

OK TCT

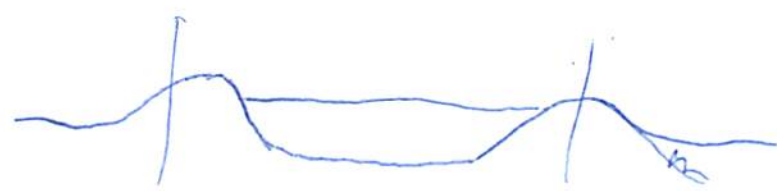
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 07241270 Date 7/20/12 Initials RAT Region (A B C D) D  
 Site \_\_\_\_\_ Location 1 mi E of Tacoma Park on 127 St  
 $Q_{100} = Q_2$  1120 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1120 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 78 ft. Flow angle at bridge = 15° Abut. Skew = 150° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = ~~78~~ 78 ft\*  $q_2 = Q_2/W_2 = \frac{1120}{78} = 14.4$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 21.9$  ft/s Final  $y_2 = q_2/V_2 = \frac{14.4}{21.9} = 0.66$  ft  $\Delta h = 0.1$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 7.5$  ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0.6-1.5 ft  
 Low Steel Elev. = ~~8.18-8.5~~ 8.2 ft  
 n (Channel) = 0.025  
 n (LOB) = 0.033  
 n (ROB) = 0.036  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 100 yr = 2



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 78$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 0.34$  From Figure 9  $W_2$  (effective) = 74.6 ft  $y_{cs} = 0.6$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.12 Using pier width a on Figure 11,  $\xi = 7$  Pier scour  $y_{ps} = 5.1$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 0$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

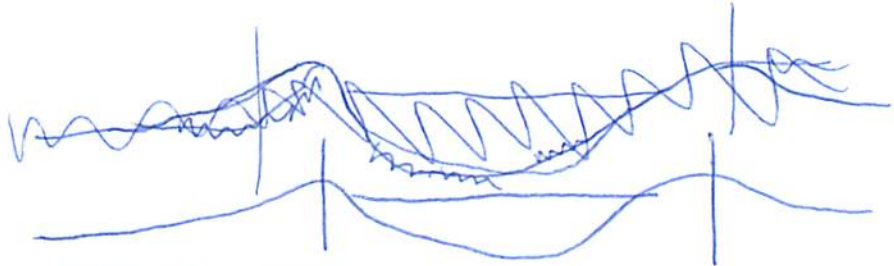
Bridge Structure No. 07241270 Date 7/20/12 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1 mi E of Tacoma St on 127 St  
 $Q_{500} =$  Q10 2250 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1356 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 78 ft. Flow angle at bridge = 18.15° Abut. Skew = 150° Effective Skew = 180°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 78 ft\*  $q_2 = Q_2/W_2 =$  17.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  2.1 ft/s Final  $y_2 = q_2/V_2 =$  8.2 ft  $\Delta h =$  0.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.615 ft  
 Low Steel Elev. = 8.2 ft  
 n (Channel) = 0.025  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 4.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  78 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  0.34 From Figure 9  $W_2$  (effective) = 74.6 ft  $y_{cs} =$  0.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.13 Using pier width a on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.2 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment



98° 13' 32.276"  
450 32' 42.864"  
45,54524  
98,22591

Route 127 St Stream Crow Ck Ditch MRM \_\_\_\_\_ Date 7/29/12 Initials RAT  
 Bridge Structure No. 07241270 Location 1 mi E of Tacoma Park on 127 St  
 GPS coordinates: N 45° 32' 43.11" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 98° 13' 33.31" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 997.62 sq. mi.  
 The average bottom of the main channel was 11.9 ft below top of guardrail at a point 35 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_5$ <u>1120</u>			$Q_{500} = Q_{10}$ <u>2280</u>		
Estimated flow passing through bridge	<u>1120</u>			<u>1356</u> <del>1356</del>		
Estimated road overflow & overtopping	<u>0</u>			<u>924</u> <del>924</del>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

7/2  
 2 271  
 5 1120  
 10 2280  
 25 4720  
 50 7360  
 100 10800  
 500 22700

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal *Only on right abutment*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *minor p/abutment/contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other no embankment along abutments.  Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )  
 Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left abt  
 2) main channel  
 3) right abt.  
 4) pier  
 5) pier scour  
 6-7) right abutment  
 8-9) left abutment  
 10) main channel

Summary of Results

	$Q_{100} Q_5$	$Q_{500} Q_{10}$
Bridge flow evaluated	<u>1120</u>	<u>1356</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (yca), in feet	<u>0.6</u>	<u>0.6</u>
Pier scour depth (yps), in feet	<u>5.1</u>	<u>5.2</u>
Left abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required