

OK RJ

SCOUR ANALYSIS AND REPORTING FORM

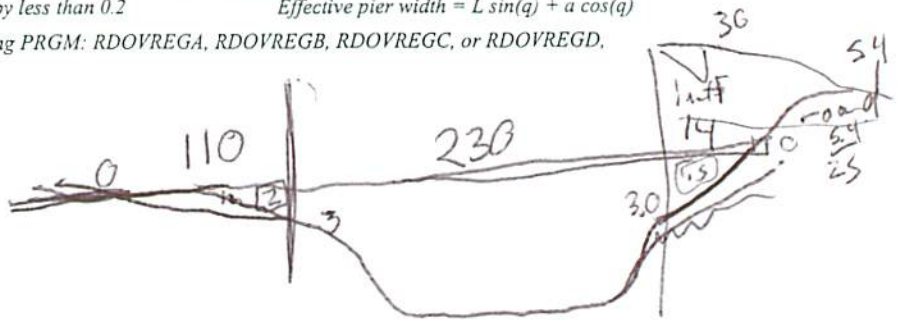
Bridge Structure No. 07088110 Date 7/22/12 Initials RAJ Region (A B C D)
Site Location ~1.1 mi W of Highway 281 on 11th St.
Q100 = Q10 3050 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = Q10 3050 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 163 ft. Flow angle at bridge = 95.6 degrees Abut. Skew = 0 degrees Effective Skew = 60 degrees
Width (W2) iteration =
Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 81.5 ft* q2 = Q2/W2 = 37.4 ft^2/s
Bridge Vel, V2 = 3 ft/s Final y2 = q2/V2 = 12.3 ft Delta h = 12.30.2 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 12.5 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2 ft 16.9
Low Steel Elev. = 15.2 ft 15.2
n (Channel) = 0.035 15.2
n (LOB) = 0.036
n (ROB) = 0.040
Pier Width = 1.3 ft
Pier Length = 31 ft
Piers for 100 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 230 ft
Width of left overbank flow at approach, Wlob = 110 ft Average left overbank flow depth, ylob = 3.62 ft
Width of right overbank flow at approach, Wrob = 14 ft Average right overbank flow depth, yrob = 1.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 25.44 From Figure 9 W2 (effective) = 77.6 ft ycs = 20.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s
Critical approach velocity, Vc = 1.17 y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 23.95 Correction factor for flow angle of attack (from Table 1), K2 = 4.6
Froude # at bridge = 0.15 Using pier width a on Figure 11, xi = 5.8 Pier scour yps = 20.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 2 ft right abutment, yarT = 1.5 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 8.2 and psiRT = 6.3
Left abutment scour, yas = psiLT (K1/0.55) = 8.2 ft Right abutment scour yas = psiRT (K1/0.55) = 6.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 07048110 Date 7/22/12 Initials Mal Region (A B C D) D
 Site _____ Location 1.1 mi W of Highway 281 on 11th St.
 $Q_{500} = Q_{25} = \underline{6830}$ by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 4536 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 163 ft. Flow angle at bridge = 60 ° Abut. Skew = 0 ° Effective Skew = 60 °
 Width (W_2) iteration = _____

Avg. flow depth at bridge, y_2 iteration = _____

Corrected channel width at bridge Section = W_2 times cos of flow angle = 81.5 ft* $q_2 = Q_2/W_2 = \underline{55.7}$ ft²/s

