = ft								
	Low Steel Elev. = ft								
	n (Channel) =								
	n (LOB) =								
	n (ROB) = ft								
	Pier Length = ft								
	# Piers for $500 \text{ yr} = $ ft								
	GOVERN LOWER VALUE GOVERN								
PGRM: Contract	CONTRACTION SCOUR								
	Width of main channel at approach section $W_1 = \underline{\hspace{1cm}}$ ft		O double						
			flow depth, y _{lob} =						
	width of right overbank flow at approach, $W_{rob} = $ ft Av	Width of right overbank flow at approach, $W_{rob} =ft$ Average right overbank flow depth, $y_{rob} =ft$							
PGR	Live Bed Contraction Scour (use if bed material is small cobbles or finer)	Live Bed Contraction Scour (use if hed material is small cobbles or finer)							
	$x =$ From Figure 9 W_2 (effective) =		ft						
EW	Clear Water Contraction Scour (use if bed material is larger than small co								
PGRM: CWCSNEW	Estimated bed material $D_{50} = $ ft Average approach		$/(y_1W_1) = \underline{\qquad \qquad ft}$	t/s					
	Critical approach velocity, $Vc = 11.52y_1^{1/6}D_{50}^{1/3} = ft/s$								
	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use	live bed scour equa	ition above.						
	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =ft$	$D_{50} >= D_{c50}, \chi = 0.0$							
	Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = $	From Figur	e 10, y _{cs} =	ft					
6									
PGRM: Pic	PIER SCOUR CALCULATION		bla IV VO -						
GRN	L/a ratio = Correction factor for flow angle Froude # at bridge = Using pier width a on Figure 11		STOCK MERCHANICAL .	G					
P	Froude # at bridge = Using pier width a on Figure 11	1, 5 –	riei scour y _{ps} –	11					
t	ABUTMENT SCOUR CALCULATIONS								
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} =ft$ rig		ft						
Abu	Shape coefficient K_1 = 1.00 for vertical-wall, 0.82 for vertical-wall			gh					
RM:	Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = $								
PG	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = ft$ Right abutment	nt scour $y_{as} = \psi_{RT}(K)$	$C_1/0.55$) = ft	t					

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ and $\psi_{RT} =$ and $\psi_{RT} =$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ ft

Route Third St. Stream James I	Ziver	MRM	Date	e	Ini	tials					
Bridge Structure No. 03248185 Lo	cation Tox	nos @	and C+	in	Turn						
GPS coordinates: HU" 21 807'	and	-									
98° 11.954'	nates: 44° 21.807' taken from: USt abutment centerline of \(\hat{\text{MRM end}}\) MRM end Datum of coordinates: WGS84 NAD27										
Drainage area = 13744.40 sq. mi.	13794	24					late				
The average bottom of the main channel wasft below top of guardrail at a point ft from left abutment											
Method used to determine flood flows: Freq	. Anal.	drainage area	ratio r	egional reg	ression eau	ations.	use gage date				
	241.05.03.039	- 0		0 0			7/3				
	MISCELLANEOUS CONSIDERATIONS										
Flows	$Q_{100} = 18300$			$Q_{500} = 32700$			3 1091				
Estimated flow passing through bridge	A MANUAL AND A MAN										
Estimated road overflow & overtopping	ļ.,,		15 "	▼ / ▼ /1000		I	10 1H608				
Consideration	Yes	No	Possibly	Yes	No	Possibly	25 35100				
Chance of overtopping Chance of Pressure flow											
Armored appearance to channel							109 94900				
Lateral instability of channel							598 2300ce				
Lateral histability of channel		<u> </u>					1				
Riprap at abutments? Yes	No	Marginal									
Contraction for the contraction of the contraction											
Debris Potential?HighMedLow											
Does scour countermeasure(s) appear to have been	n decigned?										
		!- D-		NIA							
		loDo									
Spur DikeYesNoDon't knowNA											
OtherY	esN	loDo	n't know _	NA							
Pod Material	Classification	Daaad a M	adian Dantiala	Circ (D)							
Bed Material Classification Based on Median Particle Size (D ₅₀)											
Material Silt/Clay Sand				Cobbles Boulders							
Size range, in mm <0.062 0.062-2	.00 2.00-64			64-250 >250							
Peaks from gage data Comments, Diagrams & orientation of digital pho											
Comments, Diagrams & orientation of digital pho	tos						1 1 3 1				
2 HOTO 1570 Str.	no,			right abut, under			derbridge				
approach (3rd St dom) from bridge right abut - ve							9				
2 1500 3820 approach (3rd St dam) from bridge right abut - upstro											
25 10,700 10000 bridge from left approach											
50 18300 left abutment (near)											
500 32700 left	ab Amer	nt (tar)									
Summary of Results	W										
		Q100			Q500						
Bridge flow evaluated											
Flow depth at left abutment (yaLT), in feet											
Flow depth at right abutment (yaRT), in feet											
Contraction scour depth (ycs), in feet											
Pier scour depth (yps), in feet											
Left abutment scour depth (yas), in feet											
Right abutment scour depth (yas), in feet											
1Flow angle of attack											