

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 12216030 Date 6/11/12 Initials Rat Region (A B C D) C
Site Location 4.4 mi N + 1.4 mi W of Platte on 271 St
Q100 = q1e 1060 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 67 ft. Flow angle at bridge = 15 degrees Abut. Skew = 0 degrees Effective Skew = 15 degrees
Width (W2) iteration =

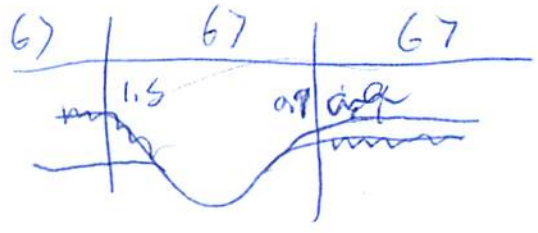
Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 64.72 ft\* q2 = Q2/W2 = 16.4 ft^2/s

Bridge Vel, V2 = 2.9 ft/s Final y2 = q2/V2 = 5.7 ft Delta h = 0.2 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 5.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(a) + a cos(a)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.2 ft
Low Steel Elev. = 6.9 ft
n (Channel) = 0.015
n (LOB) = 0.030
n (ROB) = 0.030
Pier Width = 1.35 ft
Pier Length = 1.35 ft
# Piers for 100 yr = 3



CONTRACTION SCOUR

Width of main channel at approach section W1 = 67 ft
Width of left overbank flow at approach, Wlob = 67 ft Average left overbank flow depth, ylob = 1.5 ft
Width of right overbank flow at approach, Wrob = 67 ft Average right overbank flow depth, yrob = 0.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 2.04 From Figure 9 W2 (effective) = 60.7 ft ycs = 2.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.21 Using pier width a on Figure 11, xi = 6 Pier scour yps = 4.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 1.5 ft right abutment, yaRT = 0.9 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 6.3 and psiRT = 3.9
Left abutment scour, yas = psiLT(K1/0.55) = 6.3 ft Right abutment scour yas = psiRT(K1/0.55) = 3.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 12216030 Date 6/11/12 Initials fat Region (A B C D)  
 Site \_\_\_\_\_ Location 4.4 mi N + 1.4 mi W of Platte  
 $Q_{500} =$  Q<sub>25</sub> 2150 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1502 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 67 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

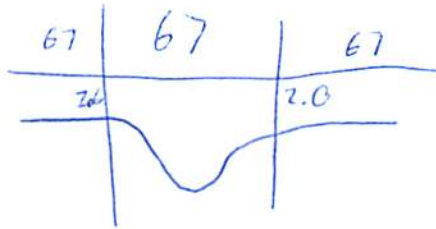
Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 64.72 ft\*  $q_2 = Q_2/W_2 =$  23.2 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.4 ft/s Final  $y_2 = q_2/V_2 =$  6.8 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 627.8 ft  
 Low Steel Elev. = 6.9 ft  
 n (Channel) = 0.045  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 500 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  67 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  67 ft Average left overbank flow depth,  $y_{lob} =$  2.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  67 ft Average right overbank flow depth,  $y_{rob} =$  2.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  4.39 From Figure 9  $W_2$  (effective) = 60.7 ft  $y_{cs} =$  5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.23 Using pier width a on Figure 11,  $\xi =$  6 Pier scour  $y_{ps} =$  4.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.6 ft right abutment,  $y_{aRT} =$  2.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  10.6 and  $\psi_{RT} =$  8.2  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  10.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  8.7 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment



pass  
bottom  
right

96.67251  
43.45658  
p 67

98° 52' 21.44"  
43° 27' 23.658"

Route 271 St Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 6/11/12 Initials Rat  
 Bridge Structure No. 12216030 Location 4.4 mi N + 1.4 mi W of Platte  
 GPS coordinates: N 130° 27' 24.0" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 98° 52' 21.3" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 110.9 sq. mi.

The average bottom of the main channel was 10.6 ft below top of guardrail at a point 22 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS *Q25*

Flows	$Q_{100} = Q_{10}$ <u>1060</u>			$Q_{500} =$ <u>2490</u>		
Estimated flow passing through bridge	<u>1060</u>			<u>1502</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>679</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/4  
8/23  
 2 125126  
 5 526  
 10 1060  
 25 2180  
 50 3360  
 100 4900  
 500 10100

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

*along left abutment (channel is about 4ft wide flowing directly into left abutment)*  
*pier contraction abutment*

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

*rose quartz on left abutment*

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand ___	Gravel ___	Cobbles ___	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

- 1. left ab
- 2. main channel
- 3. right ab
- 4-5) left abutment
- 6-7) right abutment
- 8-14) piers

- 15) Bridge entrance
- 16) main channel

Summary of Results

	$Q_{100}$ $Q_{10}$	$Q_{500}$ $Q_{25}$
Bridge flow evaluated	<u>1060</u>	<u>1502</u>
Flow depth at left abutment (yaLT), in feet	<u>1.5</u>	<u>2.6</u>
Flow depth at right abutment (yaRT), in feet	<u>0.9</u>	<u>2.0</u>
Contraction scour depth (yca), in feet	<u>2.6</u>	<u>5</u>
Pier scour depth (yca), in feet	<del>4.7</del> <u>4.7</u>	<u>4.8</u>
Left abutment scour depth (yca), in feet	<u>6.3</u>	<u>10.6</u>
Right abutment scour depth (yca), in feet	<u>3.9</u>	<u>8.2</u>
IFlow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required