

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 06131130 Date 10-12-11 Initials TJT Region (A B C D) (C)

Site \_\_\_\_\_ Location from Volga, 3E, 2N, 0.2E

$Q_{100} =$  5240 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.

Bridge discharge ( $Q_2$ ) = 5240 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 110 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width ( $W_2$ ) iteration = 110

Avg. flow depth at bridge,  $y_2$  iteration = 9.7

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 110 ft\*  $q_2 = Q_2/W_2 =$  47.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.9 ft/s Final  $y_2 = q_2/V_2 =$  9.7 ft  $\Delta h =$  0.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.4 ft

Low Steel Elev. = 9.1 ft

n (Channel) = .029

n (LOB) = .028

n (ROB) = .028

Pier Width = 2.0 ft

Pier Length = 2.0 ft

# Piers for 100 yr = 2 ft

channel has been cleaned out recently on up- and down-stream sides of bridge. Spoil piles are still present

bridge will probably pass  $Q_{100}$  with pressure flow

Road overflow may happen for  $Q > Q_{100}$

assume  $Q_{100} = Q_{max\ scour}$

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  110 ft

Width of left overbank flow at approach,  $W_{lob} =$  1 ft - Average left overbank flow depth,  $y_{lob} =$  1 ft

Width of right overbank flow at approach,  $W_{rob} =$  1 ft - Average right overbank flow depth,  $y_{rob} =$  1 ft

\* past spoil piles block overbank on both sides at approach

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.39 From Figure 9  $W_2$  (effective) = 106 ft  $y_{cs} =$  0.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.28

Using pier width a on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft

Shape coefficient  $K_1 =$  1.00 for vertical wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  \_\_\_\_\_ ft

In present condition, equations will not predict any abutment scour because of spoil piles at approach section

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNSWE

PRGM: Pier

PRGM: Abutment

# SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 06131130 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) \_\_\_\_\_  
 Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} =$ 8290 $$ by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 110 ft. Flow angle at bridge = \_\_\_\_\_° Abut. Skew = \_\_\_\_\_° Effective Skew = \_\_\_\_\_°

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = \_\_\_\_\_ ft\*  $q_2 = Q_2/W_2 =$  \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  \_\_\_\_\_ ft/s Final  $y_2 = q_2/V_2 =$  \_\_\_\_\_ ft  $\Delta h =$  \_\_\_\_\_ ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  \_\_\_\_\_ ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = \_\_\_\_\_ ft

n (Channel) = \_\_\_\_\_

n (LOB) = \_\_\_\_\_

n (ROB) = \_\_\_\_\_

Pier Width = \_\_\_\_\_ ft

Pier Length = \_\_\_\_\_ ft

# Piers for 500 yr = \_\_\_\_\_

Q<sub>max scour</sub> ≈ Q<sub>100</sub>  
 see top sheet

### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft

Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft

Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft

Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft

Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9

$W_2$  (effective) = \_\_\_\_\_ ft

$y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft

Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_

Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_

Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  \_\_\_\_\_ ft

Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  \_\_\_\_\_ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCNEW  
 PGRM: Pier  
 PGRM: Abutment

Route 209<sup>th</sup> St Stream N. Deer Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_

Bridge Structure No. 06131130 Location from Volga, 3<sup>rd</sup> 2 N, 0.2 E

GPS coordinates: N 44° 21.328' taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 51.885' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 111.25 sq. mi.

The average bottom of the main channel was 13.0 ft below top of guardrail at a point 36 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

### MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>5240</u>			Q <sub>500</sub> = <u>8290</u>		
Estimated flow passing through bridge	<u>5240</u>					
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>			
Chance of Pressure flow	<input checked="" type="checkbox"/>					
Armored appearance to channel		<input checked="" type="checkbox"/>				
Lateral instability of channel			<input checked="" type="checkbox"/>			

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal rubble + riprap (some silted under?) on  
 Evidence of past Scour? \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know right abutment. It appears that  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low deposition occurs at this site?

Does scour countermeasure(s) appear to have been designed?

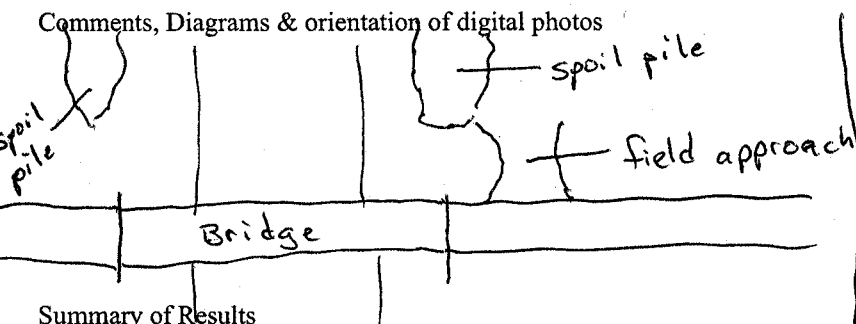
Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  NA  
 Other guide bank? \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

spoil pile at upstream left may act as guide bank until it gets eroded away

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_\_\_ Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos



photos  
structure number  
approach from bridge  
left approach from bridge  
ROB from LOB  
Bridge from approach

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>5240</u>	
Flow depth at left abutment (yaLT), in feet	—	
Flow depth at right abutment (yaRT), in feet	—	
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>0.6</u>	
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.6</u>	
Left abutment scour depth (yas), in feet	—	
Right abutment scour depth (yas), in feet	—	
Flow angle of attack	<u>0°</u>	

See Comments/Diagram for justification where required

Basin characteristics from  
Provisional Stream Stats 10-7-11

$$\text{Cont. D.A.} = 111.25 \text{ mi}^2$$

$$\text{PII} = 1.05$$

100% Subregion A

Manually Calculated Peaks

$$Q_{100} = 5240 \text{ cfs}$$

$$Q_{500} = 8290 \text{ cfs}$$