

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 05187100 Date 6/10/12 Initials RT Region (A B C D) D  
 Site \_\_\_\_\_ Location 301 St, ~ 2 mi N, 2.7 mi E Tyndall - Bon Homme Co  
 $Q_{100} =$  1740 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1740 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 49 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 48.81 ft\*  $q_2 = Q_2/W_2 =$  35.6 ft<sup>2</sup>/s

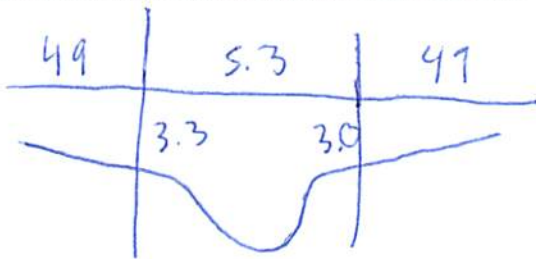
Bridge Vel,  $V_2 =$  4.2 ft/s Final  $y_2 = q_2/V_2 =$  8.4 ft  $\Delta h =$  0.4 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 6 ft  
 Low Steel Elev. = 8.55 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = ~~0.025~~ 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 1.11 ft  
 Pier Length = 1.11 ft  
 # Piers for 100 yr = 1 ft



$\frac{3.5}{\pi}$

$1.3 \cdot \frac{2.4}{2.6}$

#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  49.53 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  49 ft Average left overbank flow depth,  $y_{lob} =$  3.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  49 ft Average right overbank flow depth,  $y_{rob} =$  3.0 ft

#### Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  5.33 From Figure 9  $W_2$  (effective) = 47.7 ft  $y_{cs} =$  6 ft

#### Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / \chi_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.26 Using pier width  $a$  on Figure 11,  $\xi =$  5.2 Pier scour  $y_{ps} =$  9.2 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.3 ft right abutment,  $y_{aRT} =$  3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12 and  $\psi_{RT} =$  11.5  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  18 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  17.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

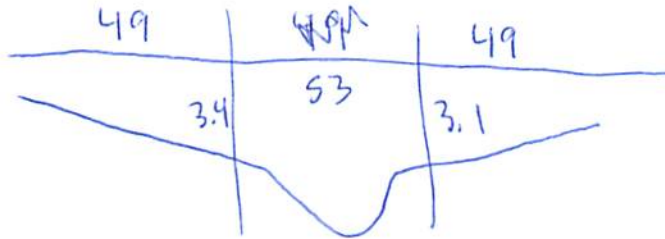
Bridge Structure No. 05187100 Date 6/10/12 Initials RAJ Region (A B C D) (D)  
 Site \_\_\_\_\_ Location 301 st, ~ 2 mi N, 2.7 mi E Tyndall - Bon Homme  
 $Q_{500} =$  338^A by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1240-1792 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 49 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 48.81 ft\*  $q_2 = Q_2/W_2 =$  36.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.3 ft/s Final  $y_2 = q_2/V_2 =$  8.6 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 8.55 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.11 ft  
 Pier Length = 1.11 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  53 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  49 ft Average left overbank flow depth,  $y_{lob} =$  3.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  49 ft Average right overbank flow depth,  $y_{rob} =$  3.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  5.54 From Figure 9  $W_2$  (effective) = 47.7 ft  $y_{cs} =$  6.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^{3/5} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.26 Using pier width a on Figure 11,  $\xi =$  5.2 Pier scour  $y_{ps} =$  4.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.4 ft right abutment,  $y_{aRT} =$  3.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.2 and  $\psi_{RT} =$  11.7  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  18.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  17.4 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment



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Vertical handwritten notes on the left side of the page, possibly identifying a section or providing additional context.

97.79847  
43.0251

Route 301 St Stream Snatch Ck MRM \_\_\_\_\_ Date 6/10/12 Initials Bar  
 Bridge Structure No. 05187100 Location 2 mi N, 2.7 mi E of Tyndall  
 GPS coordinates: N 43° 1' 30.6" W 97° 47' 54.4" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 17.85 sq. mi.  
 The average bottom of the main channel was 12.4 ft below top of guardrail at a point 36 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1740</u>			Q <sub>500</sub> = <u>3380</u>		
Estimated flow passing through bridge	<u>1740</u>			<u>1792</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1588</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/22

2	67.4
5	234
10	437.48
25	830.81
50	1230
100	1740
500	3380

6/4

2	67.5
5	234
10	438
25	831
50	1230
100	1740
500	3380

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know contraction  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left OB
- 2). main channel
- 3). right OB
- 4). piers
- 5-6). left abutment
- 7-9). ~~right~~ right abutment (damaged)

Note: channel is dry  
 10). main channel

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1740</u>	<u>1792</u>
Flow depth at left abutment (yaLT), in feet	<u>3.3</u>	<u>3.4</u>
Flow depth at right abutment (yaRT), in feet	<u>3</u>	<u>3.1</u>
Contraction scour depth (yes), in feet	<u>6</u>	<u>6.3</u>
Pier scour depth (yps), in feet	<u>4.2</u>	<u>4.5</u>
Left abutment scour depth (yas), in feet	<u>19</u>	<u>18.2</u>
Right abutment scour depth (yas), in feet	<u>17.2</u>	<u>17.4</u>
Flow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required