

DUP ok-RAT

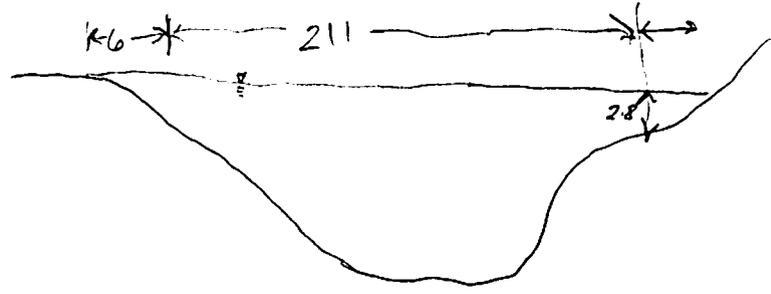
**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 07200234 Date 10-10-12 Initials RFT Region (A B C D)  
 Site \_\_\_\_\_ Location 12340 396<sup>th</sup> Ave (near Columbia), Elm River  
 $Q_{100} =$  13200 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 13200 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 211 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 211 177 182 180  
 Avg. flow depth at bridge,  $y_2$  iteration = 16.2 17.8 17.5 17.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 180 ft\*  $q_2 = Q_2/W_2 =$  73.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.2 ft/s Final  $y_2 = q_2/V_2 =$  17.6 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  17.9 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.1 ft  
 Low Steel Elev. = 19.3 @ TARE  
 $n$  (Channel) = .035  
 $n$  (LOB) = .035  
 $n$  (ROB) = .045  
 Pier Width = 2.2 ft  
 Pier Length = 2.33 ft  
 # Piers for 100 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  211 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  6 ft Average left overbank flow depth,  $y_{lob} =$  0.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  15 ft Average right overbank flow depth,  $y_{rob} =$  1.4 ft  
**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)  
 $x =$  3.63 From Figure 9  $W_2$  (effective) = 175.6 ft  $y_{cs} =$  4.2 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{0.7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.06 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.18 Using pier width  $a$  on Figure 11,  $\xi =$  8.6 Pier scour  $y_{ps} =$  6.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.3 ft right abutment,  $y_{aRT} =$  1.4 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  1.4 and  $\psi_{RT} =$  5.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  1.4 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  5.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PRGM: Contract  
 PRGM: CWCSNEW  
 PRGM: Pier  
 PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 07200234 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region ( A B C D )  
 Site \_\_\_\_\_ Location \_\_\_\_\_  
 $Q_{300}^{100} =$  20100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 20100 (should be  $Q_{300}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

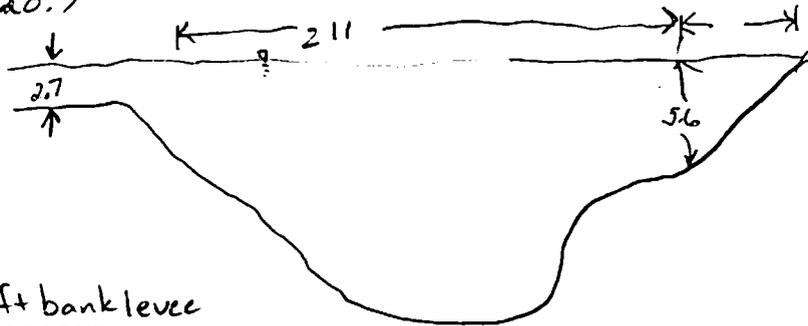
Bridge Width = 211 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 211  
 Avg. flow depth at bridge,  $y_2$  iteration = 20.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 211 ft\*  $q_2 = Q_2/W_2 =$  95.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.7 ft/s Final  $y_2 = q_2/V_2 =$  20.2 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  20.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

*road overflow will begin at  $y_2 \approx 20.7$*

Water Surface Elev. = 2.1 ft  
 Low Steel Elev. = 19.3 ft @ *top*  
 $n$  (Channel) = .035  
 $n$  (LOB) = .035  
 $n$  (ROB) = .045  
 Pier Width = 2.2 ft  
 Pier Length = 2.33 ft  
 # Piers for 500 yr = 2



*assume ineffective flow behind left bank levee*  
**CONTRACTION SCOUR**

PGRM: Contract

Width of main channel at approach section  $W_1 =$  211 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  18 ft Average left overbank flow depth,  $y_{lob} =$  2.7 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  30 ft Average right overbank flow depth,  $y_{rob} =$  2.8 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  0.58 From Figure 9  $W_2$  (effective) = 206.6 ft  $y_{cs} =$  1 ft

PGRM: CWCSNEW

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{300}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PGRM: Pie

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.06 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.18 Using pier width  $a$  on Figure 11,  $\xi =$  8.6 Pier scour  $y_{ps} =$  6.7 ft

PGRM: Abutment

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.7 ft right abutment,  $y_{aRT} =$  2.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11 and  $\psi_{RT} =$  11.2  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  11 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  11.2 ft

Route 396 Ave Stream Elm River MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_

Bridge Structure No. 07200234 Location \_\_\_\_\_

GPS coordinates: N 45° 35.927' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 98° 18.665' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1253.07 sq. mi.

The average bottom of the main channel was 24.6 ft below top of guardrail at a point 79 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	$Q_{50} = 13200$			$Q_{100} = 20100$		
Estimated flow passing through bridge	13200			20100		
Estimated road overflow & overtopping	0			0		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal

Evidence of past Scour? \_\_\_ Yes \_\_\_ No  Don't know possible contraction / pier scour

Debris Potential?  High \_\_\_ Med \_\_\_ Low debris jam on left side pier

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size ( $D_{50}$ )**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

str. no.  
 approach from bridge  
 LOB / levee from road  
 ROB from road  
 left abut. and debris jam

right abut from left  
 bridge section from left approach

**Summary of Results**

	$Q_{50}$	$Q_{100}$
Bridge flow evaluated	13200	20100
Flow depth at left abutment (yaLT), in feet	0.3	2.7
Flow depth at right abutment (yaRT), in feet	1.4	2.8
Contraction scour depth (yCS), in feet	4.2	* 1
Pier scour depth (yPS), in feet	6.6	6.7
Left abutment scour depth (yAS), in feet	1.4	11.0
Right abutment scour depth (yAS), in feet	5.9	11.2
Flow angle of attack	0°	0°

See Comments/Diagram for justification where required

\* contraction scour decreased as flow increased because the increase in stage caused a relatively large increase in wetted width at the bridge. Equation "thinks" there is more room for flow then.