

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 03350048 Date 10-6-11 Initials RT Region (A B C D) (C)
 Site _____ Location 8.5 N Yale on 411th Ave
 Q₁₀₀ = 4770 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q₂) = 4770 (should be Q₁₀₀ unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °
 Width (W₂) iteration = 88.6 ~~76.5~~ 64
 Avg. flow depth at bridge, y₂ iteration = 10.4 ~~12.2~~
 Corrected channel width at bridge Section = W₂ times cos of flow angle = 63 ft* q₂ = Q₂/W₂ = 75.7 ft²/s
 Bridge Vel, V₂ = 6.2 ft/s Final y₂ = q₂/V₂ = 12.3 ft Δh = 0.8 ft
 Average main channel depth at approach section, y₁ = Δh + y₂ = 13.0 ft

* NOTE: repeat above calculations until y₂ changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
 If y₂ is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 5.2 ft
 Low Steel Elev. = 20.3 ft
 n (Channel) = .025
 n (LOB) = .027
 n (ROB) = .026
 Pier Width = 4.25 ft
 Pier Length = 4.25 ft
 # Piers for 100 yr = 2

Piers are 2'4" square, which have been reinforced for above the bottom half of their height (see photo). Q = 4.25'
 High water mark from this spring is above the estimated Q₁₀₀ level

CONTRACTION SCOUR

Width of main channel at approach section W₁ = 68 ft
 Width of left overbank flow at approach, W_{lob} = 10 ft Average left overbank flow depth, y_{lob} = 0.3 ft
 Width of right overbank flow at approach, W_{rob} = 137 ft Average right overbank flow depth, y_{rob} = 2.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 4.98 From Figure 9 W₂ (effective) = 57 ft y_{cs} = 5.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D₅₀ = _____ ft Average approach velocity, V₁ = Q₁₀₀/(y₁W₁) = _____ ft/s

Critical approach velocity, V_c = 11.17y₁^{1/3}D₅₀^{1/3} = NA ft/s

If V₁ < V_c and D₅₀ >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

D_{c50} = 0.0006(q₂/y₁^{7/6})³ = _____ ft If D₅₀ >= D_{c50}, χ = 0.0

Otherwise, χ = 0.122y₁[q₂/(D₅₀^{1/3}y₁^{7/6})]^{6/7} - y₁ = _____ From Figure 10, y_{cs} = _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K₂ = 1
 Froude # at bridge = 0.31 Using pier width a on Figure 11, ξ = 13.8 Pier scour y_{ps} = 11.5 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, y_{aLT} = 0.3 ft right abutment, y_{aRT} = 2.9 ft
 Shape coefficient K₁ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, ψ_{LT} = 1.4 and ψ_{RT} = 11.3
 Left abutment scour, y_{as} = ψ_{LT}(K₁/0.55) = 1.4 ft Right abutment scour y_{as} = ψ_{RT}(K₁/0.55) = 11.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNSW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 00350048 Date _____ Initials _____ Region (A B C D) _____
 Site _____ Location _____
 $Q_{500} = 9580$ by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 9580 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °
 Width (W_2) iteration = 88 67 76 72 74 73
 Avg. flow depth at bridge, y_2 iteration = 14.7 17 16 16.4 16.2
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 72 ft* $q_2 = Q_2/W_2 = 133.3$ ft²/s
 Bridge Vel, $V_2 = 8.2$ ft/s Final $y_2 = q_2/V_2 = 16.3$ ft $\Delta h = 1.4$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 17.6$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.2 ft
 Low Steel Elev. = 20.3 ft
 n (Channel) = .025
 n (LOB) = .027
 n (ROB) = .026
 Pier Width = 4.25 ft
 Pier Length = 4.25 ft
 # Piers for 500 yr = 2 ft

