	SCOUR ANALYSIS AND REPORTING FORM						
	Bridge Structure No. 03758060 Date 7/23/12 Initials Region (ABCD)						
	Site Location 40190 196 St James River Que 17900 57400 by: drainage area ratio flood freq. anal. regional regression eq. ×						
	Bridge discharge $(Q_2) = \underline{57400}$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)						
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method						
PGRM: "RegionA", "RegionB", 'RegionC", or "RegionD"	Bridge Width = 296 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °						
	Width (W_2) iteration = Avg. flow depth at bridge, y_2 iteration =						
nA", 'Reg	Corrected channel width at bridge Section = W_2 times cos of flow angle = $\frac{291.5}{100}$ ft* $q_2 = \frac{196.9}{100}$ ft²/s						
egior "or"	Bridge Vel, $V_2 = 10$ ft/s Final $y_2 = q_2/V_2 = 19.5$ ft $\Delta h = 2$ ft						
I. "R	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 21.9$ ft						
GRN	* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,						
-	1) 52 S GOVE ES, MEN GEOGRAPH ROLL OF						
	Water Surface Elev. = $\frac{59}{22 \cdot 1}$ ft $\frac{26.9}{1.55}$ Low Steel Elev. = $\frac{22.1}{1.55}$ ft $\frac{26.9}{1.55}$ $\frac{1.55}{1.5}$						
	Low Steel Elev. = 22.1 ft 1.55 1.50						
	n (Channel) = 6.035 1.3 4.3						
	n(ROB) = 0.035 2.23						
	Pier Width = $\frac{2.05}{}$ ft Pier Length = $\frac{2}{}$ ft						
	Pier Length = 2 ft						
	# Piers for $100 \text{ yr} = 4 \text{ ft}$						
	CONTRACTION SCOUR						
ract	Width of main channel at approach section $W_1 = 296$ ft						
	Width of left overbank flow at approach, $W_{lob} = \frac{296}{ft}$ Average left overbank flow depth, $y_{lob} = \frac{3}{100}$						
PGRM: Contract	Width of right overbank flow at approach, $W_{\text{rob}} = 296$ ft Average right overbank flow depth, $y_{\text{rob}} = 365$ ft						
W.	With of Fight overbank now at approach, Wrob						
PGI	Live Bed Contraction Scour (use if bed material is small cobbles or finer)						
	$x = 15$ From Figure 9 W_2 (effective) = 293.3 ft $y_{cs} = 4.8$ ft						
PGRM: CWCSNEW	Clear Water Contraction Scour (use if bed material is larger than small cobbles)						
	Estimated bed material $D_{50} = $ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = $ ft/s						
Š	Critical approach velocity, $\sqrt{g} = 11.52y_1^{1/6}D_{50}^{1/3} = $ ft/s						
Z.	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.						
PGR	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = $ ft If $D_{50} >= D_{c50}$, $\gamma = 0.0$						
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
PGRM: Pier	PIER SCOUR CALCULATIONS						
RM:	L/a ratio = 0.9% Correction factor for flow angle of attack (from Table 1), K2 = Using pier width a on Figure 11, $\xi = \frac{9}{11}$ Pier scour $y_{ps} = \frac{7}{11}$ ft						
PG	Froude # at bridge = Using pier width a on Figure 11, $\xi = _{1}$ Pier scour $y_{ps} = _{1}$ ft						
	ABUTMENT SCOUR CALCULATIONS						
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{al.T} = \frac{3}{1}$ ft right abutment, $y_{aRT} = 5.5$ ft						
Abu	Average flow depth blocked by: left abutment, $y_{aLT} = \frac{3}{11}$ ft right abutment, $y_{aRT} = \frac{5.5}{11}$ ft r						
Z.	Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 11.7$ and $\psi_{RT} = 15.9$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 11.7$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 15.9$ ft						
Dd	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 15.9$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 15.9$ ft						

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COIN

SCOUR ANALYSIS AND REPORTING FORM

55545 'Ah SSS45 'Ah SLL1'36

Route 196 St Stream James R	iver	MRM	Dat	e 7/23	12 Ini	tialsRaT		
Bridge Structure No. (23258060 Loc	ation 40	190 1	96 ST					
GPS coordinates: N 44° 32′ 43,6′′ W 96° 10′ 36.6′′	taken from:	USL abutme	nt ×	centerline o	f Î MRM	end	_	
Drainage area = 13292.46 sq. mi.				111221_				
The average bottom of the main channel was			rail at a poin	110	ft from la	oft abutment		
Method used to determine flood flows: Freq.								46
	Settle Line		20,		ession equ	iations.		1-
MIS	SCELLANE	O50 COUS CONSI	DERATION	NS Q	0.6		/	15
Flows	The second second second second	7409444600		Q500 - ABLXXXX 91200			Z	1030
Estimated flow passing through bridge	57400			7 1675			5	15900
Estimated road overflow & overtopping	0			19525			10	1400
Consideration	Yes	No	Possibly	Yes	No	Possibly		
Chance of overtopping		X		\times			25	3370
Chance of Pressure flow		×		X			Sa	5740
Armored appearance to channel					X		100	9/20
Lateral instability of channel		>			×		Sce	2219
Spur Dike Other Bed Material Material Silt/Clay Sand Size range, in mm <0.062 0.062-2.	esN esN Classificatio	loDo loDo on Based on M Gravel 2.00-64	on't know on't know on't know dedian Particl	NA NA NA e Size (D ₅₀) Cobbles 64-250	- ulds on let	Boulders_ >250 Fyright over		
Comments, Diagrams & orientation of digital phot (1) Let OB (2) Main chance (3) List OB (4) Left abutant (5) Pier (6-6) Fisht abutant Summary of Results Bridge flow evaluated Flow depth at left abutment (yaLT), in feet Flow depth at right abutment (yaRT), in feet Contraction scour depth (ycs), in feet Pier scour depth (yps), in feet	os Ner Scom J. latt al	0400 (57460 3.1 5.5 4.8	50	FIN	2500 6 7(6) 6 5.9 8,3 8.5			
Left abutment scour depth (yas) in feet		11.7			167			

15.9

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Right abutment scour depth (yas), in feet

1Flow angle of attack