| | SCOUR ANALYSIS AND REPORTING FORM |
|---|--|
| | Bridge Structure No. 06 17010 Date 5-17-12 Initials CW/RaT Region (ABOD) |
| | Site Location 49 mi N of HWY 14 Bypan on 471 Are |
| | Q ₁₀₀ = 2.596 by: drainage area ratio flood freq. anal. regional regression eq. |
| | Bridge discharge $(Q_2) = 2570$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping) |
| | (with the state of |
| | Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method |
| | Bridge Width = $\frac{96}{10}$ ft. Flow angle at bridge = $\frac{15}{10}$ Abut. Skew = $\frac{15}{10}$ ° Effective Skew = $\frac{15}{10}$ ° |
| PGRM: "RegionA", "RegionB", "RegionC", or "RegionD" | Width (W_2) iteration = 96 |
| Regio | Avg. flow depth at bridge, y_2 iteration = $\frac{9}{6}$ |
| ", "I | Corrected channel width at bridge Section = W_2 times cos of flow angle = 92.73 ft* $q_2 = Q_2/W_2 = 27.9$ ft²/s |
| ionA | Bridge Vel, $V_2 = 3.7$ ft/s Final $y_2 = q_2/V_2 = 7.5$ ft $\Delta h = 0.3$ ft |
| Reg | Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \frac{7.7}{100}$ ft |
| M: Jion | *NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ |
| CR 'Reg | If y ₂ is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, |
| | 1 1 |
| | Water Surface Elev. = Offi |
| | Low Steel Elev. = ft 10.5 |
| | $ n \text{ (Channel)} = 0.040 \\ n \text{ (LOB)} = 0.035 \\ 2.9 \\ 2.6 $ |
| | n (LOB) = 0.035 $n (ROB) = 0.035$ |
| | Pier Width = $1, 3$ ft |
| | Pier Length = 33 ft |
| | # Piers for $100 \text{ yr} = 2 \text{ ft}$ |
| | |
| | CONTRACTION SCOUR 2. 9 |
| | Width of main channel at approach section $W_1 = 16$ ft |
| tract | Width of left overbank flow at approach, $W_{lob} = 96$ ft Average left overbank flow depth, $y_{lob} = 16$ |
| PGRM: Contract | Width of right overbank flow at approach, $W_{rob} = \frac{96}{100}$ ft Average right overbank flow depth, $y_{rob} = \frac{4}{100}$ ft |
| ≅ | The state of the s |
| PG | Live Bed Contraction Scour (use if bed material is small cobbles or finer) |
| | $x = 5.76$ From Figure 9 W_2 (effective) = 90.1 ft $y_{cs} = 6.5$ ft |
| | |
| EW | Clear Water Contraction Scour (use if bed material is larger than small cobbles) |
| SS | Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$ |
| CWC | Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3}$ ft/s |
| PGRM: CWCSNEW | If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above. |
| PGF | $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = ft$ $Otherwise, \chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = ft$ $From Figure 10, y_{cs} = ft$ |
| | Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = ft$ |
| | 7 10 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| ier | PIER SCOUR CALCULATIONS |
| PGRM: Pier | L/a ratio = $\frac{25}{}$ Correction factor for flow angle of attack (from Table 1), K2 = $\frac{2.5}{}$ |
| PGR | Froude # at bridge = 0.24 Using pier width a on Figure 11, $\xi = 5.8$ Pier scour $y_{ps} = 11.7$ ft |
| | от <u>го</u> |
| Ħ | ABUTMENT SCOUR CALCULATIONS |
| PGRM: Abutment | Average flow depth blocked by: left abutment, $y_{aLT} = 2.1$ ft right abutment, $y_{aRT} = 4.2$ ft Shape coefficient $K = 100$ for vertical wall $= 0.82$ for vertical wall with wingwalls $= 0.55$ for apill through |
| : Ab | Shape coefficient R vertical-wall, 0.52 for vertical-wall with whigh walls, 0.55 for spin-through |
| RM | Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 11.3$ and $\psi_{RT} = 13.6$ |
| Š | Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 8206$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 24.7$ ft |

