

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 06203110 Date 7/25/12 Initials Ral Region (A B C D) D  
 Site \_\_\_\_\_ Location 207 St, 0.4 mi E of int. of 207 St + 474 Ave  
 $Q_{100} = Q_{50}$  2440 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2440 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

96  
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 99 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 85.74 ft\*  $q_2 = Q_2/W_2 = \underline{28.5}$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = \underline{3.8}$  ft/s Final  $y_2 = q_2/V_2 = \underline{7.5}$  ft  $\Delta h = \underline{0.3}$  ft

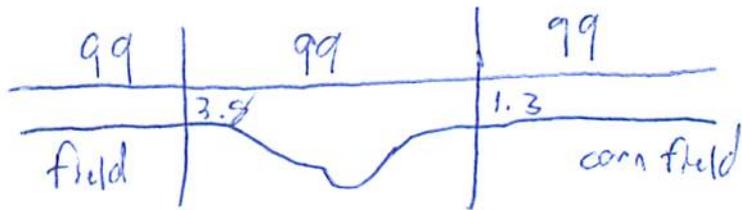
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{7.8}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

right 2.5

Water Surface Elev. = 6.8 ft  
 Low Steel Elev. = 7.9 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.030  
 n (ROB) = 0.025  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 100 yr = 2 ft



### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{99}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{99}$  ft Average left overbank flow depth,  $y_{lob} = \underline{3.9}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{99}$  ft Average right overbank flow depth,  $y_{rob} = \underline{1.3}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{6.53}$  From Figure 9  $W_2$  (effective) = 81.7 ft  $y_{cs} = \underline{7.3}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} = \underline{1}$  ft

### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.24 Using pier width  $a$  on Figure 11,  $\xi = \underline{8}$  Pier scour  $y_{ps} = \underline{6.5}$  ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{3.8}$  ft right abutment,  $y_{aRT} = \underline{1.3}$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{12.9}$  and  $\psi_{RT} = \underline{5.5}$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = \underline{12.9}$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = \underline{5.5}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 06203110 Date 7/25/12 Initials RAJ Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.4 mi. E of int. of 2075th & 474 Ave  
 $Q_{500} = Q_{ice} 3100$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2666 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 99 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

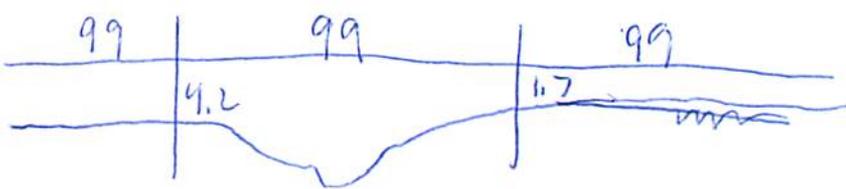
Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 85.71 ft\*  $q_2 = Q_2/W_2 = 31.3$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 4$  ft/s Final  $y_2 = q_2/V_2 = 7.9$  ft  $\Delta h = 0.3$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 8.2$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.9 ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 99$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 99$  ft Average left overbank flow depth,  $y_{lob} = 4.2$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 99$  ft Average right overbank flow depth,  $y_{rob} = 1.7$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 7.54$  From Figure 9  $W_2$  (effective) = 81.7 ft  $y_{cs} = 8.4$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.25 Using pier width  $a$  on Figure 11,  $\xi = 8$  Pier scour  $y_{ps} = 6.5$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 4.2$  ft right abutment,  $y_{aRT} = 1.7$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 13.6$  and  $\psi_{RT} = 7$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 13.6$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 7$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

96.7202  
44.38326

440 23' 4.176'  
96° 43' 12.432'

Route 207 St Stream Six Mile Ck MRM \_\_\_\_\_ Date 7/25/12 Initials Pat  
 Bridge Structure No. 06203110 Location 0.4 mi. E of int of 207 St + 474 Ave  
 GPS coordinates: N 44° 23' 1.3" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 43' 12.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 37.34 sq. mi.  
 The average bottom of the main channel was 11.9 ft below top of guardrail at a point 64 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>800</u> <u>2440</u>			Q <sub>500</sub> = <u>3100</u> <u>3100</u>		
Estimated flow passing through bridge	<u>2440</u>			<u>2686</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>414</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/3  
8/22  
2 | 283  
5 | 742  
10 | 1170  
25 | 1850  
50 | 2440  
100 | 3100  
500 | 4840

Riprap at abutments? \_\_\_\_\_ Yes  No  Marginal lots of gravel-small cobbles  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know minor contraction  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel  Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab  
 2). main channel  
 3). right ab  
 4-5). pier  
 6). right abutment  
 7). left abutment  
 8). left abutment  
 9). right abutment  
 10). main channel

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>2440</u>	<u>2686</u>
Flow depth at left abutment (yaLT), in feet	<u>3.8</u>	<u>4.2</u>
Flow depth at right abutment (yaRT), in feet	<u>1.3</u>	<u>1.7</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>2.3</u>	<u>8.4</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.5</u>	<u>6.5</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>12.9</u>	<u>13.6</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>5.5</u>	<u>7</u>
IFlow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required