

OK RT

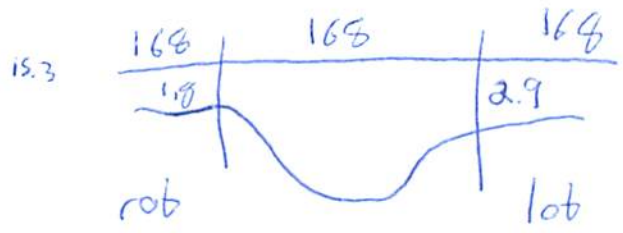
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 12560321 Date 6/10/12 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location in Dante on 400 Ave  
 $Q_{100} =$  5440 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5440 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 169 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 152.26 ft\*  $q_2 = Q_2/W_2 =$  35.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.2 ft/s Final  $y_2 = q_2/V_2 =$  8.4 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.8 ft  
 \* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 11.0 ft  
 Low Steel Elev. = 10.3 ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.060  
 $n$  (ROB) = 0.035  
 Pier Width = 2.1 ft  
 Pier Length = 2.25 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  168 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  1.8 ft Average left overbank flow depth,  $y_{lob} =$  2.9 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  2.9 ft Average right overbank flow depth,  $y_{rob} =$  1.8 ft  
 Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.51 From Figure 9  $W_2$  (effective) = 148.1 ft  $y_{cs} =$  4.1 ft

~~Clear Water Contraction Scour (use if bed material is larger than small cobbles)~~  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.07 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.02  
 Froude # at bridge = 0.26 Using pier width  $a$  on Figure 11,  $\xi =$  8.3 Pier scour  $y_{ps} =$  6.9 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.9 ft right abutment,  $y_{aRT} =$  1.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.3 and  $\psi_{RT} =$  7.4  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  11.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  7.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 12560321 Date 6/10/12 Initials kat Region (A B C D)  
 Site \_\_\_\_\_ Location in Dante on 400 Ave  
 $Q_{500} =$  4670 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 8115 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 168 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 24 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 152.26 ft\*  $q_2 = Q_2/W_2 =$  53.3 ft<sup>2</sup>/s

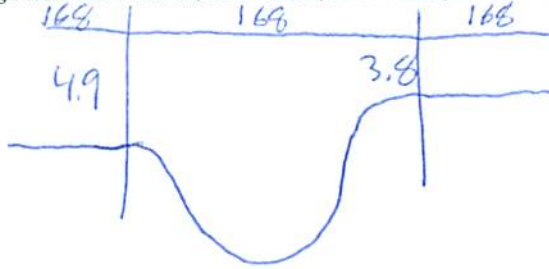
Bridge Vel,  $V_2 =$  5.2 ft/s Final  $y_2 = q_2/V_2 =$  10.3 ft  $\Delta h =$  0.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-10 ft  
 Low Steel Elev. = 10.3 ft  
 $n$  (Channel) = 0.050  
 $n$  (LOB) = 0.060  
 $n$  (ROB) = 0.035  
 Pier Width = 2.1 ft  
 Pier Length = 2.25 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  168 ft

Width of left overbank flow at approach,  $W_{lob} =$  168 ft Average left overbank flow depth,  $y_{lob} =$  4.9 ft

Width of right overbank flow at approach,  $W_{rob} =$  168 ft Average right overbank flow depth,  $y_{rob} =$  3.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  7.26 From Figure 9  $W_2$  (effective) = 148.1 ft  $y_{cs} =$  9.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{1/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.07

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.02

Froude # at bridge = 0.29

Using pier width  $a$  on Figure 11,  $\xi =$  9.3 Pier scour  $y_{ps} =$  17 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.9 ft right abutment,  $y_{aRT} =$  3.8 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  14.8 and  $\psi_{RT} =$  12.9

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  14.8 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  12.9 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

43.03746  
98.18744



Route 400 Ave Stream Choteau Ck MRM \_\_\_\_\_ Date 6/10/12 Initials Lat  
 Bridge Structure No. 12560321 Location in Dante on 400 Ave  
 GPS coordinates: N 43° 02' 14.9'' taken from: USL abutment  centerline of fl MRM end \_\_\_\_\_  
W 98° 11' 14.9'' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 478.69 sq. mi.

The average bottom of the main channel was 15.3 ft below top of guardrail at a point 96 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>Q<sub>75</sub> 5440</u>			Q <sub>500</sub> = <u>Q<sub>50</sub> 8670</u>		
Estimated flow passing through bridge	<u>5440</u>			<u>8115</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>555</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/4  
8/23  
2 256  
5 1190  
10 2520  
25 5440  
50 8670  
100 13000  
500 28400  
WGAH

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *abutment pier contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) right ab
- 2) main channel
- 3) left ab
- 4) piers
- 5) right of abutment
- 6-8) left abutment (scour)
- 9) right abutment scour
- 10) main channel

Summary of Results

	Q <sub>100</sub> <u>Q<sub>75</sub></u>	Q <sub>500</sub> <u>Q<sub>50</sub></u>
Bridge flow evaluated	<u>5440</u>	<u>8115</u>
Flow depth at left abutment (yaLT), in feet	<u>2.7</u>	<u>4.9</u>
Flow depth at right abutment (yaRT), in feet	<u>1.8</u>	<u>3.8</u>
Contraction scour depth (yca), in feet	<u>4.1</u>	<u>8.1</u>
Pier scour depth (yps), in feet	<u>6.9</u>	<u>7</u>
Left abutment scour depth (yas), in feet	<u>11.3</u>	<u>4.7</u> <u>14.8</u>
Right abutment scour depth (yas), in feet	<u>7.7</u>	<u>3.8</u> <u>12.9</u>
IFlow angle of attack	<u>25</u>	<u>25</u>

See Comments/Diagram for justification where required