

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 06122010 Date 5-17-12 Initials CW/RAT Region (A B C D) D  
 Site \_\_\_\_\_ Location 197 St, 6 mi N, 0.2 mi East Bruce  
 $Q_{100} =$  559 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 52 ft. Flow angle at bridge = 40 ° Abut. Skew = 0 ° Effective Skew = 40 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 39.83 ft\*  $q_2 = Q_2/W_2 =$  14 ft<sup>2</sup>/s

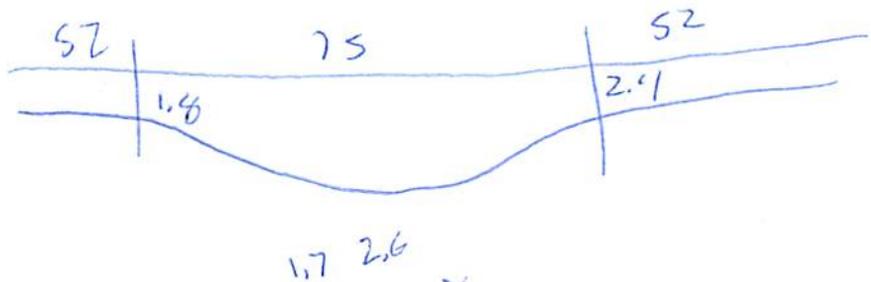
Bridge Vel,  $V_2 =$  2.7 ft/s Final  $y_2 = q_2/V_2 =$  5.3 ft  $\Delta h =$  0.1 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 6.5 ft  
 Low Steel Elev. = 5.4 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.045  
 $n$  (ROB) = 0.045  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  75 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  52 ft Average left overbank flow depth,  $y_{lob} =$  1.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  52 ft Average right overbank flow depth,  $y_{rob} =$  2.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  7.73 From Figure 9  $W_2$  (effective) = 39.8 ft  $y_{cs} =$  8.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = ∞ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  3  
 Froude # at bridge = 0.21 Using pier width  $a$  on Figure 11,  $\xi =$  0 Pier scour  $y_{ps} =$  0 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.8 ft right abutment,  $y_{aRT} =$  2.4 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  7.4 and  $\psi_{RT} =$  9.8  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  13.5 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  17.5 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 06122010 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) D  
 Site \_\_\_\_\_ Location 197 St. 6 mi. N, 0.2 mi. E of Bruce  
 $Q_{500} =$  855 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 626 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 52 ft. Flow angle at bridge = \_\_\_\_\_° Abut. Skew = \_\_\_\_\_° Effective Skew = \_\_\_\_\_°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 39.83 ft\*  $q_2 = Q_2/W_2 =$  15.7 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  2.8 ft/s Final  $y_2 = q_2/V_2 =$  5.6 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0.5 ft  
 Low Steel Elev. = 5.6 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.045  
 n (ROB) = 0.045  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  75 ft

Width of left overbank flow at approach,  $W_{lob} =$  52 ft

Average left overbank flow depth,  $y_{lob} =$  2.2 ft

Width of right overbank flow at approach,  $W_{rob} =$  52 ft

Average right overbank flow depth,  $y_{rob} =$  2.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  8.88 From Figure 9  $W_2$  (effective) = 39.8 ft  $y_{cs} =$  9.8 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1)^{7/6} =$  \_\_\_\_\_ ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = ∞

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  +

Froude # at bridge = \_\_\_\_\_

Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  0 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.2 ft right abutment,  $y_{aRT} =$  2.8 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  9 and  $\psi_{RT} =$  11.2

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  16.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  20.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 197<sup>th</sup> St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 06122010 Location 197 St, 6 mi N, 0.2 mi E of Bruce  
 GPS coordinates: N 44° 31' 43.0" taken from: USL abutment \_\_\_\_\_ centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 50' 46.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 1.94 sq. mi.  
 The average bottom of the main channel was 9.7 ft below top of guardrail at a point 0.87 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

514  
 4/22  
 2  
 5  
 10  
 25  
 50  
 100  
 500  
 49  
 133  
 213  
 337  
 443  
 559  
 855

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>559</u>			Q <sub>500</sub> = <u>855</u>		
Estimated flow passing through bridge	<u>559</u>			<u>626</u>		
Estimated road overflow & overtopping				<u>229</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

2293 Str. no  
 2294 LOB from bridge  
 2295 ~~LOB~~ approach from bridge  
 2296 ROB from bridge  
 2297 left abut. from channel in ditch  
 2298 right abut. from ditch  
 2299 bridge section from approach  
 2300 bridge section from approach  
 2301 bridge section from right ditch

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>559</u>	<del>855</del> <u>626</u>
Flow depth at left abutment (yaLT), in feet	<u>1.8</u>	<u>2.2</u>
Flow depth at right abutment (yaRT), in feet	<u>2.4</u>	<u>2.8</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>6.6</u>	<u>9.8</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<del>0</del> <u>NA</u>	<del>0</del> <u>NA</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>13.5</u>	<u>16.4</u>
Right abutment scour depth (y <sub>rs</sub> ), in feet	<u>17.8</u>	<u>20.3</u>
Flow angle of attack	<u>40°</u>	<u>40°</u>

See Comments/Diagram for justification where required