	SCOUR ANALYSIS AND REPORTING FORM
	Bridge Structure No. 10196342 Date 9-19-12 Initials RFT Region (ABCD) Site Location 2.2 m. Not HWY 212 on Arpan R4 But
	Site Location 2.2 m Not HWY 212 on Argan Rd - But Bu
	Qmax scool 7 7 Hothy: drainage area ratio flood freq. anal. regional regression eq.
	Bridge discharge $(Q_2) = 100000000000000000000000000000000000$
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method
PGRM: "RegionA", "RegionB "RegionC", or "RegionD"	Bridge Width = $\frac{6}{20}$ ft. Flow angle at bridge = $\frac{20}{20}$ Abut. Skew = $\frac{20}{20}$ ° Effective Skew = $\frac{6}{20}$ °
	Width (W_2) iteration = $\frac{U}{S}$ Avg. flow depth at bridge, y_2 iteration = $\frac{Q}{S}$
	Corrected channel width at bridge Section = W_2 times cos of flow angle = 43.9 ft* $q_2 = Q_2/W_2 = 43.3$ ft²/s
	Bridge Vel $V_2 = I_2 \cdot 7$ ft/s Final $V_2 = g_2/V_2 = g_3/V_3 = $
	Bridge Vel, $V_2 = 10.7$ ft/s Final $y_2 = q_2/V_2 = 9.5$ ft $\Delta h = 0$ ft $\Delta h = 0$ ft Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 9.5$ ft
	* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
	If y is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD, This is a bridge over an irrigation canal
	This is a bridge over an irrigation canal
	Water Surface Elev. = $\frac{3!1}{9!5}$ ft Low Steel Elev. = $\frac{3!5}{9!5}$ ft
	n (Channel) = 1)/() Smooth 1
	$n \text{ (LOB)} = \frac{300}{0.000}$ $n \text{ (ROB)} = \frac{300}{0.000}$
	"(KOD)
	Pier Width = $\frac{\sqrt{A}}{\text{Pier Length}} = \frac{\sqrt{A}}{\sqrt{A}} = \text{ft}$
	# Piers for $100 \text{ yr} = D$ ft
	CONTRACTION SCOUR
PGRM: Contract	Width of main channel at approach section $W_1 = \mathcal{L} \mathcal{S}$ ft
	Width of left overbank flow at approach, $W_{lob} = 0$ ft Average left overbank flow depth, $y_{lob} = 0$ ft
	Width of right overbank flow at approach, $W_{rob} = 0$ ft Average right overbank flow depth, $y_{rob} = 0$ ft
GRM	
P(Live Bed Contraction Scour (use if bed material is small cobbles or finer) V (offertive) = 1, 3, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,
	x =
PGRM: CWCSNEW	Clear Water Contraction Scour (use if bed material is larger than small cobbles)
	Estimated bed material $D_{50} = ft$ Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = ft/s$
CWC	Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3}$ ft/s
KM:	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
PG	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = $ ft
	Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =ft$
ь	
f: Pie	PIER SCOUR CALCULATIONS
PGRM: Pier	L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 = Froude # at bridge = Using pier width a on Figure 11, E = Pier scour y = ft
d.	Froude # at bridge =ft Using pier width a on Figure 11, ξ =ft
Ħ	ABUTMENT SCOUR CALCULATIONS
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 0$ ft right abutment, $y_{aRT} = 0$ ft
f: Ab	Shape coefficient K_1 = 1.00 for vertical-wall, Using values for y_{aLT} and y_{aRT} on figure 12, ψ_{LT} = 0.82 for vertical-wall with wingwalls, and ψ_{RT} = 0.55 for spill-through
GRN	
ď.	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = $ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = $ ft

Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ ____ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ ____ft

SCOUR ANALYSIS AND REPORTING FORM

Route Arpan Rd Stream South Ca	nal	MRM	Da	te	Init	tials		
Bridge Structure No. 1019/347 Loc	ration 2 2	m. N.	2 1/1/2	217 00	Acres	PI		
Bridge Structure No. 101 96342 Location 2,2 m; Not HWY 2/2 on Apan Rd GPS coordinates: N 410 43 080' taken from: USL abutment 1/2 centerline of fl MPM and								
1/ 1/3° 39 39/.	taken from: USL abutment centerline of \(\hat{1}\) MRM end \(\begin{align*} \text{MQ3}^6 & 39.384 \\ \text{MAD27} \\ \end{align*}							
	rainage area = * 1.64 / undefined sq. mi.							
	e average bottom of the main channel was 14.4 ft below top of guardrail at a point 31 ft from left abutment.							
Method used to determine flood flows:Freq.	Anal	drainage area	ratio	regional regi	ression equ	ations.		
MISCELLANEOUS CONSIDERATIONS								
Flows	Q+00=Qmax scar 4045 Q500=							
Estimated flow passing through bridge	4045							
Estimated road overflow & overtopping		D	T					
Consideration	Yes	No	Possibly	Yes	No	Possibly		
Chance of overtopping		×						
Chance of Pressure flow		X						
Armored appearance to channel		X						
Lateral instability of channel		X						
Riprap at abutments? Yes See notes on back regarding Comments, Diagrams & orientation of digital photos.	NoNedNesN Classification	Don't knovLow loDo loDo loDo n Based on M Gravel_X	n't know n't know n't know n't know edian Partic	NA NA NA le Size (D ₅₀)		Boulders>250		
2 33.1 Lused estimated 5 96.5 Qmox scour 25 275 50 379 100 501 500 874	str applef Ru (+ i=1)	oranch from the levee to B tabut.	mbridge From Lo	oridge				
Summary of Results bridge from approach								
		.Q100 Q	nax scor		Q500			
Bridge flow evaluated	4045				11			
Flow depth at left abutment (yaLT), in feet	0							
Flow depth at right abutment (yaRT), in feet		0						
Contraction scour depth (ycs), in feet		1.0						
Pier scour depth (yps), in feet		NA						
Left abutment scour depth (yas), in feet	O							
Right abutment scour depth (yas), in feet								
1Flow angle of attack		200/	O°eff)					

This bridge is over an irrigation canal and does not have a "natural" drainage area to compute peak flows. However, an area was estimated based on the amount of drainage area that might be intercepted if streams flowed into the canal instead of crossing it. Drainage area edited in streamstats on 8-1-12 and flows calculated based on estimated area.

103.65675