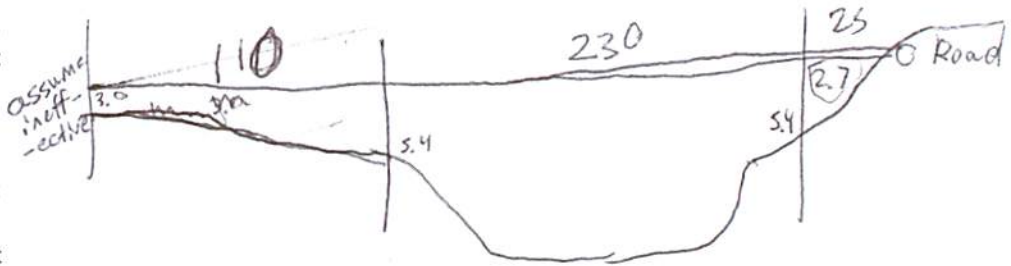
Bridge Vel, $V_2 = \underline{3.7}$ ft/s Final $y_2 = q_2/V_2 = \underline{15.2}$ ft $\Delta h = \underline{0.3}$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{15.5}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 2 ft
 Low Steel Elev. = 15.2 ft
 n (Channel) = 0.035
 n (LOB) = 0.035
 n (ROB) = 0.040
 Pier Width = 1.3 ft
 Pier Length = 31 ft
 # Piers for 500 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{230}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{110}$ ft Average left overbank flow depth, $y_{lob} = \underline{4.6}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{25}$ ft Average right overbank flow depth, $y_{rob} = \underline{2.7}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{40.02}$ From Figure 9 W_2 (effective) = ~~68.6~~ 77.6 ft $y_{cs} = \underline{28.5}$ ft 25
33.58

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{\quad}$ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 23.85 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{4.6}$
 Froude # at bridge = 0.17 Using pier width a on Figure 11, $\xi = \underline{5.8}$ Pier scour $y_{ps} = \underline{20.4}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{4.6}$ ft right abutment, $y_{aRT} = \underline{2.7}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{14.3}$ and $\psi_{RT} = \underline{11}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{14.3}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{11}$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

98.54327
45.77683
" 43.788
45046 46
98° 32' 35" 772

Route _____ Stream Elm River MRM _____ Date 7/23/12 Initials RAT

Bridge Structure No. 43.611 Location _____

GPS coordinates: N 45° 46' 47.3" W 96° 32' 30.0" taken from: USL abutment centerline of \uparrow MRM end _____
Datum of coordinates: WGS84 NAD27 _____

Drainage area = 996.5 sq. mi. 18.9

The average bottom of the main channel was 18.9 ft below top of guardrail at a point 11.61 ft from left abutment.

Method used to determine flood flows: _____ Freq. Anal. _____ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = Q ₁₀ <u>3050</u>			Q ₅₀₀ = Q ₂₅ <u>6830</u>		
Estimated flow passing through bridge	<u>3050</u>			<u>4536</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>2294</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/17

2	259
5	1370
10	3050
25	6830
50	11100
100	16800
500	36900

Riprap at abutments? _____ Yes _____ No Marginal left abutment 100% covered by riprap. Right abutment - marginal.
 Evidence of past Scour? Yes _____ No _____ Don't know some abutment contraction
 Debris Potential? _____ High _____ Med Low

Does scour countermeasure(s) appear to have been designed?
 Riprap _____ Yes No _____ Don't know _____ NA
 Spur Dike _____ Yes No _____ Don't know _____ NA
 Other _____ Yes No _____ Don't know _____ NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
 1) left ab. 11) main channel
 2) main channel
 3) right ab.
 4) pier
 6) right abutment
 7-9) left abutment
 10) right abutment
 Notes: overbank profile taken w/ 217 ft from center of bridge

Summary of Results

	Q ₁₀₀ Q ₁₀	Q ₅₀₀ Q ₂₅
Bridge flow evaluated	<u>3050</u>	<u>4536</u>
Flow depth at left abutment (yaLT), in feet	<u>2</u>	<u>4.6</u>
Flow depth at right abutment (yaRT), in feet	<u>1.5</u>	<u>2.7</u>
Contraction scour depth (y _{cs}), in feet	<u>20.6</u>	<u>28.5 25</u>
Pier scour depth (y _{ps}), in feet	<u>20.1</u>	<u>20.4</u>
Left abutment scour depth (y _{as}), in feet	<u>8.2</u>	<u>14.3</u>
Right abutment scour depth (y _{as}), in feet	<u>6.3</u>	<u>11</u>
Flow angle of attack	<u>60</u>	<u>60</u>

See Comments/Diagram for justification where required