

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 06/12080 Date 5-17-12 Initials CW/RA/T Region (A B C D) D  
 Site \_\_\_\_\_ Location 204 St, 0.5 mi S + 0.3 mi W of Bruce - Brookings Co  
 $Q_{100} = 10900$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 10900 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 235 ft. 234.11 Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 235

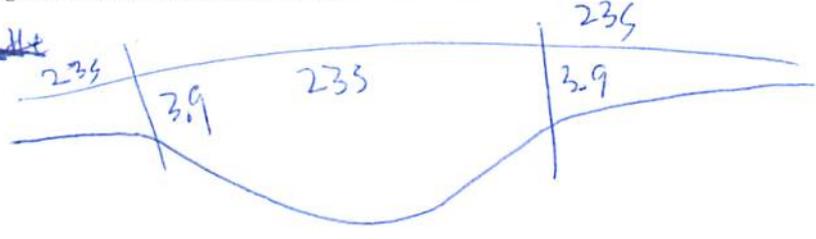
Avg. flow depth at bridge,  $y_2$  iteration = 155  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 234.11 ft\*  $q_2 = Q_2/W_2 = \frac{46.6}{0.5} = 93.2$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 4.8$  ft/s Final  $y_2 = q_2/V_2 = \frac{93.2}{4.8} = 19.4$  ft  $\Delta h = 6.8$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 10.1$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.6 ft  
 Low Steel Elev. = 10.9 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 2.4 ft  
 Pier Length = 2.4 ft  
 # Piers for 100 yr = 3 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 235$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 235$  ft Average left overbank flow depth,  $y_{lob} = 3.9$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 235$  ft Average right overbank flow depth,  $y_{rob} = 3.9$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 5.22$  From Figure 9  $W_2$  (effective) = 226.9 ft  $y_{cs} = 6$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water scour equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^{1/3} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi = 9.2$  Pier scour  $y_{ps} = 7.6$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.9$  ft right abutment,  $y_{aRT} = 3.9$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 13.1$  and  $\psi_{RT} = 13.1$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 13.1$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 13.1$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PRGM: Contract  
 PRGM: CWCSNEW  
 PRGM: Pier  
 PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

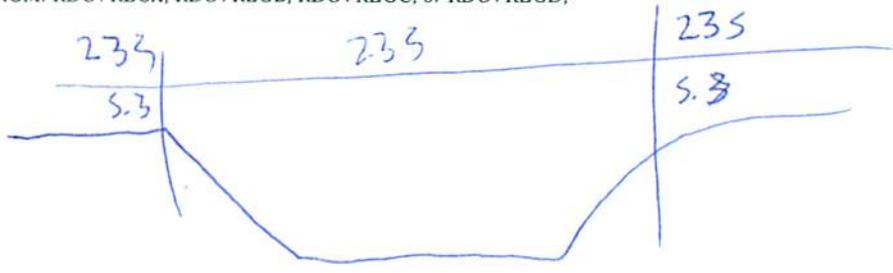
Bridge Structure No. 06112080 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) D  
 Site \_\_\_\_\_ Location 204 St, 0.5 mi S + 0.3 mi W of Bruce  
 $Q_{500} =$  ~~31100~~ ~~31100~~ ~~41100~~ by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = ~~21875~~ 13975 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 235 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 234.11 ft\*  $q_2 = Q_2/W_2 =$  ~~59.7~~ 59.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  ~~5.5~~ 5.5 ft/s Final  $y_2 = q_2/V_2 =$  ~~10.9~~ 10.9 ft  $\Delta h =$  0.6 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  ~~11.5~~ 11.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 11.6 ft  
 Low Steel Elev. = ~~10.9~~ 10.9 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 24 ft  
 Pier Length = 2.4 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  235 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  235 ft Average left overbank flow depth,  $y_{lob} =$  5.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  235 ft Average right overbank flow depth,  $y_{rob} =$  5.3 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  7.9 From Figure 9  $W_2$  (effective) = 226.9 ft  $y_{cs} =$  8.7 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi =$  9.2 Pier scour  $y_{ps} =$  7.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.3 ft right abutment,  $y_{aRT} =$  5.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.6 and  $\psi_{RT} =$  15.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  15.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  15.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

Route 204 St Stream Big Sioux River MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 06112080 Location 204 St, 0.5 mi S + 0.3 mi W of Brnca  
 GPS coordinates: N44° 25' 40.3" taken from: USL abutment \_\_\_\_\_ centerline of ↑ MRM end \_\_\_\_\_  
W 98° 54' 13.7" Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_  
 Drainage area = 1561 sq. mi. 16.6  
 The average bottom of the main channel was 15.6 ft below top of guardrail at a point 85 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

5/15  
~~8/22~~

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>25</sub> = 10900			Q <sub>500</sub> = 14700		
Estimated flow passing through bridge	10900			13975		
Estimated road overflow & overtopping	0			725		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X		X		
Chance of Pressure flow		X		X		
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

2 1610  
 5 4210  
 10 6750  
 25 10900  
 50 14700  
 100 19000  
 500 31100

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 2273 Str. no.
- 2274 bridge from left approach
- 2275 left abut from right approach
- 2276 left abut.
- 2277 right abut.
- 2278 bridge section from left ditch

Summary of Results

	Q <sub>100</sub> Q <sub>25</sub>	Q <sub>500</sub> 50
Bridge flow evaluated	10900	13975
Flow depth at left abutment (yaLT), in feet	3.9	5.3
Flow depth at right abutment (yaRT), in feet	3.9	5.3
Contraction scour depth (y <sub>cs</sub> ), in feet	7.6	8.7
Pier scour depth (y <sub>ps</sub> ), in feet	7.6	7.7
Left abutment scour depth (y <sub>as</sub> ), in feet	13.1	15.6
Right abutment scour depth (y <sub>as</sub> ), in feet	13.1	15.6
IFlow angle of attack	5	5

See Comments/Diagram for justification where required