CONTRACTION SCOUR

Width of main channel at approach section $W_1 = 72$ ft
 Width of left overbank flow at approach, $W_{lob} = 66$ ft Average left overbank flow depth, $y_{lob} = 2.25$ ft
 Width of right overbank flow at approach, $W_{rob} = 160$ ft Average right overbank flow depth, $y_{rob} = 5.9$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 8.77$ From Figure 9 W_2 (effective) = 66 ft $y_{cs} = 9.7$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = 1$
 Froude # at bridge = 0.36 Using pier width a on Figure 11, $\xi = 13.8$ Pier scour $y_{ps} = 11.8$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = 2.25$ ft right abutment, $y_{aRT} = 5.9$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 9.2$ and $\psi_{RT} = 16.6$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 9.2$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 16.6$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 411th Ave Stream Shue Creek MRM _____ Date _____ Initials _____

Bridge Structure No. 00350048 Location 8.5 N Yale

GPS coordinates: N 44° 33.712' taken from: USL abutment centerline of MRM end _____
W 97° 59.864' Datum of coordinates: WGS84 NAD27 _____

Drainage area = 119.83 sq. mi.

The average bottom of the main channel was 26.1 ft below top of guardrail at a point 37 ft from left abutment.

Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

| Flows | Q ₁₀₀ = <u>4770</u> | | | Q ₅₀₀ = <u>9580</u> | | |
|---------------------------------------|--------------------------------|-------------------------------------|-------------------------------------|--------------------------------|-------------------------------------|-------------------------------------|
| Estimated flow passing through bridge | <u>4770</u> | | | <u>9580</u> | | |
| Estimated road overflow & overtopping | <u>NA</u> | | | <u>NA</u> | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly |
| Chance of overtopping | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Chance of Pressure flow | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Armored appearance to channel | | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> |
| Lateral instability of channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |

Riprap at abutments? Yes No Marginal
 Evidence of past Scour? Yes No Don't know
 Debris Potential? High Med Low

Quartzite riprap is present on abutments under the bridge and along the low-flow channel to approx. the approach section, possibly past contraction scour.

Does scour countermeasure(s) appear to have been designed?

Riprap Yes No Don't know NA
 Spur Dike Yes No Don't know NA
 Other Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Most, if not all of the abutment and pier scour will be mitigated by the existing riprap. Pier scour was calculated using the lower (larger) diameter of 4.25', so pier scour may be overestimated.

photos structure number approach section from bridge bridge section from approach right abutment from left piers from left abutment

Summary of Results

| | Q ₁₀₀ | Q ₅₀₀ |
|--|------------------|------------------|
| Bridge flow evaluated | <u>4770</u> | <u>9580</u> |
| Flow depth at left abutment (yaLT), in feet | <u>0.3</u> | <u>2.25</u> |
| Flow depth at right abutment (yaRT), in feet | <u>2.9</u> | <u>5.9</u> |
| Contraction scour depth (y _{cs}), in feet | <u>5.7</u> | <u>9.7</u> |
| Pier scour depth (y _{ps}), in feet | <u>11.5</u> | <u>11.8</u> |
| Left abutment scour depth (y _{as}), in feet | <u>1.4</u> | <u>9.2</u> |
| Right abutment scour depth (y _{as}), in feet | <u>11.3</u> | <u>16.6</u> |
| Flow angle of attack | <u>10°</u> | <u>10°</u> |

See Comments/Diagram for justification where required

Basin Characteristics from StreamStats on 10-5-11 (Provisional)

$$\text{Contrib D.A.} = 119.83$$

$$\text{PII} = 0.92$$

18% Subregion A

$$Q_{100} = 3020 \text{ cfs}$$

$$Q_{500} = 4940 \text{ cfs}$$

$$.18 Q_{100} = 543.6$$

$$.18 Q_{500} = 889.2$$

82% Subregion B

$$Q_{100} = 5150 \text{ cfs}$$

$$Q_{500} = 10600 \text{ cfs}$$

$$.82 Q_{100} = 4223$$

$$.82 Q_{500} = 8692$$

Area weighted

$$Q_{100} = 4766.6 \approx$$

4770 cfs

$$Q_{500} = 9581.2 \approx$$

9580 cfs