

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 03286120 Date 7/17/12 Initials RAT Region (A B C D) \_\_\_\_\_  
 Site \_\_\_\_\_ Location 40470 202nd St, James River  
 $Q_{100} = 18000$  by: drainage area ratio 5860 flood freq. anal. \_\_\_\_\_ regional regression eq. RAT  
 Bridge discharge ( $Q_2$ ) = 5860 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 324 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 304.46 ft\*  $q_2 = Q_2/W_2 = 192.5$  ft<sup>2</sup>/s

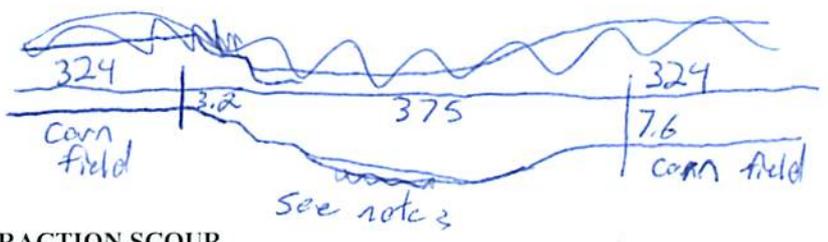
Bridge Vel,  $V_2 = 9.8$  ft/s Final  $y_2 = q_2/V_2 = 19.6$  ft  $\Delta h = 2$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 21.5$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 6.0 ft 27.7  
 Low Steel Elev. = 21.1 ft 26.6  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 29 ft  
 Pier Length = 2.9 ft  
 # Piers for 100 yr = 3 ft

27.4



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 375$  ft

Width of left overbank flow at approach,  $W_{lob} = 324$  ft Average left overbank flow depth,  $y_{lob} = 3.2$  ft

Width of right overbank flow at approach,  $W_{rob} = 324$  ft Average right overbank flow depth,  $y_{rob} = 2.6$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 11.64$  From Figure 9  $W_2$  (effective) = 295.8 ft  $y_{cs} = 12.7$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.39 Using pier width  $a$  on Figure 11,  $\xi = 10.5$  Pier scour  $y_{ps} = 9.1$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.2$  ft right abutment,  $y_{aRT} = 2.6$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 11.9$  and  $\psi_{RT} = 19.5$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 11.9$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 19.5$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

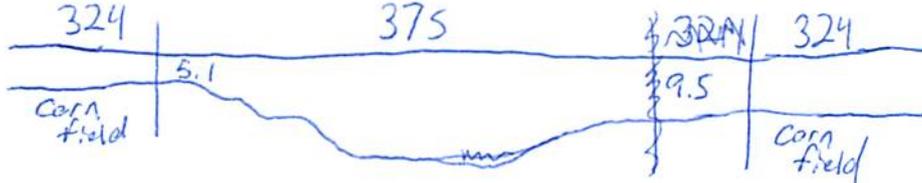
Bridge Structure No. 03286120 Date 7/17/12 Initials R-J Region (A B C D) C  
 Site 93100 Location 40470 202nd St  
 $Q_{500} = \frac{Q_{100}}{1.0} = \frac{32100}{1.0} = 32100$  by: drainage area ratio  flood freq. anal.  regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 69231 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 324 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 304.46 ft\*  $q_2 = Q_2/W_2 = \frac{224.1}{324} = 0.69$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \frac{Q_2}{W_2 y_2} = \frac{224.1}{324 \times 10.6} = 0.6$  ft/s Final  $y_2 = q_2/V_2 = \frac{0.69}{0.6} = 1.15$  ft  $\Delta h = 2.3$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 23.4$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 6.0 ft  
 Low Steel Elev. = 21.1 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.9 ft  
 Pier Length = 2.9 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 375$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 324$  ft Average left overbank flow depth,  $y_{lob} = 5.1$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 324$  ft Average right overbank flow depth,  $y_{rob} = 9.5$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 15.1$  From Figure 9  $W_2$  (effective) = 295.8 ft  $y_{cs} = 15$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.41 Using pier width a on Figure 11,  $\xi = 10.5$  Pier scour  $y_{ps} = 9.2$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 5.1$  ft right abutment,  $y_{aRT} = 9.5$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 15.2$  and  $\psi_{RT} = 20.9$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 15.2$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 20.9$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWSNEW

PGRM: Pie

PGRM: Abutment

Route 202 St Stream James River MRM \_\_\_\_\_ Date 7/17/12 Initials RAT  
 Bridge Structure No. 03286120 Location 40470 202<sup>nd</sup> St  
 GPS coordinates: N 44° 27' 26.0" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 98° 7' 14.6" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 13332.63 sq. mi. 13381.1  
 The average bottom of the main channel was 27.7 ft below top of guardrail at a point 199 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1.86000 58600</u>			Q <sub>500</sub> = <u>3.21000 93100</u>		
Estimated flow passing through bridge				<u>58600</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>24869</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

713  
 2 1050  
 5 6070  
 10 14300  
 25 34500  
 50 58600  
 100 93100  
 500 225000

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know some pier/contraction/abutment  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left OB  
 2) main channel  
 3) right OB  
 4) pier  
 5-6) right abutment  
 7) left abutment  
 8-9) right abutment  
 10) right abutment  
 11-14) left abutment  
 15) main channel

Note: water too deep for accurate pier measurements.  
 Left and right overbanks are mature corn fields. Cannot ~~not~~ accurately estimate elevation profile however, judging by the ~~the~~ uniform height of the corn, the fields are relatively level

Summary of Results

	Q <sub>100</sub> Q <sub>50</sub>	Q <sub>500</sub> Q <sub>100</sub>
Bridge flow evaluated	<del>58600</del> 58600	68231
Flow depth at left abutment (yaLT), in feet	<del>3.2</del> 3.2	5.1
Flow depth at right abutment (yaRT), in feet	<del>7.6</del> 7.6	9.5
Contraction scour depth (yca), in feet	12.7	15
Pier scour depth (yps), in feet	9.1	9.2
Left abutment scour depth (yas), in feet	11.9	15.2
Right abutment scour depth (yas), in feet	19.5	20.9
Flow angle of attack	20	20

See Comments/Diagram for justification where required