

OK TET

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 07120230 Date 7/23/12 Initials RAT Region (A B C D) D
 Site from Westport, 3S, 1E, Elm River
 $Q_{100} = \underline{0.517100} \times 12700$ by: drainage area ratio max flood freq. anal. regional regression eq. X
 Bridge discharge (Q_2) = 12700 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 241 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °

Width (W_2) iteration = 237.34 221.29 235 23.13

Avg. flow depth at bridge, y_2 iteration = 19.49 15.4 15.3

Corrected channel width at bridge Section = W_2 times cos of flow angle = 231.43 ft* $q_2 = Q_2/W_2 = \underline{54.9}$ ft²/s

Bridge Vel, $V_2 = \underline{3.6}$ ft/s Final $y_2 = q_2/V_2 = \underline{15.1}$ ft $\Delta h = \underline{0.3}$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{15.3}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0.9-3.2 ft
 Low Steel Elev. = 19.6 ft

n (Channel) = 0.035

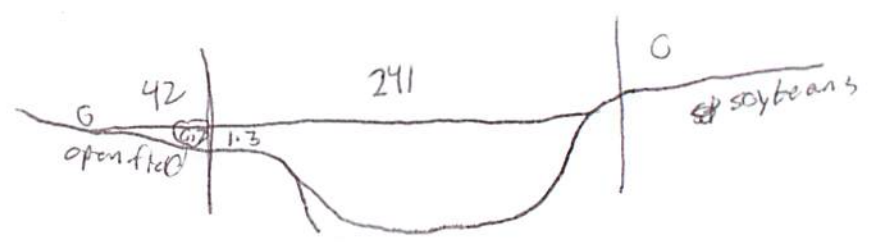
n (LOB) = 0.04

n (ROB) = 0.035

Pier Width = 2.0 ft

Pier Length = 2.0 ft

Piers for 100 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{241}$ ft

Width of left overbank flow at approach, $W_{lob} = \underline{42}$ ft

Width of right overbank flow at approach, $W_{rob} = \underline{0}$ ft

Average left overbank flow depth, $y_{lob} = \underline{0.7}$ ft

Average right overbank flow depth, $y_{rob} = \underline{0}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{1.07}$ From Figure 9 W_2 (effective) = 225.4 ft $y_{cs} = \underline{1.5}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \underline{\quad}$ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1

Froude # at bridge = 0.16

Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$

Using pier width a on Figure 11, $\xi = \underline{8}$ Pier scour $y_{ps} = \underline{6.1}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{0.7}$ ft right abutment, $y_{aRT} = \underline{0}$ ft

Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{3.1}$ and $\psi_{RT} = \underline{0}$

Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) = \underline{3.1}$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) = \underline{0}$ ft

SCOUR ANALYSIS AND REPORTING FORM

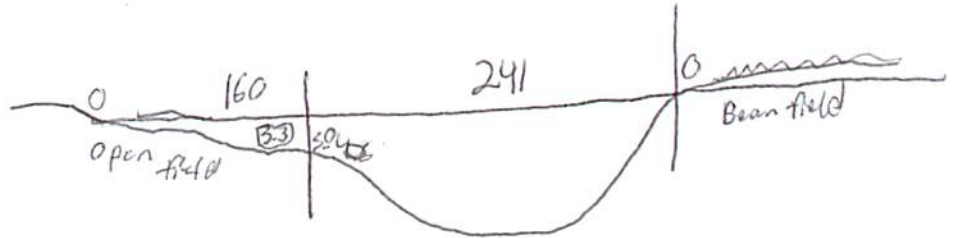
Bridge Structure No. 07120230 Date 7/23/12 Initials Dnt Region (A B C D) D
 Site 19400 Location from Westport, 3S, 1E
 $Q_{500} = \cancel{0.023000}$ by: drainage area ratio flood freq. anal. regional regression eq.
 Bridge discharge (Q_2) = 19330 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 241 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 237.31 ft* $q_2 = Q_2/W_2 = \underline{81.4}$ ft²/s
 Bridge Vel, $V_2 = \underline{4.4}$ ft/s Final $y_2 = q_2/V_2 = \underline{18.6}$ ft $\Delta h = \underline{0.4}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{19}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0.9-3.2 ft
 Low Steel Elev. = 19.2 ft
 n (Channel) = 0.035
 n (LOB) = 0.040
 n (ROB) = 0.035
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 500 yr = 3



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{241}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{160}$ ft Average left overbank flow depth, $y_{lob} = \underline{3.3}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{0}$ ft Average right overbank flow depth, $y_{rob} = \underline{0}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \underline{1.42}$ From Figure 9 W_2 (effective) = 231.3 ft $y_{cs} = \underline{1.9}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{\quad}$ ft/s
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$
 Froude # at bridge = 0.19 Using pier width a on Figure 11, $\xi = \underline{8}$ Pier scour $y_{ps} = \underline{6.2}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{3.3}$ ft right abutment, $y_{aRT} = \underline{0}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{12}$ and $\psi_{RT} = \underline{0}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{12}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{0}$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

450 36' 12.1741'
490 28' 39.2521'

45,609.49
46,477.51

STATE
E
COUNTY

PLACE

Route 123 St Stream Elm River MRM _____ Date 7/23/12 Initials Dat
 Bridge Structure No. 07120230 Location from Westport, 3S, 1E
 GPS coordinates: N 49° 36' 16.2" taken from: USL abutment centerline of ↑ MRM end _____
W 98° 29' 39.3" Datum of coordinates: WGS84 X NAD27 _____

Drainage area = 1236.86 sq. mi. 1217.55
 The average bottom of the main channel was 23.7 ft below top of guardrail at a point 131 ft from left abutment.
 Method used to determine flood flows: Freq. Anal. X drainage area ratio X regional regression equations.

MISCELLANEOUS CONSIDERATIONS Q₁₀₀

Flows	Q ₁₀₀ = 6500 <u>12700</u>			Q ₅₀₀ = 23200 <u>19400</u>		
Estimated flow passing through bridge				19330		
Estimated road overflow & overtopping				70		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		X				X
Chance of Pressure flow		X		X		
Armored appearance to channel		X			X	
Lateral instability of channel		X			X	

7/2
 2 | 290
 5 | 1550
 10 | 3470
 25 | 7820
 50 | 12700
 100 | 19400
 500 | 43000

Riprap at abutments? Yes X No Marginal
 Evidence of past Scour? X Yes No Don't know *minor pier/contraction and some abutment mostly right side.*
 Debris Potential? High Med X Low

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes X No Don't know NA
 Spur Dike Yes X No Don't know NA
 Other Yes X No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material	Silt/Clay <u>X</u>	Sand <u> </u>	Gravel <u> </u>	Cobbles <u> </u>	Boulders <u> </u>
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos
 1). left ab
 2). main channel
 3). right ab
 4). to pier
 5). pier scour
 6). left ab
 6-8). left abutment
 9-11). right abutment
 12). main channel

Summary of Results

Bridge flow evaluated	Q ₁₀₀	Q ₅₀	Q ₅₀₀	Q ₁₀₀
Flow depth at left abutment (yaLT), in feet	12700		19330	
Flow depth at right abutment (yaRT), in feet	0.7		3.3	
Contraction scour depth (yca), in feet	0		0	
Abutment scour depth (yab), in feet	1.5		1.9	
Right abutment scour depth (yas), in feet	6.1		6.2	
Left abutment scour depth (yas), in feet	3.1		12	
Flow angle of attack	0		0	
	10		10	

See Comments/Diagram for justification where required