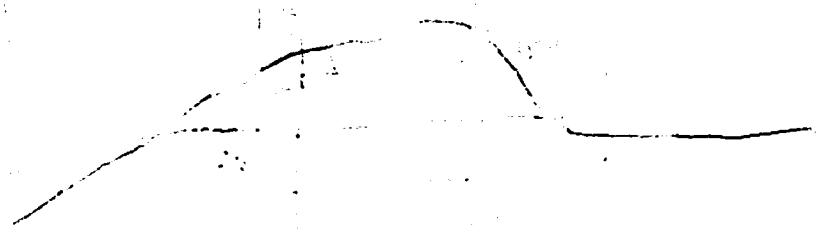


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OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 07009480 Date 7/19/12 Initials Pat Region (A B C D) D  
 Site \_\_\_\_\_ Location 148.5 ft, 6.6 mi. W of Mansfield  
 $Q_{100} = Q_{50}$  5770 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5770 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 140 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 135.23 ft\*  $q_2 = Q_2/W_2 = 42.7$  ft<sup>2</sup>/s

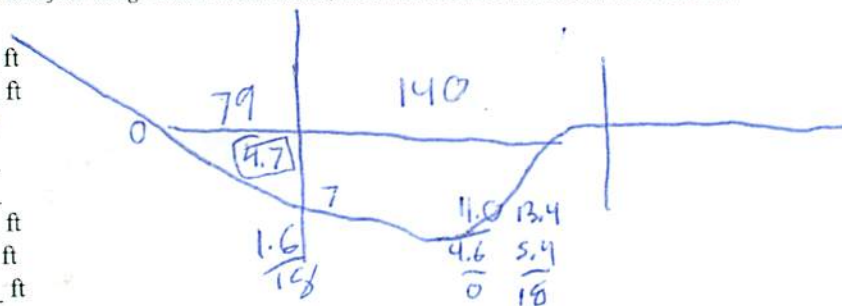
Bridge Vel,  $V_2 = 3.2$  ft/s Final  $y_2 = q_2/V_2 = 13.2$  ft  $\Delta h = 0.2$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 13.4$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.1 ft  
 Low Steel Elev. = 14.2 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 140$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 79$  ft Average left overbank flow depth,  $y_{lob} = 4.7$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 140$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 2.54$  From Figure 9  $W_2$  (effective) = 131.2 ft  $y_{cs} = 3.1$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.16 Using pier width  $a$  on Figure 11,  $\xi = 8$  Pier scour  $y_{ps} = 6$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 4.7$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 14.5$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 14.5$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 0$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 0700 8480 Date 7/19/12 Initials RT Region (A B C D) D  
 Site \_\_\_\_\_ Location 148 St, 6.6 mi. W of Mansfield  
 $Q_{500} =$  0700 8560 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 6621 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 140 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 135.23 ft\*  $q_2 = Q_2/W_2 =$  49 ft<sup>2</sup>/s

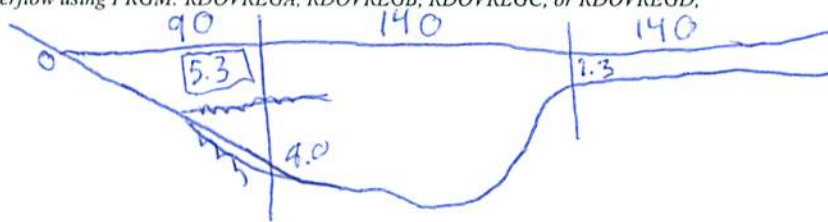
Bridge Vel,  $V_2 =$  3.4 ft/s Final  $y_2 = q_2/V_2 =$  14.2 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  14.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.1 ft  
 Low Steel Elev. = 14.2 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  140 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  140 ft Average left overbank flow depth,  $y_{lob} =$  5.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  140 ft Average right overbank flow depth,  $y_{rob} =$  1.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.47 From Figure 9  $W_2$  (effective) = 131.2 ft  $y_{cs} =$  4.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.16 Using pier width  $a$  on Figure 11,  $\xi =$  88 Pier scour  $y_{ps} =$  6.1 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.3 ft right abutment,  $y_{aRT} =$  1.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.6 and  $\psi_{RT} =$  5.5  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  15.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  5.5 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

45,24366

98,70226

450141 37.176"

980421 8.2"

Route 146 St Stream Snake Cr MRM \_\_\_\_\_ Date 7/19/12 Initials pat  
 Bridge Structure No. 0700 8480 Location 146 St, 6.6 mi W of Mansfield  
 GPS coordinates: N 45° 14' 57.3" taken from: USL abutment  centerline of fl MRM end \_\_\_\_\_  
W 98° 42' 9.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 319.36 sq. mi.  
 The average bottom of the main channel was 19.6 ft below top of guardrail at a point 104 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = Q <sub>50</sub> <u>5770</u>			Q <sub>500</sub> = Q <sub>100</sub> <u>8560</u>		
Estimated flow passing through bridge	<u>5770</u>			<u>6621</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1939</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/2  

2	169
5	802
10	1710
25	3650
50	5770
100	8560
500	18100

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *minor pier/contraction heavy abutment on left. unable to tell on right*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand ___	Gravel ___	Cobbles ___	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

1). left abutment  
 2). main channel  
 3). right abutment  
 4). pier  
 5). pier scour  
 6-7). ~~right~~ left abutment  
 8-9). ~~left~~ right abutment  
 (10-11). left abutment scour  
 12). main channel

Summary of Results

	Q <sub>100</sub> Q <sub>50</sub>	Q <sub>500</sub> Q <sub>100</sub>
Bridge flow evaluated	<u>5770</u>	<u>6621</u>
Flow depth at left abutment (yaLT), in feet	<u>4.7</u>	<u>5.3</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>1.3</u>
Contraction scour depth (yca), in feet	<u>3.1</u>	<u>4.1</u>
Pier scour depth (yps), in feet	<u>6</u>	<u>6.1</u>
Left abutment scour depth (yas), in feet	<u>14.5</u>	<u>15.6</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>5.5</u>
IFlow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required