

SCOUR ANALYSIS AND REPORTING FORM

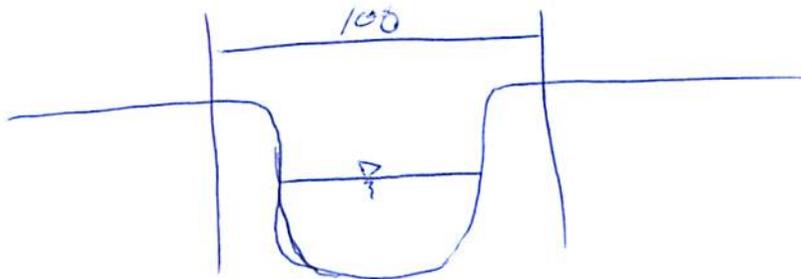
Bridge Structure No. 10262330 Date 10/28/11 Initials GW Region (A B C D) B  
 Site \_\_\_\_\_ Location ~4.7 mi E + 1 mi N of Jewell on Schmele Rd  
 $Q_{100} =$  10600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 10600 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 98 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 98 ~~73~~ 65 73 68 70  
 Avg. flow depth at bridge,  $y_2$  iteration = 12.6 ~~14.7~~ 15.7 14.7 15.3 15.1  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 69.73 ft\*  $q_2 = Q_2/W_2 =$  152 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  10.1 ft/s Final  $y_2 = q_2/V_2 =$  15.1 ft  $\Delta h =$  2.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  17.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 22.5 ft  
 n (Channel) = 0.035  
 n (LOB) = 0.033  
 n (ROB) = 0.033  
 Pier Width = 1.0 ft  
 Pier Length = 0.4/25 ft  
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  100 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  8.19 From Figure 9  $W_2$  (effective) = 67.7 ft  $y_{cs} =$  9.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = 25 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5  
 Froude # at bridge = 0.46 Using pier width a on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  6.5 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{alT} =$  0.0 ft right abutment,  $y_{arT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWC/NEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

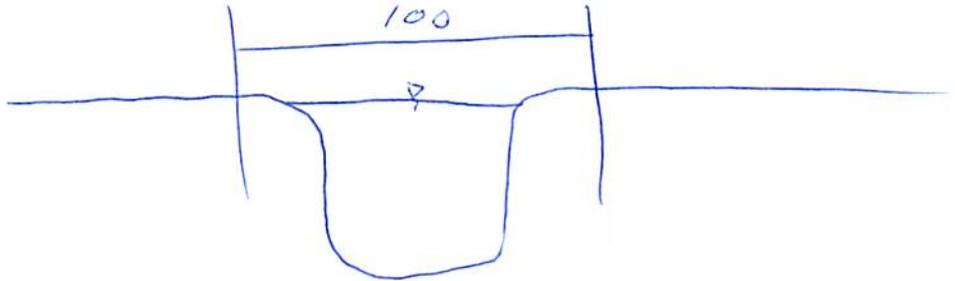
Bridge Structure No. 10262330 Date 10/28/11 Initials aw Region (A B C D) B  
 Site \_\_\_\_\_ Location ~4.7 mi W of 1 mi N of Newell on Schmele Rd  
 $Q_{500} =$  17500 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 17500 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 98 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 98 75 80 80  
 Avg. flow depth at bridge,  $y_2$  iteration = 16.4 18.9 18.3  
 Corrected channel width at bridge Section =  $W_2$  times  $\cos$  of flow angle = 79.7 ft\*  $q_2 = Q_2/W_2 =$  219.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  12.0 ft/s Final  $y_2 = q_2/V_2 =$  18.3 ft  $\Delta h =$  3.0 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  21.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 22.5 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.033  
 $n$  (ROB) = 0.033  
 Pier Width = 1 ft  
 Pier Length = 0.4/25 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  100 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  6.11 From Figure 9  $W_2$  (effective) = 77.7 ft  $y_{cs} =$  6.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 25  
 Froude # at bridge = 0.49

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.5  
 Using pier width  $a$  on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  6.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{alT} =$  0.0 ft right abutment,  $y_{arT} =$  0.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  0.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0.0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route Schmele Rd Stream Indian Ck MRM \_\_\_\_\_ Date 10/28/11 Initials CA  
 Bridge Structure No. 10262330 Location ~4.7 mi W 1 mi N of Newell on Schmele Rd  
 GPS coordinates: N 44° 44' 04.0" taken from: USL abutment  centerline of MRM end \_\_\_\_\_  
W 103° 31' 11.6" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 360.26 sq. mi.  
 The average bottom of the main channel was 27.4 ft below top of guardrail at a point 40 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>10600</u>			Q <sub>500</sub> = <u>17500</u>		
Estimated flow passing through bridge	<u>10600</u>			<u>17500</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know Degradation  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

10/4/11  
 2 713  
 5 2190  
 10 3780  
 25 6040  
 50 8200  
 100 10600  
 500 17500

\* Channel is extremely incised

Photos  
 2146 - ID  
 47 - Sign on bridge  
 44 - US  
 49 - US RB  
 50 - US LB

51 - L. Abut  
 52 - R. Abut  
 53 - Pier Config  
 54 - Piers  
 55 - Piers

56 - US Face  
 57 - LB App XS  
 58 - RB App XS  
 59 - Debris on bridge

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>10600</u>	<u>17500</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>0.0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>0.0</u>
Contraction scour depth (yca), in feet	<u>9.1</u>	<u>6.9</u>
Pier scour depth (yps), in feet	<u>6.5</u>	<u>6.6</u>
Left abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>0.0</u>
Flow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required