7.9

| Route 471 Arc Stream Branch of | Deer C 1 | MRM | Da | ite | Init | ials | | |
|--|-------------------------|------------------|--------------|----------------------------|--------------|--------------|-------|------|
| | | mi Nof | | | | 11 Ave | | |
| GPS coordinates: N 44° 23' 44. b" | | USL abutment | | centerline o | | | | |
| W96 47 15.2" | | ordinates: WO | | | | | | |
| Drainage area = 28.69 sq. mi. | | | | _ | | | | |
| The average bottom of the main channel was 14 | , 6 ft below | v top of guardra | il at a poin | nt 51 | ft from lef | ft abutment. | | |
| Method used to determine flood flows:Freq | . Anal | drainage area r | atio 🗶 | regional reg | ression equa | ations. | 0/ | 22 |
| MI | SCELLANE | OUS CONSII | ERATIO | NS | | | 01 | 1233 |
| Flows | | | EKATIO | Q ₅₀₀ = | 4040 |) | 12 | |
| Estimated flow passing through bridge | $Q_{100} = 2590$ 2590 | | | 4040 | | | 5 | 616 |
| Estimated road overflow & overtopping | 2570 | | | | 4040 | | | 974 |
| Consideration | Yes | No | Possibly | Yes | No | Possibly | 10 | 1540 |
| Chance of overtopping | 103 | X | 1 ossiony | 100 | X | Tossiory | 60 | 2040 |
| Chance of Pressure flow | 7 | X | | | | X | | 2590 |
| Armored appearance to channel | | 8 | | | X | | 100 | 4040 |
| Lateral instability of channel | | /X | | | X | | 500 | 1000 |
| 1 | / | , , | | | | | 5 | 14 |
| Riprap at abutments? Yes | No | Marginal | | | | | 2 | 233 |
| Evidence of past Scour? X Yes | No | Don't know | Pier | Scow | | | | 616 |
| Debris Potential? High | Med | Low | | | | | | 974 |
| | | | | | | | 25 | |
| Does scour countermeasure(s) appear to have been | n designed? | | | × . | | | | 1540 |
| Riprap | es N | o Don | 't know | X NA | | | 100 | 2596 |
| | es N | | 't know | NA | | | 500 | 4040 |
| • | es N | | 't know | NA | | | 300 1 | 400 |
| Olliei1 | IN | ODoi: | t Know | INA | | | | |
| Bed Material | Classificatio | n Based on Me | dian Partic | le Size (D ₅₀) | | | | |
| Material Silt/Clay Sand | | Gravel | | Cobbles | | Boulders | | |
| Size range, in mm <0.062 0.062-2 | | 2.00-64 | | 64-250 | | >250 | | |
| 5/2c range, in min | .00 | 2.00-04 | | 04-230 | | -250 | | |
| Comments, Diagrams & orientation of digital pho | tos | | | | | | | |
| 2268 Str. no. | | | | | | | | |
| | ch | | | | | | | |
| 2269 bridge from rt. approx 2270 right abutment | | | | | | | | |
| 2271 left abutment | | | | | | | | |
| | | | | | | | | |
| 2272 bridge from rt. ditch |) | | | | | | | |

Summary of Results

| | Q100 | Q500 |
|--|------|-------|
| Bridge flow evaluated | 2590 | 4040 |
| Flow depth at left abutment (yaLT), in feet | 2,9 | 5 |
| Flow depth at right abutment (yaRT), in feet | 4,2 | 6.3 |
| Contraction scour depth (ycs), in feet | 6.5 | II.Z |
| Pier scour depth (yps), in feet | 11.7 | 11.9 |
| Left abutment scour depth (yas), in feet | 20.6 | 27.3 |
| Right abutment scour depth (yas), in feet | 24.7 | 31, 5 |
| 1Flow angle of attack | 150 | 150 |